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Scientific Notebook No. 474: Documentation  
of Numerical Analyses for the Lab-Scale  
Heater Tests (11/06/2001 through 11/16/2001)

# LABORATORY NOTEBOOK

CNWRA/SwRI

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COPY 474

NOTEBOOK NO. \_\_\_\_\_

ISSUED TO Ronald Green

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This notebook is to document numerical analyses of the lab-scale heater tests. The analyses were started in Notebook 209. This is a continuation.

The previous model was mostly re-formulated with smaller elements and greater resolution in the modified version.

The MBTRA Version 1.5 input file as currently appears is attached on 5 disks/home/rgreen ~/1st/21st/1st66.dat

Simulation of laboratory-scale dripping experiment - Bldg 51 CNWRA  
Nov 16, 2001

- : lst66
- : smaller model to fit in metra element dimension limitation
- : This run started with dripl31 converted to DCM
- : dcm-sm98 inc liq sat of matrix from 0.3 to 0.35
- : lst03, repeat of dcm-sm98
- : lst04, new dcm parameters, new bcon, removed top source
- : lst06, added bottom bcon
- : lst08, set areamodf=1e-2
- : lst11, removed bottom bcon
- : lst13, reset bcon q to 1 kg/d= 5.989e-2 kg/m^2/s
- : lst14, set areamodf=1e-4, crashed at 12 days
- : lst15, set areamodf=1e-3
- : lst17, new bottom bc
- : lst18, reset infil rate at e-2 from e-3
- : lst19, set areamodf=1e-1
- : lst22, reset bottom bc to Dirichlet from Neuman
- : lst23, set areamodf=1e-0
- : lst24, set areamodf=1e-4
- : lst26, set bottom bc mat sat 0.20
- : lst27, set bot bc matr sat to 0.1, inc infil, areamodf = 1.0, top bc matr sat=0.65
- : lst28, set areamodf=1e-4
- : lst29, set top to source from bcon, same as from dcm-sm80 et al.
- : lst30, lst29 died at 7.1 days, set volj from 0.05 to 0.002
- : lst32, lst30 died at 198 days, removed bcon at bottom
- : lst33, lst32 died at 5.7 days, reduced Kt at boundaries, revised init sat=dcm-sm80
- : lst34, set areamodf=1.0
- : lst36, modified drift V-G properties
- : lst37, lst36 went 210, set areamodf=1.e-4
- : lst38, lst37 died at 11 days, inc block size from 0.002 to 0.05
- : lst39, sat at base too high, inc vol of bot, dec int sat
- : lst40, areamodf set to 1.0
- : lst41, set bottom int sat to .2
- : lst42, areamodf=1e-4
- : lst43, dec bot int sat to 0.1, inc vol to 5e0
- : lst44, areamodf=1.0
- : lst47, reduced k by 10x to 2e-18
- : lst48, inc k by 100x to 2e-16
- : lst49, inc size of bc to lower edge temp
- : lst50, inc number of elements
- : lst52, reading error in DCMXYZ corrected
- : lst53, reduced size of edge elements
- : lst56, inc size of bc, include drift properties
- : lst57, new set of bc, std mass
- : lst58, doubled heat output
- : lst59, doubled heat output again
- : lst60, dec int sat to 0.35, set bottom bc to 0.1 w/ vol = 1.0e-1
- : lst61, reduced cp on bc, reduced heat to 2X
- : lst62, heat back to 1X
- : lst63, heat back to 4X, all bc to Kt=.05 w/C-m w/ cp=1e4
- : lst64, inc Kt in interior to 0.5/1.0 from 0.4/0.7
- : lst65, changed fract alpha to 1.3e-3 from 1.3e-1
- : lst66, lowered heater by 0.1 to be consistent with exper.

```

RSTART 0
:
: XYZ = 1 table look-up; pref = ref. press.
: RADIAL = 0 correlations; tref = ref. temp.
: OTHER
:
