

December 7, 2004

U.S. Nuclear Regulatory Commission
Attention: Document Control Desk
Washington, D.C. 20555

Subject: Duke Energy Corporation
Catawba Nuclear Station, Units 1 and 2
Docket Numbers 50-413 and 50-414
Request for Relief Number 04-CN-001
Reply to Request for Additional Information

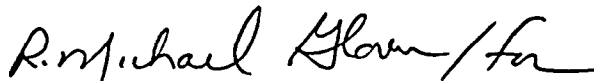
Reference: Letter from NRC to Duke Energy Corporation,
dated July 6, 2004

Pursuant to 10 CFR 50.4, please find attached the subject
reply to the reference letter. The format of the reply is to
restate the NRC question, followed by Catawba's response.

There are no regulatory commitments contained in this letter
or its attachment.

If you have any questions concerning this material, please
call L.J. Rudy at (803) 831-3084.

Very truly yours,



Dhiaa M. Jamil

LJR/s

Attachment

A047

Document Control Desk
Page 2
December 7, 2004

xc (with attachment):

W.D. Travers, Regional Administrator
U.S. Nuclear Regulatory Commission, Region II
Atlanta Federal Center
61 Forsyth St., SW, Suite 23T85
Atlanta, GA 30303

E.F. Guthrie, Senior Resident Inspector
U.S. Nuclear Regulatory Commission
Catawba Nuclear Station

S.E. Peters, Project Manager (addressee only)
U.S. Nuclear Regulatory Commission
Mail Stop O-8 G9
Washington, D.C. 20555-0001

REQUEST FOR ADDITIONAL INFORMATION

DUKE POWER COMPANY

CATAWBA NUCLEAR STATION, UNITS 1 AND 2

DOCKET NOS. 50-413 AND 50-414

The U. S. Nuclear Regulatory Commission (NRC) staff has reviewed the licensee's submittal dated February 19, 2004, regarding a request for relief associated with Category B-J full penetration welds of nozzles in vessels, branch connection welds, nominal pipe size 4 or larger. The NRC staff has identified the following information that is needed to enable the continuation of its review.

1. On page 2 of the submittal, you reference the nozzle to branch connection weld 1NC22-WN8, but no further information is provided. Please provide the non-destructive examination worksheets and associated figures for this weld.

Catawba response:

Manufacturer's drawings, profiles, and examination records from the 1993 inspections are attached.

- a. Catawba Unit 1 Drawing CNM 1201.01-181/4
- b. Catawba Unit 1 Drawing CNM 1201.01-50
- c. Catawba Unit 2 Drawing CNM 2201.01-104/4
- d. Catawba Units 1 and 2 Drawing CNM 1201.01-50/3A
- e. Examination records for Catawba Unit 1 Weld 1NC22-WN8
- f. Examination records for Catawba Unit 2 Welds 2NC11-WN8 and 2NC11-WN7

2. For the welds that you are requesting relief, identify the weld material. If a butter was used, identify the butter material. Identify the nominal reactor cooling system pipe diameter and the wall thickness for the branch connections.

Catawba response:

The weld material for all referenced branch connections is 308 stainless steel with no buttering. The reactor coolant loop piping has an inside diameter of 29 inches. The wall thickness of the branch connections are as follows:

- a. Weld 1NC22-WN8 is a 12" Schedule 140 (1.125") nozzle.

- b. Weld 2NC11-WN7 is a 14" Schedule 160 (1.406") nozzle.
c. Weld 2NC11-WN8 is a 12" Schedule 140 (1.125") nozzle.

3. The American Society of Mechanical Engineers (ASME) Boiler and Pressure Vessel Code (Code) Section XI, Appendix III, III-4450 states "Welds that cannot be examined from at least one side (edge) using the angle beam technique shall be examined by another volumetric method." On page 2 of your submittal, you state that the connection is not accessible from the inside surface and that radiography cannot be performed because of geometry. Discuss the radiography performed to satisfy Appendix III requirements and explain why radiography has not been proposed or considered.

Catawba response:

The branch connection welds were fabricated by Southwest Fabricating and Welding in accordance with the requirements of ASME Section III, 1974 Edition with no addenda. Radiography was performed in the fabricator's shop where access was available from the inside for placement of the radiographic film. After installation at Catawba Nuclear Station, access is no longer possible from the inside because of the welds connecting the piping section to the main coolant loop. Radiography for inservice inspection is not an option because there is no access for film placement.

4. On page 2 of the submittal, you indicate that the subject welds were volumetrically examined during preservice and the first 10-year inservice inspection (ISI) interval. Discuss the coverage achieved, transducers used, ultrasonic testing (UT) technique (manual/automatic), and availability of the actual data from the inspections. Describe the conditions that exist that have rendered UT ineffective for the second 10-year interval.

Catawba response:

During preservice and inservice inspections for the first interval, ultrasonic examinations were performed using a manual, contact technique. The search units contained dual element, side by side, refracted longitudinal wave transducers having a frequency of 1.0 MHz, a refracted angle of 45 degrees and a focal depth of 2.5 inches. Transducer element shapes were square with a size of 1.0" x 1.0" and rectangular with a size of 0.75" x 1.0". Combinations of flat and contoured wedges were used to scan axially and

circumferentially from the main coolant loop side of the weld to the extent practical.

ASME Section XI, Appendix III paragraphs III-4420 requires coverage of the examination volume in two beam path directions. Paragraph III-4430 requires scanning over the weld crown in two opposing directions. The weld configuration as shown on the attached profile sketches, Figures 1, 2, and 3, only allows scanning from the main coolant loop side of the weld. The aggregate coverage achieved in 1993 was approximately 35% for each weld.

Preservice ultrasonic examination was performed in accordance with the requirements of ASME Section XI, 1974 Edition through the Summer 1975 Addenda. The first interval inservice ultrasonic examination was performed in accordance with the requirements of ASME Section XI, 1980 Edition through the Winter 1981 Addenda. These earlier code editions did not require that personnel demonstrate their capability to determine the difference between geometry and flaws. The second interval code of record is ASME Section XI, 1989 Edition with no addenda. Appendix III, paragraph III-2200 (b) requires such a demonstration.

Beyond these factors is the recent acknowledgement within the industry that no effective UT technique or equipment is currently available to perform code examinations on cast stainless steel materials.

5. On page 2 of the submittal, your proposed alternative is to use liquid penetrant testing (PT) and visual testing (VT-2) in lieu of volumetric examinations. The Code-required PT is performed once per interval. Will the PT be performed more frequently than once per interval? Discuss the PT and VT-2 examination frequency for the remaining ISI interval.

Catawba response:

Duke Energy Corporation will perform the code required examinations at these weld locations for the remainder of the interval. These consist of a liquid penetrant examination (completed) and a VT-2 examination performed after each refueling outage during a system leakage test.

6. If UT examinations are not capable of providing reliable information of weld integrity, provide a discussion of the potential for flaws to develop in the weld area. Influences upon the weld region include: fluid temperature

fluctuations, fluid direction (into or out of the connection nozzle), flow fluctuations, vibrations, cycling, water chemistry, etc.

Catawba response:

Flaws are not likely to develop in the stainless steel branch line nozzle to cast stainless steel reactor coolant system weld locations due to their similar metal properties, clean water chemistry, and relatively low number of thermal cycles. Similar system operating conditions exist at the reactor coolant system to steam generator (SG) nozzle welds where dissimilar metal properties are more likely to experience flaws. However, during the most recent Catawba Unit 2 outage, all eight SG nozzle welds were examined by radiography (this technique was used because of the cast stainless issue) with no service induced flaws being identified.

