## ATTACHMENT B

Suggested Changes to Technical Specifications of CoC 1004 Amendment No. 7

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### 1.0 INTRODUCTION

This section presents the conditions which a potential user (general licensee) of the standardized NUHOMS<sup>®</sup> system must comply with, in order to use the system under the general license in accordance with the provisions of 10 CFR 72.210 and 10 CFR 72.212. These conditions have either been proposed by the system vendor, imposed by the NRC staff as a result of the review of the FSAR, or are part of the regulatory requirements expressed in 10 CFR 72.212.

### 1.1 General Requirements and Conditions

1.1.1 Regulatory Requirements for a General License

Subpart K of 10 CFR Part 72 contains conditions for using the general license to store spent fuel at an independent spent fuel storage installation at power reactor sites authorized to possess and operate nuclear power reactors under 10 CFR Part 50. Technical regulatory requirements for the licensee (user of the standardized NUHOMS<sup>®</sup> system) are contained in 10 CFR 72.212(b).

Under 10 CFR 72.212(b)(2) requirements, the licensee must perform written evaluations, before use, that establish that: (1) conditions set forth in the Certificate of Compliance have been met; (2) cask storage pads and areas have been designed to adequately support the static load of the stored casks; and (3) the requirements of 10 CFR 72.104 "Criteria for radioactive materials in effluent and direct radiation from an ISFSI or MRS," have been met. In addition, 10 CFR 72.212(b)(3) requires that the licensee review the FSAR and the associated SER, before use of the general license, to determine whether or not the reactor site parameters (including earthquake intensity and tornado missiles), are encompassed by the cask design bases considered in these reports.

The requirements of 10 CFR 72.212(b)(4) provide that, as a holder of a Part 50 license, the user, before use of the general license under Part 72, must determine whether activities related to storage of spent fuel involve any unreviewed safety issues, or changes in technical specifications as provided under 10 CFR 50.59. Under 10 CFR 72.212(b)(5), the general license holder shall also protect the spent fuel against design basis threats and radiological sabotage pursuant to 10 CFR 73.55. Other general license requirements dealing with review of reactor emergency plans, quality assurance program, training, and radiation protection program must also be satisfied pursuant to 10 CFR 72.212(b)(6). Records and procedural requirements for the general license holder are described in 10 CFR 72.212(b)(7), (8), (9) and (10).

Without limiting the requirements identified above, site-specific parameters and analyses, identified in the SER, that will need verification by the system user, are as a minimum, as follows:

- 1. The temperature of 70°F as the maximum average yearly temperature with solar incidence. The average daily ambient temperature shall be 100°F or less.
- The temperature extremes either of 125°F with incident solar radiation (for the 24P, 52B, and 61BT DSCs) or 117°F with solar incidence (for the 32PT, 24PHB, and 24PTH DSCs) and -40°F with no solar incidence for storage of the DSC inside the HSM. The 117°F extreme ambient temperature corresponds to a 24 hour calculated average temperature of 102°F.

- 3. The horizontal and vertical seismic acceleration levels of 0.25g and 0.17g, respectively.
- 4. The analyzed flood condition of 15 fps water velocity and a height of 50 feet of water (full submergence of the loaded HSM DSC).
- 5. The potential for fire and explosion should be addressed, based on site-specific considerations.
- 6. The HSM foundation design criteria are not included in the FSAR. Therefore, the nominal FSAR design or an alternative should be verified for individual sites in accordance with 10 CFR 72.212(b)(2)(ii). Also, in accordance with 10 CFR 72.212(b)(3), the foundation design should be evaluated against actual site parameters to determine whether its failure would cause the standardized NUHOMS<sup>®</sup> system to exceed the design basis accident conditions.
- 7. The potential for lightning damage to any electrical system associated with the standardized NUHOMS<sup>®</sup> system (e.g., thermal performance monitoring) should be addressed, based on site-specific considerations.
- 8. Any other site parameters or consideration that could decrease the effectiveness of cask systems important to safety.

In accordance with 10 CFR 72.212(b)(2), a record of the written evaluations must be retained by the licensee until spent fuel is no longer stored under the general license issued under 10 CFR 72.210.

### 1.1.2 Operating Procedures

Written operating procedures shall be prepared for cask handling, loading, movement, surveillance, and maintenance. The operating procedures suggested generically in the FSAR should provide the basis for the user's written operating procedure. The following additional procedure requested by NRC staff should be part of the user operating procedures:

If fuel needs to be removed from the DSC, either at the end of service life or for inspection after an accident, precautions must be taken against the potential for the presence of damaged or oxidized fuel and to prevent radiological exposure to personnel during this operation. This can be achieved with this design by the use of the purge and fill valves which permit a determination of the atmosphere within the DSC before the removal of the inner top cover and shield plugs, prior to filling the DSC cavity with water (borated water for the 24P or 32PT or 24PHB or 24PTH). If the atmosphere within the DSC is helium, then operations should proceed normally with fuel removal either via the transfer cask or in the pool. However, if air is present within the DSC, then appropriate filters should be in place to preclude the uncontrolled release of any potential airborne radioactive particulate from the DSC via the purge-fill valves. This will protect both personnel and the operations area from potential contamination. For the accident case, personnel protection in the form of respirators or supplied air should be considered in accordance with the licensee's Radiation Protection Program.

### 1.1.3 Quality Assurance

Activities at the ISFSI shall be conducted in accordance with a Commission-approved quality assurance program which satisfies the applicable requirements of 10 CFR Part 50, Appendix B, and which is established, maintained, and executed with regard to the ISFSI.

### 1.1.4 Heavy Loads Requirements

Lifts of the DSC in the TC must be made within the existing heavy loads requirements and procedures of the licensed nuclear power plant. The TC design has been reviewed under 10 CFR Part 72 and found to meet NUREG-0612 and ANSI N14.6. However, an additional safety review (under 10 CFR 50.59) is required to show operational compliance with NUREG-0612 and/or existing plant-specific heavy loads requirements.

### 1.1.5 Training Module

A training module shall be developed for the existing licensee's training program establishing an ISFSI training and certification program. This module shall include the following:

- 1. Standardized NUHOMS<sup>®</sup> Design (overview);
- 2. ISFSI Facility Design (overview);
- 3. Certificate of Compliance conditions (overview);
- 4. Fuel Loading, Transfer Cask Handling, DSC Transfer Procedures; and
- 5. Off-Normal Event Procedures.

### 1.1.6 Pre-Operational Testing and Training Exercise

A dry run of the DSC loading, TC handling and DSC insertion into the HSM shall be held. This dry run shall include, but not be limited to, the following:

- 1. Functional testing of the TC with lifting yokes to ensure that the TC can be safely transported over the entire route required for fuel loading, washdown pit (decontamination area) and trailer loading.
- 2. DSC loading into the TC to verify fit and TC/DSC annulus seal.
- 3. Testing of TC on transport trailer and transported to ISFSI along a predetermined route and aligned with an HSM.
- 4. Testing of transfer trailer alignment and docking equipment. Testing of hydraulic ram to insert a DSC loaded with test weights into an HSM and then retrieve it.
- 5. Loading a mock-up fuel assembly into the DSC.
- 6. DSC sealing, vacuum drying, and cover gas backfilling operations (using a mock-up DSC).
- 7. Opening a DSC (using a mock-up DSC).
- 8. Returning the DSC and TC to the spent fuel pool.
- 1.1.7 Special Requirements for First System in Place

The heat transfer characteristics of the cask system will be recorded by temperature measurements of the first DSC placed in service. The first DSC shall be loaded with assemblies,

constituting a source of approximately 24 kW in HSM (approximately 40.8 kW in HSM-H). The DSC shall be loaded into the HSM, and the thermal performance will be assessed by measuring the air inlet and outlet temperatures for normal airflow. Details for obtaining the measurements are provided in Section 1.2.8, under "Surveillance."

A letter report summarizing the results of the measurements shall be submitted to the NRC for evaluation and assessment of the heat removal characteristics of the cask in place within 30 days of placing the DSC in service, in accordance with 10 CFR 72.4.

Should the first user of the system not have fuel capable of producing a 24 kW heat load (40.8 kW heat load for 24PTH DSC), or be limited to a lesser heat load, as in the case of BWR fuel, the user may use a lesser load for the process, provided that a calculation of the temperature difference between the inlet and outlet temperatures is performed, using the same methodology and inputs documented in the FSAR, with lesser load as the only exception. The calculation and the measured temperature data shall be reported to the NRC in accordance with 10 CFR 72.4. The calculation and comparison need not be reported to the NRC for DSCs that are subsequently loaded with lesser loads than the initial case. However, for the first or any other user, the process needs to be performed and reported for any higher heat sources, up to 24 kW for PWR fuel stored in the 24P TH-L; 19 kW for BWR fuel stored in the 52B and 18.3 kW for BWR fuel stored in the 61BT, which are the maximum allowed under the Certificate of Compliance for these specific DSCs. The NRC will also accept the use of artificial thermal loads other than spent fuel, to satisfy the above requirement.

#### 1.1.8 Surveillance Requirements Applicability

The specified frequency for each Surveillance Requirement is met if the surveillance is performed within 1.25 times the interval specified in the frequency, as measured from the previous performance.

For frequencies specified as "once," the above interval extension does not apply.

If a required action requires performance of a surveillance or its completion time requires period performance of "once per...," the above frequency extension applies to the repetitive portion, but not to the initial portion of the completion time.

Exceptions to these requirements are stated in the individual specifications.

1.1.9 Supplemental Shielding

Supplemental shielding and engineered features (e.g., earthen berms, shield walls) that are used to ensure compliance with 10 CFR 72.104(a) by each general licensee are to be considered important to safety and must be appropriately evaluated under 10 CFR 72.212(b).

### 1.1.10 HSM-H Storage Configuration

A minimum of two (2) HSM-Hs are required to be placed adjacent to each other for stability during design basis flood loads.

## 1.2 Technical Specifications, Functional and Operating Limits

## 1.2.1 Fuel Specifications

| Limit/Specification: | The characteristics of the spent fuel which is allowed to be stored in the standardized NUHOMS <sup>®</sup> system are limited by those included in Tables 1-1a, 1-1b, 1-1c, 1-1d, 1-1e, 1-1f, 1-1g, 1-1i, 1-1j, 1-1l, and 1-1m.  |  |  |  |  |
|----------------------|---|--|--|--|--|
| Applicability:       | The specification is applicable to all fuel to be stored in the standardized $\rm NUHOMS^{\circledast}$ system.   |  |  |  |  |
| Objective:           | The specification is prepared to ensure that the peak fuel rod cladding<br>temperatures, maximum surface doses, and nuclear criticality effective<br>neutron multiplication factor are below the design limits. Furthermore,<br>the fuel weight and type ensures that structural conditions in the FSAR<br>bound those of the actual fuel being stored.   |  |  |  |  |
| Action:              | Each spent fuel assembly to be loaded into a DSC shall have the parameters listed in Tables 1-1a, 1-1b, 1-1c, 1-1d, 1-1e, 1-1f, 1-1g, 1-1i, 1-1j, 1-11, and 1-1m verified and documented. Fuel not meeting this specification shall not be stored in the standardized NUHOMS <sup>®</sup> system.   |  |  |  |  |
| Surveillance:        | Prior to loading of a spent fuel assembly into a DSC, the identity of each fuel assembly shall be independently verified and documented.  |  |  |  |  |
| Bases:               | The specification is based on consideration of the design basis parameters included in the FSAR and limitations imposed as a result of the staff review. Such parameters stem from the type of fuel analyzed, structural limitations, criteria for criticality safety, criteria for heat removal, and criteria for radiological protection. The standardized NUHOMS <sup>®</sup> system is designed for dry, horizontal storage of irradiated light water reactor (LWR) fuel. The principal design parameters of the fuel to be stored can accommodate standard PWR fuel designs manufactured by Babcock and Wilcox (B&W), Combustion Engineering (CE), and Westinghouse (WE), and standard BWR fuel manufactured by General Electric (GE) and Exxon/ANF. The NUHOMS <sup>®</sup> -24P and 52B systems are limited for use to these standard designs and to equivalent designs by other manufacturers as listed in Chapter 3 of the FSAR. The analyses presented in the FSAR are based on non-consolidated, zircaloy-clad fuel with no known or suspected gross breaches. |  |  |  |  |
|                      | The NUHOMS <sup>®</sup> -61BT, 32PT, 24PHB, and 24PTH systems are limited for<br>use to these standard designs and to equivalent designs by other<br>manufacturers as listed in Tables 1-1d, 1-1f, 1-1i, 1-1j, and 1-1m. The<br>corresponding analyses for these systems are presented in Appendix K, M,<br>N and P respectively of the FSAR.   |  |  |  |  |
|                      | The physical parameters that define the mechanical and structural design<br>of the HSM and DSC are the fuel assembly dimensions and weight. The   |  |  |  |  |

calculated stresses given in the FSAR are based on the physical parameters given in Tables 1-1a, 1-1b, 1-1c, 1-1d, 1-1e, 1-1f, 1-1g, 1-1i, 1-1j, 1-11, and 1-1m which represent the upper bound.

The design basis fuel assemblies for nuclear criticality safety are Babcock and Wilcox 15x15 fuel assemblies for the NUHOMS<sup>®</sup>-24P and 24PHB, General Electric 7x7 fuel assemblies for the NUHOMS<sup>®</sup>-52B and General Electric 10x10 fuel assemblies for the NUHOMS<sup>®</sup>-61BT designs. The nuclear criticality safety for the NUHOMS<sup>®</sup>-32PT and NUHOMS<sup>®</sup>-24PTH designs is based on an evaluation of individual fuel assembly class as listed in Table 1-1e and Table 1-11 respectively.

The NUHOMS<sup>®</sup>-24P Long Cavity DSC is designed for use with standard Burnable Poison Rod Assembly (BPRA) designs for the B&W 15x15 and Westinghouse 17x17 fuel types as listed in Appendix J of the FSAR. The NUHOMS<sup>®</sup>-24PHB Long Cavity DSC is designed for use with standard BPRA designs for the B&W 15x15 fuel types listed in Appendix N of the FSAR.

The design basis PWR BPRA for shielding source terms and thermal decay heat load is the Westinghouse 17x17 Pyrex Burnable Absorber, while the DSC internal pressure analysis is limited by B&W 15x15 BPRAs. In addition, BPRAs with cladding failures were determined to be acceptable for loading into NUHOMS<sup>®</sup>-24P Long Cavity DSC as evaluated in Appendix J of the FSAR. The acceptability of loading BPRAs, including damaged BPRAs into the long cavity versions of the 32PT and 24PTH DSC configurations is provided in Appendix M and Appendix P respectively of the FSAR.

Control Components (CCs), as listed in Table 1-11 are authorized for storage in the NUHOMS<sup>®</sup>-24PTH DSC. The acceptability of loading CCs is provided in Appendix P of the FSAR.

The NUHOMS<sup>®</sup>-24P is designed for unirradiated fuel with an initial fuel enrichment of up to 4.0 wt. % U-235, taking credit for soluble boron in the DSC cavity water during loading operations. Section 1.2.15 defines the requirements for boron concentration in the DSC cavity water for the NUHOMS<sup>®</sup>-24P design only. In addition, the fuel assemblies qualified for storage in NUHOMS<sup>®</sup>-24P DSC have an equivalent unirradiated enrichment of less than or equal to 1.45 wt. % U-235. Figure 1-1 defines the required burnup as a function of initial enrichment. The NUHOMS<sup>®</sup>-52B is designed for unirradiated fuel with an initial enrichment of less than or equal to 4.0 wt. % U-235.

The NUHOMS<sup>®</sup>-61BT has three basket configurations, based on the boron content in the poison plates as listed in Table 1-1k. The maximum lattice average enrichment authorized for Type A, B and C NUHOMS<sup>®</sup>-61BT DSC is 3.7, 4.1 and 4.4 wt. % U-235 respectively.

The NUHOMS<sup>®</sup>-32PT is designed for unirradiated fuel with an initial fuel enrichment of up to 5.0 wt. % U-235 as shown in Table 1-1g, taking credit for Poison Rod Assemblies (PRAs), poison plates, and soluble boron in the DSC cavity water during loading operations. The required number of PRAs as a function of assembly class and maximum initial enrichment is per Table 1-1g. The required PRA locations are per Figures 1-5, or 1-6 or 1-7. Table 1-1h specifies the minimum B10 content for poison plates. Specification 1.2.15a defines the requirements for boron concentration in the DSC cavity water for the NUHOMS<sup>®</sup>-32PT design only.

The NUHOMS<sup>®</sup>-24PHB is designed for unirradiated fuel with an assembly average initial enrichment of less than or equal to 4.5 wt. % U-235 as shown in Table 1-1i, taking credit for soluble boron in the DSC cavity water during loading operations. Specification 1.2.15b defines the requirements for boron concentration in the DSC cavity water for the NUHOMS<sup>®</sup>-24PHB design only.

The NUHOMS<sup>®</sup>-24PTH is designed for unirradiated fuel with an assembly average initial enrichment of less than or equal to 5.0 wt. % U-235, as shown in Table 1-11, taking credit for soluble boron in the DSC cavity water during loading operations and the boron content in the poison plates of the DSC basket, as shown in Table 1-1p for intact fuel and Table 1-1q for damaged fuel. The 24PTH DSC basket is designated as Type 1, if it is provided with aluminum inserts and Type 2 if it does not contain the aluminum inserts. Each basket type is designed with three alternate configurations, based on the boron content in the poison plates, as listed in Table 1-1r. The specification for the Metal Matrix Composite (MMC) for the 24PTH poison plates is provided in Table 1-1s. Specification 1.2.15c defines the requirements for boron concentration in the DSC cavity water as a function of the DSC basket type for the various fuel classes authorized for storage in the 24PTH DSC for the NUHOMS<sup>®</sup>-24PTH design only.

The thermal design criterion of the fuel to be stored is that the total maximum heat generation rate per assembly and BPRA or Control Components be such that the fuel cladding temperature is maintained within established limits during normal and off-normal conditions. For the NUHOMS<sup>®</sup>-24P, 52B and 61BT systems, fuel cladding temperature limits were established based on methodology in PNL-6189 and PNL-4835. For the NUHOMS<sup>®</sup>-32PT, 24PHB and 24PTH systems, fuel cladding limits are based on ISG-11, Rev. 2 (Reference 3).

The radiological design criterion is that fuel stored in the NUHOMS<sup>®</sup> system must not increase the average calculated HSM or transfer cask surface dose rates beyond those calculated for the 24P, 24PHB, 52B, 61BT, or 32PT canister full of design basis fuel assemblies with or without BPRAs. The design value average HSM and cask surface dose rates for the 24P and 52B canisters were calculated to be 48.6 mrem/hr

and 591.8 mrem/hr respectively based on storing twenty four (24) Babcock and Wilcox 15x15 PWR assemblies (without BPRAs) with 4.0 wt. % U-235 initial enrichment, irradiated to 40,000 MWd/MTU, and having a post irradiation time of five years. To account for BPRAs, the fuel assembly cooling required times are increased to maintain the above dose rate limits.

| Title or Parameter                               | Specifications   |  |  |  |  |  |
|--|--|--|--|--|--|--|
| Fuel   | Only intact, unconsolidated PWR fuel assemblies<br>(with or without BPRAs) with the following<br>requirements. |  |  |  |  |  |
| Physical Parameters (without BPRAs)              |  |  |  |  |  |  |
| Maximum Assembly Length (unirradiated)           | 165.75 in (standard cavity)<br>171.71 in (long cavity)   |  |  |  |  |  |
| Nominal Cross-Sectional Envelope                 | 8.536 in   |  |  |  |  |  |
| Maximum Assembly Weight                          | 1682 lbs   |  |  |  |  |  |
| No. of Assemblies per DSC                        | 24 intact assemblies   |  |  |  |  |  |
| Fuel Cladding                                    | Zircalloy-clad fuel with no known or suspected gross cladding breaches   |  |  |  |  |  |
| Physical Parameters (with BPRAs)                 |  |  |  |  |  |  |
| Maximum Assembly + BPRA Length<br>(unirradiated) |  |  |  |  |  |  |
| With Burnup > 32,000 and 45,000<br>MWd/MTU       | 171.71 in (long cavity)  |  |  |  |  |  |
| With Burnup 32,000 MWd/MTU                       | 171.96 in (long cavity)  |  |  |  |  |  |
| Nominal Cross-Sectional Envelope                 | 8.536 in   |  |  |  |  |  |
| Maximum Assembly + BPRA Weight                   | 1682 lbs   |  |  |  |  |  |
| No. of Assemblies per DSC                        | 24 intact assemblies   |  |  |  |  |  |
| No. of BPRAs per DSC                             | 24 BPRAs   |  |  |  |  |  |
| Fuel Cladding                                    | Zircalloy-clad fuel with no known or suspected gross cladding breaches   |  |  |  |  |  |
| Nuclear Parameters                               |  |  |  |  |  |  |
| Fuel Initial Enrichment                          | 4.0 wt. % U-235  |  |  |  |  |  |
| Fuel Burnup and Cooling Time                     | Per Table 1-2a (without BPRAs)<br>or<br>Per Table 1-2c (with BPRAs)  |  |  |  |  |  |
| BPRA Cooling Time (Minimum)                      | 5 years for B&W Designs<br>10 years for Westinghouse Designs   |  |  |  |  |  |
| Alternate Nuclear Parameters                     |  |  |  |  |  |  |
| Initial Enrichment                               | 4.0 wt. % U-235  |  |  |  |  |  |
| Burnup   | 40,000 MWd/MTU   |  |  |  |  |  |
| Decay Heat (Fuel + BPRA)                         | 1.0 kW per assembly  |  |  |  |  |  |
| Neutron Fuel Source                              | $2.23 \times 10^8$ n/sec per assy with spectrum<br>bounded by that in Chapter 7 of FSAR                        |  |  |  |  |  |
| Gamma (Fuel + BPRA) Source                       | 7.45 x $10^{15}$ g/sec per assy with spectrum bounded by that in Chapter 7 of FSAR                             |  |  |  |  |  |

## Table 1-1aPWR Fuel Specifications for Fuel to be Stored in the<br/>Standardized NUHOMS®-24P DSC

| Title or Parameter                     | Specifications   |  |  |  |  |
|--|--|--|--|--|--|
| Fuel                                   | Only intact, unconsolidated BWR fuel assemblies with the following requirements              |  |  |  |  |
| Physical Parameters                    |  |  |  |  |  |
| Maximum Assembly Length (unirradiated) | 176.16 in  |  |  |  |  |
| Nominal Cross-Sectional Envelope*      | 5.454 in   |  |  |  |  |
| Maximum Assembly Weight                | 725 lbs  |  |  |  |  |
| No. of Assemblies per DSC              | 52 intact channeled assemblies   |  |  |  |  |
| Fuel Cladding                          | Zircalloy-clad fuel with no known or suspected gross cladding breaches                       |  |  |  |  |
| Nuclear Parameters                     |  |  |  |  |  |
| Fuel Initial Lattice Enrichment        | 4.0 wt. % U-235  |  |  |  |  |
| Fuel Burnup and Cooling Time           | Per Table 1-2b   |  |  |  |  |
| Alternate Nuclear Parameters           |  |  |  |  |  |
| Initial Enrichment                     | 4.0 wt. % U-235  |  |  |  |  |
| Burnup                                 | 35,000 MWd/MTU and per Figure 1.1  |  |  |  |  |
| Decay Heat                             | 0.37 kW per assembly   |  |  |  |  |
| Neutron Source                         | 1.01 x 10 <sup>8</sup> n/sec per assy with spectrum<br>bounded by that in Chapter 7 of FSAR  |  |  |  |  |
| Gamma Source                           | 2.63 x 10 <sup>15</sup> g/sec per assy with spectrum<br>bounded by that in Chapter 7 of FSAR |  |  |  |  |

## Table 1-1bBWR Fuel Specifications for Fuel to be Stored in the<br/>Standardized NUHOMS®-52B DSC

\*Cross-Sectional Envelope is the outside dimension of the fuel channel.

## Table 1-1cBWR Fuel Specifications for Fuel to be Stored in the<br/>Standardized NUHOMS®-61BT DSC

| Physical Parameters                                    |   |  |  |  |  |  |
|--|---|--|--|--|--|--|
|  | 7x7, $8x8$ , $9x9$ , or $10x10$ BWR fuel assemblies manufactured by   |  |  |  |  |  |
| Fuel Design  | General Electric or equivalent reload fuel that are enveloped by  |  |  |  |  |  |
|  | the fuel assembly design characteristics listed in Table 1-1d.  |  |  |  |  |  |
| Cladding Material                                      | Zircaloy  |  |  |  |  |  |
| Fuel Damage  | Cladding damage in excess of pinhole leaks or hairline cracks is<br>not authorized to be stored as "Intact BWR Fuel." |  |  |  |  |  |
| Channels   | Fuel may be stored with or without fuel channels  |  |  |  |  |  |
| Maximum Assembly Length                                | 176.2 in  |  |  |  |  |  |
| Nominal Assembly Width (excluding channels)            | 5.44 in   |  |  |  |  |  |
| Maximum Assembly Weight                                | 705 lbs   |  |  |  |  |  |
| Radiological Parameters: No interpolation of Radiologi | cal Parameters is permitted between Groups.   |  |  |  |  |  |
| Group 1  |   |  |  |  |  |  |
| Maximum Burnup   | 27,000 MWd/MTU  |  |  |  |  |  |
| Minimum Cooling Time                                   | 5-years   |  |  |  |  |  |
| Maximum Lattice Average Initial Enrichment             | See Minimum Boron Loading below.  |  |  |  |  |  |
| Minimum Initial Bundle Average Enrichment              | 2.0 wt. % U-235   |  |  |  |  |  |
| Maximum Initial Uranium Content                        | 198 kg/assembly   |  |  |  |  |  |
| Maximum Decay Heat                                     | 300 W/assembly  |  |  |  |  |  |
| Group 2  |   |  |  |  |  |  |
| Maximum Burnup   | 35,000 MWd/MTU  |  |  |  |  |  |
| Minimum Cooling Time                                   | 8-years   |  |  |  |  |  |
| Maximum Lattice Average Initial Enrichment             | See Minimum Boron Loading below.  |  |  |  |  |  |
| Minimum Initial Bundle Average Enrichment              | 2.65 wt. % U-235  |  |  |  |  |  |
| Maximum Initial Uranium Content                        | 198 kg/assembly   |  |  |  |  |  |
| Maximum Decay Heat                                     | 300 W/assembly  |  |  |  |  |  |
| Group 3  |   |  |  |  |  |  |
| Maximum Burnup   | 37,200 MWd/MTU  |  |  |  |  |  |
| Minimum Cooling Time                                   | 6.5-years   |  |  |  |  |  |
| Maximum Lattice Average Initial Enrichment             | See Minimum Boron Loading below.  |  |  |  |  |  |
| Minimum Initial Bundle Average Enrichment              | 3.38 wt. % U-235  |  |  |  |  |  |
| Maximum Initial Uranium Content                        | 198 kg/assembly   |  |  |  |  |  |
|  | 300 W/assembly  |  |  |  |  |  |
| Maximum Decay Heat                                     | 500 w/assembly  |  |  |  |  |  |
| Group 4  |   |  |  |  |  |  |
| Maximum Burnup   | 40,000 MWd/MTU  |  |  |  |  |  |
| Minimum Cooling Time                                   | 10-years  |  |  |  |  |  |
| Maximum Lattice Average Initial Enrichment             | See Minimum Boron Loading below.  |  |  |  |  |  |
| Minimum Initial Bundle Average Enrichment              | 3.4 wt. % U-235   |  |  |  |  |  |
| Maximum Initial Uranium Content                        | 198 kg/assembly   |  |  |  |  |  |
| Maximum Decay Heat                                     | 300 W/assembly  |  |  |  |  |  |
| Minimum Boron Loading                                  |   |  |  |  |  |  |
| Lattice Average Enrichment (wt. % U-235)               | Minimum B-10 Content in Poison Plates   |  |  |  |  |  |
| 4.4  | Type C Basket   |  |  |  |  |  |
| 4.1  | Type B Basket   |  |  |  |  |  |
| 3.7  | Type A Basket   |  |  |  |  |  |
| Alternate Radiological Parameters:                     | - Jpo II Duokot   |  |  |  |  |  |
| Maximum Initial Enrichment:                            | See Minimum Boron Loading Above   |  |  |  |  |  |
| Fuel Burnup, Initial Bundle Average                    |   |  |  |  |  |  |
| Enrichment, and Cooling Time:                          | See Table 1-2q  |  |  |  |  |  |
| Maximum Initial Uranium Content:                       | 198 kg/assembly   |  |  |  |  |  |
| Maximum Decay Heat:                                    | 300 W/assembly  |  |  |  |  |  |

| Transnuclear, ID                           | 7 x 7-<br>49/0 <sup>(5)</sup> | 8 x 8-<br>63/1 <sup>(5)</sup> | 8 x 8-<br>62/2 <sup>(5)</sup> | 8 x 8 -<br>60/4 <sup>(5)</sup> | 8 x 8-<br>60/1 <sup>(5)</sup> | 9 x 9-<br>74/2           | 10x10-<br>92/2            | 7x7-<br>49/0 <sup>(5)</sup> | 7x7<br>48/1Z <sup>(5)</sup> | 8x8 –<br>60/4Z <sup>(5)</sup> |
|--|-------------------------------|-------------------------------|-------------------------------|--------------------------------|-------------------------------|--------------------------|---------------------------|-----------------------------|-----------------------------|-------------------------------|
|  | GE1                           |                               | GE-5                          |                                |                               |                          |                           |                             |                             | ENC Va                        |
| GE Designations                            | GE2                           | GE4                           | GE-Pres<br>GE-Barrier         | GE8<br>Type II                 | GE9<br>GE10                   | GE11<br>GE13             | GE12                      | ENC III-A                   | ENC III <sup>(3)</sup>      | & ENC                         |
|  | GE3                           |                               | GE8 Type I                    | 1900                           | 0110                          | 0110                     |                           |                             |                             | Vb                            |
| Max Length (in)<br>(Unirradiated)          | 176.2                         | 176.2                         | 176.2                         | 176.2                          | 176.2                         | 176.2                    | 176.2                     | 176.2                       | 176.2                       | 176.2                         |
| Nominal Width (in)<br>(excluding channels) | 5.44                          | 5.44                          | 5.44                          | 5.44                           | 5.44                          | 5.44                     | 5.44                      | 5.44                        | 5.44                        | 5.44                          |
| Fissile Material                           | UO <sub>2</sub>               | UO <sub>2</sub>               | UO <sub>2</sub>               | UO <sub>2</sub>                | UO <sub>2</sub>               | UO <sub>2</sub>          | UO <sub>2</sub>           | UO <sub>2</sub>             | UO <sub>2</sub>             | UO <sub>2</sub>               |
| Number of Fuel Rods                        | 49                            | 63                            | 62                            | 60                             | 60                            | 66 – Full<br>8 – Partial | 78 – Full<br>14 - Partial | 49                          | 48                          | 60                            |
| Number of Water Holes                      | 0                             | 1                             | 2                             | 4                              | 1                             | 2                        | 2                         | 0                           | 1(4)                        | 4 <sup>(4)</sup>              |

Table 1-1dBWR Fuel Assembly Design Characteristics (1) (2) (3)for the NUHOMS®-61BT DSC

(1) Any fuel channel thickness from 0.065 to 0.120 inch is acceptable on any of the fuel designs.

(2) Maximum fuel assembly weight with channel is 705 lb.

(3) Includes ENC III-E and ENC III-F.

(4) Solid Zirc rods instead of water holes.

(5) May be stored as damaged fuel.

Table 1-1ePWR Fuel Specifications for Fuel to be Stored in the NUHOMS®-32PT DSC

| PHYSICAL PARAMETERS:                       |   |  |  |  |  |
|--|---|--|--|--|--|
| Fuel Assembly Class                        | B&W 15x15, WE 17x17, CE 15x15, WE 15x15, CE 14x14 and WE 14x14 assemblies that are enveloped by the fuel assembly design characteristics listed in Table 1- |  |  |  |  |
|  | 1f.   |  |  |  |  |
| Fuel Cladding Material                     | Zircaloy  |  |  |  |  |
| Fuel Damage                                | Cladding damage in excess of pinhole leaks or hairline<br>cracks is not authorized to be stored as "Intact PWR<br>Fuel."                                    |  |  |  |  |
| Burnable Poison Rod Assemblies (BPRAs)     | Standard BPRA designs for the B&W 15x15 and<br>Westinghouse 17x17 class assemblies as listed in<br>Appendix J of the FSAR.                                  |  |  |  |  |
| Maximum Assembly plus BPRA Weight          | -1365 lbs for 32PT-S100 & 32PT-L100 System<br>-1682 lbs for 32PT-S125 & 32PT-L125 System  |  |  |  |  |
| BPRA Damage                                | BPRAs with cladding failures are acceptable for loading.  |  |  |  |  |
| THERMAL/RADIOLOGICAL PARAMETERS:           |   |  |  |  |  |
| Fuel Burnup and Cooling Time without BPRAs | Per Table 1-2d, Table 1-2e, Table 1-2f, Table 1-2g,<br>Table 1-2h, and Figure 1-2 or Figure 1-3 or Figure 1-4.  |  |  |  |  |
| Fuel Burnup and Cooling Time with BPRAs    | Per Table 1-2i, Table 1-2j, Table 1-2k, Table 1-2l, Table 1-2m and Figure 1-2 or Figure 1-3 or Figure 1-4.  |  |  |  |  |
| Initial Enrichment                         | Per Table 1-1g and Figure 1-5 or Figure 1-6 or Figure 1-7.  |  |  |  |  |
| B&W 15x15 BPRA Burnup and Cooling Time     | BPRA Burnup shall not exceed that of a BPRA irradiated<br>in fuel assemblies with a total Burnup of 36,000<br>MWd/MTU.<br>-Minimum Cooling Time 5 years     |  |  |  |  |
| WE 17x17 BPRA Burnup and Cooling Time      | BPRA Burnup shall not exceed that of a BPRA irradiated<br>in fuel assemblies with a total Burnup of 36,000<br>MWd/MTU.<br>-Minimum Cooling Time 10 years    |  |  |  |  |

| Assembly Class                                  | B&W<br>15x15          | WE<br>17x17           | CE<br>15x15     | WE<br>15x15      | CE<br>14x14     | WE<br>14x14     |
|---|-----------------------|-----------------------|-----------------|------------------|-----------------|-----------------|
| DSC Configuration                               |                       |                       | Max Unirradia   | nted Length (in) | )               |                 |
| 32PT-S100/32PT-S125                             | 165.75                | 165.75                | 165.75          | 165.75           | 165.75          | 165.75          |
| 32PT-L100/32PT-L125                             | 171.71 <sup>(1)</sup> | 171.71 <sup>(1)</sup> | 171.71          | 171.71           | 171.71          | 171.71          |
| Fissile Material                                | UO <sub>2</sub>       | UO <sub>2</sub>       | UO <sub>2</sub> | UO <sub>2</sub>  | UO <sub>2</sub> | UO <sub>2</sub> |
| Maximum<br>MTU/assembly <sup>(2)</sup>          | 0.475                 | 0.475                 | 0.475           | 0.475            | 0.475           | 0.475           |
| Maximum Number<br>of Fuel Rods                  | 208                   | 264                   | 216             | 204              | 176             | 179             |
| Maximum Number<br>of Guide/ Instrument<br>Tubes | 17                    | 25                    | 9               | 21               | 5               | 17              |

Table 1-1f PWR Fuel Assembly Design Characteristics for the NUHOMS®-32PT DSC

Maximum Assembly + BPRA Length (unirradiated)
 The maximum MTU/assembly is based on the shielding analysis. The listed value is higher than the actual.

Table 1-1gInitial Enrichment and Required Number of PRAs (NUHOMS®-32PT DSC)

| Assembly                 |                                  | Initial Enrichment, wt. % U-235 |                  |                  |                  |  |
|--------------------------|----------------------------------|---------------------------------|------------------|------------------|------------------|--|
| Class                    | Assembly Type                    | 0 PRAs                          | 4 PRAs           | 8 PRAs           | 16 PRAs          |  |
| WE 17x17 <sup>(1)</sup>  | Westinghouse 17x17 LOPAR/Std     | 3.40                            | 4.00             | 4.50             | 5.00             |  |
| WE I/XI/                 | Westinghouse 17x17 OFA/Vantage 5 | 5.40                            | 4.00             | 4.50             | 5.00             |  |
| B&W 15x15 <sup>(1)</sup> | B&W 15x15 Mark B                 | 3.30                            | 3.90             | NA               | 5.00             |  |
| CE 15x15                 | CE 15x15 Palisades               | 3.40                            | Not<br>Evaluated | Not<br>Evaluated | Not<br>Evaluated |  |
| CE IJXIJ                 | Exxon/ANF 15x15 CE               | 5.40                            |                  |                  |                  |  |
| WE 15x15                 | Westinghouse 15x15 Std/ZC        | 3.40                            | 4.00             | 4.60             | 5.00             |  |
| WE ISXIS                 | Exxon/ANF 15x15 WE               | 3.40                            | 4.00             |                  |                  |  |
| CE 14x14                 | CE 14x14 Std/Generic             | 3.80                            | 4.60             | 5.00             | Not Evaluated    |  |
| CE 14X14                 | CE 14x14 Fort Calhoun            | 5.80                            | 4.00             | 5.00             |                  |  |
|                          | Westinghouse 14x14 ZCA/ZCB       |                                 |                  |                  |                  |  |
| WE 14x14                 | Westinghouse 14x14 OFA           | 4.00                            | 5.00             | Not<br>Evaluated | Not Evaluated    |  |
|                          | Exxon/ANF 14x14 WE               |                                 |                  | Eralduled        |                  |  |

(1) With or without BPRAs. BPRAs shall not be stored in basket locations where a PRA is required.

