From: <eddie.grant@exeloncorp.com>
To: <nvg@nrc.gov>
Date: 10/12/04 12:34PM
Subject: Response to RAI Letter No. 6

Nannette Gilles
Attached is your copy of the response to RAI letter No. 6 that was signed out yesterday.
Note that this version includes the attachments. With the mailed original, the attachments were on a CD-ROM.

Thanks,

Exelon
Early Site Permit Project
Eddie R. Grant
610.765.5001 voice
610.765.5755 fax
850.598.9801 cell

****
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****

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Subject: Response to RAI Letter No. 6
Creation Date: 10/12/04 12:31PM
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Created By: eddie.grant@exeloncorp.com

Recipients
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NVG (Nanette Gilles)

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MESSAGE	1243	10/12/04 12:31PM
TEXT.htm	3907	
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Ltr - 2004-10-11 Kray RAI No 6 Response with Attachments.pdf	4430754	

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Exelon Nuclear
200 Exelon Way
KSA3-N
Kennett Square, PA 19348

Telephone 610.765.5610
Fax 610.765.5755
www.exeloncorp.com

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52.17

October 11, 2004

U.S. Nuclear Regulatory Commission
ATTN: Document Control Desk
Washington, DC 20555

Subject: Response to Request for Additional Information (RAI) Letter No. 6 – Exelon Early Site Permit (ESP) Application for the Clinton ESP Site (TAC No. MC1122)

Re: Letter, U.S. Nuclear Regulatory Commission (N. V. Gilles) to Exelon Generation Company, LLC, (M. Kray), dated July 26, 2004, Request for Additional Information Letter No. 6 – Exelon Early Site Permit Application for the Clinton ESP Site (TAC No. MC1122)

Enclosed, as requested in the referenced letter, are responses to the requests for additional information (RAIs) associated with the hydrology portions of the Exelon Generation Company, LLC (EGC) ESP application. The attachments identified in the responses to specific RAIs are provided on the enclosed CD-ROM.

Please contact Eddie Grant of my staff at 610-765-5001 if you have any questions regarding this submittal.

Sincerely yours,

Marilyn C. Kray

Marilyn C. Kray
Vice President, Project Development

TPM/ERG

cc: U.S. NRC Regional Office (w/ enclosures)
Ms. Nanette V. Gilles (w/ enclosures)

Enclosure: Response to RAI 2.4.1-1 through 2.4.1-5 (and associated attachments)
Response to RAI 2.4.2-1 through 2.4.2-5
Response to RAI 2.4.3-1 through 2.4.3-2
Response to RAI 2.4.7-1 through 2.4.7-8
Response to RAI 2.4.8-1 through 2.4.8-4
Response to RAI 2.4.9-1
Response to RAI 2.4.10-1
Response to RAI 2.4.12-1
Response to RAI 2.4.13-1
Response to RAI 3.2.2-1 through 3.2.2-2 (and associated attachments)

Attachments: (Note – These are provided on the enclosed CD-ROM.)
RAI 2.4.1-1 Attachment (Revised Figure 1.2-4)
RAI 3.2.2-1 Attachment (New Figure 3.2-1)
RAI 2.4.1-5 Attachment 1 (MRCC 2002a)
RAI 2.4.1-5 Attachment 2 (MRCC 2002b)

AFFIDAVIT OF MARILYN C. KRAY

State of Pennsylvania

County of Chester

The foregoing document was acknowledged before me, in and for the County and State aforesaid, by Marilyn C. Kray, who is Vice President, Project Development, of Exelon Generation Company, LLC. She has affirmed before me that she is duly authorized to execute and file the foregoing document on behalf of Exelon Generation Company, LLC, and that the statements in the document are true to the best of her knowledge and belief.

Acknowledged and affirmed before me this 11th day of October, 2004.

My commission expires 10-6-07.

Vivia V. Gallimore

Notary Public

COMMONWEALTH OF PENNSYLVANIA
Notarial Seal
Vivia V. Gallimore, Notary Public
Kennett Square Boro, Chester County
My Commission Expires Oct. 6, 2007
Member, Pennsylvania Association Of Notaries

NRC Letter Dated: 07/26/2004

NRC RAI No. 2.4.1-1

Please provide survey coordinates (including elevations) for the bounding areas of all ESP safety-related structures including intake tunnels and piping corridors. Also provide the coordinates of existing aquifers in the bounding areas, particularly perched aquifers.

EGC RAI ID: R9-1

EGC RESPONSE:

SSAR Chapter 1, Figure 1.2-4, has been revised (see RAI 2.4.1-1 Attachment) to show the approximate location of safety-related structures, with a grid system provided on the figure, for the EGC ESP. The safety related structures are the intake structure, the essential service water cooling towers, and some of the structures that would be located within the power block area. The final size of the safety-related structures and locations will be determined after the selection of a reactor for the construction phase. No specific survey coordinates are established during the ESP process.

The location of the EGC ESP intake structure at approximately 65 feet south of the CPS intake structure was selected to provide a location where the ESP piping can be routed without disturbing the CPS shutdown cooling water piping to and from the CPS ultimate heat sink (UHS). The piping for CPS exits the intake structure on the side away from the lake (east side). The CPS nonsafety service water discharge and the fire protection discharge exit near the north end and turn north east at a 45º angle. The circulating water (CW) discharge piping is the next piping exiting the intake structure as three pipes and combining into a common pipe. The CPS CW pipe exits south of the service water pipe and north of the E-W centerline of the intake structure before turning north east at a 45º angle to the turbine building. South of the CPS CW piping is CW piping that was installed for the canceled CPS Unit 2 and also follows the northeast route of the CPS unit CW piping. The last piping exiting the intake structure and near the south end of the CPS intake structure is the shutdown service water piping which turns south east at 45º after leaving the intake structure and continues for approximately 250 ft before turning east and then north to the CPS diesel generator and HVAC building. Two trains of shutdown service water plus a fire protection line follow this path. The shutdown service water return lines follow the same routing as the supply lines and are located above the supply lines to a point approximately 175 ft east of where the supply lines turned east. The discharge lines turn 45º southwest at this point and slope downward to a discharge to the CPS UHS pond with the bottom of the discharge pipes at elevation 675 ft.

The piping from the EGC ESP facility intake structure will be routed similar to the CPS piping with an expected horizontal distance of about fifty feet maintained between the ESP facility piping and the CPS piping. The ESP facility piping will be south of the CPS piping and will be routed sufficiently south before turning east to provide adequate clearance and cover where it passes over the sloping CPS discharge piping to the CPS UHS pond. The ESP facility piping elevation will be selected to provide 3 ft – 9 in clearance (vertical distance) between the ESP and CPS pipes where they cross. After crossing over the CPS discharge piping, the ESP facility piping will continue generally in an east direction to reach the two cooling tower areas where it provides make-up. The physical location and elevation of the ESP facility piping will not be established until after the required diameters are determined based on the selection of a reactor type. The ESP facility piping exiting its intake structure will include the make-up supply to the

normal heat sink tower, fire protection supply and two trains of make-up to the Ultimate Heat Sink cooling towers if the selected reactor type does not use passive systems for safety related cooling.

The discussion of the regional and local groundwater system is presented in SSAR 2.4.13. Groundwater beneath the ESP site occurs in the upper glacial deposits (Wisconsinan) and in the underlying Illinoian and Kansan tills. Because the Wisconsinan, Illinoian, and Kansan deposits are regional and not limited to any specific area within the ESP site, there are no specific coordinates for the aquifers. The depths to elevations of the different hydrogeologic units and the measured water levels based on the borings and piezometers recently installed within the footprint of the ESP are summarized below.

Hydrogeologic Unit	Top of Unit		Water Surface	
	Depth (ft)	Elevation (ft)	Depth (ft)	Elevation (ft)
Wisconsinan	8 to 13	724.2 to 726.1	3.7 to 6.5	733.5 to 727.5
Illinoian	58	679.8	27.8 to 27.3	710.8 to 711.3
Kansan	189	548.2	Not measured	Not measured

Additional geological cross sections through the EGC ESP site are provided in SSAR Appendix A-Geotechnical Report (see Figures 2-1 and 5-2).

Section 3.2.2.3 of the SSAR will be revised to provide additional information on the location of structures.

ASSOCIATED EGC ESP APPLICATION REVISIONS:

Revise SSAR, Chapter 3, Section 3.2.2.3, to include the following new paragraph as the second paragraph in Section 3.2.2.3:.

The location of the EGC ESP intake structure at approximately 65 feet south of the CPS intake structure was selected to provide a location where the ESP piping can be routed without disturbing the CPS shutdown cooling water piping to and from the CPS UHS.

Revise SSAR, Chapter 1, Figure 1.2-4 as shown in RAI 2.4.1-1 Attachment 1.

ATTACHMENTS:

RAI 2.4.1-1 Attachment (Revised Figure 1.2-4)

NRC Letter Dated: 07/26/2004

NRC RAI No. 2.4.1-2

Please identify any limits on plant operation due to either water supply or intake water temperature for the ESP unit (e.g., need to derate or shutdown reactors if the intake temperature exceeds a certain threshold). Estimate the frequency and duration of the applicability of these operating limits.

EGC RAI ID: R9-2

EGC RESPONSE:

Limits on plant operation due to water level and temperature are typically based on the volume and temperature of the ultimate heat sink (as assumed in the safe shutdown analyses). Since the design of the station has not yet been finalized and the safe shutdown analyses have not been performed, no such operating limits have been identified. These analyses would be expected to be performed as part of the design certification or combined license applications.

SSAR Section 2.4.11.5 indicates a plant shutdown would be initiated if the level in Clinton Lake drops to elevation 677 ft. However, this elevation is not based on any safety analysis or the ultimate heat sink volume. This is the highest minimum level for continued power generation, i.e., the normal cooling water source, and is based on a not yet finalized design of the intake structure (which could be designed to operate with lower water levels). Simulation of lake water levels over the 24 years of meteorological records since construction of the Clinton Lake Dam have shown water levels well within the minimum lake operating levels with both the existing CPS and proposed ESP facility in operation at 100 percent power. The lake drawdown analysis presented in SSAR section 2.4.11.3 demonstrates that elevation 677 ft is not reached during a 100-year drought (elevation 681.4 ft above msl).

Thermal modeling has indicated that essentially all of the water temperature increase due to plant operation for CPS is dissipated before the water is circulated to the plant intake (Edinger, 1989). Intake temperatures are more directly influenced by ambient weather conditions. The temperature of the water taken from Clinton Lake for make-up to the cooling towers is a small fraction of the total flow through the cooling towers and has minor impact on the cooling towers basin cold water temperature. The ESP facility will have the capability to add the cooling tower make-up water to the inlet side of the cooling towers and therefore it can be cooled to the design temperature. Therefore, no unit derating or shutdown will occur due to make-up (intake) water temperatures. Also, as with the volume/level, no safety analysis for safe shutdown has been performed, and therefore, no assumptions of maximum water temperature have been made for the safety analysis.

ASSOCIATED EGC ESP APPLICATION REVISIONS:

None

ATTACHMENTS:

None

NRC Letter Dated: 07/26/2004

NRC RAI No. 2.4.1-3

The application states that no dams exist upstream of Clinton Lake that could affect the availability of water to the ESP site. Please provide references that confirm this assertion and that no future dams upstream of the site are currently proposed.

EGC RAI ID: R9-3

EGC RESPONSE:

SSAR, Chapter 2, Section 2.4.1.2 will be revised to add information regarding dams upstream and downstream of Clinton Lake that supports the statement that the dams could not affect the availability of water at the ESP site.

With regard to future dams, a representative of the Illinois Department of Natural Resources, Office of Water, Division of Water Resources Management, Dam Safety Section advised that there are no recent or pending permits for recreational or water supply dams upstream of Clinton Lake.

ASSOCIATED EGC ESP APPLICATION REVISIONS:

Revise SSAR, Chapter 2, Section 2.4.1.2 from:

There are currently no existing reservoirs or dams upstream or downstream from Clinton Lake that could affect the availability of water to Clinton Lake (CPS, 1982).

To read:

There are currently no existing reservoirs or dams upstream or downstream from Clinton Lake that could affect the availability of water to Clinton Lake (CPS, 1982). Four recreational dams were identified, two on the North Fork of Salt Creek upstream of Clinton Lake and two downstream of Clinton Lake (USACOE, 2004). The information on these four dams is provided in Table 2.4-1A. Because these dams were constructed for the recreational purposes and have limited storage capacities, water is not withdrawn from the watershed.

Salt Creek (downstream of Clinton Lake) is not a likely candidate for changes that would result in additional demand since the flow of the creek is often low for long periods of time.

Revise SSAR, Chapter 2, Section 2.4, to add new Table 2.4-1a:

TABLE 2.4-1A

Dams Upstream and Downstream of Clinton Lake

Dam Name	Location	Owner/ Purpose	Date Built	Dam Height	Storage and Drainage Area
Moraine View Dam (or Dawson Lake)	Near the city of Leroy in McLean County (about 25 miles upstream of Clinton Lake)	Illinois DNR/ Recreation	1963	42 ft	Storage (acre-feet): Maximum = 4,133 Normal = 1,620 Drainage area: 4.5 acres
Vance Lake Dam (or Clyde Vance Lake)	DeWitt County (about 15 miles upstream of Clinton Lake)	John M. Clark/ Recreation	1955	20 ft	Storage (acre-feet): Maximum = 313 Normal = 134 Drainage area: not provided
Weldon Springs State Park Lake Dam	DeWitt County (about 2.5 miles downstream of Clinton Lake)	Illinois DNR/ Recreation	1900	30	Storage (acre-feet): Maximum = 532 Normal = 303 Drainage area: 1.4 acres
Little Galilee Lake Dam	DeWitt County (about 10 miles down stream of Clinton Lake)	Little Galilee Christian	1954	35	Storage (acre-feet): Maximum = 60 Normal = 41 Drainage area: not provided

Source: USACOE, 2004

Revise SSAR, Chapter 2, Section 2.4 References to add the following new reference:

U.S. Army Corps of Engineers (USACOE). National Inventory of Dams (NIOD). Available at: http://crunch.tec.army.mil/nid/webpages/nid.cfm. September 2004.

ATTACHMENTS:

None

NRC Letter Dated: 07/26/2004

NRC RAI No. 2.4.1-4

Please provide any information regarding proposed land use changes that might result in increased bed load in the tributaries upstream of Clinton Lake or sediment deposition in the ultimate heat sink (UHS).

EGC RAI ID: R9-4

EGC RESPONSE:

EGC has no information regarding proposed land use changes upstream of Clinton Lake. Current land use upstream of Clinton Lake and the CPS ultimate heat sink is mainly agricultural. The agricultural use, especially in early spring when the soils are exposed from farming and the fields have not yet been planted results in the maximum expected sediment load to the tributaries. Future development will tend to create a more impervious watershed and decrease the amount of soil erosion and sediment carried to the tributaries.

ASSOCIATED EGC ESP APPLICATION REVISIONS:

None

ATTACHMENTS:

None

NRC Letter Dated: 07/26/2004

NRC RAI No. 2.4.1-5

Table 2.4-2 shows the percentage of rainfall as runoff and mean lake evaporation. Please provide copies of the references for these estimates.

EGC RAI ID: R9-5

EGC RESPONSE:

SSAR Chapter 2, Table 2.4-2, shows the percentages of rainfall and mean lake evaporation. A copy of each of the following references is included as an attachment to this RAI response:

Midwest Regional Climate Center (MRCC). Database File of Evaporation Data 1963-2002. August 12, 2002a.

Midwest Regional Climate Center (MRCC). Database File of Rainfall Data 1910-2002. August 12, 2002b.

ASSOCIATED EGC ESP APPLICATION REVISIONS:

None

ATTACHMENTS:

RAI 2.4.1-5 Attachment 1 (MRCC 2002a)

RAI 2.4.1-5 Attachment 2 (MRCC 2002b)

NRC Letter Dated: 07/26/2004

NRC RAI No. 2.4.2-1

The Probable Maximum Precipitation (PMP) for Clinton Dam was obtained using Hydrometeorological Report No. 33 (HMR 33); however, the current standards are American National Standards Institute/American Nuclear Society (ANSI/ANS)-2.8-1992, HMR 51, and HMR 52. Please explain why the current standards were not used. Also, please explain why an estimate based on HMR 33 is conservative relative to an estimate based on HMR 51 and HMR 52.

EGC RAI ID: R9-6

EGC RESPONSE:

The 48-hour probable maximum precipitation (PMP) referred to in SSAR, Chapter 2, Section 2.4.2.3, "Effects of Local Intense Precipitation," and Section 2.4.3.1, "Probable Maximum Precipitation," was taken directly from the CPS USAR (CPS, 2002). The PMP information in the CPS USAR was originally obtained or derived from U.S. Weather Bureau Hydrometeorological Report No. 33 (HMR-33). As indicated in the RAI, more recent procedures than those provided in HMR-33 for determining maximum precipitation (PMP) are available. In order to update the PMP information presented in the SSAR, four reports were reviewed which relate directly to estimating PMP at a given location. A brief description of each report and their purpose and objectives is provided below:

HMR-33: Hydrometeorological Report No. 33 "Seasonal Variation of the Probable Maximum Precipitation East of the 105th Meridian for Areas from 10 to 1000 Square Miles and Durations of 6, 12, 24, and 48 Hours" (Reidel, Appleby, and Schloemer, April 1956). This document provides a generalized set of charts indicating monthly and seasonal variations of the 24-hour PMP for a 200 square mile area. The report also provides a method for estimating the PMP for areas ranging from 10 to 1000 square miles, and for durations of 6 to 48 hours.

HMR-51: Hydrometeorological Report No. 51 "Probable Maximum Precipitation Estimates, United States East of the 105th Meridian" (Schreiner and Reidel, June 1978.) This report provides an update to HMR-33; with all-season PMP's for 6, 12, 24, 48, and 72 hours and for 10, 200, 1000, 5000, 10,000, and 20,000 square miles.

HMR-52: Hydrometeorological Report No. 52 "Application of Probable Maximum Precipitation Estimates - United States East of the 105th Meridian" (National Weather Service, August 1982.) This report provides a methodology to determine the temporal and spatial distribution of PMP estimates derived from HMR-51 for situations where this information is needed for a specific drainage.

HMR-53: Hydrometeorological Report No. 53 "Seasonal Variation of 10-Square-Mile Probable Maximum Precipitation Estimates, United States East of the 105th Meridian". (National Weather Service, April 1980.) This report provides seasonal variations of PMP estimates for 10 square mile areas for duration's of 6, 24, and 72 hours. All-season estimates of PMP in HMR-51 were assumed to represent upper bounds of PMP for the results presented in this report. Because the all-season values of HMR-51 were found to differ from those of HMR-33, the seasonal results in this report were intended to supersede the seasonal results in HMR-33.

The 48-hour all-season PMP referenced in the SSAR is 25.2 inches (SSAR Table 2.4-8) and is assumed to be uniformly distributed over the entire 296 mi^2 drainage area. The corresponding 24-hour all-season PMP for the same area (SSAR Table 2.4-8) is 22.6 inches, and the 24-hour all-season PMP for a 200 mi^2 area is 24.0 inches (SSAR Table 2.4-5). The PMP for the 296 mi^2 area was based on the use of a scaling factor "F" of 0.94 obtained from HMR-33 (i.e., $PMP_{296} = PMP_{200} \times F$). A review of the more recent HMR-51, -52, and -53 publications indicates that the 24-hour PMP for a 200 mi^2 area is 25.0 inches (HMR-51) and the 48-hour PMP for a 200 mi^2 area is 28.0 inches (HMR-51). Using the HMR-33 scaling factor of 0.94 to convert from 200 to 296 mi^2, the 24- and 48-hour PMP estimates for the 296 mi^2 Salt Creek Drainage Basin would be approximately 23.5 and 26.3 inches, respectively.

A summary of this information is as follows:

Period (hr)	Area (mi^2)	Source	PMP (in.)	Factor "F"[1]
24	200	HMR-33 (Figure 1) USAR Table 2.4-5	24.0	
24	296	HMR-33 PMP x F USAR Table 2.4-8	22.6	0.94
24	200	HMR-51 (Figure 25)	25.0	
24	296	HMR-51 PMP x F	23.5	0.94
48	296	HMR-33 (Figure 2) USAR Table 2.4-8	25.2	
48	200	HMR-51 (Figure 26)	28.0	
48	296	HMR-51 PMP x F	26.3	0.94

[1] Factor "F" (obtained from USAR and HMR-33, Figure 2) is used to determine PMP for 296 mi^2 area (i.e., $PMP_{296} = PMP_{200} \times F$)

Based on the information provided and discussed above, the 24- and 48-hour PMP estimates derived from the information contained in the more recent HMR publications are approximately 4 percent greater than those predicted by the previous HMR-33 report and summarized in the CPS USAR. The increase in the 48-hour PMP from 25.2 to 26.3 was evaluated to estimate the associated increase in the PMF and potential hazard to the plant site. A mass balance approach was used by estimating the increased volume of rainfall over the lake watershed and associated runoff. The runoff is added to the lake at previously calculated PMF levels (Elevation 809.9) to determine changes in lake discharge and lake level.

Assuming a 1.1-inch increase in the 48-hour PMP and an estimated 29.8 percent runoff to rainfall ratio (measured value from measured rainfall and runoff at the USGS Rowell Gauging Station, Table 2.3-2 of the EGC ESP Environmental Report) there is an estimated 0.1-inch increase in the lake water surface elevation. This increase includes consideration for a nominal increased discharge (1,300 cfs) at the dam due to the higher water surface elevation over the 48-hour period of the PMP. The change in lake level is not considered a hazard to the plant site because there is still 20 plus feet of elevation difference between the high lake level and the plant site.

Table 1.4-1, Item 1.2.2 and Sections 2.4.3.1 and 2.4.2.2 of the SSAR will be revised to provide additional information on the use of procedures HMR-51, HMR-52 and HMR-53 on the calculated PMP and PMF values.

ASSOCIATED EGC ESP APPLICATION REVISIONS:

Revise SSAR, Chapter 2, Section 2.4.3.1, third paragraph, from:

The maximum potential snow accumulation was studied and estimated to correspond to a weight of 35 psf, which would be attributable to the 100 yr snowpack of 22 psf (ASCE, 2000) plus the snow accumulated from the…

To read (add new paragraph to section 2.4.3.1 & change third paragraph, first sentence (35 to 40))

The 48 hour PMP of 25.2 inches developed above was based on methods described in Hydrometeorological Report No. 33. More recent procedures for developing PMP values are presented in Hydrometeorological Report No. 51 (USDOC, 1978), Hydrometeorological Report No. 52 (USWB, 1982) and Hydrometeorological Report No. 53 (USNRC, 1980). The use of these later procedures results in a calculated PMP of 26.3 inches, which is an increase of 1.1 inches, or 4 percent, compared to the 25.2 inches using the previous method. Subsequent analyses of the potential effects of the PMP on other ESP site characteristics (including probable maximum flood (PMF)) have indicated that this increase is essentially insignificant.

The maximum potential snow accumulation was studied and estimated to correspond to a weight of 40 psf, which would be attributable to the 100 yr snowpack of 22 psf (ASCE, 2000) plus the snow accumulated from the…

Revise SSAR, Chapter 2, Section 2.4.2.2, from:

At the dam site, the PMF water surface elevation in the Clinton Lake is 708.8 ft above msl. The top of the dam is at an elevation of 711.8 ft above msl. A minimum freeboard of 3 ft from the PMF water level was provided in order to determine the elevation at the top of the dam. This provides for protection against overtopping of the dam by the PMF and wave action. The maximum wave run-up elevation at the dam, due to sustained 40 mph wind acting on the PMF water level, is 711 ft above msl.

To read:

At the dam site, the PMF water surface elevation in the Clinton Lake is 708.8 ft above msl using the 48-hr duration CPS PMP value of 25.2 inches. As noted in SSAR section 2.4.3.1 use of more recent procedures to estimate PMP results in an increase of 1.1 inches for the 48-hr ESP PMP (total of 26.3 inches). Use of this value would result in an increase of the PMF water surface elevation of Clinton Lake to 708.9 ft above msl, which represents a negligible increase compared to the previous estimate of 708.8 ft msl. The top of the dam is at an elevation of 711.8 ft above msl which provides a freeboard of approximately 3 ft from the PMF water level. This provides for protection against overtopping of the dam by the PMF and wave action. The wave run-up elevation due to sustained wind acting on the PMF water level is discussed in Sections 2.4.3.6 and 2.4.10.

Revise SSAR, Chapter 2, Section 2.4 References, to include the following two new references:

U. S. Department of Commerce (USDOC) and U.S Army Corp of Engineers (USACOE). L.C. Schreiner and J.T. Reidel. Probable Maximum Precipitation Estimates, United States East of the 105th Meridian. Hydrometeorological Report No. 51. June 1978.

U.S. Nuclear Regulatory Commission (USNRC). NUREG/CR-1486. Seasonal Variation of 10-Square-Mile Probable Maximum Precipitation Estimates, United States East of the 105th Meridian. Hydrometeorological Report No. 53. April 1980.

Revise SSAR, Chapter 1, Table 1.4-1, Item 1.2.2, from:

1.2.2 Snow Load 35 lb/ft2

To read:

1.2.2 Snow Load 40 lb/ft2

ATTACHMENTS:

None

NRC Letter Dated: 07/26/2004

NRC RAI No. 2.4.2-2

Please provide a description of likely changes to both upstream land use and downstream water demand that would alter either the intensity or frequency of flood risk and low-flow conditions.

EGC RAI ID: R9-7

EGC RESPONSE:

A shift in upstream land use to a more impervious watershed (with development) will tend to deliver more precipitation as runoff to Clinton Lake. This will also tend to decrease the duration of low flows because more water will be routed through the lake. No change is expected in the 100-year flood levels because of the large flow attenuation capacity of the lake.

Salt Creek (downstream of Clinton Lake) is not a likely candidate for changes that would result in additional demand since the flow of the creek is often low for long periods of time.

ASSOCIATED EGC ESP APPLICATION REVISIONS:

Revisions to SSAR, Chapter 2, Section 2.4.1.2, are provided in the response to RAI 2.4.1-3

ATTACHMENTS:

None

NRC Letter Dated: 07/26/2004

NRC RAI No. 2.4.2-3

Please document any historical hill slope failures in the watershed. Also, please analyze the ability of a hypothetical hillslope failure to impact the plant. What would be the maximum terminal height of such a hypothetical wave?

EGC RAI ID: R9-8

EGC RESPONSE:

As discussed in SSAR, Appendix A, Section 5.1.3.5, there are no landslides documented for DeWitt County, and the landslide potential on the ISGS map is low. Although SSAR, Appendix A, Section 5.1.3.5 also indicates that the slopes near the EGC ESP Site associated with Clinton Lake have been very stable for the past 30 years, and do not pose a landslide hazard, the effects of a hypothetical hill slope failure and the maximum generated wave height have been postulated and estimated at 0.4 ft. SSAR Section 2.4.6 will be revised to provide this additional information.

ASSOCIATED EGC ESP APPLICATION REVISIONS:

Revise SSAR, Chapter 2, Section 2.4.6, from:

The site will not be subjected to the effects of tsunami flooding because the site is not adjacent to a coastal area (CPS, 2002).

To read:

The site will not be subjected to the effects of tsunami flooding because the site is not adjacent to a coastal area (CPS, 2002). However, the impacts to the plant were determined for a lake tsunami generated from hypothetical hillside slope failures. The tsunami analysis was performed using very conservative assumptions that yielded a maximum tsunami wave height estimated to be 0.4-foot. The relatively small landslide velocity, slope angle, and thickness of the landslide contribute to the minimal creation of waves in Clinton Lake. Based on this analysis, it is concluded that landslide-induced tsunamis do not pose a risk to the EGC ESP site.

ATTACHMENTS:

None

NRC Letter Dated: 07/26/2004

NRC RAI No. 2.4.2-4

Please document any seismically-induced seiches in Clinton Lake.

EGC RAI ID: R9-9

EGC RESPONSE:

A search of existing literature was performed to determine if any seismically induced seiches have occurred in Clinton Lake or any other lake in the area. The occurrence of seiches and other seismic wave activity are extremely rare in the non-coastal Midwest; subsequently no seismically-induced seiche information was identified. Additionally, CPS personnel did not report any seiches in Clinton Lake during the June 2004, magnitude 4.5 earthquake.

ASSOCIATED EGC ESP APPLICATION REVISIONS:

None

ATTACHMENTS:

None

NRC Letter Dated: 07/26/2004

NRC RAI No. 2.4.2-5

Please demonstrate that the drainage capacity at the existing grade is sufficient to accommodate local intense precipitation. If the capacity is not sufficient, please describe any active safety-related drainage systems that will be installed for the new units.

EGC RAI ID: R9-10

EGC RESPONSE:

The proposed plant site generally drains to the southeast with no significant internally drained areas for storm water to accumulate during local intense precipitation. The proposed ESP plant buildings and site drainage components will generally direct drainage in the same direction and will be designed so that no building or critical plant facility will be inundated by local intense precipitation. Examples of drainage features that may be incorporated, as necessary, include raised building entrance points, surface drains, subsurface drainage pipes, and surface drainage channels to Clinton Lake.

The site drainage for the ESP facility is not designed at this time since portions of the system will be dependent upon the reactor selected. The nominal grade elevation of 735 ft provides over 20 ft of elevation difference for drainage based on the maximum flood elevation for Clinton Lake. This is a large enough elevation difference to allow designing a drainage system to handle maximum site precipitation without requiring any active components.

ASSOCIATED EGC ESP APPLICATION REVISIONS:

None

ATTACHMENTS:

None

NRC Letter Dated: 07/26/2004

NRC RAI No. 2.4.3-1

Please describe the status of the U.S. Army Corps of Engineers SPRAT computer program referenced in Section 2.4.3.3 and any software quality assurance measures that were used to augment use of this software in support of the ESP application.