7. Are any of these welds included in risk-informed examination requirements? Are there other locations with similar materials and operating conditions that can be volumetrically examined?

Catawba response:

The Catawba plant does not have a risk informed inservice inspection (RI-ISI) program, but the McGuire plant does. Since the two plants have nearly identical Westinghouse reactor coolant systems, some conclusions may be drawn by comparing RI examinations required at McGuire with what could be expected for Catawba. Main coolant loop branch connection welds of this type were not evaluated to be within a high safety significant piping segment that required examination. There are circumferential piping welds joining static cast stainless steel elbows to carbon steel nozzles that can be volumetrically examined using radiography at Catawba Unit 2; however, because of the steam generator replacement at Catawba Unit 1, no such welds are in the inservice inspection plan.

8. The ASME Code provides minimum prescriptive-based examination criteria in Section XI, Appendix III. In Appendix III, Supplement 4, Paragraph 4(c), the Code recommends licensees qualify examiners and procedures using welded samples and simulated or actual flaws located in positions where geometry may make them more difficult to detect. The purpose of the examination procedure

qualification is to determine that the proposed examination technique is capable of detecting the specified flaws of interest and that the examination capabilities and limitations are identified.

In the first paragraph of page 2 of the submittal, you indicate that the demonstration used a mock-up of similar materials with flaw depths required by Section XI, Appendix VIII, Supplement 2, 1995 Edition with 1996 Addenda. The Supplement 2 flaw depths can be any through-wall depth and the inspection volume is the inner 1/3 of the through-wall depth. What are the specific flaw depths, orientations, and locations used for the demonstrations? Identify the flaw depths that can be effectively detected.

Catawba response:

The flaw depths used in the demonstration are shown below:

Flaw Depth	Flaw Orientation	Flaw Location	Flaw Length
24.5%	Circumferential	Wrought SS Safe End	0.750"
10%	Circumferential	Cast Stainless Elbow	0.400"
15.5%	Circumferential	Wrought SS Safe End	0.650"
8%	Circumferential	Wrought SS Safe End	0.485"
16%	Circumferential	Cast Stainless Elbow	0.810"

All flaws were normal to the inside surface within manufacturer's tolerance. All scanning was performed from the cast stainless steel elbow. None of the flaws were detected.

9. The ASME Code provides the minimum criteria for performing prescriptive-based UT. The licensee may use additional equipment and expertise to perform an examination. Extensive research, round-robin testing, and demonstrations have been performed on cast austenitic material using different transducer configurations (phase array, SAFT-UT, low frequency twin crystal, etc.) and data manipulation (computer) techniques. Discuss any other

equipment and UT techniques that were considered and were determined ineffective for this application.

Catawba response:

Other ultrasonic techniques were considered and rejected for these welds because of the weld joint geometry and a review of the data contained in EPRI Report TR-107481, "Status of the Ultrasonic Examination of Reactor Coolant Loop Cast Stainless Steel Materials," issued in March 1998. The results of this study indicate that an ultrasonic examination of welds in cast stainless steel main loop piping is unreliable with currently available techniques including Phased Array, SAFT, and EMAT technology when performed from the outside surface. Duke Energy Corporation is aware that Pacific Northwest National Laboratory is investigating low frequency phased array in combination with SAFT to improve flaw detection in cast stainless steel piping and will remain cognizant of changing technology that can be employed in an operating nuclear plant environment. Duke Energy Corporation will employ the latest proven techniques as they become commercially available.

10. With current capabilities for detecting flaws at depths beyond the volume identified in Figure IWB-2500-11, what is the maximum acceptable IWB-3600 flaw depth for each of the subject welds? The maximum depth should include flaw growth (based on the different flaw types, such as, low/high cycle fatigue, creep, primary water stress corrosion cracking) between examinations. Discuss the effectiveness of using UT to detect the maximum flaw depth.

Catawba response:

There are three welds associated with this relief request. Two are the welds between the Loop B hot leg and the pressurizer surge line on Units 1 and 2. The other weld is between the Loop B hot leg and the RHR suction line on Unit 2. These welds are between the centrifugally cast stainless steel piping and stainless steel nozzle forgings. Creep and primary water stress corrosion cracking are not a concern at this location based on properties of the base and weld filler materials.

For Duke Energy Corporation to respond to this question, expensive analytical work would have to be performed to establish a location-specific maximum allowable flaw depth in the piping based on IWB-3600 rules. This would involve:

- 1) Postulating an initial flaw size and shape,
- 2) Determining the stresses at the location for all operating conditions,
- 3) Performing a fatigue crack growth analysis (a validation that stress corrosion cracking and thermal aging in cast austenitic stainless steels are not significant concerns will be required),
- 4) Determining the maximum flaw dimensions at the end of the evaluation period (10 year interval between inspections), and
- 5) Comparing the maximum calculated flaw size to the maximum allowable flaw size for normal and upset conditions and for emergency and faulted conditions, then repeating this process to maximize the initial postulated flaw depth considering different flaw shapes while minimizing the margin between the final calculated and allowable flaw sizes.

The intent of this activity is to evaluate a location-specific flaw size with the capability of UT to detect this particular flaw. An estimate for the determination of this location-specific flaw size is roughly \$75,000 for the three locations based on other recent analytical fracture mechanics evaluations. Qualified vendors to perform this work are Westinghouse, Structural Integrity Associates, and AREVA.

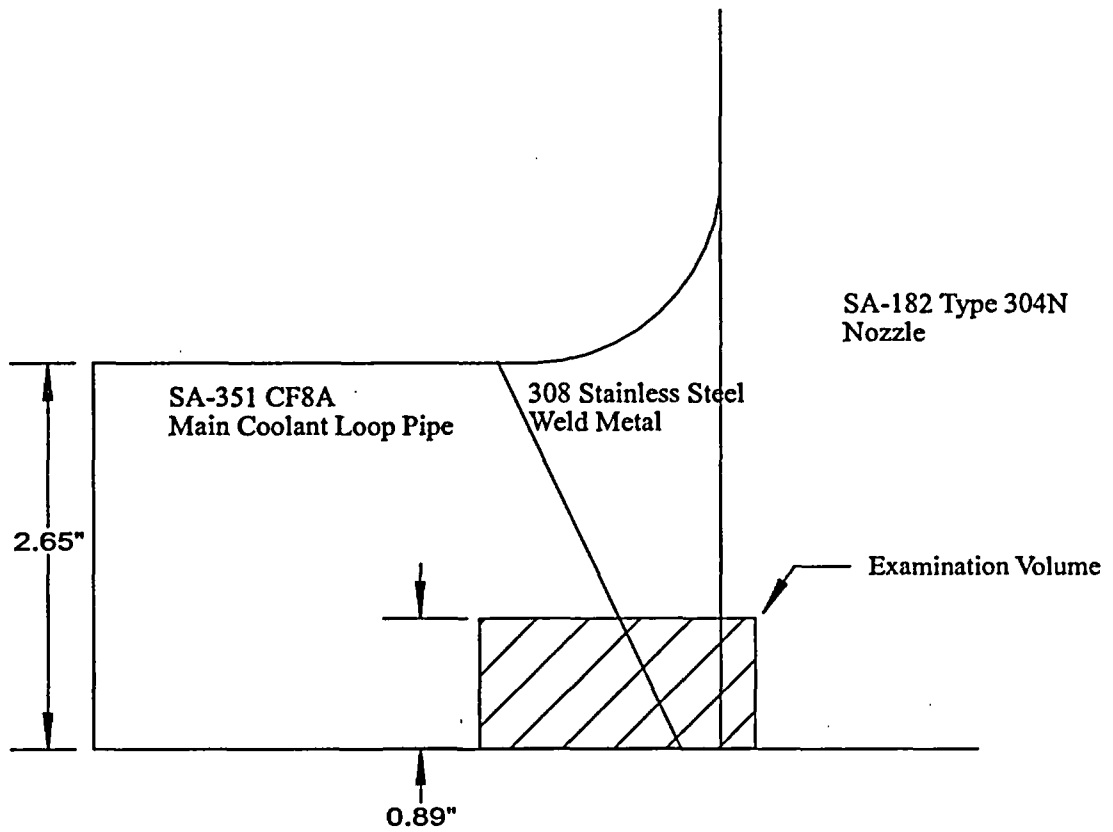
Alternatively, in the event of flaw development, it can be stated that due to the weld configuration geometry, flaw path propagation would be longer through the weld material than through the pipe material.