## Table 1-1hB10 Content Specification for Poison Plates (NUHOMS®-32PT DSC)

| DSC Configuration                                   | Poison Plate Specification                           |
|---|--|
| 32PT-S100 or 32PT-S125 or<br>32PT-L100 or 32PT-L125 | Minimum B10 areal density = 0.007 gm/cm <sup>2</sup> |

| Title or Parameter  | Specifications   |
|---|--|
| Fuel  | Only intact, unconsolidated B&W 15x15 class<br>PWR fuel assemblies (with or without BPRAs) |
| Maximum No. of Reconstituted Assemblies per<br>DSC with Stainless Steel rods            | with the following requirements<br>4   |
| Maximum No. of Stainless Steel Rods per   | 10   |
| Reconstituted Assembly  |  |
| Maximum No. of Reconstituted Assemblies per<br>DSC with low enriched uranium oxide rods | 24   |
| Physical Parameters (without BPRAs)   |  |
| Maximum Assembly Length (unirradiated)  | 165.785 in (standard cavity)<br>171.96 in (long cavity)                                    |
| Nominal Cross-Sectional Envelope  | 8.536 in   |
| Maximum Assembly Weight   | 1682 lbs   |
| No. of Assemblies per DSC   | 24 intact assemblies   |
| Fuel Cladding   | Zircaloy-clad fuel with no known or suspected  |
|   | gross cladding breaches  |
| Physical Parameters (with BPRAs)  |  |
| Maximum Assembly + BPRA Length (unirradiated)   | 171.96 in (long cavity)  |
| Nominal Cross-Sectional Envelope  | 8.536 in   |
| Maximum Assembly + BPRA Weight  | 1682 lbs   |
| No. of Assemblies per DSC   | 24 intact assemblies   |
| No. of BPRAs per DSC  | 24 BPRAs   |
| Fuel Cladding   | Zircaloy-clad fuel with no known or suspected gross cladding breaches                      |
| Nuclear Parameters  |  |
| Maximum Fuel Initial Enrichment   | 4.5 wt. % U-235  |
| Maximum Initial Uranium loading per assembly  | 0.490 MTU  |
| Allowable loading configurations for each 24PHB<br>DSC                                  | As specified in Figure 1-8 or 1-9  |
| Burnup, Enrichment, and Minimum Cooling Time  | Table 1-2n for Zone 1 fuel; Table 1-20 for Zone  |
| for Configuration 1 (Figure 1-8)  | 2 fuel; Table 1-2p for Zone 3 fuel   |
| Burnup, Enrichment, and Minimum Cooling Time  | Table 1-2p for Zone 3 fuel   |
| for Configuration 2 (Figure 1-9)  |  |
| Minimum Cooling Time for BPRAs  | 5 years  |
| Total Decay Heat per DSC  | 24 kW  |
| Decay Heat Limits for Zone 1, 2 and 3 fuel  | As specified in Figures 1-8 and 1-9.   |

## Table 1-1iPWR Fuel Specifications for Fuel to be Stored in the<br/>Standardized NUHOMS®-24PHB DSC

# Table 1-1jBWR Fuel Specification of Damaged Fuel to be Stored in the StandardizedNUHOMS®-61BT DSC

| PHYSICAL PARAMETERS:   |  |
|--|--|
| Fuel Design:   | 7x7, 8x8 BWR damaged fuel assemblies manufactured by<br>General Electric or Exxon/ANF or equivalent reload fuel that are<br>enveloped by the Fuel assembly design characteristics listed in<br>Table 1-1d for the 7x7 and 8x8 designs only.  |
| Cladding Material:   | Zircaloy   |
| Fuel Damage:   | Damaged BWR fuel assemblies are fuel assemblies containing<br>fuel rods with known or suspected cladding defects greater than<br>hairline cracks or pinhole leaks. Missing cladding and/or crack<br>size in the fuel pins is to be limited such that a fuel pellet is not<br>able to pass through the gap created by the cladding opening<br>during handling and retrievability is assured following<br>Normal/Off-Normal conditions. Damaged fuel shall be stored<br>with Top and Bottom Caps for Failed Fuel. Damaged fuel may<br>only be stored in the 2x2 compartments of the "Type C"<br>NUHOMS®-61BT Canister. |
| Channels:  | Fuel may be stored with or without fuel channels.  |
| Maximum Assembly Length (unirradiated)                               | 176.2 in   |
| Nominal Assembly Width (excluding channels)                          | 5.44 in  |
| Maximum Assembly Weight  | 705 lbs  |
| RADIOLOGICAL PARAMETERS:   | No interpolation of Radiological Parameters is permitted between groups.   |
| Group 1:   | 5F   |
| Maximum Burnup:  | 27,000 MWd/MTU   |
| Minimum Cooling Time:  | 5-years  |
| Maximum Initial Lattice Average Enrichment:                          | 4.0 wt. % U-235  |
| Maximum Pellet Enrichment:   | 4.4 wt. % U-235  |
| Minimum Initial Bundle Average Enrichment:                           | 2.0 wt. % U-235  |
| Maximum Initial Uranium Content:                                     | 198 kg/assembly  |
| Maximum Decay Heat:  | 300 W/assembly   |
| Group 2:   |  |
| Maximum Burnup:  | 35,000 MWd/MTU   |
| Minimum Cooling Time:<br>Maximum Initial Lattice Average Enrichment: | 8-years  |
| Maximum Pellet Enrichment:   | 4.0 wt. % U-235<br>4.4 wt. % U-235   |
| Minimum Initial Bundle Average Enrichment:                           | 4.4 wt. % U-235<br>2.65 wt. % U-235  |
| Maximum Initial Uranium Content:                                     | 198 kg/assembly  |
| Maximum Decay Heat:  | 300 W/assembly   |
| maximum Doday mat.   | 500 Wrasseniory  |
| Group 3:<br>Maximum Burnup:  | 37,200 MWd/MTU   |
| Minimum Cooling Time:  | 6.5-years  |
| Maximum Initial Lattice Average Enrichment:                          | 4.0 wt. % U-235  |
| Maximum Pellet Enrichment:   | 4.4 wt. % U-235  |
| Minimum Initial Bundle Average Enrichment:                           | 3.38 wt. % U-235   |
| Maximum Initial Uranium Content:                                     | 198 kg/assembly  |
| Maximum Decay Heat:  | 300 W/assembly   |

# Table 1-1jBWR Fuel Specification of Damaged Fuel to be Stored in the StandardizedNUHOMS®-61BT DSC

### (Concluded)

| RADIOLOGICAL PARAMETERS:  |                 |
|---|-----------------|
| Group 4:  |                 |
| Maximum Burnup:   | 40,000 MWd/MTU  |
| Minimum Cooling Time:   | 10-years        |
| Maximum Initial Lattice Average Enrichment:                       | 4.0 wt. % U-235 |
| Maximum Pellet Enrichment:  | 4.4 wt. % U-235 |
| Minimum Initial Bundle Average Enrichment:                        | 3.4 wt. % U-235 |
| Maximum Initial Uranium Content:                                  | 198 kg/assembly |
| Maximum Decay Heat:   | 300 W/assembly  |
| ALTERNATE RADIOLOGICAL PARAMETERS:                                |                 |
| Maximum Initial Lattice Average Enrichment:                       | 4.0 wt. % U-235 |
| Fuel Burnup, Initial Bundle Average Enrichment, and Cooling Time: | See Table 1-2q  |
| Maximum Pellet Enrichment:  | 4.4 wt. % U-235 |
| Maximum Initial Uranium Content:                                  | 198 kg/assembly |
| Maximum Decay Heat:   | 300 W/assembly  |

|  | Minimum B10 Aerial Density, gm/cm <sup>2</sup>              |   |  |  |
|--|---|---|--|--|
| NUHOMS <sup>®</sup> -61BT DSC Basket<br>Type | Enriched Boron Aluminum Alloy<br>or Boralyn <sup>®(1)</sup> | Boral <sup>®</sup> or Metamic <sup>®(2)</sup> |  |  |
| А  | .021  | .025  |  |  |
| В  | .032  | .038  |  |  |
| С  | .040  | .048  |  |  |

## Table 1-1kB10 Specification for the NUHOMS®-61BT Poison Plates

Note 1: An alternate metal matrix composite with properties equivalent to Boralyn<sup>®</sup> is acceptable. Note 2: An alternate metal matrix composite with properties equivalent to Metamic<sup>®</sup> is acceptable.

## Table 1-11PWR Fuel Specification for the Fuel to be Stored in the NUHOMS®-24PTH DSC

| Physical Parameters:   |  |
|--|--|
| Fuel Class   | Intact or damaged unconsolidated B&W 15x15, WE 17x17, CE 15x15, WE 15x15, CE 14x14 and WE 14x14 class PWR assemblies (with or without control components) that are enveloped by the fuel assembly design characteristics listed in Table 1-1m. Equivalent reload fuel manufactured by other vendors but enveloped by the design characteristics listed in Table 1-1m is also acceptable.   |
| Fuel Damage  | Damaged PWR fuel assemblies are assemblies containing<br>missing or partial fuel rods or fuel rods with known or<br>suspected cladding defects greater than hairline cracks or<br>pinhole leaks. The extent of cladding damage in the fuel rods<br>is to be limited such that a fuel pellet is not able to pass<br>through the damaged cladding opening during handling and<br>retrievability is assured following normal and off-normal<br>conditions.      |
| <ul> <li>Reconstituted Fuel Assemblies:</li> <li>Maximum No. of Reconstituted Assemblies per<br/>DSC With Stainless Steel Rods</li> <li>Maximum No. of Stainless Steel Rods per<br/>Reconstituted Fuel Assembly</li> <li>Maximum No. of Reconstituted Assemblies per<br/>DSC with low enriched UO2 rods</li> </ul> | 41024  |
| Control Components (CCs)   | <ul> <li>Up to 24 CCs are authorized for storage in 24PTH-L and 24PTH-S-LC DSCs only.</li> <li>Authorized CCs include Burnable Poison Rod Assemblies (BPRAs), Thimble Plug Assemblies (TPAs), Control Rod Assemblies (CRAs), Axial Power Shaping Assembly Rods (APSRAs), Orifice Rod Assemblies (ORAs) and Neutron Source Assemblies (NSAs).</li> <li>Design basis thermal and radiological characteristics for the CCs are listed in Table 1-1n.</li> </ul> |
| Nominal Assembly Width   | 8.536 inches   |
| No. of Intact Assemblies   | 24   |
| No. and Location of Damaged Assemblies   | Maximum of 12 damaged fuel assemblies. Balance may be<br>intact fuel assemblies, empty slots, or dummy assemblies<br>depending on the specific heat load zoning configuration.<br>Damaged fuel assemblies are to be placed in Location A<br>and/or B as shown in Figure 1-16. The DSC basket cells<br>which store damaged fuel assemblies are provided with top<br>and bottom end caps to assure retrievability.   |
| Maximum Assembly plus CC Weight  | 1682 lbs   |

## Table 1-11 PWR Fuel Specification for the Fuel to be Stored in the NUHOMS®-24PTH DSC (Concluded)

| Per Figure 1-11 or Figure 1-12 or Figure 1-13 or  |
|---|
| Figure 1-14 or Figure 1-15.                       |
|   |
| Per Table 1-3a for Zone 1 fuel.                   |
|   |
| Per Table 1-3b for Zone 2 fuel.                   |
|   |
| Per Table 1-3b for Zone 2 fuel and Table 1-3c for |
| Zone 3 fuel.                                      |
| Per Table 1-3d for Zone 4 fuel.                   |
|   |
| Per Table 1-3c for Zone 3 fuel and Table 1-3d for |
| Zone 4 fuel.                                      |
| Per Table 1-3e for Zone 1 fuel.                   |
| Per l'able 1-se lor Zolle l'Iuel.                 |
| Per Table 1-3f for Zone 2 fuel.                   |
|   |
| Per Table 1-3f for Zone 2 fuel and per Table 1-3g |
| for Zone 3 fuel.                                  |
| Per Table 1-3h for Zone 4 fuel.                   |
|   |
| Per Table 1-3g for Zone 3 fuel and per Table 1-3h |
| for Zone 4 fuel.                                  |
|   |
| 5.0 wt. % U-235                                   |
| Per Figure 1-11 or Figure 1-12 or Figure 1-13 or  |
| Figure 1-14 or Figure 1-15.                       |
| 40.8 kW for 24PTH-S and 24PTH-L DSCs (Type 1      |
| Basket)   |
| 31.2 kW for 24PTH-S and 24PTH-L DSCs (Type 2      |
| Basket)   |
| 24.0 kW for 24PTH-S-L DSC (Type 2 Basket)         |
| Per Table 1-1r                                    |
|   |

| Assembly Class  |            | B&W<br>15x15    | WE<br>17x17        | CE<br>15x15        | WE<br>15x15        | CE<br>14x14        | WE<br>14x14        |
|---|------------|-----------------|--------------------|--------------------|--------------------|--------------------|--------------------|
| Maximum<br>Unirradiated<br>Length (in) <sup>(1)</sup> | 24PTH-S    | 165.75          | 165.75             | 165.75             | 165.75             | 165.75             | 165.75             |
|   | 24PTH-L    | 171.93          | 171.93             | 171.93             | 171.93             | 171.93             | 171.93             |
|   | 24PTH-S-LC | 171.93          | N/A <sup>(3)</sup> |
| Fissile Material                                      |            | UO <sub>2</sub> | UO <sub>2</sub>    | UO <sub>2</sub>    | UO <sub>2</sub>    | UO <sub>2</sub>    | UO <sub>2</sub>    |
| Maximum MTU/Assembly <sup>(2)</sup>                   |            | 0.49            | 0.49               | 0.49               | 0.49               | 0.49               | 0.49               |
| Maximum Number of Fuel Rods                           |            | 208             | 264                | 216                | 204                | 176                | 179                |
| Maximum Number of Guide/<br>Instrument Tubes          |            | 17              | 25                 | 9                  | 21                 | 5                  | 17                 |

Table 1-1mPWR Fuel Assembly Design Characteristics for the NUHOMS®-24PTH DSC

(3) Not authorized for storage.

<sup>(1)</sup> Maximum Assembly + Control Component Length (unirradiated)

<sup>(2)</sup> The maximum MTU/assembly is based on the shielding analysis. The listed value is higher than the actual.

## Table 1-1n Thermal and Radiological Characteristics for Control Components Stored in the NUHOMS<sup>®</sup> -24PTH DSC

| Parameter                           | BPRAs, NSAs,<br>CRAs and APSRAs | TPAs and ORAs |  |
|-------------------------------------|---------------------------------|---------------|--|
| Maximum Gamma Source<br>(γ/sec/DSC) | 9.3E+14                         | 9.8E+13       |  |
| Decay Heat (Watts/DSC)              | 192.0                           | 192.0         |  |

# Table 1-1pMaximum Assembly Average Initial Enrichment v/s Neutron Poison Requirements for<br/>the NUHOMS® -24PTH DSC (Intact Fuel)

| Fuel Assembly Class     | Maximum Assembly Average Initial Enrichment (wt. % U-235)<br>as a Function of Soluble Boron Concentration and Basket Type<br>(Fixed Poison Loading) |             |          |          |  |  |
|-------------------------|---|-------------|----------|----------|--|--|
|                         | Minimum   | Basket Type |          |          |  |  |
|                         | Soluble Boron<br>(ppm)  | 1A or 2A    | 1B or 2B | 1C or 2C |  |  |
|                         | 2100  | 4.5         | 4.9      | NR       |  |  |
|                         | 2200  | 4.60        | 5        | NR       |  |  |
| CE 14x14 <sup>(1)</sup> | 2300  | 4.7         | NR       | NR       |  |  |
|                         | 2400  | 4.80        | NR       | NR       |  |  |
|                         | 2500  | 4.90        | NR       | NR       |  |  |
|                         | 2600  | 5.00        | NR       | NR       |  |  |
| WE 14x14 <sup>(2)</sup> | 2100  | 4.80        | 5        | NR       |  |  |
|                         | 2200  | 4.90        | NR       | NR       |  |  |
|                         | 2300  | 5.00        | NR       | NR       |  |  |
| CE 15x15 <sup>(2)</sup> | 2100  | 3.90        | 4.2      | 4.6      |  |  |
|                         | 2200  | 4.00        | 4.40     | 4.7      |  |  |
|                         | 2300  | 4.10        | 4.50     | 4.8      |  |  |
|                         | 2400  | 4.20        | 4.60     | 4.90     |  |  |
|                         | 2500  | 4.30        | 4.70     | 5        |  |  |
|                         | 2600  | 4.40        | 4.8      | NR       |  |  |
|                         | 2700  | 4.50        | 4.90     | NR       |  |  |
|                         | 2800  | 4.5         | 5        | NR       |  |  |
|                         | 2900  | 4.60        | NR       | NR       |  |  |
|                         | 3000  | 4.70        | NR       | NR       |  |  |
| WE 15x15 <sup>(2)</sup> | 2100  | 3.80        | 4.20     | 4.6      |  |  |
|                         | 2200  | 3.9         | 4.30     | 4.7      |  |  |
|                         | 2300  | 4           | 4.4      | 4.8      |  |  |
|                         | 2400  | 4.1         | 4.50     | 4.9      |  |  |
|                         | 2500  | 4.2         | 4.60     | 5        |  |  |
|                         | 2600  | 4.3         | 4.70     | NR       |  |  |
|                         | 2700  | 4.3         | 4.80     | NR       |  |  |
|                         | 2800  | 4.40        | 4.90     | NR       |  |  |
|                         | 2900  | 4.50        | 5        | NR       |  |  |
|                         | 3000  | 4.60        | NR       | NR       |  |  |

## Table 1-1p Maximum Assembly Average Initial Enrichment v/s Neutron Poison Requirements for the NUHOMS<sup>®</sup> -24PTH DSC (Intact Fuel)

|                          |                        |             | ll Enrichment (wt.<br>atration and Baske<br>bading) |          |  |  |  |  |  |  |  |
|--------------------------|------------------------|-------------|---|----------|--|--|--|--|--|--|--|
| Fuel Assembly Class      | Minimum                | Basket Type |   |          |  |  |  |  |  |  |  |
|                          | Soluble Boron<br>(ppm) | 1A or 2A    | 1B or 2B  | 1C or 2C |  |  |  |  |  |  |  |
| WE 17x17 <sup>(2)</sup>  | 2100                   | 3.80        | 4.10  | 4.5      |  |  |  |  |  |  |  |
|                          | 2200                   | 3.90        | 4.20  | 4.6      |  |  |  |  |  |  |  |
|                          | 2300                   | 4.00        | 4.30  | 4.70     |  |  |  |  |  |  |  |
|                          | 2400                   | 4           | 4.4   | 4.8      |  |  |  |  |  |  |  |
|                          | 2500                   | 4.1         | 4.50  | 4.9      |  |  |  |  |  |  |  |
|                          | 2600                   | 4.20        | 4.60  | 5        |  |  |  |  |  |  |  |
|                          | 2700                   | 4.30        | 4.70  | NR       |  |  |  |  |  |  |  |
|                          | 2800                   | 4.40        | 4.80  | NR       |  |  |  |  |  |  |  |
|                          | 2900                   | 4.50        | 4.90  | NR       |  |  |  |  |  |  |  |
|                          | 3000                   | 4.60        | 5.00  | NR       |  |  |  |  |  |  |  |
| B&W 15x15 <sup>(2)</sup> | 2100                   | 3.60        | 4.00  | 4.3      |  |  |  |  |  |  |  |
|                          | 2200                   | 3.70        | 4.10  | 4.50     |  |  |  |  |  |  |  |
|                          | 2300                   | 3.80        | 4.20  | 4.60     |  |  |  |  |  |  |  |
|                          | 2400                   | 3.90        | 4.30  | 4.70     |  |  |  |  |  |  |  |
|                          | 2500                   | 4.00        | 4.40  | 4.80     |  |  |  |  |  |  |  |
|                          | 2600                   | 4.10        | 4.50  | 4.90     |  |  |  |  |  |  |  |
|                          | 2700                   | 4.2         | 4.60  | 5.00     |  |  |  |  |  |  |  |
|                          | 2800                   | 4.2         | 4.70  | NR       |  |  |  |  |  |  |  |
|                          | 2900                   | 4.30        | 4.80  | NR       |  |  |  |  |  |  |  |
|                          | 3000                   | 4.40        | 4.90  | NR       |  |  |  |  |  |  |  |

(Concluded)

#### Notes:

- (1) When CCs that extend into the active fuel region are stored, the maximum assembly average initial enrichment shall be reduced by 0.2 wt. %.
- (2) When CCs that extend into the active fuel region are stored, the maximum assembly average initial enrichment shall be reduced by 0.05 wt. % or the soluble boron concentration shall increased by 50 ppm.

NR = Not Required.

 Table 1-1q

 Maximum Assembly Average Initial Enrichment v/s Neutron Poison Requirements for the NUHOMS<sup>®</sup> -24PTH DSC (Damaged Fuel)

|                          |                                | · · · · · ·  | <u> </u> | ,<br>erage Initial I | Enrichment |  |  |  |  |  |  |  |
|--------------------------|--------------------------------|--|----------|----------------------|------------|--|--|--|--|--|--|--|
|                          | Maximum                        | (wt. % U-235) as a Function of Soluble Boron<br>Concentration and Basket Type (Fixed Poison Loading) |          |                      |            |  |  |  |  |  |  |  |
| Assembly Class           | Number of                      |  |          |                      |            |  |  |  |  |  |  |  |
| Assembly Class           | Damaged Fuel<br>Assemblies per | Minimum<br>Soluble   |          | Basket Type          |            |  |  |  |  |  |  |  |
|                          | DSC                            | Boron  | 1A or 2A | 1B or 2B             | 1C or 2C   |  |  |  |  |  |  |  |
|                          |                                | (ppm)  | IA OI ZA | ID OI 2D             | 10 01 20   |  |  |  |  |  |  |  |
| CE 14x14 <sup>(1)</sup>  | 8                              | 2150   | NR       | 4.8                  | NR         |  |  |  |  |  |  |  |
|                          | 12                             | 2150   | NR       | 4.7                  | NR         |  |  |  |  |  |  |  |
|                          | 12                             | 2450   | 4.50     | 5                    | NR         |  |  |  |  |  |  |  |
| WE 14x14 <sup>(2)</sup>  | 12                             | 2150   | 4.50     | 5                    | NR         |  |  |  |  |  |  |  |
| CE 15x15 <sup>(2)</sup>  | 12                             | 2150   | NR       | NR                   | 4.5        |  |  |  |  |  |  |  |
|                          | 12                             | 2550   | NR       | NR                   | 5          |  |  |  |  |  |  |  |
| WE 15x15 <sup>(2)</sup>  | 8                              | 2150   | NR       | NR                   | 4.5        |  |  |  |  |  |  |  |
|                          | 12                             | 2250   | NR       | NR                   | 4.5        |  |  |  |  |  |  |  |
|                          | 8                              | 2550   | NR       | NR                   | 5          |  |  |  |  |  |  |  |
|                          | 12                             | 2650   | NR       | NR                   | 5          |  |  |  |  |  |  |  |
| B&W 15x15 <sup>(2)</sup> | 12                             | 2350   | NR       | NR                   | 4.5        |  |  |  |  |  |  |  |
|                          | 12                             | 2800   | NR       | NR                   | 5          |  |  |  |  |  |  |  |
| WE 17x17 <sup>(2)</sup>  | 12                             | 2250   | NR       | NR                   | 4.5        |  |  |  |  |  |  |  |
|                          | 12                             | 2650   | NR       | NR                   | 5          |  |  |  |  |  |  |  |

Notes:

- (1) When CCs that extend into the active fuel region are stored, the maximum assembly average initial enrichment shall be reduced by 0.2 wt. %.
- (2) When CCs that extend into the active fuel region are stored, the maximum assembly average initial enrichment shall be reduced by 0.05 wt. % or the soluble boron concentration shall increased by 50 ppm.

NR = Not Required.

|   | Minimum B10 Aerial  | Density, gm/cm <sup>2</sup> |
|---|---|-----------------------------|
| NUHOMS <sup>®</sup> 24PTH DSC Basket<br>Type <sup>(1)</sup> | Natural or Enriched Boron<br>Aluminum Alloy / Metal Matric<br>Composite (MMC) | Boral®                      |
| 1A or 2A  | 0.007   | 0.009                       |
| 1B or 2B  | 0.015   | 0.019                       |
| 1C or 2C  | 0.032   | 0.04                        |

## Table 1-1rB10 Specification for the NUHOMS®-24PTH Poison Plates

(1) Basket Type 1 contains aluminum inserts in the R45 transition rails of the basket, Type 2 does not contain aluminum inserts.

## Table 1-1s Specification for the Metal Matrix Composite (MMC) for the NUHOMS®-24PTH Poison Plates

| No. | Specification   |  |  |  |  |  |  |  |  |  |  |  |
|-----|---|--|--|--|--|--|--|--|--|--|--|--|
| 1   | The metal matrix composite shall consist of boron carbide powder in an aluminum alloy matrix.   |  |  |  |  |  |  |  |  |  |  |  |
| 2   | The boron carbide content shall be limited to a maxim volume.   | num 40% by                                 |  |  |  |  |  |  |  |  |  |  |
| 3   | No more than 10 wt % of the boron carbide powder shall be larger than 60 microns.   |  |  |  |  |  |  |  |  |  |  |  |
| 4   | The product shall be at least 98% of theoretical densit   | ty.  |  |  |  |  |  |  |  |  |  |  |
| 5   | The composite final product form shall have the tensi     Minimum yield strength, 0.2% offset:     Minimum ultimate strength:     Minimum elongation in 2 inches: | le properties:<br>1.5 ksi<br>5.0 ksi<br>1% |  |  |  |  |  |  |  |  |  |  |

 Table 1-2a

 PWR Fuel Qualification Table for the Standardized NUHOMS®-24P DSC (Fuel Without BPRAs)

| ( | Minimum | required | years of | cooling | time a | after reactor | core discharge) | ) |
|---|---------|----------|----------|---------|--------|---------------|-----------------|---|
|   |         |          |          |         |        |               |                 |   |

| D             | Initial Enrichment (wt. % U-235) |     |     |     |        |        |     |     |        |       |      |       |        |     |     |     |     | - U | /   |     |     |
|---------------|----------------------------------|-----|-----|-----|--------|--------|-----|-----|--------|-------|------|-------|--------|-----|-----|-----|-----|-----|-----|-----|-----|
| Burnup        |                                  |     |     |     |        |        |     | In  | tial E | nrich | ment | wt. % | 6 U-2. | 35) |     |     |     |     |     |     |     |
| (GWd/<br>MTU) | 2.0                              | 2.1 | 2.2 | 2.3 | 2.4    | 2.5    | 2.6 | 2.7 | 2.8    | 2.9   | 3.0  | 3.1   | 3.2    | 3.3 | 3.4 | 3.5 | 3.6 | 3.7 | 3.8 | 3.9 | 4.0 |
| 10            | а                                | а   | а   | a   | a      | а      | а   | а   | a      | а     | а    | а     | а      | а   | а   | а   | a   | а   | а   | а   | а   |
| 15            | 5                                | 5   | а   | а   | а      | а      | а   | а   | а      | а     | а    | а     | а      | а   | а   | а   | а   | а   | а   | а   | а   |
| 20            | 5                                | 5   | 5   | 5   | 5      | а      | а   | а   | а      | а     | а    | а     | а      | а   | а   | а   | а   | а   | а   | а   | а   |
| 25            |                                  | 5   | 5   | 5   | 5      | 5      | 5   | 5   | 5      | а     | а    | а     | а      | а   | а   | а   | а   | а   | а   | а   | a   |
| 28            |                                  |     |     | 5   | 5      | 5      | 5   | 5   | 5      | 5     | 5    | 5     | а      | а   | а   | а   | а   | а   | а   | а   | a   |
| 30            |                                  |     |     |     |        | 5      | 5   | 5   | 5      | 5     | 5    | 5     | 5      | а   | а   | а   | а   | а   | а   | а   | a   |
| 32            |                                  |     |     |     |        |        | 5   | 5   | 5      | 5     | 5    | 5     | 5      | 5   | 5   | а   | а   | а   | а   | а   | а   |
| 34            |                                  |     |     |     |        |        |     | 6   | 5      | 5     | 5    | 5     | 5      | 5   | 5   | 5   | 5   | а   | а   | а   | а   |
| 36            |                                  |     |     |     |        |        |     |     | 6      | 6     | 6    | 6     | 5      | 5   | 5   | 5   | 5   | 5   | 5   | а   | а   |
| 38            |                                  |     |     |     |        |        |     |     |        |       | 7    | 6     | 6      | 6   | 6   | 6   | 6   | 6   | 5   | 5   | 5   |
| 40            |                                  |     |     | No  | ot Ace | ceptab | ole |     |        |       |      | 8     | 8      | 8   | 7   | 6   | 6   | 6   | 6   | 6   | 6   |
| 41            |                                  |     |     |     | C      |        |     |     |        |       |      | 9     | 9      | 9   | 8   | 8   | 8   | 8   | 8   | 8   | 8   |
| 42            |                                  |     |     | N   | lot Ar | nalyze | ed  |     |        |       |      |       | 10     | 9   | 9   | 9   | 9   | 9   | 9   | 8   | 8   |
| 43            |                                  |     |     |     |        |        |     |     |        |       |      |       | 10     | 10  | 10  | 10  | 10  | 9   | 9   | 9   | 9   |
| 44            |                                  |     |     |     |        |        |     |     |        |       |      |       |        | 11  | 11  | 11  | 11  | 10  | 10  | 10  | 10  |
| 45            |                                  |     |     |     |        |        |     |     |        |       |      |       |        | 12  | 12  | 11  | 11  | 11  | 11  | 11  | 11  |

a) Minimum Cooling Time 5 years, and Minimum 2350 ppm soluble boron required in the DSC cavity water during loading or unloading.

Notes:

- Use burnup and enrichment to lookup minimum cooling time in years. Licensee is responsible for ensuring that uncertainties in fuel enrichment and burnup are correctly accounted for during fuel qualification.
- Round burnup UP to next higher entry, round enrichments DOWN to next lower entry.
- Fuel with an initial enrichment less than 2.0 wt. % U-235 must be qualified for storage using the alternate nuclear parameters specified in Table 1-1a. Fuel with an initial enrichment greater than 4.0 wt. % U-235 is unacceptable for storage.
- Fuel with a burnup greater than 45 GWd/MTU is unacceptable for storage.
- Example: An assembly with an initial enrichment of 3.65 wt. % U-235 and a burnup of 42.5 GW d/MTU is acceptable for storage after a ten-year cooling time as defined at the intersection of 3.6 wt. % U-235 (rounding down) and 43 GW d/MTU (rounding up) on the qualification table.

## Table 1-2bBWR Fuel Qualification Table for the Standardized NUHOMS®-52B DSC

(Minimum required years of cooling time after reactor core discharge)

| Burnup       |     |     |     |        |          |      |     | Ini | tial Ei | arichi | nent ( | wt. % | 6 U-2 | 35) |     |     |     |     |     |     |     |
|--------------|-----|-----|-----|--------|----------|------|-----|-----|---------|--------|--------|-------|-------|-----|-----|-----|-----|-----|-----|-----|-----|
| (GWď<br>MTU) | 2.0 | 2.1 | 2.2 | 2.3    | 2.4      | 2.5  | 2.6 | 2.7 | 2.8     | 2.9    | 3.0    | 3.1   | 3.2   | 3.3 | 3.4 | 3.5 | 3.6 | 3.7 | 3.8 | 3.9 | 4.0 |
| 15           | 3   | 3   | 3   | 3      | 3        | 3    | 3   | 3   | 3       | 3      | 3      | 3     | 3     | 3   | 3   | 3   | 3   | 3   | 3   | 3   | 3   |
| 20           | 5   | 5   | 5   | 5      | 5        | 5    | 5   | 5   | 5       | 5      | 5      | 5     | 5     | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   |
| 25           | 5   | 5   | 5   | 5      | 5        | 5    | 5   | 5   | 5       | 5      | 5      | 5     | 5     | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   |
| 30           |     |     |     | 5      | 5        | 5    | 5   | 5   | 5       | 5      | 5      | 5     | 5     | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   |
| 32           |     |     |     |        | б        | б    | б   | 5   | 5       | 5      | 5      | 5     | 5     | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   |
| 34           |     |     |     |        |          | 8    | 8   | 8   | 8       | 8      | 8      | 8     | 8     | 7   | б   | 6   | 6   | 6   | б   | 6   | 6   |
| 35           |     |     |     |        |          |      | 10  | 10  | 10      | 10     | 9      | 8     | 8     | 8   | 8   | 8   | 8   | 8   | 6   | 6   | 6   |
| 36           |     |     |     |        |          |      | 11  | 11  | 11      | 11     | 11     | 10    | 10    | 10  | 10  | 10  | 10  | 9   | 8   | 8   | 8   |
| 37           |     |     |     |        |          |      |     | 13  | 13      | 12     | 12     | 12    | 12    | 11  | 11  | 11  | 11  | 11  | 10  | 10  | 10  |
| 38           |     |     |     |        |          |      |     | 15  | 14      | 14     | 14     | 13    | 13    | 13  | 13  | 12  | 12  | 12  | 12  | 12  | 11  |
| 39           |     |     | No  | ot Acc | : ep tal | ble  |     | 18  | 17      | 17     | 16     | 16    | 16    | 15  | 14  | 14  | 14  | 14  | 13  | 13  | 13  |
| 40           |     |     |     |        | Г        |      |     |     | 21      | 21     | 20     | 20    | 19    | 18  | 17  | 17  | 16  | 16  | 16  | 16  | 15  |
| 42           |     |     | N   | ot Ar  | nalyze   | ed 👘 |     |     |         | 22     | 22     | 22    | 21    | 21  | 20  | 20  | 20  | 19  | 18  | 17  | 17  |
| 44           |     |     |     |        |          |      |     |     |         | 24     | 24     | 23    | 23    | 23  | 22  | 22  | 21  | 21  | 21  | 20  | 20  |
| 45           |     |     |     |        |          |      |     |     |         |        | 25     | 24    | 24    | 23  | 23  | 23  | 22  | 22  | 22  | 21  | 21  |

Notes:

- Use burnup and enrichment to lookup minimum cooling time in years. Licensee is responsible for ensuring that uncertainties in fuel enrichment and burnup are correctly accounted for during fuel qualification.
- Round burnup UP to next higher entry, round enrichments DOWN to next lower entry.
- Fuel with an initial enrichment less than 2.0 wt. % U-235 must be qualified for storage using the alternate nuclear parameters specified in Table 1-1b. Fuel with an initial enrichment greater than 4.0 wt. % U-235 is unacceptable for storage.
- Fuel with a burnup greater than 45 GW d/MTU is unacceptable for storage. Fuel with a burnup less than 15 Gwd/MTU is acceptable after three years cooling time provided the physical parameters from Table 1-1b have been met.
- Example: An assembly with an initial enrichment of 3.05 wt. % U-235 and a burnup of 34.5 GWd/MTU is acceptable for storage after a nine-year cooling time as defined at the intersection of 3.0 wt. % U-235 (rounding down) and 35 GWd/MTU (rounding up) on the qualification table.

## Table 1-2c PWR Fuel Qualification Table for the Standardized NUHOMS®-24P DSC (Fuel With BPRAs)

| Burnup       |     |     |     |     |        |        |      | Ini | tial Es | nricht | nent ( | (wt. % | 6 U-2 | 35) |     |     |     |     |     |     |     |
|--------------|-----|-----|-----|-----|--------|--------|------|-----|---------|--------|--------|--------|-------|-----|-----|-----|-----|-----|-----|-----|-----|
| (GWď<br>MTU) | 2.0 | 2.1 | 2.2 | 2.3 | 2.4    | 2.5    | 2.6  | 2.7 | 2.8     | 2.9    | 3.0    | 3.1    | 3.2   | 3.3 | 3.4 | 3.5 | 3.6 | 3.7 | 3.8 | 3.9 | 4.0 |
| 10           | a   | a   | a   | a   | a      | a      | a    | a   | a       | a      | a      | a      | a     | a   | a   | a   | a   | a   | a   | a   | a   |
| 15           | 5   | 5   | a   | a   | a      | a      | a    | a   | a       | a      | a      | a      | a     | a   | a   | a   | a   | a   | a   | a   | a   |
| 20           | 5   | 5   | 5   | 5   | 5      | a      | a    | a   | a       | a      | a      | a      | a     | a   | a   | a   | a   | a   | a   | a   | a   |
| 25           |     | 5   | 5   | 5   | 5      | 5      | 5    | 5   | 5       | a      | a      | a      | a     | a   | a   | a   | a   | a   | a   | a   | a   |
| 28           |     |     |     | 5   | 5      | 5      | 5    | 5   | 5       | 5      | 5      | 5      | a     | a   | a   | a   | a   | a   | a   | a   | a   |
| 30           |     |     |     |     |        | б      | 6    | 6   | 5       | 5      | 5      | 5      | 5     | a   | a   | a   | a   | a   | a   | a   | a   |
| 32           |     |     |     |     |        |        | 6    | 6   | б       | 6      | 6      | б      | 5     | 5   | 5   | a   | a   | a   | a   | a   | a   |
| 34           |     |     |     |     |        |        |      | 7   | 6       | б      | 6      | б      | б     | б   | б   | б   | б   | a   | a   | a   | a   |
| 36           |     |     |     |     |        |        |      |     | 8       | 7      | 7      | 7      | 6     | 6   | 6   | 6   | 6   | 6   | 6   | a   | a   |
| 38           |     |     |     |     |        |        |      |     |         |        | 8      | 8      | 7     | 7   | 7   | 7   | 6   | 6   | 6   | 6   | 6   |
| 40           |     |     |     | No  | t Ace  | æp tal | ble  |     |         |        |        | 9      | 9     | 8   | 8   | 8   | 7   | 7   | 7   | 7   | 6   |
| 41           |     |     |     |     | 0      |        |      |     |         |        |        | 10     | 9     | 9   | 9   | 9   | 8   | 8   | 8   | 8   | 8   |
| 42           |     |     |     | N   | iot Ar | lalyze | al 🛛 |     |         |        |        |        | 10    | 10  | 9   | 9   | 9   | 9   | 9   | 9   | 9   |
| 43           |     |     |     |     |        |        |      |     |         |        |        |        | 11    | 11  | 11  | 10  | 10  | 10  | 10  | 9   | 9   |
| 44           |     |     |     |     |        |        |      |     |         |        |        |        |       | 12  | 11  | 11  | 11  | 11  | 10  | 10  | 10  |
| 45           |     |     |     |     |        |        |      |     |         |        |        |        |       | 13  | 12  | 12  | 12  | 11  | 11  | 11  | 11  |

(Minimum required years of cooling time after reactor core discharge)

a) Minimum Cooling Time 5 years, and Minimum 2350 ppm soluble boron required in the DSC cavity water during loading or unloading.

Notes:

- BPRA Burnup shall not exceed that of a BPRA irradiated in fuel assemblies with a total burnup of 36,000 Mwd/MTU.
- Minimum cooling time for a BPRA is 5 years for B&W designs and 10 years for Westinghouse designs, regardless of the required assembly cooling time.
- Use burnup and enrichment to lookup minimum cooling time in years. Licensee is responsible for ensuring that uncertainties in fuel enrichment and burnup are correctly accounted for during fuel qualification.
- Round burnup UP to next higher entry, round enrichments DOWN to next lower entry.
- Fuel with an initial enrichment less than 2.0 wt. % U-235 must be qualified for storage using the alternate nuclear parameters specified in Table 1-1a. Fuel with an initial enrichment greater than 4.0 wt. % U-235 is unacceptable for storage.
- Fuel with a burnup greater than 45 GWd/MTU is unacceptable for storage.
- Example: An assembly with an initial enrichment of 3.65 wt. % U-235 and a burnup of 42.5 GWd/MTU is acceptable for storage after a ten-year cooling time as defined at the intersection of 3.6 wt. % U-235 (rounding down) and 43 GWd/MTU (rounding up) on the qualification table.

## Table 1-2dPWR Fuel Qualification Table for 1.2 kW per Assembly Fuel Without BPRAs for the NUHOMS®-32PT DSC

|        |     |     |     |       |       |     |     |     |     |     |     |     | Ini | tial E | nrich | men | t wt 9 | % U-2 | 235 |     |     |     |     |     |     |     |     |     |     |     |     |
|--------|-----|-----|-----|-------|-------|-----|-----|-----|-----|-----|-----|-----|-----|--------|-------|-----|--------|-------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
| B(WIT) | 2.0 | 2.1 | 2.2 | 2.3   | 2.4   | 2.5 | 2.6 | 2.7 | 2.8 | 2.9 | 3.0 | 3.1 | 3.2 | 3.3    | 3.4   | 3.5 | 3.6    | 3.7   | 3.8 | 3.9 | 4.0 | 4.1 | 4.2 | 4.3 | 4.4 | 4.5 | 4.6 | 4.7 | 4.8 | 4.9 | 5.0 |
| 10     | 5   | 5   | 5   | 5     | 5     | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5      | 5     | 5   | 5      | 5     | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   |
| 15     | 5   | 5   | 5   | 5     | 5     | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5      | 5     | 5   | 5      | 5     | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   |
| 20     | 5   | 5   | 5   | 5     | 5     | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5      | 5     | 5   | 5      | 5     | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   |
| 25     |     | 5   | 5   | 5     | 5     | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5      | 5     | 5   | 5      | 5     | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   |
| 28     |     |     |     | 5     | 5     | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5      | 5     | 5   | 5      | 5     | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   |
| 30     |     |     |     |       |       | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5      | 5     | 5   | 5      | 5     | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   |
| 32     |     |     |     |       |       |     | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5      | 5     | 5   | 5      | 5     | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   |
| 34     |     |     |     |       |       |     |     | 5   | 5   | 5   | 5   | 5   | 5   | 5      | 5     | 5   | 5      | 5     | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   |
| 36     |     |     |     |       |       |     |     |     | 5   | 5   | 5   | 5   | 5   | 5      | 5     | 5   | 5      | 5     | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   |
| 38     |     |     |     |       |       |     |     |     |     |     | 5   | 5   | 5   | 5      | 5     | 5   | 5      | 5     | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   |
| 39     |     |     |     |       |       |     |     |     |     |     | 5   | 5   | 5   | 5      | 5     | 5   | 5      | 5     | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   |
| 40     |     |     | Nc  | ot A1 | nalyz | zed |     |     |     |     |     | 5   | 5   | 5      | 5     | 5   | 5      | 5     | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   |
| 41     |     |     |     |       |       |     |     |     |     |     |     | 5   | 5   | 5      | 5     | 5   | 5      | 5     | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   |
| 42     |     |     |     |       |       |     |     |     |     |     |     | 6   | 6   | 6      | 6     | 6   | 6      | 6     | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   |
| 43     |     |     |     |       |       |     |     |     |     |     |     |     | 6   | 6      | 6     | 6   | 6      | 6     | 6   | 6   | 6   | 6   | 6   | 6   | 6   | 5   | 5   | 5   | 5   | 5   | 5   |
| 44     |     |     |     |       |       |     |     |     |     |     |     |     |     | 6      | 6     | 6   | 6      | 6     | 6   | 6   | 6   | 6   | 6   | 6   | 6   | 6   | 6   | 6   | 6   | 6   | 6   |
| 45     |     |     |     |       |       |     |     |     |     |     |     |     |     | 6      | 6     | 6   | 6      | 6     | 6   | 6   | 6   | 6   | 6   | 6   | 6   | 6   | 6   | 6   | 6   | 6   | 6   |

(Minimum required years of cooling time after reactor core discharge)

• Use burnup and enrichment to lookup minimum cooling time in years. Licensee is responsible for ensuring that uncertainties in fuel enrichment and burnup are correctly accounted for during fuel qualification.