EGC RAI ID: R9-11

EGC RESPONSE:

A significant portion of the CPS Dam design included preparation of a discharge rating curve. Discharge rates at various lake levels are established based on dam, lake and watershed hydrologic characteristics. The dam designer used the SPRAT model as the design tool and to prepare the current discharge rating curve for the dam. The ESP facility does not require that the discharge rating curve for the dam be revised, and therefore does not require use of the SPRAT model.

SSAR Section 2.4.3 will be revised to indicate that the hydraulic modeling, i.e., SPRAT and Water Surface Profiles were performed as part of the dam design and not part of the ESP Application.

ASSOCIATED EGC ESP APPLICATION REVISIONS:

Revise SSAR, Chapter 2, Section 2.4.3, paragraphs 2 and 3, from:

The floodwater surface elevations in the lake were determined by routing the floods through the lake using the Spillway Rating and Flood Routing (SPRAT) computer program (USACOE, 1966a). The 100 yr flood level in the lake at the dam site is at an elevation of 697 ft. The routed peak outflow through the service spillway is 11,610 cfs. Based on the flood frequency analysis, the 100 yr flood flow at the dam site, based on records before the dam was built (that is, before November 1977), was estimated to be 26,400 cfs. As shown by the analysis of the post-dam, however, the attenuation effect of the lake will reduce the expected magnitude of the flood flows downstream from the dam. The PMF level with an antecedent standard project flood is at an elevation of 708.8 ft above msl at the dam and 708.9 ft above msl at the plant sites.

The flooding effects on the headwater area of the cooling lake were determined by backwater computations using the computer program, "Water Surface Profiles" (USACOE, 1968). Figure 2.4-7 and Figure 2.4-8 depict the water surface profiles of the 100 yr flood and the PMF under natural conditions for Salt Creek and the North Fork of Salt Creek, respectively. The Illinois Central Railroad depicted on Figure 2.4-8 was procured by the Canadian National Railroad.

To read:

The floodwater surface elevations in the lake were determined during the design of the dam for CPS by routing the floods through the lake using the USACOE's Spillway Rating and Flood Routing (SPRAT) computer program (CPS, 2002). The results of the CPS modeling indicated that the 100 yr flood level in the lake at the dam site is at an elevation of 697 ft. The routed peak outflow through the service spillway is 11,610 cfs. Based on

the flood frequency analysis, the 100 yr flood flow at the dam site (based on records before the dam was built, i.e., before November 1977), was estimated to be 26,400 cfs. As shown by the analysis of the post-dam, however, the attenuation effect of the lake will reduce the expected magnitude of the flood flows downstream from the dam. The PMF level with an antecedent standard project flood is at an elevation of 708.8 ft above msl at the dam and 708.9 ft above msl at the plant sites (CPS, 2002).

The flooding effects on the headwater area of the cooling lake were also evaluated during the dam design and were determined by backwater computations using the USACOE's computer program, "Water Surface Profiles" (CPS, 2002). Figure 2.4-7 and Figure 2.4-8 depict the water surface profiles of the 100 yr flood and the PMF under natural conditions for Salt Creek and the North Fork of Salt Creek, respectively. The Illinois Central Railroad depicted on Figure 2.4-8 was procured by the Canadian National Railroad.

ATTACHMENTS:

None

NRC Letter Dated: 07/26/2004

NRC RAI No. 2.4.3-2

Please explain how the wave runup calculations were bounded through the examination of the Combined Events Criteria indicated in the ANS 2.8 1992 Standard. Discuss coincident wave calculation and the basis for applying a 40 miles per hour (mph) design wind.

EGC RAI ID: R9-12

EGC RESPONSE:

The maximum wave run-up elevation at the dam and the CPS site, due to a sustained 40 mph overland wind speed acting on the PMF water level, was previously estimated to be 711 ft above mean sea level (CPS USAR Section 2.4.2.2, "Flood Design Considerations"). Additionally, CPS USAR Section 2.4.10, "Flooding Protection Requirements," considered a 48 mph overland wind speed coincident with the PMF pool in the design of the circulating water screen house at CPS. The use of these values in the USAR did not result in any safety related issues for the CPS station site since the site was determined to be 22.2 feet above the calculated wave run-up level and 27.1 feet above the calculated PMF level, with the conclusion that the CPS plant facility could not flood under any circumstances.

The ESP Facility Site is considered to be a "dry site", consistent with Condition 3 of Attachment 2, Section 2.4.3 of NRC's RS-002 Review Standard, and will not be susceptible to flooding under any circumstances. Furthermore, the operation of the ESP Facility will not impact the potential for flooding at the existing dam or the plant site. Therefore, the use of *any* wind speed for the purpose of calculating wave run-up effects on PMF levels should be inconsequential. The use of the 40 mph wind speed was retained in the ESP SSAR wave run-up analysis to be consistent with what was originally prepared for the CPS SAR and what is currently relied upon in the CPS USAR. A review of more recent information published by the American Nuclear Society (ANSI/ANS-2.8-1992, "Determining Design Basis Flooding at Power Reactor Sites") has in fact indicated that a wind speed of somewhat greater magnitude may be appropriate for design considerations when estimating the impact of wind speeds on flooding. Figure 1 from the 1992 ANS publication, "Isotach 0.50 Quantiles (in miles per hour): Annual Extreme-Mile, 30 ft Above Ground, 2-yr Mean Recurrence Interval," indicates that a wind speed of 52 mph may be more appropriate for calculating wave run-up height coincident with the PMF pool height.

Screening analyses to conservatively estimate the impact of a 52 mph wind speed on wave run-up calculations have been performed, primarily to determine the incremental impact on the PMF attributable to the increase in wind speed as compared to the original wind speed of 40 mph. New coincident wave heights have been established based on the 52 mph coincident wind speed as 3.81 feet (or 0.94 feet over 40 mph wind wave height) for the significant waves and 6.39 feet (or 1.58 feet over the 40 mph wind wave height) for maximum waves. Wave height increases are not considered significant in terms of the 20 plus feet of elevation between the PMF and the plant site.

SSAR Sections 2.4.3.6 and 2.4.10 were revised to provide additional information on wave run-up, including revisions identified in the response to RAI 2.4.10-1.

ASSOCIATED EGC ESP APPLICATION REVISIONS:

Revise SSAR, Chapter 2, Section 2.4.3.6, from:

The maximum runup elevation at the dam for significant waves was calculated by superimposing the significant wave effects of a coincident 40 mph wind on the probable maximum flood water level at the dam site. The calculations are based on an effective fetch of 0.9 mi, a windtide fetch of 4 mi, a water depth of 58 ft, and an upstream slope of the dam of 3:1 (horizontal to vertical) with riprap. The wave runup obtained is 2.2 ft, resulting in a significant wave runup elevation of 711.0 ft above msl at the dam site. The top of dam is at elevation 711.8 ft above msl.

To read:

Using the same assumptions regarding fetch, water depth, and shore slope, and assuming non-breaking waves, the wave runup was recalculated with an increased wind velocity from 40 mph to 52 mph (ANSI, 1992). This coincident wind velocity increase showed an increase in the significant (33.3% probability) wave runup to 3.81 feet. Similarly for the maximum (1% probability) wave runup, the runup value increased to 6.39 feet. Superimposing the wave runup values on the probable maximum flood level at the plant (station) site resulted in a wave runup elevation of 712.8 feet for significant waves and elevation of 715.4 feet for the maximum (1%) waves. Both elevations are significantly below the approximate grade elevation of 735 feet above msl.

Revise SSAR, Chapter 2, Section 2.4.10, from:

The maximum (1 percent) wave runup elevation at the station site is 713.8 ft above msl, produced by a sustained 40 mph overland wind acting on the PMF still water elevation of 708.9 ft above msl. The approximate grade elevation for the EGC ESP Facility of 735 ft above msl is approximately 21 ft above the maximum wave runup level and 26 ft above the PMF water level. The safety-related facilities in the station area would not be affected by the PMF conditions in the lake. The only EGC ESP Facility structure that would be affected by the PMF is the intake structure, which will be designed for flood protection of the safety-related equipment located in the intake structure.

Wind-wave forces caused by a sustained 48 mph overland wind coincident with the PMF pool and 67 mph overland wind coincident with normal pool will be considered in the design of the EGC ESP Facility intake structure. Both breaking and non-breaking wave forces will be considered. The flooding effects of the local PMP are design related and will be addressed at the COL stage.

To read:

The maximum (1 percent) wave runup elevation at the station site is 715.4 ft above msl, produced by a sustained 52 mph overland wind acting on the PMF still water elevation of 708.9 ft above msl. The approximate grade elevation for the EGC ESP Facility of 735 ft above msl is approximately 20 ft above the maximum wave runup level and 26 ft above the PMF water level. The safety-related facilities in the station area would not be affected by the PMF conditions in the lake. The only EGC ESP Facility structure that would be affected by the PMF is the intake structure, which will be designed to consider flood protection of the safety-related equipment located in the intake structure.

The flooding effects of the local intense precipitation (i.e., the local PMP values) are design related (since the effects are dependent on site grading and drainage design) and will be addressed at the COL stage as indicated in Section 2.4.2.3.

Revise SSAR, Chapter 2, Section 2.4 Reference, to include the following new reference:

American National Standards Institute / American Nuclear Society (ANSI/ANS). ANSI/ANS-2.8-1983. "Determining Design Basis Flooding at Power Reactor Sites." American Nuclear Society. La Grange Park, IL. 1992.

ATTACHMENTS:

None

NRC Letter Dated: 07/26/2004

NRC RAI No. 2.4.7-1

Please discuss the potential for ice sheet collision impacts on the intake structure and quantify the force of impact.

EGC RAI ID: R9-13

EGC RESPONSE:

There is potential for ice sheet effects on the intake structure. As such, the ice sheet effects will be considered at the COL stage.

ASSOCIATED EGC ESP APPLICATION REVISIONS:

Revise SSAR, Chapter 2, Section 2.4.7, to add the following at the end of the section:

Since there is a potential for ice sheet effects on the ESP intake structure, the final intake structure design at the COL stage will include the effects of the applicable ice forces. The force resulting when a moving ice sheet and a structure interact is limited to the magnitude of force necessary to fail the ice sheet in crushing, bending, buckling, splitting, or a combination of these modes. The total force on the entire structure is important for designing foundations to resist sliding and overturning. Contact forces over small areas, or local contact pressures, are important for designing internal structural members and the external skin of a structure.

ATTACHMENTS:

None

NRC Letter Dated: 07/26/2004

NRC RAI No. 2.4.7-2

Please explain how the ice sheet thickness identified in Section 2.4.7 was calculated and provide the input assumptions.

EGC RAI ID: R9-14

EGC RESPONSE:

The ice sheet thickness was calculated using the standard methodology described in USACOE, *Engineering and Design-Ice Engineering (EM1110-2-1612)*.

General assumptions used include:

Ice formation occurs over a four month period from November through February.

Little snow accumulation is expected on the ice surface. Therefore, snow ice which can form on the lake ice surface is not included in the calculation.

Because there are no records of freeze up for Clinton Lake, an approximate date was determined using the *observed* freeze up dates for Lake Monona in Madison, Wisconsin, located approximately 180 miles north of Clinton Lake. The two lakes are of similar size and volume.

Clinton Lake began filling with water in October 1977. Winter seasons 1978 through 2003 were used in the analysis.

The input parameters include:

Temperature data from Decatur, Illinois (10 miles to the south) were used for computing freezing degree days.

A conservative approach was taken in which the coefficient of ice cover of 0.80 was used. This assumes a windy lake with no snow cover which will tend towards a greater estimation of ice thickness.

The results of the analysis indicate that a maximum ice thickness on Clinton Lake is estimated at 22.2 inches, with an average thickness of 14.2 inches, for years in which the lake freezes.

Section 2.4.7 of the SSAR will be revised to provide additional information on ice depth.

ASSOCIATED EGC ESP APPLICATION REVISIONS:

Revise SSAR, Chapter 2, Section 2.4.7, second paragraph, from:

The average thickness of sheet-ice that could form in the lake area is estimated to be 10 in, without considering the increase in lake water temperature due to station operation. The calculation is based on the empirical method developed by Assur (Chow, 1964), using a coefficient of snow cover of 0.85 and a value of 115 for the accumulated degree-days since freeze-up obtained from the average temperature data of Decatur, Urbana, and Springfield (USWB, 1964).

To read:

Ice thickness calculations were completed for Clinton Lake for 26-years extending back from the 2003-2004 winter. The average thickness of sheet-ice calculated over that period is 14.2-inches. The maximum thickness calculated was in the 1978-1979 winter of 22.2-inches. The calculations did not consider the influence of heat discharge from the power plant. The thickness was estimated using the standard method from the U. S. Army Corps of Engineers (USACOE, 2002). The coefficient of ice cover condition used in the calculation was 0.80 with freezing degree days calculated for each year from temperature data from Decatur, Illinois (MRCC, 2004).

Revise SSAR, Chapter 2, Section 2.4.7, first portion of third paragraph, from:

The inlet to the CPS screen house is at elevation 670 ft above msl, 5 ft below the design water level of the ultimate heat sink, giving a water depth of 12.3 ft for station operation during lake low water level conditions. The occurrence of an estimated ice thickness of 10 in in the intake area when the water level is at elevation 675 ft above msl would not block the flow into the CPS screen house. The availability of CPS station cooling water will not be affected by ice formation in the screen house area.

To read:

The inlet to a screen house at elevation 670 ft above msl is 5 ft below the design water level of the ultimate heat sink, giving a water depth of 12.3 ft for station operation during lake low water level conditions. The occurrence of a maximum ice thickness of 22.2 inches in the intake area when the water level is at elevation 675 ft above msl would not block the flow into the screen house. Thus, the availability of EGC ESP facility cooling water will not be affected by ice formation in the screen house area.

Revise SSAR, Chapter 2, Section 2.4 References, to include the following new reference:

Midwestern Regional Climate Center (MRCC). Champaign, IL. Daily Freezing Degree Days from 1978-2004 for Decatur, Illinois. 2004.

ATTACHMENTS:

None

NRC Letter Dated: 07/26/2004

NRC RAI No. 2.4.7-3

Please describe the relationship (layout and depth) of the ESP intake relative to the current Clinton Power Station (CPS) intake.

EGC RAI ID: R9-15

EGC RESPONSE:

The ESP plant intake will be located approximately 65 ft west of the existing CPS plant intake. The bottom concrete slab of the CPS intake structure is at elevation 657 ft 6 in and the inlet extends from elevation 670 ft up to elevation 697 ft. The lake bottom is at elevation 668 ft 6 in. The layout of the ESP facility intake will be similar to the CPS intake. The bottom of the inlet will be at elevation 670 ft and the inlet opening will extend upwards to at least the normal water level in Clinton Lake of 690 ft. The base mat of the ESP facility intake will be located at approximately elevation 657 ft 6 in with the final elevation dependent on the submergence required for the pumps when they are purchased. The pumps will be mounted at approximately elevation 699 ft, the same as CPS.

ASSOCIATED EGC ESP APPLICATION REVISIONS:

None

ATTACHMENTS:

None

NRC Letter Dated: 07/26/2004

NRC RAI No. 2.4.7-4

Please describe the site characteristics of frazil and anchor ice formation.

EGC RAI ID: R9-16

EGC RESPONSE:

The site characteristics for frazil ice and anchor ice are addressed in a new Section 2.4.7.1 added to the SSAR, Chapter 2.

ASSOCIATED EGC ESP APPLICATION REVISIONS:

Revise SSAR, Chapter 2, to add new Section 2.4.7.1, Frazil Ice and Anchor Ice:

2.4.7.1 Frazil Ice and Anchor Ice

At power plants, accumulations of frazil ice or anchor ice can cause blockages of the intakes of water systems by accumulating on any trash racks or screens in the intake path. Frazil ice is fine, small, needle-like structures or thin, flat circular plates of ice suspended in water. In supercooled water, frazil ice particles can adhere to each other forming clusters or flocs that accumulate. Frazil ice on the surface of supercooled water can form floating ice pans, or on the bottom of solid ice cover can form hanging ice dams. Anchor ice is submerged ice attached or anchored to a streambed. Generally anchor ice forms in shallow turbulent water. These conditions could occur in streams that empty into Clinton Lake but these conditions are not expected in the intake structure area. When the anchor ice breaks loose from the streambed it would flow into Clinton Lake and form or join with the cover ice on the lake. However, this anchor ice would not interfere with the operation of the ESP intake structure.

The current CPS facility water intake is designed to avoid obstruction from surface ice and accumulations of frazil ice. Protection against any probable ice blockage in the intake area is provided by recirculating waste heat through a warming line back to the inlet to the screen house. The warming line is designed to maintain a minimum water temperature of 40 degrees F at the intake during winter operation. The CPS plant has not experienced operational problems with frazil ice accumulation on intake facilities.

The ESP facility intake will be located in the vicinity of the existing CPS intake. A means will be provided in the design of the ESP intake, e.g., a warming line from the hot side of the cooling towers, to prevent the formation of frazil ice at the intake for the essential service water cooling tower make-up to protect against the effects of ice blockage. These features will be designed for operation of the EGC ESP facility independent of the CPS facility.

ATTACHMENTS:

None

NRC Letter Dated: 07/26/2004

NRC RAI No. 2.4.7-5

Please discuss the impacts to ice formation if the existing unit was no longer operating.

EGC RAI ID: R9-17

EGC RESPONSE:

The impact of ice formation if the existing CPS unit is no longer operating is discussed in two new paragraphs of text added to the end of SSAR, Chapter 2, Section 2.4.7 and in new Section 2.4.7.1 provided in response to RAI 2.4.7-1.

ASSOCIATED EGC ESP APPLICATION REVISIONS:

Revise SSAR, Chapter 2, Section 2.4.7, to add the following to the end of Section 2.4.7 (and following the additions included with the response to RAI 2.4.7-1):

No ice formation currently occurs in the discharge channel with the CPS operating. No change is expected to occur with the addition of the proposed ESP facility. The channel capacity is roughly 1,372,000 gpm at 1.5 fps. The CPS discharges about 445,000 gpm of warm cooling water during winter months. Adding the proposed ESP facility warm blowdown water discharge of approximately 12,000 gpm would increase the discharge rate to 457,000 gpm. The combined capacity is well within the capacity of the channel.

There is some potential for ice formation on portions of the discharge channel if the ESP facility is operated alone, without the CPS online. The warm water discharge volume would be significantly reduced to only the ESP warm water blowdown discharge rate of approximately 12,000 gpm. This would result in a lower heat output and flow velocity roughly proportional to the reduction in the flow rate. Under these conditions there is an increased potential for surface ice accumulation particularly at locations away from the point of discharge. The accumulation would be much thinner than the predicted normal lake accumulation because of the heat and velocity components of the ESP facility discharge. If ice does form it will tend to be thin and remain in place on the water surface allowing unrestricted flow below the water surface. Therefore, ice movement (and associated jamming or clogging of the discharge channel) is not expected.

ATTACHMENTS:

None

NRC Letter Dated: 07/26/2004

NRC RAI No. 2.4.7-6

Please discuss whether or not ice sheet formation is likely to constrain the intake depth.

EGC RAI ID: R9-18

EGC RESPONSE:

Ice sheet formation on Clinton Lake will not constrain the ESP intake depth. The thickness of ice cover is a small percentage of the intake height, and the warming water used to prevent Frazil ice will retard the formation of an ice cover in the immediate area of the intake trash racks or screens for the essential service water cooling tower make-up.

Section 2.4.7 of the SSAR will be revised to provide additional information on ice effects related to intake depth.

ASSOCIATED EGC ESP APPLICATION REVISIONS:

Revise SSAR, Chapter 2, Section 2.4.7, first portion of the fourth paragraph, from:

The only EGC ESP Facility structure exposed to the effect of ice on Clinton Lake is the new intake structure. The new intake structure will be similar to the existing CPS intake structure except it will be considerably smaller. It is planned to draw water from the same bottom elevation as the CPS intake structure.

To read:

The only EGC ESP Facility structure exposed to the effect of ice on Clinton Lake is the new intake structure. The new intake structure will be similar to the existing CPS intake structure except it will be smaller. The intake opening(s) to the ESP intake structure will extend vertically from elevation 690 feet, or higher, down to approximately elevation 669 feet. The formation of ice on Clinton Lake would potentially block only a small portion of the intake opening since the separation distance between the surface ice and the bottom of the intake is significant.

ATTACHMENTS:

None

NRC Letter Dated: 07/26/2004

NRC RAI No. 2.4.7-8

Please describe the reduction of UHS capacity caused by a loss of Clinton Dam during periods when an ice sheet is covering the lake.

EGC RAI ID: R9-19

EGC RESPONSE:

The ultimate heat sink for the EGC ESP facility will be safety related cooling towers if the selected reactor type does not use passive cooling methods. Clinton Lake is used as a make-up water source for the ESP cooling towers, not as a heat sink. If Clinton Dam is lost, the ice would be expected to be lost also since it would float on the surface. If it is postulated that the ice drops to the CPS ultimate heat sink surface following the loss of Clinton Dam there would be a small decrease in the water mass available as a heat sink for CPS which is more than offset by the additional heat removal capacity gained by having the latent heat of fusion of the ice available for heat removal. Adequate water volume for make-up to the ESP cooling towers would be available since the required shutdown of CPS after a dam failure would supply heat to convert the ice back into water.

ASSOCIATED EGC ESP APPLICATION REVISIONS:

None

ATTACHMENTS:

None

NRC Letter Dated: 07/26/2004

NRC RAI No. 2.4.8-1

Please explain how the cooling needs for the CPS and ESP facilities were calculated as discussed in Section 2.4.8.1.5.

EGC RAI ID: R9-20

EGC RESPONSE:

The 30-day cooling needs for emergency shutdown of the CPS were calculated using the LAKET model, a one dimensional lake temperature prediction program. The LAKET modeling was conducted as part of the design of the CPS Ultimate Heat Sink (UHS) assuming dual 992 MWe power facilities. The model results for cooling volume along with volume estimates for physical processes of sedimentation from a 100-year flood, sedimentation introduced by liquefaction caused by a seismic event, and fire protection were used to established the minimum UHS volume. The minimum volume calculated for the CPS UHS is 849 ac-ft (CPS, 2002, USAR page A2.5-2).

The 30-day cooling needs for emergency shutdown of the EGC ESP are proposed to be satisfied with new cooling towers for an ultimate heat sink. The cooling towers provide the necessary heat dissipation but require make-up water that is proposed to be drawn from the CPS UHS. The estimated 30-day volume of make-up water required for emergency shutdown is 87 ac-ft. This volume was calculated based on the PPE 30-day make-up water volume, plus a 33 percent factor for blowdown, plus an overall 20 percent margin.

The volume of the CPS UHS is periodically measured and was recently measured to be 1,022 ac-ft. If the CPS UHS minimum volume of 849 ac-ft is subtracted from the recently measured UHS volume of 1,022 ac-ft the resulting available volume is 173 ac-ft. This available volume is significantly greater than the needed EGC ESP make-up water volume of 87 ac-ft by 86 ac-ft. Therefore the current CPS UHS has sufficient volume for both the CPS and ESP facilities.

Surface area was also checked, as it is the single most important factor for CPS heat dissipation to the atmosphere. The design surface area of the UHS at elevation 675 ft above msl is about 150 acres. The as-built area (at elevation 675 ft above msl) is about 158 acres, slightly grater than the design area. Drawing 87 ac-ft of water from the UHS to accommodate the EGC ESP make-up water volume reduces the UHS depth by about 0.5 feet. The surface area is also reduced but it remains higher than the design surface area of 150 acres. Therefore the design heat dissipation capacity associated with surface area is maintained.

Additional detail on the modeling review and volumetric and heat dissipation analysis is provided below.

<u>Review of the Original CPS Modeling</u>. The original analysis of the UHS was performed using the LAKET computer program (transient one-dimensional lake temperature prediction program). The modeling was performed to determine the maximum possible starting temperature of the UHS and not exceed the 95°F UHS outlet temperature during a two-unit LOCA and LOOP. The model was updated in 1985 and a sensitivity test was performed in 1986. The sensitivity analysis calculated maximum temperatures for the UHS with various depths to determine if dredging was necessary to remove silt. In

addition, the maximum UHS temperature which will allow one of the dual units to shut down from 100 percent power and not exceed the 95°F UHS outlet temperature was also examined. The results of the modeling indicate that the maximum outlet temperature of 95° will not be exceeded with an initial volume of 590 acre-feet and initial UHS temperatures ranging from 84 to 95°F.

Review of the model documentation indicates that the inputs to the original 1995 LAKET model, and additional modeling performed in 1985 and 1986, were based on worst-case (most conservative) environmental parameters. Salt Creek temperature (downstream from Clinton Lake) and wind speed data were examined for the period of time prior to 1975 and recent time periods and no significant changes in these parameters were noted between the two periods of time (USGS, 2002). The original model results remain applicable and acceptable.

EGC notes that the previous modeling was based on a one-dimensional vertically and laterally averaged approach. Such a model does not account for thermal stratification. Stratification would result in higher surface temperatures than the depth-averaged value. This would enhance heat transfer to the atmosphere, making model predictions more conservative (lower than expected heat transfer rates and faster cooling of the UHS). The existing intake structure is located so that it is taking in water from the vertical depth of the lake. The new intake structure will also be designed to take water from the vertical depth of the lake. Therefore, in the existing and anticipated designs, the initial model approach and results remain valid and appropriate.

Volumetric Analysis for Exelon ESP**.** The UHS for the CPS is designed to provide sufficient water volume and cooling capacity to safely shut down two 992 MWe BWR units and maintain the plant in a shutdown condition for 30 days with no make up water. The minimum UHS volume of 849 acre-feet accounts for the minimum cooling capacity requirement to meet 95º F shutdown service water inlet temperature (590 acre-feet), fire protection (3 acre-feet), sedimentation from a 100-year flood (35 acre-feet), and sediment inflow from liquefaction (221 acre-feet) (CPS USAR, page A2.5-2, 2002). The minimum CPS UHS volume of 849 acre-feet of water, based on the 30-day emergency shut down of the two 992 MWe units, is considered more than sufficient for the existing single 1138.5 MWe CPS Facility.

Annual surveys have been conducted as part of the UHS sedimentation-monitoring program. The Ultimate Heat Sink Monitoring Program reports #20-23 (1998-2002) indicate that immediately following the dredging in 1991, the volume of the UHS was 1,054 acre-feet, and in 2001 the volume was reduced by sedimentation to 1,022 acre-feet.

The EGC ESP Facility is expected to require ≤ 87 acre-feet of cooling water from the UHS for the required 30-day emergency shut down supply. This water volume provides approximately 20% margin compared to the makeup water quantity for 30 days based on PPE data. Assuming no return flow to the UHS (i.e., the 87 acre-feet of water is unavailable for use), 935 acre-feet of the total of 1,022 acre-feet capacity of the UHS will be available for shut down and allocations for sedimentation and fire suppression for CPS. The withdrawal of the 87 acre-feet for the Exelon ESP plant and the minimum volume requirement of 849 acre-feet for CPS will allow a reserve volume of 86 acre-feet for accumulated sedimentation (based on the 2001 measured UHS volume).

Adequate UHS volume will be maintained for CPS and the Exelon ESP Facility if the total UHS volume is maintained to account for the initial required volume of 849 acre-feet

plus the 87 acre-feet required by the Exelon ESP Facility. The current practice calling for dredging the UHS when sedimentation decreases the total UHS volume to less than the 849 acre-feet will be carried out at a schedule so that UHS volume does not decrease to below 936 acre-feet. The estimated annual sedimentation amount is about 5 acre-feet. While dredging should occur based on observed volume measurements, the new dredging trigger volume of 936 acre-feet is expected to result in dredging at least once every 23 years.

Heat Load Analysis**.** The relationship between UHS surface area and volume based on the design and as-built data found in the September 1975 and April 1985 modeling documents indicates that the immediate reduction of the existing volume by 87 acre-feet would result in a decrease of the water level by approximately 0.5 feet. The change in the UHS water level will not significantly impact the surface area, and in fact the surface area remains the same or greater than the original design. This indicates that the capacity of the UHS to reject heat to the atmosphere is maintained. In addition, the CPS USAR Section 9.2.5.3 identifies that the total heat rejection to the UHS for an emergency shutdown, over 30 days, for the Clinton Power Station Facility is less than that assumed in the original design basis modeling (CPS, 2002). Therefore, the original modeling of UHS is still applicable for the new proposed conditions, and the heat capacity of the UHS is adequate.

Section 2.4.8.1.5 of the SSAR will be revised to provide additional information on the calculation of cooling requirements.

ASSOCIATED EGC ESP APPLICATION REVISIONS:

Revise SSAR Chapter 2, Section 2.4.8.1.5 from:

The EGC ESP Facility will use the existing UHS submerged pond as the supply source for makeup water to any required safety-related cooling tower(s) if Clinton Lake is not available. The makeup water will be supplied from the new intake structure located next to the existing screen house. The UHS pond capacity has been evaluated as sufficient volume to provide shutdown cooling for the existing CPS and makeup water to the EGC ESP Facility safety-related cooling tower(s) for 30 days.

To read:

The EGC ESP Facility will use the existing UHS submerged pond as the supply source of makeup water to any required safety-related cooling tower(s) if Clinton Lake is not available. The makeup water will be supplied from the new ESP intake structure located next to the existing CPS screen house. The UHS pond capacity has been evaluated and found to have sufficient volume to provide 30-day emergency shutdown cooling for the existing CPS and makeup water to the EGC ESP Facility safety-related cooling tower(s). The CPS safety-related cooling water volume is conservatively based upon the volume established for the original dual 992 MWe plants. The EGC ESP safety related volume for cooling tower make-up water was calculated based on the PPE evaporation rates for the UHS cooling towers plus a 33% margin for blowdown plus an overall 20% margin above the value obtained using the PPE values. With the combined CPS and ESP emergency cooling volumes there is enough excess UHS volume to provide for a dredging interval in excess of 20 years.

