

## **Attachment 2**



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NRC RAIs  
MDNR Tobico Marsh SGA DP, Revision 1

### ***Dose from LCTS System Operation***

*MicroShield Version 6.02 Calculations*

|   |   |
|---|---|
| MicroShield Source Term / Exposure Setting Parameters ..... | 1 |
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**MicroShield v6.02 (6.02-00140)**  
**MACTEC Development Corp.**

**Page** : 1  
**DOS File** : Tobico LCTS Exposure.ms6  
**Run Date** : October 8, 2004  
**Run Time** : 7:43:47 AM  
**Duration** : 00:00:01  
**File Ref** : Response to NRC RAIs  
**Date** : October 8, 2004  
**By** : Jeffrey W. Lively  
**Checked** : Michael McDonald

*Jeffrey W. Lively*  
*Michael McDonald*

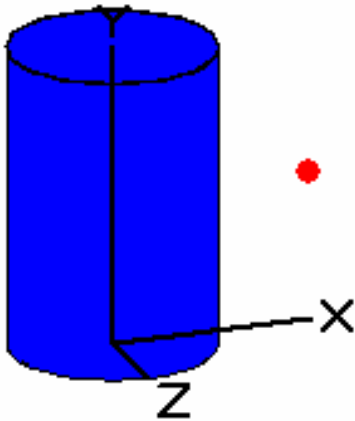
**Case Title:** MDNR Tobico SGA Site  
**Description:** Calculate Exposure to Workers Involved in Future LCTS Operations  
**Geometry:** Cylinder Volume - Side Shields (#7)  
**Scenario:** Simulates a large tank or vessel containing leachate from the MDNR cell. The source term is derived from the RESRAD Model (Leakage Scenario) and is equal to the highest concentration of radioactivity present in the leachate at any time (1000 years)

**Source Dimensions:**

**Height** 300.0 cm (9 ft 10.1 in)  
**Radius** 100.0 cm (3 ft 3.4 in)

**Dose Points**

| A   | X                        | Y                      | Z              |
|-----|--------------------------|------------------------|----------------|
| # 1 | 200.15 cm<br>6 ft 6.8 in | 150 cm<br>4 ft 11.1 in | 0 cm<br>0.0 in |



**Shields**

| Shield N   | Dimension                | Material | Density |
|------------|--------------------------|----------|---------|
| Source     | 9.42e+06 cm <sup>3</sup> | Water    | 1       |
| Transition |                          | Air      | 0.00122 |
| Air Gap    |                          | Air      | 0.00122 |
| Wall Clad  | .15 cm                   | Iron     | 7.8     |
| Top Clad   | .15 cm                   | Iron     | 7.8     |

**Source Input : Grouping Method - Actual Photon Energies**

| Nuclide | curies      | becquerels  | μCi/cm <sup>3</sup> | Bq/cm <sup>3</sup> |
|---------|-------------|-------------|---------------------|--------------------|
| Pb-210  | 3.7888e-006 | 1.4018e+005 | 4.0200e-007         | 1.4874e-002        |
| Ra-226  | 6.5219e-006 | 2.4131e+005 | 6.9200e-007         | 2.5604e-002        |
| Ra-228  | 2.5604e-002 |             |                     |                    |
| Th-228  | 2.5604e-002 |             |                     |                    |
| Th-230  | 2.5604e-002 |             |                     |                    |
| Th-232  | 2.5604e-002 |             |                     |                    |

**Buildup : The material reference is - Source  
Integration Parameters**

|                     |    |
|---------------------|----|
| Radial              | 10 |
| Circumferential     | 10 |
| Y Direction (axial) | 20 |

| Results       |                         |  |  |                                      |  |
|---------------|-------------------------|--|--|--------------------------------------|--|
| Energy<br>MeV | Activity<br>Photons/sec | Fluence Rate<br>MeV/cm <sup>2</sup> /sec<br>No Buildup | Fluence Rate<br>MeV/cm <sup>2</sup> /sec<br>With Buildup | Exposure Rate<br>mR/hr<br>No Buildup | Exposure Rate<br>mR/hr<br>With Buildup |
| 0.0108        | 3.410e+04               | 1.207e-36  | 1.174e-29  | 2.904e-37                            | 2.826e-30                              |
| 0.0117        | 1.936e+03               | 7.421e-38  | 7.221e-31  | 1.390e-38                            | 1.352e-31                              |
| 0.0465        | 5.677e+03               | 4.477e-07  | 9.570e-06  | 1.384e-09                            | 2.959e-08                              |
| 0.0811        | 4.349e+02               | 1.051e-06  | 1.432e-05  | 1.655e-09                            | 2.256e-08                              |
| 0.0838        | 7.224e+02               | 1.937e-06  | 2.538e-05  | 3.021e-09                            | 3.957e-08                              |
| 0.0949        | 3.275e+02               | 1.245e-06  | 1.410e-05  | 1.905e-09                            | 2.158e-08                              |
| 0.1862        | 7.915e+03               | 1.068e-04  | 6.659e-04  | 1.855e-07                            | 1.156e-06                              |
| 0.3097        | 1.610e+01               | 4.655e-07  | 1.996e-06  | 8.864e-10                            | 3.801e-09                              |
| Totals        | 5.113e+04               | 1.120e-04  | 7.313e-04  | 1.944e-07                            | 1.274e-06                              |

## Conclusion:

MDNR chose to perform a conservative, bounding calculation to assess the theoretical possible future dose to workers or visitors from an operating LCTS. While it is considered an unlikely prospect, based upon conversations with representatives of S.C. Holdings, MDNR's dose assessment assumes that a large leachate-holding tank will be installed at the site. (Note: S.C. Holdings indicated to MDNR that their plan is to pipe leachate extracted from the MDNR cell directly to a single, common leachate collection/processing facility located at on the Waste Management Site property.) The assumption that a large leachate-holding tank will be installed at the MDNR site is bounding in that it represents a potential source term far larger than would be possible with above ground piping or other smaller vessels and containers that might be envisioned.

The conceptual tank containing leachate from the MDNR cell is assumed to have a large capacity ( $\approx 10,000$  liters or 2,500 gal.) and is modeled completely full of leachate. The concentration of residual radioactivity assumed present in the leachate is taken from the maximum concentration projected over the 1000-year outlook by RESRAD using the "system leakage" scenario described in Attachment 1. The "system leakage" scenario itself is exceptionally conservative in that it assumes the presence of thorium radioactivity in slag at the specific activity limit.

The MicroShield photon transport modeling code projects a maximum potential gamma radiation exposure rate at a distance of 1 meter from the tank of  $1.27 \times 10^{-6}$  mR/h. Assuming a worker spent an entire work year in immediate proximity to an operating LCTS system under prohibitively unlikely radiological conditions, the resulting annual gamma radiation dose would be well less than 1 mrem/y.

Where:

$$H_A = R_{EXP} * t$$

$H_A$  is the annual external gamma radiation dose

$R_{EXP}$  is the calculated gamma exposure rate in mR/h

$t$  is the worker's annual exposure time in hours per year

$$H_A = \left( 1.27 \times 10^{-6} \frac{mR}{h} \right) * \left( \frac{2000 h}{y} \right) = 0.003 mR / y$$

Even if one were to assume that a number of such vessels were present as components of the LCTS operation, the resulting dose to the most exposed individuals would be well less than 1 mrem/year.