• Round burnup UP to next higher entry, round enrichments DOWN to next lower entry.

• Fuel with an initial enrichment less than 2.0 and greater than 5.0 wt.% U-235 is unacceptable for storage.

• Fuel with a burnup greater than 45 GW d/MTU is unacceptable for storage

• Fuel with a burnup less than 10 GW d/MTU is acceptable for storage after 5-years cooling.

• Example: An assembly with an initial enrichment of 3.75 wt. % U-235 and a burnup of 41.5 GWd/MTU is acceptable for storage after a six-year cooling time as defined by 3.7 wt. % U-235 (rounding down) and 42 GWd/MTU (rounding up) on the qualification table.

Table 1-2ePWR Fuel Qualification Table for 0.87 kW per Assembly Fuel Without BPRAs for the NUHOMS®-32PT DSC

|        |   |     |     |       |      |     |     |     |     |     |     |     | Ini | tial E | nrich | ment | t wt % | 6 U-2 | 235 |     |     |     |     |     |     |     |     |     |     |     |     |
|--------|---|-----|-----|-------|------|-----|-----|-----|-----|-----|-----|-----|-----|--------|-------|------|--------|-------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
| B(WM)) | 2 | 2.1 | 2.2 | 2.3   | 2.4  | 2.5 | 2.6 | 2.7 | 2.8 | 2.9 | 3.0 | 3.1 | 3.2 | 3.3    | 3.4   | 3.5  | 3.6    | 3.7   | 3.8 | 3.9 | 4.0 | 4.1 | 4.2 | 4.3 | 4.4 | 4.5 | 4.6 | 4.7 | 4.8 | 4.9 | 5.0 |
| 10     | 5 | 5   | 5   | 5     | 5    | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5      | 5     | 5    | 5      | 5     | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   |
| 15     | 5 | 5   | 5   | 5     | 5    | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5      | 5     | 5    | 5      | 5     | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   |
| 20     | 5 | 5   | 5   | 5     | 5    | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5      | 5     | 5    | 5      | 5     | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   |
| 25     |   | 5   | 5   | 5     | 5    | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5      | 5     | 5    | 5      | 5     | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   |
| 28     |   |     |     | 5     | 5    | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5      | 5     | 5    | 5      | 5     | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   |
| 30     |   |     |     |       |      | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5      | 5     | 5    | 5      | 5     | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   |
| 32     |   |     |     |       |      |     | 6   | 6   | 5   | 5   | 5   | 5   | 5   | 5      | 5     | 5    | 5      | 5     | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   |
| 34     |   |     |     |       |      |     |     | 6   | 6   | 6   | 6   | 6   | 6   | 6      | 6     | 6    | 6      | 6     | 6   | 6   | 6   | 6   | 6   | 6   | 6   | 6   | 6   | 6   | 6   | 5   | 5   |
| 36     |   |     |     |       |      |     |     |     | 6   | 6   | 6   | 6   | 6   | 6      | 6     | 6    | 6      | 6     | 6   | 6   | 6   | 6   | 6   | 6   | 6   | 6   | 6   | 6   | 6   | 6   | 6   |
| 38     |   |     |     |       |      |     |     |     |     |     | 7   | 7   | 7   | 7      | 7     | 7    | 7      | 7     | 7   | 7   | 7   | 7   | 7   | 7   | 7   | 7   | 6   | 6   | 6   | 6   | 6   |
| 39     |   |     |     |       |      |     |     |     |     |     | 7   | 7   | 7   | 7      | 7     | 7    | 7      | 7     | 7   | 7   | 7   | 7   | 7   | 7   | 7   | 7   | 7   | 7   | 7   | 7   | 7   |
| 40     |   |     | Ν   | ot Ar | alyz | ed  |     |     |     |     |     | 8   | 8   | 8      | 7     | 7    | 7      | 7     | 7   | 7   | 7   | 7   | 7   | 7   | 7   | 7   | 7   | 7   | 7   | 7   | 7   |
| 41     |   |     |     |       |      |     |     |     |     |     |     | 8   | 8   | 8      | 8     | 8    | 8      | 8     | 8   | 8   | 8   | 8   | 8   | 7   | 7   | 7   | 7   | 7   | 7   | 7   | 7   |
| 42     |   |     |     |       |      |     |     |     |     |     |     | 8   | 8   | 8      | 8     | 8    | 8      | 8     | 8   | 8   | 8   | 8   | 8   | 8   | 8   | 8   | 8   | 8   | 8   | 8   | 8   |
| 43     |   |     |     |       |      |     |     |     |     |     |     |     | 9   | 9      | 9     | 9    | 9      | 9     | 9   | 8   | 8   | 8   | 8   | 8   | 8   | 8   | 8   | 8   | 8   | 8   | 8   |
| 44     |   |     |     |       |      |     |     |     |     |     |     |     |     | 9      | 9     | 9    | 9      | 9     | 9   | 9   | 9   | 9   | 9   | 9   | 9   | 9   | 9   | 9   | 9   | 8   | 8   |
| 45     |   |     |     |       |      |     |     |     |     |     |     |     |     | 10     | 10    | 10   | 10     | 10    | 10  | 9   | 9   | 9   | 9   | 9   | 9   | 9   | 9   | 9   | 9   | 9   | 9   |

• Use burnup and enrichment to lookup minimum cooling time in years. Licensee is responsible for ensuring that uncertainties in fuel enrichment and burnup are correctly accounted for during fuel qualification.

• Round burnup UP to next higher entry, round enrichments DOWN to next lower entry.

• Fuel with an initial enrichment less than 2.0 and greater than 5.0 wt.% U-235 is unacceptable for storage.

• Fuel with a burnup greater than 45 GW d/MTU is unacceptable for storage

• Fuel with a burnup less than 10 GWd/MTU is acceptable for storage after 5-years cooling.

• Example: An assembly with an initial enrichment of 3.75 wt. % U-235 and a burnup of 41.5 GW d/MTU is acceptable for storage after an eight-year cooling time as defined by 3.7 wt. % U-235 (rounding down) and 42 GW d/MTU (rounding up) on the qualification table.

Table 1-2fPWR Fuel Qualification Table for 0.7 kW Fuel Without BPRAs per Assembly for the NUHOMS®-32PT DSC

|         |     |     |     |       |      |     |     |     |     |     |     |     | Ini | tial E | nrich | ment | t wt % | 6 U-2 | 235 |     |     |     |     |     |     |     |     |     |     |     |    |
|---------|-----|-----|-----|-------|------|-----|-----|-----|-----|-----|-----|-----|-----|--------|-------|------|--------|-------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|----|
| B(GWAT) | 2.0 | 2.1 | 2.2 | 2.3   | 2.4  | 2.5 | 2.6 | 2.7 | 2.8 | 2.9 | 3.0 | 3.1 | 3.2 | 3.3    | 3.4   | 3.5  | 3.6    | 3.7   | 3.8 | 3.9 | 4.0 | 4.1 | 4.2 | 4.3 | 4.4 | 4.5 | 4.6 | 4.7 | 4.8 | 4.9 | 5  |
| 10      | 5   | 5   | 5   | 5     | 5    | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5      | 5     | 5    | 5      | 5     | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5  |
| 15      | 5   | 5   | 5   | 5     | 5    | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5      | 5     | 5    | 5      | 5     | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5  |
| 20      | 5   | 5   | 5   | 5     | 5    | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5      | 5     | 5    | 5      | 5     | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5  |
| 25      |     | 5   | 5   | 5     | 5    | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5      | 5     | 5    | 5      | 5     | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5  |
| 28      |     |     |     | 6     | 6    | 6   | 6   | 6   | 6   | 6   | 6   | 6   | 6   | 6      | 6     | 6    | 6      | 6     | 6   | 6   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5  |
| 30      |     |     |     |       |      | 6   | 6   | 6   | 6   | 6   | 6   | 6   | 6   | 6      | 6     | 6    | 6      | 6     | 6   | 6   | 6   | 6   | 6   | 6   | 6   | 6   | 6   | 6   | 6   | 6   | 6  |
| 32      |     |     |     |       |      |     | 7   | 7   | 7   | 7   | 7   | 7   | 7   | 7      | 7     | 7    | 7      | 7     | 7   | 7   | 7   | 7   | 7   | 7   | 7   | 7   | 7   | 6   | 6   | 6   | 6  |
| 34      |     |     |     |       |      |     |     | 8   | 8   | 8   | 8   | 8   | 8   | 8      | 8     | 8    | 7      | 7     | 7   | 7   | 7   | 7   | 7   | 7   | 7   | 7   | 7   | 7   | 7   | 7   | 7  |
| 36      |     |     |     |       |      |     |     |     | 9   | 9   | 9   | 9   | 9   | 9      | 8     | 8    | 8      | 8     | 8   | 8   | 8   | 8   | 8   | 8   | 8   | 8   | 8   | 8   | 8   | 8   | 8  |
| 38      |     |     |     |       |      |     |     |     |     |     | 10  | 10  | 10  | 10     | 10    | 10   | 10     | 9     | 9   | 9   | 9   | 9   | 9   | 9   | 9   | 9   | 9   | 9   | 9   | 9   | 9  |
| 39      |     |     |     |       |      |     |     |     |     |     | 11  | 11  | 10  | 10     | 10    | 10   | 10     | 10    | 10  | 10  | 10  | 10  | 10  | 10  | 10  | 10  | 10  | 10  | 10  | 10  | 10 |
| 40      |     |     | Ne  | ot Ar | alyz | ed  |     |     |     |     |     | 11  | 11  | 11     | 11    | 11   | 11     | 11    | 11  | 11  | 11  | 11  | 11  | 11  | 11  | 10  | 10  | 10  | 10  | 10  | 10 |
| 41      |     |     |     |       |      |     |     |     |     |     |     | 12  | 12  | 12     | 12    | 12   | 12     | 12    | 12  | 12  | 12  | 11  | 11  | 11  | 11  | 11  | 11  | 11  | 11  | 11  | 11 |
| 42      |     |     |     |       |      |     |     |     |     |     |     | 13  | 13  | 13     | 13    | 13   | 13     | 13    | 13  | 12  | 12  | 12  | 12  | 12  | 12  | 12  | 12  | 12  | 12  | 12  | 12 |
| 43      |     |     |     |       |      |     |     |     |     |     |     |     | 14  | 14     | 14    | 14   | 14     | 14    | 14  | 13  | 13  | 13  | 13  | 13  | 13  | 13  | 13  | 13  | 13  | 13  | 13 |
| 44      |     |     |     |       |      |     |     |     |     |     |     |     |     | 15     | 15    | 15   | 15     | 15    | 15  | 15  | 14  | 14  | 14  | 14  | 14  | 14  | 14  | 14  | 14  | 14  | 14 |
| 45      |     |     |     |       |      |     |     |     |     |     |     |     |     | 16     | 16    | 16   | 16     | 16    | 16  | 16  | 15  | 15  | 15  | 15  | 15  | 15  | 15  | 15  | 15  | 15  | 15 |

• Use burnup and enrichment to lookup minimum cooling time in years. Licensee is responsible for ensuring that uncertainties in fuel enrichment and burnup are correctly accounted for during fuel qualification.

Round burnup UP to next higher entry, round enrichments DOWN to next lower entry.

Fuel with an initial enrichment less than 2.0 and greater than 5.0 wt.% U-235 is unacceptable for storage.

Fuel with a burnup greater than 45 GWd/MTU is unacceptable for storage

Fuel with a burnup less than 10 GWd/MTU is acceptable for storage after 5-years cooling.

Example: An assembly with an initial enrichment of 3.75 wt. % U-235 and a burnup of 41.5 GWd/MTU is acceptable for storage after a thirteen-year cooling time as defined

by 3.7 wt. % U-235 (rounding down) and 42 GWd/MTU (rounding up) on the qualification table.

Table 1-2gPWR Fuel Qualification Table for 0.63 kW per Assembly Fuel Without BPRAs for the NUHOMS®-32PT DSC

|          |   |     |     |        |        |     |     |     |     |     |     |     | Ini | tial E | nrich | ment | wt % | 6 U-2 | 235 |     |     |     |     |     |     |     |     |     |     |     |    |
|----------|---|-----|-----|--------|--------|-----|-----|-----|-----|-----|-----|-----|-----|--------|-------|------|------|-------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|----|
| B.(GWNI) | 2 | 2.1 | 2.2 | 2.3    | 2.4    | 2.5 | 2.6 | 2.7 | 2.8 | 2.9 | 3.0 | 3.1 | 3.2 | 3.3    | 3.4   | 3.5  | 3.6  | 3.7   | 3.8 | 3.9 | 4.0 | 4.1 | 4.2 | 4.3 | 4.4 | 4.5 | 4.6 | 4.7 | 4.8 | 4.9 | 5  |
| 10       | 5 | 5   | 5   | 5      | 5      | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5      | 5     | 5    | 5    | 5     | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5  |
| 15       | 5 | 5   | 5   | 5      | 5      | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5      | 5     | 5    | 5    | 5     | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5  |
| 20       | 5 | 5   | 5   | 5      | 5      | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5      | 5     | 5    | 5    | 5     | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5  |
| 25       |   | 6   | 6   | 6      | 6      | 6   | 6   | 6   | 6   | 6   | 5   | 5   | 5   | 5      | 5     | 5    | 5    | 5     | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5  |
| 28       |   |     |     | 7      | 7      | 7   | 6   | 6   | 6   | 6   | 6   | 6   | 6   | 6      | 6     | 6    | 6    | 6     | 6   | 6   | 6   | 6   | 6   | 6   | 6   | 6   | 6   | 6   | 6   | 6   | 6  |
| 30       |   |     |     |        |        | 7   | 7   | 7   | 7   | 7   | 7   | 7   | 7   | 7      | 7     | 7    | 7    | 7     | 7   | 7   | 7   | 7   | 7   | 7   | 7   | 7   | 7   | 7   | 7   | 7   | 7  |
| 32       |   |     |     |        |        |     | 8   | 8   | 8   | 8   | 8   | 8   | 8   | 8      | 8     | 8    | 8    | 8     | 8   | 8   | 8   | 8   | 8   | 8   | 8   | 8   | 8   | 8   | 8   | 8   | 7  |
| 34       |   |     |     |        |        |     |     | 9   | 9   | 9   | 9   | 9   | 9   | 9      | 9     | 9    | 9    | 9     | 9   | 9   | 9   | 9   | 9   | 9   | 9   | 9   | 9   | 9   | 9   | 9   | 9  |
| 36       |   |     |     |        |        |     |     |     | 11  | 11  | 11  | 11  | 11  | 10     | 10    | 10   | 10   | 10    | 10  | 10  | 10  | 10  | 10  | 10  | 10  | 10  | 10  | 10  | 10  | 10  | 10 |
| 38       |   |     |     |        |        |     |     |     |     |     | 13  | 12  | 12  | 12     | 12    | 12   | 12   | 12    | 12  | 12  | 12  | 12  | 12  | 12  | 12  | 12  | 12  | 11  | 11  | 11  | 11 |
| 39       |   |     |     |        |        |     |     |     |     |     | 14  | 13  | 13  | 13     | 13    | 13   | 13   | 13    | 13  | 13  | 13  | 13  | 13  | 13  | 13  | 13  | 13  | 12  | 12  | 12  | 12 |
| 40       |   |     | ľ   | Not Ai | nalyze | ed  |     |     |     |     |     | 15  | 15  | 14     | 14    | 14   | 14   | 14    | 14  | 14  | 14  | 14  | 14  | 14  | 14  | 14  | 14  | 13  | 13  | 13  | 13 |
| 41       |   |     |     |        |        |     |     |     |     |     |     | 16  | 16  | 16     | 16    | 15   | 15   | 15    | 15  | 15  | 15  | 15  | 15  | 15  | 15  | 15  | 15  | 15  | 15  | 15  | 14 |
| 42       |   |     |     |        |        |     |     |     |     |     |     | 17  | 17  | 17     | 17    | 17   | 17   | 16    | 16  | 16  | 16  | 16  | 16  | 16  | 16  | 16  | 16  | 16  | 16  | 16  | 16 |
| 43       |   |     |     |        |        |     |     |     |     |     |     |     | 18  | 18     | 18    | 18   | 18   | 18    | 18  | 18  | 18  | 17  | 17  | 17  | 17  | 17  | 17  | 17  | 17  | 17  | 17 |
| 44       |   |     |     |        |        |     |     |     |     |     |     |     |     | 20     | 19    | 19   | 19   | 19    | 19  | 19  | 19  | 19  | 19  | 19  | 18  | 18  | 18  | 18  | 18  | 18  | 18 |
| 45       |   |     |     |        |        |     |     |     |     |     |     |     |     | 21     | 21    | 21   | 21   | 20    | 20  | 20  | 20  | 20  | 20  | 20  | 20  | 20  | 20  | 20  | 20  | 19  | 19 |

Use burnup and enrichment to lookup minimum cooling time in years. Licensee is responsible for ensuring that uncertainties in fuel enrichment and burnup are correctly

accounted for during fuel qualification.

Round burnup UP to next higher entry, round enrichments DOWN to next lower entry.

Fuel with an initial enrichment less than 2.0 and greater than 5.0 wt.% U-235 is unacceptable for storage.

Fuel with a burnup greater than 45 GWd/MTU is unacceptable for storage

Fuel with a burnup less than 10 GWd/MTU is acceptable for storage after 5-years cooling.

Example: An assembly with an initial enrichment of 3.75 wt. % U-235 and a burnup of 41.5 GWd/MTU is acceptable for storage after a sixteen-year cooling time as defined

by 3.7 wt. % U-235 (rounding down) and 42 GWd/MTU (rounding up) on the qualification table.

 Table 1-2h

 PWR Fuel Qualification Table for 0.6 kW per Assembly Fuel Without BPRAs for the NUHOMS®-32PT DSC

| B.GWM  |     |     |     |       |      |     |     |     |     |     |     |     | Ini | tial E | nrich | men | twt % | 6 U-2 | 235 |     |     |     |     |     |     |     |     |     |     |     |    |
|--------|-----|-----|-----|-------|------|-----|-----|-----|-----|-----|-----|-----|-----|--------|-------|-----|-------|-------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|----|
| D(WWI) | 2.0 | 2.1 | 2.2 | 2.3   | 2.4  | 2.5 | 2.6 | 2.7 | 2.8 | 2.9 | 3.0 | 3.1 | 3.2 | 3.3    | 3.4   | 3.5 | 3.6   | 3.7   | 3.8 | 3.9 | 4.0 | 4.1 | 4.2 | 4.3 | 4.4 | 4.5 | 4.6 | 4.7 | 4.8 | 4.9 | 5  |
| 10     | 5   | 5   | 5   | 5     | 5    | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5      | 5     | 5   | 5     | 5     | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5  |
| 15     | 5   | 5   | 5   | 5     | 5    | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5      | 5     | 5   | 5     | 5     | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5  |
| 20     | 5   | 5   | 5   | 5     | 5    | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5      | 5     | 5   | 5     | 5     | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5  |
| 25     |     | 6   | 6   | 6     | 6    | 6   | 6   | 6   | 6   | 6   | 6   | 6   | 6   | 6      | 6     | 6   | 6     | 6     | 6   | 6   | 6   | 6   | 6   | 6   | 6   | 6   | 6   | 5   | 5   | 5   | 5  |
| 28     |     |     |     | 7     | 7    | 7   | 7   | 7   | 7   | 7   | 7   | 7   | 7   | 7      | 7     | 7   | 7     | 7     | 7   | 7   | 7   | 7   | 6   | 6   | 6   | 6   | 6   | 6   | 6   | 6   | 6  |
| 30     |     |     |     |       |      | 8   | 8   | 8   | 8   | 8   | 8   | 8   | 8   | 8      | 8     | 7   | 7     | 7     | 7   | 7   | 7   | 7   | 7   | 7   | 7   | 7   | 7   | 7   | 7   | 7   | 7  |
| 32     |     |     |     |       |      |     | 9   | 9   | 9   | 9   | 9   | 9   | 9   | 9      | 9     | 9   | 8     | 8     | 8   | 8   | 8   | 8   | 8   | 8   | 8   | 8   | 8   | 8   | 8   | 8   | 8  |
| 34     |     |     |     |       |      |     |     | 10  | 10  | 10  | 10  | 10  | 10  | 10     | 10    | 10  | 10    | 10    | 10  | 10  | 10  | 10  | 10  | 10  | 10  | 9   | 9   | 9   | 9   | 9   | 9  |
| 36     |     |     |     |       |      |     |     |     | 12  | 12  | 12  | 12  | 12  | 12     | 12    | 12  | 12    | 11    | 11  | 11  | 11  | 11  | 11  | 11  | 11  | 11  | 11  | 11  | 11  | 11  | 11 |
| 38     |     |     |     |       |      |     |     |     |     |     | 14  | 14  | 14  | 14     | 14    | 14  | 14    | 14    | 14  | 13  | 13  | 13  | 13  | 13  | 13  | 13  | 13  | 13  | 13  | 13  | 13 |
| 39     |     |     |     |       |      |     |     |     |     |     | 15  | 15  | 15  | 15     | 15    | 15  | 15    | 15    | 15  | 15  | 15  | 15  | 14  | 14  | 14  | 14  | 14  | 14  | 14  | 14  | 14 |
| 40     |     |     | No  | ot An | alyz | ed  |     |     |     |     |     | 17  | 16  | 16     | 16    | 16  | 16    | 16    | 16  | 16  | 16  | 16  | 16  | 16  | 16  | 15  | 15  | 15  | 15  | 15  | 15 |
| 41     |     |     |     |       |      |     |     |     |     |     |     | 18  | 18  | 18     | 18    | 18  | 17    | 17    | 17  | 17  | 17  | 17  | 17  | 17  | 17  | 17  | 17  | 17  | 17  | 17  | 16 |
| 42     |     |     |     |       |      |     |     |     |     |     |     | 19  | 19  | 19     | 19    | 19  | 19    | 19    | 19  | 19  | 18  | 18  | 18  | 18  | 18  | 18  | 18  | 18  | 18  | 18  | 18 |
| 43     |     |     |     |       |      |     |     |     |     |     |     |     | 21  | 20     | 20    | 20  | 20    | 20    | 20  | 20  | 20  | 20  | 20  | 20  | 20  | 19  | 19  | 19  | 19  | 19  | 19 |
| 44     |     |     |     |       |      |     |     |     |     |     |     |     |     | 22     | 22    | 22  | 22    | 21    | 21  | 21  | 21  | 21  | 21  | 21  | 21  | 21  | 21  | 21  | 21  | 20  | 20 |
| 45     |     |     |     |       |      |     |     |     |     |     |     |     |     | 23     | 23    | 23  | 23    | 23    | 23  | 23  | 23  | 22  | 22  | 22  | 22  | 22  | 22  | 22  | 22  | 22  | 22 |

• Use burnup and enrichment to lookup minimum cooling time in years. Licensee is responsible for ensuring that uncertainties in fuel enrichment and burnup are correctly accounted for during fuel qualification.

Round burnup UP to next higher entry, round enrichments DOWN to next lower entry.

Fuel with an initial enrichment less than 2.0 and greater than 5.0 wt.% U-235 is unacceptable for storage.

Fuel with a burnup greater than 45 GWd/MTU is unacceptable for storage

Fuel with a burnup less than 10 GWd/MTU is acceptable for storage after 5-years cooling.

• Example: An assembly with an initial enrichment of 3.75 wt. % U-235 and a burnup of 41.5 GWd/MTU is acceptable for storage after a nineteen-year cooling time as defined by 3.7 wt. % U-235 (rounding down) and 42 GWd/MTU (rounding up) on the qualification table.

# Table 1-2iPWR Fuel Qualification Table for 1.2 kW per Assembly Fuel With BPRAs for the NUHOMS®-32PT DSC

|           |   |     |     |       |      |     |     |     |     |     |     |     | Iı  | nitial | Enrich | nment | wt % | U-23 | 35  |     |     |     |     |     |     |     |     |     |     |     |   |
|-----------|---|-----|-----|-------|------|-----|-----|-----|-----|-----|-----|-----|-----|--------|--------|-------|------|------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|---|
| B (SWM)() | 2 | 2.1 | 2.2 | 2.3   | 2.4  | 2.5 | 2.6 | 2.7 | 2.8 | 2.9 | 3.0 | 3.1 | 3.2 | 3.3    | 3.4    | 3.5   | 3.6  | 3.7  | 3.8 | 3.9 | 4.0 | 4.1 | 4.2 | 4.3 | 4.4 | 4.5 | 4.6 | 4.7 | 4.8 | 4.9 | 5 |
| 10        | 5 | 5   | 5   | 5     | 5    | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5      | 5      | 5     | 5    | 5    | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5 |
| 15        | 5 | 5   | 5   | 5     | 5    | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5      | 5      | 5     | 5    | 5    | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5 |
| 20        | 5 | 5   | 5   | 5     | 5    | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5      | 5      | 5     | 5    | 5    | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5 |
| 25        |   | 5   | 5   | 5     | 5    | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5      | 5      | 5     | 5    | 5    | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5 |
| 28        |   |     |     | 5     | 5    | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5      | 5      | 5     | 5    | 5    | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5 |
| 30        |   |     |     |       |      | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5      | 5      | 5     | 5    | 5    | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5 |
| 32        |   |     |     |       |      |     | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5      | 5      | 5     | 5    | 5    | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5 |
| 34        |   |     |     |       |      |     |     | 5   | 5   | 5   | 5   | 5   | 5   | 5      | 5      | 5     | 5    | 5    | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5 |
| 36        |   |     |     |       |      |     |     |     | 5   | 5   | 5   | 5   | 5   | 5      | 5      | 5     | 5    | 5    | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5 |
| 38        |   |     |     |       |      |     |     |     |     |     | 5   | 5   | 5   | 5      | 5      | 5     | 5    | 5    | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5 |
| 39        |   |     |     |       |      |     |     |     |     |     | 5   | 5   | 5   | 5      | 5      | 5     | 5    | 5    | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5 |
| 40        |   |     | N   | ot Ar | alyz | ed  |     |     |     |     |     | 5   | 5   | 5      | 5      | 5     | 5    | 5    | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5 |
| 41        |   |     |     |       |      |     |     |     |     |     |     | 6   | 6   | 5      | 5      | 5     | 5    | 5    | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5 |
| 42        |   |     |     |       |      |     |     |     | -   |     |     | 6   | 6   | 6      | 6      | 6     | 6    | 6    | 6   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5 |
| 43        |   |     |     |       |      |     |     |     | -   |     |     |     | 6   | 6      | 6      | 6     | 6    | 6    | 6   | 6   | 6   | 6   | 6   | 6   | 6   | 6   | 6   | 6   | 5   | 5   | 5 |
| 44        |   |     |     |       |      |     |     |     |     |     |     |     |     | 6      | 6      | 6     | 6    | 6    | 6   | 6   | 6   | 6   | 6   | 6   | 6   | 6   | 6   | 6   | 6   | 6   | 6 |
| 45        |   |     |     |       |      |     |     |     |     |     |     |     |     | 6      | 6      | 6     | 6    | 6    | 6   | 6   | 6   | 6   | 6   | 6   | 6   | 6   | 6   | 6   | 6   | 6   | 6 |

(Minimum required years of cooling time after reactor core discharge)

• Use burnup and enrichment to lookup minimum cooling time in years. Licensee is responsible for ensuring that uncertainties in fuel enrichment and burnup are correctly accounted for during fuel qualification.

Round burnup UP to next higher entry, round enrichments DOWN to next lower entry.

Fuel with an initial enrichment less than 2.0 and greater than 5.0 wt.% U-235 is unacceptable for storage.

Fuel with a burnup greater than 45 GWd/MTU is unacceptable for storage

Fuel with a burnup less than 10 GWd/MTU is acceptable for storage after 5-years cooling

Example: An assembly with an initial enrichment of 3.75 wt. % U-235 and a burnup of 41.5 GWd/MTU is acceptable for storage after a six-year cooling time as defined by

3.7 wt. % U-235 (rounding down) and 42 GWd/MTU (rounding up) on the qualification table.

# Table 1-2jPWR Fuel Qualification Table for 0.87 kW per Assembly Fuel With BPRAs for the NUHOMS®-32PT DSC

|          |   |     |     |       |      |     |     |     |     |     |     |     | Ini | tial E | nrich | men | t wt % | 6 U-2 | 235 |     |     |     |     |     |     |     |     |     |     |     |     |
|----------|---|-----|-----|-------|------|-----|-----|-----|-----|-----|-----|-----|-----|--------|-------|-----|--------|-------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
| B(GWANT) | 2 | 2.1 | 2.2 | 2.3   | 2.4  | 2.5 | 2.6 | 2.7 | 2.8 | 2.9 | 3.0 | 3.1 | 3.2 | 3.3    | 3.4   | 3.5 | 3.6    | 3.7   | 3.8 | 3.9 | 4.0 | 4.1 | 4.2 | 4.3 | 4.4 | 4.5 | 4.6 | 4.7 | 4.8 | 4.9 | 5.0 |
| 10       | 5 | 5   | 5   | 5     | 5    | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5      | 5     | 5   | 5      | 5     | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   |
| 15       | 5 | 5   | 5   | 5     | 5    | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5      | 5     | 5   | 5      | 5     | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   |
| 20       | 5 | 5   | 5   | 5     | 5    | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5      | 5     | 5   | 5      | 5     | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   |
| 25       |   | 5   | 5   | 5     | 5    | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5      | 5     | 5   | 5      | 5     | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   |
| 28       |   |     |     | 5     | 5    | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5      | 5     | 5   | 5      | 5     | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   |
| 30       |   |     |     |       |      | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5      | 5     | 5   | 5      | 5     | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   |
| 32       |   |     |     |       |      |     | 6   | 6   | 6   | 6   | 5   | 5   | 5   | 5      | 5     | 5   | 5      | 5     | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   |
| 34       |   |     |     |       |      |     |     | 6   | 6   | 6   | 6   | 6   | 6   | 6      | 6     | 6   | 6      | 6     | 6   | 6   | 6   | 6   | 6   | 6   | 6   | 6   | 6   | 6   | 6   | 6   | 6   |
| 36       |   |     |     |       |      |     |     |     | 7   | 6   | 6   | 6   | 6   | 6      | 6     | 6   | 6      | 6     | 6   | 6   | 6   | 6   | 6   | 6   | 6   | 6   | 6   | 6   | 6   | 6   | 6   |
| 38       |   |     |     |       |      |     |     |     |     |     | 7   | 7   | 7   | 7      | 7     | 7   | 7      | 7     | 7   | 7   | 7   | 7   | 7   | 7   | 7   | 7   | 7   | 7   | 7   | 6   | 6   |
| 39       |   |     |     |       |      |     |     |     |     |     | 7   | 7   | 7   | 7      | 7     | 7   | 7      | 7     | 7   | 7   | 7   | 7   | 7   | 7   | 7   | 7   | 7   | 7   | 7   | 7   | 7   |
| 40       |   |     | N   | ot An | alyz | ed  |     |     |     |     |     | 8   | 8   | 8      | 8     | 8   | 7      | 7     | 7   | 7   | 7   | 7   | 7   | 7   | 7   | 7   | 7   | 7   | 7   | 7   | 7   |
| 41       |   |     |     |       |      |     |     |     |     |     |     | 8   | 8   | 8      | 8     | 8   | 8      | 8     | 8   | 8   | 8   | 8   | 8   | 8   | 8   | 8   | 8   | 7   | 7   | 7   | 7   |
| 42       |   |     |     |       |      |     |     |     |     |     |     | 9   | 9   | 8      | 8     | 8   | 8      | 8     | 8   | 8   | 8   | 8   | 8   | 8   | 8   | 8   | 8   | 8   | 8   | 8   | 8   |
| 43       |   |     |     |       |      |     |     |     |     |     |     |     | 9   | 9      | 9     | 9   | 9      | 9     | 9   | 9   | 9   | 9   | 8   | 8   | 8   | 8   | 8   | 8   | 8   | 8   | 8   |
| 44       |   |     |     |       |      |     |     |     |     |     |     |     |     | 9      | 9     | 9   | 9      | 9     | 9   | 9   | 9   | 9   | 9   | 9   | 9   | 9   | 9   | 9   | 9   | 9   | 9   |
| 45       |   |     |     |       |      |     |     |     |     |     |     |     |     | 10     | 10    | 10  | 10     | 10    | 10  | 10  | 10  | 10  | 9   | 9   | 9   | 9   | 9   | 9   | 9   | 9   | 9   |

(Minimum required years of cooling time after reactor core discharge)

• Use burnup and enrichment to lookup minimum cooling time in years. Licensee is responsible for ensuring that uncertainties in fuel enrichment and burnup are correctly accounted for during fuel qualification.

Round burnup UP to next higher entry, round enrichments DOWN to next lower entry.

Fuel with an initial enrichment less than 2.0 and greater than 5.0 wt.% U-235 is unacceptable for storage.

Fuel with a burnup greater than 45 GWd/MTU is unacceptable for storage

Fuel with a burnup less than 10 GWd/MTU is acceptable for storage after 5-years cooling.

• Example: An assembly with an initial enrichment of 3.75 wt. % U-235 and a bumup of 41.5 GWd/MTU is acceptable for storage after a eight-year cooling time as defined by 3.7 wt. % U-235 (rounding down) and 42 GWd/MTU (rounding up) on the qualification table.

 Table 1-2k

 PWR Fuel Qualification Table for 0.7 kW per Assembly Fuel With BPRAs for the NUHOMS®-32PT DSC

|          |   |     |     |       |       |     |     |     |     |     |     |     | Ini | tial E | nrich | men | t wt % | 6 U-2 | 235 |     |     |     |     |     |     |     |     |     |     |     |    |
|----------|---|-----|-----|-------|-------|-----|-----|-----|-----|-----|-----|-----|-----|--------|-------|-----|--------|-------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|----|
| B(GW/II) | 2 | 2.1 | 2.2 | 2.3   | 2.4   | 2.5 | 2.6 | 2.7 | 2.8 | 2.9 | 3.0 | 3.1 | 3.2 | 3.3    | 3.4   | 3.5 | 3.6    | 3.7   | 3.8 | 3.9 | 4.0 | 4.1 | 4.2 | 4.3 | 4.4 | 4.5 | 4.6 | 4.7 | 4.8 | 4.9 | 5  |
| 10       | 5 | 5   | 5   | 5     | 5     | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5      | 5     | 5   | 5      | 5     | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5  |
| 15       | 5 | 5   | 5   | 5     | 5     | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5      | 5     | 5   | 5      | 5     | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5  |
| 20       | 5 | 5   | 5   | 5     | 5     | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5      | 5     | 5   | 5      | 5     | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5  |
| 25       |   | 5   | 5   | 5     | 5     | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5      | 5     | 5   | 5      | 5     | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5  |
| 28       |   |     |     | 6     | 6     | 6   | 6   | 6   | 6   | 6   | 6   | 6   | 6   | 6      | 6     | 6   | 6      | 6     | 6   | 6   | 6   | 6   | 6   | 6   | 5   | 5   | 5   | 5   | 5   | 5   | 5  |
| 30       |   |     |     |       |       | 6   | 6   | 6   | 6   | 6   | 6   | 6   | 6   | 6      | 6     | 6   | 6      | 6     | 6   | 6   | 6   | 6   | 6   | 6   | 6   | 6   | 6   | 6   | 6   | 6   | 6  |
| 32       |   |     |     |       |       |     | 7   | 7   | 7   | 7   | 7   | 7   | 7   | 7      | 7     | 7   | 7      | 7     | 7   | 7   | 7   | 7   | 7   | 7   | 7   | 7   | 7   | 7   | 7   | 7   | 7  |
| 34       |   |     |     |       |       |     |     | 8   | 8   | 8   | 8   | 8   | 8   | 8      | 8     | 8   | 8      | 8     | 8   | 7   | 7   | 7   | 7   | 7   | 7   | 7   | 7   | 7   | 7   | 7   | 7  |
| 36       |   |     |     |       |       |     |     |     | 9   | 9   | 9   | 9   | 9   | 9      | 9     | 9   | 9      | 9     | 8   | 8   | 8   | 8   | 8   | 8   | 8   | 8   | 8   | 8   | 8   | 8   | 8  |
| 38       |   |     |     |       |       |     |     |     |     |     | 10  | 10  | 10  | 10     | 10    | 10  | 10     | 10    | 10  | 10  | 10  | 10  | 9   | 9   | 9   | 9   | 9   | 9   | 9   | 9   | 9  |
| 39       |   |     |     |       |       |     |     |     |     |     | 11  | 11  | 11  | 11     | 11    | 11  | 10     | 10    | 10  | 10  | 10  | 10  | 10  | 10  | 10  | 10  | 10  | 10  | 10  | 10  | 10 |
| 40       |   |     | Ν   | ot Ar | ıalyz | ed  |     |     |     |     |     | 12  | 11  | 11     | 11    | 11  | 11     | 11    | 11  | 11  | 11  | 11  | 11  | 11  | 11  | 11  | 11  | 11  | 11  | 11  | 11 |
| 41       |   |     |     |       |       |     |     |     |     |     |     | 13  | 13  | 12     | 12    | 12  | 12     | 12    | 12  | 12  | 12  | 12  | 12  | 12  | 12  | 12  | 12  | 11  | 11  | 11  | 11 |
| 42       |   |     |     |       |       |     |     |     |     |     |     | 14  | 14  | 13     | 13    | 13  | 13     | 13    | 13  | 13  | 13  | 13  | 13  | 13  | 12  | 12  | 12  | 12  | 12  | 12  | 12 |
| 43       |   |     |     |       |       |     |     |     |     |     |     |     | 15  | 14     | 14    | 14  | 14     | 14    | 14  | 14  | 14  | 14  | 14  | 14  | 13  | 13  | 13  | 13  | 13  | 13  | 13 |
| 44       |   |     |     |       |       |     |     |     |     |     |     |     |     | 16     | 15    | 15  | 15     | 15    | 15  | 15  | 15  | 15  | 15  | 15  | 15  | 14  | 14  | 14  | 14  | 14  | 14 |
| 45       |   |     |     |       |       |     | ·   |     |     |     |     |     |     | 17     | 17    | 16  | 16     | 16    | 16  | 16  | 16  | 16  | 16  | 16  | 16  | 16  | 15  | 15  | 15  | 15  | 15 |

Use burnup and enrichment to lookup minimum cooling time in years. Licensee is responsible for ensuring that uncertainties in fuel enrichment and burnup are correctly

accounted for during fuel qualification.

Round burnup UP to next higher entry, round enrichments DOWN to next lower entry.

Fuel with an initial enrichment less than 2.0 and greater than 5.0 wt.% U-235 is unacceptable for storage.

Fuel with a burnup greater than 45 GWd/MTU is unacceptable for storage

Fuel with a burnup less than 10 GWd/MTU is acceptable for storage after 5-years cooling.

Example: An assembly with an initial enrichment of 3.75 wt. % U-235 and a burnup of 41.5 GWd/MTU is acceptable for storage after a thirteen-year cooling time as defined

by 3.7 wt. % U-235 (rounding down) and 42 GWd/MTU (rounding up) on the qualification table.