ATTACHMENTS:

None

NRC Letter Dated: 07/26/2004

NRC RAI No. 2.4.8-2

Please discuss how the flow velocities were computed over the crest and toe of the submerged UHS dam discussed in Section 2.4.8.1.5. Please provide figures indicating where the toe of the UHS dam is relative to the fill shown in Figures 2.4-14 and 2.4-15.

EGC RAI ID: R9-21

EGC RESPONSE:

The SSAR, Chapter 2, Section 2.4.8.1.5, discussion of flow velocities over the crest and toe of the submerged UHS dam is unnecessary detail for an ESP review and the section will be revised by removing the discussion of velocities over the crest.

ASSOCIATED EGC ESP APPLICATION REVISIONS:

Revise SSAR, Chapter 2, Section 2.4.8.1.5, from:

The area of the ultimate heat sink at the design water surface elevation of 675 ft above msl is 158 ac with a total volume of 1,067 ac-ft. The velocities over the submerged dam were analyzed for flow conditions resulting from a sudden breach in the main dam. The breach was conservatively assumed to occur at the time of the PMF with the lake water level at elevation 708.8 ft above msl. An instantaneous breach 100 ft wide and extending down to the Salt Creek bed was postulated. The ultimate heat sink and the lake area downstream of the submerged dam were analyzed to evaluate the flow conditions due to the breach. The conventional level pool reservoir routing method was used. This method is based on the premise that the inflow volume minus the outflow volume equals the change in storage. The inflow volume is the flow through a control section, which is the constriction due to a railroad bridge upstream of the ultimate heat sink. The water surface elevations upstream and downstream of the submerged dam were determined from the flood routing calculations. Based on the water surface elevations and the corresponding flow over the submerged dam, the maximum velocities at the crest and at the toe of the dam were calculated. The maximum velocities obtained are 3.8 and 11.8 fps at the crest and at the toe of the submerged dam, respectively, occurring 43 hours after the main dam breach. Correspondingly, a maximum velocity of 1.2 fps on the face of the baffle dike is obtained. The maximum velocity on the baffle dike is lower than the maximum velocity at the crest of the submerged dam because the induced flow is primarily parallel to the baffle dike.

The velocities over the submerged dam and baffle dike were also analyzed with the occurrence of a PMF on the North Fork when the lake level is at the 100 yr drought water surface elevation of 682.3 ft above msl. The maximum velocities obtained over the submerged dam and baffle dike are 2.1 and 2.6 fps, respectively.

The compacted soil-cement provided over the surface of submerged dam and baffle dike will protect these structures against the erosive effect of the velocities and flow conditions due to the postulated dam breach and the occurrence of a probable maximum flood on North Fork coincident with the 100 yr drought lake water level of elevation 682.3 ft above msl.

To read:

The area of the ultimate heat sink at the design water surface elevation of 675 ft above msl is 158 ac with a total volume of 1,067 ac-ft. The UHS for the CPS is designed to provide sufficient water volume and cooling capacity to safely shut down two 992 MWe BWR units and maintain the plant in a shutdown condition for 30 days with no make up water. The minimum UHS volume of 849 acre-feet accounts for the minimum cooling capacity requirement to meet 95º F shutdown service water inlet temperature (590 acre-feet), fire protection (3 acre-feet), sedimentation from a 100-year flood (35 acre-feet), and sediment inflow from liquefaction (221 acre-feet) (CPS, 2002, USAR page A2.5-2). The minimum UHS volume of 849 acre-feet of water, based on the 30-day emergency shut down of the two 992 MWe units is more than sufficient for the existing single uprated 1138.5 MWe CPS Facility.

Analysis conducted during the design of the submerged UHS dam and the baffle dike included evaluating flow conditions and velocities resulting from a sudden breach in the main dam that was conservatively assumed to occur at the time of the PMF. The flow conditions resulting from an occurrence of a PMF on the North Fork when the lake is at the 100 yr drought were also analyzed as part of the UHS design. As a result of the analysis, a compacted soil-cement was provided over the surface of the submerged dam and baffle dike to protect these structures against the erosive effect of the velocities and flow conditions due to the postulated dam breach and the occurrence of a probable maximum flood on North Fork coincident with the 100 yr drought lake water level of elevation 682.3 ft above msl (CPS, 2002).

ATTACHMENTS:

None

NRC Letter Dated: 07/26/2004

NRC RAI No. 2.4.8-3

Please describe lake drawdown calculations.

EGC RAI ID: R9-22

EGC RESPONSE:

SSAR section 2.4.11.1 discusses the Clinton Lake drawdown evaluation. SSAR Section 2.4.11.1 will be updated to provide additional description of the evaluation.

ASSOCIATED EGC ESP APPLICATION REVISIONS:

Revise SSAR, Chapter 2, Section 2.4.11.1 from:

A design drought with a recurrence interval of 100 yrs was used in the determination of the minimum water level in the cooling lake for the CPS. Factors considered in the evaluation include runoff, evaporation, and forced evaporation.

A drawdown analysis of Clinton Lake, for the original Clinton Power Station, was made for two 991 MWe units operating at a 70% load factor, starting at a normal pool elevation of 690 ft above msl, using a minimum reservoir release of 5 cfs and assuming a seepage loss of 0.5% of the lake capacity per month. The original Clinton Power Station drawdown analysis was used to evaluate the capability of Clinton Lake to provide cooling tower makeup water for the EGC ESP Facility and the cooling water requirements for CPS. The forced evaporation rate (evaporation loss due to heat rejection from CPS) was corrected as follows for use in the EGC ESP evaluation:

- Divided by 2 since only one of the two units originally planned was constructed.
- Divided by 0.7 to conservatively adjust the evaporation for a 100 % load factor.
- Multiplied by 1.20 to conservatively adjust for the additional heat load due to power uprate of CPS.

The drawdown evaluation performed for the EGC ESP Facility determined that the quantity of water available for cooling tower makeup based on a 50 yr drought is 15,808 gpm and the quantity available with a 100 yr drought is 10,222 gpm. The available water quantities maintain the lake level at or above the CPS minimum lake elevation of 677 ft above msl with both the CPS and the EGC ESP Facility in operation.

To read:

Two design droughts were established having a 5-year duration at 50-year and 100-year recurrence intervals. Factors considered in the evaluation include runoff, evaporation, and forced evaporation. Low flow runoff data for both design droughts were obtained from the CPS USAR, which cited the source Low Flows of Illinois Stream for Impounding Reservoir Design published as Bulletin 51 by the Illinois State Water Authority (Stall, 1964).

A normal lake elevation level of 690 ft above msl was used as the starting water surface level. Lake stage storage relationships were obtained from CPS ER (OLS) based on the

original lake volume of 74,200 ac-ft at normal lake level (CPS, 1982). Inflow to the lake (in acre-feet) was computed on a monthly basis by multiplying the rainfall runoff (in feet) by the watershed area (in acres). Outflow from the lake was assumed to be comprised of downstream discharge; net lake evaporation minus lake precipitation; forced evaporation due to existing plant operations; seepage; and the cooling water consumed by the new facility. Rainfall runoff flows for both drought events were obtained from the CPS USAR. Runoff values were multiplied by the watershed area of 296 square miles to establish a runoff volume. Downstream discharge through the dam was assumed to be a minimum discharge of 5 cubic feet per second (cfs); or 298 acre-feet/month, when lake levels are at or below the 690-foot spill elevation. For the purpose of drought analysis calculations, the lake elevation was not allowed to exceed 690 ft above msl. The discharge was allowed to be greater than 5 cfs if inflows would increase the lake level to a level above the spillway elevation of 690 ft above msl (CPS, 2002).

Net lake evaporation minus precipitation data was obtained from CPS USAR for both the 50-year and 100-year recurrence interval droughts.

Existing plant forced evaporation data used in this analysis was developed from data given in the CPS USAR, which was based upon two originally planned 992 MWe BWR plants at a 70 percent load factor (CPS, 2002). Forced evaporation is defined as the additional evaporation produced due to an increase in lake water temperature caused by the discharge of cooling water to the lake under the open-cycle lake cooling process for the two original plants. This factor accounts for the total evaporative loss that results from dissipation of the heat rejected to the lake. The evaporative loss will occur through the cooling loop. The term forced evaporation is used because the rejected heat and associated increase in lake temperature will "force" an increase in the rate of evaporation over ambient levels to dissipate the rejected heat.

Forced evaporation rate for the two proposed plants was revised to reflect the rate for the existing single uprated plant. Only one of the two original plants was constructed at 992 MWe but was uprated in 2002 to an 1138 MWe plant. The forced evaporation rates from the CPS USAR were divided by 0.7 to obtain the evaporation rate for a 100 percent load factor. The forced evaporation rates were then divided by two to account for the fact that only one plant is present. To account for the power uprate, the forced evaporation rates were then multiplied by 1.147 (1138/992). The combination of these three factors is equal to multiplying the original forced evaporation rates by a factor of 0.82.

The forced evaporation values for the original 992 MWe plant operating at 100 percent were recently checked using an independent thermal analysis. The forced evaporation rates determined by that exercise closely matched the CPS USAR forced evaporation rates, but were slightly smaller, so the more conservative CPS USAR forced evaporation rates were used. The method used to check the forced evaporation rates is described below.

Forced and natural evaporation occur simultaneously as the circulating water flows through the cooling loop. In order to differentiate between the amounts of natural and forced evaporation, the equilibrium temperature for the lake was determined on a monthly basis using monthly climactic data over the period of record. The equilibrium temperature is the temperature of the lake water (about 1 foot below the surface) where the heat input to the lake water is exactly balanced by the heat output from the lake water. This equilibrium temperature is determined by performing a heat balance for solar heat gain, heat loss by convection, evaporative cooling and radiant heat transfer

from the water to the surroundings. The amount of natural evaporation (per unit area of lake) is determined based on this equilibrium temperature.

To determine the amount of forced evaporation, a model that follows the method of Langhaar (Langhaar, 1953) was developed, and was validated by good agreement with results of an earlier study (Edinger, 1989). The model was then applied to simulate the cooling lake for each month, using monthly average climactic conditions over the period of record. The simulation quantifies the aforementioned modes of heat transfer per unit area of lake. The evaporative cooling that is determined by the model is a "total" value (forced plus natural evaporation). The amount of forced evaporation is simply the difference between the total and natural evaporation determined from the equilibrium temperature.

Existing and proposed plants assume a 100 percent load factor in their operation. It was assumed that each drought event would begin during January of the first year of the drought. As in the CPS USAR, seepage was assumed to be equal to 0.5 percent of the lake volume.

By definition, a 100-year recurrence interval event has a 1 percent exceedance probability to occur in any given year. Similarly, a 50-year recurrence interval event has a 2 percent exceedance probability to occur in any given year. Calculations were carried out to determine the likelihood of 50-year and 100-year recurrence interval events during the 40-year life of the proposed plant. It was determined that there is a 56 percent exceedance probability that at least one 50-year recurrence interval drought will occur during the 40-year life of the plant. There is a 33 percent exceedance probability that at least one, 100-year recurrence interval drought will occur during the same 40 year period.

Calculations were carried out for each month; a net volume gain or loss was calculated by subtracting lake volume losses and adding lake volume gains (both in acre-feet). This net change was then added to the initial volume for that month to obtain the initial volume for the next month. The lake elevation-area capacity and -volume capacity relationships found in the CPS ER (OLS) were then used to estimate the lake elevation level and lake area for the following month (CPS, 1982). These calculations were carried out separately for 60 months (the 5-year duration period) of the 50-year and 100-year recurrence interval droughts.

A determination of the amount of water available for cooling water use during drought periods was also conducted. The amount of water consumed on an average annual basis by the existing CPS plant at 100 percent of its rated capacity is 1,100 acre-feet/month (12.0 MGD or 8,300 gpm). The total amount of water available for consumption for the 100-year drought event is equal to 2,400 acre-feet/month (25.6 MGD or 17,800 gpm). Thus, the amount of water available for use in addition to the amount already used by the existing plant is 1,300 acre-feet/month (13.7 MGD or 9,500 gpm).

A similar analysis was performed for the 50-year drought event. The amount of water consumed on an annual basis by the existing plant was calculated out to a rate of 1,100 acre-feet/month (12.0 MGD or 8,300 gpm). The total amount of water available for consumption is equal to 3,100 acre-feet/month (33.7 MGD or 23,400 gpm). Thus, the amount of water available for use in addition to the amount already used by the existing plant is 2,000 acre-feet/month (21.7 MGD or 15,100 gpm).

The available water quantities maintain the lake level at or above the CPS minimum lake elevation of 677 ft above msl with both the CPS and the EGC ESP Facility in operation.

Revise SSAR, Chapter 2, Section 2.4 References to add the following new references:

J.E. Edinger & Associates, Inc. Probabilistic Hydrothermal Modeling Study of Clinton Lake. Document 89-15-R. February 1989.

Langhaar, J. W. Cooling Pond May Answer Your Water Cooling Problem. Chemical Engineering. 60(8), 194,1953.

Stall, J.B. Low Flows of Illinois Stream for Impounding Reservoir Design. Illinois State Water Authority. Bulletin 51. 1964.

ATTACHMENTS:

None

NRC Letter Dated: 07/26/2004

NRC RAI No. 2.4.8-4

Please describe how UHS capacity loss due to sediment or debris loads during extreme events was estimated.

EGC RAI ID: R9-23

EGC RESPONSE:

The ESP facility will use safety-related cooling towers as the ultimate heat sink, if one is required, and will only use the CPS ultimate heat sink pond as a source of make-up. Therefore, the ESP facility ultimate heat sink is not directly affected by sediment or debris.

The basis for the CPS ultimate heat sink is discussed as follows. According to "Soil Survey of DeWitt County, Illinois" (Roger D. Windhorn, Illinois Experiment Station Soil Report No. 137, issued September 1991), early spring rains in areas where soils are exposed by farming can cause extensive erosion when the soils are partially frozen and more water runs off the surface. ESP SSAR Table 2.4-5-Monthly Probable Maximum Precipitation for 24-Hour Duration for Zone 7 indicates that the highest 24-hour PMP occurs in the summer and fall (June through October with a PMP range of 24.4 to 31.2 inches) and not during the early spring. Thus, the occurrence of the PMP would not be coincident with the conditions for maximum runoff (i.e., when the fields are not planted).

According to Attachment A2.5-"Ultimate Heat Sink Liquefaction Analysis" provided in the CPS USAR (CPS, 2002), the design of the UHS considered four failure modes including:

- Loss of cooling water inventory due to its displacement by alluvial flow slides into the UHS;
- Loss of the service water system due to blockage of the service water pump intakes from unstable soil flow blocking or entering the intake structure;
- Loss of the UHS circulation pattern due to local slides producing dikes or dams across the circulation channel; and
- Loss of UHS water because the UHS dam or its flanks are breached by the combination of seismic loadings, liquefaction, and wash out.

In addition to the storage requirements for cooling purposes and fire water supply, the storage capacity was provided to account for sedimentation. The design bases used in determining the minimum UHS volume included the following (CPS, 2002, USAR page A2.5-2):

Sediment inflow from liquefaction - 221 acre-feet

Required fire water storage capacity - 3 acre-feet

Minimum cooling capacity requirement to meet 95º F shutdown service water inlet temperature 590 acre-feet

Maximum sedimentation due to a 100-year flood - 35 acre-feet

As indicated in the ESP SSAR, Section 2.4.11.6, the CPS UHS is monitored for sediment accumulation periodically and after a major flood passes through the cooling lake (CPS, 2002). Dredging will be performed as necessary to prevent the accumulation

from exceeding the capacity provided for sediment storage. The procedures used in the CPS UHS Sedimentation Monitoring Program are described in Attachment B of the CPS USAR (page 2.4-37; 2002).

ASSOCIATED EGC ESP APPLICATION REVISIONS:

None

ATTACHMENTS:

None

NRC Letter Dated: 07/26/2004

NRC RAI No. 2.4.9-1

Please provide references to studies related to geological features or other characteristics that preclude any likelihood of channel diversion upstream of the site.

EGC RAI ID: R9-24

EGC RESPONSE:

The studies of the geological features and other characteristics related to potential channel diversion upstream of the site were performed specifically for the EGC ESP Application. This project specific examination did not rely upon previously existing studies or references (other than the topographic maps), and thus, there are no references to studies to provide. Examination of the topographic maps of the Salt Creek and North Fork of Salt Creek did not find evidence for natural channel diversions (e.g., oxbow lakes or broad well-developed floodplains). The creeks and streams in the watershed generally occur in well-defined valleys. Diversions of water out of these valleys into an adjacent drainage basin would require the energy to overcome the topography to cut a new drainage channel. Based on the physical characteristics of the drainage area and creek system, it is unlikely that a potential naturally-occurring channel diversion will shift water out of the Clinton Lake watershed. The text in SSAR, Chapter 2, Section 2.4.9, will be revised to add clarification.

ASSOCIATED EGC ESP APPLICATION REVISIONS:

Revise SSAR, Chapter 2, Section 2.4.9 from:

There is no historical evidence of channel diversion of Salt Creek and North Fork of Salt Creek upstream of the dam site. The dam site is located on the upper reaches of Salt Creek, 28 mi from its source. The topographic characteristics and geological features of the drainage basin indicate that there is no possibility for the occurrence of a landslide that will cut off the streamflow into the lake. The history of ice jam formation discussed in Section 2.4.7, Ice Effects, did not show evidence of flow diversion during winter months.

To read:

There is no historical evidence of channel diversion of Salt Creek and North Fork of Salt Creek upstream of the dam site. The dam site is located on the upper reaches of Salt Creek, 28 mi from its source. Examination of the topographic maps of the Salt Creek and North Fork of Salt Creek did not find evidence for natural channel diversions (e.g., oxbow lakes or broad well-developed floodplains). The creeks and streams in the watershed generally occur in well-defined valleys. Diversions of water out of these valleys into an adjacent drainage basin would require the energy to overcome the topography to cut a new drainage channel. Based on the physical characteristics of the drainage area and creek system, it is unlikely that a potential naturally-occurring channel diversion will shift water out of the Clinton Lake watershed. The topographic characteristics and geological features of the drainage basin indicate that there is no possibility for the occurrence of a landslide that will cut off the streamflow into the lake.

The history of ice jam formation discussed in Section 2.4.7, Ice Effects, did not show evidence of flow diversion during winter months.

ATTACHMENTS:

None

NRC Letter Dated: 07/26/2004

NRC RAI No. 2.4.10-1

A design wind of 40 mph was mentioned in the second paragraph of Section 2.4.10 and earlier in Section 2.4.3.6. In the third paragraph of Section 2.4.10, 48 and 67 mph winds are mentioned for wave run up consideration at the intake facility. Please discuss the differences in these design winds and the methods for determining both these design winds.

EGC RAI ID: R9-25

EGC RESPONSE:

The maximum wave run-up elevation at the dam and the CPS site, due to a sustained 40 mph overland wind speed acting on the PMF water level, was previously estimated to be 711 ft above mean sea level (CPS USAR Section 2.4.2.2, "Flood Design Considerations"). Additionally, CPS USAR Section 2.4.10, "Flooding Protection Requirements," considered a 48 mph overland wind speed coincident with the PMF pool in the design of the circulating water screen house at CPS. The use of these values in the CPS USAR did not result in any safety related issues for the CPS station site since the site was determined to be 22.2 feet above the calculated wave run-up level and 27.1 feet above the calculated PMF level, with the conclusion that the CPS plant facility could not flood under any circumstances. The ESP Facility Site is considered to be a "dry site", consistent with Condition 3 of Attachment 2, Section 2.4.3, "Probable Maximum Flood (PMF) on Streams and Rivers," of NRC's RS-002 Review Standard, and will not be susceptible to flooding under any circumstances. Furthermore, the operation of the ESP Facility will not impact the potential for flooding at the existing dam or the plant site and, therefore, the calculation of wave run-up effects on PMF levels is inconsequential. The use of the 40 mph wind speed was retained in the ESP SSAR wave run-up analysis to be consistent with what was originally prepared for the CPS USAR and what is currently relied upon in the CPS USAR. A review of more recent information published by the American Nuclear Society (ANSI/ANS-2.8-1992 "Determining Design Basis Flooding at Power Reactor Sites") has in fact indicated that a wind speed of somewhat greater magnitude may be appropriate for design considerations when estimating the impact of wind speeds on flooding. Figure 1 from the 1992 ANS publication entitled "Isotach 0.50 Quantiles (in miles per hour): Annual Extreme-Mile, 30 ft Above Ground, 2-yr Mean Recurrence Interval" indicates that a wind speed of 52 mph is more appropriate for calculating wave run-up height coincident with the PMF pool height.

Sections 2.4.3.6 and 2.4.10 of the SSAR will be revised to use a wind speed of 52 mph.

ASSOCIATED EGC ESP APPLICATION REVISIONS:

Revise SSAR, Chapter 2, Section 2.4.3.6, Section 2.4.10, and Section 2.4 References, as provided with the response to RAI 2.4.3-2.

ATTACHMENTS:

None

NRC Letter Dated: 07/26/2004

NRC RAI No. 2.4.12-1

Please provide additional information regarding the likelihood for liquid effluents to reach a surface water body.

EGC RAI ID: R9-26

EGC RESPONSE:

The design basis for the ESP facility regarding the potential for release of radioactive liquid effluents to reach a surface body of water following a postulated failure of a tank is that the liquid will be retained inside the structure due to the hydrostatic forces of the groundwater outside the structure. The discussion of the regional and local groundwater system is presented in SSAR 2.4.13 and the potential for accidental releases is discussed in SSAR Section 2.4.13.3. As discussed in SSAR Section 2.4.13.3, accidental releases to subsurface and surface water are unlikely since the level of radioactive liquids in the building would have to exceed the groundwater level before seepage could occur. The water levels measured in the recently installed piezometers (July 2002), within the ESP footprint, indicate that the uppermost groundwater naturally occurs at a shallow depth of about 5 feet below ground surface (see the table below). Based on the maximum seasonal variation in the groundwater level of 12 ft, the lowest water levels were at about elevation 718 ft above msl or about 17 ft below the ESP Facility grade elevation of 735 ft above msl.

Hydrogeologic Unit	Top of Unit		Water Surface	
	Depth (ft)	Elevation (ft)	Depth (ft)	Elevation (ft)
Wisconsinan	8 to 13	724.2 to 726.1	3.7 to 6.5	733.5 to 727.5
Illinoian	58	679.8	27.8 to 27.3	710.8 to 711.3

Recent water levels are consistent with those reported in previous site investigations, indicating that the construction and operation of the CPS has not caused significant changes to the depth to the uppermost groundwater. The construction of the EGC ESP Facility is also not anticipated to cause changes to the groundwater system. Groundwater levels will be measured as part the Pre-Application, Construction, Pre-operational, and Operational Hydrologic Monitoring Programs in order to detect impacts to the groundwater system. This issue will be reviewed at the COL stage when an NSSS vendor is selected and the final plant layout of the structures and components is determined to assure that the inward gradient is maintained relative to final plant elevations and layout.

Sections 2.4.12 of the SSAR will be revised to provide additional discussion.

ASSOCIATED EGC ESP APPLICATION REVISIONS:

Revise SSAR, Chapter 2, Section 2.4.12 from:

As discussed in Section 2.4.13.3, it is extremely unlikely that the effluents can move out of the buildings containing radioactive liquids due to high groundwater elevation. In addition, tanks located outside of structures potentially containing radioactive fluids will have positive means to collect and prevent uncontrolled releases such as dikes and collection basins. Therefore, it is extremely unlikely for the effluents to reach a surface water body.

To read:

As discussed in Section 2.4.13.3, it is extremely unlikely that the effluents can move out of the buildings containing radioactive liquids due to high groundwater elevation. Recent water level measurements, from within the ESP footprint, indicate that the uppermost groundwater naturally occurs at a shallow depth of about 5 feet below ground surface. Based on the maximum seasonal variation in the groundwater level of 12 ft, the lowest water levels were at about elevation 718 ft above msl or about 17 ft below the ESP Facility grade elevation of 735 ft above msl. Thus, the level of radioactive effluents in the building would have to exceed the groundwater level before seepage out of the building could occur. In addition, tanks located outside of structures potentially containing radioactive fluids will have positive means to collect and prevent uncontrolled releases such as dikes and collection basins. Therefore, it is extremely unlikely for the effluents to reach a surface water body.

Groundwater levels will be measured as part the Pre-Application, Construction, Pre-operational, and Operational Hydrologic Monitoring Programs in order to detect impacts to the groundwater system. This issue will be reviewed at the COL stage when an NSSS vendor is selected and the final plant layout of the structures and components is determined to verify that the inward gradient is maintained relative to final plant elevations and layout.

ATTACHMENTS:

None

NRC Letter Dated: 07/26/2004

NRC RAI No. 2.4.13-1

Please provide a description of the local subsurface environment adequate to understand groundwater pathways from the plant including subsurface disturbances of local strata from structures and perched aquifers.

EGC RAI ID: R9-27

EGC RESPONSE:

The discussion of the regional and local subsurface environment is presented in SSAR 2.4.13. The following provides a synopsis of the information:

Groundwater beneath the ESP site occurs in unconfined conditions in the upper glacial deposits (Wisconsinan) and confined conditions in the underlying Illinoian and Kansan tills. The shallow groundwater moves along short flow paths and discharges to local surface water bodies (e.g., North Fork of Salt Creek or Clinton Lake). The remainder circulates to the deeper sand and gravel that fills the Mahomet Valley or to bedrock aquifers. The water levels measured in the recently installed piezometers (July 2002), within the ESP footprint, indicate that the uppermost groundwater naturally occurs at a shallow depth of about 5 feet below ground surface. Recent water levels are consistent with those reported in previous site investigations, indicating that the construction and operation of the CPS has not caused significant changes to the depth to the uppermost groundwater. The construction of the EGC ESP Facility is also not anticipated to cause changes to the groundwater system.

The water level measurements collected during the CPS site investigations and the description of impacts to water levels in response to filling the impoundment, indicate that lake filling did not cause a substantial readjustment of groundwater levels at the plant site. The lack of response in the uppermost water levels was anticipated because the base of the overlying Wisconsinan deposits in onsite borings (averaging 698 feet msl) is above the normal pool elevation of 690 ft msl (CPS USAR). Based on the results of the CPS investigations, changes in the lake levels are not anticipated to result in major changes in gradients across the site. In addition, the low permeability of the shallow glacial material will tend to minimize impacts from sudden changes in site conditions.

Groundwater levels will be measured as part the Pre-Application, Construction, Pre-operational, and Operational Hydrologic Monitoring Programs in order to detect impacts to the groundwater system (see SSAR Section 2.4.13.4). If construction of the plant causes the hydrologic system to change, the impact of these changes will be evaluated at the COL stage.

ASSOCIATED EGC ESP APPLICATION REVISIONS:

None

ATTACHMENTS:

None

NRC Letter Dated: 07/26/2004

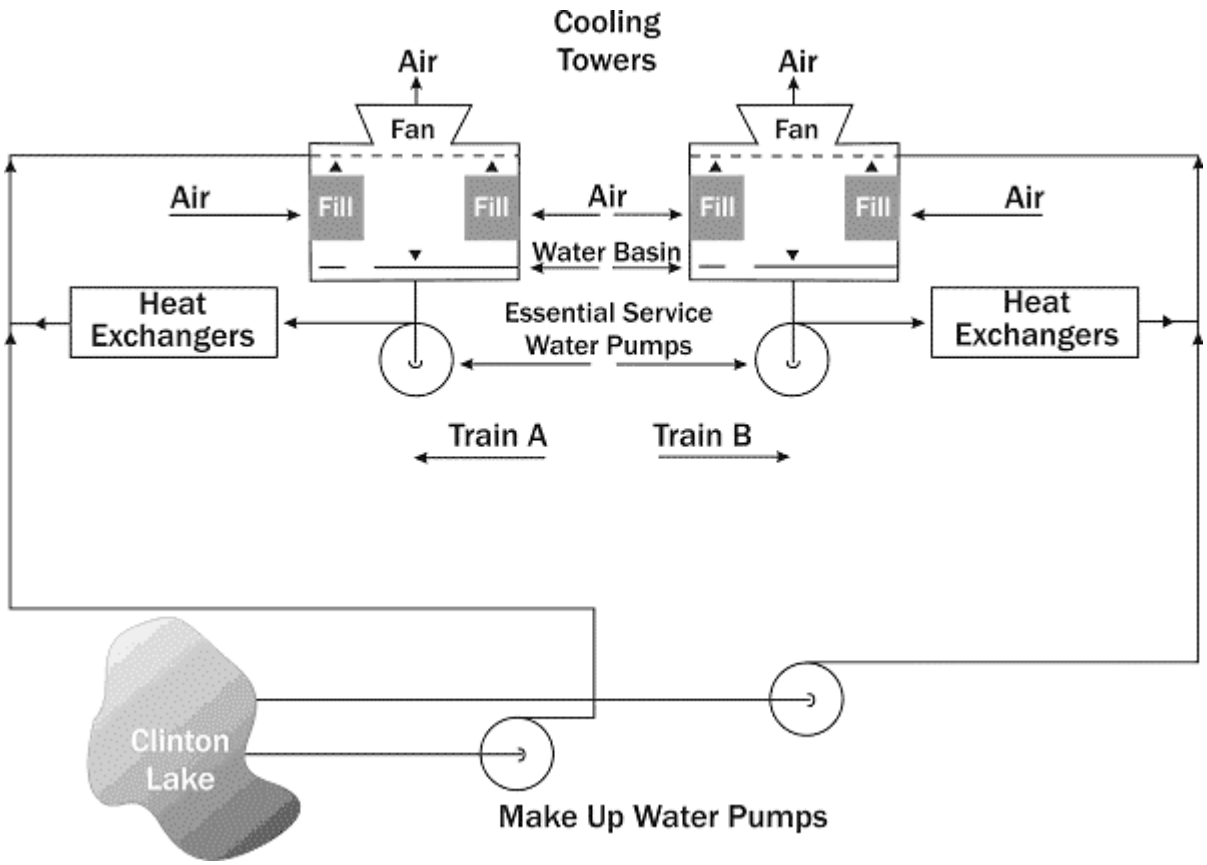
NRC RAI No. 3.2.2-1

Please provide a schematic that describes water circulation in the UHS.