11. The inspectability of cast austenitic cast material is dependent on the material microstructure which is dependent on material cleanliness, second phase precipitates, super-cooled liquid, and heat extraction from the mold surface. Because of the variability between similar cast products, the results from a mock-up may also be a variable. Besides material specification and configuration, discuss other comparisons between the subject welds and the mock-up that support the existence of comparable microstructures.

Catawba response:

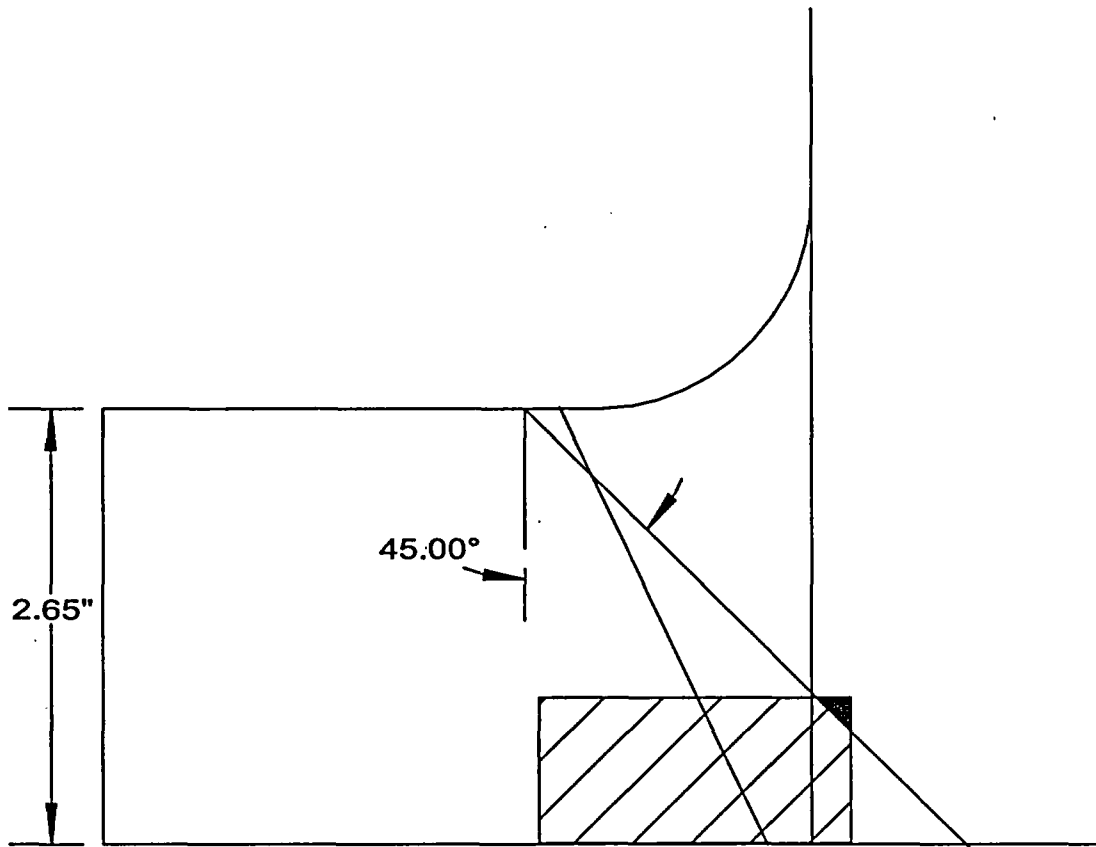
The demonstration mock-up used a statically cast stainless steel elbow with an equi-axial grain structure. The main

coolant loop piping is made of centrifugally cast stainless steel. The microstructure of the main coolant loop piping is unknown, as only destructive means can determine this and no investigations were performed during construction or preservice inspection.



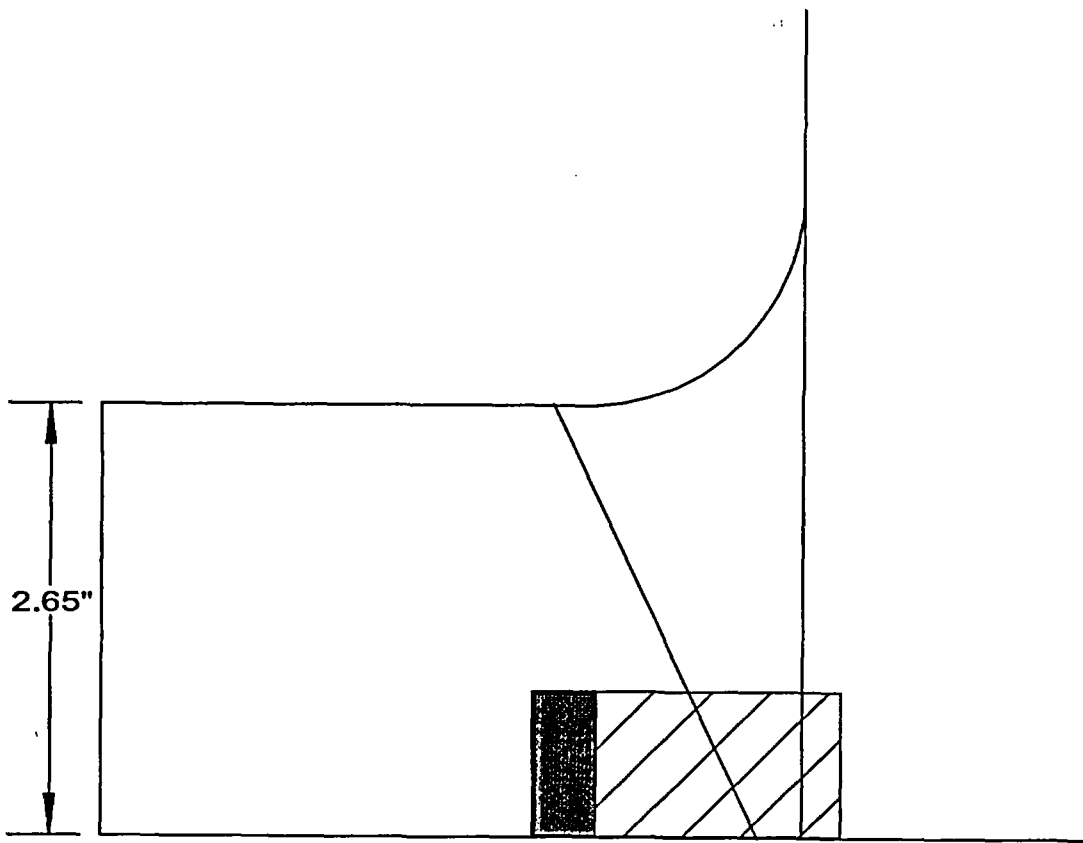
Cross section view 90 deg. to the axis of the main run of pipe

Figure 1 Cross-section Typical Branch Connection



Coverage in the axial direction = 98.8% from one direction
 Red triangle shows portion not covered by sound beam.