# Table 1-2lPWR Fuel Qualification Table for 0.63 kW per Assembly Fuel with BPRAs for the NUHOMS®-32PT DSC

|        |   |     |     |       |      |     |     |     |     |     |     |     | Ini | tial E | nrich | ment | twt % | 6 U-2 | 235 |     |     |     |     |     |     |     |     |     |     |     |    |
|--------|---|-----|-----|-------|------|-----|-----|-----|-----|-----|-----|-----|-----|--------|-------|------|-------|-------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|----|
| B(WM)) | 2 | 2.1 | 2.2 | 2.3   | 2.4  | 2.5 | 2.6 | 2.7 | 2.8 | 2.9 | 3.0 | 3.1 | 3.2 | 3.3    | 3.4   | 3.5  | 3.6   | 3.7   | 3.8 | 3.9 | 4.0 | 4.1 | 4.2 | 4.3 | 4.4 | 4.5 | 4.6 | 4.7 | 4.8 | 4.9 | 5  |
| 10     | 5 | 5   | 5   | 5     | 5    | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5      | 5     | 5    | 5     | 5     | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5  |
| 15     | 5 | 5   | 5   | 5     | 5    | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5      | 5     | 5    | 5     | 5     | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5  |
| 20     | 5 | 5   | 5   | 5     | 5    | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5      | 5     | 5    | 5     | 5     | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5  |
| 25     |   | 6   | 6   | 6     | 6    | 6   | 6   | 6   | 6   | 6   | 6   | 6   | 6   | 6      | 6     | 6    | 6     | 6     | 6   | 6   | 6   | 6   | 6   | 6   | 6   | 6   | 6   | 6   | 6   | 6   | 6  |
| 28     |   |     |     | 7     | 7    | 7   | 7   | 7   | 7   | 6   | 6   | 6   | 6   | 6      | 6     | 6    | 6     | 6     | 6   | 6   | 6   | 6   | 6   | 6   | 6   | 6   | 6   | 6   | 6   | 6   | 6  |
| 30     |   |     |     |       |      | 7   | 7   | 7   | 7   | 7   | 7   | 7   | 7   | 7      | 7     | 7    | 7     | 7     | 7   | 7   | 7   | 7   | 7   | 7   | 7   | 7   | 7   | 7   | 7   | 7   | 7  |
| 32     |   |     |     |       |      |     | 8   | 8   | 8   | 8   | 8   | 8   | 8   | 8      | 8     | 8    | 8     | 8     | 8   | 8   | 8   | 8   | 8   | 8   | 8   | 8   | 8   | 8   | 8   | 8   | 8  |
| 34     |   |     |     |       |      |     |     | 10  | 10  | 9   | 9   | 9   | 9   | 9      | 9     | 9    | 9     | 9     | 9   | 9   | 9   | 9   | 9   | 9   | 9   | 9   | 9   | 9   | 9   | 9   | 9  |
| 36     |   |     |     |       |      |     |     |     | 11  | 11  | 11  | 11  | 11  | 11     | 11    | 11   | 11    | 11    | 11  | 10  | 10  | 10  | 10  | 10  | 10  | 10  | 10  | 10  | 10  | 10  | 10 |
| 38     |   |     |     |       |      |     |     |     |     |     | 13  | 13  | 13  | 13     | 13    | 13   | 12    | 12    | 12  | 12  | 12  | 12  | 12  | 12  | 12  | 12  | 12  | 12  | 12  | 12  | 12 |
| 39     |   |     |     |       |      |     |     |     |     |     | 14  | 14  | 14  | 14     | 14    | 14   | 14    | 13    | 13  | 13  | 13  | 13  | 13  | 13  | 13  | 13  | 13  | 13  | 13  | 13  | 13 |
| 40     |   |     | N   | ot Ar | alyz | ed  |     |     |     |     |     | 15  | 15  | 15     | 15    | 15   | 15    | 15    | 14  | 14  | 14  | 14  | 14  | 14  | 14  | 14  | 14  | 14  | 14  | 14  | 14 |
| 41     |   |     |     |       |      |     |     |     |     |     |     | 16  | 16  | 16     | 16    | 16   | 16    | 16    | 16  | 16  | 16  | 16  | 15  | 15  | 15  | 15  | 15  | 15  | 15  | 15  | 15 |
| 42     |   |     |     |       |      |     |     |     |     |     |     | 18  | 18  | 17     | 17    | 17   | 17    | 17    | 17  | 17  | 17  | 17  | 17  | 17  | 16  | 16  | 16  | 16  | 16  | 16  | 16 |
| 43     |   |     |     |       |      |     |     |     |     |     |     |     | 19  | 19     | 19    | 19   | 18    | 18    | 18  | 18  | 18  | 18  | 18  | 18  | 18  | 18  | 18  | 18  | 17  | 17  | 17 |
| 44     |   |     |     |       |      |     |     |     |     |     |     |     |     | 20     | 20    | 20   | 20    | 20    | 20  | 20  | 19  | 19  | 19  | 19  | 19  | 19  | 19  | 19  | 19  | 19  | 19 |
| 45     |   |     |     |       |      |     |     |     |     |     |     |     |     | 22     | 21    | 21   | 21    | 21    | 21  | 21  | 21  | 21  | 21  | 20  | 20  | 20  | 20  | 20  | 20  | 20  | 20 |

(Minimum required years of cooling time after reactor core discharge)

Use burnup and enrichment to lookup minimum cooling time in years. Licensee is responsible for ensuring that uncertainties in fuel enrichment and burnup are correctly accounted for during fuel qualification.

Round burnup UP to next higher entry, round enrichments DOWN to next lower entry.

Fuel with an initial enrichment less than 2.0 and greater than 5.0 wt.% U-235 is unacceptable for storage.

Fuel with a burnup greater than 45 GWd/MTU is unacceptable for storage

Fuel with a burnup less than 10 GWd/MTU is acceptable for storage after 5-years cooling.

• Example: An assembly with an initial enrichment of 3.75 wt. % U-235 and a burnup of 41.5 GWd/MTU is acceptable for storage after a seventeen-year cooling time as defined by 3.7 wt. % U-235 (rounding down) and 42 GWd/MTU (rounding up) on the qualification table.

# Table 1-2mPWR Fuel Qualification Table for 0.6 kW per Assembly Fuel With BPRAs for the NUHOMS®-32PT DSC

|         |     |     |     |       |       |     |     |     |     |     |     |     | Ini | tial E | nrich | ment | t wt % | 6 U-2 | 235 |     |     |     |     |     |     |     |     |     |     |     |     |
|---------|-----|-----|-----|-------|-------|-----|-----|-----|-----|-----|-----|-----|-----|--------|-------|------|--------|-------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
| B(GWM)) | 2.0 | 2.1 | 2.2 | 2.3   | 2.4   | 2.5 | 2.6 | 2.7 | 2.8 | 2.9 | 3.0 | 3.1 | 3.2 | 3.3    | 3.4   | 3.5  | 3.6    | 3.7   | 3.8 | 3.9 | 4.0 | 4.1 | 4.2 | 4.3 | 4.4 | 4.5 | 4.6 | 4.7 | 4.8 | 4.9 | 5.0 |
| 10      | 5   | 5   | 5   | 5     | 5     | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5      | 5     | 5    | 5      | 5     | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   |
| 15      | 5   | 5   | 5   | 5     | 5     | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5      | 5     | 5    | 5      | 5     | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   |
| 20      | 5   | 5   | 5   | 5     | 5     | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5      | 5     | 5    | 5      | 5     | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   |
| 25      |     | 6   | 6   | 6     | 6     | 6   | 6   | 6   | 6   | 6   | 6   | 6   | 6   | 6      | 6     | 6    | 6      | 6     | 6   | 6   | 6   | 6   | 6   | 6   | 6   | 6   | 6   | 6   | 6   | 6   | 6   |
| 28      |     |     |     | 7     | 7     | 7   | 7   | 7   | 7   | 7   | 7   | 7   | 7   | 7      | 7     | 7    | 7      | 7     | 7   | 7   | 7   | 7   | 7   | 7   | 7   | 7   | 7   | 7   | 7   | 7   | 6   |
| 30      |     |     |     |       |       | 8   | 8   | 8   | 8   | 8   | 8   | 8   | 8   | 8      | 8     | 8    | 8      | 8     | 8   | 8   | 8   | 7   | 7   | 7   | 7   | 7   | 7   | 7   | 7   | 7   | 7   |
| 32      |     |     |     |       |       |     | 9   | 9   | 9   | 9   | 9   | 9   | 9   | 9      | 9     | 9    | 9      | 9     | 9   | 9   | 9   | 9   | 9   | 9   | 9   | 8   | 8   | 8   | 8   | 8   | 8   |
| 34      |     |     |     |       |       |     |     | 11  | 11  | 11  | 10  | 10  | 10  | 10     | 10    | 10   | 10     | 10    | 10  | 10  | 10  | 10  | 10  | 10  | 10  | 10  | 10  | 10  | 10  | 10  | 10  |
| 36      |     |     |     |       |       |     |     |     | 12  | 12  | 12  | 12  | 12  | 12     | 12    | 12   | 12     | 12    | 12  | 12  | 12  | 12  | 12  | 12  | 12  | 12  | 11  | 11  | 11  | 11  | 11  |
| 38      |     |     |     |       |       |     |     |     |     |     | 15  | 15  | 14  | 14     | 14    | 14   | 14     | 14    | 14  | 14  | 14  | 14  | 14  | 14  | 14  | 14  | 14  | 14  | 14  | 13  | 13  |
| 39      |     |     |     |       |       |     |     |     |     |     | 16  | 16  | 16  | 16     | 16    | 15   | 15     | 15    | 15  | 15  | 15  | 15  | 15  | 15  | 15  | 15  | 15  | 15  | 15  | 15  | 15  |
| 40      |     |     | N   | ot An | ıalyz | ed  |     |     |     |     |     | 17  | 17  | 17     | 17    | 17   | 17     | 17    | 17  | 16  | 16  | 16  | 16  | 16  | 16  | 16  | 16  | 16  | 16  | 16  | 16  |
| 41      |     |     |     |       |       |     |     |     |     |     |     | 19  | 18  | 18     | 18    | 18   | 18     | 18    | 18  | 18  | 18  | 18  | 18  | 17  | 17  | 17  | 17  | 17  | 17  | 17  | 17  |
| 42      |     |     |     |       |       |     |     |     |     |     |     | 20  | 20  | 20     | 20    | 19   | 19     | 19    | 19  | 19  | 19  | 19  | 19  | 19  | 19  | 19  | 19  | 19  | 19  | 19  | 19  |
| 43      |     |     |     |       |       |     |     |     |     |     |     |     | 21  | 21     | 21    | 21   | 21     | 21    | 21  | 21  | 20  | 20  | 20  | 20  | 20  | 20  | 20  | 20  | 20  | 20  | 20  |
| 44      |     |     |     |       |       |     |     |     |     |     |     |     |     | 23     | 22    | 22   | 22     | 22    | 22  | 22  | 22  | 22  | 22  | 22  | 22  | 21  | 21  | 21  | 21  | 21  | 21  |
| 45      |     |     |     |       |       |     |     |     |     |     |     |     |     | 24     | 24    | 24   | 24     | 24    | 23  | 23  | 23  | 23  | 23  | 23  | 23  | 23  | 23  | 23  | 23  | 23  | 22  |

## (Minimum required years of cooling time after reactor core discharge)

Use burnup and enrichment to lookup minimum cooling time in years. Licensee is responsible for ensuring that uncertainties in fuel enrichment and burnup are correctly

accounted for during fuel qualification.

Round burnup UP to next higher entry, round enrichments DOWN to next lower entry.

Fuel with an initial enrichment less than 2.0 and greater than 5.0 wt.% U-235 is unacceptable for storage.

Fuel with a burnup greater than 45 GWd/MTU is unacceptable for storage

Fuel with a burnup less than 10 GWd/MTU is acceptable for storage after 5-years cooling.

Example: An assembly with an initial enrichment of 3.75 wt. % U-235 and a burnup of 41.5 GWd/MTU is acceptable for storage after a nineteen-year cooling time as defined

by 3.7 wt. % U-235 (rounding down) and 42 GWd/MTU (rounding up) on the qualification table.

#### Table 1-2n

## PWR Fuel Qualification Table for Zone 1 with 0.7 kW per Assembly, Fuel With or Without BPRAs, for the NUHOMS<sup>®</sup>-24PHB DSC

|          |     |     |     | (1     | <b>VIIII</b> | 11141 |     | 1411 |     |     |      |      | -    |      |      |      |       |      | aise | marg | <b>~</b> ) |      |      |      |      |      |
|----------|-----|-----|-----|--------|--------------|-------|-----|------|-----|-----|------|------|------|------|------|------|-------|------|------|------|------------|------|------|------|------|------|
| BU (Gwd/ |     |     |     |        |              |       |     |      | 1   | 1   |      |      |      | 1    | 1    | 1    | (wt % |      | • •  | • •  |            |      |      |      |      |      |
| MTU)     | 2   | 2.1 | 2.2 | 2.3    | 2.4          | 2.5   | 2.6 | 2.7  | 2.8 | 2.9 | 3.0  | 3.1  | 3.2  | 3.3  | 3.4  | 3.5  | 3.6   | 3.7  | 3.8  | 3.9  | 4.0        | 4.1  | 4.2  | 4.3  | 4.4  | 4.5  |
| 10       | 5   | 5.0 | 5.0 | 5.0    | 5.0          | 5.0   | 5.0 | 5.0  | 5.0 | 5.0 | 5.0  | 5.0  | 5    | 5.0  | 5.0  | 5.0  | 5.0   | 5.0  | 5.0  | 5.0  | 5.0        | 5.0  | 5.0  | 5.0  | 5.0  | 5.0  |
| 15       | 5.0 | 5.0 | 5.0 | 5.0    | 5.0          | 5.0   | 5.0 | 5.0  | 5.0 | 5.0 | 5.0  | 5.0  | 5.0  | 5.0  | 5.0  | 5.0  | 5.0   | 5.0  | 5.0  | 5.0  | 5.0        | 5.0  | 5.0  | 5.0  | 5.0  | 5.0  |
| 20       | 5   | 5.0 | 5.0 | 5.0    | 5.0          | 5.0   | 5.0 | 5.0  | 5.0 | 5.0 | 5.0  | 5.0  | 5.0  | 5.0  | 5.0  | 5.0  | 5.0   | 5.0  | 5.0  | 5.0  | 5.0        | 5.0  | 5.0  | 5.0  | 5.0  | 5.0  |
| 25       |     | 5.0 | 5.0 | 5.0    | 5.0          | 5.0   | 5.0 | 5.0  | 5.0 | 5.0 | 5.0  | 5.0  | 5.0  | 5.0  | 5.0  | 5.0  | 5.0   | 5.0  | 5.0  | 5.0  | 5.0        | 5.0  | 5.0  | 5.0  | 5.0  | 5.0  |
| 28       |     |     | 5.5 | 5.5    | 5.5          | 5.5   | 5.5 | 5.5  | 5.5 | 5.5 | 5.5  | 5.5  | 5.5  | 5.5  | 5.5  | 5.5  | 5.5   | 5.5  | 5.5  | 5.5  | 5.5        | 5.5  | 5.5  | 5.5  | 5.5  | 5.5  |
| 30       |     |     |     |        |              | 6.5   | 6.5 | 6.0  | 6.0 | 6.0 | 6.0  | 6.0  | 6.0  | 6.0  | 6.0  | 6.0  | 6.0   | 6.0  | 6.0  | 6.0  | 6.0        | 6.0  | 6.0  | 6.0  | 6.0  | 6.0  |
| 32       |     |     |     |        |              |       | 7.0 | 7.0  | 7.0 | 7.0 | 7.0  | 7.0  | 7.0  | 7.0  | 6.5  | 6.5  | 6.5   | 6.5  | 6.5  | 6.5  | 6.5        | 6.5  | 6.5  | 6.5  | 6.5  | 6.5  |
| 34       |     |     |     |        |              |       |     | 8.0  | 8.0 | 8.0 | 8.0  | 7.5  | 7.5  | 7.5  | 7.5  | 7.5  | 7.5   | 7.5  | 7.5  | 7.5  | 7.5        | 7.5  | 7.5  | 7.5  | 7.5  | 7.5  |
| 36       |     |     |     |        |              |       |     |      | 9.0 | 9.0 | 9.0  | 9.0  | 9.0  | 9.0  | 8.5  | 8.5  | 8.5   | 8.5  | 8.5  | 8.5  | 8.5        | 8.5  | 8.5  | 8.5  | 8.5  | 8.5  |
| 38       |     |     |     |        |              |       |     |      |     |     | 10.5 | 10.5 | 10.5 | 10.0 | 10.0 | 10.0 | 10.0  | 10.0 | 10.0 | 10.0 | 10.0       | 10.0 | 9.5  | 9.5  | 9.5  | 9.5  |
| 39       |     |     |     |        |              |       |     |      |     |     | 11.5 | 11.0 | 11   | 11.0 | 11.0 | 11.0 | 11.0  | 11.0 | 10.5 | 10.5 | 10.5       | 10.5 | 10.5 | 10.5 | 10.5 | 10.5 |
| 40       |     |     |     |        |              |       |     |      |     |     | 12.0 | 12.0 | 12.0 | 12.0 | 12.0 | 12.0 | 11.5  | 11.5 | 11.5 | 11.5 | 11.5       | 11.5 | 11.5 | 11.0 | 11.0 | 11.0 |
| 41       |     |     |     |        |              |       |     |      |     |     | 13.0 | 13.0 | 13.0 | 13.0 | 13.0 | 13.0 | 12.5  | 12.5 | 12.5 | 12.5 | 12.5       | 12.5 | 12.5 | 12.0 | 12.0 | 12.0 |
| 42       |     |     |     |        |              |       |     |      |     |     | 14.5 | 14.5 | 14.0 | 14.0 | 14.0 | 14.0 | 13.5  | 13.5 | 13.5 | 13.5 | 13.5       | 13.5 | 13.5 | 13.0 | 13.0 | 13.0 |
| 43       |     |     |     | lot An | مايرم        | a     |     |      |     |     | 15.5 | 15.5 | 15.5 | 15.0 | 15.0 | 15.0 | 15.0  | 15.0 | 14.5 | 14.5 | 14.5       | 14.5 | 14.5 | 14.5 | 14.0 | 14.0 |
| 44       |     |     |     | OUAD   | aryze        | u     |     |      |     |     | 17.0 | 16.5 | 16.5 | 16.5 | 16.5 | 16.0 | 16.0  | 16.0 | 16.0 | 16.0 | 15.5       | 15.5 | 15.5 | 15.5 | 15.5 | 15.5 |
| 45       |     |     |     |        |              |       |     |      |     |     |      |      | 18.0 | 17.5 | 17.5 | 17.5 | 17.5  | 17.0 | 17.0 | 17.0 | 17.0       | 17.0 | 16.5 | 16.5 | 16.5 | 16.5 |
| 46       |     |     |     |        |              |       |     |      |     |     |      |      | 18.8 | 18.7 | 18.5 | 18.5 | 18.3  | 18.2 | 18.1 | 18.0 | 17.9       | 17.8 | 17.7 | 17.6 | 17.5 | 17.4 |
| 47       |     |     |     |        |              |       |     |      |     |     |      |      | 20.1 | 20.0 | 19.9 | 19.6 | 19.6  | 19.5 | 19.4 | 19.2 | 19.1       | 19.0 | 18.9 | 18.8 | 18.7 | 18.7 |
| 48       |     |     |     |        |              |       |     |      |     |     |      |      | 21.4 | 21.3 | 21.1 | 21.0 | 20.8  | 20.8 | 20.7 | 20.5 | 20.4       | 20.3 | 20.2 | 20.1 | 20.0 | 19.9 |
| 49       |     |     |     |        |              |       |     |      |     |     |      |      | 22.7 | 22.6 | 22.4 | 22.3 | 22.1  | 22.1 | 21.9 | 21.8 | 21.7       | 21.6 | 21.5 | 21.4 | 21.3 | 21.2 |
| 50       |     |     |     |        |              |       |     |      |     |     |      |      |      |      | 23.7 | 23.6 | 23.5  | 23.4 | 23.3 | 23.2 | 23.0       | 22.9 | 22.8 | 22.7 | 22.6 | 22.5 |
| 51       |     |     |     |        |              |       |     |      |     |     |      |      |      |      | 25.0 | 24.9 | 24.8  | 24.6 | 24.5 | 24.4 | 24.3       | 24.2 | 24.0 | 23.9 | 23.8 | 23.7 |
| 52       |     |     |     |        |              |       |     |      |     |     |      |      |      |      | 26.3 | 26.2 | 26.0  | 25.9 | 25.8 | 25.7 | 25.6       | 25.4 | 25.3 | 25.2 | 25.2 | 25.0 |
| 53       |     |     |     |        |              |       |     |      |     |     |      |      |      |      | 27.5 | 27.3 | 27.2  | 27.1 | 27.0 | 26.9 | 26.8       | 26.7 | 26.5 | 26.4 | 26.4 | 26.2 |
| 54       |     |     |     |        |              |       |     |      |     |     |      |      |      |      | 28.8 | 28.6 | 28.5  | 28.3 | 28.2 | 28.1 | 28.0       | 28.0 | 27.8 | 27.7 | 27.6 | 27.5 |
| 55       |     |     |     |        |              |       |     |      |     |     |      |      |      |      | 29.9 | 29.8 | 29.7  | 29.6 | 29.5 | 29.3 | 29.2       | 29.1 | 29.0 | 28.9 | 28.8 | 28.7 |
|          |     | 1 1 |     |        |              |       |     |      |     |     |      |      |      |      |      |      |       |      |      |      |            |      |      |      |      |      |

|     | ( ) <i>(</i> ) · · · | • 1      | C        | 1.      |            |         | 1. 1           |   |
|-----|----------------------|----------|----------|---------|------------|---------|----------------|---|
| - ( | Minimiim             | required | vears of | cooling | time attei | reactor | core discharge | ) |
|     |                      |          |          |         |            |         |                |   |

• BU = Assembly average burnup

• Use burnup and enrichment to lookup minimum cooling time in years. For fuel assemblies reconstituted with up to 10 stainless steel rods only, if the lookup cooling time is less than 9.0 years then a minimum cooling time of 9.0 years shall be used. Licensee is responsible for ensuring that uncertainties in fuel enrichment and burnup are correctly accounted for during fuel qualification.

- Round burnup UP to next higher entry, round enrichments DOWN to next lower entry.
- Fuel with an initial enrichment greater than 4.5 wt.% U-235 is unacceptable for storage.
- Fuel with a burnup less than 10 GWd/MTU is acceptable for storage after 5-years cooling.
- Example: An assembly with an initial enrichment of 3.75 wt. % U-235 and a burnup of 46.5 GWd/MTU is acceptable for storage after a 19.5 years cooling time as defined by 3.7 wt. % U-235 (rounding down) and 47 GWd/MTU (rounding up) on the qualification table.
- See Figure 1-8 for a description of zones.
- For assemblies fuel reconstituted with Zircaloy clad uranium-oxide rods use the assembly average enrichment to determine the minimum cooling time.

# Table 1-20 PWR Fuel Qualification Table for Zone 2 with 1.0 kW per Assembly, Fuel With or Without BPRAs, for the NUHOMS®-24PHB DSC

| (Minimum required years | of cooling time a | after reactor core discharge) |
|-------------------------|-------------------|-------------------------------|
|-------------------------|-------------------|-------------------------------|

| BU        |     | Assembly Average Initial U-235 Enrichmen |     |        |       |     |     |     |     |     |     |     |     |     |      | t %) |      |      |      |      | 0 /  |      |      |      |      |      |
|-----------|-----|--|-----|--------|-------|-----|-----|-----|-----|-----|-----|-----|-----|-----|------|------|------|------|------|------|------|------|------|------|------|------|
| (Gwd/MTU) | 2.0 | 2.1                                      | 2.2 | 2.3    | 2.4   | 2.5 | 2.6 | 2.7 | 2.8 | 2.9 | 3.0 | 3.1 | 3.2 | 3.3 | 3.4  | 3.5  | 3.6  | 3.7  | 3.8  | 3.9  | 4.0  | 4.1  | 4.2  | 4.3  | 4.4  | 4.5  |
| 10        | 5.0 | 5.0                                      | 5.0 | 5.0    | 5.0   | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0  | 5.0  | 5.0  | 5.0  | 5.0  | 5.0  | 5.0  | 5.0  | 5.0  | 5.0  | 5.0  | 5.0  |
| 15        | 5.0 | 5.0                                      | 5.0 | 5.0    | 5.0   | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0  | 5.0  | 5.0  | 5.0  | 5.0  | 5.0  | 5.0  | 5.0  | 5.0  | 5.0  | 5.0  | 5.0  |
| 20        | 5.0 | 5.0                                      | 5.0 | 5.0    | 5.0   | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0  | 5.0  | 5.0  | 5.0  | 5.0  | 5.0  | 5.0  | 5.0  | 5.0  | 5.0  | 5.0  | 5.0  |
| 25        |     | 5.0                                      | 5.0 | 5.0    | 5.0   | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0  | 5.0  | 5.0  | 5.0  | 5.0  | 5.0  | 5.0  | 5.0  | 5.0  | 5.0  | 5.0  | 5.0  |
| 28        |     |  | 5.0 | 5.0    | 5.0   | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0  | 5.0  | 5.0  | 5.0  | 5.0  | 5.0  | 5.0  | 5.0  | 5.0  | 5.0  | 5.0  | 5.0  |
| 30        |     |  |     |        |       | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0  | 5.0  | 5.0  | 5.0  | 5.0  | 5.0  | 5.0  | 5.0  | 5.0  | 5.0  | 5.0  | 5.0  |
| 32        |     |  |     |        |       |     | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0  | 5.0  | 5.0  | 5.0  | 5.0  | 5.0  | 5.0  | 5.0  | 5.0  | 5.0  | 5.0  | 5.0  |
| 34        |     |  |     |        |       |     |     | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0  | 5.0  | 5.0  | 5.0  | 5.0  | 5.0  | 5.0  | 5.0  | 5.0  | 5.0  | 5.0  | 5.0  |
| 36        |     |  |     |        |       |     |     |     | 5.5 | 5.5 | 5.5 | 5.5 | 5.5 | 5.0 | 5.0  | 5.0  | 5.0  | 5.0  | 5.0  | 5.0  | 5.0  | 5.0  | 5.0  | 5.0  | 5.0  | 5.0  |
| 38        |     |  |     |        |       |     |     |     |     |     | 6.0 | 5.5 | 5.5 | 5.5 | 5.5  | 5.5  | 5.5  | 5.5  | 5.5  | 5.5  | 5.5  | 5.5  | 5.5  | 5.5  | 5.5  | 5.5  |
| 39        |     |  |     |        |       |     |     |     |     |     | 6.0 | 6.0 | 6   | 6.0 | 6.0  | 6.0  | 6.0  | 6.0  | 6.0  | 5.5  | 5.5  | 5.5  | 5.5  | 5.5  | 5.5  | 5.5  |
| 40        |     |  |     |        |       |     |     |     |     |     | 6.5 | 6.5 | 6   | 6.0 | 6.0  | 6.0  | 6.0  | 6.0  | 6.0  | 6.0  | 6.0  | 6.0  | 6.0  | 6.0  | 6.0  | 6.0  |
| 41        |     |  |     |        |       |     |     |     |     |     | 6.5 | 6.5 | 6.5 | 6.5 | 6.5  | 6.5  | 6.5  | 6.5  | 6.5  | 6.0  | 6.0  | 6.0  | 6.0  | 6.0  | 6.0  | 6.0  |
| 42        |     |  |     |        |       |     |     |     |     |     | 7.0 | 7.0 | 7.0 | 7.0 | 6.5  | 6.5  | 6.5  | 6.5  | 6.5  | 6.5  | 6.5  | 6.5  | 6.5  | 6.5  | 6.5  | 6.5  |
| 43        |     |  |     |        |       |     |     |     |     |     | 7.5 | 7.0 | 7.0 | 7.0 | 7.0  | 7.0  | 7.0  | 7.0  | 7.0  | 7.0  | 7.0  | 7.0  | 6.5  | 6.5  | 6.5  | 6.5  |
| 44        |     |  |     |        |       |     |     |     |     |     | 7.5 | 7.5 | 7.5 | 7.5 | 7.5  | 7.5  | 7.5  | 7.5  | 7.0  | 7.0  | 7.0  | 7.0  | 7.0  | 7.0  | 7.0  | 7.0  |
| 45        |     |  | ľ   | Not Ar | alyze | d   |     |     |     |     |     |     | 8   | 8.0 | 8.0  | 8.0  | 7.5  | 7.5  | 7.5  | 7.5  | 7.5  | 7.5  | 7.5  | 7.5  | 7.5  | 7.4  |
| 46        |     |  |     |        |       |     |     |     |     |     |     |     | 8.2 | 8.1 | 8.0  | 8.0  | 7.9  | 7.8  | 7.8  | 7.7  | 7.7  | 7.6  | 7.6  | 7.5  | 7.5  | 7.4  |
| 47        |     |  |     |        |       |     |     |     |     |     |     |     | 8.7 | 8.6 | 8.5  | 8.4  | 8.4  | 8.3  | 8.2  | 8.2  | 8.1  | 8.0  | 8.0  | 7.9  | 7.9  | 7.8  |
| 48        |     |  |     |        |       |     |     |     |     |     |     |     | 9.2 | 9.1 | 9.0  | 9.0  | 8.9  | 8.8  | 8.7  | 8.6  | 8.6  | 8.5  | 8.5  | 8.4  | 8.3  | 8.3  |
| 49        |     |  |     |        |       |     |     |     |     |     |     |     | 9.8 | 9.7 | 9.6  | 9.5  | 9.4  | 9.3  | 9.2  | 9.2  | 9.1  | 9.0  | 9.0  | 8.9  | 8.8  | 8.7  |
| 50        |     |  |     |        |       |     |     |     |     |     |     |     |     |     | 10.2 | 10.1 | 10.0 | 9.9  | 9.8  | 9.7  | 9.6  | 9.6  | 9.5  | 9.4  | 9.3  | 9.3  |
| 51        |     |  |     |        |       |     |     |     |     |     |     |     |     |     | 10.9 | 10.8 | 10.7 | 10.6 | 10.5 | 10.3 | 10.3 | 10.2 | 10.1 | 10.0 | 9.9  | 9.9  |
| 52        |     |  |     |        |       |     |     |     |     |     |     |     |     |     | 11.6 | 11.5 | 11.3 | 11.2 | 11.1 | 11.0 | 10.9 | 10.8 | 10.7 | 10.6 | 10.5 | 10.5 |
| 53        |     |  |     |        |       |     |     |     |     |     |     |     |     |     | 12.4 | 12.2 | 12.1 | 12.0 | 11.9 | 11.8 | 11.6 | 11.5 | 11.4 | 11.3 | 11.2 | 11.1 |
| 54        |     |  |     |        |       |     |     |     |     |     |     |     |     |     | 13.2 | 13.1 | 13.0 | 12.8 | 12.7 | 12.5 | 12.4 | 12.3 | 12.2 | 12.1 | 12.0 | 11.9 |
| 55        |     |  |     |        |       |     |     |     |     |     |     |     |     |     | 14.1 | 13.9 | 13.8 | 13.6 | 13.5 | 13.4 | 13.2 | 13.1 | 13.0 | 12.9 | 12.8 | 12.6 |

• BU = Assembly average burnup

• Use burnup and enrichment to lookup minimum cooling time in years. For fuel assemblies reconstituted with up to 10 stainless steel rods only, if the lookup cooling time is less than 9.0 years then a minimum cooling time of 9.0 years shall be used. Licensee is responsible for ensuring that uncertainties in fuel enrichment and burnup are correctly accounted for during fuel qualification.

- Round burnup UP to next higher entry, round enrichments DOWN to next lower entry.
- Fuel with an initial enrichment greater than 4.5 wt.% U-235 is unacceptable for storage.
- Fuel with a burnup less than 10 GWd/MTU is acceptable for storage after 5-years cooling.
- Example: An assembly with an initial enrichment of 3.75 wt. % U-235 and a burnup of 46.5 GWd/MTU is acceptable for storage after a 8.3 years cooling time as defined by 3.7 wt. % U-235 (rounding down) and 47 GWd/MTU (rounding up) on the qualification table.
- See Figure 1-8 for a description of zones.

 For assemblies fuel reconstituted with Zircaloy clad uranium-oxide rods use the assembly average enrichment to determine the minimum cooling time.

# Table 1-2p PWR Fuel Qualification Table for Zone 3 with 1.3 kW per Assembly, Fuel With or Without BPRAs, for the NUHOMS®-24PHB DSC

| (M | inimum | required | years of | cooling | time after | r reactor | core discharg | ge) |
|----|--------|----------|----------|---------|------------|-----------|---------------|-----|
|    |        |          |          |         |            |           |               |     |

| BU        |     |     |     |        |       |     |     | Ass | embly | Avera | ge Init | ial U-2 | 235 En | richme | ent (w | t %) |     |     |     |     | /   |     |     |     |     |     |
|-----------|-----|-----|-----|--------|-------|-----|-----|-----|-------|-------|---------|---------|--------|--------|--------|------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
| (Gwd/MTU) | 2.0 | 2.1 | 2.2 | 2.3    | 2.4   | 2.5 | 2.6 | 2.7 | 2.8   | 2.9   | 3.0     | 3.1     | 3.2    | 3.3    | 3.4    | 3.5  | 3.6 | 3.7 | 3.8 | 3.9 | 4.0 | 4.1 | 4.2 | 4.3 | 4.4 | 4.5 |
| 10        | 5.0 | 5.0 | 5.0 | 5.0    | 5.0   | 5.0 | 5.0 | 5.0 | 5.0   | 5.0   | 5.0     | 5.0     | 5.0    | 5.0    | 5.0    | 5.0  | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| 15        | 5.0 | 5.0 | 5.0 | 5.0    | 5.0   | 5.0 | 5.0 | 5.0 | 5.0   | 5.0   | 5.0     | 5.0     | 5.0    | 5.0    | 5.0    | 5.0  | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| 20        | 5.0 | 5.0 | 5.0 | 5.0    | 5.0   | 5.0 | 5.0 | 5.0 | 5.0   | 5.0   | 5.0     | 5.0     | 5.0    | 5.0    | 5.0    | 5.0  | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| 25        |     | 5.0 | 5.0 | 5.0    | 5.0   | 5.0 | 5.0 | 5.0 | 5.0   | 5.0   | 5.0     | 5.0     | 5.0    | 5.0    | 5.0    | 5.0  | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| 28        |     |     | 5.0 | 5.0    | 5.0   | 5.0 | 5.0 | 5.0 | 5.0   | 5.0   | 5.0     | 5.0     | 5.0    | 5.0    | 5.0    | 5.0  | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| 30        |     |     |     |        |       | 5.0 | 5.0 | 5.0 | 5.0   | 5.0   | 5.0     | 5.0     | 5.0    | 5.0    | 5.0    | 5.0  | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| 32        |     |     |     |        |       |     | 5.0 | 5.0 | 5.0   | 5.0   | 5.0     | 5.0     | 5.0    | 5.0    | 5.0    | 5.0  | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| 34        |     |     |     |        |       |     |     | 5.0 | 5.0   | 5.0   | 5.0     | 5.0     | 5.0    | 5.0    | 5.0    | 5.0  | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| 36        |     |     |     |        |       |     |     |     | 5.0   | 5.0   | 5.0     | 5.0     | 5.0    | 5.0    | 5.0    | 5.0  | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| 38        |     |     |     |        |       |     |     |     |       |       | 5.5     | 5.5     | 5.5    | 5.5    | 5.5    | 5.5  | 5.5 | 5.5 | 5.5 | 5.5 | 5.5 | 5.5 | 5.5 | 5.5 | 5.5 | 5.5 |
| 39        |     |     |     |        |       |     |     |     |       |       | 5.5     | 5.5     | 5.5    | 5.5    | 5.5    | 5.5  | 5.5 | 5.5 | 5.5 | 5.5 | 5.5 | 5.5 | 5.5 | 5.5 | 5.5 | 5.5 |
| 40        |     |     |     |        |       |     |     |     |       |       | 5.5     | 5.5     | 5.5    | 5.5    | 5.5    | 5.5  | 5.5 | 5.5 | 5.5 | 5.5 | 5.5 | 5.5 | 5.5 | 5.5 | 5.5 | 5.5 |
| 41        |     |     |     |        |       |     |     |     |       |       | 5.5     | 5.5     | 5.5    | 5.5    | 5.5    | 5.5  | 5.5 | 5.5 | 5.5 | 5.5 | 5.5 | 5.5 | 5.5 | 5.5 | 5.5 | 5.5 |
| 42        |     |     |     |        |       |     |     |     |       |       | 6.0     | 6.0     | 6.0    | 6.0    | 6.0    | 6.0  | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 |
| 43        |     |     |     |        |       |     |     |     |       |       | 6.0     | 6.0     | 6.0    | 6.0    | 6.0    | 6.0  | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 |
| 44        |     |     |     |        |       |     |     |     |       |       | 6.0     | 6.0     | 6.0    | 6.0    | 6.0    | 6.0  | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 |
| 45        |     |     | ľ   | lot An | alyze | d   |     |     |       |       |         |         | 6.0    | 6.0    | 6.0    | 6.0  | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 |
| 46        |     |     |     | ,      | ,     | ,   |     |     |       |       |         |         | 6.1    | 6.1    | 6.1    | 6.1  | 6.1 | 6.1 | 6.1 | 6.1 | 6.1 | 6.1 | 6.1 | 6.1 | 6.1 | 6.1 |
| 47        |     |     |     |        |       |     |     |     |       |       |         |         | 6.2    | 6.2    | 6.2    | 6.2  | 6.2 | 6.2 | 6.2 | 6.2 | 6.2 | 6.2 | 6.2 | 6.2 | 6.2 | 6.2 |
| 48        |     |     |     |        |       |     |     |     |       |       |         |         | 6.3    | 6.3    | 6.3    | 6.3  | 6.3 | 6.3 | 6.3 | 6.3 | 6.3 | 6.3 | 6.3 | 6.3 | 6.3 | 6.3 |
| 49        |     |     |     |        |       |     |     |     |       |       |         |         | 6.5    | 6.5    | 6.5    | 6.5  | 6.5 | 6.5 | 6.5 | 6.5 | 6.5 | 6.5 | 6.5 | 6.5 | 6.5 | 6.5 |
| 50        |     |     |     |        |       |     |     |     |       |       |         |         |        |        | 6.5    | 6.5  | 6.5 | 6.5 | 6.5 | 6.5 | 6.5 | 6.5 | 6.5 | 6.5 | 6.5 | 6.5 |
| 51        |     |     |     |        |       |     |     |     |       |       |         |         |        |        | 6.7    | 6.6  | 6.6 | 6.6 | 6.6 | 6.6 | 6.6 | 6.6 | 6.6 | 6.6 | 6.6 | 6.6 |
| 52        |     |     |     |        |       |     |     |     |       |       |         |         |        |        | 7.0    | 6.9  | 6.9 | 6.8 | 6.8 | 6.8 | 6.8 | 6.8 | 6.8 | 6.8 | 6.8 | 6.8 |
| 53        |     |     |     |        |       |     |     |     |       |       |         |         |        |        | 7.3    | 7.2  | 7.2 | 7.1 | 7.1 | 7.0 | 6.9 | 6.9 | 6.9 | 6.9 | 6.9 | 6.9 |
| 54        |     |     |     |        |       |     |     |     |       |       |         |         |        |        | 7.7    | 7.6  | 7.5 | 7.4 | 7.4 | 7.3 | 7.3 | 7.2 | 7.1 | 7.1 | 7.0 | 7.0 |
| 55        |     |     |     |        |       |     |     |     |       |       |         |         |        |        | 8.0    | 8.0  | 7.9 | 7.8 | 7.7 | 7.7 | 7.6 | 7.5 | 7.5 | 7.4 | 7.3 | 7.3 |

• BU = Assembly average burnup

• Use burnup and enrichment to lookup minimum cooling time in years. For fuel assemblies reconstituted with up to 10 stainless steel rods only, if the lookup cooling time is less than 9.0 years then a minimum cooling time of 9.0 years shall be used. Licensee is responsible for ensuring that uncertainties in fuel enrichment and burnup are correctly accounted for during fuel qualification.

• Round burnup UP to next higher entry, round enrichments DOWN to next lower entry.

• Fuel with an initial enrichment greater than 4.5 wt.% U-235 is unacceptable for storage.

• Fuel with a burnup less than 10 GWd/MTU is acceptable for storage after 5-years cooling.

• Example: An assembly with an initial enrichment of 3.75 wt. % U-235 and a burnup of 46.5 GWd/MTU is acceptable for storage after a 6.2 years cooling time as defined by 3.7 wt. % U-235 (rounding down) and 47 GWd/MTU (rounding up) on the qualification table.

• See Figure 1-8 and 1-9 for a description of zones.

• For fuel assemblies reconstituted with Zircaloy clad uranium-oxide rods use the assembly average enrichment to determine the minimum cooling time.