EGC RAI ID: R9-28

EGC RESPONSE:

A schematic that describes typical water circulation in the EGC ESP UHS (should one be required) will be included in Section 3.2.2 as shown below:



ASSOCIATED EGC ESP APPLICATION REVISIONS:

Revise SSAR, Chapter 3, Section 3.2.2, to include the following additional sentence at the end of the first paragraph:

Figure 3.2-1 shows a schematic diagram that describes typical water circulation in the UHS system for the EGC ESP Facility (should one be required).

Revise SSAR, Chapter 3, Section 3.2, to include new Figure 3.2-1 as shown in the attachment to this RAI response.

NRC Letter Dated: 07/26/2004

NRC RAI No. 3.2.2-2

Please describe the consequences of a failure of the baffle in the UHS.

EGC RAI ID: R9-29

EGC RESPONSE:

There is no baffle in the ESP facility UHS. The failure of the baffle in the CPS ultimate heat sink has no effect on the ESP facility since the ESP facility will use cooling towers as the UHS, if one is required, and only uses the CPS UHS pond as a source of make-up to the cooling towers. The volume of water available for make-up to the ESP facility is not impacted by the failure of the CPS UHS baffle.

ASSOCIATED EGC ESP APPLICATION REVISIONS:

None

ATTACHMENTS:

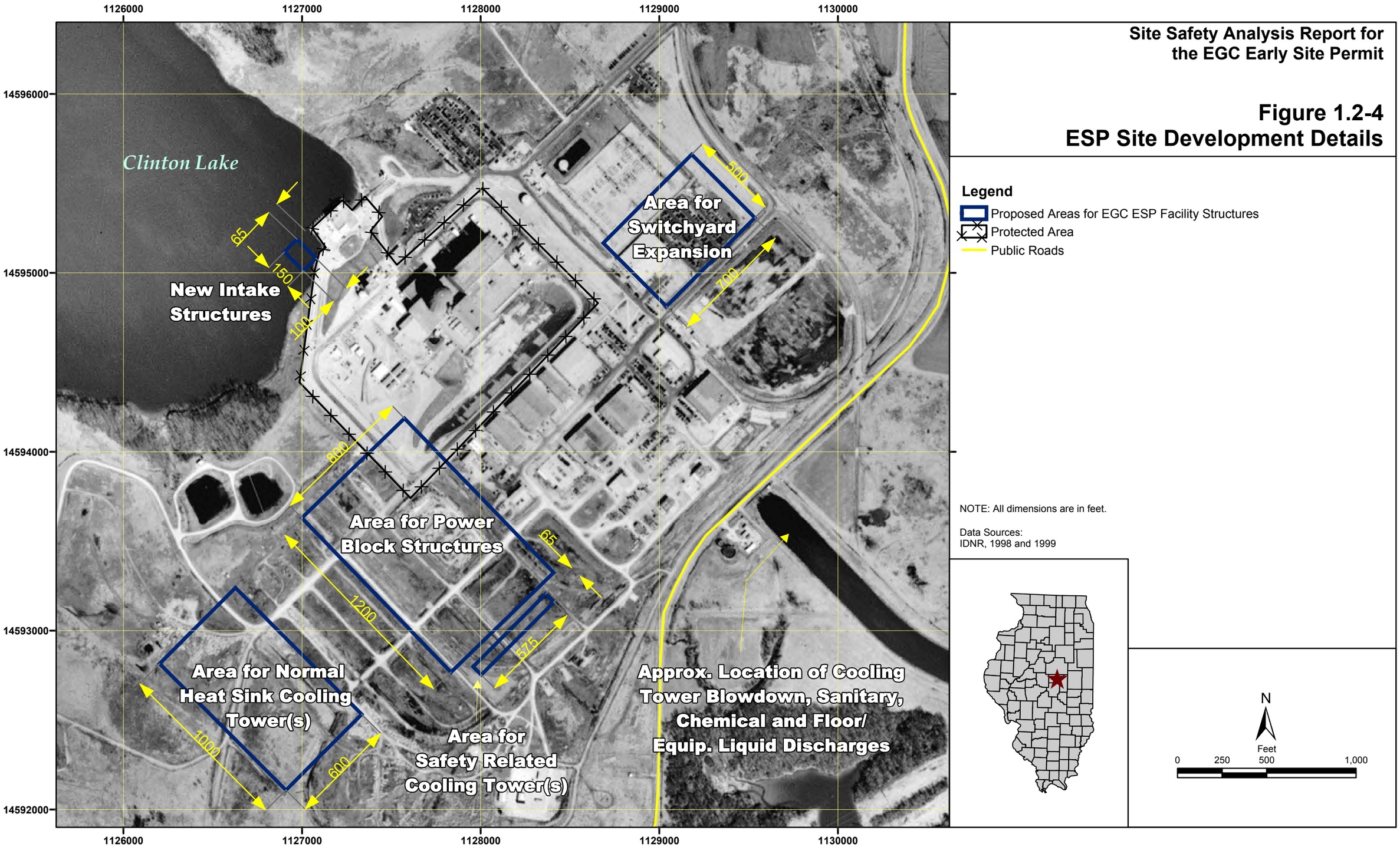
None

RAI ATTACHMENT

RAI 2.4.1-1 Attachment (Revised Figure 1.2-4)

(Note – This attachment provided on the enclosed CD-ROM.)

See file: RAI 2.4.1-1 Attachment (Revised Figure 1.2-4).pdf


Site Safety Analysis Report for the EGC Early Site Permit
Figure 1.2-4
ESP Site Development Details
Legend
Proposed Areas for EGC ESP Facility Structures
Protected Area
Public Roads
NOTE: All dimensions are in feet.
Data Sources:
IDNR, 1998 and 1999
Clinton Lake
New Intake Structures
65
150
100
Area for Switchyard Expansion
500
700
Area for Power Block Structures
800
65
1200
575
Area for Normal Heat Sink Cooling Tower(s)
1000
600
Area for Safety Related Cooling Tower(s)
Approx. Location of Cooling Tower Blowdown, Sanitary, Chemical and Floor/ Equip. Liquid Discharges
1126000
1127000
1128000
1129000
1130000
14596000
14595000
14594000
14593000
14592000
N
Feet
0
250
500
1,000

RAI ATTACHMENT

RAI 2.4.1-5 Attachment 1 (MRCC 2002a)

(Note – This attachment provided on the enclosed CD-ROM.)

See file: RAI 2.4.1-5 Attachment 1 (MRCC 2002a).pdf

Technical Editing Guidance Reference Source Documentation

Source Document No. SSAR-065-SD-MRCC Database File of Evap Data 1963-2002

Document Title:	Database File of Evaporation Data, 1963-2002
Originating Organization:	Midwest Regional Climate Center
Author:	
Document No:	
Volume/Page/Date:	2002
Site Data obtained from:	
Describe the relevance of the reference to the report topic.	
SSAR Section 2.4: Evaporation data.	
[Also used for ER-086. erg 20031024]	

DSET	COOPID	WBNID	CD	ELEM	UN	YEARMO	DAHR	DAY01	DAHR	DAY02	DAHR	DAY03	DAHR	DAY04	DAHR	DAY05	DAHR	DAY06	DAHR	DAY07	DAHR	DAY08
3200	118740	99999	5	EVAP	HI	196308	118	10	218	26	318	27	418	29	518	27	618	17	718	7	818	28
3200	118740	99999	5	EVAP	HI	196309	118	11	218	19	318	9	418	13	518	15	618	17	718	14	818	11
3200	118740	99999	5	EVAP	HI	196310	118	18	218	26	318	32	418	20	518	16	618	21	718	29	818	25
3200	118740	99999	5	EVAP	HI	196404	118	8	218	10	318	13	418	14	518	10	618	3	718	21	818	15
3200	118740	99999	5	EVAP	HI	196405	118	4	218	14	318	16	418	36	518	26	618	28	718	25	818	24
3200	118740	99999	5	EVAP	HI	196406	118	36	218	21	318	13	418	34	599	-99999	618	4	718	2	818	26
3200	118740	99999	5	EVAP	HI	196407	118	24	218	32	318	35	418	19	518	23	618	36	718	10	818	11
3200	118740	99999	5	EVAP	HI	196408	118	23	218	31	318	33	418	32	518	34	618	34	718	28	818	38
3200	118740	99999	5	EVAP	HI	196409	118	24	218	21	318	23	418	26	518	29	618	18	718	29	818	25
3200	118740	99999	5	EVAP	HI	196410	118	16	218	12	318	16	418	15	518	29	618	13	718	12	818	25
3200	118740	99999	5	EVAP	HI	196504	118	14	218	4	318	11	418	7	518	5	699	-99999	718	21	818	24
3200	118740	99999	5	EVAP	HI	196505	118	26	218	33	318	45	418	34	518	22	618	18	718	10	818	23
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3200	118740	99999	5	EVAP	HI	196507	118	29	299	-99999	318	15	418	21	518	27	618	26	718	26	818	19
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3200	118740	99999	5	EVAP	HI	196609	118	21	218	25	318	27	418	17	518	36	618	25	718	24	818	23
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3200	118740	99999	5	EVAP	HI	197105	118	24	218	35	318	11	418	25	518	23	618	14	718	14	818	19
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DSET	COOPID	WBNID	CD	ELEM	UN	YEARMO	DAHR	DAY01	DAHR	DAY02	DAHR	DAY03	DAHR	DAY04	DAHR	DAY05	DAHR	DAY06	DAHR	DAY07	DAHR	DAY08
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3200	118740	99999	5	EVAP	HI	197108	118	22	218	24	318	25	418	38	518	9	618	24	718	32	818	16
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3200	118740	99999	5	EVAP	HI	197209	118	22	218	12	318	7	418	9	518	19	618	16	718	31	899	-99999
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3200	118740	99999	5	EVAP	HI	197910	118	10	218	12	318	3	418	5	518	9	618	9	718	6	818	12
3200	118740	99999	5	EVAP	HI	198004	199	-99999	299	-99999	318	8	418	5	518	2	618	11	718	16	818	11

DSET	COOPID	WBNID	CD	ELEM	UN	YEARMO	DAHR	DAY01	DAHR	DAY02	DAHR	DAY03	DAHR	DAY04	DAHR	DAY05	DAHR	DAY06	DAHR	DAY07	DAHR	DAY08
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3200	118740	99999	5	EVAP	HI	198007	118	22	218	17	318	18	499	-99999	599	-99999	618	21	718	27	818	14
3200	118740	99999	5	EVAP	HI	198008	118	19	218	20	399	-99999	418	25	518	22	618	12	718	14	818	20
3200	118740	99999	5	EVAP	HI	198009	118	12	218	11	318	12	418	16	518	9	618	5	718	25	818	17
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3200	118740	99999	5	EVAP	HI	198109	118	13	218	6	318	5	418	3	599	-99999	618	10	799	-99999	899	-99999
3200	118740	99999	5	EVAP	HI	198110	118	13	218	20	318	13	418	9	518	7	618	31	718	15	818	22
3200	118740	99999	5	EVAP	HI	198204	199	-99999	299	-99999	307	7	407	15	507	15	699	-99999	799	-99999	899	-99999
3200	118740	99999	5	EVAP	HI	198205	107	7	207	16	307	17	407	22	507	22	607	24	707	22	807	10
3200	118740	99999	5	EVAP	HI	198206	107	24	207	19	307	17	407	17	507	2	607	8	707	25	807	7
3200	118740	99999	5	EVAP	HI	198207	107	21	207	13	399	-99999	407	3	507	29	607	16	707	24	807	24
3200	118740	99999	5	EVAP	HI	198208	107	19	207	19	307	20	407	24	507	21	607	17	707	15	807	8
3200	118740	99999	5	EVAP	HI	198209	107	6	207	16	307	24	407	18	599	-99999	699	-99999	707	8	807	12
3200	118740	99999	5	EVAP	HI	198210	107	13	207	20	307	2	407	10	507	7	607	12	707	16	807	12
3200	118740	99999	5	EVAP	HI	198308	107	29	207	20	307	26	407	10	507	16	607	20	707	20	807	29
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3200	118740	99999	5	EVAP	HI	198310	107	5	207	24	307	18	407	5	507	15	607	4	707	26	807	10
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3200	118740	99999	5	EVAP	HI	198406	107	25	207	24	307	24	407	34	507	16	607	31	707	25	807	21
3200	118740	99999	5	EVAP	HI	198407	107	20	207	20	307	22	407	44	507	7	607	12	707	28	899	-99999
3200	118740	99999	5	EVAP	HI	198408	107	14	207	19	307	18	407	12	507	17	607	17	707	22	807	25
3200	118740	99999	5	EVAP	HI	198409	107	25	207	21	307	21	407	14	507	13	607	15	707	9	807	22
3200	118740	99999	5	EVAP	HI	198505	107	10	207	21	307	12	407	12	507	32	607	19	707	11	807	19
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3200	118740	99999	5	EVAP	HI	198507	107	29	207	14	307	27	407	19	507	23	607	15	707	16	807	36
3200	118740	99999	5	EVAP	HI	198508	107	13	207	15	307	15	499	-99999	599	-99999	699	-99999	799	-99999	807	27
3200	118740	99999	5	EVAP	HI	198510	199	-99999	299	-99999	399	-99999	499	-99999	599	-99999	699	-99999	799	-99999	899	-99999
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3200	118740	99999	5	EVAP	HI	198610	199	-99999	207	18	399	-99999	407	16	507	12	607	20	707	9	807	14
3200	118740	99999	5	EVAP	HI	198611	107	8	207	1	307	11	499	-99999	507	4	607	1	707	1	807	5
3200	118740	99999	5	EVAP	HI	198703	199	-99999	299	-99999	399	-99999	499	-99999	599	-99999	699	-99999	799	-99999	899	-99999
3200	118740	99999	5	EVAP	HI	198704	199	-99999	299	-99999	399	-99999	499	-99999	599	-99999	607	20	707	19	807	23
3200	118740	99999	5	EVAP	HI	198705	107	23	207	23	307	11	407	24	507	10	607	18	707	48	807	46
3200	118740	99999	5	EVAP	HI	198706	107	29	207	29	307	22	407	32	507	27	607	23	707	22	807	50
3200	118740	99999	5	EVAP	HI	198707	199	-99999	207	11	307	13	407	48	507	4	607	19	707	17	807	24
3200	118740	99999	5	EVAP	HI	198708	199	-99999	299	-99999	399	-99999	407	35	507	16	607	23	707	20	807	23
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3200	118740	99999	5	EVAP	HI	198804	107	13	207	1	399	-99999	407	10	507	17	607	27	707	11	807	23
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3200	118740	99999	5	EVAP	HI	198807	107	33	207	26	399	-99999	407	59	599	-99999	607	31	707	30	807	34
3200	118740	99999	5	EVAP	HI	198808	199	-99999	207	24	307	34	407	15	507	23	607	18	799	-99999	807	45
3200	118740	99999	5	EVAP	HI	198809	107	23	207	22	307	12	499	-99999	507	21	607	18	707	15	807	19
3200	118740	99999	5	EVAP	HI	198810	107	7	299	-99999	307	7	407	12	507	12	607	9	707	7	807	13
3200	118740	99999	5	EVAP	HI	198904	199	-99999	299	-99999	399	-99999	499	-99999	599	-99999	699	-99999	799	-99999	899	-99999
3200	118740	99999	5	EVAP	HI	198905	107	24	207	18	307	11	407	17	507	4	607	20	799	-99999	807	25

DSET	COOPID	WBNID	CD	ELEM	UN	YEARMO	DAHR	DAY01	DAHR	DAY02	DAHR	DAY03	DAHR	DAY04	DAHR	DAY05	DAHR	DAY06	DAHR	DAY07	DAHR	DAY08
3200	118740	99999	5	EVAP	HI	198906	107	26	207	14	307	21	499	-99999	507	29	607	19	707	21	807	23
3200	118740	99999	5	EVAP	HI	198907	107	24	299	-99999	307	41	499	-99999	507	21	607	36	707	25	807	24
3200	118740	99999	5	EVAP	HI	198908	107	19	207	18	307	19	407	28	507	29	699	-99999	707	47	807	19
3200	118740	99999	5	EVAP	HI	198909	199	-99999	299	-99999	399	-99999	407	45	507	10	607	12	707	6	807	13
3200	118740	99999	5	EVAP	HI	199005	107	19	207	19	307	13	407	0	507	8	699	-99999	799	-99999	807	25
3200	118740	99999	5	EVAP	HI	199006	107	22	207	31	399	-99999	407	31	507	13	607	11	707	9	807	15
3200	118740	99999	5	EVAP	HI	199007	199	-99999	207	46	307	22	407	28	507	35	607	27	707	25	899	-99999
3200	118740	99999	5	EVAP	HI	199008	107	23	207	19	307	36	407	3	599	-99999	607	32	707	21	807	20
3200	118740	99999	5	EVAP	HI	199009	107	20	299	-99999	307	36	407	17	507	17	607	23	707	27	807	7
3200	118740	99999	5	EVAP	HI	199010	107	19	207	12	307	10	407	19	507	19	607	19	707	99999	807	28
3200	118740	99999	5	EVAP	HI	199010	107	19	207	12	307	10	407	19	507	19	607	19	799	-99999	807	28
3200	118740	99999	5	EVAP	HI	199104	199	-99999	299	-99999	399	-99999	499	-99999	599	-99999	607	16	799	-99999	807	38
3200	118740	99999	5	EVAP	HI	199105	107	24	207	23	307	24	407	9	507	99999	699	-99999	707	12	807	11
3200	118740	99999	5	EVAP	HI	199106	107	27	207	99999	307	50	407	30	599	-99999	607	28	707	26	807	26
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3200	118740	99999	5	EVAP	HI	199108	107	27	207	27	307	27	407	99999	507	44	607	3	707	8	807	21
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3200	118740	99999	5	EVAP	HI	199305	107	17	207	99999	307	13	407	3	507	10	607	15	707	17	807	22
3200	118740	99999	5	EVAP	HI	199306	107	15	207	17	307	5	407	9	507	14	607	18	707	13	807	17
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3200	118740	99999	5	EVAP	HI	199404	199	-99999	207	20	399	-99999	499	-99999	507	142	607	6	799	-99999	807	3
3200	118740	99999	5	EVAP	HI	199405	107	99999	207	23	307	12	407	15	507	14	607	22	799	-99999	807	99999
3200	118740	99999	5	EVAP	HI	199406	107	29	207	25	307	12	407	23	507	99999	607	48	707	23	807	33
3200	118740	99999	5	EVAP	HI	199407	107	21	207	24	307	99999	407	31	507	31	607	35	707	24	807	22
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3200	118740	99999	5	EVAP	HI	199505	107	4	207	7	307	14	407	13	507	5	607	18	707	99999	807	38
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3200	118740	99999	5	EVAP	HI	199509	107	18	207	34	307	99999	407	25	507	19	607	19	707	20	807	8
3200	118740	99999	5	EVAP	HI	199605	199	-99999	207	19	307	12	407	17	507	99999	607	9	707	11	807	3
3200	118740	99999	5	EVAP	HI	199606	107	21	207	99999	307	30	407	12	507	13	607	23	707	10	807	28
3200	118740	99999	5	EVAP	HI	199607	199	-99999	207	20	307	33	407	13	507	40	607	27	707	99999	807	51
3200	118740	99999	5	EVAP	HI	199608	107	24	207	17	307	20	407	99999	507	38	607	25	707	26	807	25
3200	118740	99999	5	EVAP	HI	199609	107	99999	207	37	307	16	407	13	507	12	607	34	707	13	807	99999
3200	118740	99999	5	EVAP	HI	199610	107	14	207	12	307	19	407	14	507	10	607	99999	707	24	807	12
3200	118740	99999	5	EVAP	HI	199704	199	-99999	299	-99999	307	23	407	16	507	2	607	99999	707	37	807	22
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3200	118740	99999	5	EVAP	HI	199709	199	-99999	207	11	307	21	407	18	507	13	607	18	707	99999	807	31
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3200	118740	99999	5	EVAP	HI	199804	107	11	207	11	307	7	407	7	507	99999	607	22	707	14	807	4
3200	118740	99999	5	EVAP	HI	199805	107	3	207	29	399	-99999	499	-99999	507	7	607	18	707	4	807	7
3200	118740	99999	5	EVAP	HI	199806	107	57	207	22	307	37	407	10	507	7	607	16	799	-99999	807	22
3200	118740	99999	5	EVAP	HI	199807	107	23	207	19	307	25	407	24	507	99999	607	41	707	11	807	14
3200	118740	99999	5	EVAP	HI	199808	107	18	207	99999	307	44	407	9	507	15	607	7	707	13	807	6
3200	118740	99999	5	EVAP	HI	199809	199	-99999	207	13	307	23	407	19	507	23	607	99999	707	49	807	17

DSET	COOPID	WBNID	CD	ELEM	UN	YEARMO	DAHR	DAY01	DAHR	DAY02	DAHR	DAY03	DAHR	DAY04	DAHR	DAY05	DAHR	DAY06	DAHR	DAY07	DAHR	DAY08
3200	118740	99999	5	EVAP	HI	199810	107	16	207	13	307	9	407	99999	507	6	607	14	707	9	807	10
3200	118740	99999	5	EVAP	HI	199904	199	-99999	299	-99999	399	-99999	499	-99999	599	-99999	699	-99999	799	-99999	807	25
3200	118740	99999	5	EVAP	HI	199905	107	20	207	99999	307	42	407	20	507	27	607	18	707	12	807	14
3200	118740	99999	5	EVAP	HI	199906	107	15	207	28	307	12	407	15	507	22	607	99999	707	52	807	31
3200	118740	99999	5	EVAP	HI	199907	107	20	207	14	307	99999	407	99999	507	99999	607	99999	707	25	807	25
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3200	118740	99999	5	EVAP	HI	199909	107	14	207	15	307	19	407	21	507	99999	607	99999	707	64	807	19
3200	118740	99999	5	EVAP	HI	199910	107	15	207	99999	307	99999	407	18	507	14	607	99999	707	11	807	99999
3200	118740	99999	5	EVAP	HI	200004	199	-99999	299	-99999	399	-99999	499	-99999	507	15	607	22	707	22	807	12
3200	118740	99999	5	EVAP	HI	200005	199	-99999	207	2	307	17	407	16	507	23	607	25	707	99999	807	26
3200	118740	99999	5	EVAP	HI	200006	107	9	207	26	307	99999	407	50	507	12	607	15	707	15	807	29
3200	118740	99999	5	EVAP	HI	200007	107	99999	207	99999	307	61	407	99999	507	33	607	13	707	21	807	99999
3200	118740	99999	5	EVAP	HI	200010	199	-99999	299	-99999	307	20	407	18	507	8	607	6	707	99999	807	99999
3200	118740	99999	5	EVAP	HI	200011	107	9	207	12	307	4	407	99999	507	99999	607	28	707	1	807	5
3200	118740	99999	5	EVAP	HI	200104	199	-99999	299	-99999	399	-99999	499	-99999	599	-99999	699	-99999	799	-99999	899	-99999
3200	118740	99999	5	EVAP	HI	200105	107	29	207	29	307	25	407	26	599	-99999	699	-99999	707	51	807	6
3200	118740	99999	5	EVAP	HI	200106	107	2	207	99999	307	99999	407	36	507	7	699	-99999	707	10	807	17
3200	118740	99999	5	EVAP	HI	200107	107	99999	207	68	307	20	407	99999	599	-99999	607	29	707	99999	807	99999
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3200	118740	99999	5	EVAP	HI	200109	107	99999	207	99999	307	99999	407	73	507	24	607	18	707	18	899	-99999
3200	118740	99999	5	EVAP	HI	200110	107	31	207	18	307	24	407	24	507	8	607	99999	707	99999	807	99999
3202	118740	99999	5	EVAP	HI	200204	199	-99999	299	-99999	399	-99999	499	-99999	599	-99999	699	-99999	799	-99999	899	-99999
3201	118740	99999	5	EVAP	HI	200204	199	-99999	299	-99999	399	-99999	499	-99999	599	-99999	699	-99999	799	-99999	899	-99999
3201	118740	99999	5	EVAP	HI	200205	107	11	207	9	307	13	407	99999	507	99999	607	59	707	13	807	13
3201	118740	99999	5	EVAP	HI	200206	107	99999	207	99999	307	72	407	26	507	28	607	9	707	8	807	99999

YEARMO	DAHR	DAY09	DAHR	DAY10	DAHR	DAY11	DAHR	DAY12	DAHR	DAY13	DAHR	DAY14	DAHR	DAY15	DAHR	DAY16	DAHR	DAY17	DAHR	DAY18	DAHR	DAY19	DAHR
196308	918	9	1018	19	1118	16	1218	27	1318	3	1418	18	1518	22	1618	17	1718	23	1818	13	1918	10	2018
196309	918	20	1018	20	1118	22	1218	13	1318	20	1418	20	1518	16	1618	16	1718	21	1818	19	1918	24	2018
196310	918	20	1018	18	1118	35	1218	16	1318	28	1418	14	1518	20	1618	21	1718	23	1818	18	1918	11	2018
196404	918	4	1018	17	1118	18	1218	19	1318	12	1418	29	1518	23	1618	21	1718	37	1818	38	1918	8	2099
196405	918	27	1018	20	1118	35	1218	5	1318	19	1418	9	1518	23	1618	27	1718	12	1818	37	1918	39	2018
196406	918	37	1018	45	1118	38	1218	27	1318	29	1418	12	1518	39	1618	28	1718	26	1818	16	1918	26	2099
196407	918	17	1018	21	1118	13	1218	25	1318	21	1418	20	1518	19	1618	25	1718	25	1818	19	1918	12	2018
196408	918	26	1018	34	1118	24	1218	37	1318	16	1418	25	1518	25	1618	19	1718	35	1818	23	1918	26	2018
196409	918	26	1018	26	1118	30	1218	14	1318	18	1418	20	1518	22	1618	16	1718	6	1818	16	1918	12	2018
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YEARMO	DAHR	DAY09	DAHR	DAY10	DAHR	DAY11	DAHR	DAY12	DAHR	DAY13	DAHR	DAY14	DAHR	DAY15	DAHR	DAY16	DAHR	DAY17	DAHR	DAY18	DAHR	DAY19	DAHR
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YEARMO	DAHR	DAY09	DAHR	DAY10	DAHR	DAY11	DAHR	DAY12	DAHR	DAY13	DAHR	DAY14	DAHR	DAY15	DAHR	DAY16	DAHR	DAY17	DAHR	DAY18	DAHR	DAY19	DAHR
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YEARMO	DAHR	DAY09	DAHR	DAY10	DAHR	DAY11	DAHR	DAY12	DAHR	DAY13	DAHR	DAY14	DAHR	DAY15	DAHR	DAY16	DAHR	DAY17	DAHR	DAY18	DAHR	DAY19	DAHR
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YEARMO	DAHR	DAY09	DAHR	DAY10	DAHR	DAY11	DAHR	DAY12	DAHR	DAY13	DAHR	DAY14	DAHR	DAY15	DAHR	DAY16	DAHR	DAY17	DAHR	DAY18	DAHR	DAY19	DAHR
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198308	25	2107	31	2207	19	2307	5	2407	18	2599	-99999	2699	-99999	2707	24	2807	15	2907	20	3007	8	3107	18
198309	7	2107	9	2207	9	2307	9	2407	9	2507	7	2607	2	2707	12	2807	24	2907	12	3007	16	3199	-99999
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198406	28	2107	23	2207	5	2307	22	2407	32	2507	26	2607	28	2707	21	2807	30	2907	22	3007	26	3199	-99999
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198409	18	2107	19	2207	17	2307	4	2407	4	2507	6	2607	10	2707	14	2807	4	2907	9	3007	12	3199	-99999
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198508	14	2107	16	2207	14	2307	9	2407	7	2507	17	2607	7	2799	-99999	2899	-99999	2999	-99999	3099	-99999	3199	-99999
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198804	20	2107	17	2207	8	2307	11	2499	-99999	2507	32	2607	16	2707	19	2807	9	2907	21	3007	27	3199	-99999
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198905	13	2199	-99999	2207	37	2307	3	2407	23	2507	20	2699	-99999	2707	22	2899	-99999	2907	33	3007	19	3107	27

YEARMO	DAY20	DAHR	DAY21	DAHR	DAY22	DAHR	DAY23	DAHR	DAY24	DAHR	DAY25	DAHR	DAY26	DAHR	DAY27	DAHR	DAY28	DAHR	DAY29	DAHR	DAY30	DAHR	DAY31
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199306	99999	2107	43	2207	22	2307	27	2407	30	2507	25	2607	15	2707	99999	2807	54	2907	14	3007	23	3199	-99999
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199406	58	2107	28	2207	33	2307	26	2407	24	2507	9	2607	99999	2707	30	2807	23	2907	31	3007	27	3199	-99999
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199408	29	2107	99999	2207	23	2307	16	2407	15	2507	22	2607	20	2707	9	2807	99999	2907	33	3007	15	3107	6
199409	17	2107	19	2207	18	2307	4	2407	4	2599	-99999	2699	-99999	2799	-99999	2807	8	2907	14	3007	14	3199	-99999
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199506	29	2107	26	2207	21	2307	21	2407	22	2507	99999	2607	30	2707	21	2807	16	2907	41	3007	19	3199	-99999
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199607	28	2107	99999	2207	29	2307	15	2407	29	2507	22	2607	23	2707	23	2807	99999	2907	39	3007	23	3107	22
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199706	29	2107	22	2207	99999	2307	37	2407	29	2507	30	2607	25	2707	28	2807	29	2907	99999	3007	42	3199	-99999
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199808	20	2107	20	2207	21	2307	99999	2407	45	2507	27	2607	23	2707	18	2807	17	2907	8	3007	99999	3107	47
199809	99999	2107	36	2207	17	2307	17	2407	15	2507	0	2607	15	2707	99999	2807	49	2907	14	3007	14	3199	-99999

YEARMO	DAY20	DAHR	DAY21	DAHR	DAY22	DAHR	DAY23	DAHR	DAY24	DAHR	DAY25	DAHR	DAY26	DAHR	DAY27	DAHR	DAY28	DAHR	DAY29	DAHR	DAY30	DAHR	DAY31
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199904	11	2107	11	2207	15	2307	13	2407	10	2507	99999	2607	34	2707	6	2807	6	2907	11	3007	23	3199	-99999
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200108	47	2107	17	2207	13	2307	28	2407	13	2507	99999	2607	99999	2707	41	2807	22	2907	21	3007	17	3107	32
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RAI ATTACHMENT

RAI 2.4.1-5 Attachment 2 (MRCC 2002b)

(Note – This attachment provided on the enclosed CD-ROM.)