Figure 2 Typical Coverage Plot



Circumferential scan coverage = 20% in two directions.
Shaded area covered, cross-hatch area no coverage.

Figure 3 Typical Coverage Plot

Component/Weld ID: <u>1NC 22-WN8</u>	Item No: <u>B09.031.003</u>	remarks:
<input type="checkbox"/> NO SCAN SURFACE BEAM DIRECTION <input checked="" type="checkbox"/> LIMITED SCAN <input checked="" type="checkbox"/> 1 <input type="checkbox"/> 2 <input type="checkbox"/> 1 <input checked="" type="checkbox"/> 2 <input checked="" type="checkbox"/> cw <input checked="" type="checkbox"/> ccw FROM _____ to _____ INCHES FROM WO <u>0.0"</u> to <u>2.0"</u> ANGLE: <input type="checkbox"/> 0 <input checked="" type="checkbox"/> 45L <input type="checkbox"/> 60 other _____ FROM <u>0</u> DEG to <u>360</u> DEG	Due to Branch Connection weld.	
<input checked="" type="checkbox"/> NO SCAN SURFACE BEAM DIRECTION <input type="checkbox"/> LIMITED SCAN <input type="checkbox"/> 1 <input checked="" type="checkbox"/> 2 <input checked="" type="checkbox"/> 1 <input type="checkbox"/> 2 <input checked="" type="checkbox"/> cw <input checked="" type="checkbox"/> ccw FROM _____ to _____ INCHES FROM WO _____ to _____ ANGLE: <input type="checkbox"/> 0 <input checked="" type="checkbox"/> 45L <input type="checkbox"/> 60 other _____ FROM <u>0</u> DEG to <u>360</u> DEG	Not required by ISI Plan	
<input type="checkbox"/> NO SCAN SURFACE BEAM DIRECTION <input type="checkbox"/> LIMITED SCAN <input type="checkbox"/> 1 <input type="checkbox"/> 2 <input type="checkbox"/> 1 <input type="checkbox"/> 2 <input type="checkbox"/> cw <input type="checkbox"/> ccw FROM _____ to _____ INCHES FROM WO _____ to _____ ANGLE: <input type="checkbox"/> 0 <input type="checkbox"/> 45 <input type="checkbox"/> 60 other _____ FROM _____ DEG to _____ DEG		
<input type="checkbox"/> NO SCAN SURFACE BEAM DIRECTION <input type="checkbox"/> LIMITED SCAN <input type="checkbox"/> 1 <input type="checkbox"/> 2 <input type="checkbox"/> 1 <input type="checkbox"/> 2 <input type="checkbox"/> cw <input type="checkbox"/> ccw FROM _____ to _____ INCHES FROM WO _____ to _____ ANGLE: <input type="checkbox"/> 0 <input type="checkbox"/> 45 <input type="checkbox"/> 60 other _____ FROM _____ DEG to _____ DEG	Sketch(s) attached <input checked="" type="checkbox"/> yes <input type="checkbox"/> no	
Prepared By: <u>Richard & Childers</u>	Level: <u>II</u>	Date: <u>11-11-93</u>
Reviewed By: <u>Larry Mauldin</u>	Date: <u>11-11-93</u>	Authorized Inspector: <u>Robert McNeil</u>
		Sheet <u>2</u> of <u>3</u>
		Date: <u>NOV 15 1993</u>

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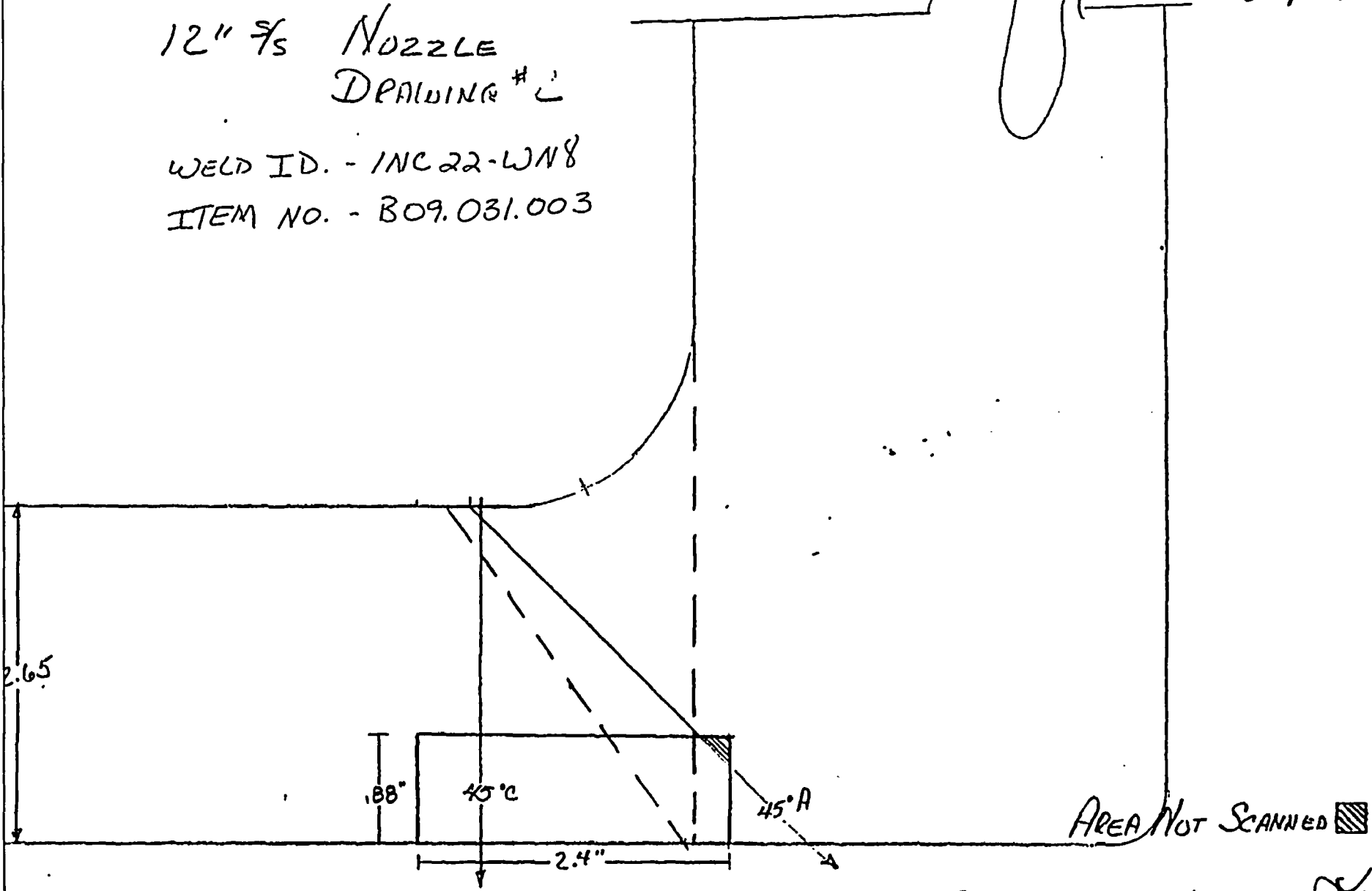
0 0 0 0 2 1 7 1 7