# Table 1-2qBWR Fuel Qualification Table for NUHOMS®-61BT DSC

(Minimum required years of cooling time after reactor core discharge)

| BU<br>(GWd/ |     |       |             |     |     |     |     |     |     |     |     |     |     | Ι   | nitial | Enric | hmen | ıt  |     |     |     |     |     |     |     |     |     |     |     |     |     |
|-------------|-----|-------|-------------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|--------|-------|------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
| MTU         | 1.4 | 1.5   | 1.6         | 1.7 | 1.8 | 1.9 | 2.0 | 2.1 | 2.2 | 2.3 | 2.4 | 2.5 | 2.6 | 2.7 | 2.8    | 2.9   | 3.0  | 3.1 | 3.2 | 3.3 | 3.4 | 3.5 | 3.6 | 3.7 | 3.8 | 3.9 | 4.0 | 4.1 | 4.2 | 4.3 | 4.4 |
| 10          | 4   | 4     | 4           | 4   | 4   | 4   | 4   | 4   | 4   | 4   | 4   | 4   | 4   | 4   | 4      | 4     | 4    | 4   | 4   | 4   | 4   | 4   | 4   | 4   | 4   | 4   | 4   | 4   | 4   | 4   | 4   |
| 15          | 4   | 4     | 4           | 4   | 4   | 4   | 4   | 4   | 4   | 4   | 4   | 4   | 4   | 4   | 4      | 4     | 4    | 4   | 4   | 4   | 4   | 4   | 4   | 4   | 4   | 4   | 4   | 4   | 4   | 4   | 4   |
| 20          | 5   | 5     | 4           | 4   | 4   | 4   | 4   | 4   | 4   | 4   | 4   | 4   | 4   | 4   | 4      | 4     | 4    | 4   | 4   | 4   | 4   | 4   | 4   | 4   | 4   | 4   | 4   | 4   | 4   | 4   | 4   |
| 25          | 5   | 5     | 5           | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5      | 5     | 5    | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 4   | 4   | 4   |
| 28          |     |       |             |     | 6   | 6   | 6   | 6   | 6   | 6   | 6   | 6   | 6   | 6   | 6      | 6     | 6    | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   | 5   |
| 30          |     |       |             |     | 7   | 7   | 7   | 7   | 7   | 7   | 6   | 6   | 6   | 6   | 6      | 6     | 6    | 6   | 6   | 6   | 6   | 6   | 6   | 6   | 6   | 6   | 6   | 6   | 6   | 6   | 6   |
| 32          | NT. |       |             | 1.  | 8   | 8   | 8   | 8   | 8   | 7   | 7   | 7   | 7   | 7   | 7      | 7     | 7    | 7   | 7   | 7   | 7   | 7   | 6   | 6   | 6   | 6   | 6   | 6   | 6   | 6   | 6   |
| 34          | N   | 00 AC | ceptal<br>r | Die | 9   | 9   | 9   | 9   | 9   | 9   | 8   | 8   | 8   | 8   | 8      | 8     | 8    | 8   | 8   | 7   | 7   | 7   | 7   | 7   | 7   | 7   | 7   | 7   | 7   | 7   | 7   |
| 36          | N   |       | n<br>alyze  | d   | 11  | 11  | 11  | 10  | 10  | 10  | 10  | 10  | 9   | 9   | 9      | 9     | 9    | 9   | 9   | 9   | 8   | 8   | 8   | 8   | 8   | 8   | 8   | 8   | 8   | 8   | 8   |
| 38          |     |       |             |     | 14  | 13  | 13  | 12  | 12  | 12  | 12  | 11  | 11  | 11  | 11     | 11    | 10   | 10  | 10  | 10  | 10  | 10  | 9   | 9   | 9   | 9   | 9   | 9   | 9   | 9   | 9   |
| 39          |     |       |             |     | 15  | 14  | 14  | 14  | 13  | 13  | 13  | 12  | 12  | 12  | 12     | 11    | 11   | 11  | 11  | 11  | 10  | 10  | 10  | 10  | 10  | 10  | 10  | 9   | 9   | 9   | 9   |
| 40          |     |       |             |     | 16  | 16  | 15  | 15  | 15  | 14  | 14  | 14  | 13  | 13  | 13     | 12    | 12   | 12  | 12  | 12  | 11  | 11  | 11  | 11  | 11  | 10  | 10  | 10  | 10  | 10  | 10  |

This Table provides an alternate methodology as cross referenced in Table 1-1c and 1-1j for determination of fuel assemblies qualified for storage in NUHOMS<sup>®</sup>-61BT DSC.

- Use burnup and enrichment to lookup minimum cooling time in years. Licensee is responsible for ensuring that uncertainties in fuel enrichment and burnup are conservatively applied in determination of actual values for these two parameters.
- Round burnup UP to next higher entry, round enrichments DOWN to next lower entry.
- Fuel with an initial enrichment less than 1.4 and greater than 4.4 wt.% U-235 is unacceptable for storage.
- Fuel with a burnup greater than 40 GWd/MTU is unacceptable for storage.
- Fuel with a burnup less than 10 GWd/MTU is acceptable for storage after 4 years cooling.
- Example: An assembly with an initial enrichment of 3.75 wt. % U-235 and a burnup of 39.5 GWd/MTU is acceptable for storage after a eleven-year cooling time as defined by 3.7 wt. % U-235 (rounding down) and 40 GWd/MTU (rounding up) on the qualification table.

 Table 1-3a

 PWR Fuel Qualification Table for Zone 1 Fuel with 1.7 kW per Assembly for the NUHOMS®-24PTH DSC (Fuel w/o CCs)

|   | ( <b>, , , , , , , , , , , , , , , , , , ,</b> | • 1      | 0        | 1.      |             |            | 1. 1         | ``       |
|---|--|----------|----------|---------|-------------|------------|--------------|----------|
| 1 | Minimi   | raduirad | VANCE OF | cooling | tima ottar  | ranctor    | ore discharg | <b>D</b> |
| L | winnin   | Icquircu | veals of | COOTINE | unite atter | I Cacior C | uischarg     |          |
|   |  |          |          |         |             |            |              |          |

| Burn-         |     |   |       |       |       |        |                 |       |       | A     | ssen  | nbly i     | Aver       | age l      | nitial     | U-2        | 35 E       | nrich | men        | t, wt      | %          |            |            |            |     |            |            |            |            |            |            |            |
|---------------|-----|---|-------|-------|-------|--------|-----------------|-------|-------|-------|-------|------------|------------|------------|------------|------------|------------|-------|------------|------------|------------|------------|------------|------------|-----|------------|------------|------------|------------|------------|------------|------------|
| Up,<br>GWD/MT | 1.5 | 2.0   | 2.1   | 2.2   | 2.3   | 2.4    | 2.5             | 2.6   | 2.7   | 2.8   | 2.9   | 3.0        | 3.1        | 3.2        | 3.3        | 3.4        | 3.5        | 3.6   | 3.7        | 3.8        | 3.9        | 4.0        | 4.1        | 4.2        | 4.3 | 4.4        | 4.5        | 4.6        | 4.7        | 4.8        | 4.9        | 5.0        |
| 10            | 3.0 | 3.0   | 3.0   | 3.0   | 3.0   | 3.0    | 3.0             | 3.0   | 3.0   | 3.0   | 3.0   | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | _     | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0 | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        |
| 15            | 3.0 | 3.0   | 3.0   | 3.0   | 3.0   | 3.0    | 3.0             | 3.0   | 3.0   | 3.0   | 3.0   | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0   | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0 | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        |
| 20            | 3.0 | 3.0   | 3.0   | 3.0   | 3.0   | 3.0    | 3.0             | 3.0   | 3.0   | 3.0   | 3.0   | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0   | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0 | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        |
| 25            |     |   | 3.0   | 3.0   | 3.0   | 3.0    | 3.0             | 3.0   | 3.0   | 3.0   | 3.0   | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0   | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0 | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        |
| 28            |     |   |       | 3.0   | 3.0   | 3.0    | 3.0             | 3.0   | 3.0   | 3.0   | 3.0   | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0   | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0 | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        |
| 30            |     |   |       |       |       |        | 3.0             | 3.0   | 3.0   | 3.0   | 3.0   |            | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        |       | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0 | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        |
| 32            |     |   |       |       |       |        |                 | 3.0   | 3.0   | 3.0   | 3.0   |            | 3.0        | 3.0        | 3.0        | 3.0        |            |       | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | _   | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        |
| 34            |     |   |       |       |       |        |                 |       | 3.0   | 3.0   | 3.0   |            | 3.0        | 3.0        | 3.0        | 3.0        |            |       | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        |     | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        |
| 36            |     | 3.5 3.5 3.5 3.5 3.5 3.5   |       |       |       |        |                 |       |       |       |       |            |            |            |            |            |            |       | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        |     | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        |
| 38            |     | 3.5         3.5         3.5         3.5         3.5         3.5           3.5         3.5         3.5         3.5         3.5         3.5         3.5 |       |       |       |        |                 |       |       |       |       |            |            |            |            |            |            |       | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        |     | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        |
| 39<br>40      |     | 3.5 3.5 3.5 3.5 3.5 3.  |       |       |       |        |                 |       |       |       |       |            |            |            |            |            |            |       | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        |     | 3.5        | 3.5        | 3.5        |            | 3.5        | 3.5        | 3.5        |
| 40            |     | 3.5       3.5       3.5       3.5       3.5       3.5         3.5       3.5       3.5       3.5       3.5       3.5       3.5                         |       |       |       |        |                 |       |       |       |       |            |            |            |            |            |            |       | 3.5        | 3.5        | 3.5        | 3.5        | 3.5<br>3.5 | 3.5<br>3.5 |     | 3.5        | 3.5<br>3.5 | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        |
| 47            |     |   |       |       |       |        |                 |       |       |       |       | 4.0<br>4.0 | 4.0<br>4.0 | 3.5<br>4.0 | 3.5<br>4.0 | 3.5<br>4.0 | 3.5<br>4.0 |       | 3.5<br>3.5 | 3.5<br>3.5 | 3.5<br>3.5 | 3.5<br>3.5 | 3.5<br>3.5 | 3.5        |     | 3.5<br>3.5 |
| 42            |     |   |       |       |       |        |                 |       |       |       |       | 4.0        | 4.0<br>4.0 | 4.0        | 4.0<br>4.0 | 4.0<br>4.0 | 4.0        |       | 4.0        | 3.5<br>4.0 | 3.5<br>4.0 | 3.5<br>4.0 | 3.5<br>4.0 | 4.0        |     | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        |
| 44            |     |   |       |       |       |        |                 |       |       |       |       | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        |       | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        |     | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        |
| 45            |     |   |       |       |       |        |                 |       |       |       |       | 1.0        | 1.0        | 4.0        | 4.0        | 4.0        | 4.0        |       | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        |     | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        |
| 46            |     |   |       |       |       |        |                 |       |       |       |       |            |            | 4.5        | 4.5        | 4.5        | 4.5        | 4.0   | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        |     | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        |
| 47            |     |   |       |       |       |        |                 |       |       |       |       |            |            | 4.5        | 4.5        | 4.5        | 4.5        | 4.5   | 4.5        | 4.5        | 4.5        | 4.5        | 4.0        | 4.0        |     | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        |
| 48            |     |   |       |       |       |        |                 |       |       |       |       |            |            | 4.5        | 4.5        | 4.5        | 4.5        | 4.5   | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5 | 4.5        | 4.5        | 4.5        | 4.0        | 4.0        | 4.0        | 4.0        |
| 49            |     |   |       |       |       |        |                 |       |       |       |       |            |            | 4.5        | 4.5        | 4.5        | 4.5        | 4.5   | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5 | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        |
| 50            |     |   |       |       |       | Not    | <sup>•</sup> An | aly:  | zed   |       |       |            |            |            |            | 5.0        | 5.0        | 5.0   | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5 | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        |
| 51            |     |   |       |       |       |        |                 |       |       |       |       |            |            |            |            | 5.0        | 5.0        | 5.0   | 5.0        | 5.0        | 5.0        | 5.0        | 4.5        | 4.5        | 4.5 | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        |
| 52            |     |   |       |       |       |        |                 |       |       |       |       |            |            |            |            | 5.0        | 5.0        |       | 5.0        | 5.0        |            | 5.0        | 5.0        | 5.0        |     | 5.0        | 5.0        | 5.0        |            | 4.5        | 4.5        | 4.5        |
| 53            |     |   |       |       |       |        |                 |       |       |       |       |            |            |            | ٦.         | 5.5        | 5.0        |       | 5.0        | 5.0        |            | 5.0        | 5.0        | 5.0        |     | 5.0        | 5.0        | 5.0        | _          | 5.0        | 5.0        | 5.0        |
| 54            |     | 1   | Note  | If    | stain | less   | stee            | l rec | onsti | itute | d ro  | ds ar      | e          |            |            | 5.5        | 5.5        |       | 5.5        | 5.5        |            | 5.5        | 5.0        | 5.0        |     | 5.0        | 5.0        | 5.0        |            | 5.0        | 5.0        | 5.0        |
| 55            |     | ľ   | orese | nt in | the   | fuel   | asse            | embl  | y, ac | ld ar | ı ado | litio      | nal        |            |            | 5.5        | 5.5        |       | 5.5        | 5.5        |            | 5.5        | 5.5        | 5.5        |     | 5.5        | 5.0        | 5.0        |            | 5.0        | 5.0        | 5.0        |
| 56            |     | 3   | vear  | ofco  | oolin | ig tir | ne.             |       |       |       |       |            |            |            | İ          | 6.0        | 6.0        |       | 5.5        | 5.5        |            | 5.5        | 5.5        | 5.5        |     | 5.5        | 5.5        | 5.5        |            | 5.5        | 5.5        | 5.0        |
| 57            |     |   |       |       |       |        |                 |       |       |       |       |            |            |            | J '        | 6.0        | 6.0        |       | 6.0        | 6.0        |            | 5.5        | 5.5        | 5.5        |     | 5.5        | 5.5        | 5.5        |            | 5.5        | 5.5        | 5.5        |
| 58            |     |   |       |       |       |        |                 |       |       |       |       |            |            |            |            | 6.0        | 6.0        |       | 6.0        | 6.0        |            | 6.0        | 6.0        | 6.0        |     | 6.0        | 5.5        | 5.5        |            | 5.5        | 5.5        | 5.5        |
| 59<br>60      |     |   |       |       |       |        |                 |       |       |       |       |            |            |            |            | 6.5        | 6.5        |       | 6.5        | 6.0        |            | 6.0        | 6.0        | 6.0        |     | 6.0        | 6.0        | 6.0        | 6.0        | 6.0        | 6.0        | 5.5        |
| 60<br>61      |     |   |       |       |       |        |                 |       |       |       |       |            |            |            |            | 6.5        | 6.5        |       | 6.5        | 6.5        | 6.5        | 6.5        | 6.5        | 6.5        |     | 6.0        | 6.0        | 6.0        | 6.0        | 6.0        | 6.0        | 6.0        |
| 67            |     |   |       |       |       |        |                 |       |       |       |       |            |            |            |            | 7.0<br>7.0 | 7.0<br>7.0 |       | 6.5<br>7.0 | 6.5<br>7.0 |            | 6.5<br>7.0 | 6.5<br>6.5 | 6.5<br>6.5 |     | 6.5<br>6.5 | 6.5<br>6.5 | 6.0<br>6.5 | 6.0<br>6.5 | 6.0<br>6.5 | 6.0<br>6.5 | 6.0<br>6.5 |
| 02            |     |   |       |       |       |        |                 |       |       |       |       |            |            |            |            | 7.0        | 7.0        | 7.0   | 1.0        | 7.0        | 7.0        | 1.0        | 0.0        | 0.5        | 0.5 | 0.5        | 0.5        | 0.5        | 0.5        | 0.5        | 0.3        | 0.5        |

Table 1-3bPWR Fuel Qualification Table for Zone 2 Fuel with 2.0 kW per Assembly for the NUHOMS®-24PTH DSC (Fuel w/o Ccs)

| Burn-         |     |                     |      |       |       |         |       |        |        | As    | ssemi  | bly Av | erage | e Initia | al U -2 | 35 Er      | nrichm     | ent, v     | vt %       |            |            |            |            | - /        |            |            |            |            |            |            |            |            |
|---------------|-----|---------------------|------|-------|-------|---------|-------|--------|--------|-------|--------|--------|-------|----------|---------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|
| Up,<br>GWD/MT | 1.5 | 2.0                 | 2.1  | 2.2   | 2.3   | 2.4     | 2.5   | 2.6    | 2.7    | 2.8   | 2.9    | 3.0    | 3.1   | 3.2      | 3.3     | 3.4        | 3.5        | 3.6        | 3.7        | 3.8        | 3.9        | 4.0        | 4.1        | 4.2        | 4.3        | 4.4        | 4.5        | 4.6        | 4.7        | 4.8        | 4.9        | 5.0        |
| 10            | 3.0 | 3.0                 | 3.0  | 3.0   | 3.0   | 3.0     | 3.0   | 3.0    | 3.0    | 3.0   | 3.0    | 3.0    | 3.0   | 3.0      | 3.0     | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        |
| 15            | 3.0 | 3.0                 | 3.0  | 3.0   | 3.0   | 3.0     | 3.0   | 3.0    | 3.0    | 3.0   | 3.0    | 3.0    | 3.0   | 3.0      | 3.0     | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        |
| 20            | 3.0 | 3.0                 | 3.0  | 3.0   | 3.0   | 3.0     | 3.0   | 3.0    | 3.0    | 3.0   | 3.0    | 3.0    | 3.0   | 3.0      | 3.0     | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        |
| 25            |     |                     | 3.0  | 3.0   | 3.0   | 3.0     | 3.0   | 3.0    | 3.0    | 3.0   | 3.0    | 3.0    | 3.0   | 3.0      | 3.0     | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        |
| 28            |     |                     |      | 3.0   | 3.0   | 3.0     | 3.0   | 3.0    | 3.0    | 3.0   | 3.0    | 3.0    | 3.0   | 3.0      | 3.0     | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        |
| 30            |     |                     |      |       |       | -       | 3.0   | 3.0    | 3.0    | 3.0   | 3.0    | 3.0    | 3.0   | 3.0      | 3.0     | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        |
| 32            |     |                     |      |       |       |         |       | 3.0    | 3.0    | 3.0   | 3.0    | 3.0    | 3.0   | 3.0      | 3.0     | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        |
| 34            |     |                     |      |       |       |         |       |        | 3.0    | 3.0   | 3.0    | 3.0    | 3.0   | 3.0      | 3.0     | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        |
| 36            |     |                     |      |       |       |         |       |        |        |       |        |        |       |          |         |            | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        |
| 38            |     |                     |      |       |       |         |       |        |        |       |        |        |       |          |         |            | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        |
| 39            |     |                     |      |       |       |         |       |        |        |       |        |        |       |          |         |            | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        |
| 40            |     | 3.0 3.0 3.0 3.0 3.0 |      |       |       |         |       |        |        |       |        |        |       |          |         |            | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        |
| 41            |     | 3.5 3.5 3.0 3.0 3.1 |      |       |       |         |       |        |        |       |        |        |       |          |         |            | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        |
| 42            |     |                     |      |       |       |         |       |        |        |       |        | 3.5    | 3.5   | 3.5      | 3.5     | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        |
| 43            |     |                     |      |       |       |         |       |        |        |       |        | 3.5    | 3.5   | 3.5      | 3.5     | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        |
| 44            |     |                     |      |       |       |         |       |        |        |       |        | 3.5    | 3.5   | 3.5      | 3.5     | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        |
| 45            |     |                     |      |       |       |         |       |        |        |       |        |        |       |          |         |            | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        |
| 46            |     | 3.5 3.5 3.5 3.      |      |       |       |         |       |        |        |       |        |        |       |          |         |            | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        |
| 47            |     | 4.0 4.0 4.0 4.      |      |       |       |         |       |        |        |       |        |        |       |          |         |            | 4.0        | 4.0        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        |
| 48            |     | 4.0 4.0 4.0 4       |      |       |       |         |       |        |        |       |        |        |       |          |         |            | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        |
| 49<br>50      |     | 4.0 4.0 4.0 4       |      |       |       |         |       |        |        |       |        |        |       |          |         |            | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 3.5        | 3.5        | 3.5        |
| 50<br>51      |     | Not Analyzed        |      |       |       |         |       |        |        |       |        |        |       |          |         |            | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        |
| 57            |     |                     |      |       |       |         |       |        |        |       |        |        |       |          |         | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        |
| 52<br>53      |     |                     |      |       |       |         |       |        |        |       |        |        |       |          |         | 4.5        | 4.5<br>4.5 | 4.5<br>4.5 | 4.5<br>4.5 | 4.0<br>4.5 | 4.0<br>4.5 | 4.0<br>4.5 | 4.0<br>4.5 | 4.0<br>4.5 | 4.0<br>4.0 | 4.0        |
| 53            |     | Г                   |      |       |       |         |       |        |        |       |        |        |       | ٦        |         | 4.5<br>4.5 | 4.5        | 4.5        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0<br>4.5 | 4.0        | 4.0<br>4.0 | 4.0<br>4.0 |
| 55            |     |                     | Note | e: If | stain | less    | steel | recon  | nstitu | ted r | ods a  | ire    |       |          |         | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.0<br>4.5 | 4.0        |
| 56            |     |                     | nres | ent i | n the | fuel    | asset | mhlv   | add    | an a  | dditid | nal    |       | l i      |         | 4.5<br>5.0 | 4.5        | 4.5        | 4.5<br>4.5 | 4.5        |
| 57            |     |                     |      |       |       | ng tin  |       | linery | , uuu  | un u  | aarti  | Jiiui  |       |          |         | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 4.5<br>5.0 | 4.5<br>5.0 | 4.5<br>5.0 | 5.0        |
| 58            |     |                     | year | 010   | 00111 | ig till | 10.   |        |        |       |        |        |       |          |         | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        |
| 59            |     |                     |      |       |       |         |       |        |        |       |        |        |       |          |         | 5.5        | 5.5        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        |
| 60            |     |                     |      |       |       |         |       |        |        |       |        |        |       |          |         | 6.0        | 5.5        | 5.5        | 5.5        | 5.5        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        |
| 61            |     |                     |      |       |       |         |       |        |        |       |        |        |       |          |         | 5.5        | 5.5        | 5.5        | 5.5        | 5.5        | 5.5        | 5.5        | 5,5        | 5.5        | 5.5        | 5.5        | 5.5        | 5.5        | 5.5        | 5.5        | 5.5        | 5.5        |
| 62            |     |                     |      |       |       |         |       |        |        |       |        |        |       |          |         | 6.0        | 5.5        | 5.5        | 5.5        | 5.5        | 5.5        | 5.5        | 5.5        | 5.5        | 5.5        | 5.5        | 5.5        | 5.5        | 5.5        | 5.5        | 5.5        | 5.5        |
|               |     |                     |      |       |       |         |       |        |        |       |        |        |       |          |         |            |            |            |            |            | L          |            |            |            |            |            |            |            |            |            |            |            |

(Minimum required years of cooling time after reactor core discharge)

 Table 1-3c

 PWR Fuel Qualification Table for Zone 3 Fuel with 1.5 kW per Assembly for the NUHOMS®-24PTH DSC (Fuel w/o CCs)

 (Minimum required users of excline time after reactor age discharge)

| (Minimum required years of cooling time after reactor co | e discharge) | 1 |
|--|--------------|---|
|--|--------------|---|

| Bum-          |     |   |       |        |       |       |       |       |        | As    | sseml  | blv Av | erade | e Initia | IU-2 | 35 En      | richm      | nent, v    | vt %       |            |            |            |            |            |            |            |            |            |            |            |            |            |
|---------------|-----|---|-------|--------|-------|-------|-------|-------|--------|-------|--------|--------|-------|----------|------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|
| Up,<br>GWD/MT | 1.5 | 2.0   | 2.1   | 2.2    | 2.3   | 2.4   | 2.5   | 2.6   | 2.7    | 2.8   | 2.9    | 3.0    | 3.1   | 3.2      | 3.3  | 3.4        | 3.5        | 3.6        | 3.7        | 3.8        | 3.9        | 4.0        | 4.1        | 4.2        | 4.3        | 4.4        | 4.5        | 4,6        | 4.7        | 4.8        | 4.9        | 5.0        |
| 10            | 3.0 | 3.0   | 3.0   | 3.0    | 3.0   | 3.0   | 3.0   | 3.0   | 3.0    | 3.0   | 3.0    | 3.0    | 3.0   | 3.0      | 3.0  | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        |
| 15            | 3.0 | 3.0   | 3.0   | 3.0    | 3.0   | 3.0   | 3.0   | 3.0   | 3.0    | 3.0   | 3.0    | 3.0    | 3.0   | 3.0      | 3.0  | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        |
| 20            | 3.0 | 3.0   | 3.0   | 3.0    | 3.0   | 3.0   | 3.0   | 3.0   | 3.0    | 3.0   | 3.0    | 3.0    | 3.0   | 3.0      | 3.0  | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        |
| 25            |     |   | 3.0   | 3.0    | 3.0   | 3.0   | 3.0   | 3.0   | 3.0    | 3.0   | 3.0    | 3.0    | 3.0   | 3.0      | 3.0  | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        |
| 28            |     |   |       | 3.0    | 3.0   | 3.0   | 3.0   | 3.0   | 3.0    | 3.0   | 3.0    | 3.0    | 3.0   | 3.0      | 3.0  | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        |
| 30            |     |   |       |        |       |       | 3.0   | 3.0   | 3.0    | 3.0   | 3.0    | 3.0    | 3.0   | 3.0      | 3.0  | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        |
| 32            |     |   |       |        |       |       |       | 3.0   | 3.0    | 3.0   | 3.0    | 3.0    | 3.0   | 3.0      | 3.0  | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        |
| 34            |     |   |       |        |       |       |       |       | 3.5    | 3.5   | 3.5    | 3.5    | 3.5   | 3.5      | 3.5  | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        |
| 36            |     | 3.5         3.5         3.5         3.5         3.5         3.5         3.5           4.0         4.0         4.0         4.0         4.0 |       |        |       |       |       |       |        |       |        |        |       |          |      |            | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        |
| 38            |     |   |       |        |       |       |       |       |        |       |        |        |       |          |      |            | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        |
| 39            |     |   |       |        |       |       |       |       |        |       |        |        |       |          |      |            | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        |
| 40            |     | 4.04.04.04.04.04.04.04.04.04.0  |       |        |       |       |       |       |        |       |        |        |       |          |      |            | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 3.5        |
| 41            |     |   |       |        |       |       |       |       |        |       |        | 4.0    | 4.0   | 4.0      | 4.0  | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        |
| 42            |     |   |       |        |       |       |       |       |        |       |        | 4.5    | 4.5   | 4.5      | 4.5  | 4.5        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        |
| 43            |     |   |       |        |       |       |       |       |        |       |        | 4.5    | 4.5   | 4.5      | 4.5  | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        |
| 44            |     |   |       |        |       |       |       |       |        |       |        | 4.5    | 4.5   | 4.5      | 4.5  | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.0        | 4.0        | 4.0        | 4.0        |
| 45            |     |   |       |        |       |       |       |       |        |       |        |        |       | 4.5      | 4.5  | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        |
| 46            |     |   |       |        |       |       |       |       |        |       |        |        |       |          |      |            | 5.0        | 5.0        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        |
| 47            |     | 5.0 5.0 5.0   |       |        |       |       |       |       |        |       |        |        |       |          |      |            | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        |
| 48<br>49      |     | 5.0 5.0 5.0   |       |        |       |       |       |       |        |       |        |        |       |          |      |            | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 4.5        | 4.5        |
| 49<br>50      |     | 5.5 5.5 5.5   |       |        |       |       |       |       |        |       |        |        |       |          |      |            | 5.5        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        |
| 50            |     |   |       |        |       | ΝΟί   | Alla  | iyze  | u      |       |        |        |       |          |      | 5.5<br>5.5 | 5.0<br>5.5 | 5.0<br>5.0 | 5.0<br>5.0 | 5.0<br>5.0 |
| 52            |     |   |       |        |       |       |       |       |        |       |        |        |       |          |      | 5.5<br>6.0 | 5.5<br>6.0 | 5.5<br>6.0 | 5.5<br>5.5 | 5.0<br>5.5 | 5.0<br>5.5 | 5.0        |
| 53            |     |   |       |        |       |       |       |       |        |       |        |        |       |          |      | 6.0        | 6.0        | 6.0        | 5.5<br>6.0 | 5.5<br>6.0 | 5.5<br>6.0 | 5.5<br>6.0 | 5.5<br>6.0 | 5.5<br>6.0 | 5.5<br>5.5 | 5.5<br>5.5 | 5.5        | 5.5<br>5.5 | 5.5        | 5.5<br>5.5 | 5.5        | 5.5        |
| 54            |     |   |       | TC     |       |       | . 1   |       |        | 1     | 1      |        |       | 1        |      | 6.5        | 6.5        | 6.0        | 6.0        | 6.0        | 6.0        | 6.0        | 6.0        | 6.0        | 6.0        | 6.0        | 6.0        | 6.0        | 6.0        | 5.5        | 5.5        | 5.5        |
| 55            |     |   |       |        |       |       |       |       | stitut |       |        |        |       |          |      | 6.5        | 6.5        | 6.5        | 6.5        | 6.5        | 6.5        | 6.5        | 6.0        | 6.0        | 6.0        | 6.0        | 6.0        | 6.0        | 6.0        | 6.0        | 6.0        | 6.0        |
| 56            |     |   | prese | ent in | the f | fuel, | assen | nbly, | add    | an ac | lditic | onal   |       |          |      | 7.0        | 6.5        | 6.5        | 6.5        | 6.5        | 6.5        | 6.5        | 6.5        | 6.5        | 6,5        | 6.5        | 6.5        | 6.0        | 6.0        | 6,0        | 6.0        | 6.0        |
| 57            |     |   | year  | ofco   | oling | g tim | e.    |       |        |       |        |        |       |          |      | 7.0        | 7.0        | 7.0        | 7.0        | 7.0        | 7.0        | 6.5        | 6.5        | 6.5        | 6.5        | 6.5        | 6.5        | 6.5        | 6.5        | 6.5        | 6.5        | 6.5        |
| 58            |     |   |       |        |       |       |       |       |        | _     | _      |        |       |          |      | 7.5        | 7.5        | 7.5        | 7.0        | 7.0        | 7.0        | 7.0        | 7.0        | 7.0        | 7.0        | 7.0        | 6.5        | 6.5        | 6.5        | 6.5        | 6.5        | 6.5        |
| 59            |     |   |       |        |       |       |       |       |        |       |        |        |       |          |      | 7.5        | 7.5        | 7.5        | 7.5        | 7.5        | 7.5        | 7.5        | 7.5        | 7.0        | 7.0        | 7.0        | 7.0        | 7.0        | 7.0        | 7.0        | 6.5        | 7.0        |
| 60            |     |   |       |        |       |       |       |       |        |       |        |        |       |          |      | 8.0        | 8.0        | 8.0        | 7.5        | 7.5        | 7.5        | 7.5        | 7.5        | 7.5        | 7.5        | 7.5        | 7.5        | 7.0        | 7.0        | 7.0        | 7.0        | 7.0        |
| 61            |     |   |       |        |       |       |       |       |        |       |        |        |       |          |      | 8.5        | 8.0        | 8.0        | 8.0        | 8.0        | 8.0        | 8.0        | 8.0        | 7.5        | 7.5        | 7.5        | 7.5        | 7.5        | 7.5        | 7.5        | 7.5        | 7.5        |
| 62            |     |   |       |        |       |       |       |       |        |       |        |        |       |          |      | 8.5        | 8.5        | 8.5        | 8.5        | 8.5        | 8.5        | 8.0        | 8.0        | 8.0        | 8.0        | 8.0        | 8.0        | 8.0        | 7.5        | 7.5        | 7.5        | 7.5        |

## Table 1-3d PWR Fuel Qualification Table for Zone 4 Fuel with 1.3 kW per Assembly for the NUHOMS®-24PTH DSC (Fuel w/o CCs)

| _   |     |     |     |     |     |     |     |     |     |      |        |       |          |         |       |        |         |      |     |     |     |     |     |     |     |     |     |     |     | _ |
|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|------|--------|-------|----------|---------|-------|--------|---------|------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|---|
|     |     |     |     |     |     |     |     |     | A   | ssem | bly Av | erage | e Initia | al U -2 | 35 Er | nrichm | ient, v | vt % |     |     |     |     |     |     |     |     |     |     |     |   |
| 1.5 | 2.0 | 2.1 | 2.2 | 2.3 | 2.4 | 2.5 | 2.6 | 2.7 | 2.8 | 2.9  | 3.0    | 3.1   | 3.2      | 3.3     | 3.4   | 3.5    | 3.6     | 3.7  | 3.8 | 3.9 | 4.0 | 4.1 | 4.2 | 4.3 | 4.4 | 4.5 | 4.6 | 4.7 | 4.8 |   |
| 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0  | 3.0    | 3.0   | 3.0      | 3.0     | 3.0   | 3.0    | 3.0     | 3.0  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | Γ |
| 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0  | 3.0    | 3.0   | 3.0      | 3.0     | 3.0   | 3.0    | 3.0     | 3.0  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |   |
| 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0  | 3.0    | 3.0   | 3.0      | 3.0     | 3.0   | 3.0    | 3.0     | 3.0  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |   |
|     |     | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0  | 3.0    | 3.0   | 3.0      | 3.0     | 3.0   | 3.0    | 3.0     | 3.0  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |   |
|     |     |     | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0  | 3.0    | 3.0   | 3.0      | 3.0     | 3.0   | 3.0    | 3.0     | 3.0  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |   |
|     |     |     |     |     |     | 3.5 | 3.5 | 3.5 | 3.5 | 3.5  | 3.5    | 3.5   | 3.5      | 3.5     | 3.0   | 3.0    | 3.0     | 3.0  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |   |
|     |     |     |     |     |     |     | 3.5 | 3.5 | 3.5 | 3.5  | 3.5    | 3.5   | 3.5      | 3.5     | 3.5   | 3.5    | 3.5     | 3.5  | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 |   |
|     |     |     |     |     |     |     |     | 4.0 | 4.0 | 4.0  | 4.0    | 4.0   | 4.0      | 3.5     | 3.5   | 3.5    | 3.5     | 3.5  | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 |   |
|     |     |     |     |     |     |     |     |     | 4.0 | 4.0  | 4.0    | 4.0   | 4.0      | 4.0     | 4.0   | 4.0    | 4.0     | 4.0  | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |   |
|     |     |     |     |     |     |     |     |     |     |      | 4.5    | 4.5   | 4.5      | 4.5     | 4.5   | 4.0    | 4.0     | 4.0  | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |   |
|     |     |     |     |     |     |     |     |     |     |      | 4.5    | 4.5   | 4.5      | 4.5     | 4.5   | 4.5    | 4.5     | 4.5  | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |   |
|     |     |     |     |     |     |     |     |     |     |      | 4.5    | 4.5   | 4.5      | 4.5     | 4.5   | 4.5    | 4.5     | 4.5  | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 |   |
|     |     |     |     |     |     |     |     |     |     |      | 5.0    | 5.0   | 5.0      | 4.5     | 4.5   | 4.5    | 4.5     | 4.5  | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 |   |
|     |     |     |     |     |     |     |     |     |     |      | 5.0    | 5.0   | 5.0      | 5.0     | 5.0   | 5.0    | 5.0     | 5.0  | 5.0 | 5.0 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 |   |
|     |     |     |     |     |     |     |     |     |     |      | 5.0    | 5.0   | 5.0      | 5.0     | 5.0   | 5.0    | 5.0     | 5.0  | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 4.5 | 4.5 |   |
|     |     |     |     |     |     |     |     |     |     |      | 5.5    | 5.5   | 5.5      | 5.5     | 5.5   | 5.0    | 5.0     | 5.0  | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |   |
|     |     |     |     |     |     |     |     |     |     |      |        |       | 5.5      | 5.5     | 5.5   | 5.5    | 5.5     | 5.5  | 5.5 | 5.5 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |   |
|     |     |     |     |     |     |     |     |     |     |      |        |       | 5.5      | 5.5     | 5.5   | 5.5    | 5.5     | 5.5  | 5.5 | 5.5 | 5.5 | 5.5 | 5.5 | 5.5 | 5.5 | 5.5 | 5.0 | 5.0 | 5.0 |   |
|     |     |     |     |     |     |     |     |     |     |      |        |       | 6.0      | 6.0     | 6.0   | 6.0    | 5.5     | 5.5  | 5.5 | 5.5 | 5.5 | 5.5 | 5.5 | 5.5 | 5.5 | 5.5 | 5.5 | 5.5 | 5.5 |   |
|     |     |     |     |     |     |     |     |     |     |      |        |       | 6.0      | 6.0     | 6.0   | 6.0    | 6.0     | 6.0  | 6.0 | 6.0 | 6.0 | 5.5 | 5.5 | 5.5 | 5.5 | 5.5 | 5.5 | 5.5 | 5.5 | Г |

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7.0

7.0

7.5

7.5 7.5

8.0

8.5

9.0

9.0

10.0

10.0

6.0

7.0 7.0 7.0 7.0 7.0

7.5 7.0 7.0 7.0 7.0

7.5

8.5 8.5 8.0

9.0 8.5 8.5 8.5 8.5

9.0 9.0 9.0 9.0 9.0

9.5 9.5 9.5 9.5 9.5

6.5 6.5 6.5 6.5

7.5

8.0 8.0 8.0 8.0

11.0 10.5 10.5 10.5 10.5 10.5

6.0

6.0 6.0

6.5 6.5

8.0 7.5

8.0 8.0

6.0

7.5 7.5 7.5 7.5

10.0

10.0 10.0 10.0 5.0 5.0

5.0 5.0

5.5 5.5

5.5

6.0 6.0

6.0

8.0

5.0

3.0

3.5

4.5

5.5

6.0

6.5

7.0

8.0

9.5

10.0

Page A-53 provides the explanatory notes and limitations regarding the use of this Table. Note:

Not Analyzed

Note: If stainless steel reconstituted rods are

present in the fuel, assembly, add an additional

year of cooling time or for cooling times less than

Burn Up, GWD/MT

> 10 3

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20 3

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10 years.