See file: RAI 2.4.1-5 Attachment 2 (MRCC 2002b).pdf

Technical Editing Guidance Reference Source Documentation

Source Document No. SSAR-066-SD-MRCC Database File of Rainfall Data 1910-2002

Document Title:	Database File of Rainfall Data, 1910-2002
Originating Organization:	Midwest Regional Climate Center
Author:	
Document No:	
Volume/Page/Date:	2002
Site Data obtained from:	
Describe the relevance of the reference to the report topic.	
SSAR Section 2.4: Rainfall data.	
[Also used for ER-087. erg 20031024]	

DSET	COOPID	WBNID	CD	ELEM	UN	YEARMO	DAHR	DAY01	DAHR	DAY02	DAHR	DAY03	DAHR	DAY04	DAHR	DAY05	DAHR	DAY06	DAHR	DAY07	DAHR	DAY08	DAHR
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DSET	COOPID	WBNID	CD	ELEM	UN	YEARMO	DAHR	DAY01	DAHR	DAY02	DAHR	DAY03	DAHR	DAY04	DAHR	DAY05	DAHR	DAY06	DAHR	DAY07	DAHR	DAY08	DAHR
3200	118740	99999	5	EVAP	HI	198205	107	7	207	16	307	17	407	22	507	22	607	24	707	22	807	10	907
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3200	118740	99999	5	EVAP	HI	198207	107	21	207	13	399	-99999	407	3	507	29	607	16	707	24	807	24	907
3200	118740	99999	5	EVAP	HI	198208	107	19	207	19	307	20	407	24	507	21	607	17	707	15	807	8	907
3200	118740	99999	5	EVAP	HI	198209	107	6	207	16	307	24	407	18	599	-99999	699	-99999	707	8	807	12	907
3200	118740	99999	5	EVAP	HI	198210	107	13	207	20	307	2	407	10	507	7	607	12	707	16	807	12	907
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3200	118740	99999	5	EVAP	HI	198406	107	25	207	24	307	24	407	34	507	16	607	31	707	25	807	21	907
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3200	118740	99999	5	EVAP	HI	198704	199	-99999	299	-99999	399	-99999	499	-99999	599	-99999	607	20	707	19	807	23	999
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3200	118740	99999	5	EVAP	HI	198709	107	22	207	18	307	15	407	24	507	7	699	-99999	707	43	807	0	907
3200	118740	99999	5	EVAP	HI	198710	107	17	207	23	307	11	407	7	507	22	607	10	707	5	899	-99999	999
3200	118740	99999	5	EVAP	HI	198804	107	13	207	1	399	-99999	407	10	507	17	607	27	707	11	807	23	907
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3200	118740	99999	5	EVAP	HI	198807	107	33	207	26	399	-99999	407	59	599	-99999	607	31	707	30	807	34	907
3200	118740	99999	5	EVAP	HI	198808	199	-99999	207	24	307	34	407	15	507	23	607	18	799	-99999	807	45	907
3200	118740	99999	5	EVAP	HI	198809	107	23	207	22	307	12	499	-99999	507	21	607	18	707	15	807	19	907
3200	118740	99999	5	EVAP	HI	198810	107	7	299	-99999	307	7	407	12	507	12	607	9	707	7	807	13	999
3200	118740	99999	5	EVAP	HI	198904	199	-99999	299	-99999	399	-99999	499	-99999	599	-99999	699	-99999	799	-99999	899	-99999	999
3200	118740	99999	5	EVAP	HI	198905	107	24	207	18	307	11	407	17	507	4	607	20	799	-99999	807	25	907
3200	118740	99999	5	EVAP	HI	198906	107	26	207	14	307	21	499	-99999	507	29	607	19	707	21	807	23	907
3200	118740	99999	5	EVAP	HI	198907	107	24	299	-99999	307	41	499	-99999	507	21	607	36	707	25	807	24	999
3200	118740	99999	5	EVAP	HI	198908	107	19	207	18	307	19	407	28	507	29	699	-99999	707	47	807	19	907
3200	118740	99999	5	EVAP	HI	198909	199	-99999	299	-99999	399	-99999	407	45	507	10	607	12	707	6	807	13	999
3200	118740	99999	5	EVAP	HI	199005	107	19	207	19	307	13	407	0	507	8	699	-99999	799	-99999	807	25	907
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3200	118740	99999	5	EVAP	HI	199105	107	24	207	23	307	24	407	9	507	99999	699	-99999	707	12	807	11	907
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3200	118740	99999	5	EVAP	HI	199109	107	99999	207	35	307	14	407	14	507	23	607	20	707	22	807	99999	907
3200	118740	99999	5	EVAP	HI	199205	107	19	207	37	307	99999	407	48	507	14	607	12	707	21	807	17	907
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DSET	COOPID	WBNID	CD	ELEM	UN	YEARMO	DAHR	DAY01	DAHR	DAY02	DAHR	DAY03	DAHR	DAY04	DAHR	DAY05	DAHR	DAY06	DAHR	DAY07	DAHR	DAY08	DAHR
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3200	118740	99999	5	EVAP	HI	199209	107	25	207	6	307	3	407	19	507	18	607	12	707	10	807	18	907
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3200	118740	99999	5	EVAP	HI	199305	107	17	207	99999	307	13	407	3	507	10	607	15	707	17	807	22	907
3200	118740	99999	5	EVAP	HI	199306	107	15	207	17	307	5	407	9	507	14	607	18	707	13	807	17	907
3200	118740	99999	5	EVAP	HI	199307	107	27	207	14	307	24	407	99999	507	43	607	47	707	17	807	13	907
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3200	118740	99999	5	EVAP	HI	199610	107	14	207	12	307	19	407	14	507	10	607	99999	707	24	807	12	907
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3200	118740	99999	5	EVAP	HI	199805	107	3	207	29	399	-99999	499	-99999	507	7	607	18	707	4	807	7	907
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3200	118740	99999	5	EVAP	HI	200108	107	24	207	22	307	16	407	99999	507	99999	607	66	707	24	807	24	907
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3202	118740	99999	5	EVAP	HI	200204	199	-99999	299	-99999	399	-99999	499	-99999	599	-99999	699	-99999	799	-99999	899	-99999	999
3201	118740	99999	5	EVAP	HI	200204	199	-99999	299	-99999	399	-99999	499	-99999	599	-99999	699	-99999	799	-99999	899	-99999	999
3201	118740	99999	5	EVAP	HI	200205	107	11	207	9	307	13	407	99999	507	99999	607	59	707	13	807	13	907
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YEARMO	DAY09	DAHR	DAY10	DAHR	DAY11	DAHR	DAY12	DAHR	DAY13	DAHR	DAY14	DAHR	DAY15	DAHR	DAY16	DAHR	DAY17	DAHR	DAY18	DAHR	DAY19	DAHR	DAY20
196308	9	1018	19	1118	16	1218	27	1318	3	1418	18	1518	22	1618	17	1718	23	1818	13	1918	10	2018	4
196309	20	1018	20	1118	22	1218	13	1318	20	1418	20	1518	16	1618	16	1718	21	1818	19	1918	24	2018	26
196310	20	1018	18	1118	35	1218	16	1318	28	1418	14	1518	20	1618	21	1718	23	1818	18	1918	11	2018	12
196404	4	1018	17	1118	18	1218	19	1318	12	1418	29	1518	23	1618	21	1718	37	1818	38	1918	8	2099	-99999
196405	27	1018	20	1118	35	1218	5	1318	19	1418	9	1518	23	1618	27	1718	12	1818	37	1918	39	2018	44
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YEARMO	DAY09	DAHR	DAY10	DAHR	DAY11	DAHR	DAY12	DAHR	DAY13	DAHR	DAY14	DAHR	DAY15	DAHR	DAY16	DAHR	DAY17	DAHR	DAY18	DAHR	DAY19	DAHR	DAY20
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YEARMO	DAHR	DAY21	DAHR	DAY22	DAHR	DAY23	DAHR	DAY24	DAHR	DAY25	DAHR	DAY26	DAHR	DAY27	DAHR	DAY28	DAHR	DAY29	DAHR	DAY30	DAHR	DAY31
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YEARMO	DAHR	DAY21	DAHR	DAY22	DAHR	DAY23	DAHR	DAY24	DAHR	DAY25	DAHR	DAY26	DAHR	DAY27	DAHR	DAY28	DAHR	DAY29	DAHR	DAY30	DAHR	DAY31
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198308	2107	31	2207	19	2307	5	2407	18	2599	-99999	2699	-99999	2707	24	2807	15	2907	20	3007	8	3107	18
198309	2107	9	2207	9	2307	9	2407	9	2507	7	2607	2	2707	12	2807	24	2907	12	3007	16	3199	-99999
198310	2199	-99999	2207	12	2307	12	2407	2	2507	7	2607	7	2707	11	2807	13	2907	8	3007	5	3107	2
198311	2107	5	2299	-99999	2399	-99999	2499	-99999	2599	-99999	2699	-99999	2799	-99999	2899	-99999	2999	-99999	3099	-99999	3199	-99999
198405	2107	18	2207	7	2399	-99999	2407	20	2507	23	2607	12	2707	16	2807	15	2907	3	3007	17	3107	20
198406	2107	23	2207	5	2307	22	2407	32	2507	26	2607	28	2707	21	2807	30	2907	22	3007	26	3199	-99999
198407	2107	7	2207	20	2307	23	2407	20	2507	20	2607	4	2707	18	2807	17	2907	17	3007	20	3107	22
198408	2107	22	2207	18	2307	24	2407	12	2507	17	2607	12	2707	12	2807	9	2907	24	3007	18	3107	29
198409	2107	19	2207	17	2307	4	2407	4	2507	6	2607	10	2707	14	2807	4	2907	9	3007	12	3199	-99999
198505	2107	34	2207	15	2307	24	2407	28	2507	8	2699	-99999	2707	41	2807	10	2907	22	3007	20	3107	15
198506	2107	25	2207	29	2399	-99999	2407	45	2507	18	2607	20	2707	8	2899	-99999	2907	4	3007	11	3199	-99999
198507	2107	6	2207	17	2307	27	2407	20	2507	20	2607	11	2707	24	2807	20	2907	21	3007	17	3107	14
198508	2107	16	2207	14	2307	9	2407	7	2507	17	2607	7	2799	-99999	2899	-99999	2999	-99999	3099	-99999	3199	-99999
198510	2107	8	2207	5	2307	5	2407	10	2507	13	2607	7	2707	12	2807	17	2907	13	3007	2	3107	10
198604	2107	6	2207	9	2307	13	2407	22	2507	23	2607	27	2707	25	2807	41	2907	5	3007	23	3199	-99999
198605	2107	18	2207	13	2307	21	2407	19	2507	13	2607	41	2707	26	2807	16	2907	15	3007	20	3107	22
198606	2107	28	2207	24	2307	42	2407	23	2507	32	2607	23	2707	25	2807	33	2907	16	3007	27	3199	-99999
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198608	2107	28	2207	26	2307	18	2407	25	2507	17	2607	24	2707	26	2807	21	2907	21	3007	16	3107	14
198609	2107	1	2207	40	2307	23	2407	6	2507	11	2607	18	2707	10	2807	1	2907	5	3007	19	3199	-99999
198610	2107	7	2207	8	2307	8	2407	2	2507	4	2607	1	2707	0	2807	4	2907	10	3007	4	3107	7
198611	2199	-99999	2299	-99999	2399	-99999	2499	-99999	2599	-99999	2699	-99999	2799	-99999	2899	-99999	2999	-99999	3099	-99999	3199	-99999
198703	2107	19	2207	10	2307	20	2407	27	2507	3	2607	0	2799	-99999	2807	3	2907	6	3099	-99999	3199	-99999
198704	2107	14	2299	-99999	2307	24	2499	-99999	2507	15	2607	4	2799	-99999	2807	18	2907	31	3007	36	3199	-99999
198705	2107	15	2207	42	2307	22	2407	16	2599	-99999	2607	38	2707	29	2807	31	2907	33	3007	34	3107	9
198706	2107	8	2207	40	2307	23	2407	18	2507	12	2607	31	2707	31	2807	9	2907	46	3007	41	3199	-99999
198707	2107	26	2207	23	2307	21	2407	21	2507	23	2607	17	2707	35	2807	7	2907	14	3099	-99999	3199	-99999
198708	2107	20	2207	8	2307	9	2407	34	2507	13	2607	5	2799	-99999	2899	-99999	2907	14	3007	8	3107	30
198709	2107	17	2207	25	2307	2	2407	17	2507	18	2699	-99999	2707	12	2807	27	2907	13	3007	27	3199	-99999
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198804	2107	17	2207	8	2307	11	2499	-99999	2507	32	2607	16	2707	19	2807	9	2907	21	3007	27	3199	-99999
198805	2107	22	2299	-99999	2307	33	2407	16	2507	30	2607	18	2707	26	2807	31	2999	-99999	3007	59	3107	29
198806	2107	39	2207	41	2307	37	2407	39	2507	24	2699	-99999	2707	84	2807	31	2907	35	3007	12	3199	-99999
198807	2107	9	2207	27	2307	22	2499	-99999	2599	-99999	2607	71	2707	23	2807	25	2907	26	3007	23	3199	-99999
198808	2199	-99999	2207	34	2307	12	2407	24	2507	28	2607	37	2707	18	2899	-99999	2907	18	3007	18	3107	20
198809	2107	31	2207	1	2307	23	2407	18	2599	-99999	2607	22	2707	16	2807	16	2907	14	3007	12	3199	-99999
198810	2107	2	2207	7	2399	-99999	2407	15	2507	9	2607	3	2799	-99999	2899	-99999	2999	-99999	3099	-99999	3199	-99999
198904	2107	15	2207	20	2399	-99999	2407	18	2507	18	2607	19	2707	20	2807	28	2907	21	3099	-99999	3199	-99999
198905	2199	-99999	2207	37	2307	3	2407	23	2507	20	2699	-99999	2707	22	2899	-99999	2907	33	3007	19	3107	27
198906	2107	20	2207	28	2307	26	2407	29	2599	-99999	2607	54	2799	-99999	2807	20	2907	33	3007	25	3199	-99999
198907	2107	5	2207	14	2399	-99999	2407	36	2507	19	2607	19	2707	21	2807	29	2907	27	3099	-99999	3107	20
198908	2107	31	2207	11	2307	15	2407	21	2507	10	2607	6	2799	-99999	2807	25	2999	-99999	3099	-99999	3107	17
198909	2107	11	2207	11	2307	18	2499	-99999	2507	11	2607	20	2707	16	2807	11	2907	14	3007	15	3199	-99999
199005	2199	-99999	2207	5	2307	19	2407	1	2507	8	2607	6	2799	-99999	2899	-99999	2907	19	3007	27	3107	16
199006	2107	14	2207	26	2307	21	2499	-99999	2507	39	2607	27	2707	16	2807	28	2907	26	3007	21	3199	-99999
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199008	2107	14	2207	4	2307	10	2407	11	2599	-99999	2699	-99999	2707	49	2807	18	2907	31	3007	23	3107	21
199009	2107	12	2207	7	2399	-99999	2407	24	2507	15	2607	17	2707	15	2807	16	2907	9	3099	-99999	3199	-99999
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199104	2107	99999	2207	25	2307	16	2407	13	2507	14	2607	10	2707	13	2807	99999	2907	17	3007	12	3199	-99999
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199106	2107	28	2207	15	2307	99999	2407	34	2507	19	2607	24	2707	31	2807	14	2907	32	3099	-99999	3199	-99999
199107	2107	99999	2207	55	2307	36	2407	33	2507	11	2607	25	2707	30	2807	99999	2907	39	3007	16	3107	21
199108	2107	18	2207	24	2307	26	2407	25	2507	99999	2607	41	2707	23	2807	13	2907	22	3007	11	3107	16
199109	2107	12	2207	99999	2307	18	2407	13	2507	9	2607	17	2707	15	2807	6	2907	99999	3007	27	3199	-99999
199205	2107	20	2299	-99999	2307	10	2407	17	2507	17	2607	8	2707	7	2807	16	2907	25	3007	18	3199	-99999
199206	2107	99999	2207	37	2307	18	2407	23	2507	15	2607	37	2707	22	2807	99999	2907	41	3007	21	3199	-99999
199207	2107	5	2207	18	2307	5	2407	15	2507	18	2607	99999	2707	29	2807	12	2907	34	3007	19	3199	-99999

YEARMO	DAHR	DAY21	DAHR	DAY22	DAHR	DAY23	DAHR	DAY24	DAHR	DAY25	DAHR	DAY26	DAHR	DAY27	DAHR	DAY28	DAHR	DAY29	DAHR	DAY30	DAHR	DAY31
199208	2107	12	2207	19	2307	15	2407	17	2507	14	2607	21	2707	18	2807	7	2907	20	3007	99999	3107	39
199209	2107	10	2207	4	2307	23	2407	13	2507	11	2607	7	2707	99999	2807	23	2907	16	3007	9	3199	-99999
199210	2199	-99999	2299	-99999	2399	-99999	2499	-99999	2599	-99999	2699	-99999	2799	-99999	2899	-99999	2999	-99999	3099	-99999	3199	-99999
199305	2107	15	2207	21	2307	99999	2407	35	2507	25	2607	20	2707	25	2807	27	2907	24	3007	13	3107	13
199306	2107	43	2207	22	2307	27	2407	30	2507	25	2607	15	2707	99999	2807	54	2907	14	3007	23	3199	-99999
199307	2107	2	2207	35	2307	4	2407	16	2599	-99999	2699	-99999	2707	17	2807	20	2907	39	3007	27	3107	23
199308	2107	24	2207	99999	2307	25	2407	24	2507	11	2607	19	2707	22	2807	21	2907	99999	3007	37	3107	23
199309	2107	9	2207	9	2307	7	2499	-99999	2599	-99999	2699	-99999	2799	-99999	2899	-99999	2999	-99999	3099	-99999	3199	-99999
199404	2107	9	2207	8	2307	19	2499	-99999	2507	51	2607	26	2707	29	2807	22	2907	19	3007	2	3199	-99999
199405	2107	13	2207	99999	2307	62	2407	27	2507	43	2607	28	2707	13	2807	20	2907	99999	3007	55	3107	23
199406	2107	28	2207	33	2307	26	2407	24	2507	9	2607	99999	2707	30	2807	23	2907	31	3007	27	3199	-99999
199407	2107	35	2207	12	2307	7	2407	99999	2507	64	2607	26	2707	25	2807	18	2907	25	3007	19	3199	-99999
199408	2107	99999	2207	23	2307	16	2407	15	2507	22	2607	20	2707	9	2807	99999	2907	33	3007	15	3107	6
199409	2107	19	2207	18	2307	4	2407	4	2599	-99999	2699	-99999	2799	-99999	2807	8	2907	14	3007	14	3199	-99999
199505	2107	99999	2207	46	2307	22	2407	23	2507	6	2607	9	2707	12	2807	99999	2907	47	3007	8	3107	22
199506	2107	26	2207	21	2307	21	2407	22	2507	99999	2607	30	2707	21	2807	16	2907	41	3007	19	3199	-99999
199507	2107	4	2207	22	2307	99999	2407	26	2507	37	2607	24	2707	25	2807	30	2907	29	3007	99999	3107	50
199508	2107	33	2207	26	2307	23	2407	21	2507	19	2607	20	2707	99999	2807	34	2907	18	3007	21	3107	22
199509	2107	10	2207	8	2307	16	2407	99999	2507	23	2607	14	2707	18	2807	18	2907	17	3007	20	3199	-99999
199605	2107	30	2207	22	2307	11	2407	15	2507	8	2699	-99999	2799	-99999	2899	-99999	2907	10	3007	21	3107	20
199606	2107	24	2207	21	2307	99999	2407	44	2507	29	2607	26	2707	23	2807	25	2907	39	3099	-99999	3199	-99999
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199608	2107	22	2207	22	2307	21	2407	16	2507	99999	2607	39	2707	15	2807	16	2907	14	3007	18	3107	17
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199610	2107	9	2207	2	2307	4	2407	4	2507	8	2607	10	2707	99999	2807	13	2907	10	3007	13	3199	-99999
199704	2107	15	2207	14	2307	19	2407	13	2507	12	2607	35	2707	99999	2807	1	2907	13	3007	20	3199	-99999
199705	2107	20	2207	21	2307	21	2407	23	2507	99999	2607	24	2707	4	2807	16	2907	3	3007	0	3107	12
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199710	2199	-99999	2299	-99999	2399	-99999	2499	-99999	2599	-99999	2699	-99999	2799	-99999	2899	-99999	2999	-99999	3099	-99999	3199	-99999
199804	2107	16	2207	7	2307	10	2407	18	2507	23	2607	99999	2707	32	2807	15	2907	6	3007	11	3199	-99999
199805	2107	9	2207	17	2307	2	2499	-99999	2599	-99999	2699	-99999	2707	20	2807	19	2907	25	3007	25	3199	-99999
199806	2199	-99999	2207	41	2307	17	2407	22	2507	28	2607	33	2707	32	2899	-99999	2907	55	3007	24	3199	-99999
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199808	2107	20	2207	21	2307	99999	2407	45	2507	27	2607	23	2707	18	2807	17	2907	8	3007	99999	3107	47
199809	2107	36	2207	17	2307	17	2407	15	2507	0	2607	15	2707	99999	2807	49	2907	14	3007	14	3199	-99999
199810	2107	12	2207	11	2307	7	2407	4	2507	99999	2607	23	2707	10	2807	11	2907	3	3007	5	3107	8
199904	2107	11	2207	15	2307	13	2407	10	2507	99999	2607	34	2707	6	2807	6	2907	11	3007	23	3199	-99999
199905	2107	23	2207	19	2307	99999	2407	29	2507	20	2607	25	2707	17	2807	26	2907	28	3007	99999	3107	38
199906	2107	49	2207	17	2307	22	2407	15	2507	4	2607	99999	2707	99999	2807	52	2907	20	3007	15	3199	-99999
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199909	2107	20	2207	13	2307	17	2407	23	2507	14	2607	99999	2707	51	2807	17	2999	-99999	3099	-99999	3199	-99999
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200010	2107	99999	2207	99999	2307	22	2407	5	2507	6	2607	6	2707	10	2807	99999	2907	99999	3007	27	3107	9
200011	2199	-99999	2299	-99999	2399	-99999	2499	-99999	2599	-99999	2699	-99999	2799	-99999	2899	-99999	2999	-99999	3099	-99999	3199	-99999
200104	2107	99999	2207	99999	2307	57	2407	19	2507	19	2607	7	2707	25	2807	99999	2907	99999	3007	67	3199	-99999
200105	2107	46	2207	13	2307	18	2407	12	2507	13	2699	-99999	2799	-99999	2807	37	2907	18	3007	25	3107	13
200106	2107	14	2207	6	2307	99999	2407	99999	2507	59	2607	25	2707	22	2807	20	2907	24	3099	-99999	3199	-99999
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200108	2107	17	2207	13	2307	28	2407	13	2507	99999	2607	99999	2707	41	2807	22	2907	21	3007	17	3107	32
200109	2107	12	2207	99999	2307	99999	2407	44	2507	14	2607	12	2707	17	2807	14	2999	-99999	3099	-99999	3199	-99999
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200204	2199	-99999	2207	45	2307	5	2407	10	2507	15	2607	21	2707	99999	2807	99999	2907	75	3007	13	3199	-99999
200204	2199	-99999	2207	45	2307	5	2407	10	2507	15	2607	21	2707	99999	2807	99999	2907	75	3007	13	3199	-99999
200205	2107	16	2207	16	2307	23	2407	18	2507	99999	2607	99999	2707	46	2807	20	2907	17	3007	8	3107	23
200206	2107	23	2207	99999	2307	99999	2407	75	2507	20	2607	15	2707	29	2807	25	2999	-99999	3099	-99999	3199	-99999

STATION: CLINTON (Station ID: 111743)

Year	Mo	Dy	Precip-itation (in)	Observe Time	Source
1910	1	1	0	AM	F
1910	1	2	0	AM	F
1910	1	3	T	AM	F
1910	1	4	0.2	AM	F
1910	1	5	0.47	AM	F
1910	1	6	0	AM	F
1910	1	7	0	AM	F
1910	1	8	0	AM	F
1910	1	9	T	AM	F
1910	1	10	0	AM	F
1910	1	11	0	AM	F
1910	1	12	0.71	AM	F
1910	1	13	0.3	AM	F
1910	1	14	0.03	AM	F
1910	1	15	0	AM	F
1910	1	16	T	AM	F
1910	1	17	0.14	AM	F
1910	1	18	T	AM	F
1910	1	19	0	AM	F
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1911	9	2	0	AM	F
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1919	6	5 T		AM	F
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1919	12	5 T		AM	F
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1920	1	17 T		AM	F
1920	1	18 T		AM	F
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1931	7	31	0	AM	F
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1931	8	3	0	AM	F
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1931	8	5	0	AM	F
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1931	8	7	0	AM	F
1931	8	8	0	AM	F
1931	8	9	0	AM	F
1931	8	10	1.55	AM	F
1931	8	11	0	AM	F
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1931	8	13	0	AM	F
1931	8	14	0	AM	F
1931	8	15	0	AM	F
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1931	8	17	0	AM	F
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1931	8	20	0.28	AM	F
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1931	8	22	0	AM	F
1931	8	23	0	AM	F
1931	8	24	0.06	AM	F
1931	8	25	0	AM	F
1931	8	26	0.9	AM	F
1931	8	27	0	AM	F
1931	8	28	0.75	AM	F
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1931	8	30	0	AM	F
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1931	9	12	0	AM	F
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1931	9	14	0.18	AM	F
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1931	9	16	0.46	AM	F

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1931	9	24		0	AM	F
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1931	9	27		0	AM	F
1931	9	28		0	AM	F
1931	9	29		0	AM	F
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1931	10	5		0.03	AM	F
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1931	10	24	T		AM	F
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1931	10	27	T		AM	F
1931	10	28		0	AM	F
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1931	10	30		0.05	AM	F
1931	10	31		0.06	AM	F
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1931	11	7		0	AM	F
1931	11	8		0	AM	F
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1931	11	28		0	AM	F
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1931	11	30		0	AM	F
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1931	12	2		0	AM	F
1931	12	3	T		AM	F
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1931	12	5		0	AM	F
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1931	12	7		0	AM	F
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1931	12	27		0	AM	F
1931	12	28		0	AM	F
1931	12	29		0	AM	F
1931	12	30		0.3	AM	F
1931	12	31		0.41	AM	F
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1932	1	3		0	AM	F
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1932	1	5		0.32	AM	F
1932	1	6		0	AM	F
1932	1	7	T		AM	F
1932	1	8	T		AM	F
1932	1	9	T		AM	F

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1932	1	20	T		AM	F
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1932	1	23		0.1	AM	F
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1932	1	25		0	AM	F
1932	1	26		0.06	AM	F
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1932	2	15	T		AM	F
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1932	2	18		0	AM	F
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1932	2	20		0	AM	F
1932	2	21	T		AM	F
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1932	3	7	T		AM	F
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1932	3	20	T		AM	F
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1932	3	23		0	AM	F
1932	3	24		0.08	AM	F
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1932	3	26		0	AM	F
1932	3	27		0.06	AM	F
1932	3	28	T		AM	F
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1932	4	18	M		AM	F
1932	4	19	M		AM	F
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1932	7	29	0	AM	F
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1932	8	23	0	AM	F
1932	8	24	0	AM	F
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1932	8	29	0	AM	F
1932	8	30	0	AM	F
1932	8	31	0.08	AM	F
1932	9	1	0	AM	F
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1932	9	4	0	AM	F
1932	9	5	0	AM	F
1932	9	6	0	AM	F
1932	9	7	0	AM	F
1932	9	8	0	AM	F
1932	9	9	0	AM	F
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1932	9	29	0	AM	F
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1932	10	7	0	AM	F
1932	10	8	0	AM	F
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1932	10	14	0	AM	F
1932	10	15	0	AM	F
1932	10	16	0	AM	F
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1932	10	18	0	AM	F
1932	10	19	0	AM	F
1932	10	20	0	AM	F
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1932	10	23	T	AM	F
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1932	10	27	0	AM	F
1932	10	28	0	AM	F
1932	10	29	0	AM	F
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1932	11	24	0	AM	F
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1932	11	27	0	AM	F
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1932	11	29	0	AM	F
1932	11	30	0	AM	F
1932	12	1	0	AM	F
1932	12	2	0	AM	F
1932	12	3	0.06	AM	F
1932	12	4	0	AM	F
1932	12	5	0	AM	F
1932	12	6	0.25	AM	F
1932	12	7	T	AM	F
1932	12	8	T	AM	F
1932	12	9	T	AM	F
1932	12	10	0.08	AM	F
1932	12	11	0.22	AM	F
1932	12	12	0	AM	F
1932	12	13	0	AM	F
1932	12	14	0	AM	F
1932	12	15	0	AM	F
1932	12	16	0	AM	F
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1932	12	18	0	AM	F
1932	12	19	0	AM	F