:grid geometry nx ny nz ivplwr iptvcal iout pref tref href
Grid DCMXYZ 24 14 30 1 1 2 0 0 0 0
:
: data taken from sandia report:Green et al. 1995, NUREG/CR-6348
: relative perm and pc
Pckr
: 1 type-curv swirm rpmm(lamda) alpham swext sgc iecm
: 1 Van-Gen 0.05 .3717 6.36e-7 0 0.0 0 ! matrix block
:
: 1 type-curv swirm unused unused p#0-sat sgc iecm
: 2 linear 0.00 0.000 0.00 1.0 0.0 0 ! emplacement drift

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1 type-curv swrim unused unused p0-sat sgc iecm
2 linear 0.01 0.800 1.0e-1 0.0 0.0 0 ! emplacement drift

1 type-curv swrim unused unused p0-sat sgc iecm
3 linear 0.01 0.000 0.00 1.0 0.0 0 ! primary fracture

1 type-curv swrif rpmf(lamda) alphaf swext sgc iecm
4 Van-Gen 0.08 0.7619 1.3e-3 0.0 0.0 0 ! matrix fractures
:blank line

Debug 1
0
Thermal-prop
: no rho cpr ckdry cksat crp crt tau cdiff cexp enbd
1 1.600e+03 840.0 0.50 1.00 0 0 .5 2.13e-5 1.8 0.0 !matrix
2 1.600e+03 840.0 10.0 10.0 0 0 .5 2.13e-5 1.8 0.0 !drift

skip
3 1.600e+03 5.0e+7 0.50 1.00 0 0 .5 2.13e-5 1.8 0.0 !side boundaries
4 1.600e+03 1.0e+9 0.50 1.00 0 0 .5 2.13e-5 1.8 0.0 !bottom boundary
5 1.600e+03 5.0e+7 0.50 1.00 0 0 .5 2.13e-5 1.8 0.0 !top boundary
6 1.600e+03 5.0e+8 1.50 2.00 0 0 .5 2.13e-5 1.8 0.0 !front bc near heater

noskip
3 1.600e+03 840.0 0.50 1.00 0 0 .5 2.13e-5 1.8 0.0 !side boundaries
4 1.600e+03 840.0 0.50 1.00 0 0 .5 2.13e-5 1.8 0.0 !bottom boundary
5 1.600e+03 840.0 0.50 1.00 0 0 .5 2.13e-5 1.8 0.0 !top boundary
6 1.600e+03 840.0 1.50 2.00 0 0 .5 2.13e-5 1.8 0.0 !front bc near heater

noskip
3 1.600e+03 1.0e4 0.05 0.05 0 0 .5 2.13e-5 1.8 0.0 !side boundaries
4 1.600e+03 1.0e4 0.05 0.05 0 0 .5 2.13e-5 1.8 0.0 !bottom boundary
5 1.600e+03 1.0e4 0.05 0.05 0 0 .5 2.13e-5 1.8 0.0 !top boundary
6 1.600e+03 1.0e4 0.05 0.05 0 0 .5 2.13e-5 1.8 0.0 !front bc near heater

0
: igrid rw re
DXYZ 0
: (dx(i),i=1,nx)
0.004 .008 .015 .015 .015 .015 .03 .03 .03 !total for line 0.177
0.03 .03 .03 .03 .03 .03 .03 .03 .03 !total for line 0.3
0.03 .03 .03 .03 .03 .03 .03 .03 .03 !total for line 0.105
:total in x-direction is 0.582 plus .019 beyond edge elements, 24 elements
: (dy(j),j=1,ny)
0.02 .02 .02 .02 .02 .02 .02 .02 .02 !total for line 0.2
0.02 .02 .02 .01 !total for line .07
:total in y-direction is 0.27 plus .03 beyond edge elements, 14 elements
: (dz(k),k=1,nz)
skip
0.03 .06 .06 .06 .06 .06 .06 .04 .02 .02 !total for line 0.51, and 0.54 from top
0.015 .015 .02 .03 .03 .02 .015 .015 .02 !total for line 0.20
0.04 .06 .06 .06 .06 .06 .06 .03 !total for line 0.43 and 0.46 from bottom
noskip
: lowered heater by 0.1
0.03 .06 .06 .06 .06 .06 .06 .04 .04 !total for line 0.53, and 0.56 from top
0.02 .02 .015 .015 .025 .03 .03 .025 .015 .015 !total for line 0.21
0.02 .02 .04 .04 .06 .06 .06 .06 .06 .03 !total for line 0.45 and 0.48 from bottom
:total z-direction is 1.19 plus .06 beyond end elements, 30 elements

PhiK
: i1 i2 j1 j2 k1 k2 ist ithrm vb porf permxf permyf permzf porzn perzm istm ithrmm
1 24 1 14 1 30 4 1 1.0e-2 1.00 1.e-10 1.e-10 0.42 2.e-16 1 1 ! matrix

skip
: following are new bc with more mass to have lower edge temps
1 24 14 14 1 30 4 3 1.0e-2 1.00 1.e-10 1.e-10 0.42 2.e-17 1 3 ! front
24 24 1 14 1 30 4 3 1.0e-2 1.00 1.e-10 1.e-10 0.42 2.e-17 1 3 ! side