 Table 1-3e

 PWR Fuel Qualification Table for Zone 1 Fuel with 1.7 kW per Assembly for the NUHOMS®-24PTH DSC (Fuel w/ CCs) (Minimum required years of cooling time after reactor core discharge)

| Burn-         |     |                     |       |        |       |        |        |       |       | A     | ssen  | nbly A | Avera | age l | nitial | U-2        | 35 E       | nrich | men        | t, wt      | %          |            |            |            |            |            |            |            |            |            |            |            |
|---------------|-----|---------------------|-------|--------|-------|--------|--------|-------|-------|-------|-------|--------|-------|-------|--------|------------|------------|-------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|
| Up,<br>GWD/MT | 1.5 | 2.0                 | 2.1   | 2.2    | 2.3   | 2.4    | 2.5    | 2.6   | 2.7   | 2.8   | 2.9   | 3.0    | 3.1   | 3.2   | 3.3    | 3.4        | 3.5        |       | 3.7        | 3.8        | 3.9        | 4.0        | 4.1        | 4.2        | 4.3        | 4.4        | 4.5        | 4.6        | 4.7        | 4.8        | 4.9        | 5.0        |
| 10            | 3.0 | 3.0                 | 3.0   | 3.0    | 3.0   | 3.0    | 3.0    | 3.0   | 3.0   | 3.0   | 3.0   | 3.0    | 3.0   | 3.0   | 3.0    | 3.0        | 3.0        | 3.0   | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        |
| 15            | 3.0 | 3.0                 | 3.0   | 3.0    | 3.0   | 3.0    | 3.0    | 3.0   | 3.0   | 3.0   | 3.0   | 3.0    | 3.0   | 3.0   | 3.0    | 3.0        | 3.0        | 3.0   | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        |
| 20            | 3.0 | 3.0                 | 3.0   | 3.0    | 3.0   | 3.0    | 3.0    | 3.0   | 3.0   | 3.0   | 3.0   | 3.0    | 3.0   | 3.0   | 3.0    | 3.0        | 3.0        | 3.0   | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        |
| 25            |     |                     | 3.0   | 3.0    | 3.0   | 3.0    | 3.0    | 3.0   | 3.0   | 3.0   | 3.0   | 3.0    | 3.0   | 3.0   | 3.0    | 3.0        | 3.0        | 3.0   | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        |
| 28            |     |                     |       | 3.0    | 3.0   | 3.0    | 3.0    | 3.0   | 3.0   | 3.0   | 3.0   | 3.0    | 3.0   | 3.0   | 3.0    | 3.0        | 3.0        | 3.0   | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        |
| 30            |     |                     |       |        |       |        | 3.0    | 3.0   | 3.0   | 3.0   | 3.0   | 3.0    | 3.0   | 3.0   | 3.0    | 3.0        | 3.0        | 3.0   | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        |
| 32            |     |                     |       |        |       |        |        | 3.0   | 3.0   | 3.0   | 3.0   | 3.0    | 3.0   | 3.0   | 3.0    | 3.0        | 3.0        | 3.0   | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        |
| 34            |     |                     |       |        |       |        |        |       | 3.0   | 3.0   | 3.0   | 3.0    | 3.0   | 3.0   | 3.0    | 3.0        | 3.0        | 3.0   | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        |
| 36            |     |                     |       |        |       |        |        |       |       |       |       |        |       |       |        |            |            |       | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        |
| 38            |     |                     |       |        |       |        |        |       |       |       |       |        |       |       |        |            |            |       | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        |            | 3.5        | 3.5        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        |
| 39            |     | 3.5 3.5 3.5 3.5 3.5 |       |        |       |        |        |       |       |       |       |        |       |       |        |            |            |       | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        |            | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        |
| 40            |     |                     |       |        |       |        |        |       |       |       |       | 3.5    | 3.5   | 3.5   | 3.5    | 3.5        |            |       | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        |            | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        |
| 41            |     |                     |       |        |       |        |        |       |       |       |       | 4.0    | 4.0   | 4.0   | 3.5    | 3.5        |            |       | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        |            | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        |
| 42            |     |                     |       |        |       |        |        |       |       |       |       | 4.0    | 4.0   | 4.0   | 4.0    | 4.0        | _          | _     | 4.0        | 4.0        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        |
| 43            |     |                     |       |        |       |        |        |       |       |       |       | 4.0    | 4.0   | 4.0   | 4.0    | 4.0        | 4.0        |       | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        |
| 44            |     |                     |       |        |       |        |        |       |       |       |       | 4.0    | 4.0   | 4.0   | 4.0    | 4.0        |            |       | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        |
| 45            |     |                     |       |        |       |        |        |       |       |       |       |        |       | 4.0   | 4.0    | 4.0        |            |       | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        |
| 46<br>47      |     |                     |       |        |       |        |        |       |       |       |       |        |       | 4.5   | 4.5    |            |            |       | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        |
| 47<br>48      |     |                     |       |        |       |        |        |       |       |       |       |        |       | 4.5   | 4.5    |            |            |       | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        |
| 48<br>49      |     |                     |       |        |       |        |        |       |       |       |       |        |       | 4.5   | 4.5    |            |            |       | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.0        | 4.0        | 4.0        |
| 49<br>50      |     |                     |       |        |       | Not    | f An   |       | -     |       |       |        |       | 4.5   | 4.5    |            | 4.5        |       | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        |
| 50<br>51      |     | Not Analyzed        |       |        |       |        |        |       |       |       |       |        |       |       |        |            | 5.0<br>5.0 |       | 5.0<br>5.0 | 4.5        | 4.5<br>5.0 | 4.5<br>5.0 | 4.5        | 4.5<br>5.0 | 4.5<br>4.5 | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        |
| 52            |     |                     |       |        |       |        |        |       |       |       |       |        |       |       | ٦.     | 5.0<br>5.0 | 5.0        |       | 5.0<br>5.0 | 5.0<br>5.0 | 5.0<br>5.0 | 5.0<br>5.0 | 5.0<br>5.0 | 5.0<br>5.0 | 4.5<br>5.0 | 4.5<br>5.0 | 4.5<br>5.0 | 4.5<br>5.0 | 4.5<br>5.0 | 4.5<br>4.5 | 4.5<br>4.5 | 4.5<br>4.5 |
| 53            |     | 1                   | Note  | : If   | stain | less   | stee   | l rec | onsti | itute | d roo | ds ar  | e     |       |        | 5.0<br>5.5 | 5.0<br>5.5 |       | 5.0<br>5.0 | 5.0        | 5.0<br>5.0 | 5.0<br>5.0 | 5.0        | 5.0<br>5.0 | 5.0<br>5.0 | 5.0<br>5.0 | 5.0<br>5.0 | 5.0        | 5.0        | 4.5<br>5.0 | 4.5<br>5.0 | 4.5<br>5.0 |
| 54            |     | 1                   | orese | ent ir | 1 the | fuel   | l, ass | emb   | ly, a | dd a  | n ad  | ditio  | nal   |       | Í      | 5.5<br>5.5 | 5.5        |       | 5.0        | 5.0        | 5.5        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        |
| 55            |     |                     |       |        |       | ng tir |        |       | •     |       |       |        |       |       | l i    | 5.5        | 5.5        |       | 5.5        | 5.5        | 5.5        | 5.5        | 5.5        | 5.5        | 5.5        | 5.5        | 5.5        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        |
| 56            |     | Ľ                   |       |        |       | 8      |        |       |       |       |       |        |       |       | _ ' _  | 6.0        | 6.0        |       | 5.5        | 5.5        | 5.5        | 5.5        | 5.5        | 5.5        | 5.5        | 5.5        | 5.5        | 5.5        | 5.5        | 5.5        | 5.5        | 5.5        |
| 57            |     |                     |       |        |       |        |        |       |       |       |       |        |       |       |        | 6.0        | 6.0        | 6.0   | 6.0        | 6.0        | 6.0        | 6.0        | 5.5        | 5.5        | 5.5        | 5.5        | 5.5        | 5.5        | 5.5        | 5.5        | 5.5        | 5.5        |
| 58            |     |                     |       |        |       |        |        |       |       |       |       |        |       |       |        | 6.5        | 6.0        | 6.0   | 6.0        | 6.0        | 6.0        | 6.0        | 6.0        | 6.0        | 6.0        | 6.0        | 6.0        | 5.5        | 5.5        | 5.5        | 5.5        | 5.5        |
| 59            |     |                     |       |        |       |        |        |       |       |       |       |        |       |       |        | 6.5        | 6.5        | 6.5   | 6.5        | 6.5        | 6.0        | 6.0        | 6.0        | 6.0        | 6.0        | 6.0        | 6.0        | 6.0        | 6.0        | 6.0        | 6.0        | 6.0        |
| 60            |     |                     |       |        |       |        |        |       |       |       |       |        |       |       |        | 6.5        | 6.5        | 6.5   | 6.5        | 6.5        | 6.5        | 6.5        | 6.5        | 6.5        | 6.0        | 6.0        | 6.0        | 6.0        | 6.0        | 6.0        | 6.0        | 6.0        |
| 61            |     |                     |       |        |       |        |        |       |       |       |       |        |       |       |        | 7.0        | 7.0        | 7.0   | 7.0        | 6.5        | 6.5        | 6.5        | 6.5        | 6.5        | 6.5        | 6.5        | 6.5        | 6.5        | 6.5        | 6.0        | 6.0        | 6.0        |
| 62            |     |                     |       |        |       |        |        |       |       |       |       |        |       |       |        | 7.0        | 7.0        | 7.0   | 7.0        | 7.0        | 7.0        | 7.0        | 7.0        | 6.5        | 6.5        | 6.5        | 6.5        | 6.5        | 6.5        | 6.5        | 6.5        | 6.5        |

 Table 1-3f

 PWR Fuel Qualification Table for Zone 2 Fuel with 2.0 kW per Assembly for the NUHOMS®-24PTH DSC (Fuel w/ CCs)

| ( | Minimum | required | vears of | f cooling | time | after reacto | r core | discharge | ) |
|---|---------|----------|----------|-----------|------|--------------|--------|-----------|---|
|   |         |          |          |           |      |              |        |           |   |

| Burn-    |     |       |      |            |            |            |            |            |            | As         | ssemi      | olv Av     | erage      | e Initia   | I U -2     | 35 Er      | richm      | ent. v     | vt %       |            |            |            |            |            |            |            |            |            |            |            |            |            |
|----------|-----|-------|------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|
| Up,      |     |       |      |            |            |            |            |            |            |            |            |            |            |            |            |            |            |            |            |            |            |            |            |            |            |            |            |            |            |            |            |            |
| GWD/MT   | 1.5 | 2.0   | 2.1  | 2.2        | 2.3        | 2.4        | 2.5        | 2.6        | 2.7        | 2.8        |            | 3.0        | 3.1        | 3.2        | 3.3        | 3.4        | 3.5        | 3.6        | 3.7        | 3.8        | 3.9        | 4.0        | 4.1        | 4.2        | 4.3        | 4.4        | 4.5        | 4.6        | 4.7        | 4.8        | 4.9        | 5.0        |
| 10       | 3.0 | 3.0   | 3.0  | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        |            | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        |
| 15       | 3.0 | 3.0   | 3.0  | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        |
| 20<br>25 | 3.0 | 3.0   | 3.0  | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        |
| 25       |     |       | 3.0  | 3.0<br>3.0 | 3.0<br>3.0 | 3.0<br>3.0 | 3.0<br>3.0 | 3.0<br>3.0 | 3.0        | 3.0<br>3.0 | 3.0<br>3.0 | 3.0        | 3.0<br>3.0 | 3.0<br>3.0 | 3.0<br>3.0 | 3.0        | 3.0<br>3.0 | 3.0<br>3.0 | 3.0        | 3.0<br>3.0 | 3.0<br>3.0 | 3.0<br>3.0 | 3.0<br>3.0 | 3.0<br>3.0 | 3.0        | 3.0<br>3.0 | 3.0<br>3.0 | 3.0<br>3.0 | 3.0        | 3.0        | 3.0<br>3.0 | 3.0        |
| 30       |     |       |      | 3.0        | 3.0        | 3.0        | 3.0        | 3.0<br>3.0 | 3.0<br>3.0 | 3.0        | 3.0        | 3.0<br>3.0 | 3.0<br>3.0 | 3.0<br>3.0 | 3.0<br>3.0 | 3.0<br>3.0 | 3.0        | 3.0<br>3.0 | 3.0<br>3.0 | 3.0        | 3.0<br>3.0 | 3.0        | 3.0        | 3.0        | 3.0<br>3.0 | 3.0<br>3.0 | 3.0        | 3.0        | 3.0<br>3.0 | 3.0<br>3.0 | 3.0        | 3.0<br>3.0 |
| 32       |     |       |      |            |            |            | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        |
| 34       |     |       |      |            |            |            |            | 5.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        |
| 36       |     |       |      |            |            |            |            |            | 0.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        |
| 38       |     |       |      |            |            |            |            |            | L          | 0.0        | 0.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        |
| 39       |     |       |      |            |            |            |            |            |            |            |            | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        |
| 40       |     |       |      |            |            |            |            |            |            |            |            | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        |
| 41       |     |       |      |            |            |            |            |            |            |            |            | 3.5        | 3.5        | 3.5        | 3.5        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        |
| 42       |     |       |      |            |            |            |            |            |            |            |            | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        |
| 43       |     |       |      |            |            |            |            |            |            |            |            | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        |
| 44       |     |       |      |            |            |            |            |            |            |            |            |            |            |            | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        |
| 45       |     |       |      |            |            |            |            |            |            |            |            |            |            |            | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        |
| 46       |     |       |      |            |            |            |            |            |            |            |            |            |            |            | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        |
| 47       |     | 4.0 4 |      |            |            |            |            |            |            |            |            |            |            |            | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        |
| 48       |     |       |      |            |            |            |            |            |            |            |            |            |            |            | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        |
| 49       |     |       |      |            |            |            | _          |            |            |            |            |            |            | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 3.5        |
| 50       |     |       |      |            |            | Not        | Ana        | lyze       | d          |            |            |            |            |            |            | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        |
| 51       |     | Г     |      |            |            |            |            |            |            |            |            |            |            |            |            | 4.5        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        |
| 52       |     |       | Note | : If s     | stainl     | less s     | teel r     | econ       | stituto    | ed ro      | ds ar      | e          | _          |            |            | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        |
| 53       |     |       | pres | ent in     | n the      | fuel,      | asser      | nbly,      | add a      | an ad      | ditio      | nal        | _          |            |            | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        |
| 54       |     |       | year | ofco       | oolin      | g tim      | e.         |            |            |            |            |            | _          | İ          |            | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.0        | 4.0        |
| 55       |     | L     | 5    |            |            | <u> </u>   |            |            |            |            |            |            | _          | 1          |            | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        |
| 56       |     |       |      |            |            |            |            |            |            |            |            |            |            |            |            | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 4.5        | 4.5        | 4.5        | 4.5        |
| 57       |     |       |      |            |            |            |            |            |            |            |            |            |            |            |            | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        |
| 58       |     |       |      |            |            |            |            |            |            |            |            |            |            |            |            | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        |
| 59       |     |       |      |            |            |            |            |            |            |            |            |            |            |            |            | 5.5        | 5.5        | 5.5        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        |
| 60<br>61 |     |       |      |            |            |            |            |            |            |            |            |            |            |            |            | 6.0        | 5.5        | 5.5        | 5.5        | 5.5        | 5.5        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        |
| 61<br>62 |     |       |      |            |            |            |            |            |            |            |            |            |            |            |            | 6.0        | 5.5        | 5.5        | 5.5        | 5.5        | 5.5        | 5.5        | 5.5        | 5.5        | 5.5        | 5.5        | 5.5        | 5.5        | 5.5        | 5.5        | 5.5        | 5.5        |
| 62       |     |       |      |            |            |            |            |            |            |            |            |            |            |            |            | 6.0        | 6.0        | 5.5        | 5.5        | 5.5        | 5.5        | 5.5        | 5.5        | 5.5        | 5.5        | 5.5        | 5.5        | 5.5        | 5.5        | 5.5        | 5.5        | 5.5        |

 Table 1-3g

 PWR Fuel Qualification Table for Zone 3 Fuel with 1.5 kW per Assembly for the NUHOMS®-24PTH DSC (Fuel w/ CCs)

| ( | Minimum | required ve | ars of cooling | g time afte | r reactor core | discharge) |
|---|---------|-------------|----------------|-------------|----------------|------------|
|   |         |             |                |             |                |            |

| Up,<br>GWD/MT 1.5<br>10 3.0<br>15 3.0<br>20 3.0<br>25<br>28 | 0 3.0<br>0 3.0     | 2.1<br>3.0<br>3.0<br>3.0<br>3.0 | 2.2<br>3.0<br>3.0<br>3.0 | 2.3<br>3.0<br>3.0 | 2.4<br>3.0 | 2.5<br>3.0 | 2.6     | 2.7   | 2.8  | 2.9   | 3.0 |     |     |     |            | 1          | - 1        |            |            |            |            |            |            |            |            |            |            |            |            |            |            |
|---|--------------------|---------------------------------|--------------------------|-------------------|------------|------------|---------|-------|------|-------|-----|-----|-----|-----|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|
| 15 3.0<br>20 3.0<br>25                                      | 0 3.0              | 3.0<br>3.0                      | 3.0<br>3.0               |                   |            | 3.0        |         |       |      |       | 3.0 | 3.1 | 3.2 | 3.3 | 3.4        | 3.5        | 3.6        | 3.7        | 3.8        | 3.9        | 4.0        | 4.1        | 4.2        | 4.3        | 4.4        | 4.5        | 4.6        | 4.7        | 4.8        | 4.9        | 5.0        |
| 15 3.0<br>20 3.0<br>25                                      | 0 3.0              | 3.0                             | 3.0                      |                   |            |            | 3.0     | 3.0   | 3.0  | 3.0   | 3.0 | 3.0 | 3.0 | 3.0 | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        |
| 25  | 0 3.0              |                                 |                          |                   | 3.0        | 3.0        | 3.0     | 3.0   | 3.0  | 3.0   | 3.0 | 3.0 | 3.0 | 3.0 | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        |
|   |                    | 3.0                             |                          | 3.0               | 3.0        | 3.0        | 3.0     | 3.0   | 3.0  | 3.0   | 3.0 | 3.0 | 3.0 | 3.0 | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        |
| 28  |                    |                                 | 3.0                      | 3.0               | 3.0        | 3.0        | 3.0     | 3.0   | 3.0  | 3.0   | 3.0 | 3.0 | 3.0 | 3.0 | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        |
|   |                    |                                 | 3.0                      | 3.0               | 3.0        | 3.0        | 3.0     | 3.0   | 3.0  | 3.0   | 3.0 | 3.0 | 3.0 | 3.0 | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        |
| 30  |                    |                                 |                          |                   |            | 3.0        | 3.0     | 3.0   | 3.0  | 3.0   | 3.0 | 3.0 | 3.0 | 3.0 | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        |
| 32  |                    |                                 |                          |                   |            |            | 3.5     | 3.0   | 3.0  | 3.0   | 3.0 | 3.0 | 3.0 | 3.0 | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        |
| 34  |                    |                                 |                          |                   |            |            |         | 3.5   | 3.5  | 3.5   | 3.5 | 3.5 | 3.5 | 3.5 | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        | 3.0        |
| 36  |                    |                                 |                          |                   |            |            |         |       | 3.5  | 3.5   | 3.5 | 3.5 | 3.5 | 3.5 | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        |
| 38  |                    |                                 |                          |                   |            |            |         |       |      |       | 4.0 | 4.0 | 4.0 | 4.0 | 4.0        | 4.0        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        |
| 39  |                    |                                 |                          |                   |            |            |         |       |      |       | 4.0 | 4.0 | 4.0 | 4.0 | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        | 3.5        |
| 40  |                    |                                 |                          |                   |            |            |         |       |      |       | 4.0 | 4.0 | 4.0 | 4.0 | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        |
| 41  |                    |                                 |                          |                   |            |            |         |       |      |       | 4.0 | 4.0 | 4.0 | 4.0 | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        |
| 42  |                    |                                 |                          |                   |            |            |         |       |      |       | 4.5 | 4.5 | 4.5 | 4.5 | 4.5        | 4.5        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        |
| 43  |                    |                                 |                          |                   |            |            |         |       |      |       | 4.5 | 4.5 | 4.5 | 4.5 | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        | 4.0        |
| 44  | 4.5 4.5 4.5<br>5.0 |                                 |                          |                   |            |            |         |       |      |       |     |     |     | 4.5 | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.0        |
| 45  | 5.0                |                                 |                          |                   |            |            |         |       |      |       |     |     |     | 4.5 | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        |
| 46<br>47  |                    |                                 |                          |                   |            |            |         |       |      |       |     |     |     | 5.0 | 5.0        | 5.0        | 5.0        | 5.0        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        |
| 47  |                    |                                 |                          |                   |            |            |         |       |      |       |     |     |     | 5.0 | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        | 4.5        |
| 48<br>49  |                    |                                 |                          |                   |            |            |         |       |      |       |     |     |     | 5.0 | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        | 5.0        |
| 49<br>50  |                    |                                 |                          |                   | Not        | Ano        | alyze   | d     |      |       |     |     | 5.5 | 5.5 | 5.5        | 5.5<br>5.5 | 5.5        | 5.0<br>5.5 | 5.0<br>5.5 | 5.0<br>5.5 | 5.0<br>5.5 | 5.0<br>5.5 | 5.0<br>5.0 | 5.0        | 5.0        | 5.0<br>5.0 | 5.0<br>5.0 | 5.0        | 5.0        | 5.0        | 5.0<br>5.0 |
| 50  |                    |                                 |                          |                   | NOL        | Alla       | iiyze   | u     |      |       |     |     |     |     | 5.5<br>5.5 | 5.5<br>5.5 | 5.5<br>5.5 | 5.5<br>5.5 | 5.5<br>5.5 | 5.5<br>5.5 | 5.5<br>5.5 | 5.5<br>5.5 | 5.0<br>5.5 | 5.0<br>5.5 | 5.0<br>5.5 | 5.0<br>5.5 | 5.0<br>5.5 | 5.0<br>5.5 | 5.0<br>5.0 | 5.0<br>5.0 | 5.0<br>5.0 |
| 52  |                    |                                 |                          |                   |            |            |         |       |      |       |     |     |     |     | 5.5<br>6.0 | 5.5<br>6.0 | 5.5<br>6.0 | 5.5<br>6.0 | 5.5<br>5.5 | 5.5<br>5.5 | 5.5<br>5.5 | 5.5<br>5.5 | 5.5<br>5.5 | 5.5<br>5.5 | 5.5<br>5.5 | 5.5<br>5.5 | 5.5<br>5.5 | 5.5<br>5.5 | 5.0<br>5.5 | 5.0<br>5.5 | 5.0<br>5.5 |
| 53  |                    |                                 |                          |                   |            |            |         |       |      |       |     |     |     |     | 6.0        | 6.0        | 6.0        | 6.0        | 5.5<br>6.0 | 5.5<br>6.0 | 5.5<br>6.0 | 5.5<br>6.0 | 5.5<br>6.0 | 5.5<br>6.0 | 5.5<br>6.0 | 5.5        | 5.5        | 5.5<br>5.5 | 5.5<br>5.5 | 5.5        | 5.5        |
| 54  |                    |                                 |                          |                   |            |            |         |       |      |       |     | ٦.  |     |     | 6.5        | 6.5        | 6.5        | 6.0        | 6.0        | 6.0        | 6.0        | 6.0        | 6.0        | 6.0        | 6.0        | 6.0        | 6.0        | 6.0        | 6.0        | 6.0        | 5.5        |
| 55  | 1                  | lote:                           | If sta                   | ainles            | ss ste     | el rec     | consti  | tuted | rods | are   |     |     |     |     | 6.5        | 6.5        | 6.5        | 6.5        | 6.5        | 6.5        | 6.5        | 6.5        | 6.0        | 6.0        | 6.0        | 6.0        | 6.0        | 6.0        | 6.0        | 6.0        | 6.0        |
| 56  | 1                  | reser                           | nt in t                  | he fu             | iel, as    | ssemt      | oly, ao | dd an | addi | tiona | 1   |     |     |     | 7.0        | 7.0        | 6.5        | 6.5        | 6.5        | 6.5        | 6.5        | 6.5        | 6.5        | 6.5        | 6.5        | 6.5        | 6.5        | 6.0        | 6.0        | 6.0        | 6.0        |
| 57  |                    | ear o                           | f coo                    | ling              | time.      |            |         |       |      |       |     | l i |     |     | 7.0        | 7.0        | 7.0        | 7.0        | 7.0        | 7.0        | 7.0        | 6.5        | 6.5        | 6.5        | 6.5        | 6.5        | 6.5        | 6.5        | 6.5        | 6.5        | 6.5        |
| 58  | Ľ                  |                                 |                          |                   |            |            |         |       | _    |       |     |     |     |     | 7.5        | 7.5        | 7.5        | 7.0        | 7.0        | 7.0        | 7.0        | 7.0        | 7.0        | 7.0        | 7.0        | 7.0        | 6.5        | 6.5        | 6.5        | 6.5        | 6.5        |
| 59  |                    |                                 |                          |                   |            |            |         |       |      |       |     |     |     |     | 7.5        | 7.5        | 7.5        | 7.5        | 7.5        | 7.5        | 7.5        | 7.5        | 7.0        | 7.0        | 7.0        | 7.0        | 7.0        | 7.0        | 7.0        | 7.0        | 7.0        |
| 60  |                    |                                 |                          |                   |            |            |         |       |      |       |     |     |     |     | 8.0        | 8.0        | 8.0        | 8.0        | 8.0        | 7.5        | 7.5        | 7.5        | 7.5        | 7.5        | 7.5        | 7.5        | 7.0        | 7.0        | 7.0        | 7.0        | 7.0        |
| 61  |                    |                                 |                          |                   |            |            |         |       |      |       |     |     |     |     | 8.5        | 8.5        | 8.5        | 8.0        | 8.0        | 8.0        | 8.0        | 8.0        | 8.0        | 7.5        | 7.5        | 7.5        | 7.5        | 7.5        | 7.5        | 7.5        | 7.5        |
| 62  |                    |                                 |                          |                   |            |            |         |       |      |       |     |     |     |     | 9.0        | 8.5        | 8.5        | 8.5        | 8.5        | 8.5        | 8.5        | 8.0        | 8.0        | 8.0        | 8.0        | 8.0        | 8.0        | 8.0        | 7.5        | 7.5        | 7.5        |

 Table 1-3h

 PWR Fuel Qualification Table for Zone 4 Fuel with 1.3 kW per Assembly for the NUHOMS®-24PTH DSC (Fuel w/ CCs)

|  |  |  |  |  | discharge |  |
|--|--|--|--|--|-----------|--|
|  |  |  |  |  |           |  |
|  |  |  |  |  |           |  |
|  |  |  |  |  |           |  |
|  |  |  |  |  |           |  |

| GWDMT       1.5       2.0       2.1       2.2       2.3       2.4       2.5       2.6       2.7       2.8       2.9       3.0       3.1       3.2       3.3       3.4       3.5       3.6       3.7       3.8       3.9       4.0       4.1       4.2       4.3       4.4       4.5       4.6       4.7       4.8         10       3.0   |                |            |     |     |     |     |     |     |     |     |     |     |     |     |     |     | IU-2 |            |     |       |       |        |       |       |        |        |       |       |        |     |     | Burn-         |
|--|----------------|------------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|------|------------|-----|-------|-------|--------|-------|-------|--------|--------|-------|-------|--------|-----|-----|---------------|
| 15       3.0       3.  | 4.9 5          | 4.8        | 4.7 | 4.6 | 4.5 | 4.4 | 4.3 | 4.2 | 4.1 | 4.0 | 3.9 | 3.8 | 3.7 | 3.6 | 3.5 | 3.4 | 3.3  | 3.2        | 3.1 | 3.0   | 2.9   | 2.8    | 2.7   | 2.6   | 2.5    | 2.4    | 2.3   | 2.2   | 2.1    | 2.0 | 1.5 | Up,<br>GWD/MT |
| 15       3.0       3.  | 3.0 3          | 3.0        | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0  | 3.0        | 3.0 | 3.0   | 3.0   | 3.0    | 3.0   | 3.0   | 3.0    | 3.0    | 3.0   | 3.0   | 3.0    | 3.0 | 3.0 | 10            |
| 25       30 <td< td=""><td>3.0 3</td><td>3.0</td><td>3.0</td><td>3.0</td><td>3.0</td><td>3.0</td><td>3.0</td><td>3.0</td><td>3.0</td><td>3.0</td><td>3.0</td><td>3.0</td><td>3.0</td><td></td><td>3.0</td><td>3.0</td><td>3.0</td><td>3.0</td><td>3.0</td><td></td><td>3.0</td><td>3.0</td><td>3.0</td><td>3.0</td><td>3.0</td><td></td><td>3.0</td><td>3.0</td><td>3.0</td><td>3.0</td><td>3.0</td><td></td></td<>  | 3.0 3          | 3.0        | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |     | 3.0 | 3.0 | 3.0  | 3.0        | 3.0 |       | 3.0   | 3.0    | 3.0   | 3.0   | 3.0    |        | 3.0   | 3.0   | 3.0    | 3.0 | 3.0 |               |
| 28       30 <td< td=""><td>3.0 3</td><td>3.0</td><td>3.0</td><td>3.0</td><td>3.0</td><td>3.0</td><td>3.0</td><td>3.0</td><td>3.0</td><td>3.0</td><td>3.0</td><td>3.0</td><td>3.0</td><td>3.0</td><td>3.0</td><td>3.0</td><td>3.0</td><td>3.0</td><td>3.0</td><td>3.0</td><td>3.0</td><td>3.0</td><td>3.0</td><td>3.0</td><td>3.0</td><td>3.0</td><td>3.0</td><td>3.0</td><td>3.0</td><td>3.0</td><td>3.0</td><td>20</td></td<>   | 3.0 3          | 3.0        | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0  | 3.0        | 3.0 | 3.0   | 3.0   | 3.0    | 3.0   | 3.0   | 3.0    | 3.0    | 3.0   | 3.0   | 3.0    | 3.0 | 3.0 | 20            |
| 30       35 <td< td=""><td>3.0 3</td><td>3.0</td><td>3.0</td><td>3.0</td><td>3.0</td><td>3.0</td><td>3.0</td><td>3.0</td><td>3.0</td><td>3.0</td><td>3.0</td><td>3.0</td><td>3.0</td><td>3.0</td><td>3.0</td><td>3.0</td><td>3.0</td><td>3.0</td><td>3.0</td><td>3.0</td><td>3.0</td><td>3.0</td><td>3.0</td><td>3.0</td><td>3.0</td><td>3.0</td><td>3.0</td><td>3.0</td><td>3.0</td><td></td><td></td><td></td></td<>   | 3.0 3          | 3.0        | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0  | 3.0        | 3.0 | 3.0   | 3.0   | 3.0    | 3.0   | 3.0   | 3.0    | 3.0    | 3.0   | 3.0   | 3.0    |     |     |               |
| 32       3.5       3.  | 3.0 3          | 3.0        | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0  | 3.0        | 3.0 | 3.0   | 3.0   | 3.0    | 3.0   | 3.0   | 3.0    | 3.0    | 3.0   | 3.0   |        |     |     |               |
| 34         36         36         36         36         36         37         40   | 3.0 3          | 3.0        | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.5 | 3.5 | 3.5  | 3.5        | 3.5 | 3.5   | 3.5   | 3.5    | 3.5   | 3.5   | 3.5    |        |       |       |        |     |     |               |
| 36         38         38         39         40  | 3.5 3          | 3.5        | 3.5 |     | 3.5 | 3.5 | 3.5 |     |     | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5  | 3.5        | 3.5 | 3.5   | 3.5   | 3.5    | 3.5   | 3.5   |        |        |       |       |        |     |     |               |
| 38         39         40         40         40         40         40         40         40         40         40         40         40         40         40         40         40         40         40         40         41         41         50   | 3.5 3          | 3.5        | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 4.0 | 4.0  | 4.0        | 4.0 | 4.0   | 4.0   | 4.0    | 4.0   |       |        |        |       |       |        |     |     |               |
| 39         40         40         40         40         40         40         41         50  | 4.0 4          | 4.0        | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0  | 4.0        | 4.0 | 4.0   | 4.0   | 4.0    |       |       |        |        |       |       |        |     |     |               |
| 40         41         41         42         42         43         44         50   | 4.0 4          | 4.0        | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |     |     |     | 4.0 |     |     | 4.5 |     |     | 4.5  |            | 4.5 | 4.5   |       |        |       |       |        |        |       |       |        |     |     |               |
| 41         42         42         43         44         50   | 4.0 4          | 4.0        |     |     |     |     |     |     |     |     |     |     |     |     |     |     | 4.5  |            | 4.5 | 4.5   |       |        |       |       |        |        |       |       |        |     |     |               |
| 42         43         43         44         44         45         45         46         47         46         47         48         49         48         49         50   | 4.5 4          | 4.5        |     |     |     |     |     |     |     |     |     |     |     |     |     |     | 4.5  |            |     | 4.5   |       |        |       |       |        |        |       |       |        |     |     |               |
| 43         44         44         44         45         45         46         47         46         47         48         49         50       50       55 <td>4.5 4</td> <td>4.5</td> <td></td> <td>5.0</td> <td></td>   | 4.5 4          | 4.5        |     |     |     |     |     |     |     |     |     |     |     |     |     |     |      |            |     | 5.0   |       |        |       |       |        |        |       |       |        |     |     |               |
| 44         45         45         46         46         46         47         47         48         49         50  | 4.5 4          | 4.5        |     |     |     |     |     |     |     |     |     |     |     |     |     |     |      |            |     |       |       |        |       |       |        |        |       |       |        |     |     |               |
| 45         46         46         46         47         48         49         50       50       50       50       50       50       50       50       50       50       50       50       50       55   | 4.5 4          | 5.0        |     |     |     |     |     | _   |     |     |     |     |     |     |     |     |      |            |     |       |       |        |       |       |        |        |       |       |        |     |     |               |
| 46         47         47         48         49         50       Not Analyzed         51         51   | 5.0 5          |            |     |     |     |     |     |     |     |     |     |     |     |     |     |     |      |            |     |       |       |        |       |       |        |        |       |       |        |     |     |               |
| 47         48         49         50       Not Analyzed         51  | 5.0 5          |            |     |     |     |     |     |     |     |     |     |     |     |     |     |     |      | 5.5<br>6.0 |     |       |       |        |       |       |        |        |       |       |        |     |     |               |
| 48         49         50         Not Analyzed         51   | 5.0 5          |            |     |     |     |     |     |     |     |     |     |     |     |     |     |     |      |            |     |       |       |        |       |       |        |        |       |       |        |     |     |               |
| 49         6.5         6.5         6.5         6.5         6.0   | 5.5 5          |            |     |     |     |     |     |     | _   |     |     |     |     |     |     |     |      |            |     |       |       |        |       |       |        |        |       |       |        |     |     |               |
| 50         Not Analyzed         6.5 <th< td=""><td>5.5 5</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></th<> | 5.5 5          |            |     |     |     |     |     |     |     |     |     |     |     |     |     |     |      |            |     |       |       |        |       |       |        |        |       |       |        |     |     |               |
| 51 7.0 7.0 7.0 6.5 6.5 6.5 6.5 6.5 6.5 6.5 6.5 6.5 6.5   | 6.0 6          |            |     |     |     |     |     |     |     |     |     |     |     |     |     |     | 6.5  | 6.5        | ļ   |       |       |        | ส     | h     | 100    | Nat    |       |       |        |     |     |               |
|  | 6.0 6          |            |     |     |     |     |     |     |     |     |     |     |     |     |     |     |      |            |     |       |       |        | u     | iyze  | Апа    | NOL    |       |       |        | _   |     |               |
|  | 6.0 6          |            |     |     |     |     |     |     |     |     |     |     |     |     |     |     |      |            | 1   |       | s are | d rod  | itute | const | eel re | ss ste | ainle | If st | Note:  |     |     |               |
|  | 6.5 6<br>6.5 6 | 6.5<br>7.0 |     |     |     |     |     |     |     |     |     |     |     |     |     |     |      |            | i   | a1    |       |        |       |       |        |        |       |       |        |     |     |               |
|  | 6.5 6<br>7.0 7 | 7.0        |     |     |     |     |     |     |     |     |     |     |     |     |     |     |      |            |     |       |       |        |       | •     |        |        |       |       | •      |     |     |               |
| 55   | 7.5 7          | 7.5        |     |     |     |     |     |     |     |     |     |     |     |     |     |     |      |            |     | an 10 | ss ma | les le | g un  | 00111 | lor c  | time   | Jung  |       | •      |     |     |               |
| ycais.   | 7.5 7          | 7.5        |     |     |     |     |     |     |     |     |     |     |     |     |     |     |      |            |     |       |       |        |       |       |        |        |       |       | years. |     |     |               |
|  | 8.0 8          | 8.0        |     |     |     |     |     |     |     |     |     |     |     |     |     |     |      |            |     |       |       |        |       |       |        |        |       |       |        |     |     |               |
|  | 8.5 8          | 8.0<br>8.5 |     |     |     |     |     |     |     |     |     |     |     |     |     |     |      |            |     |       |       |        |       |       |        |        |       |       |        |     |     |               |
|  | 8.5 8          | 8.5<br>8.5 |     |     |     |     |     |     |     |     |     | _   |     | _   |     |     |      |            |     |       |       |        |       |       |        |        |       |       |        |     |     |               |
|  | 9.0 9          | 9.5        |     |     |     |     |     |     |     |     |     |     |     |     |     |     |      |            |     |       |       |        |       |       |        |        |       |       |        |     |     |               |
|  | 9.5 9          | 9.5        |     |     |     |     |     |     |     |     |     |     |     |     |     |     |      |            |     |       |       |        |       |       |        |        |       |       |        |     |     |               |
|  | 10.0 10        | 10.0       |     |     |     |     |     |     |     |     |     |     |     |     |     |     |      |            |     |       |       |        |       |       |        |        |       |       |        |     |     |               |

### Notes: Tables 1-3a through 1-3h:

- Burnup = Assembly Average burnup.
- Use burnup and enrichment to lookup minimum cooling time in years. Licensee is responsible for ensuring that uncertainties in fuel enrichment and burnup are correctly accounted for during fuel qualification.
- Round burnup UP to next higher entry, round enrichments DOWN to next lower entry.
- Fuel with an assembly average initial enrichment less than 1.5 (or less than the minimum provided above for each burnup) and greater than 5.0 wt.% U-235 is unacceptable for storage.
- Fuel with a burnup greater than 62 GWd/MTU is unacceptable for storage.
- Fuel with a burnup less than 10 GWd/MTU is acceptable for storage after 3-years cooling.
- See Figures 1-11 through 1-15 for the description of Zones.
- For fuel assemblies reconstituted with uranium-oxide rods, use the assembly average equivalent enrichment to determine the minimum cooling time.
- The cooling times for damaged and intact assemblies are identical.
- *Example*: An intact fuel assembly without CCs, with a decay heat load of 1.7 kW or less, an initial enrichment of 3.65 wt. % U-235 and a burnup of 41.5 GWd/MTU is acceptable for storage after a 4.0 year cooling time as defined by 3.6 wt. % U-235 (rounding down) and 42 GWd/MTU (rounding up) in Table 1-3a.