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1932	12	21	0	AM	F
1932	12	22	0.06	AM	F
1932	12	23	0.85	AM	F
1932	12	24	0.7	AM	F
1932	12	25	0.05	AM	F
1932	12	26	0	AM	F
1932	12	27	0	AM	F
1932	12	28	0	AM	F
1932	12	29	0	AM	F
1932	12	30	0	AM	F
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1933	1	2	0	AM	F
1933	1	3	0	AM	F
1933	1	4	0	AM	F
1933	1	5	0	AM	F
1933	1	6	0	AM	F
1933	1	7	0	AM	F
1933	1	8	0	AM	F
1933	1	9	0	AM	F
1933	1	10	0	AM	F
1933	1	11	0.03	AM	F
1933	1	12	0	AM	F
1933	1	13	0	AM	F
1933	1	14	0	AM	F
1933	1	15	0	AM	F
1933	1	16	0	AM	F
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1933	1	23	0	AM	F
1933	1	24	0	AM	F
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1933	1	28	0	AM	F
1933	1	29	0	AM	F
1933	1	30	0	AM	F
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1933	2	2	0	AM	F
1933	2	3	0	AM	F
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1933	2	9	0	AM	F
1933	2	10	T	AM	F
1933	2	11	T	AM	F
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1933	2	14	T	AM	F
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1933	2	17	0	AM	F
1933	2	18	0	AM	F
1933	2	19	T	AM	F
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1933	2	22	0	AM	F
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1933	4	13	0	AM	F

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1934	10	10	0	AM	F
1934	10	11	0	AM	F
1934	10	12	0	AM	F
1934	10	13	0	AM	F
1934	10	14	0	AM	F
1934	10	15	0	AM	F
1934	10	16	0	AM	F
1934	10	17	0	AM	F
1934	10	18	0	AM	F
1934	10	19	0.03	AM	F
1934	10	20	0.65	AM	F
1934	10	21	0.05	AM	F
1934	10	22	0	AM	F
1934	10	23	0	AM	F
1934	10	24	1.1	AM	F
1934	10	25	0.85	AM	F
1934	10	26	0	AM	F
1934	10	27	0	AM	F
1934	10	28	0	AM	F
1934	10	29	0	AM	F
1934	10	30	0	AM	F
1934	10	31	0.05	AM	F
1934	11	1	0	AM	F
1934	11	2	0	AM	F
1934	11	3	1.62	AM	F
1934	11	4	0.23	AM	F
1934	11	5	0.13	AM	F
1934	11	6	0	AM	F
1934	11	7	0	AM	F
1934	11	8	0	AM	F
1934	11	9	0	AM	F

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1934	11	12		0	AM	F
1934	11	13		0	AM	F
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1934	11	18		0.6	AM	F
1934	11	19		0.05	AM	F
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1934	11	23		0	AM	F
1934	11	24		0	AM	F
1934	11	25		0	AM	F
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1934	11	27		0	AM	F
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1934	11	30		0.4	AM	F
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1934	12	2		0	AM	F
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1934	12	5		0	AM	F
1934	12	6	T		AM	F
1934	12	7	T		AM	F
1934	12	8	T		AM	F
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1934	12	18		0	AM	F
1934	12	19		0.4	AM	F
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1934	12	21		0.05	AM	F
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1934	12	27		0	AM	F
1934	12	28		0.11	AM	F
1934	12	29		0	AM	F
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1934	12	31	T		AM	F
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1935	1	2		0	AM	F
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1935	1	5		0	AM	F
1935	1	6		0	AM	F
1935	1	7		0	AM	F
1935	1	8		0.26	AM	F
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1935	1	10		0	AM	F
1935	1	11		0	AM	F
1935	1	12	T		AM	F
1935	1	13	T		AM	F
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1935	1	16		0.33	AM	F
1935	1	17		0	AM	F
1935	1	18		0	AM	F
1935	1	19		0.28	AM	F
1935	1	20	T		AM	F
1935	1	21		0.1	AM	F
1935	1	22		0	AM	F
1935	1	23		0	AM	F
1935	1	24		0	AM	F
1935	1	25		0	AM	F
1935	1	26	T		AM	F
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1935	1	28		0	AM	F
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1935	2	4		0	AM	F
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1935	2	17	T		AM	F
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1935	2	19	T		AM	F
1935	2	20	T		AM	F
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1935	2	26	T		AM	F
1935	2	27	T		AM	F
1935	2	28		0	AM	F
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1935	3	2		0	AM	F
1935	3	3		0.05	AM	F
1935	3	4		0.25	AM	F

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1935	3	7		1.25	AM	F
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1935	3	16	T		AM	F
1935	3	17	T		AM	F
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1935	3	29		0	AM	F
1935	3	30		0.2	AM	F
1935	3	31		0.05	AM	F
1935	4	1		0	AM	F
1935	4	2	T		AM	F
1935	4	3		0	AM	F
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1935	4	5		0	AM	F
1935	4	6	T		AM	F
1935	4	7		1	AM	F
1935	4	8		0.1	AM	F
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1935	4	12		0.15	AM	F
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1935	4	14		0	AM	F
1935	4	15	T		AM	F
1935	4	16		0	AM	F
1935	4	17	T		AM	F
1935	4	18		0.19	AM	F
1935	4	19		0	AM	F
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1935	4	21		0	AM	F
1935	4	22		0	AM	F
1935	4	23		0	AM	F
1935	4	24		0	AM	F
1935	4	25		0	AM	F
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1935	4	27		0.5	AM	F
1935	4	28		0	AM	F
1935	4	29		0.28	AM	F
1935	4	30		0	AM	F
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1935	5	4		0	AM	F
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1935	5	6		1.5	AM	F
1935	5	7		0	AM	F
1935	5	8		0	AM	F
1935	5	9		1.75	AM	F
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1935	5	11		0	AM	F
1935	5	12		0.25	AM	F
1935	5	13		1.75	AM	F
1935	5	14		0.5	AM	F
1935	5	15		0	AM	F
1935	5	16		0.35	AM	F
1935	5	17		0	AM	F
1935	5	18		0	AM	F
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1935	5	20		0.06	AM	F
1935	5	21		0	AM	F
1935	5	22	T		AM	F
1935	5	23		0.25	AM	F
1935	5	24		0	AM	F
1935	5	25		0	AM	F
1935	5	26		0	AM	F
1935	5	27		0.65	AM	F
1935	5	28		0	AM	F
1935	5	29		0	AM	F
1935	5	30	T		AM	F
1935	5	31		0	AM	F
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1935	6	2		0.1	AM	F
1935	6	3		0	AM	F
1935	6	4		0	AM	F
1935	6	5		0.05	AM	F
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1935	6	9		0	AM	F
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1935	6	15		0.12	AM	F
1935	6	16		1.1	AM	F
1935	6	17		0.75	AM	F
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1935	6	27		0	AM	F

1935	6	28	0	AM	F
1935	6	29	1.25	AM	F
1935	6	30	0.1	AM	F
1935	7	1	0.75	AM	F
1935	7	2	0	AM	F
1935	7	3	0	AM	F
1935	7	4	0	AM	F
1935	7	5	0	AM	F
1935	7	6	0	AM	F
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1935	7	8	0	AM	F
1935	7	9	0	AM	F
1935	7	10	0	AM	F
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1935	7	16	0	AM	F
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1935	7	18	0	AM	F
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1935	7	23	0.1	AM	F
1935	7	24	1.1	AM	F
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1935	7	26	0	AM	F
1935	7	27	0	AM	F
1935	7	28	0	AM	F
1935	7	29	0	AM	F
1935	7	30	0	AM	F
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1935	8	4	0	AM	F
1935	8	5 T		AM	F
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1935	8	12	0	AM	F
1935	8	13	0	AM	F
1935	8	14	0	AM	F
1935	8	15	0	AM	F
1935	8	16	0.75	AM	F
1935	8	17	0.36	AM	F
1935	8	18	0	AM	F
1935	8	19	0	AM	F
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1935	8	22	0	AM	F
1935	8	23	0	AM	F
1935	8	24	0	AM	F
1935	8	25	0	AM	F
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1935	8	27	0	AM	F
1935	8	28	0	AM	F
1935	8	29 T		AM	F
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1935	8	31	0.06	AM	F
1935	9	1	0	AM	F
1935	9	2	0.66	AM	F
1935	9	3	0	AM	F
1935	9	4	0	AM	F
1935	9	5	0	AM	F
1935	9	6	0	AM	F
1935	9	7	0	AM	F
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1935	9	17	0	AM	F
1935	9	18	0	AM	F
1935	9	19	0	AM	F
1935	9	20	0	AM	F
1935	9	21	0.11	AM	F
1935	9	22	0	AM	F
1935	9	23	0.03	AM	F
1935	9	24	0	AM	F
1935	9	25	0	AM	F
1935	9	26	0.73	AM	F
1935	9	27	0.11	AM	F
1935	9	28	0	AM	F
1935	9	29	0	AM	F
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1935	10	2	0	AM	F
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1935	10	5	0	AM	F
1935	10	6	0	AM	F
1935	10	7	0	AM	F
1935	10	8 T		AM	F
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1935	10	10	0.84	AM	F
1935	10	11	0.1	AM	F
1935	10	12 T		AM	F
1935	10	13	0	AM	F
1935	10	14	0	AM	F
1935	10	15	0	AM	F
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1935	10	17	0.42	AM	F
1935	10	18	0	AM	F
1935	10	19	0	AM	F
1935	10	20	0	AM	F

1935	10	21	0.21	AM	F
1935	10	22	0.05	AM	F
1935	10	23	0	AM	F
1935	10	24	0	AM	F
1935	10	25	0	AM	F
1935	10	26	0	AM	F
1935	10	27	0.11	AM	F
1935	10	28	0.95	AM	F
1935	10	29	0	AM	F
1935	10	30	0	AM	F
1935	10	31	T	AM	F
1935	11	1	1.62	AM	F
1935	11	2	T	AM	F
1935	11	3	0.51	AM	F
1935	11	4	1.75	AM	F
1935	11	5	0	AM	F
1935	11	6	0	AM	F
1935	11	7	0	AM	F
1935	11	8	0	AM	F
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1935	11	13	0.05	AM	F
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1935	11	18	0	AM	F
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1935	11	27	0	AM	F
1935	11	28	0.29	AM	F
1935	11	29	0.03	AM	F
1935	11	30	0	AM	F
1935	12	1	T	AM	F
1935	12	2	0	AM	F
1935	12	3	0	AM	F
1935	12	4	0	AM	F
1935	12	5	0	AM	F
1935	12	6	0.51	AM	F
1935	12	7	0.06	AM	F
1935	12	8	0	AM	F
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1935	12	15	T	AM	F
1935	12	16	0	AM	F
1935	12	17	0	AM	F
1935	12	18	T	AM	F
1935	12	19	T	AM	F
1935	12	20	T	AM	F
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1935	12	22	0.16	AM	F
1935	12	23	0	AM	F
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1935	12	25	0	AM	F
1935	12	26	0	AM	F
1935	12	27	0	AM	F
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1935	12	29	0	AM	F
1935	12	30	0	AM	F
1935	12	31	0	AM	F
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1936	1	2	0.11	AM	F
1936	1	3	T	AM	F
1936	1	4	T	AM	F
1936	1	5	0	AM	F
1936	1	6	0.18	AM	F
1936	1	7	0	AM	F
1936	1	8	0.14	AM	F
1936	1	9	0	AM	F
1936	1	10	0	AM	F
1936	1	11	0	AM	F
1936	1	12	0	AM	F
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1936	1	14	0	AM	F
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1936	1	17	0.03	AM	F
1936	1	18	0.05	AM	F
1936	1	19	0.01	AM	F
1936	1	20	0	AM	F
1936	1	21	0.06	AM	F
1936	1	22	0.21	AM	F
1936	1	23	0	AM	F
1936	1	24	0	AM	F
1936	1	25	0.03	AM	F
1936	1	26	0	AM	F
1936	1	27	0	AM	F
1936	1	28	0	AM	F
1936	1	29	0.04	AM	F
1936	1	30	0	AM	F
1936	1	31	0	AM	F
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1936	2	5	0	AM	F
1936	2	6	0	AM	F
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1936	2	12	0.01	AM	F

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1936	2	16	0.06	AM	F
1936	2	17	0.04	AM	F
1936	2	18	0	AM	F
1936	2	19	0	AM	F
1936	2	20	0	AM	F
1936	2	21 T		AM	F
1936	2	22	0.03	AM	F
1936	2	23	0	AM	F
1936	2	24	0	AM	F
1936	2	25	0	AM	F
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1936	2	27 T		AM	F
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1936	3	4	0	AM	F
1936	3	5	0	AM	F
1936	3	6	0	AM	F
1936	3	7	0	AM	F
1936	3	8	0.06	AM	F
1936	3	9	0	AM	F
1936	3	10	0	AM	F
1936	3	11	0	AM	F
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1936	3	17	0	AM	F
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1936	4	3	0.03	AM	F
1936	4	4	0.05	AM	F
1936	4	5	0.21	AM	F
1936	4	6	0.05	AM	F
1936	4	7 T		AM	F
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1936	4	16	0	AM	F
1936	4	17	0	AM	F
1936	4	18	0	AM	F
1936	4	19	0	AM	F
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1936	4	22	0	AM	F
1936	4	23	0	AM	F
1936	4	24	0	AM	F
1936	4	25	0	AM	F
1936	4	26 T		AM	F
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1936	4	28	1.1	AM	F
1936	4	29	0.96	AM	F
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1936	5	5	0	AM	F
1936	5	6	0	AM	F
1936	5	7	0	AM	F
1936	5	8	0	AM	F
1936	5	9	0	AM	F
1936	5	10 T		AM	F
1936	5	11 T		AM	F
1936	5	12	0	AM	F
1936	5	13 T		AM	F
1936	5	14	0	AM	F
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1936	5	16	0	AM	F
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1936	5	27	0	AM	F
1936	5	28	0	AM	F
1936	5	29	0	AM	F
1936	5	30	0	AM	F
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1936	6	2	0	AM	F
1936	6	3	0	AM	F
1936	6	4	0	AM	F
1936	6	5	0	AM	F
1936	6	6	0	AM	F

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1936	9	4		0.28	AM	F
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1936	9	7		0	AM	F
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1936	9	9		0	AM	F
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1936	9	27		1.34	AM	F
1936	9	28		1.04	AM	F
1936	9	29		0	AM	F

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1936	10	3	0	AM	F
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1936	10	15	0	AM	F
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1936	10	27	0	AM	F
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1936	10	29	0	AM	F
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1936	11	2	2.1	AM	F
1936	11	3 T		AM	F
1936	11	4	0	AM	F
1936	11	5	0	AM	F
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1936	11	7	0	AM	F
1936	11	8 T		AM	F
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1936	11	14 T		AM	F
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1936	12	2	0	AM	F
1936	12	3 T		AM	F
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1936	12	7	0	AM	F
1936	12	8	0	AM	F
1936	12	9	0	AM	F
1936	12	10 T		AM	F
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1936	12	19	0	AM	F
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1936	12	26	0.14	AM	F
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1936	12	28	0	AM	F
1936	12	29	0	AM	F
1936	12	30	1.21	AM	F
1936	12	31	0	AM	F
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1937	1	2	0.11	AM	F
1937	1	3 T		AM	F
1937	1	4 T		AM	F
1937	1	5	0	AM	F
1937	1	6	0.05	AM	F
1937	1	7	1.51	AM	F
1937	1	8	0.41	AM	F
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1937	1	10 T		AM	F
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1937	1	12	0	AM	F
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1937	1	16	0	AM	F
1937	1	17	0	AM	F
1937	1	18	0	AM	F
1937	1	19	0	AM	F
1937	1	20	0.05	AM	F
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1937	1	22	0.04	AM	F

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1937	1	24	0.16	AM	F
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1937	1	26	0	AM	F
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1937	1	28	0	AM	F
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1937	2	2	0	AM	F
1937	2	3	0	AM	F
1937	2	4	T	AM	F
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1937	2	6	0	AM	F
1937	2	7	0.06	AM	F
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1937	2	9	0	AM	F
1937	2	10	0	AM	F
1937	2	11	0	AM	F
1937	2	12	0	AM	F
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1937	2	14	0	AM	F
1937	2	15	0.06	AM	F
1937	2	16	0.09	AM	F
1937	2	17	0.02	AM	F
1937	2	18	0.04	AM	F
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1937	2	22	0	AM	F
1937	2	23	0	AM	F
1937	2	24	0	AM	F
1937	2	25	T	AM	F
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1937	2	27	T	AM	F
1937	2	28	0	AM	F
1937	3	1	0	AM	F
1937	3	2	0	AM	F
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1937	3	4	0	AM	F
1937	3	5	0	AM	F
1937	3	6	0	AM	F
1937	3	7	0	AM	F
1937	3	8	0	AM	F
1937	3	9	T	AM	F
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1937	3	11	0	AM	F
1937	3	12	0	AM	F
1937	3	13	T	AM	F
1937	3	14	0.02	AM	F
1937	3	15	0	AM	F
1937	3	16	0	AM	F
1937	3	17	0	AM	F
1937	3	18	0	AM	F
1937	3	19	0.05	AM	F
1937	3	20	0.02	AM	F
1937	3	21	0	AM	F
1937	3	22	0	AM	F
1937	3	23	0	AM	F
1937	3	24	0.11	AM	F
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1937	3	28	0	AM	F
1937	3	29	0	AM	F
1937	3	30	0	AM	F
1937	3	31	0	AM	F
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1937	4	6	0	AM	F
1937	4	7	0	AM	F
1937	4	8	T	AM	F
1937	4	9	0	AM	F
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1937	4	16	0	AM	F
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1937	4	18	0.18	AM	F
1937	4	19	0	AM	F
1937	4	20	0.22	AM	F
1937	4	21	1.02	AM	F
1937	4	22	0	AM	F
1937	4	23	0	AM	F
1937	4	24	0	AM	F
1937	4	25	0.42	AM	F
1937	4	26	T	AM	F
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1937	5	3	0.1	AM	F
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1937	5	7	0	AM	F
1937	5	8	0	AM	F
1937	5	9	0	AM	F
1937	5	10	0	AM	F
1937	5	11	0	AM	F
1937	5	12	0.06	AM	F
1937	5	13	0	AM	F
1937	5	14	T	AM	F
1937	5	15	0.04	AM	F
1937	5	16	0.06	AM	F
1937	5	17	0	AM	F

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1937	5	19	0	AM	F
1937	5	20	0.12	AM	F
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1937	5	23	0	AM	F
1937	5	24	0	AM	F
1937	5	25	T	AM	F
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1937	5	30	0	AM	F
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1937	6	14	0	AM	F
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1937	6	17	0	AM	F
1937	6	18	0	AM	F
1937	6	19	0	AM	F
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1937	6	22	0	AM	F
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1937	6	28	0	AM	F
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1937	6	30	0	AM	F
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1937	7	2	0	AM	F
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1937	7	8	0	AM	F
1937	7	9	0	AM	F
1937	7	10	0	AM	F
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1937	7	12	0.3	AM	F
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1937	7	23	0	AM	F
1937	7	24	0	AM	F
1937	7	25	0.46	AM	F
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1937	7	27	0	AM	F
1937	7	28	0	AM	F
1937	7	29	0	AM	F
1937	7	30	0	AM	F
1937	7	31	0	AM	F
1937	8	1	0	AM	F
1937	8	2	0	AM	F
1937	8	3	T	AM	F
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1937	8	6	0	AM	F
1937	8	7	0	AM	F
1937	8	8	T	AM	F
1937	8	9	T	AM	F
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1937	8	18	0.76	AM	F
1937	8	19	0	AM	F
1937	8	20	0.03	AM	F
1937	8	21	1.02	AM	F
1937	8	22	0	AM	F
1937	8	23	0	AM	F
1937	8	24	0	AM	F
1937	8	25	0	AM	F
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1937	8	28	0	AM	F
1937	8	29	0	AM	F
1937	8	30	0	AM	F
1937	8	31	0	AM	F
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1937	9	2	0	AM	F
1937	9	3	0	AM	F
1937	9	4	0.81	AM	F
1937	9	5	0	AM	F
1937	9	6	0	AM	F
1937	9	7	0	AM	F
1937	9	8	0	AM	F
1937	9	9	0	AM	F

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1937	9	11	0	AM	F
1937	9	12 T		AM	F
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1937	9	14	0	AM	F
1937	9	15	0	AM	F
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1937	9	20	0	AM	F
1937	9	21	0	AM	F
1937	9	22	0	AM	F
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1937	9	26	0	AM	F
1937	9	27	0	AM	F
1937	9	28 T		AM	F
1937	9	29	0	AM	F
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1937	10	2	0	AM	F
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1937	10	7	0	AM	F
1937	10	8	0	AM	F
1937	10	9	0.16	AM	F
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1937	10	11	0.06	AM	F
1937	10	12	0.19	AM	F
1937	10	13	0	AM	F
1937	10	14	0	AM	F
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1937	10	17	0.16	AM	F
1937	10	18	0.9	AM	F
1937	10	19	0.58	AM	F
1937	10	20	0.12	AM	F
1937	10	21	0	AM	F
1937	10	22	0	AM	F
1937	10	23 T		AM	F
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1937	10	25	0	AM	F
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1937	10	29	0	AM	F
1937	10	30	0	AM	F
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1937	11	11	0	AM	F
1937	11	12	0	AM	F
1937	11	13	0	AM	F
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1937	11	15	0	AM	F
1937	11	16	0	AM	F
1937	11	17	0	AM	F
1937	11	18	0	AM	F
1937	11	19	0.15	AM	F
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1937	11	23	0	AM	F
1937	11	24	0	AM	F
1937	11	25	0	AM	F
1937	11	26	0	AM	F
1937	11	27	0	AM	F
1937	11	28	0.4	AM	F
1937	11	29	0.04	AM	F
1937	11	30	0	AM	F
1937	12	1	0	AM	F
1937	12	2	0	AM	F
1937	12	3	0.46	AM	F
1937	12	4	0.35	AM	F
1937	12	5 T		AM	F
1937	12	6 T		AM	F
1937	12	7	0.06	AM	F
1937	12	8 T		AM	F
1937	12	9	0	AM	F
1937	12	10	0	AM	F
1937	12	11	0	AM	F
1937	12	12 T		AM	F
1937	12	13	0.42	AM	F
1937	12	14	0.11	AM	F
1937	12	15	0.21	AM	F
1937	12	16 T		AM	F
1937	12	17 T		AM	F
1937	12	18 T		AM	F
1937	12	19	0	AM	F
1937	12	20	0	AM	F
1937	12	21	0	AM	F
1937	12	22	0	AM	F
1937	12	23	0	AM	F
1937	12	24	0.03	AM	F
1937	12	25	0	AM	F
1937	12	26	0	AM	F
1937	12	27	0	AM	F
1937	12	28 T		AM	F
1937	12	29	0	AM	F
1937	12	30	0.04	AM	F
1937	12	31 T		AM	F
1938	1	1	0	AM	F
1938	1	2	0	AM	F

1938	1	3	T	AM	F
1938	1	4	0	AM	F
1938	1	5	0	AM	F
1938	1	6	T	AM	F
1938	1	7	T	AM	F
1938	1	8	0	AM	F
1938	1	9	0.11	AM	F
1938	1	10	0	AM	F
1938	1	11	0	AM	F
1938	1	12	0.05	AM	F
1938	1	13	0.06	AM	F
1938	1	14	0.21	AM	F
1938	1	15	0	AM	F
1938	1	16	0	AM	F
1938	1	17	T	AM	F
1938	1	18	T	AM	F
1938	1	19	0.01	AM	F
1938	1	20	0	AM	F
1938	1	21	T	AM	F
1938	1	22	0	AM	F
1938	1	23	0.05	AM	F
1938	1	24	0.89	AM	F
1938	1	25	0.06	AM	F
1938	1	26	0	AM	F
1938	1	27	0	AM	F
1938	1	28	0	AM	F
1938	1	29	0	AM	F
1938	1	30	0.16	AM	F
1938	1	31	0	AM	F
1938	2	1	0	AM	F
1938	2	2	0.01	AM	F
1938	2	3	0.05	AM	F
1938	2	4	0	AM	F
1938	2	5	0.28	AM	F
1938	2	6	0	AM	F
1938	2	7	T	AM	F
1938	2	8	0	AM	F
1938	2	9	0	AM	F
1938	2	10	0	AM	F
1938	2	11	0.33	AM	F
1938	2	12	0.13	AM	F
1938	2	13	0	AM	F
1938	2	14	0	AM	F
1938	2	15	0	AM	F
1938	2	16	T	AM	F
1938	2	17	0.63	AM	F
1938	2	18	0.09	AM	F
1938	2	19	0.12	AM	F
1938	2	20	0.16	AM	F
1938	2	21	T	AM	F
1938	2	22	0.06	AM	F
1938	2	23	0.05	AM	F
1938	2	24	0.04	AM	F
1938	2	25	0.02	AM	F
1938	2	26	0.01	AM	F
1938	2	27	0	AM	F
1938	2	28	0	AM	F
1938	3	1	0	AM	F
1938	3	2	T	AM	F
1938	3	3	0.16	AM	F
1938	3	4	0.18	AM	F
1938	3	5	T	AM	F
1938	3	6	0	AM	F
1938	3	7	0	AM	F
1938	3	8	0	AM	F
1938	3	9	0.18	AM	F
1938	3	10	0.06	AM	F
1938	3	11	0	AM	F
1938	3	12	0.16	AM	F
1938	3	13	0.14	AM	F
1938	3	14	0	AM	F
1938	3	15	1.05	AM	F
1938	3	16	0.14	AM	F
1938	3	17	0	AM	F
1938	3	18	0	AM	F
1938	3	19	0.02	AM	F
1938	3	20	0	AM	F
1938	3	21	0	AM	F
1938	3	22	0	AM	F
1938	3	23	1.25	AM	F
1938	3	24	0	AM	F
1938	3	25	0.23	AM	F
1938	3	26	0	AM	F
1938	3	27	0	AM	F
1938	3	28	0	AM	F
1938	3	29	0.18	AM	F
1938	3	30	0	AM	F
1938	3	31	0.82	AM	F
1938	4	1	0	AM	F
1938	4	2	0	AM	F
1938	4	3	0	AM	F
1938	4	4	0	AM	F
1938	4	5	T	AM	F
1938	4	6	1.65	AM	F
1938	4	7	0.26	AM	F
1938	4	8	0.93	AM	F
1938	4	9	0	AM	F
1938	4	10	0	AM	F
1938	4	11	0	AM	F
1938	4	12	0	AM	F
1938	4	13	0	AM	F
1938	4	14	0	AM	F
1938	4	15	0	AM	F
1938	4	16	0.21	AM	F
1938	4	17	0	AM	F
1938	4	18	0	AM	F
1938	4	19	0	AM	F
1938	4	20	0.27	AM	F
1938	4	21	0	AM	F
1938	4	22	0	AM	F
1938	4	23	0	AM	F
1938	4	24	0.14	AM	F
1938	4	25	0	AM	F
1938	4	26	0	AM	F
1938	4	27	0	AM	F

1938	4	28	0.1	AM	F
1938	4	29	T	AM	F
1938	4	30	0.11	AM	F
1938	5	1	0	AM	F
1938	5	2	0	AM	F
1938	5	3	0	AM	F
1938	5	4	0	AM	F
1938	5	5	0.43	AM	F
1938	5	6	0	AM	F
1938	5	7	0.12	AM	F
1938	5	8	T	AM	F
1938	5	9	0	AM	F
1938	5	10	T	AM	F
1938	5	11	T	AM	F
1938	5	12	0	AM	F
1938	5	13	0	AM	F
1938	5	14	0.28	AM	F
1938	5	15	0	AM	F
1938	5	16	0	AM	F
1938	5	17	1.52	AM	F
1938	5	18	0.12	AM	F
1938	5	19	0.4	AM	F
1938	5	20	0.08	AM	F
1938	5	21	0.65	AM	F
1938	5	22	0	AM	F
1938	5	23	1.81	AM	F
1938	5	24	0	AM	F
1938	5	25	0	AM	F
1938	5	26	0	AM	F
1938	5	27	T	AM	F
1938	5	28	0.85	AM	F
1938	5	29	0.15	AM	F
1938	5	30	0	AM	F
1938	5	31	0	AM	F
1938	6	1	0.14	AM	F
1938	6	2	0.11	AM	F
1938	6	3	0	AM	F
1938	6	4	0	AM	F
1938	6	5	0	AM	F
1938	6	6	0	AM	F
1938	6	7	0.75	AM	F
1938	6	8	0	AM	F
1938	6	9	0.11	AM	F
1938	6	10	0.28	AM	F
1938	6	11	1.25	AM	F
1938	6	12	0	AM	F
1938	6	13	0	AM	F
1938	6	14	0.18	AM	F
1938	6	15	0	AM	F
1938	6	16	0	AM	F
1938	6	17	0	AM	F
1938	6	18	0	AM	F
1938	6	19	0	AM	F
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1938	6	21	0	AM	F
1938	6	22	0	AM	F
1938	6	23	0	AM	F
1938	6	24	0.71	AM	F
1938	6	25	0.65	AM	F
1938	6	26	1.45	AM	F
1938	6	27	0	AM	F
1938	6	28	0	AM	F
1938	6	29	0	AM	F
1938	6	30	0.02	AM	F
1938	7	1	0	AM	F
1938	7	2	0.82	AM	F
1938	7	3	0	AM	F
1938	7	4	0	AM	F
1938	7	5	0	AM	F
1938	7	6	0	AM	F
1938	7	7	0.12	AM	F
1938	7	8	0	AM	F
1938	7	9	0	AM	F
1938	7	10	0	AM	F
1938	7	11	0	AM	F
1938	7	12	0	AM	F
1938	7	13	0	AM	F
1938	7	14	0	AM	F
1938	7	15	0	AM	F
1938	7	16	0	AM	F
1938	7	17	1.24	AM	F
1938	7	18	0	AM	F
1938	7	19	0	AM	F
1938	7	20	0.55	AM	F
1938	7	21	0	AM	F
1938	7	22	0	AM	F
1938	7	23	0	AM	F
1938	7	24	0	AM	F
1938	7	25	0	AM	F
1938	7	26	0	AM	F
1938	7	27	0	AM	F
1938	7	28	0.54	AM	F
1938	7	29	0	AM	F
1938	7	30	0	AM	F
1938	7	31	2.2	AM	F
1938	8	1	0.16	AM	F
1938	8	2	0	AM	F
1938	8	3	0	AM	F
1938	8	4	0	AM	F
1938	8	5	0	AM	F
1938	8	6	0	AM	F
1938	8	7	0	AM	F
1938	8	8	0.11	AM	F
1938	8	9	0	AM	F
1938	8	10	0	AM	F
1938	8	11	0.06	AM	F
1938	8	12	0	AM	F
1938	8	13	0	AM	F
1938	8	14	0	AM	F
1938	8	15	0	AM	F
1938	8	16	0.09	AM	F
1938	8	17	0	AM	F
1938	8	18	0	AM	F
1938	8	19	0.55	AM	F
1938	8	20	0	AM	F