ATTACHMENT #

2 of 3 - 884

12" $\frac{7}{8}$ NOZZLE
DRAWING # 2

WELD ID. - INC 22-WN8
ITEM NO. - B09.031.003

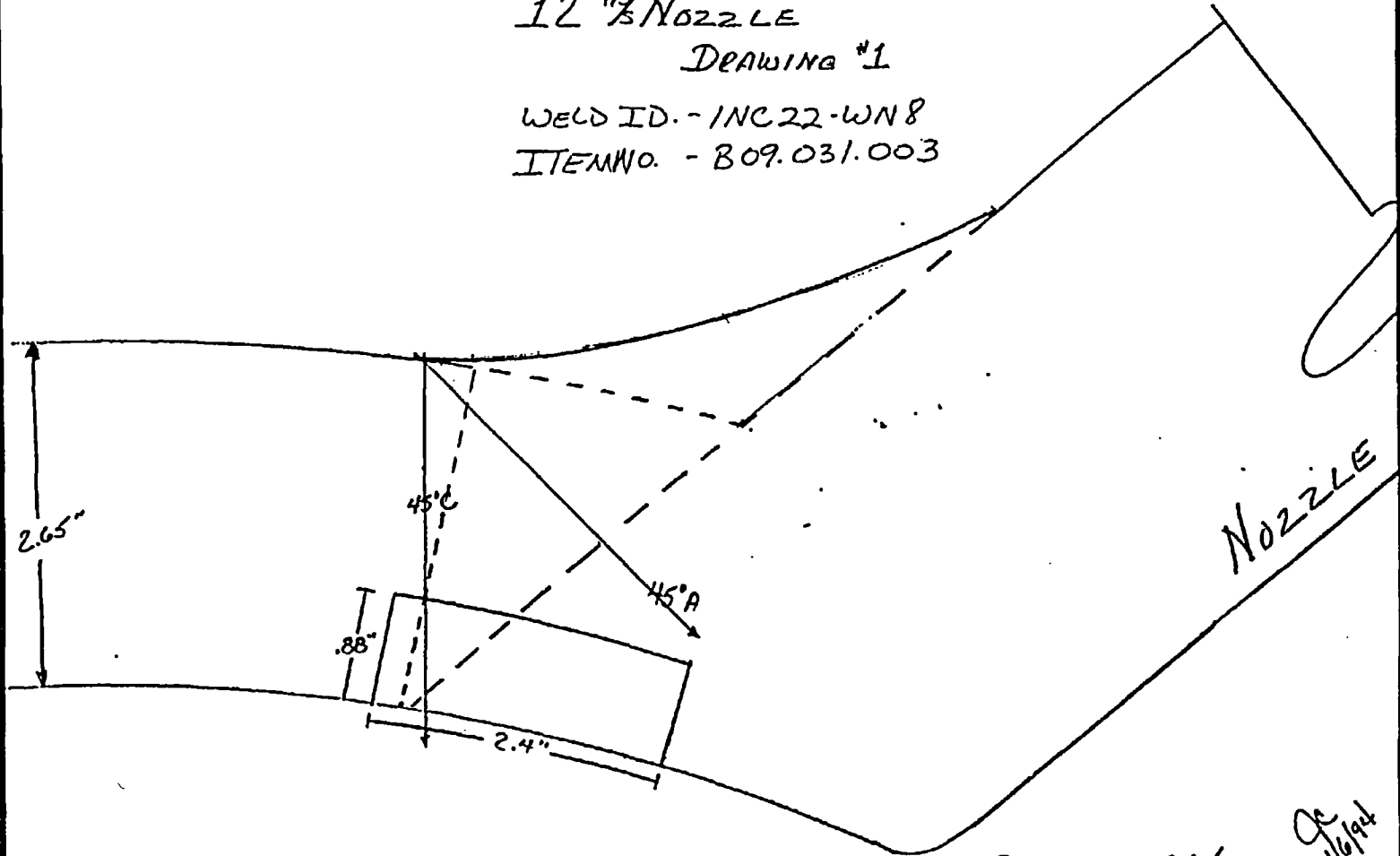


ATTACHMENT-4
Page 4 of 7
3 of 3 rpm

12 1/2" NOZZLE

DRAWING #1

WELD ID. - INC22-WN8
ITEM NO. - 809.031.003



By: Richard B. Childers
REVIEWED BY: Larry Maulder

RC
11/6/94

DUKE POWER COMPANY
ULTRASONIC CALIBRATION SHEET FOR ANALOG INSTRUMENTS

FORM NDE UT-1A

REVISION 2

Station: Catawba	Unit: 1	Date: 11-11-93	Sheet number: 9301009
Procedure: NDE 610	Rev: 1	FC: N/A	Couplant: Ultragel II
Examiner: <i>Richard B. Childers</i>	Level: II	Calibration Block ID: 50386	Batch No: 093001
Examiner: <i>Nancy Moss</i>	Level: II	Calibration Block Temp: 22°C	Pyrometer S/N: MCNDE27016 Cal. due: 940701

REFERENCE BLOCK	SIMULATOR BLOCK
ID: 610C	ID: N/A
Type: MOD IIV Block	Material: s/s
Reflector Type: _____	Metal Path: _____
Signal Amp: _____	Gain: _____

INSTRUMENT	TRANSDUCER
Model: USK-7D	Type: Single <input type="checkbox"/> Dual <input checked="" type="checkbox"/>
Manufacturer: Krautkramer	Size: 2-.75"X1.0" Freq: 1 Mhz
Serial No: 32810-922	Manufacturer: Megasonics
Serial No: 90145	Nominal Δ 45°

INSTRUMENT SETTINGS	CALIBRATION	METHOD	CABLES
Reject: 0	Reflector Type: Hole	<p>1 Major Screen Div = .500" inches</p>	RG62 <input type="checkbox"/>
PRF: DUAL	amplitude % FSH		RG58 <input type="checkbox"/>
Delay: 7.6	metal path inches		RG174 <input checked="" type="checkbox"/>
Range: 5.0"	1/8 node 80 % .946		Belden 8218 <input type="checkbox"/>
Velocity: 220.9	2/8 node 66 % 1.52		Length: 6'
Frequency: .5-7	3/8 node 50 % 2.43		Initial Calibration Time: 0905
Gain: 50	5/8 node %		CAL CHECKS
Filter: Full Wave	7/8 node %		Time: 1045
ZERO: 9.16	other %		Initials: RAC
Thru <input type="checkbox"/> Pulse/Echo <input checked="" type="checkbox"/>	opposite notch 36 % 3.19		

Jack Used: T <input checked="" type="checkbox"/>	Wave Mode: longitudinal: <input checked="" type="checkbox"/>	shear: <input type="checkbox"/>	surface: <input type="checkbox"/>
R <input checked="" type="checkbox"/>	cal. direction: axial <input checked="" type="checkbox"/>	circ. <input checked="" type="checkbox"/>	

REMARKS: New reference is -52dB due to notch gain.