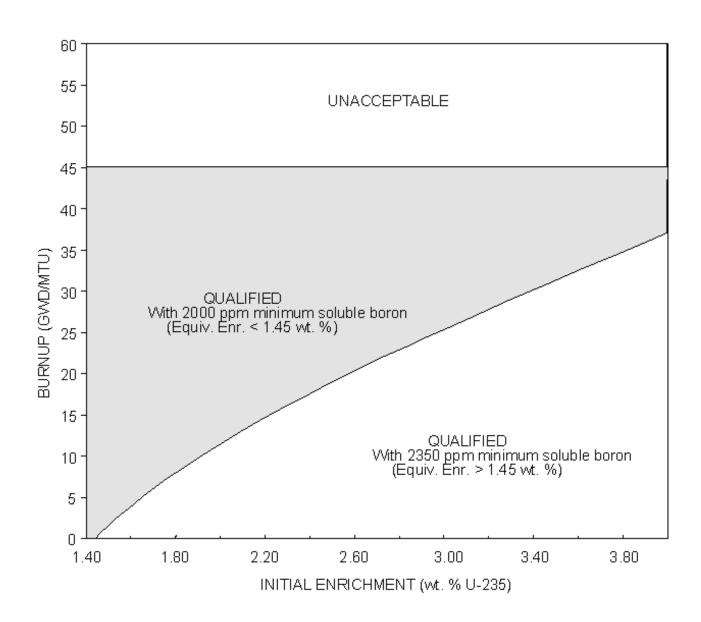


Figure 1-1 PWR Fuel Criticality Acceptance Curve

|      |      |      |      | · · · · · · · · · · · · · · · · · · · |      |
|------|------|------|------|---------------------------------------|------|
|      | 0.87 | 0.87 | 0.87 | 0.87                                  |      |
| 0.87 | 0.63 | 0.63 | 0.63 | 0.63                                  | 0.87 |
| 0.87 | 0.63 | 0.63 | 0.63 | 0.63                                  | 0.87 |
| 0.87 | 0.63 | 0.63 | 0.63 | 0.63                                  | 0.87 |
| 0.87 | 0.63 | 0.63 | 0,63 | 0,63                                  | 0.87 |
|      | 0.87 | 0.87 | 0.87 | 0.87                                  |      |
|      |      |      |      | F5483                                 |      |

Figure 1-2 Heat Load Zoning Configuration 1 for the NUHOMS<sup>®</sup>-32PT DSC

|     | 1.2 | 0.6 | 0.6 | 1.2  |     |
|-----|-----|-----|-----|------|-----|
| 1.2 | 0.6 | 0.6 | 0.6 | 0.6  | 1.2 |
| 0.6 | 0.6 | 0.6 | 0.6 | 0.6  | 0.6 |
| 0.6 | 0.6 | 0.6 | 0.6 | 0.6  | 0.6 |
| 1.2 | Q.6 | 0.6 | 0.6 | 0.6  | 1.2 |
|     | 1.2 | 0.6 | 0.6 | 1.2  |     |
|     |     |     | F   | 5485 |     |

Figure 1-3 Heat Load Zoning Configuration 2 for the NUHOMS<sup>®</sup>-32PT DSC

|     | 0.7 | 0.7 | 0.7 | 0.7  |             |
|-----|-----|-----|-----|------|-------------|
| 0.7 | 0.7 | 0.7 | 0.7 | 0.7  | 0.7         |
| 0.7 | 0.7 | 0.7 | 0.7 | 0.7  | 0. <b>7</b> |
| 0.7 | 0.7 | 0.7 | 0.7 | 0.7  | 0.7         |
| 0.7 | 0.7 | 0.7 | 0.7 | 0.7  | 0.7         |
|     | 0.7 | 0.7 | 0.7 | 0.7  |             |
|     |     |     | F   | 5484 |             |

Figure 1-4 Heat Load Zoning Configuration 3 for the NUHOMS<sup>®</sup>-32PT DSC

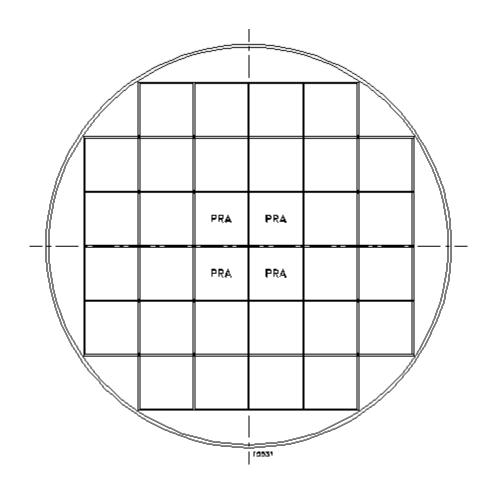
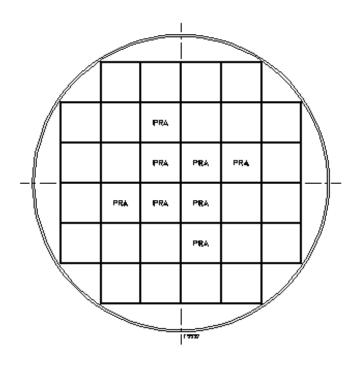


Figure 1-5 Required PRA Locations for the NUHOMS<sup>®</sup>-32PT DSC Configuration with Four PRAs



Or

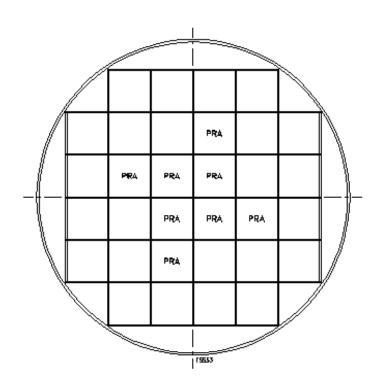


Figure 1-6 Required PRA Locations for the NUHOMS<sup>®</sup>-32PT DSC Configuration with Eight PRAs

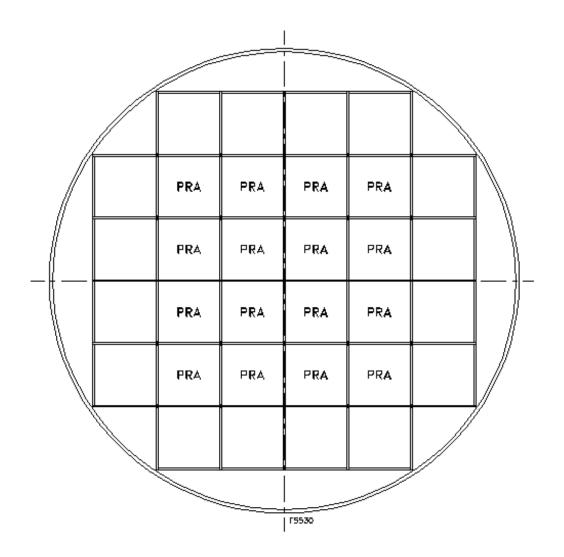
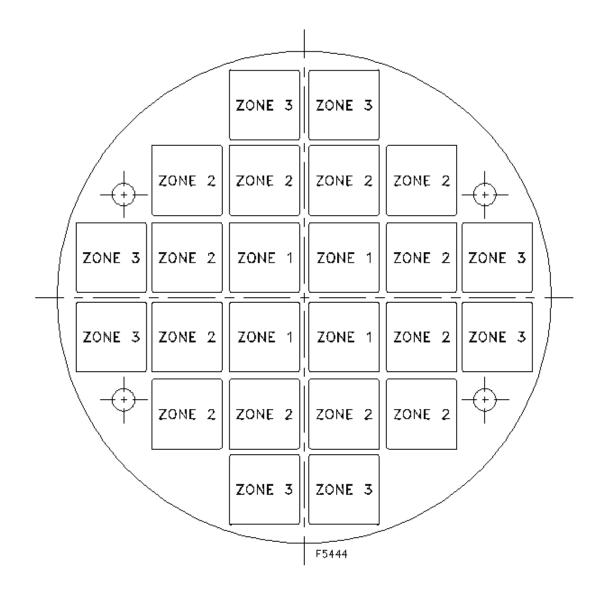
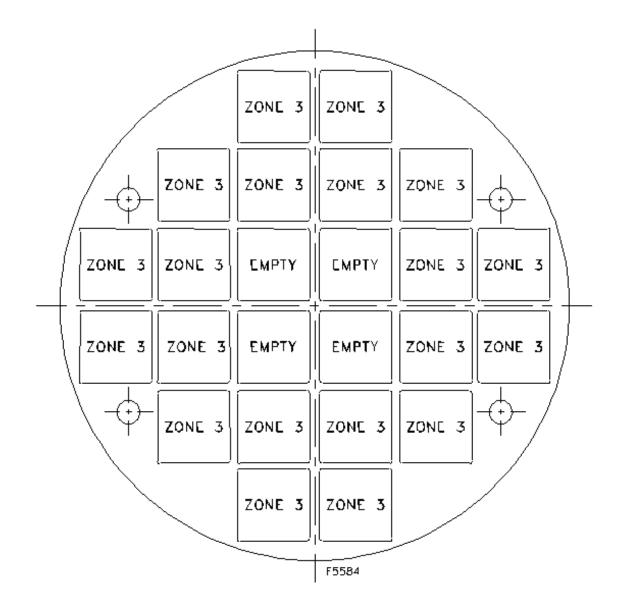


Figure 1-7 Required PRA Locations for the NUHOMS<sup>®</sup>-32PT DSC Configuration with Sixteen PRAs



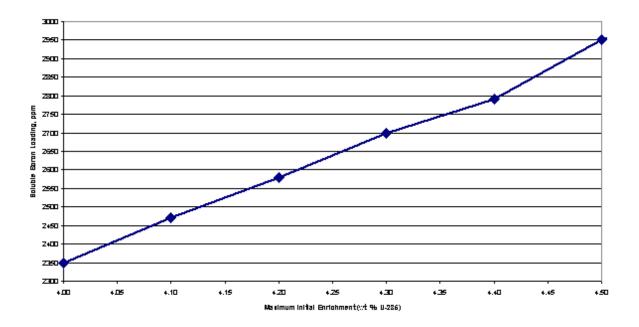
|                                  | Zone 1 | Zone 2 | Zone 3 |
|----------------------------------|--------|--------|--------|
| Maximum Decay Heat (kW / FA)     | 0.7    | 1      | 1.3    |
| Maximum Decay Heat per Zone (kW) | 2.8    | 10.8   | 10.4   |

Figure 1-8 Heat Load Zoning Configuration for Fuel Assemblies (With or Without BPRAs) Stored in NUHOMS<sup>®</sup>-24PHB DSC – Configuration 1



|                                     | Zone 1 | Zone 2 | Zone 3 |
|-------------------------------------|--------|--------|--------|
| Maximum Decay Heat<br>(kW / FA)     | NA     | NA     | 1.3    |
| Maximum Decay Heat per<br>Zone (kW) | NA     | NA     | 24.0   |

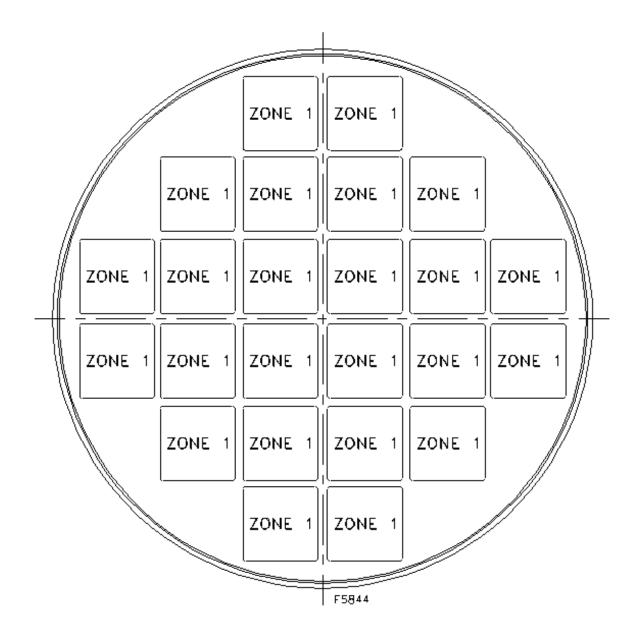
## Figure 1-9 Heat Load Zoning Configuration for Fuel Assemblies (With or Without BPRAs) Stored in NUHOMS<sup>®</sup>-24PHB DSC – Configuration 2



Linear Interpolation allowed between points

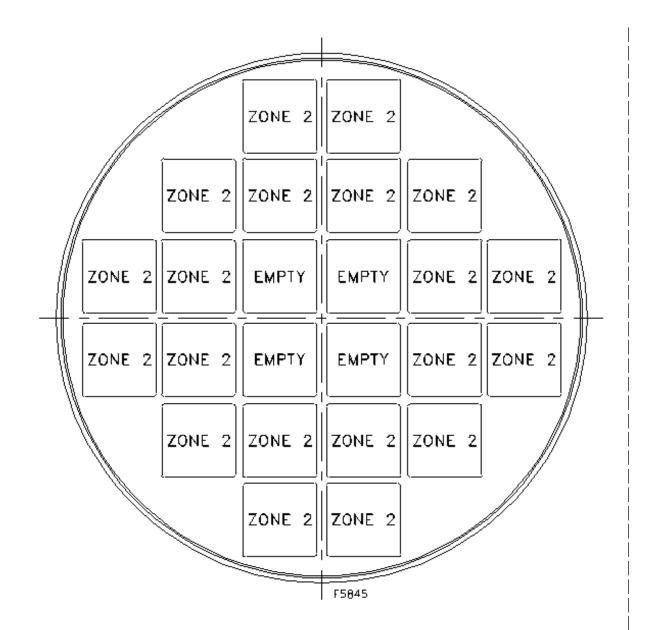
| Initial<br>Enrichment | Boron Loading, ppm |
|-----------------------|--------------------|
| 4.0                   | 2350               |
| 4.1                   | 2470               |
| 4.2                   | 2580               |
| 4.3                   | 2700               |
| 4.4                   | 2790               |
| 4.5                   | 2950               |

Figure 1-10 Soluble Boron Concentration vs. Fuel Initial U-235 Enrichment for the 24PHB System



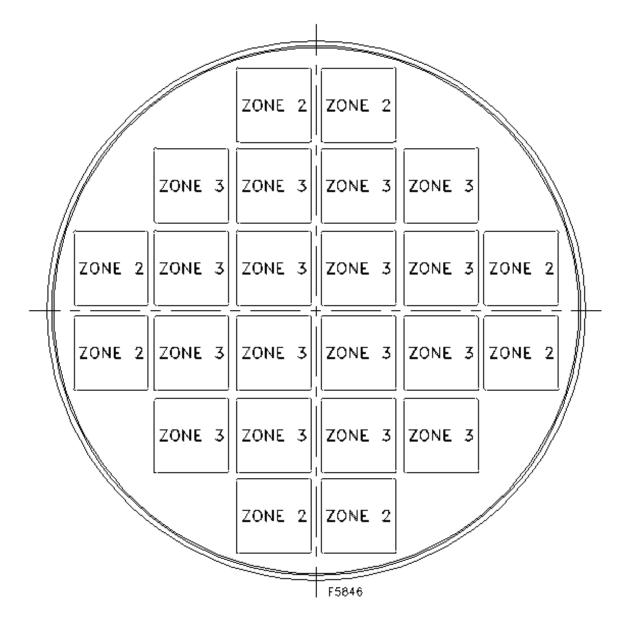
|                                     | Zone 1 | Zone 2 | Zone 3 | Zone 4 |
|-------------------------------------|--------|--------|--------|--------|
| Maximum Decay<br>Heat (kW/FA)       | 1.7    | NA     | NA     | NA     |
| Maximum Decay<br>Heat per Zone (kW) | 40.8   | NA     | NA     | NA     |

Figure 1-11 Heat Load Zoning Configuration No. 1 for 24PTH-S and 24PTH-L DSCs (with or without Control Components)



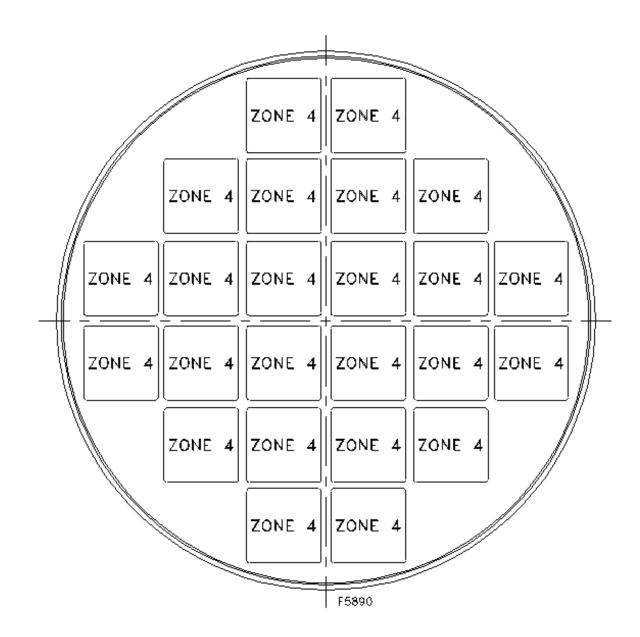
|                                     | Zone 1 | Zone 2 | Zone 3 | Zone 4 |
|-------------------------------------|--------|--------|--------|--------|
| Maximum Decay<br>Heat (kW/FA)       | NA     | 2      | NA     | NA     |
| Maximum Decay<br>Heat per Zone (kW) | NA     | 40     | NA     | NA     |

Figure 1-12 Heat Load Zoning Configuration No. 2 for 24PTH-S and 24PTH-L DSCs (with or without Control Components)



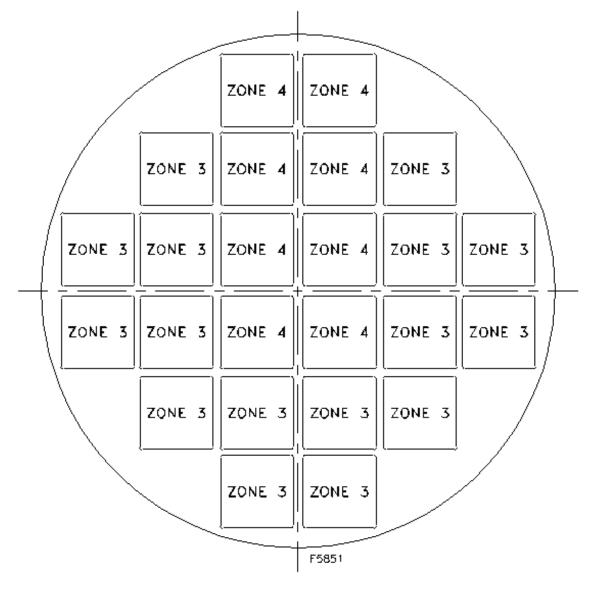
|               | Zone 1 | Zone 2 | Zone 3 | Zone 4 |
|---------------|--------|--------|--------|--------|
| Maximum Decay | NA     | 2      | 1.5    | NA     |
| Heat (kW/FA)  |        | -      | 1.0    |        |
| Maximum Decay |        |        |        |        |
| Heat per Zone | NA     | 16     | 24     | NA     |
| (kW)          |        |        |        |        |

Figure 1-13 Heat Load Zoning Configuration No. 3 for 24PTH-S and 24PTH-L DSCs (with or without Control Components)



|               | Zone 1 | Zone 2 | Zone 3 | Zone 4 |
|---------------|--------|--------|--------|--------|
| Maximum Decay | NA     | NA     | NA     | 13     |
| Heat (kW/FA)  |        |        |        | 1.5    |
| Maximum Decay |        |        |        |        |
| Heat per Zone | NA     | NA     | NA     | 31.2   |
| (kW)          |        |        |        |        |

Figure 1-14 Heat Load Zoning Configuration No. 4 for 24PTH-S and 24PTH-L DSCs (with or without Control Components)



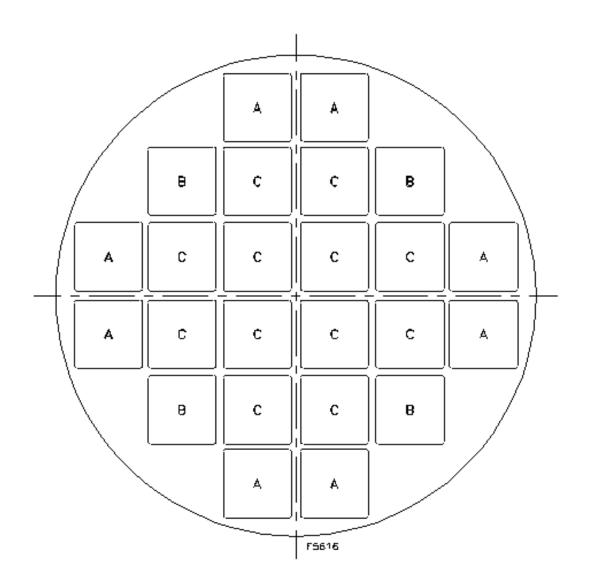
|  | Zone 1 | Zone 2 | Zone 3 | Zone 4 |
|--|--------|--------|--------|--------|
| Maximum Decay<br>Heat (kW/FA)          | NA     | NA     | 1.5    | 1.3    |
| Maximum Decay<br>Heat per Zone<br>(kW) | NA     | NA     | Note 1 | 10.4   |

Notes:

- 1. Fuel assemblies with a maximum heat load of 1.5 kW are permitted in Zone 3 as long as the total of 24 kW/canister maximum heat load is maintained.
- 2. This configuration is applicable to Basket Types 2A, 2B, or 2C only (without aluminum inserts).

Figure 1-15

Heat Load Zoning Configuration No. 5 for 24PTH-S-LC DSC (with or without Control Components)



#### Notes:

- 1. Locations identified as "A" are for placement of up to 8 damaged or intact fuel assemblies.
- 2. Locations identified as "B" are for placement of up to 4 additional damaged or intact fuel assemblies (Maximum of 12 damaged fuel assemblies allowed, Locations "A" and "B" combined).
- 3. Locations identified as "C" are for placement of up to 12 intact fuel assemblies, including 4 empty slots in the center as shown in Figure 1-12.

#### Figure 1-16 Location of Damaged Fuel Inside 24PTH DSC

# 1.2.2 DSC Vacuum Pressure During Drying

## Limit/Specification:

|                | Vacuum Pressure: $\leq 3 \text{ mm Hg}$   |
|----------------|---|
|                | Time at Pressure: $\geq$ 30 minutes following evacuation  |
|                | Number of Pump-Downs: 2   |
| Applicability: | This is applicable to all DSCs. The term "inner top cover" as used in this and<br>other Technical Specifications means either the inner top cover plate or the top<br>shield plug assembly.                 |
| Objective:     | To ensure a minimum water content.  |
| Action:        | If the required vacuum pressure cannot be obtained:   |
|                | 1. Confirm that the vacuum drying system is properly installed.   |
|                | 2. Check and repair, or replace, the vacuum pump.   |
|                | 3. Check and repair the system as necessary.  |
|                | 4. Check and repair the seal weld between the inner top cover and the DSC shell.  |
| Surveillance:  | No maintenance or tests are required during normal storage. Surveillance of the vacuum gauge is required during the vacuum drying operation.  |
| Bases:         | A stable vacuum pressure of 3 mm Hg further ensures that all liquid water has evaporated in the DSC cavity, and that the resulting inventory of oxidizing gases in the DSC is well below the 0.25 volume %. |

#### 1.2.3 24P and 52B DSC Helium Backfill Pressure

## Limit/Specifications:

|                | Helium 2.5 $psig \pm 2.5 psig$ backfill pressure (stable for 30 minutes after filling).   |
|----------------|---|
| Applicability: | This specification is applicable to 24P and 52B DSCs only.  |
| Objective:     | To ensure that: (1) the atmosphere surrounding the irradiated fuel is a non-<br>oxidizing inert gas; (2) the atmosphere is favorable for the transfer of decay heat.      |
| Action:        | If the required pressure cannot be obtained:  |
|                | 1. Confirm that the vacuum drying system and helium source are properly installed.  |
|                | 2. Check and repair or replace the pressure gauge.  |
|                | 3. Check and repair or replace the vacuum drying system.  |
|                | 4. Check and repair or replace the helium source.   |
|                | 5. Check and repair the seal weld between the inner top cover and the DSC shell.  |
|                | If pressure exceeds the criterion, release a sufficient quantity of helium to lower<br>the DSC cavity pressure.   |
| Surveillance:  | No maintenance or tests are required during the normal storage. Surveillance of the pressure gauge is required during the helium backfilling operation.                   |
| Bases:         | The value of 2.5 psig was selected to ensure that the pressure within the DSC is within the design limits during any expected normal and off-normal operating conditions. |

|

## 1.2.3a 61BT, 32PT, 24PHB and 24PTH DSC Helium Backfill Pressure

| Limit/Specifications: | Helium 2.5 psig $\pm$ 1.0 psig backfill pressure (stable for 30 minutes after filling).   |
|-----------------------|---|
| Applicability:        | This specification is applicable to 61BT, 32PT, 24PHB and 24PTH DSC only.   |
| Objective:            | To ensure that: (1) the atmosphere surrounding the irradiated fuel is a non-<br>oxidizing inert gas; (2) the atmosphere is favorable for the transfer of decay heat.      |
| Action:               | If the required pressure cannot be obtained:  |
|                       | 1. Confirm that the vacuum drying system and helium source are properly installed.  |
|                       | 2. Check and repair or replace the pressure gauge.  |
|                       | 3. Check and repair or replace the vacuum drying system.  |
|                       | 4. Check and repair or replace the helium source.   |
|                       | 5. Check and repair the seal weld between the inner top cover and the DSC shell.  |
|                       | If pressure exceeds the criterion, release a sufficient quantity of helium to lower<br>the DSC cavity pressure.   |
| Surveillance:         | No maintenance or tests are required during the normal storage. Surveillance of the pressure gauge is required during the helium backfilling operation.                   |
| Bases:                | The value of 2.5 psig was selected to ensure that the pressure within the DSC is within the design limits during any expected normal and off-normal operating conditions. |

#### 1.2.4 24P and 52B DSC Helium Leak Rate of Inner Seal Weld

Limit/Specification:

|                | $\leq$ 1.0 x 10-^4 atm $\bullet$ cubic centimeters per second (atm $\bullet$ cm³/s) at the highest DSC limiting pressure.   |
|----------------|---|
| Applicability: | This specification is applicable to the inner top cover seal weld of the 24P and 52B DSCs only.   |
| Objective:     | 1. To limit the total radioactive gases normally released by each canister to negligible levels. Should fission gases escape the fuel cladding, they will remain confined by the DSC confinement boundary.  |
|                | 2. To retain helium cover gases within the DSC and prevent oxygen from entering the DSC. The helium improves the heat dissipation characteristics of the DSC and prevents any oxidation of fuel cladding.   |
| Action:        | If the leak rate test of the inner seal weld exceeds $1.0 \times 10^{-4}$ (atm • cm <sup>3</sup> /s):   |
|                | 1. Check and repair the DSC drain and fill port fittings for leaks.   |
|                | 2. Check and repair the inner seal weld.  |
|                | 3. Check and repair the inner top cover for any surface indications resulting in leakage.   |
| Surveillance:  | After the welding operation has been completed, perform a leak test with a helium leak detection device.  |
| Bases:         | If the DSC leaked at the maximum acceptable rate of $1.0 \times 10^{-4}$ atm • cm <sup>3</sup> /s for a period of 20 years, about 63,100 cc of helium would escape from the DSC. This is about 1% of the 6.3 x 10 <sup>6</sup> cm <sup>3</sup> of helium initially introduced in the DSC. This amount of leakage would have a negligible effect on the inert environment of the DSC cavity. (Reference: American National Standards Institute, ANSI N14.5-1987, For Radioactive Materials— Leakage Tests on Packages for Shipment," Appendix B3). |

# 1.2.4a 61BT, 32PT, 24PHB and 24PTH DSC Helium Leak Rate of Inner Seal Weld

| Limit/Specification: |  |
|----------------------|--|
|                      | $\leq$ 1.0 x 10- <sup>7</sup> reference cubic centimeters per second (cc/s).   |
| Applicability:       | This specification is applicable to the inner top cover seal weld of 61BT, 32PT 24PHB and 24PTH DSC only.  |
| Objective:           | <ol> <li>To demonstrate that the top cover to be "leak tight", as defined in "American<br/>National Standard for Leakage Tests on Packages for Shipment of<br/>Radioactive Materials," ANSI N14.5 – 1997.</li> </ol> |
|                      | 2. To retain helium cover gases within the DSC and prevent oxygen from entering the DSC. The helium improves the heat dissipation characteristics of the DSC and prevents any oxidation of fuel cladding.            |
| Action:              | If the leak rate test of the inner seal weld exceeds $1.0 \times 10^{-7}$ reference cc/s:  |
|                      | 1. Check and repair the inner seal weld.   |
|                      | 2. Check and repair the inner top cover for any surface indications resulting in leakage.  |
| Surveillance:        | After the welding operation has been completed, perform a leak test with a helium leak detection device.   |
| Bases:               | The 61BT, 32PT, 24PHB and 24PTH DSC will maintain an inert atmosphere around the fuel and radiological consequences will be negligible, since it is designed and tested to be leak tight.                            |

# 1.2.5 DSC Dye Penetrant Test of Closure Welds

Limit/Specification:

|                | All DSC closure welds except those subjected to full volumetric inspection shall<br>be dye penetrant tested in accordance with the requirements of the ASME Boiler<br>and Pressure Vessel Code Section III, Division 1, Article NB-5000. The liquid<br>penetrant test acceptance standards shall be those described in Subsection NB-<br>5350 of the Code. |
|----------------|--|
| Applicability: | This is applicable to all DSCs. The welds include inner and outer top and bottom covers, and vent and siphon port covers.  |
| Objective:     | To ensure that the DSC is adequately sealed in a redundant manner and leak tight.  |
| Action:        | If the liquid penetrant test indicates that the weld is unacceptable:  |
|                | 1. The weld shall be repaired in accordance with approved ASME procedures.   |
|                | 2. The new weld shall be re-examined in accordance with this specification.  |
| Surveillance:  | During DSC closure operations. No additional surveillance is required for this operation.  |
| Bases:         | Article NB-5000 Examination, ASME Boiler and Pressure Vessel Code, Section III, Division 1, Sub-Section NB.  |

1.2.6 Deleted

# 1.2.7 HSM Dose Rates with a Loaded 24P, 52B or 61BT DSC

|                | Dose rates at the following locations shall be limited to levels which are less than or equal to:   |
|----------------|---|
|                | a. 400 mrem/hr at 3 feet from the HSM surface.  |
|                | b. Outside of HSM door on center line of DSC 100 mrem/hr.   |
|                | c. End shield wall exterior 20 mrem/hr.   |
| Applicability: | This specification is applicable to all HSMs which contain a loaded 24P, 52B or 61BT DSC.   |
| Objective:     | The dose rate is limited to this value to ensure that the cask (DSC) has not been inadvertently loaded with fuel not meeting the specifications in Section 1.2.1 and to maintain dose rates as-low-as-is-reasonably achievable (ALARA) at locations on the HSMs where surveillance is performed, and to reduce off-site exposures during storage. |
| Action:        | a. If specified dose rates are exceeded, the following actions should be taken:   |
|                | 1. Ensure that the DSC is properly positioned on the support rails.   |
|                | 2. Ensure proper installation of the HSM door.  |
|                | 3. Ensure that the required module spacing is maintained.   |
|                | 4. Confirm that the spent fuel assemblies contained in the DSC conform to the specifications of Section 1.2.1.  |
|                | 5. Install temporary or permanent shielding to mitigate the dose to acceptable levels in accordance with 10 CFR Part 20, 10 CFR 72.104(a), and ALARA.   |
|                | b. Submit a letter report to the NRC within 30 days summarizing the action taken and the results of the surveillance, investigation and findings. The report must be submitted using instructions in 10 CFR 72.4 with a copy sent to the administrator of the appropriate NRC regional office.  |
| Surveillance:  | The HSM and ISFSI shall be checked to verify that this specification has been met after the DSC is placed into storage and the HSM door is closed.  |
| Basis:         | The basis for this limit is the shielding analysis presented in Section 7.0,<br>Appendix J, and Appendix K of the FSAR. The specified dose rates provide as-<br>low-as-is-reasonably-achievable on-site and off-site doses in accordance with 10<br>CFR Part 20 and 10 CFR 72.104(a).   |

# 1.2.7a HSM Dose Rates with a Loaded 32PT DSC Only

|                | Dose rates at the following locations shall be limited to levels which are less than or equal to:   |
|----------------|---|
|                | a. 800 mrem/hr on the HSM front surface.  |
|                | b. 200 mrem/hr on the HSM door centerline.  |
|                | c. 8 mrem/hr on the end shield wall exterior.   |
| Applicability: | This specification is applicable to all HSMs which contain a loaded 32PT DSC.   |
| Objective:     | The dose rate is limited to this value to ensure that the cask (DSC) has not been inadvertently loaded with fuel not meeting the specifications in Section 1.2.1 and to maintain dose rates as-low-as-is-reasonably achievable (ALARA) at locations on the HSMs where surveillance is performed, and to reduce off-site exposures during storage. |
| Action:        | a. If specified dose rates are exceeded, the following actions should be taken:   |
|                | 1. Ensure that the DSC is properly positioned on the support rails.   |
|                | 2. Ensure proper installation of the HSM door.  |
|                | 3. Ensure that the required module spacing is maintained.   |
|                | 4. Confirm that the spent fuel assemblies contained in the DSC conform to the specifications of Section 1.2.1.  |
|                | 5. Install temporary or permanent shielding to mitigate the dose to acceptable levels in accordance with 10 CFR Part 20, 10 CFR 72.104(a), and ALARA.   |
|                | b. Submit a letter report to the NRC within 30 days summarizing the action taken and the results of the surveillance, investigation and findings. The report must be submitted using instructions in 10 CFR 72.4 with a copy sent to the administrator of the appropriate NRC regional office.  |
| Surveillance:  | The HSM and ISFSI shall be checked to verify that this specification has been met after the DSC is placed into storage and the HSM door is closed.  |
| Basis:         | The basis for this limit is the shielding analysis presented in Appendix M of the FSAR. The specified dose rates provide as-low-as-is-reasonably-achievable on-<br>site and off-site doses in accordance with 10 CFR Part 20 and 10 CFR 72.104(a).  |

# 1.2.7b HSM Dose Rates with a Loaded 24PHB DSC Only

| Ĩ              |    | Peak dose rates at the following locations shall be limited to levels which are less than or equal to:   |
|----------------|----|--|
|                |    | a. 500 mrem/hr on the HSM front surface.   |
|                |    | b. 20 mrem/hr on the HSM door centerline.  |
|                |    | c. 300 mrem/hr on the end shield wall exterior.  |
| Applicability: |    | This specification is applicable to all HSMs which contain a loaded 24PHB DSC.   |
| Objective:     |    | The peak dose rate is limited to this value to ensure that the cask (DSC) has not<br>been inadvertently loaded with fuel not meeting the specifications in Section 1.2.1<br>and to maintain dose rates as-low-as-is-reasonably achievable (ALARA) at<br>locations on the HSMs where surveillance is performed, and to reduce off-site<br>exposures during storage.   |
| Action:        | a. | If specified dose rates are exceeded, the following actions should be taken:   |
|                |    | <ol> <li>Ensure that the DSC is properly positioned on the support rails.</li> <li>Ensure proper installation of the HSM door.</li> <li>Ensure that the required module spacing is maintained.</li> <li>Confirm that the spent fuel assemblies contained in the DSC conform to the specifications of Section 1.2.1.</li> <li>Install temporary or permanent shielding to mitigate the dose to acceptable levels in accordance with 10 CFR Part 20, 10 CFR 72.104(a), and ALARA.</li> </ol> |
|                | b. | Submit a letter report to the NRC within 30 days summarizing the action taken<br>and the results of the surveillance, investigation and findings. The report must be<br>submitted using instructions in 10 CFR 72.4 with a copy sent to the administrator<br>of the appropriate NRC regional office.   |
| Surveillance:  |    | The HSM and ISFSI shall be checked to verify that this specification has been met after the DSC is placed into storage and the HSM door is closed.   |
| Basis:         |    | The basis for this limit is the shielding analysis presented in Appendix N of the FSAR. The specified dose rates provide as-low-as-is-reasonably- achievable on-<br>site and off-site doses in accordance with 10 CFR Part 20 and 10 CFR 72.104(a).  |

# 1.2.7c HSM-H Dose Rates with a Loaded 24PTH-S or 24PTH-L DSC Only

| I              |    | Peak dose rates at the following locations shall be limited to levels which are less than or equal to:   |
|----------------|----|--|
|                |    | a. 1300 mrem/hr on the HSM-H front surface.  |
|                |    | b. 5 mrem/hr on the HSM-H door centerline.   |
|                |    | c. 10 mrem/hr on the end shield wall exterior.   |
| Applicability: |    | This specification is applicable to all HSM-H modules which contain a loaded 24PTH-S or 24PTH-L DSC.   |
| Objective:     |    | The peak dose rate is limited to this value to ensure that the cask (DSC) has not<br>been inadvertently loaded with fuel not meeting the specifications in Section 1.2.1<br>and to maintain dose rates as-low-as-is-reasonably achievable (ALARA) at<br>locations on the HSM-H where surveillance is performed, and to reduce off-site<br>exposures during storage.  |
| Action:        | a. | If specified dose rates are exceeded, the following actions should be taken:   |
|                |    | <ol> <li>Ensure that the DSC is properly positioned on the support rails.</li> <li>Ensure proper installation of the HSM-H door.</li> <li>Confirm that the spent fuel assemblies contained in the DSC conform to the specifications of Section 1.2.1.</li> <li>Install temporary or permanent shielding to mitigate the dose to acceptable levels in accordance with 10 CFR Part 20, 10 CFR 72.104(a), and ALARA.</li> </ol> |
|                | b. | Submit a letter report to the NRC within 30 days summarizing the action taken<br>and the results of the surveillance, investigation and findings. The report must be<br>submitted using instructions in 10 CFR 72.4 with a copy sent to the administrator<br>of the appropriate NRC regional office.   |
| Surveillance:  |    | The HSM-H and ISFSI shall be checked to verify that this specification has been met after the DSC is placed into storage and the HSM-H door is closed.   |
| Basis:         |    | The basis for this limit is the shielding analysis presented in Appendix P of the FSAR. The specified dose rates provide as-low-as-is-reasonably- achievable on-<br>site and off-site doses in accordance with 10 CFR Part 20 and 10 CFR 72.104(a).  |

# 1.2.7d HSM or HSM-H Dose Rates with a Loaded 24PTH-S-LC DSC Only

|                | Peak dose rates at the following locations shall be limited to levels which are less than or equal to:  |
|----------------|---|
|                | a. 500 mrem/hr on the HSM or HSM-H front surface.   |
|                | b. 70 mrem/hr on the HSM or HSM-H door centerline.  |
|                | c. 300 mrem/hr on the end shield wall exterior.   |
| Applicability: | This specification is applicable to all HSMs or HSM-Hs which contain a loaded 24PTH-S-LC DSC.   |
| Objective:     | The peak dose rate is limited to this value to ensure that the cask (DSC) has not<br>been inadvertently loaded with fuel not meeting the specifications in Section 1.2.1<br>and to maintain dose rates as-low-as-is-reasonably achievable (ALARA) at<br>locations on the HSMs or HSM-Hs where surveillance is performed, and to<br>reduce off-site exposures during storage.  |
| Action: a.     | If specified dose rates are exceeded, the following actions should be taken:  |
|                | <ol> <li>Ensure that the DSC is properly positioned on the support rails.</li> <li>Ensure proper installation of the HSM or HSM-H door.</li> <li>Confirm that the spent fuel assemblies contained in the DSC conform to the specifications of Section 1.2.1.</li> <li>Install temporary or permanent shielding to mitigate the dose to acceptable levels in accordance with 10 CFR Part 20, 10 CFR 72.104(a), and ALARA.</li> </ol> |
| b.             | Submit a letter report to the NRC within 30 days summarizing the action taken<br>and the results of the surveillance, investigation and findings. The report must be<br>submitted using instructions in 10 CFR 72.4 with a copy sent to the administrator<br>of the appropriate NRC regional office.  |
| Surveillance:  | The HSM or HSM-H and ISFSI shall be checked to verify that this specification has been met after the DSC is placed into storage and the HSM or HSM-H door is closed.  |
| Basis:         | The basis for this limit is the shielding analysis presented in Appendix P of the FSAR. The specified dose rates provide as-low-as-is-reasonably- achievable on-<br>site and off-site doses in accordance with 10 CFR Part 20 and 10 CFR 72.104(a).   |

1.2.8 HSM Maximum Air Exit Temperature with a Loaded 24P, 52B, 61BT, 32PT, 24PHB or 24PTH-S-LC Only

| Limit/Specification: |   |
|----------------------|---|
|                      | Following initial DSC transfer to the HSM or the occurrence of accident conditions, the equilibrium air temperature difference between ambient temperature and the vent outlet temperature shall not exceed 100°F for <sup>3</sup> 5 year cooled fuel, when fully loaded with 24 kW heat.   |
| Applicability:       | This specification is applicable to all HSMs stored in the ISFSI. If a DSC is placed in the HSM with a heat load less than 24 kW, the limiting difference between outlet and ambient temperatures shall be determined by a calculation performed by the user using the same methodology and inputs documents in the FSAR and SER.   |
| Objective:           | The objective of this limit is to ensure that the temperatures of the fuel cladding and the HSM concrete do not exceed the temperatures calculated in Section 8 of the FSAR. That section shows that if the air outlet temperature difference is less than or equal to $100^{\circ}$ F (with a thermal heat load of 24 kW), the fuel cladding and concrete will be below the respective temperature limits for normal long-term operation.  |
| Action:              | If the temperature rise is greater than that specified, then the air inlets and exits should be checked for blockage. If the blockage is cleared and the temperature is still greater than that specified, the DSC and HSM cavity may be inspected using video equipment or other suitable means. If environmental factors can be ruled out as the cause of excessive temperatures, then the fuel bundles are producing heat at a rate higher than the upper limit specified in the Specification of Section 1.2.1 and will require additional measurements and analysis to assess the actual performance of the system. If excessive temperatures cause the system to perform in an unacceptable manner and/or the temperatures cannot be controlled to acceptable limits, then the cask shall be unloaded within the time period as determined by the analysis. |
| Surveillance:        | The temperature rise shall be measured and recorded daily following DSC insertion until equilibrium temperature is reached, 24 hours after insertion, and again on a daily basis after insertion into the HSM or following the occurrence of accident conditions. If the temperature rise is within the specifications or the calculated value for a heat load less than 24 kW, then the HSM and DSC are performing as designed to meet this specification and no further maximum air exit temperature measurements are required. Air temperatures must be measured in such a manner as to obtain representative values of inlet and outlet air temperatures.   |
| Basis:               | The specified temperature rise is selected to ensure the fuel clad and concrete temperatures are maintained at or below acceptable long-term storage limits.  |