1938	8	21	0	AM	F
1938	8	22	0	AM	F
1938	8	23	0	AM	F
1938	8	24	0	AM	F
1938	8	25	0	AM	F
1938	8	26	0	AM	F
1938	8	27	0	AM	F
1938	8	28	0.1	AM	F
1938	8	29	0	AM	F
1938	8	30	0	AM	F
1938	8	31	2.12	AM	F
1938	9	1	0	AM	F
1938	9	2	0	AM	F
1938	9	3	0	AM	F
1938	9	4	0	AM	F
1938	9	5	T	AM	F
1938	9	6	T	AM	F
1938	9	7	T	AM	F
1938	9	8	0.04	AM	F
1938	9	9	0.1	AM	F
1938	9	10	0	AM	F
1938	9	11	0.2	AM	F
1938	9	12	0.65	AM	F
1938	9	13	0.12	AM	F
1938	9	14	0.16	AM	F
1938	9	15	0.06	AM	F
1938	9	16	T	AM	F
1938	9	17	0.07	AM	F
1938	9	18	0.61	AM	F
1938	9	19	0.09	AM	F
1938	9	20	T	AM	F
1938	9	21	0	AM	F
1938	9	22	0	AM	F
1938	9	23	0	AM	F
1938	9	24	0	AM	F
1938	9	25	0	AM	F
1938	9	26	0	AM	F
1938	9	27	0	AM	F
1938	9	28	0	AM	F
1938	9	29	0	AM	F
1938	9	30	0	AM	F
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1938	10	2	0	AM	F
1938	10	3	0	AM	F
1938	10	4	0	AM	F
1938	10	5	0	AM	F
1938	10	6	0	AM	F
1938	10	7	0	AM	F
1938	10	8	0	AM	F
1938	10	9	0	AM	F
1938	10	10	0	AM	F
1938	10	11	0	AM	F
1938	10	12	0	AM	F
1938	10	13	0.15	AM	F
1938	10	14	0	AM	F
1938	10	15	0	AM	F
1938	10	16	0	AM	F
1938	10	17	0	AM	F
1938	10	18	0.1	AM	F
1938	10	19	1.57	AM	F
1938	10	20	0	AM	F
1938	10	21	0	AM	F
1938	10	22	0	AM	F
1938	10	23	0	AM	F
1938	10	24	0	AM	F
1938	10	25	0	AM	F
1938	10	26	0	AM	F
1938	10	27	0	AM	F
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1938	10	31	0	AM	F
1938	11	1	0	AM	F
1938	11	2	0	AM	F
1938	11	3	0	AM	F
1938	11	4	0.16	AM	F
1938	11	5	0	AM	F
1938	11	6	0	AM	F
1938	11	7	0.76	AM	F
1938	11	8	T	AM	F
1938	11	9	0	AM	F
1938	11	10	0	AM	F
1938	11	11	0	AM	F
1938	11	12	0	AM	F
1938	11	13	0.09	AM	F
1938	11	14	0	AM	F
1938	11	15	0	AM	F
1938	11	16	0	AM	F
1938	11	17	0	AM	F
1938	11	18	0.06	AM	F
1938	11	19	0	AM	F
1938	11	20	0	AM	F
1938	11	21	0	AM	F
1938	11	22	0	AM	F
1938	11	23	0.03	AM	F
1938	11	24	0	AM	F
1938	11	25	0	AM	F
1938	11	26	0.08	AM	F
1938	11	27	T	AM	F
1938	11	28	0	AM	F
1938	11	29	0	AM	F
1938	11	30	0	AM	F
1938	12	1	0	AM	F
1938	12	2	0.03	AM	F
1938	12	3	1.91	AM	F
1938	12	4	0	AM	F
1938	12	5	0.1	AM	F
1938	12	6	0	AM	F
1938	12	7	0	AM	F
1938	12	8	0	AM	F
1938	12	9	0.1	AM	F
1938	12	10	0	AM	F
1938	12	11	0	AM	F
1938	12	12	0	AM	F
1938	12	13	0	AM	F

1938	12	14	0	AM	F
1938	12	15	0	AM	F
1938	12	16	0	AM	F
1938	12	17	0.17	AM	F
1938	12	18	0	AM	F
1938	12	19	0	AM	F
1938	12	20	0	AM	F
1938	12	21	0	AM	F
1938	12	22	0	AM	F
1938	12	23	0.14	AM	F
1938	12	24	0	AM	F
1938	12	25	0	AM	F
1938	12	26	0.12	AM	F
1938	12	27 T		AM	F
1938	12	28	0	AM	F
1938	12	29	0	AM	F
1938	12	30	0	AM	F
1938	12	31	0	AM	F
1939	1	1	0	AM	F
1939	1	2	0	AM	F
1939	1	3	0	AM	F
1939	1	4	0.17	AM	F
1939	1	5	0.31	AM	F
1939	1	6	0	AM	F
1939	1	7	0	AM	F
1939	1	8	0	AM	F
1939	1	9	0.26	AM	F
1939	1	10	0	AM	F
1939	1	11	0	AM	F
1939	1	12 T		AM	F
1939	1	13	0.12	AM	F
1939	1	14	0.16	AM	F
1939	1	15	0.04	AM	F
1939	1	16 T		AM	F
1939	1	17 T		AM	F
1939	1	18	0.06	AM	F
1939	1	19	0	AM	F
1939	1	20	0	AM	F
1939	1	21	0	AM	F
1939	1	22 T		AM	F
1939	1	23	0.18	AM	F
1939	1	24	0.03	AM	F
1939	1	25	0	AM	F
1939	1	26	0	AM	F
1939	1	27 T		AM	F
1939	1	28	0.12	AM	F
1939	1	29	0.06	AM	F
1939	1	30	1.3	AM	F
1939	1	31	0	AM	F
1939	2	1	0	AM	F
1939	2	2 T		AM	F
1939	2	3	0	AM	F
1939	2	4	0	AM	F
1939	2	5	0	AM	F
1939	2	6	0.05	AM	F
1939	2	7	0	AM	F
1939	2	8	0	AM	F
1939	2	9	0.11	AM	F
1939	2	10	1.61	AM	F
1939	2	11	0	AM	F
1939	2	12	0	AM	F
1939	2	13	0	AM	F
1939	2	14	0	AM	F
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1939	2	16	0	AM	F
1939	2	17	0	AM	F
1939	2	18	0	AM	F
1939	2	19	1.74	AM	F
1939	2	20 T		AM	F
1939	2	21	0.14	AM	F
1939	2	22	0	AM	F
1939	2	23	0	AM	F
1939	2	24	0	AM	F
1939	2	25	0.06	AM	F
1939	2	26	0.05	AM	F
1939	2	27	0	AM	F
1939	2	28	0.61	AM	F
1939	3	1	0	AM	F
1939	3	2	0	AM	F
1939	3	3	0	AM	F
1939	3	4	0	AM	F
1939	3	5	0.16	AM	F
1939	3	6	0	AM	F
1939	3	7	0	AM	F
1939	3	8	0	AM	F
1939	3	9	0	AM	F
1939	3	10	0	AM	F
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1939	3	18	0	AM	F
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1939	3	20	0	AM	F
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1939	3	22	0	AM	F
1939	3	23	0	AM	F
1939	3	24	0	AM	F
1939	3	25	0	AM	F
1939	3	26	0.16	AM	F
1939	3	27	0	AM	F
1939	3	28	0	AM	F
1939	3	29	0.13	AM	F
1939	3	30	0	AM	F
1939	3	31	0.05	AM	F
1939	4	1	0.26	AM	F
1939	4	2	0.06	AM	F
1939	4	3	0	AM	F
1939	4	4	0	AM	F
1939	4	5	0.16	AM	F
1939	4	6	0.1	AM	F
1939	4	7	0	AM	F

1939	4	8	0.03	AM	F
1939	4	9	0	AM	F
1939	4	10	1.04	AM	F
1939	4	11	0.05	AM	F
1939	4	12	0	AM	F
1939	4	13	0	AM	F
1939	4	14	0.33	AM	F
1939	4	15	1.15	AM	F
1939	4	16 T		AM	F
1939	4	17	0.41	AM	F
1939	4	18	0.06	AM	F
1939	4	19	0.08	AM	F
1939	4	20 T		AM	F
1939	4	21	0.71	AM	F
1939	4	22	0	AM	F
1939	4	23	0	AM	F
1939	4	24	0	AM	F
1939	4	25	0	AM	F
1939	4	26	0.18	AM	F
1939	4	27	0.22	AM	F
1939	4	28	0	AM	F
1939	4	29	0	AM	F
1939	4	30	0	AM	F
1939	5	1	0	AM	F
1939	5	2	0	AM	F
1939	5	3	0	AM	F
1939	5	4	0.06	AM	F
1939	5	5	0	AM	F
1939	5	6	0	AM	F
1939	5	7 T		AM	F
1939	5	8	0.16	AM	F
1939	5	9	0.03	AM	F
1939	5	10 T		AM	F
1939	5	11	0	AM	F
1939	5	12	0	AM	F
1939	5	13	0	AM	F
1939	5	14	0	AM	F
1939	5	15	0.4	AM	F
1939	5	16	0	AM	F
1939	5	17	0	AM	F
1939	5	18	0	AM	F
1939	5	19	0	AM	F
1939	5	20	0.11	AM	F
1939	5	21	0.46	AM	F
1939	5	22	0	AM	F
1939	5	23	0	AM	F
1939	5	24	0	AM	F
1939	5	25	0	AM	F
1939	5	26	0.21	AM	F
1939	5	27	0.13	AM	F
1939	5	28	0.32	AM	F
1939	5	29	0	AM	F
1939	5	30	0	AM	F
1939	5	31	0	AM	F
1939	6	1	0	AM	F
1939	6	2	0	AM	F
1939	6	3 T		AM	F
1939	6	4	0	AM	F
1939	6	5	0	AM	F
1939	6	6	0.11	AM	F
1939	6	7	0	AM	F
1939	6	8	0.21	AM	F
1939	6	9	0.14	AM	F
1939	6	10	2.25	AM	F
1939	6	11	0.1	AM	F
1939	6	12	0.03	AM	F
1939	6	13	0	AM	F
1939	6	14	0	AM	F
1939	6	15	0	AM	F
1939	6	16	0	AM	F
1939	6	17	0	AM	F
1939	6	18	0	AM	F
1939	6	19	0.18	AM	F
1939	6	20	0.05	AM	F
1939	6	21	0.81	AM	F
1939	6	22	0	AM	F
1939	6	23	0	AM	F
1939	6	24	0	AM	F
1939	6	25	0	AM	F
1939	6	26 T		AM	F
1939	6	27	0	AM	F
1939	6	28	1.04	AM	F
1939	6	29	0.14	AM	F
1939	6	30	0	AM	F
1939	7	1	0	AM	F
1939	7	2	0	AM	F
1939	7	3	0	AM	F
1939	7	4	0.49	AM	F
1939	7	5	1.75	AM	F
1939	7	6	1.65	AM	F
1939	7	7	0	AM	F
1939	7	8	0	AM	F
1939	7	9	0	AM	F
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1939	7	11	0	AM	F
1939	7	12	0	AM	F
1939	7	13	0	AM	F
1939	7	14	0	AM	F
1939	7	15	0.14	AM	F
1939	7	16	0	AM	F
1939	7	17	0	AM	F
1939	7	18	0.49	AM	F
1939	7	19 T		AM	F
1939	7	20	0	AM	F
1939	7	21	0	AM	F
1939	7	22	0	AM	F
1939	7	23	0	AM	F
1939	7	24	0	AM	F
1939	7	25	0.11	AM	F
1939	7	26	0	AM	F
1939	7	27	0	AM	F
1939	7	28	0.11	AM	F
1939	7	29	0	AM	F
1939	7	30	0	AM	F
1939	7	31	0	AM	F

1939	8	1	0	AM	F
1939	8	2	0	AM	F
1939	8	3	0	AM	F
1939	8	4	0	AM	F
1939	8	5	0	AM	F
1939	8	6 T		AM	F
1939	8	7	1.02	AM	F
1939	8	8	0	AM	F
1939	8	9	0	AM	F
1939	8	10	0	AM	F
1939	8	11 T		AM	F
1939	8	12	0.73	AM	F
1939	8	13	0	AM	F
1939	8	14	0	AM	F
1939	8	15	0	AM	F
1939	8	16	0	AM	F
1939	8	17	0	AM	F
1939	8	18	0.81	AM	F
1939	8	19	0	AM	F
1939	8	20	0.11	AM	F
1939	8	21	0	AM	F
1939	8	22	0	AM	F
1939	8	23	0.41	AM	F
1939	8	24	0	AM	F
1939	8	25	0	AM	F
1939	8	26	0	AM	F
1939	8	27	0	AM	F
1939	8	28	0	AM	F
1939	8	29	0	AM	F
1939	8	30	0	AM	F
1939	8	31	0	AM	F
1939	9	1	0	AM	F
1939	9	2	0	AM	F
1939	9	3	0.21	AM	F
1939	9	4	0	AM	F
1939	9	5	0	AM	F
1939	9	6	0	AM	F
1939	9	7	0	AM	F
1939	9	8	0	AM	F
1939	9	9	0	AM	F
1939	9	10	0	AM	F
1939	9	11	0	AM	F
1939	9	12	0	AM	F
1939	9	13	0	AM	F
1939	9	14	0	AM	F
1939	9	15	0	AM	F
1939	9	16	0	AM	F
1939	9	17	0	AM	F
1939	9	18	0	AM	F
1939	9	19	0	AM	F
1939	9	20	0	AM	F
1939	9	21	0	AM	F
1939	9	22	0	AM	F
1939	9	23	0	AM	F
1939	9	24	0	AM	F
1939	9	25	0	AM	F
1939	9	26 T		AM	F
1939	9	27	0	AM	F
1939	9	28	0	AM	F
1939	9	29 T		AM	F
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1939	10	2	0	AM	F
1939	10	3	0	AM	F
1939	10	4	0	AM	F
1939	10	5 T		AM	F
1939	10	6	0	AM	F
1939	10	7	0.21	AM	F
1939	10	8	0.2	AM	F
1939	10	9	0.67	AM	F
1939	10	10	1.23	AM	F
1939	10	11	0	AM	F
1939	10	12	0	AM	F
1939	10	13 T		AM	F
1939	10	14	0	AM	F
1939	10	15	0	AM	F
1939	10	16	0	AM	F
1939	10	17	0	AM	F
1939	10	18	0	AM	F
1939	10	19	0.02	AM	F
1939	10	20	0	AM	F
1939	10	21	0	AM	F
1939	10	22	0	AM	F
1939	10	23	0	AM	F
1939	10	24	0	AM	F
1939	10	25	0	AM	F
1939	10	26	0.09	AM	F
1939	10	27	0.31	AM	F
1939	10	28	0	AM	F
1939	10	29	0	AM	F
1939	10	30	0.06	AM	F
1939	10	31	0	AM	F
1939	11	1	0	AM	F
1939	11	2	0	AM	F
1939	11	3 T		AM	F
1939	11	4	0	AM	F
1939	11	5	0	AM	F
1939	11	6	0	AM	F
1939	11	7	0	AM	F
1939	11	8	0	AM	F
1939	11	9	0	AM	F
1939	11	10	0.37	AM	F
1939	11	11	0	AM	F
1939	11	12	0	AM	F
1939	11	13	0	AM	F
1939	11	14	0	AM	F
1939	11	15	0	AM	F
1939	11	16	0	AM	F
1939	11	17	0	AM	F
1939	11	18	0.12	AM	F
1939	11	19	0.1	AM	F
1939	11	20	0	AM	F
1939	11	21 T		AM	F
1939	11	22	0	AM	F
1939	11	23	0	AM	F

1939	11	24	0.11	AM	F
1939	11	25	T	AM	F
1939	11	26	0	AM	F
1939	11	27	0	AM	F
1939	11	28	0	AM	F
1939	11	29	0	AM	F
1939	11	30	0.05	AM	F
1939	12	1	0.4	AM	F
1939	12	2	0.3	AM	F
1939	12	3	T	AM	F
1939	12	4	0	AM	F
1939	12	5	0	AM	F
1939	12	6	0	AM	F
1939	12	7	0	AM	F
1939	12	8	0	AM	F
1939	12	9	0	AM	F
1939	12	10	0	AM	F
1939	12	11	0	AM	F
1939	12	12	0.03	AM	F
1939	12	13	0	AM	F
1939	12	14	0	AM	F
1939	12	15	0	AM	F
1939	12	16	0	AM	F
1939	12	17	0	AM	F
1939	12	18	0	AM	F
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1939	12	20	T	AM	F
1939	12	21	T	AM	F
1939	12	22	0	AM	F
1939	12	23	0	AM	F
1939	12	24	0	AM	F
1939	12	25	0	AM	F
1939	12	26	0	AM	F
1939	12	27	0.31	AM	F
1939	12	28	0.04	AM	F
1939	12	29	0.04	AM	F
1939	12	30	0.01	AM	F
1939	12	31	0	AM	F
1940	1	1	0	AM	F
1940	1	2	0	AM	F
1940	1	3	0	AM	F
1940	1	4	0.05	AM	F
1940	1	5	0	AM	F
1940	1	6	0	AM	F
1940	1	7	0.37	AM	F
1940	1	8	T	AM	F
1940	1	9	0	AM	F
1940	1	10	T	AM	F
1940	1	11	0.11	AM	F
1940	1	12	0	AM	F
1940	1	13	0.18	AM	F
1940	1	14	0.39	AM	F
1940	1	15	0	AM	F
1940	1	16	0	AM	F
1940	1	17	0.03	AM	F
1940	1	18	0	AM	F
1940	1	19	0	AM	F
1940	1	20	0	AM	F
1940	1	21	0	AM	F
1940	1	22	0	AM	F
1940	1	23	T	AM	F
1940	1	24	0	AM	F
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1940	1	31	0	AM	F
1940	2	1	0	AM	F
1940	2	2	0	AM	F
1940	2	3	0	AM	F
1940	2	4	0.04	AM	F
1940	2	5	0	AM	F
1940	2	6	0	AM	F
1940	2	7	T	AM	F
1940	2	8	0.11	AM	F
1940	2	9	0.08	AM	F
1940	2	10	0	AM	F
1940	2	11	0	AM	F
1940	2	12	0	AM	F
1940	2	13	0	AM	F
1940	2	14	T	AM	F
1940	2	15	0	AM	F
1940	2	16	0	AM	F
1940	2	17	0	AM	F
1940	2	18	0.1	AM	F
1940	2	19	0.18	AM	F
1940	2	20	0	AM	F
1940	2	21	T	AM	F
1940	2	22	0.04	AM	F
1940	2	23	T	AM	F
1940	2	24	0.1	AM	F
1940	2	25	0	AM	F
1940	2	26	0	AM	F
1940	2	27	0.05	AM	F
1940	2	28	0.22	AM	F
1940	2	29	0	AM	F
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1940	3	2	0.8	AM	F
1940	3	3	0.75	AM	F
1940	3	4	0.07	AM	F
1940	3	5	T	AM	F
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1940	3	8	0	AM	F
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1940	3	12	0.18	AM	F
1940	3	13	0.02	AM	F
1940	3	14	0	AM	F
1940	3	15	T	AM	F
1940	3	16	0	AM	F
1940	3	17	0	AM	F

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1940	3	19	0	AM	F
1940	3	20	0	AM	F
1940	3	21 T		AM	F
1940	3	22	0	AM	F
1940	3	23	0.04	AM	F
1940	3	24	0	AM	F
1940	3	25	0	AM	F
1940	3	26	0	AM	F
1940	3	27	0	AM	F
1940	3	28	0.45	AM	F
1940	3	29	0.2	AM	F
1940	3	30	0	AM	F
1940	3	31	0	AM	F
1940	4	1	0	AM	F
1940	4	2	0	AM	F
1940	4	3	0	AM	F
1940	4	4	0	AM	F
1940	4	5	0	AM	F
1940	4	6	0	AM	F
1940	4	7	0.4	AM	F
1940	4	8	0.2	AM	F
1940	4	9	0	AM	F
1940	4	10 T		AM	F
1940	4	11	0.45	AM	F
1940	4	12	0	AM	F
1940	4	13	0	AM	F
1940	4	14	0	AM	F
1940	4	15	0	AM	F
1940	4	16	0	AM	F
1940	4	17	0.2	AM	F
1940	4	18	0	AM	F
1940	4	19	0	AM	F
1940	4	20	0	AM	F
1940	4	21	0	AM	F
1940	4	22	0	AM	F
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1940	4	24	0	AM	F
1940	4	25	0	AM	F
1940	4	26	0.06	AM	F
1940	4	27	0	AM	F
1940	4	28	0	AM	F
1940	4	29	0.43	AM	F
1940	4	30	2.05	AM	F
1940	5	1	0.75	AM	F
1940	5	2 T		AM	F
1940	5	3	0	AM	F
1940	5	4	0	AM	F
1940	5	5	0	AM	F
1940	5	6	0	AM	F
1940	5	7	0	AM	F
1940	5	8 T		AM	F
1940	5	9	0	AM	F
1940	5	10	0.05	AM	F
1940	5	11	0	AM	F
1940	5	12	0	AM	F
1940	5	13	0	AM	F
1940	5	14	0.6	AM	F
1940	5	15	0.1	AM	F
1940	5	16	0	AM	F
1940	5	17	0	AM	F
1940	5	18	0.31	AM	F
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1940	5	20	0	AM	F
1940	5	21	0.03	AM	F
1940	5	22	0	AM	F
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1940	5	25	0.71	AM	F
1940	5	26	0.07	AM	F
1940	5	27	0.11	AM	F
1940	5	28	0.17	AM	F
1940	5	29	0.07	AM	F
1940	5	30	0.04	AM	F
1940	5	31 T		AM	F
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1940	6	2	0	AM	F
1940	6	3	0	AM	F
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1940	6	8	0	AM	F
1940	6	9	0	AM	F
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1940	6	13	0	AM	F
1940	6	14	0	AM	F
1940	6	15	0	AM	F
1940	6	16	0	AM	F
1940	6	17	0.21	AM	F
1940	6	18 T		AM	F
1940	6	19 T		AM	F
1940	6	20	0	AM	F
1940	6	21	0	AM	F
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1940	6	24	0.56	AM	F
1940	6	25	0	AM	F
1940	6	26 T		AM	F
1940	6	27	0	AM	F
1940	6	28	0	AM	F
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1940	6	30 T		AM	F
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1940	7	5	0	AM	F
1940	7	6	0	AM	F
1940	7	7	0	AM	F
1940	7	8	0	AM	F
1940	7	9	0	AM	F
1940	7	10	0	AM	F

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1940	7	12	0.61	AM	F
1940	7	13	0	AM	F
1940	7	14	0	AM	F
1940	7	15	0	AM	F
1940	7	16	0	AM	F
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1940	7	27	0	AM	F
1940	7	28	0	AM	F
1940	7	29	0	AM	F
1940	7	30	0	AM	F
1940	7	31	0	AM	F
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1940	8	2	0	AM	F
1940	8	3	0	AM	F
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1940	8	5	0.04	AM	F
1940	8	6	0	AM	F
1940	8	7	0	AM	F
1940	8	8	0	AM	F
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1940	8	10	0.14	AM	F
1940	8	11	0.04	AM	F
1940	8	12	0	AM	F
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1940	8	16	0	AM	F
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1940	8	19	0	AM	F
1940	8	20	0	AM	F
1940	8	21	0	AM	F
1940	8	22	0	AM	F
1940	8	23	0.04	AM	F
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1940	8	28	0	AM	F
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1940	8	30	0	AM	F
1940	8	31	0	AM	F
1940	9	1	0	AM	F
1940	9	2	0	AM	F
1940	9	3	0	AM	F
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1940	9	5	0	AM	F
1940	9	6	0	AM	F
1940	9	7	0	AM	F
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1940	9	10	0	AM	F
1940	9	11	0	AM	F
1940	9	12	0	AM	F
1940	9	13	0	AM	F
1940	9	14	0	AM	F
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1940	9	19	0	AM	F
1940	9	20	0	AM	F
1940	9	21	0	AM	F
1940	9	22	0	AM	F
1940	9	23	0.11	AM	F
1940	9	24	0.08	AM	F
1940	9	25	0	AM	F
1940	9	26	0	AM	F
1940	9	27	0	AM	F
1940	9	28	0	AM	F
1940	9	29	0	AM	F
1940	9	30	0	AM	F
1940	10	1	0	AM	F
1940	10	2	0	AM	F
1940	10	3	0	AM	F
1940	10	4	0.07	AM	F
1940	10	5	0.08	AM	F
1940	10	6	1.22	AM	F
1940	10	7	0	AM	F
1940	10	8	0	AM	F
1940	10	9	0	AM	F
1940	10	10	0	AM	F
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1940	10	12	0	AM	F
1940	10	13	0	AM	F
1940	10	14	0.41	AM	F
1940	10	15	0.05	AM	F
1940	10	16	0	AM	F
1940	10	17	0	AM	F
1940	10	18	0	AM	F
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1940	10	20	0	AM	F
1940	10	21	0	AM	F
1940	10	22	0	AM	F
1940	10	23	0	AM	F
1940	10	24	0	AM	F
1940	10	25	0	AM	F
1940	10	26	0	AM	F
1940	10	27	0	AM	F
1940	10	28	0.04	AM	F
1940	10	29	0.9	AM	F
1940	10	30	0	AM	F
1940	10	31	0	AM	F
1940	11	1	0.22	AM	F
1940	11	2	T	AM	F

1940	11	3	0	AM	F
1940	11	4	0.02	AM	F
1940	11	5	0	AM	F
1940	11	6	0	AM	F
1940	11	7	0	AM	F
1940	11	8	0	AM	F
1940	11	9	0	AM	F
1940	11	10	0.31	AM	F
1940	11	11	0.08	AM	F
1940	11	12	0	AM	F
1940	11	13	0	AM	F
1940	11	14	0	AM	F
1940	11	15	0	AM	F
1940	11	16	0	AM	F
1940	11	17	0	AM	F
1940	11	18	0	AM	F
1940	11	19	0	AM	F
1940	11	20	0.22	AM	F
1940	11	21	0.48	AM	F
1940	11	22	0	AM	F
1940	11	23	0.49	AM	F
1940	11	24	0	AM	F
1940	11	25	0	AM	F
1940	11	26	1.3	AM	F
1940	11	27	T	AM	F
1940	11	28	0	AM	F
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1940	12	3	0	AM	F
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1940	12	5	0	AM	F
1940	12	6	0	AM	F
1940	12	7	0	AM	F
1940	12	8	0	AM	F
1940	12	9	0	AM	F
1940	12	10	0	AM	F
1940	12	11	0.06	AM	F
1940	12	12	0.11	AM	F
1940	12	13	T	AM	F
1940	12	14	0	AM	F
1940	12	15	0.15	AM	F
1940	12	16	T	AM	F
1940	12	17	0	AM	F
1940	12	18	0	AM	F
1940	12	19	T	AM	F
1940	12	20	0	AM	F
1940	12	21	0	AM	F
1940	12	22	0	AM	F
1940	12	23	T	AM	F
1940	12	24	T	AM	F
1940	12	25	0.11	AM	F
1940	12	26	T	AM	F
1940	12	27	0.04	AM	F
1940	12	28	T	AM	F
1940	12	29	0.02	AM	F
1940	12	30	0	AM	F
1940	12	31	0.03	AM	F
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1941	1	2	0	AM	F
1941	1	3	0	AM	F
1941	1	4	T	AM	F
1941	1	5	0	AM	F
1941	1	6	0	AM	F
1941	1	7	T	AM	F
1941	1	8	0.04	AM	F
1941	1	9	T	AM	F
1941	1	10	0	AM	F
1941	1	11	0	AM	F
1941	1	12	0	AM	F
1941	1	13	0	AM	F
1941	1	14	0.15	AM	F
1941	1	15	0.04	AM	F
1941	1	16	0.09	AM	F
1941	1	17	0.18	AM	F
1941	1	18	0.18	AM	F
1941	1	19	T	AM	F
1941	1	20	0	AM	F
1941	1	21	0	AM	F
1941	1	22	0	AM	F
1941	1	23	0	AM	F
1941	1	24	0.11	AM	F
1941	1	25	0	AM	F
1941	1	26	0.2	AM	F
1941	1	27	T	AM	F
1941	1	28	0	AM	F
1941	1	29	T	AM	F
1941	1	30	0	AM	F
1941	1	31	0	AM	F
1941	2	1	0	AM	F
1941	2	2	0	AM	F
1941	2	3	0	AM	F
1941	2	4	T	AM	F
1941	2	5	0.04	AM	F
1941	2	6	0.02	AM	F
1941	2	7	0.04	AM	F
1941	2	8	0.01	AM	F
1941	2	9	0	AM	F
1941	2	10	0	AM	F
1941	2	11	0	AM	F
1941	2	12	0	AM	F
1941	2	13	0.31	AM	F
1941	2	14	T	AM	F
1941	2	15	0	AM	F
1941	2	16	0.2	AM	F
1941	2	17	0	AM	F
1941	2	18	T	AM	F
1941	2	19	0	AM	F
1941	2	20	0	AM	F
1941	2	21	0	AM	F
1941	2	22	0	AM	F
1941	2	23	0	AM	F
1941	2	24	T	AM	F
1941	2	25	0	AM	F