REVIEWED BY: <i>Nancy Maulder</i>	LEVEL: II	DATE: 11-11-93	Authorized Inspector: <i>Robert McMillan</i>	DATE: NOV 15 1993
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OP

Attachment 2
Page 7 of 7

Form NDE-35A Revision 1

DUKE POWER COMPANY
 STATION CATAWBA UNIT 1
LIQUID PENETRANT EXAMINATION REPORT

Weld/ID No. 1NC22-WN8 Material Type: SS CS
 Diameter 12.00 Schedule/Thickness 02.300 Inconel
 Work Order No. N/A ISI PSI Other

Procedure Revision No. 14
 Surface Temperature 91°F
 M&TE S/N: CNNDE0004
 Penetrant Materials Category:
 A A(SE) B C D
 A(SE) Approved _____

SKETCH OF ITEM EXAMINED

Penetrant Materials Data:
 Batch Numbers
 Cleaner 90A043
 Penetrant 78E084
 Developer 92D06K
 Remover N/A

Fluorescent Nonfluorescent
 Black Light Intensity Verified
 Time N/A Date N/A
 Light Meter S/N: N/A

Acceptance Standards Used: Appendix A F
 B G
 C H
 E J
 Other Acceptance Standards Used: N/A Other K

Indication Number	Indication Type / Dimensions	Reference Documents	Construction Rejectable	ISI Reportable
	NONE			

PIR S/N: N/A Acceptable
 Exam Limitations: None, (100 % Examined) _____ % Examined
 Comments: CNM1201.01-181/4 PC. C TO PC. P1

Examiner Roger L. Burnett Level II Date 11-11-93
 Examiner _____ Level _____ Date _____
 Reviewed By: [Signature] Level II Date 11-11-93
 Final Review Date 11-11-93 ANII Review Date 11-93 Item No. B09.031.003A

JTC
11-22-93

00075 1138

DUKE POWER COMPANY						FORM NDE UT-1A		
ULTRASONIC CALIBRATION SHEET FOR ANALOG INSTRUMENTS						REVISION 2		
Station: Catawba		Unit: 2		Date: 2-11-93		Sheet number: 9302006		
Procedure: NDE 610		Rev: 0		FC: 91-19 91-17 92-02 92-03 92-07 92-14 93-04		Couplant: Ultragel II		
Examiner: <i>J. Bebb</i>		Level: II		Calibration Block ID: 50386		Pyrometer S/N: MCQUA-32848 Cal. due: 7/28/93		
Examiner: <i>Larry Thawles</i>		Level: II		Calibration Block Temp: 22°C				
REFERENCE BLOCK			SIMULATOR BLOCK					
ID: 91-6549			ID: R111		Signal Amp: 62%		Gain: 34.5	
Type: D.S.C. Block			Material: s/s		Reflector Type: Hole		Metal Path: .983"	
INSTRUMENT			TRANSDUCER					
Model: USK-7D		Type: Single <input type="checkbox"/> Dual <input checked="" type="checkbox"/>		Size: 2-.75"X1.0"		Freq: 1 Mhz		
Manufacturer: Krautkramer		Serial No: 32810-950		Serial No: 90145		Meas. <input checked="" type="checkbox"/> 45°		
Serial No: 32810-950		Serial No: 90145		Manufacturer: Megasonics		Nominal <input checked="" type="checkbox"/> 45°		
INSTRUMENT SETTINGS		CALIBRATION		METHOD		CABLES		
Reject	0	Reflector	amplitude	metal path			RG62 <input type="checkbox"/>	
PRF	DUAL	Type: Hole	% FSH	inches			RG58 <input type="checkbox"/>	
Delay	9.3	1/8 node	80 %	.903			RG174 <input checked="" type="checkbox"/>	
Range	5.0"	2/8 node	66 %	1.729			Bolden 8218 <input type="checkbox"/>	
Velocity	229.6	3/8 node	50 %	2.4			Length: 6'	
Frequency	.5-7	1/8 node	%				Initial Calibration	
Gain	48	1/8 node	%				Time: 0630	
Filter	Full Wave	1/8 node	%				CAL CHECKS	
Thru <input type="checkbox"/> Pulse/Echo <input checked="" type="checkbox"/>		other	%				Time	
		opposite notch	36 %	3.19			Initials	
Jack Used: T	<input checked="" type="checkbox"/>	cal. direction: axial <input checked="" type="checkbox"/> circ. <input checked="" type="checkbox"/>			0844 <i>ASB</i>			
R	<input checked="" type="checkbox"/>				0916 <i>ASB</i>			
Wave Mode:		longitudinal: <input checked="" type="checkbox"/>		shear: <input type="checkbox"/>		1025 <i>ASB</i>		
		surface: <input type="checkbox"/>		Component/Item No:		B09.031.005 B09.031.006		
REMARKS: Simulator was performed with pulser on high with gain at 34.5 dB. New reference is 53dB due to notch gain.								
REVIEWED BY: <i>W. C. Leaper</i>		LEVEL: II		DATE: 2-15-93		Authorized Inspector: <i>Robert Marshall</i>		
FEB 18 1993								

0 0 7 J 1 3 6 3

DUKE POWER COMPANY

ISI LIMITATION REPORT

FORM NDE-UT-4

Revision 1

Component/Weld ID: 2NC 11-WN8 Item No: 809.031.006

remarks:

NO SCAN SURFACE BEAM DIRECTION
 LIMITED SCAN 1 2 1 2 cw ccw
 FROM _____ to _____ INCHES FROM WO 0.0" to 2.0"
 ANGLE: 0 45L 60 other _____ FROM 0 DEG to 360 DEG

Due to Branch Connection weld.

NO SCAN SURFACE BEAM DIRECTION
 LIMITED SCAN 1 2 1 2 cw ccw
 FROM _____ to _____ INCHES FROM WO _____ to _____
 ANGLE: 0 45L 60 other _____ FROM 0 DEG to 360 DEG

Not required by ISI Plan

NO SCAN SURFACE BEAM DIRECTION
 LIMITED SCAN 1 2 1 2 cw ccw
 FROM _____ to _____ INCHES FROM WO _____ to _____
 ANGLE: 0 45 60 other _____ FROM _____ DEG to _____ DEG

NO SCAN SURFACE BEAM DIRECTION
 LIMITED SCAN 1 2 1 2 cw ccw
 FROM _____ to _____ INCHES FROM WO _____ to _____
 ANGLE: 0 45 60 other _____ FROM _____ DEG to _____ DEG

Sketch(s) attached
 yes ^{wet 4.40} no

Prepared By: Larry Mauldin Level: II Date: 2-11-93

Sheet 2 of 25

Reviewed By: W. C. Leeper Date: 2-15-93

Authorized Inspector: Robert McGill Date: FEB 18 1993

Handwritten initials and date:
 [Signature] 4/15/93

ATTACHMENT F Page 4 of 11

Station CATAWBA Unit 2 Rev. _____ File No. 2NC-WNB Sheet 3 of 5
 Subject LIMITED EXAM DATA
12" 3/8 NOZZLE By Rory Thauler Date 2-11-93
 Prob No. B09.031.006 Checked By W.C. Lopez Date 2-15-93

DRAWING #1

CROSS SECTIONAL AREA: $88" \times 2.4" = 2.112 \text{ sq.in.}$

$\times 2 \text{ SCANS}$
 $\hline 4.224 \text{ sq.in.}$

AREA OF LOSS:

AXIAL: $2.112 \div 4.224 \times 100 = 50\%$

CIRC: No Loss

DRAWING #2

CROSS SECTIONAL AREA: $88" \times 2.4" = 2.112 \text{ sq.in.}$

$\times 2 \text{ SCANS}$
 $\hline 4.224 \text{ sq.in.}$

AREA OF LOSS:

AXIAL: $\frac{254.25}{2} + 2.4 = 2.43125$

$2.43125 \div 4.224 \times 100 = 57.558$

CIRC: 100%

DRAWING #1

	AXIAL	CIRC
DRAWING #1	50	0
DRAWING #2	57.6	100
	107.6	100%

DRAWING #2

107.6

$53.8 + 50 \div 2 = 51.9\%$

∴ A 45° L-WAVE WAS USED TO SCAN WELD FROM 1 DIRECTION ONLY.
 NO SCAN WAS PERFORMED FROM SUB 2 (NOZZLE WELD) DUE TO
 NOZZLE WELD CONFIGURATION.