1.2.8a HSM-H Maximum Air Exit Temperature with a Loaded 24PTH DSC

| Linit specification. | Following initial DSC transfer to the HSM-H or the occurrence of accident conditions, the equilibrium air temperature difference between ambient  |
|----------------------|---|
|                      | temperature and the vent outlet temperature shall not exceed 100°F; when fully loaded with 40.8 kW heat for 24PTH-S or 24PTH-L DSC (or 70°F when fully loaded with 24PTH-S-LC DSC).   |
| Applicability:       | This specification is applicable to all HSM-H modules stored in the ISFSI. If a DSC is placed in the HSM-H with a heat load less than 40.8 kW, the limiting difference between outlet and ambient temperatures shall be determined by a calculation performed by the user using the same methodology and inputs documents in Appendix P of the FSAR.  |
| Objective:           | The objective of this limit is to ensure that the temperatures of the fuel cladding<br>and the HSM-H concrete do not exceed the temperatures calculated in Appendix<br>P of the FSAR. That section shows that if the air outlet temperature difference is<br>less than or equal to 100°F with a thermal heat load of 40.8 kW for 24PTH-S or<br>24PTH-L DSC (or 70°F with a thermal heat load of 24.0 kW for 24PTH-S-LC),<br>the fuel cladding and concrete will be below the respective temperature limits for<br>normal long-term operation.   |
| Action:              | If the temperature rise is greater than that specified, then the air inlets and exits should be checked for blockage. If the blockage is cleared and the temperature is still greater than that specified, the DSC and HSM-H cavity may be inspected using video equipment or other suitable means. If environmental factors can be ruled out as the cause of excessive temperatures, then the fuel bundles are producing heat at a rate higher than the upper limit specified in the specification of Section 1.2.1 and will require additional measurements and analysis to assess the actual performance of the system. If excessive temperatures cause the system to perform in an unacceptable manner and/or the temperatures cannot be controlled to acceptable limits, then the cask shall be unloaded within the time period as determined by the analysis. |
| Surveillance:        | The temperature rise shall be measured and recorded daily following DSC insertion until equilibrium temperature is reached, 24 hours after insertion, and again on a daily basis after insertion into the HSM-H or following the occurrence of accident conditions. If the temperature rise is within the specifications or the calculated value for a heat load less than 40.8 kW for 24PTH-S or 24PTH-L DSC (or 24.0 kW for 24PTH-S-LC DSC) then the HSM-H and DSC are performing as designed to meet this specification and no further maximum air exit temperature measurements are required. Air temperatures must be measured in such a manner as to obtain representative values of inlet and outlet air temperatures.   |
| Basis:               | The specified temperature rise is selected to ensure the fuel clad and concrete temperatures are maintained at or below acceptable long-term storage limits.  |

# 1.2.9 Transfer Cask Alignment with HSM or HSM-H

# Limit/Specification:

|                | The cask must be aligned with respect to the HSM or HSM-H that the longitudinal centerline of the DSC in the transfer cask is within $\pm 1/8$ inch of its true position when the cask is docked with the HSM front access opening. |  |
|----------------|---|--|
| Applicability: | This specification is applicable during the insertion and retrieval of all DSCs.  |  |
| Objective:     | To ensure smooth transfer of the DSC from the transfer cask to HSM or HSM-H and back.   |  |
| Action:        | If the alignment tolerance is exceeded, the following actions should be taken:  |  |
|                | a. Confirm that the transfer system is properly configured.   |  |
|                | b. Check and repair the alignment equipment.  |  |
|                | c. Confirm the locations of the alignment targets on the transfer cask and HSM or HSM-H.  |  |
| Surveillance:  | Before initiating DSC insertion or retrieval, confirm the alignment. Observe the transfer system during DSC insertion or retrieval to ensure that motion or excessive vibration does not occur.                                     |  |
| Basis:         | The basis for the true position alignment tolerance is the clearance between the DSC shell, the transfer cask cavity, the HSM or HSM-H access opening, and the DSC support rails inside the HSM or HSM-H.                           |  |

# 1.2.10 DSC Handling Height Outside the Spent Fuel Pool Building

| Limit/Specification: | 1.  | The loaded TC/DSC shall not be handled at a height greater than 80 inches outside the spent fuel pool building.   |
|----------------------|---|---|
|                      | 2.  | In the event of a drop of a loaded TC/DSC from a height greater than 15 inches: (a) fuel in the DSC shall be returned to the reactor spent fuel pool; (b) the DSC shall be removed from service and evaluated for further use; and (c) the TC shall be inspected for damage and evaluated for further use.  |
| Applicability:       |   | e specification applies to handling the TC, loaded with the DSC, on route to,<br>at, the storage pad.   |
| Objective:           | 1.  | To preclude a loaded TC/DSC drop from a height greater than 80 inches.  |
|                      | 2.  | To maintain spent fuel integrity, according to the spent fuel specification for storage, continued confinement integrity, and DSC functional capability, after a tip-over or drop of a loaded DSC from a height greater than 15 inches.   |
| Surveillance:        | read  | he event of a loaded TC/DSC drop accident, the system will be returned to the ctor fuel handling building, where, after the fuel has been returned to the spent l pool, the DSC and TC will be inspected and for future use.  |
| Basis:               | incl<br>con<br>crit:<br>be e<br>the<br>incl<br>droj<br>requ | e NRC evaluation of the TC/DSC drop analysis concurred that drops up to 80<br>hes, of the DSC inside the TC, can be sustained without breaching the<br>finement boundary, preventing removal of spent fuel assemblies, or causing a<br>icality accident. This specification ensures that handling height limits will not<br>exceeded in transit to, or at the storage pad. Acceptable damage may occur to<br>TC, DSC, and the fuel stored in the DSC, for drops of height greater than 15<br>hes. The specification requiring inspection of the DSC and fuel following a<br>p of 15 inches or greater ensures that the spent fuel will continue to meet the<br>uirements for storage, the DSC will continue to provide confinement, and the<br>will continue to provide its design functions of DSC transfer and shielding. |

# 1.2.11 Transfer Cask Dose Rates with a Loaded 24P, 52B, 61BT, or 32PT DSC

|                | Dose rates 7 from the transfer cask shall be limited to levels which are less than or equal to:  |
|----------------|--|
|                | a. 200 mrem/hr at 3 feet with water in the DSC cavity.   |
|                | b. 500 mrem/hr at 3 feet without water in the DSC cavity.  |
| Applicability: | This specification is applicable to the transfer cask containing a loaded 24P, 52B, 61BT, or 32PT DSC.   |
| Objective:     | The dose rate is limited to this value to ensure that the DSC has not been inadvertently loaded with fuel not meeting the specifications in Section 1.2.1 and to maintain dose rates as-low-as-is-reasonably achievable during DSC transfer operations.  |
| Action:        | If specified dose rates are exceeded, place temporary shielding around affected areas of transfer cask and review the plant records of the fuel assemblies which have been placed in DSC to ensure they conform to the fuel specifications of Section 1.2.1. Submit a letter report to the NRC within 30 days summarizing the action taken and the results of the surveillance, investigation and findings. The report must be submitted using instructions in 10 CFR 72.4 with a copy sent to the administrator of the appropriate NRC regional office. |
| Surveillance:  | The dose rates should be measured as soon as possible after the transfer cask is removed from the spent fuel pool.   |
| Basis:         | The basis for this limit is the shielding analysis presented in Section 7.0, Appendix J, Appendix K and Appendix M of the FSAR.  |

#### 1.2.11a Transfer Cask Dose Rates with a Loaded 24PHB DSC

|                | Dose rates from the transfer cask shall be limited to levels which are less than or equal to:  |
|----------------|--|
|                | a. 1700 mrem/hr at 3 feet from the top of the Cask at the cover plate edge with water in the DSC cavity.   |
|                | b. 500 mrem/hr at 3 feet radially from the Cask surface without water in the DSC cavity.   |
| Applicability: | This specification is applicable to the transfer cask containing a loaded 24PHB DSC.   |
| Objective:     | The dose rate is limited to this value to ensure that the DSC has not been<br>inadvertently loaded with fuel not meeting the specifications in Section 1.2.1 and<br>to maintain dose rates as-low-as-is-reasonably achievable during DSC transfer<br>operations.   |
| Action:        | If specified dose rates are exceeded, place temporary shielding around affected areas of transfer cask and review the plant records of the fuel assemblies which have been placed in DSC to ensure they conform to the fuel specifications of Section 1.2.1. Submit a letter report to the NRC within 30 days summarizing the action taken and the results of the surveillance, investigation and findings. The report must be submitted using instructions in 10 CFR 72.4 with a copy sent to the administrator of the appropriate NRC regional office. |
| Surveillance:  | The dose rates should be measured as soon as possible after the transfer cask is removed from the spent fuel pool.   |
| Basis:         | The basis for this limit is the shielding analysis presented in Appendix N of the FSAR.  |

1.2.11b Transfer Cask Dose Rates with a Loaded 24PTH-S or 24PTH-L DSC

|                | <ul> <li>Dose rates from the transfer cask shall be limited to levels which are less than or equal to:</li> <li>a. 500 mrem/hr at 3 feet from the top of the Cask at the cover plate edge with water in the DSC cavity.</li> <li>b. 600 mrem/hr at 3 feet radially from the Cask surface without water in the DSC cavity.</li> </ul>   |
|----------------|--|
| Applicability: | This specification is applicable to the transfer cask containing a loaded 24PTH-S or 24PTH-L DSC.  |
| Objective:     | The dose rate is limited to this value to ensure that the DSC has not been inadvertently loaded with fuel not meeting the specifications in Section 1.2.1 and to maintain dose rates as-low-as-is-reasonably achievable during DSC transfer operations.  |
| Action:        | If specified dose rates are exceeded, place temporary shielding around affected areas of transfer cask and review the plant records of the fuel assemblies which have been placed in DSC to ensure they conform to the fuel specifications of Section 1.2.1. Submit a letter report to the NRC within 30 days summarizing the action taken and the results of the surveillance, investigation and findings. The report must be submitted using instructions in 10 CFR 72.4 with a copy sent to the administrator of the appropriate NRC regional office. |
| Surveillance:  | The dose rates should be measured as soon as possible after the transfer cask is removed from the spent fuel pool.   |
| Basis:         | The basis for this limit is the shielding analysis presented in Appendix P of the FSAR.  |

#### 1.2.11c Transfer Cask Dose Rates with a Loaded 24PTH-S-LC DSC

| Emili Specification. |  |
|----------------------|--|
|                      | Dose rates from the transfer cask shall be limited to levels which are less than or equal to:  |
|                      | a. 20 mrem/hr at 3 feet from the top of the Cask at the cover plate edge with water in the DSC cavity.   |
|                      | b. 250 mrem/hr at 3 feet radially from the Cask surface without water in the DSC cavity.   |
| Applicability:       | This specification is applicable to the transfer cask containing a loaded 24PTH-S-LC DSC.  |
| Objective:           | The dose rate is limited to this value to ensure that the DSC has not been inadvertently loaded with fuel not meeting the specifications in Section 1.2.1 and to maintain dose rates as-low-as-is-reasonably achievable during DSC transfer operations.  |
| Action:              | If specified dose rates are exceeded, place temporary shielding around affected areas of transfer cask and review the plant records of the fuel assemblies which have been placed in DSC to ensure they conform to the fuel specifications of Section 1.2.1. Submit a letter report to the NRC within 30 days summarizing the action taken and the results of the surveillance, investigation and findings. The report must be submitted using instructions in 10 CFR 72.4 with a copy sent to the administrator of the appropriate NRC regional office. |
| Surveillance:        | The dose rates should be measured as soon as possible after the transfer cask is removed from the spent fuel pool.   |
| Basis:               | The basis for this limit is the shielding analysis presented in Appendix P of the FSAR.  |

#### 1.2.12 Maximum DSC Removable Surface Contamination

Limit/Specification:

|                | 2,200 dpm/100 cm <sup>2</sup> for beta-gamma sources 220 dpm/100 cm <sup>2</sup> for alpha sources.  |
|----------------|--|
| Applicability: | This specification is applicable to all DSCs.  |
| Objective:     | To ensure that release of non-fixed contamination above accepted limits does not occur.  |
| Action:        | If the required limits are not met:  |
|                | a. Flush the DSC/transfer cask annulus with demineralized water and repeat surface contamination surveys of the DSC upper surface.   |
|                | b. If contamination of the DSC cannot be reduced to an acceptable level by this means, direct surface cleaning techniques shall be used following removal of the fuel assemblies from the DSC and removal of the DSC from the transfer cask.   |
|                | c. Check and replace the DSC/transfer cask annulus seal to ensure proper installation and repeat canister loading process.   |
| Surveillance:  | Following placement of each loaded DSC/transfer cask into the cask decontamination area, fuel pool water above the top shield plug shall be removed and the top region of the DSC and cask shall be decontaminated. A contamination survey of the upper 1 foot of the DSC shall be taken.  |
| Basis:         | This non-fixed contamination level is consistent with the requirements of 10 CFR 71.87(i)(1) and 49 CFR 173.443, which regulate the use of spent fuel shipping containers. Consequently, these contamination levels are considered acceptable for exposure to the general environment. This level will also ensure that contamination levels of the inner surfaces of the HSM and potential releases of radioactive material to the environment are minimized. |

#### 1.2.13 TC/DSC Lifting Heights as a Function of Low Temperature and Location

Limit/Specification: 1. No lifts or handling of the TC/DSC at any height are permissible at DSC basket temperatures below -20°F inside the spent fuel pool building.

- 2. The maximum lift height of the TC/DSC shall be 80 inches if the basket temperature is below 0°F but higher than -20°F inside the spent fuel pool building.
- 3. No lift height restriction is imposed on the TC/DSC if the basket temperature is higher than 0°F inside the spent fuel pool building.
- 4. The maximum lift height and handling height for all transfer operations outside the spent fuel pool building shall be 80 inches and the basket temperature may not be lower than 0°F.
- Applicability:These temperature and height limits apply to lifting and transfer of all loaded<br/>TC/DSCs inside and outside the spent fuel pool building.

The requirements of 10 CFR Part 72 apply outside the spent fuel building. The requirements of 10 CFR Part 50 apply inside the spent fuel pool building.

- Objective: The low temperature and height limits are imposed to ensure that brittle fracture of the ferritic steels, used in the TC trunnions and shell and in the DSC basket, does not occur during transfer operations.
- Action: Confirm the basket temperature before transfer of the TC. If calculation or measurement of this value is available, then the ambient temperature may conservatively be used.
- Surveillance: The ambient temperature shall be measured before transfer of the TC/DSC.
- Bases: The basis for the low temperature and height limits is ANSI N14.6-1986 paragraph 4.2.6 which requires at least 40°F higher service temperature than nil ductility transition (NDT) temperature for the TC. In the case of the standardized TC, the test temperature is -40°F; therefore, although the NDT temperature is not determined, the material will have the required 40°F margin if the ambient temperature is 0°F or higher. This assumes the material service temperature is equal to the ambient temperature.

The basis for the low temperature limit for the DSC is NUREG/CR-1815. The basis for the handling height limits is the NRC evaluation of the structural integrity of the DSC to drop heights of 80 inches and less.

| Limit/Specification: | 1. The ambient temperature for transfer operations of a loaded TC/DSC shall not be greater that 100°F (when cask is exposed to direct insolation).   |
|----------------------|--|
|                      | 2. For transfer operations when ambient temperatures exceed 100°F, a solar shield shall be used to provide protection against direct solar radiation.  |
| Applicability:       | This ambient temperature limit applies to all transfer operations of loaded TC/DSCs outside the spent fuel pool building.  |
| Objective:           | The high temperature limit (100°F) is imposed to ensure that:  |
|                      | 1. The fuel cladding temperature limit is not exceeded,  |
|                      | 2. The solid neutron shield material temperature limit is not exceeded, and  |
|                      | 3. The corresponding TC cavity pressure limit is not exceeded.   |
| Action:              | Confirm what the ambient temperature is and provide appropriate solar shade if ambient temperature is expected to exceed 100°F.  |
| Surveillance:        | The ambient temperature shall be measured before transfer of the TC/DSC.   |
| Bases:               | For the NUHOMS <sup>®</sup> -24P, 52B and 61BT systems, the basis for the high temperature limit is PNL-6189 (Reference 1) for the fuel clad limit, the manufacturer's specification for neutron shield, and the design basis pressure of the TC internal cavity pressure. For the NUHOMS <sup>®</sup> -32PT, 24PHB and 24PTH systems, the fuel cladding limits are based on ISG-11, Revision 2 (Reference 3). |

#### 1.2.14 TC/DSC Transfer Operations at High Ambient Temperatures

# 1.2.15 Boron Concentration in the DSC Cavity Water for the 24-P Design Only

#### Limit/Specification:

|                | The DSC cavity shall be filled only with water having a boron concentration equal to, or greater than:   |
|----------------|--|
|                | 1) 2,000 ppm for fuel with an equivalent unirradiated enrichment of less than or equal to 1.45 wt. % U-235 per Figure 1-1.   |
|                | <ol> <li>2,350 ppm for fuel with an equivalent unirradiated enrichment of greater than<br/>1.45 wt. % U-235 per Figure 1-1.</li> </ol>   |
| Applicability: | This limit applies only to the standardized NUHOMS <sup>®</sup> -24P design. No boration in the cavity water is required for the standardized NUHOMS <sup>®</sup> -52B or NUHOMS <sup>®</sup> -61BT system since that system uses fixed absorber plates.   |
| Objective:     | 1) To ensure a subcritical configuration is maintained in the case of accidental loading of the DSC with unirradiated fuel.  |
|                | 2) To ensure a subcritical configuration is maintained in the case of loading of the DSC with fuel with an equivalent unirradiated enrichment of greater than 1.45 wt. % U-235.  |
| Action:        | If the boron concentration is below the required weight percentage concentration (gm boron/ $10^6$ gm water), add boron and re-sample, and test the concentration until the boron concentration is shown to be greater than that required.   |
| Surveillance:  | Written procedures shall be used to independently determine (two samples analyzed by different individuals) the boron concentration in the water used to fill the DSC cavity.  |
|                | 1. Within 24 hours before insertion of the first fuel assembly into the DSC, the dissolved boron concentration in water in the spent fuel pool, and in the water that will be introduced in the DSC cavity, shall be independently determined (two samples chemically analyzed by two individuals).      |
|                | 2. Within 24 hours before flooding the DSC cavity for unloading the fuel assemblies, the dissolved boron concentration in water in the spent pool, and in the water that will be introduced into the DSC cavity, shall be independently determined (two samples analyzed chemically by two individuals). |

3. The dissolved boron concentration in the water shall be reconfirmed at intervals not to exceed 48 hours until such time as the DSC is removed from the spent fuel pool or the fuel has been removed from the DSC.

Bases:

- 1) The required boron concentration is based on the criticality analysis for an accidental misloading of the DSC with unburned fuel, maximum enrichment, and optimum moderation conditions.
- 2) The required boron concentration is based on the criticality analysis for loading of the DSC with unirradiated fuel, maximum enrichment, and optimum moderation conditions.

# 1.2.15a Boron Concentration in the DSC Cavity Water for the 32PT Design Only

Limit/Specification:

|                | The DSC cavity shall be filled only with water having a boron concentration equal to, or greater than 2500 ppm.  |  |
|----------------|--|--|
| Applicability: | This limit applies only to the standardized NUHOMS®- 32PT design.  |  |
| Objective:     | To ensure a subcritical configuration is maintained in the case of loading of the DSC with design basis fuel.  |  |
| Action:        | If the boron concentration is below the required weight percentage concentration (gm boron/ $10^6$ gm water), add boron and re-sample, and test the concentration until the boron concentration is shown to be greater than that required.   |  |
| Surveillance:  | Written procedures shall be used to independently determine (two samples analyzed by different individuals) the boron concentration in the water used to fill the DSC cavity.  |  |
|                | 1. Within 24 hours before insertion of the first fuel assembly into the DSC, the dissolved boron concentration in water in the spent fuel pool, and in the water that will be introduced in the DSC cavity, shall be independently determined (two samples chemically analyzed by two individuals).      |  |
|                | 2. Within 24 hours before flooding the DSC cavity for unloading the fuel assemblies, the dissolved boron concentration in water in the spent pool, and in the water that will be introduced into the DSC cavity, shall be independently determined (two samples analyzed chemically by two individuals). |  |
|                | 3. The dissolved boron concentration in the water shall be reconfirmed at intervals not to exceed 48 hours until such time as the DSC is removed from the spent fuel pool or the fuel has been removed from the DSC.   |  |
| Bases:         | The required boron concentration is based on the criticality analysis presented in Appendix M of this FSAR for loading of the DSC with unirradiated fuel, maximum enrichment, and optimum moderation conditions.   |  |

# 1.2.15b Boron Concentration in the DSC Cavity Water for the 24PHB Design Only

Limit/Specification:

|                | • The DSC cavity shall be filled only with water having a boron concentration equal to, or greater than 2,350 ppm for enrichment of less than or equal to 4.0 wt. % U-235 based on the spent fuel assembly with the maximum initial enrichment in the DSC.   |
|----------------|--|
|                | • The DSC cavity shall be filled only with water having a minimum boron concentration per Figure 1-10 for initial enrichment of greater than or equal to 4.0 wt. % U-235 based on the spent fuel assembly with the maximum initial enrichment in the DSC.  |
| Applicability: | This limit applies only to the standardized NUHOMS <sup>®</sup> -24PHB design.   |
| Objective:     | To ensure a subcritical configuration is maintained in the case of accidental loading of the DSC with unirradiated fuel.   |
| Action:        | If the boron concentration is below the required weight percentage concentration (gm boron/ $10^6$ gm water), add boron and re-sample, and test the concentration until the boron concentration is shown to be greater than that required.   |
| Surveillance:  | Written procedures shall be used to independently determine (two samples analyzed by different individuals) the boron concentration in the water used to fill the DSC cavity.  |
|                | <ol> <li>Within 24 hours before insertion of the first fuel assembly into the DSC, the<br/>dissolved boron concentration in water in the spent fuel pool, and in the water<br/>that will be introduced in the DSC cavity, shall be independently determined<br/>(two samples chemically analyzed by two individuals).</li> </ol> |
|                | 2. Within 24 hours before flooding the DSC cavity for unloading the fuel assemblies, the dissolved boron concentration in water in the spent pool, and in the water that will be introduced into the DSC cavity, shall be independently determined (two samples analyzed chemically by two individuals).                         |
|                | 3) The dissolved boron concentration in the water shall be reconfirmed at intervals not to exceed 48 hours until such time as the DSC is removed from the spent fuel pool or the fuel has been removed from the DSC.   |
| Bases:         | The required boron concentration is based on the criticality analysis for loading of the DSC with unirradiated fuel, initial enrichment, and optimum moderation conditions.  |

1.2.15c Boron Concentration in the DSC Cavity Water for the 24PTH Design Only

| Limit/Specificat | •  | The DSC cavity shall only be filled with water having a minimum boron<br>concentration which meets the requirements of Table 1-1p, when loading intact<br>fuel. Table 1-1p lists the minimum soluble boron concentration as a function of<br>the fuel assembly class, DSC basket type and the corresponding assembly average<br>initial enrichment values.<br>The DSC cavity shall only be filled with water having a minimum boron<br>concentration which meets the requirements of Table 1-1q, when loading<br>damaged fuel. Table 1-1q lists the minimum soluble boron concentration as a<br>function of the fuel assembly class, DSC basket type, the maximum number of<br>damaged fuel assemblies allowed and the corresponding maximum assembly<br>average initial enrichment values. |
|------------------|----|---|
| Applicability:   |    | This limit applies only to the NUHOMS <sup>®</sup> -24PTH design.   |
| Objective:       |    | To ensure a subcritical configuration is maintained in the case of accidental loading of the DSC with unirradiated fuel.  |
| Action:          |    | If the boron concentration is below the required weight percentage concentration (gm boron/ $10^6$ gm water), add boron and re-sample, and test the concentration until the boron concentration is shown to be greater than that required.  |
| Surveillance:    |    | Written procedures shall be used to independently determine (two samples analyzed by different individuals) the boron concentration in the water used to fill the DSC cavity.   |
|                  | 1. | Within 24 hours before insertion of the first fuel assembly into the DSC, the dissolved boron concentration in water in the spent fuel pool, and in the water that will be introduced in the DSC cavity, shall be independently determined (two samples chemically analyzed by two individuals).  |
|                  | 2. | Within 24 hours before flooding the DSC cavity for unloading the fuel assemblies, the dissolved boron concentration in water in the spent pool, and in the water that will be introduced into the DSC cavity, shall be independently determined (two samples analyzed chemically by two individuals).   |
|                  | 3. | The dissolved boron concentration in the water shall be reconfirmed at intervals<br>not to exceed 48 hours until such time as the DSC is removed from the spent fuel<br>pool or the fuel has been removed from the DSC.   |
| Bases:           |    | The required boron concentration is based on the criticality analysis in FSAR<br>Appendix P for loading of the DSC with unirradiated fuel, initial enrichment, and<br>optimum moderation conditions.  |

1.2.16 Provision of TC Seismic Restraint Inside the Spent Fuel Pool Building as a Function of Horizontal Acceleration and Loaded Cask Weight

## Limit/Specification:

|                | Seismic restraints shall be provided to prevent overturning of a loaded TC during a seismic event if a certificate holder determines that the horizontal acceleration is 0.40 g or greater. The determination of horizontal acceleration acting at the center of gravity (CG) of the loaded TC must be based on a peak horizontal ground acceleration at the site, but shall not exceed 0.25 g. |
|----------------|---|
| Applicability: | This condition applies to all TCs which are subject to horizontal accelerations of 0.40 g or greater.   |
| Objective:     | To prevent overturning of a loaded TC inside the spent fuel pool building.  |
| Action:        | Determine what the horizontal acceleration is for the TC.   |
| Surveillance:  | Determine need for TC restraint before any operations inside the spent fuel pool building.  |
| Bases:         | Calculation of overturning and restoring moments.   |

# 1.2.17 61BT DSC Vacuum Drying Duration Limit

|                | Time limit for duration of Vacuum Drying is 96 hours after completion of 61BT DSC draining.  |  |  |
|----------------|--|--|--|
| Applicability: | This specification is only applicable to a 61BT DSC with greater than 17.6 kW heat load.   |  |  |
| Objective:     | To ensure that 61BT DSC basket structure does not exceed 800°F.  |  |  |
| Action:        | 1. If the DSC vacuum drying pressure limit of Technical Specification 1.2.2 cannot be achieved at 72 hours after completion of DSC draining, the DSC must be backfilled with 0.1 atm or greater helium pressure within 24 hours. |  |  |
|                | 2. Determine the cause of failure to achieve the vacuum drying pressure limit as defined in Technical Specification 1.2.2.   |  |  |
|                | 3. Initiate vacuum drying after actions in Step 2 are completed or unload the DSC within 30 days.  |  |  |
| Surveillance:  | No maintenance or tests are required during the normal storage. Monitoring of the time duration during the vacuum drying operation is required .   |  |  |
| Bases:         | The time limit of 96 hours was selected to ensure that the temperature within the DSC is within the design limits during vacuum drying.  |  |  |

# 1.2.17a 32PT DSC Vacuum Drying Duration Limit

|                | <ol> <li>The limit for duration of Vacuum Drying is 31 hrs for a 32PT DSC with a heat load greater than 8.4 kW and up to 24 kW after initiation of vacuum drying.</li> <li>The limit for duration of Vacuum Drying is 36 hrs for a 32PT DSC with a</li> </ol>   |  |
|----------------|---|--|
|                | heat load of up to 8.4 kW after initiation of vacuum drying.  |  |
| Applicability: | This specification is applicable to a 32PT DSC with heat load as described above.   |  |
| Objective:     | To ensure the fuel cladding temperature in the 32PT DSC does not exceed 752°F during drying and also to meet the thermal cycling limit of 117°F during drying, helium backfilling and transfer operations.  |  |
| Action:        | <ol> <li>If the DSC vacuum drying pressure limit of Technical Specification 1.2.2<br/>cannot be achieved at the specified time limits after initiation of vacuum<br/>drying, the DSC must be backfilled with 0.1 atm or greater helium pressure<br/>within 2 hours.</li> </ol>  |  |
|                | 2. Determine the cause of failure to achieve the vacuum drying pressure limit as defined in Technical Specification 1.2.2.  |  |
|                | 3. Initiate vacuum drying after actions in Step 2 are completed or unload the DSC within 30 days.   |  |
| Surveillance:  | No maintenance or tests are required during the normal storage. Monitoring of the time duration during the vacuum drying operation is required.   |  |
| Bases:         | The time limits for the 32PT DSC were selected to ensure that the maximum cladding temperature is within the acceptable limit of 752°F during vacuum drying. These time limits also ensure that the cladding temperature meets the thermal cycling criteria of 117°F during drying, helium backfilling and transfer operations. |  |

# 1.2.17b 24PHB DSC Vacuum Drying Duration Limit

|                | <ol> <li>The limit for duration of Vacuum Drying is 29 hrs for a 24PHB DSC with a heat load greater than 12.0 kW and up to 24 kW after initiation of vacuum drying.</li> <li>The limit for duration of Vacuum Drying is 32 hrs for a 24PHB DSC with a heat load of up to 12.0 kW after initiation of vacuum during.</li> </ol>   |  |  |
|----------------|--|--|--|
| Applicability: | This specification is applicable to a 24PHB DSC with heat load as described above.   |  |  |
| Objective:     | To ensure the fuel cladding temperature in the 24PHB DSC does not exceed 752°F during drying and also to meet the thermal cycling limit of 117°F during drying, helium backfilling and transfer operations.  |  |  |
| Action:        | 1. If the DSC vacuum drying pressure limit of Technical Specification 1.2.2 cannot be achieved at the specified time limits after initiation of vacuum drying, the DSC must be backfilled with 0.1 atm or greater helium pressure within 2 hours.  |  |  |
|                | 2. Determine the cause of failure to achieve the vacuum drying pressure limit as defined in Technical Specification 1.2.2.   |  |  |
|                | 3. Initiate vacuum drying after actions in Step 2 are completed or unload the DSC within 30 days.  |  |  |
| Surveillance:  | No maintenance or tests are required during the normal storage. Monitoring of the time duration during the vacuum drying operation is required.  |  |  |
| Bases:         | The time limit for the 24PHB DSC were selected to ensure that the maximum cladding temperature is within the acceptable limits of 752°F during vacuum drying. These time limits also ensure that the cladding temperature meets the thermal cycling criteria of 117°F during drying, helium backfilling and transfer operations. |  |  |

# 1.2.17c 24PTH DSC Vacuum Drying Duration Limit

|                | 1. If air is used for blowdown, the time duration of vacuum drying for a 24PTH DSC after initiation of vacuum drying shall be less than or equal to:   |
|----------------|--|
|                | <ul> <li>17 hours for Heat Load Configuration No.1, 2 and 3</li> <li>23 hours for Heat Load Configuration No. 4</li> <li>26 hours for Heat Load Configuration No. 5</li> </ul>   |
|                | 2. No time limits apply for vacuum drying of 24PTH DSC if helium is used for blowdown.   |
| Applicability: | This specification is applicable to a 24PTH DSC with heat load configuration following blowdown using air or nitrogen as described above.  |
| Objective:     | To ensure the fuel cladding temperature in the 24PTH DSC does not exceed 752°F during drying and also to meet the thermal cycling limit of 117°F during drying, helium backfilling and transfer operations.  |
| Action:        | 1. If the DSC vacuum drying pressure limit of Technical Specification 1.2.2 cannot be achieved at the specified time limits after initiation of vacuum drying, the DSC must be backfilled with 0.1 atm or greater helium pressure within 2 hours.  |
|                | 2. Determine the cause of failure to achieve the vacuum drying pressure limit as defined in Technical Specification 1.2.2.   |
|                | 3. Initiate vacuum drying after actions in Step 2 are completed or unload the DSC within 30 days.  |
| Surveillance:  | No maintenance or tests are required during the normal storage. Monitoring of the time duration during the vacuum drying operation is required.  |
| Bases:         | The time limit for the 24PTH DSC were selected to ensure that the maximum cladding temperature is within the acceptable limits of 752°F during vacuum drying. These time limits also ensure that the cladding temperature meets the thermal cycling criteria of 117°F during drying, helium backfilling and transfer operations. |

# 1.2.18 Time Limit for Completion of 24PTH DSC Transfer Operation

|                |    | The time limit for completion of transfer of a loaded and welded 24PTH DSC with a heat load greater than 24.0 kW from the cask handling area to the HSM-H is dependent on the heat load as follows:  |
|----------------|----|--|
|                |    | • 9.5 hours for a DSC with a heat load greater than 31.2 kW but less than or equal to 40.8 kW with basket types 1A, 1B or 1C.  |
|                |    | • 25 hours for a DSC with a heat load greater than 24.0 kW but less than or equal to 31.2 kW with a basket type 2A, 2B or 2C (without aluminum inserts).   |
|                |    | • No time limits apply for a 24PTH DSC with a heat load greater than 24.0 kW but less than or equal to 31.2 kW, with a basket type 1A, 1B, or 1C (with aluminum inserts).  |
| Applicability: |    | This specification is only applicable to a 24PTH-S or 24PTH-L DSC when transferred in OS197FC cask with heat loads greater than 24.0 kW. The time limit is defined as the time elapsed after the initiation of draining of Cask/DSC annulus water and bolting of the transfer cask top cover plate until it is unbolted for insertion of the DSC into the HSM-H. |
| Objective:     |    | To ensure that the fuel cladding temperatures in the 24PTH DSC do not exceed 752°F during transfer operations.   |
| Actions:       |    | Initiate one of the following corrective actions within two hours if specified time limits are exceeded.   |
|                | 1. | Complete the transfer of the DSC from the transfer cask to the HSM-H, or   |
|                | 2. | If the transfer cask is in the cask handling area in a vertical orientation, unbolt the cask top cover plate and fill the cask/DSC annulus with clean water, or  |
|                | 3. | If the cask is in a horizontal orientation on the transfer skid, then initiate air circulation in the Cask/DSC annulus by starting one of the blowers provided on the cask transfer skid, or   |
|                | 4. | Initiate appropriate external cooling of the cask outer surface by other means to limit the temperature increase or return the cask to the cask handling area, unbolt the cask top cover plate and fill the cask/DSC annulus with clean water.   |
| Surveillance:  |    | Monitoring of the time duration following the completion of the DSC sealing  |
|                |    | until the completion of unbolting of the transfer cask top plate is required.  |
| Bases:         |    | The required time limit is based on the transient thermal analysis presented in Appendix P of the FSAR for the transfer of the 24PTH DSC.  |

#### 1.3 Surveillance and Monitoring

One of the two alternate surveillance activities listed below (1.3.1 or 1.3.2) shall be performed for monitoring the HSM or HSM-H thermal performance.

| 1.3.1 Visual Insp   | 3.1 Visual Inspection of HSM or HSM-H Air Inlets and Outlets (Front Wall and Roof Birdscreen)   |  |  |
|---------------------|---|--|--|
| Limit/Surveillance: | A visual surveillance of the exterior of the air inlets and outlets shall be conducted daily. In addition, a close-up inspection shall be performed to ensure that no materials accumulate between the modules to block the air flow.   |  |  |
| Objective:          | To ensure that HSM or HSM-H air inlets and outlets are not blocked for more<br>than 40 hours to prevent exceeding the allowable HSM or HSM-H concrete and<br>or the fuel cladding temperatures.   |  |  |
| Applicability:      | This specification is applicable to all HSMs or HSM-Hs loaded with a DSC loaded with spent fuel.  |  |  |
| Action:             | If the surveillance shows blockage of air vents (inlets or outlets), they shall be cleared. If the screen is damaged, it shall be replaced.   |  |  |
| Basis:              | The concrete temperature could exceed 350°F in the accident circumstances of complete blockage of all vents if the period exceeds approximately 40 hours for HSM. Concrete temperatures over 350°F in accidents (without the presence of water or steam) can have uncertain impact on concrete strength and durability. A conservative analysis (adiabatic heat case) of complete blockage of all air inlets or outlets indicates that the concrete can reach the accident temperature limit of 350°F in the time periods specified for HSM. For HSM-H, the time period specified ensures that blockage will not exist for periods longer than that assumed in the Safety analysis presented in Appendix P of the FSAR. At the 40 hour time limit, the fuel cladding temperature remains well below the accident limit of 1058°F. |  |  |

## 1.3.2 HSM or HSM-H Thermal Performance

| Surveillance: | Verify a temperature measurement of the thermal performance, for each HSM or HSM-H, on a daily basis. The temperature measurement could be any parameter such as (1) a direct measurement of the HSM or HSM-H temperatures, (2) a direct measurement of the DSC temperatures, (3) a comparison of the inlet and outlet temperature difference to predicted temperature differences for each individual HSM or HSM-H, or (4) other means that would identify and allow for the correction of off-normal thermal conditions that could lead to exceeding the concrete and fuel clad temperature criteria. If air temperatures are measured, they must be measured in such a manner as to obtain representative values of inlet and outlet air temperatures. Also due to the proximity of adjacent HSM or HSM-H modules, care must be exercised to ensure that measured air temperatures reflect only the thermal performance of an individual module, and not the combined performance of adjacent modules. |
|---------------|---|
| Action:       | If the temperature measurement shows a significant unexplained difference, so as to indicate the approach of materials to the concrete or fuel clad temperature criteria, take appropriate action to determine the cause and return the canister to normal operation. If the measurement or other evidence suggests that the concrete accident temperature criteria (350°F) has been exceeded for more than 24 hours, the HSM or HSM-H must be removed from service unless the licensee can provide test results in accordance with ACI-349, appendix A.4.3, demonstrating that the structural strength of the HSM or HSM-H has an adequate margin of safety.   |
| Basis:        | The temperature measurement should be of sufficient scope to provide the licensee with a positive means to identify conditions which threaten to approach temperature criteria for proper HSM or HSM-H operation and allow for the correction of off-normal thermal conditions that could lend to exceeding the concrete and fuel clad temperature criteria.  |

| Sur | veillance or Monitoring   | Period | <b>Reference Section</b>                          |
|-----|---|--------|---|
| 1.  | Fuel Specification  | PL     | 1.2.1   |
| 2.  | DSC Vacuum Pressure During Drying   | L      | 1.2.2   |
| 3.  | DSC Helium Backfill Pressure  | L      | 1.2.3 or 1.2.3a                                   |
| 4.  | DSC Helium Leak Rate of Inner Seal Weld   | L      | 1.2.4 or 1.2.4a                                   |
| 5.  | DSC Dye Penetrant Test of Closure Welds   | L      | 1.2.5   |
| 6.  | DELETED   | -      | -   |
| 7.  | HSM or HSM-H Dose Rates   | L      | 1.2.7 or 1.2.7a, or<br>1.2.7b or 1.2.7c or 1.2.7d |
| 8.  | HSM or HSM-H Maximum Air Exit Temperature   | 24 hrs | 1.2.8 or 1.2.8a                                   |
| 9.  | TC Alignment with HSM or HSM-H  | S      | 1.2.9   |
| 10. | DSC Handling Height Outside Spent Fuel Pool<br>Building   | AN     | 1.2.10  |
| 11. | Transfer Cask Dose Rates  | L      | 1.2.11 or 1.2.11a or<br>1.2.11b or 1.2.11c        |
| 12. | Maximum DSC Removable Surface Contamination   | L      | 1.2.12  |
| 13. | TC/DSC Lifting Heights as a Function of Low<br>Temperature and Location   | L      | 1.2.13  |
| 14. | TC/DSC Transfer Operations at High Ambient<br>Temperatures  | L      | 1.2.14  |
| 15. | Boron Concentration in DSC Cavity Water   | PL     | 1.2.15, or 1.2.15a, or<br>1.2.15b or 1.2.15c      |
|     | Provision of TC Seismic Restraint Inside the Spent<br>Pool Building as a Function of Horizontal<br>eleration and Loaded Cask Weight | PL     | 1.2.16  |
| 17. | Vacuum Drying Duration Limits   | L      | 1.2.17 or 1.2.17a, or<br>1.2.17b, or 1.2.17c      |
| 18. | 24PTH DSC Transfer Time   | L      | 1.2.18  |
| 19. | Visual Inspection of HSM or HSM-H Air Inlets and<br>Outlets or HSM or HSM-H Thermal Performance                                     | D      | 1.3.1 or 1.3.2                                    |

# Table 1.3.1 Summary of Surveillance and Monitoring Requirements

#### **LEGEND**

PL ..... Prior to Loading

L ...... During loading and prior to movement to HSM or HSM-H pad

24 hrs Time following DSC insertion to HSM or HSM-H

S ...... Prior to movement of DSC to or from HSM or HSM-H

AN .... As necessary

D ..... Daily (24 hour frequency)

#### References

- Levy, I.S., et al., "Recommended Temperature Limits for Dry Storage of Spent Light Water Reactor Zircaloy-Clad Fuel Rods in Inert Gas," Pacific Northwest Laboratory Report, <u>PNL-6189</u>, May 1987.
- 2. Johnson, A.B., Jr., and E.R. Gilbert, "Technical Basis for Storage of Zircaloy-Clad Spent Fuel in Inert Gases," <u>PNL-4835</u>, September 1983.
- 3. Interim Staff Guidance No. 11, Revision 2, "Cladding Considerations for the Transportation and Storage of Spent Fuel," July 30, 2002.