1 4 14 14 14 19 4 6 1.0e-2 1.00 1.e-10 1.e-10 0.42 2.e-17 1 6 ! front at heater
1 24 1 14 1 1 4 5 1.0e-2 1.00 1.e-10 1.e-10 0.42 2.e-17 1 5 ! top
1 24 1 14 30 30 4 4 5.0e-0 1.00 1.e-10 1.e-10 0.42 2.e-17 1 4 ! bottom

noskip
: following are new bc with standard mass for edge elements
1 24 14 14 1 30 4 3 0.1 1.00 1.e-10 1.e-10 0.42 2.e-17 1 3 ! front
24 24 1 14 1 30 4 3 0.1 1.00 1.e-10 1.e-10 0.42 2.e-17 1 3 ! side

1 4 14 14 14 19 4 6 0.1 1.00 1.e-10 1.e-10 0.42 2.e-17 1 6 ! front at heater
1 24 1 14 1 1 4 5 0.1 1.00 1.e-10 1.e-10 0.42 2.e-17 1 5 ! top
1 24 1 14 30 30 4 4 1.0e-1 1.00 1.e-10 1.e-10 0.42 2.e-17 1 4 ! bottom

end of bc elements
noskip
1 3 1 14 14 14 2 2 0.1 1.00 1.e-10 1.e-10 0.99 1.e-12 4 2 ! drift
1 5 1 14 15 15 2 2 0.1 1.00 1.e-10 1.e-10 0.99 1.e-12 4 2 ! drift
1 6 1 14 16 16 2 2 0.1 1.00 1.e-10 1.e-10 0.99 1.e-12 4 2 ! drift
1 6 1 14 17 17 2 2 0.1 1.00 1.e-10 1.e-10 0.99 1.e-12 4 2 ! drift
1 5 1 14 18 18 2 2 0.1 1.00 1.e-10 1.e-10 0.99 1.e-12 4 2 ! drift
1 3 1 14 19 19 2 2 0.1 1.00 1.e-10 1.e-10 0.99 1.e-12 4 2 ! drift

noskip
0
Init
: i1 i2 j1 j2 k1 k2 p t sg xg2 pm tm sgm xgm
1 24 1 14 1 30 1.0315e5 20.0 0.65 0. 1.0315e5 20.0 .65 0. ! matrix
1 24 1 14 30 30 1.0315e5 20.0 0.90 0. 1.0315e5 20.0 .90 0. ! bottom

skip
1 3 1 14 14 14 1.0315e5 20.0 0.99 0. 1.0315e5 20.0 .99 0. ! drift
1 5 1 14 15 15 1.0315e5 20.0 0.99 0. 1.0315e5 20.0 .99 0. ! drift
1 6 1 14 16 16 1.0315e5 20.0 0.99 0. 1.0315e5 20.0 .99 0. ! drift
1 6 1 14 17 17 1.0315e5 20.0 0.99 0. 1.0315e5 20.0 .99 0. ! drift
1 5 1 14 18 18 1.0315e5 20.0 0.99 0. 1.0315e5 20.0 .99 0. ! drift
1 3 1 14 19 19 1.0315e5 20.0 0.99 0. 1.0315e5 20.0 .99 0. ! drift

noskip
0
DCMPARA
: i1 i2 j1 j2 k1 k2 wolf areamodf xlm ylm zlm
1 24 1 14 1 30 0.050 1.0 .05 0.03 .05 1.000 ! matrix
0

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Recurrent
: ns fach facm (fach and facm are multipliers)
Source 2 4.00 1.
: this is for the heat source
: is1 is2 js1 js2 ks1 ks2 istyp
1 3 1 3 17 17 33
:0.0 0.0
1.e+4 3.51e+1
1.e+10 3.51e+1
0
: this for the water infiltration
: is1 is2 js1 js2 ks1 ks2 istyp
1 2 1 7 1 1 13
0.0 20.0 0.0
2.60e5 20.0 0.0
3.60e5 20.0 2.894e-6
1.486e7 20.0 2.894e-6
1.815e7 20.0 7.534e-7
1.e+10 20.0 7.534e-7
0
Output C=-10 Q=-10 T=1 G=1 P=1
: isolv newtnm north nitmax level
Solve 4 2 12 4 100
:AUTO-step DPMXE DSMXE DTPMXE DP2MXE TACCCEL IAUTOYF FACI
AUTO-step 5.0E+4 0.03 5.0 1.e4 1.0e-3 0 0
:TOLR TOLP TOLS TOLT TOLP2 TOLM TOLA TOLE rtwtol rmtol smxtol
Tolr 1.5.e-4 5.e-3 1. 1.e-3 1.e-3 1.e-3 1.e-12 1.e-12 1.e-12
:Limit dpmx dsxm dtmpmx dp2mx dtmm dtm icutmx
LIMIT 1.e5 .08 10. 1.e5 1.e-9 .8
: target dt dpmx dsxm dp2mx dtmpmx
: print all at every target time
PLOTS 1 0 4
1 10 451 541

Time[d] 5.
Time[d] 10.
Time[d] 50.
Time[d] 110.
Time[d] 172.
Time[d] 210.
Ends

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The major difference from earlier models of the list is that this model has 24 x 14 x 30 elements for 10,080 total elements, using 2 planes of symmetry (z-plane in 2 orientations) RHH W/16/01

I have reviewed the SW and determined that it complies with QAP-001. To fully understand and replicate the work described herein, the qualified thermohydrologic modeler would need to refer to SW 209.

*Arden Wittmeyer* 9/21/2004

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