∴ NO OTHER LIMITATIONS

AREA OF LOSS 51.9%

0.073 | 364

0075 1138

DUKE POWER COMPANY				FORM NDE UT-1A									
ULTRASONIC CALIBRATION SHEET FOR ANALOG INSTRUMENTS				REVISION 2									
Station: Catawba		Unit: 2	Date: 2-11-93	Sheet number: 9302006									
Procedure: NDE 610	Rev: 0	FC: 91-13 91-17 92-02 92-03 92-07 92-14 93-04	Couplant: Ultragel II	Batch No: 092041									
Examiner: <i>H. Bibb</i>	Level: II	Calibration Block ID: 50386	Pyrometer S/N: MCQUA-32848		Cal. due: 7/28/93								
Examiner: <i>Larry Thawles</i>	Level: II	Calibration Block Temp: 22°C											
REFERENCE BLOCK		SIMULATOR BLOCK											
ID: 91-6549	ID: R111	Signal Amp: 62%	Gain: 34.5										
Type: D S C Block	Material: s/s	Reflector Type: Hole	Metal Path: .983"										
INSTRUMENT		TRANSDUCER											
Model: USK-7D	Type: Single <input type="checkbox"/> Dual <input checked="" type="checkbox"/>	Size: 2-.75"X1.0"	Freq: 1 Mhz	Meas. Δ 45°									
Manufacturer: Krautkramer	Serial No: 90145	Manufacturer: Megasonics	Nominal Δ 45°										
Serial No: 32810-950													
INSTRUMENT SETTINGS		CALIBRATION		METHOD									
Reject: 0	Reflector Type: Hole	amplitude % FSH	metal path inches										
PRF: DUAL	1/8 node	80 %	.903										
Delay: 9.3	2/8 node	66 %	1.729										
Range: 5.0"	3/8 node	50 %	2.4										
Velocity: 229.6	1/8 node	%											
Frequency: .5-7	1/8 node	%											
Gain: 48	1/8 node	%											
Filter: Full Wave	1/8 node	%											
Thru <input type="checkbox"/> Pulse/Echo <input checked="" type="checkbox"/>	other	%											
Jack Used: T <input checked="" type="checkbox"/> R <input checked="" type="checkbox"/>	opposite notch	36 %	3.19										
Wave Mode:		cal. direction: axial <input checked="" type="checkbox"/> circ. <input checked="" type="checkbox"/>		CABLES									
longitudinal: <input checked="" type="checkbox"/>	shear: <input type="checkbox"/>	surface: <input type="checkbox"/>	RG62 <input type="checkbox"/> RG58 <input type="checkbox"/> RG174 <input checked="" type="checkbox"/> Bolden 8218 <input type="checkbox"/> Length: 6' Initial Calibration Time: 0630 CAL CHECKS <table border="1" style="width:100%; border-collapse: collapse;"> <thead> <tr> <th>Time</th> <th>Initials</th> </tr> </thead> <tbody> <tr> <td>0844</td> <td><i>ddb</i></td> </tr> <tr> <td>0916</td> <td><i>ddb</i></td> </tr> <tr> <td>1025</td> <td><i>ddb</i></td> </tr> </tbody> </table>			Time	Initials	0844	<i>ddb</i>	0916	<i>ddb</i>	1025	<i>ddb</i>
Time	Initials												
0844	<i>ddb</i>												
0916	<i>ddb</i>												
1025	<i>ddb</i>												
REMARKS: Simulator was performed with pulser on high with gain at 34.5 dB. New reference is 53dB due to notch gain.		Component/Item No: B09.031.005 B09.031.006											
REVIEWED BY: <i>W. C. Leaper</i>	LEVEL: II	DATE: 2-15-93	Authorized Inspector: <i>Robert McNeil</i>	FEB 18 1993									

ATTACHMENT - F Page 6 of 11

Form 28294 (RS-88)

Form NDE-25A

Revision 1

DUKE POWER COMPANY

PROJECT CATAWBA

MAGNETIC PARTICLE/LIQUID PENETRANT EXAMINATION REPORT

Weld No. 2NC11-WN8 Unit No. 2 Date 2-11-93
 Diameter 12.00 Schedule/Thickness 2.300 Type Material SS CS
 Work Order No. N/A QA Condition 1

Procedure NDE35A-E / Rev 13
 NDE-98 Approved N/A
 Radiation Level N/A

SKETCH OF ITEM EXAMINED

Inspector	Level
<i>Bob Spillars</i>	II

00750810

Indication Number	Indication Dimensions Length/Width/Diameter, etc.	Acceptable	Reportable	Reference Documents
NONE				

<p>MT DATA MT Method Used <input type="checkbox"/> Fluorescent <input type="checkbox"/> Nonfluorescent <input type="checkbox"/> Wet <input type="checkbox"/> Dry</p> <p>MT Unit Serial No. _____ Particle Batch No. _____</p> <p>MT Technique Used: <u>N A</u> <input type="checkbox"/> Circular <input type="checkbox"/> Direct Contact Amp _____ <input type="checkbox"/> Central Conductor Amp _____</p> <p>MT Field Indicator Used <input type="checkbox"/> Yes <input type="checkbox"/> No <input type="checkbox"/> Yoke <input type="checkbox"/> AC <input type="checkbox"/> DC <input type="checkbox"/> Prod</p> <p><input type="checkbox"/> Longitudinal Number Turns in Coil _____ Amp _____</p>	<p>PT DATA PT Batch Number Cleaner <u>91B04K</u> Penetrant <u>78E084</u> Developer <u>92G07K</u> Remover <u>N/A</u> <input type="checkbox"/> Fluorescent <input checked="" type="checkbox"/> Nonfluorescent</p> <p>Black Light Intensity Verified Time _____ Serial No. Light Meter <u>A</u> Serial No. Black Light _____</p> <p>Remarks <u>CNM 2201.01-104/4</u> <u>PC C TO PC P1</u></p>
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ANI Review <i>Robert Hill</i>	Date FEB 11 1993	Final QA Review <i>Rm Hill</i>	Date <u>..11-93</u>	Item No. B09.031.006A
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Doc 2/23/93

00701354

DUKE POWER COMPANY								Exam Start: 8:45		FORM NDE UT-2A					
ULTRASONIC EXAMINATION DATA SHEET FOR PLANAR REFLECTORS								Exam Finish: 9:00		Revision: 3					
Station: Catawba			Unit: 2		Component/weld ID: 2NC11-WN7				Date: 2-11-93						
Nominal Material Thickness (in.)			2.3"		Weld Length (in.): 69"		Surface Temperature: 25° C deg F								
Measured Material Thickness (in.)			2.65"		Lo: A		Pyrometer S/N: MCQUA 32848								
Surface Condition: BUFFED					SCANS: 45 <input checked="" type="checkbox"/> 59 dB			Configuration: Branch Connection							
Examiner: <i>A. Bibb</i> Level: II					45T <input checked="" type="checkbox"/> 59 dB 60 <input type="checkbox"/> dB			S1 Flow S2							
Examiner: <i>Lorey Mauldin</i> Level: II					0 <input type="checkbox"/> dB 60T <input type="checkbox"/> dB			PIPE to Branch Connection							
Calibration sheet No: 9302006					Applies only to NDE-620, 640 and 680				Applies to NDE-680 only						
Procedure: NDE 610 Rev: 0 FC:SEE NOTES									Skew angle: N/A						
IND NO.	Max % dac	W Max	L Max	MP Max	L1 20%dac HMA 50%dac	L2 20%dac HMA 50%dac	W1 20%dac HMA 50%dac	W2 20%dac HMA 50%dac	Mp1 20%dac HMA 50%dac	Mp2 20%dac HMA 50%dac	Beam Dir	Exam Surf.	Scan	Damps	
	45°	NO RECORDABLE INDICATIONS													
Remarks: 91-13 91-17 92-02 92-03 92-07 92-14 93-04															
Limitations: see NDE-UT-4								<input checked="" type="checkbox"/> None: <input type="checkbox"/>		sheet 1 of 86					
Reviewed By: <i>W.C. Leaper</i>			Level: II		Date: 2-15-93		Authorized Inspector: <i>Robert M. Hill</i>			Date: FEB 18 1993		Item No: 809.031.005			

WCH 4-9-93
WCH 4/15/93

00701355

DUKE POWER COMPANY

ISI LIMITATION REPORT

FORM NDE-UT-4
Revision 1

Component/Weld ID: 2NC 11-WN7 Item No: B09.031.005

remarks:

NO SCAN SURFACE BEAM DIRECTION

LIMITED SCAN 1 2 1 2 cw ccw

FROM L _____ to L _____ INCHES FROM WO 0.0" to 2.0"

ANGLE: 0 45L 60 other _____ FROM 0 DEG to 360 DEG

Due to Branch Connection weld.

NO SCAN SURFACE BEAM DIRECTION

LIMITED SCAN 1 2 1 2 cw ccw

FROM L _____ to L _____ INCHES FROM WO _____ to _____

ANGLE: 0 45L 60 other _____ FROM 0 DEG to 360 DEG

Not required by ISI Plan

NO SCAN SURFACE BEAM DIRECTION

LIMITED SCAN 1 2 1 2 cw ccw

FROM L _____ to L _____ INCHES FROM WO 28" to 38"

ANGLE: 0 45L 60 other _____ FROM _____ DEG to _____ DEG

Due to Ultrasonic Level Detector and 2.0" nozzle

NO SCAN SURFACE BEAM DIRECTION

LIMITED SCAN 1 2 1 2 cw ccw

FROM L _____ to L _____ INCHES FROM WO _____ to _____

ANGLE: 0 45 60 other _____ FROM _____ DEG to _____ DEG

Sketch(s) attached yes no

Prepared By: Kerry Maudsley Level: H Date: 2-11-93

Sheet 2 of 26

Reviewed By: W.C. Leaper Date: 2-15-93

Authorized Inspector: Robert McMillin Date: FEB 18 1993

Handwritten signature and date:
4/15/93

Station CATAWBA Unit 2 Rev. _____ File No 2NC11-WN7 Sheet 3 Of 6

Subject LIMITED EXAM DATA
4" 5/8 NOZZLE By Larry Macklin Date 2-11-93

Prob No. B09.031.005 Checked By L.C. Lynn Date 2-15-93

DRAWING #1

CROSS SECTIONAL AREA: $.88" \times 3.0" = 2.64 \text{ sq. in.}$

$\times 2 \text{ SCANS}$
5.28 sq. in.

AREA of LOSS:

AXIAL: $2.64 \div 5.28 \times 100 = \underline{50\%}$

CIRC: No Loss

DRAWING #2

CROSS SECTIONAL AREA: $.88" \times 2.45" = 2.156 \text{ sq. in.}$

$\times 2 \text{ SCANS}$
4.312 sq. in.

AREA of LOSS:

AXIAL: $\frac{.20 \times .20}{2} + 2.156 = 2.1875 \text{ sq. in.}$

$2.1875 \div 4.312 \times 100 = 50.724 =$

50.7%

CIRC: 100%

	AXIAL	CIRC
DRAWING 1	50%	0%
DRAWING 2	50.7%	100%
	$\frac{100.7}{2}$	$\frac{100}{2}$

$50.35 + 50 \div 2 = \underline{50.175 = 50.2\% \text{ LOSS}}$

\therefore A 45° L-WAVE WAS USED TO SCAN WELD FROM 1 DIRECTION ONLY. NO SCAN WAS PERFORMED FROM SUR. 2 (NOZZLE SIDE) DUE TO NOZZLE WELD CONFIGURATION.

ATTACHMENT-F

00731356

[Handwritten initials]

ATTACHMENT-F Case No. 11

Station CATARAUGUS Unit 2 Rev. _____ File No. 2NC11-61N7 Sheet 4 Of 6
 Subject LIMITED EXAM DATA
14" 5/8 NOZZLE By LOANY TRAVELLE Date 2-11-95
 Prob No. B09.031.005 Checked By _____ Date _____

ADDITIONAL LOSS DUE TO PERMANENT HANDED: DEC 11/95

6.9" CIRCUMFERENCE WITH 10" LIMITATION THEREFORE:

$$50.2\% \text{ of LOSS FOR } 59" = \frac{59}{69} \times 50.2 = 42.9\%$$

$$10\% \text{ of LOSS FOR } 10" = \frac{10}{69} \times 100 = 14.5\%$$

$$\underline{\hspace{10em}} 57.4\%$$

TOTAL AREA OF LOSS

57.4%

00701357

Page 11 of 11
ATTACHMENT-F

Form 28294 (R5-89)

Form NDE-25A

Revision 1

DUKE POWER COMPANY

PROJECT CATAWBA

MAGNETIC PARTICLE/LIQUID PENETRANT EXAMINATION REPORT

Weld No. 2NC11-WN7 Unit No. 2 Date 2-11-93
Diameter 14.00 Schedule/Thickness 2.300 Type Material SS CS
Work Order No. N/A QA Condition 1

Procedure NDE35A-E / Rev 13
NDE-98 Approved N/A
Radiation Level N/A

SKETCH OF ITEM EXAMINED

Inspector	Level
<i>Kirby L. Whitworth</i>	II

Indication Number	Indication Dimensions Length/Width/Diameter, etc.	Acceptable	Reportable	Reference Documents
NONE				

MT DATA
 MT Method Used
 Fluorescent Nonfluorescent Wet Dry
 MT Unit Serial No. _____
 Particle Batch No. _____
 MT Technique Used: N A
 Circular
 Direct Contact Amp _____
 Central Conductor Amp _____
 MT Field Indicator Used
 Yes No
 Yoke AC DC Prod
 Longitudinal Number Turns in Coil _____
 Amp _____

PT DATA
 PT Batch Number
 Cleaner 91B04K
 Penetrant 78E084
 Developer 92G07K
 Remover N/A
 Fluorescent Nonfluorescent

Black Light Intensity Verified
 Time N/A Date A
 Serial No. Light Meter _____
 Serial No. Black Light _____

Remarks CNM 2201.01-104/4
PC B TO PC P1

ANI Review <i>Robert McMillan</i>	Date FEB 11 1993	Final QA Review <i>Rm S. Lee</i>	Date <u>2-11-93</u>	Item No. <u>B09.031.005A</u>
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*Free
2/23/93*

00730809

**THIS PAGE IS AN
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DWG. NO. CN-1680-23R/3
"DUKE POWER COMPANY
CATAWBA NUCLEAR STATION
UNIT 1 SPIN: RCPCFB"**

Attachment A

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23 R/3**

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D-01

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**"A.S.M.E. SECTION III CLASS 1
BUTT WELDING NOZZLES"
Attachment B**

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**DWG. NO. CN-2680-1 (R/1)
"ADDED AS BUILT DATA"
Attachment C**

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**"A.S.M.E. SECTION III
CLASS 1 BUTT WELDING
NOZZLES"**

Attachment D

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D-04