1941	2	26	0.02	AM	F
1941	2	27	T	AM	F
1941	2	28	0.01	AM	F
1941	3	1	0	AM	F
1941	3	2	0	AM	F
1941	3	3	0.04	AM	F
1941	3	4	T	AM	F
1941	3	5	0	AM	F
1941	3	6	0	AM	F
1941	3	7	0	AM	F
1941	3	8	0	AM	F
1941	3	9	0	AM	F
1941	3	10	0.18	AM	F
1941	3	11	0	AM	F
1941	3	12	0	AM	F
1941	3	13	0	AM	F
1941	3	14	0	AM	F
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1941	3	16	0	AM	F
1941	3	17	0	AM	F
1941	3	18	0	AM	F
1941	3	19	0	AM	F
1941	3	20	0	AM	F
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1941	3	23	0	AM	F
1941	3	24	0	AM	F
1941	3	25	0	AM	F
1941	3	26	0	AM	F
1941	3	27	0	AM	F
1941	3	28	0.04	AM	F
1941	3	29	0	AM	F
1941	3	30	0	AM	F
1941	3	31	0.18	AM	F
1941	4	1	0.12	AM	F
1941	4	2	0.05	AM	F
1941	4	3	0.83	AM	F
1941	4	4	0.8	AM	F
1941	4	5	0.21	AM	F
1941	4	6	0	AM	F
1941	4	7	0	AM	F
1941	4	8	T	AM	F
1941	4	9	0.21	AM	F
1941	4	10	0	AM	F
1941	4	11	0	AM	F
1941	4	12	0	AM	F
1941	4	13	0	AM	F
1941	4	14	0.13	AM	F
1941	4	15	0	AM	F
1941	4	16	0.56	AM	F
1941	4	17	0.13	AM	F
1941	4	18	0.12	AM	F
1941	4	19	0.95	AM	F
1941	4	20	0.26	AM	F
1941	4	21	0	AM	F
1941	4	22	0	AM	F
1941	4	23	0	AM	F
1941	4	24	0	AM	F
1941	4	25	0	AM	F
1941	4	26	0	AM	F
1941	4	27	0	AM	F
1941	4	28	0	AM	F
1941	4	29	0	AM	F
1941	4	30	0	AM	F
1941	5	1	T	AM	F
1941	5	2	0	AM	F
1941	5	3	0	AM	F
1941	5	4	0	AM	F
1941	5	5	0.1	AM	F
1941	5	6	0.11	AM	F
1941	5	7	0	AM	F
1941	5	8	0.05	AM	F
1941	5	9	0	AM	F
1941	5	10	0	AM	F
1941	5	11	0	AM	F
1941	5	12	T	AM	F
1941	5	13	0	AM	F
1941	5	14	1.1	AM	F
1941	5	15	0	AM	F
1941	5	16	0.44	AM	F
1941	5	17	0	AM	F
1941	5	18	0	AM	F
1941	5	19	0	AM	F
1941	5	20	0	AM	F
1941	5	21	0	AM	F
1941	5	22	0	AM	F
1941	5	23	0.44	AM	F
1941	5	24	0	AM	F
1941	5	25	0	AM	F
1941	5	26	0	AM	F
1941	5	27	0	AM	F
1941	5	28	0	AM	F
1941	5	29	0	AM	F
1941	5	30	0	AM	F
1941	5	31	0.42	AM	F
1941	6	1	0.14	AM	F
1941	6	2	0.44	AM	F
1941	6	3	0	AM	F
1941	6	4	0	AM	F
1941	6	5	0	AM	F
1941	6	6	0	AM	F
1941	6	7	0	AM	F
1941	6	8	0	AM	F
1941	6	9	0.42	AM	F
1941	6	10	0.61	AM	F
1941	6	11	0.41	AM	F
1941	6	12	0	AM	F
1941	6	13	0.21	AM	F
1941	6	14	0.11	AM	F
1941	6	15	0.21	AM	F
1941	6	16	0	AM	F
1941	6	17	0	AM	F
1941	6	18	0	AM	F
1941	6	19	0	AM	F
1941	6	20	0	AM	F

1941	6	21		0	AM	F
1941	6	22		0.75	AM	F
1941	6	23		0	AM	F
1941	6	24		0	AM	F
1941	6	25		0	AM	F
1941	6	26		0	AM	F
1941	6	27		0	AM	F
1941	6	28		0	AM	F
1941	6	29		1.05	AM	F
1941	6	30		0	AM	F
1941	7	1		0.21	AM	F
1941	7	2		0	AM	F
1941	7	3		2.25	AM	F
1941	7	4		0	AM	F
1941	7	5		0	AM	F
1941	7	6		0	AM	F
1941	7	7		0	AM	F
1941	7	8		0.06	AM	F
1941	7	9	T		AM	F
1941	7	10	T		AM	F
1941	7	11		0	AM	F
1941	7	12		0	AM	F
1941	7	13		0	AM	F
1941	7	14		0	AM	F
1941	7	15		0	AM	F
1941	7	16	T		AM	F
1941	7	17		0	AM	F
1941	7	18		0.06	AM	F
1941	7	19		0	AM	F
1941	7	20		0	AM	F
1941	7	21		0	AM	F
1941	7	22		0	AM	F
1941	7	23		0.95	AM	F
1941	7	24	T		AM	F
1941	7	25		0	AM	F
1941	7	26		0	AM	F
1941	7	27		0	AM	F
1941	7	28		0	AM	F
1941	7	29		0	AM	F
1941	7	30		0	AM	F
1941	7	31		0	AM	F
1941	8	1		0	AM	F
1941	8	2		0	AM	F
1941	8	3		0	AM	F
1941	8	4		0	AM	F
1941	8	5		0.12	AM	F
1941	8	6		0	AM	F
1941	8	7		0	AM	F
1941	8	8		0	AM	F
1941	8	9		0	AM	F
1941	8	10		0	AM	F
1941	8	11		0	AM	F
1941	8	12		0.25	AM	F
1941	8	13		0	AM	F
1941	8	14		0.3	AM	F
1941	8	15		0.04	AM	F
1941	8	16		0	AM	F
1941	8	17		0.4	AM	F
1941	8	18		0.9	AM	F
1941	8	19		0	AM	F
1941	8	20		0	AM	F
1941	8	21		0	AM	F
1941	8	22		0	AM	F
1941	8	23		0	AM	F
1941	8	24		0.11	AM	F
1941	8	25		0	AM	F
1941	8	26		0.97	AM	F
1941	8	27		0	AM	F
1941	8	28		0	AM	F
1941	8	29		0	AM	F
1941	8	30		0	AM	F
1941	8	31		0	AM	F
1941	9	1		0	AM	F
1941	9	2		0.11	AM	F
1941	9	3		0.02	AM	F
1941	9	4		0	AM	F
1941	9	5		0	AM	F
1941	9	6		0	AM	F
1941	9	7		3.1	AM	F
1941	9	8		0	AM	F
1941	9	9		0.66	AM	F
1941	9	10		0.11	AM	F
1941	9	11		0	AM	F
1941	9	12		0	AM	F
1941	9	13		0	AM	F
1941	9	14		0	AM	F
1941	9	15		0	AM	F
1941	9	16	T		AM	F
1941	9	17		0	AM	F
1941	9	18		0	AM	F
1941	9	19		0	AM	F
1941	9	20		0	AM	F
1941	9	21		0	AM	F
1941	9	22		0	AM	F
1941	9	23		0	AM	F
1941	9	24		0	AM	F
1941	9	25		1.3	AM	F
1941	9	26		0	AM	F
1941	9	27		0	AM	F
1941	9	28		0.26	AM	F
1941	9	29		0.05	AM	F
1941	9	30		0.34	AM	F
1941	10	1		0	AM	F
1941	10	2		0.45	AM	F
1941	10	3		0.12	AM	F
1941	10	4		2.75	AM	F
1941	10	5		0.75	AM	F
1941	10	6		1.6	AM	F
1941	10	7		0.7	AM	F
1941	10	8		0	AM	F
1941	10	9		1.5	AM	F
1941	10	10		0	AM	F
1941	10	11		0	AM	F
1941	10	12		0	AM	F
1941	10	13	T		AM	F

1941	10	14	0	AM	F
1941	10	15	0	AM	F
1941	10	16	0	AM	F
1941	10	17	0.08	AM	F
1941	10	18	0.42	AM	F
1941	10	19	0	AM	F
1941	10	20	0	AM	F
1941	10	21	0.65	AM	F
1941	10	22	0.11	AM	F
1941	10	23	0	AM	F
1941	10	24	0	AM	F
1941	10	25	0	AM	F
1941	10	26	0.11	AM	F
1941	10	27	0.5	AM	F
1941	10	28	0	AM	F
1941	10	29	0.14	AM	F
1941	10	30	0.86	AM	F
1941	10	31	1	AM	F
1941	11	1	0.86	AM	F
1941	11	2	0	AM	F
1941	11	3	0	AM	F
1941	11	4	0	AM	F
1941	11	5	0.24	AM	F
1941	11	6	1.12	AM	F
1941	11	7 T		AM	F
1941	11	8	0.08	AM	F
1941	11	9 T		AM	F
1941	11	10	0	AM	F
1941	11	11	0	AM	F
1941	11	12	0	AM	F
1941	11	13	0	AM	F
1941	11	14	0	AM	F
1941	11	15	0	AM	F
1941	11	16	0	AM	F
1941	11	17	0	AM	F
1941	11	18	0	AM	F
1941	11	19	0.27	AM	F
1941	11	20	0.21	AM	F
1941	11	21	0	AM	F
1941	11	22	0.25	AM	F
1941	11	23	0.27	AM	F
1941	11	24	0	AM	F
1941	11	25	0	AM	F
1941	11	26	0	AM	F
1941	11	27	0	AM	F
1941	11	28	0	AM	F
1941	11	29	0	AM	F
1941	11	30	0	AM	F
1941	12	1	0.05	AM	F
1941	12	2 T		AM	F
1941	12	3 T		AM	F
1941	12	4 T		AM	F
1941	12	5	0	AM	F
1941	12	6	0	AM	F
1941	12	7	0	AM	F
1941	12	8	0	AM	F
1941	12	9	0	AM	F
1941	12	10	0	AM	F
1941	12	11	0	AM	F
1941	12	12	0.06	AM	F
1941	12	13	0	AM	F
1941	12	14	0	AM	F
1941	12	15	0	AM	F
1941	12	16	0	AM	F
1941	12	17	0	AM	F
1941	12	18	0	AM	F
1941	12	19	0	AM	F
1941	12	20	0	AM	F
1941	12	21	0	AM	F
1941	12	22	1	AM	F
1941	12	23	0.26	AM	F
1941	12	24	0	AM	F
1941	12	25	0.06	AM	F
1941	12	26	0.19	AM	F
1941	12	27 T		AM	F
1941	12	28 T		AM	F
1941	12	29 T		AM	F
1941	12	30	0.04	AM	F
1941	12	31 T		AM	F
1942	1	1	0.18	AM	F
1942	1	2 T		AM	F
1942	1	3	0	AM	F
1942	1	4	0	AM	F
1942	1	5	0	AM	F
1942	1	6	0	AM	F
1942	1	7	0	AM	F
1942	1	8	0	AM	F
1942	1	9	0.25	AM	F
1942	1	10	0	AM	F
1942	1	11	0	AM	F
1942	1	12	0	AM	F
1942	1	13	0	AM	F
1942	1	14	0	AM	F
1942	1	15	0	AM	F
1942	1	16	0	AM	F
1942	1	17 T		AM	F
1942	1	18	0.15	AM	F
1942	1	19	0	AM	F
1942	1	20	0	AM	F
1942	1	21	0	AM	F
1942	1	22	0	AM	F
1942	1	23	0	AM	F
1942	1	24	0	AM	F
1942	1	25	0	AM	F
1942	1	26	0	AM	F
1942	1	27 T		AM	F
1942	1	28	0	AM	F
1942	1	29	0	AM	F
1942	1	30	0.32	AM	F
1942	1	31	0.67	AM	F
1942	2	1	0.05	AM	F
1942	2	2	0	AM	F
1942	2	3	0	AM	F
1942	2	4	1.76	AM	F
1942	2	5	0.7	AM	F

1942	2	6	0.62	AM	F
1942	2	7	T	AM	F
1942	2	8	0	AM	F
1942	2	9	0.26	AM	F
1942	2	10	0.11	AM	F
1942	2	11	T	AM	F
1942	2	12	0.02	AM	F
1942	2	13	T	AM	F
1942	2	14	0	AM	F
1942	2	15	0.21	AM	F
1942	2	16	0	AM	F
1942	2	17	0.03	AM	F
1942	2	18	0.02	AM	F
1942	2	19	0	AM	F
1942	2	20	0.06	AM	F
1942	2	21	0	AM	F
1942	2	22	0	AM	F
1942	2	23	0.06	AM	F
1942	2	24	T	AM	F
1942	2	25	T	AM	F
1942	2	26	T	AM	F
1942	2	27	0	AM	F
1942	2	28	0	AM	F
1942	3	1	0	AM	F
1942	3	2	0.08	AM	F
1942	3	3	0	AM	F
1942	3	4	0	AM	F
1942	3	5	0.09	AM	F
1942	3	6	0	AM	F
1942	3	7	0.11	AM	F
1942	3	8	0.3	AM	F
1942	3	9	0.06	AM	F
1942	3	10	0	AM	F
1942	3	11	0	AM	F
1942	3	12	0	AM	F
1942	3	13	0.2	AM	F
1942	3	14	T	AM	F
1942	3	15	0.04	AM	F
1942	3	16	0.7	AM	F
1942	3	17	0.73	AM	F
1942	3	18	T	AM	F
1942	3	19	0	AM	F
1942	3	20	0.02	AM	F
1942	3	21	0.02	AM	F
1942	3	22	0	AM	F
1942	3	23	0	AM	F
1942	3	24	0	AM	F
1942	3	25	0	AM	F
1942	3	26	0.42	AM	F
1942	3	27	0.22	AM	F
1942	3	28	0.03	AM	F
1942	3	29	0.06	AM	F
1942	3	30	0.06	AM	F
1942	3	31	0.09	AM	F
1942	4	1	0	AM	F
1942	4	2	0	AM	F
1942	4	3	0.12	AM	F
1942	4	4	0	AM	F
1942	4	5	0	AM	F
1942	4	6	0.75	AM	F
1942	4	7	0.73	AM	F
1942	4	8	0.12	AM	F
1942	4	9	0.41	AM	F
1942	4	10	0.07	AM	F
1942	4	11	0	AM	F
1942	4	12	0	AM	F
1942	4	13	0.06	AM	F
1942	4	14	0	AM	F
1942	4	15	0	AM	F
1942	4	16	0	AM	F
1942	4	17	0.12	AM	F
1942	4	18	0	AM	F
1942	4	19	0	AM	F
1942	4	20	0	AM	F
1942	4	21	0	AM	F
1942	4	22	0	AM	F
1942	4	23	0	AM	F
1942	4	24	T	AM	F
1942	4	25	T	AM	F
1942	4	26	0.12	AM	F
1942	4	27	0.05	AM	F
1942	4	28	0	AM	F
1942	4	29	0	AM	F
1942	4	30	0	AM	F
1942	5	1	0	AM	F
1942	5	2	0.26	AM	F
1942	5	3	0	AM	F
1942	5	4	0	AM	F
1942	5	5	0	AM	F
1942	5	6	0.85	AM	F
1942	5	7	0	AM	F
1942	5	8	T	AM	F
1942	5	9	0	AM	F
1942	5	10	0.1	AM	F
1942	5	11	0.11	AM	F
1942	5	12	0.12	AM	F
1942	5	13	0.21	AM	F
1942	5	14	0	AM	F
1942	5	15	1.1	AM	F
1942	5	16	0	AM	F
1942	5	17	0.04	AM	F
1942	5	18	0.52	AM	F
1942	5	19	0	AM	F
1942	5	20	T	AM	F
1942	5	21	0	AM	F
1942	5	22	0	AM	F
1942	5	23	0	AM	F
1942	5	24	0	AM	F
1942	5	25	0	AM	F
1942	5	26	T	AM	F
1942	5	27	0	AM	F
1942	5	28	0	AM	F
1942	5	29	0	AM	F
1942	5	30	0	AM	F
1942	5	31	0	AM	F

1942	6	1	0	AM	F
1942	6	2	0	AM	F
1942	6	3	0	AM	F
1942	6	4	0.05	AM	F
1942	6	5	0	AM	F
1942	6	6	0.16	AM	F
1942	6	7	0.17	AM	F
1942	6	8	0.02	AM	F
1942	6	9	0.55	AM	F
1942	6	10	0	AM	F
1942	6	11	1.1	AM	F
1942	6	12	0.11	AM	F
1942	6	13	1.01	AM	F
1942	6	14	0.07	AM	F
1942	6	15 T		AM	F
1942	6	16	0	AM	F
1942	6	17	0	AM	F
1942	6	18	0	AM	F
1942	6	19	0.61	AM	F
1942	6	20	0.08	AM	F
1942	6	21	0	AM	F
1942	6	22	0	AM	F
1942	6	23	0	AM	F
1942	6	24	0	AM	F
1942	6	25	0.11	AM	F
1942	6	26	2.52	AM	F
1942	6	27	0	AM	F
1942	6	28	0	AM	F
1942	6	29	0	AM	F
1942	6	30	0	AM	F
1942	7	1	0	AM	F
1942	7	2	0	AM	F
1942	7	3	0.02	AM	F
1942	7	4	0.13	AM	F
1942	7	5	0	AM	F
1942	7	6	1.23	AM	F
1942	7	7	0	AM	F
1942	7	8	1.87	AM	F
1942	7	9	0	AM	F
1942	7	10	1.07	AM	F
1942	7	11	0	AM	F
1942	7	12	0.07	AM	F
1942	7	13	0.61	AM	F
1942	7	14	0.61	AM	F
1942	7	15	0.45	AM	F
1942	7	16	0	AM	F
1942	7	17	0	AM	F
1942	7	18	0	AM	F
1942	7	19	0	AM	F
1942	7	20	0.04	AM	F
1942	7	21	0	AM	F
1942	7	22	0	AM	F
1942	7	23	0	AM	F
1942	7	24	0	AM	F
1942	7	25	0	AM	F
1942	7	26	0	AM	F
1942	7	27	0	AM	F
1942	7	28	0	AM	F
1942	7	29	0.87	AM	F
1942	7	30	0	AM	F
1942	7	31	0	AM	F
1942	8	1	0	AM	F
1942	8	2	0	AM	F
1942	8	3	0	AM	F
1942	8	4	0	AM	F
1942	8	5	0	AM	F
1942	8	6	0	AM	F
1942	8	7	0.51	AM	F
1942	8	8	0.03	AM	F
1942	8	9	0	AM	F
1942	8	10	0	AM	F
1942	8	11	0	AM	F
1942	8	12	0	AM	F
1942	8	13	0	AM	F
1942	8	14	0	AM	F
1942	8	15	0.08	AM	F
1942	8	16	0	AM	F
1942	8	17	0	AM	F
1942	8	18	0	AM	F
1942	8	19	0	AM	F
1942	8	20	0	AM	F
1942	8	21	0	AM	F
1942	8	22	0	AM	F
1942	8	23	0.42	AM	F
1942	8	24	0	AM	F
1942	8	25	0	AM	F
1942	8	26 T		AM	F
1942	8	27	0.21	AM	F
1942	8	28	0.26	AM	F
1942	8	29	0	AM	F
1942	8	30	0	AM	F
1942	8	31	0	AM	F
1942	9	1	0	AM	F
1942	9	2	0	AM	F
1942	9	3	0	AM	F
1942	9	4	0	AM	F
1942	9	5	0	AM	F
1942	9	6	0	AM	F
1942	9	7	0.21	AM	F
1942	9	8	0	AM	F
1942	9	9	0.14	AM	F
1942	9	10	1.02	AM	F
1942	9	11	0	AM	F
1942	9	12	0	AM	F
1942	9	13	0	AM	F
1942	9	14	0	AM	F
1942	9	15	0	AM	F
1942	9	16	0.21	AM	F
1942	9	17 T		AM	F
1942	9	18	0	AM	F
1942	9	19	0.64	AM	F
1942	9	20	0	AM	F
1942	9	21	0	AM	F
1942	9	22	0	AM	F
1942	9	23	0	AM	F

1942	9	24	0	AM	F
1942	9	25	0.91	AM	F
1942	9	26	2.64	AM	F
1942	9	27	0	AM	F
1942	9	28	0	AM	F
1942	9	29	0	AM	F
1942	9	30	0	AM	F
1942	10	1	0	AM	F
1942	10	2	T	AM	F
1942	10	3	0	AM	F
1942	10	4	0.17	AM	F
1942	10	5	0	AM	F
1942	10	6	0	AM	F
1942	10	7	0	AM	F
1942	10	8	0	AM	F
1942	10	9	0.11	AM	F
1942	10	10	0	AM	F
1942	10	11	0	AM	F
1942	10	12	0	AM	F
1942	10	13	0	AM	F
1942	10	14	T	AM	F
1942	10	15	0	AM	F
1942	10	16	0.01	AM	F
1942	10	17	0	AM	F
1942	10	18	0	AM	F
1942	10	19	0	AM	F
1942	10	20	0	AM	F
1942	10	21	0	AM	F
1942	10	22	0.2	AM	F
1942	10	23	0	AM	F
1942	10	24	0	AM	F
1942	10	25	0.05	AM	F
1942	10	26	0	AM	F
1942	10	27	T	AM	F
1942	10	28	0	AM	F
1942	10	29	0.65	AM	F
1942	10	30	1.75	AM	F
1942	10	31	0.15	AM	F
1942	11	1	0	AM	F
1942	11	2	0.42	AM	F
1942	11	3	0	AM	F
1942	11	4	0	AM	F
1942	11	5	0.72	AM	F
1942	11	6	0	AM	F
1942	11	7	0	AM	F
1942	11	8	0	AM	F
1942	11	9	1.26	AM	F
1942	11	10	0.78	AM	F
1942	11	11	0	AM	F
1942	11	12	0	AM	F
1942	11	13	0	AM	F
1942	11	14	0	AM	F
1942	11	15	0	AM	F
1942	11	16	0	AM	F
1942	11	17	0.24	AM	F
1942	11	18	0.16	AM	F
1942	11	19	0.02	AM	F
1942	11	20	T	AM	F
1942	11	21	0.75	AM	F
1942	11	22	1.5	AM	F
1942	11	23	0.15	AM	F
1942	11	24	0	AM	F
1942	11	25	0	AM	F
1942	11	26	0	AM	F
1942	11	27	0	AM	F
1942	11	28	0.2	AM	F
1942	11	29	0.6	AM	F
1942	11	30	0	AM	F
1942	12	1	0.04	AM	F
1942	12	2	0.06	AM	F
1942	12	3	0	AM	F
1942	12	4	0	AM	F
1942	12	5	0.4	AM	F
1942	12	6	0.08	AM	F
1942	12	7	0	AM	F
1942	12	8	T	AM	F
1942	12	9	0	AM	F
1942	12	10	0	AM	F
1942	12	11	0.06	AM	F
1942	12	12	0	AM	F
1942	12	13	0	AM	F
1942	12	14	0	AM	F
1942	12	15	0	AM	F
1942	12	16	0	AM	F
1942	12	17	0.06	AM	F
1942	12	18	0	AM	F
1942	12	19	0	AM	F
1942	12	20	0.06	AM	F
1942	12	21	0	AM	F
1942	12	22	0.21	AM	F
1942	12	23	T	AM	F
1942	12	24	0	AM	F
1942	12	25	0	AM	F
1942	12	26	0.11	AM	F
1942	12	27	0.86	AM	F
1942	12	28	T	AM	F
1942	12	29	T	AM	F
1942	12	30	T	AM	F
1942	12	31	0	AM	F
1943	1	1	0	AM	F
1943	1	2	0	AM	F
1943	1	3	0.18	AM	F
1943	1	4	T	AM	F
1943	1	5	0	AM	F
1943	1	6	0.03	AM	F
1943	1	7	0.06	AM	F
1943	1	8	0.04	AM	F
1943	1	9	0.1	AM	F
1943	1	10	0	AM	F
1943	1	11	0	AM	F
1943	1	12	0	AM	F
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1943	1	14	0	AM	F
1943	1	15	0.14	AM	F
1943	1	16	0	AM	F

1943	1	17		0	AM	F
1943	1	18		0.04	AM	F
1943	1	19		0	AM	F
1943	1	20		0	AM	F
1943	1	21		0	AM	F
1943	1	22		0	AM	F
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1943	1	25	T		AM	F
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1943	1	27		0	AM	F
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1943	2	6		0.5	AM	F
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1943	2	12		0.08	AM	F
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1943	2	15	T		AM	F
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1943	2	27		0	AM	F
1943	2	28		0	AM	F
1943	3	1	T		AM	F
1943	3	2		0.03	AM	F
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1943	3	14		0	AM	F
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1943	3	18		0.02	AM	F
1943	3	19		0.57	AM	F
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1943	3	25		0	AM	F
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1943	4	6		0	AM	F
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1943	4	14	T		AM	F
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1943	4	17		0	AM	F
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1943	4	19	T		AM	F
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1943	4	24		0	AM	F
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1943	4	29		0.36	AM	F
1943	4	30		0.08	AM	F
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1943	5	2		0.05	AM	F
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1943	5	4	T		AM	F
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1943	5	12	0	AM	F
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1943	5	14	0	AM	F
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1943	5	16	0	AM	F
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1943	5	18	1.45	AM	F
1943	5	19	0	AM	F
1943	5	20	0.43	AM	F
1943	5	21	0	AM	F
1943	5	22	0	AM	F
1943	5	23	T	AM	F
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1943	5	25	0	AM	F
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1943	5	28	0	AM	F
1943	5	29	0	AM	F
1943	5	30	T	AM	F
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1943	6	3	0	AM	F
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1943	6	12	0	AM	F
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1943	6	26	0.03	AM	F
1943	6	27	0.03	AM	F
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1943	6	29	0	AM	F
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1943	7	2	0	AM	F
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1943	7	10	0	AM	F
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1943	7	13	0	AM	F
1943	7	14	0	AM	F
1943	7	15	0	AM	F
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1943	7	19	0	AM	F
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1943	7	22	0	AM	F
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1943	7	24	0	AM	F
1943	7	25	0	AM	F
1943	7	26	0	AM	F
1943	7	27	0	AM	F
1943	7	28	0.35	AM	F
1943	7	29	0.1	AM	F
1943	7	30	0	AM	F
1943	7	31	T	AM	F
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1943	8	2	0	AM	F
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1943	8	5	0	AM	F
1943	8	6	0	AM	F
1943	8	7	0	AM	F
1943	8	8	0	AM	F
1943	8	9	0.04	AM	F
1943	8	10	0	AM	F
1943	8	11	0	AM	F
1943	8	12	0	AM	F
1943	8	13	0	AM	F
1943	8	14	0	AM	F
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1943	8	18	0	AM	F
1943	8	19	0	AM	F
1943	8	20	0	AM	F
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1943	8	22	0.51	AM	F
1943	8	23	0.06	AM	F
1943	8	24	0	AM	F
1943	8	25	0	AM	F
1943	8	26	0	AM	F
1943	8	27	0	AM	F
1943	8	28	0	AM	F
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1943	8	31	0	AM	F
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1943	9	2	0	AM	F
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1943	10	25 T		AM	F
1943	10	26 T		AM	F
1943	10	27	0	AM	F
1943	10	28	0	AM	F
1943	10	29	0	AM	F
1943	10	30	0	AM	F
1943	10	31	0.11	AM	F
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1943	11	3	0	AM	F
1943	11	4	0	AM	F
1943	11	5 T		AM	F
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1943	11	12	0	AM	F
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1943	11	18	0	AM	F
1943	11	19	0	AM	F
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1943	11	25	0	AM	F
1943	11	26	0	AM	F
1943	11	27	0	AM	F
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1943	11	30	0	AM	F
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1943	12	2	0	AM	F
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1943	12	4	0	AM	F
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1943	12	18	0	AM	F
1943	12	19	0	AM	F
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1943	12	24	0	AM	F
1943	12	25	0	AM	F
1943	12	26	0	AM	F
1943	12	27 T		AM	F

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1943	12	29	0	AM	F
1943	12	30	0	AM	F
1943	12	31	0	AM	F
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1944	1	2	0	AM	F
1944	1	3	0	AM	F
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1944	2	6	0	AM	F
1944	2	7	0	AM	F
1944	2	8	0	AM	F
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1944	2	12	0	AM	F
1944	2	13	0	AM	F
1944	2	14	0.18	AM	F
1944	2	15	0	AM	F
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1944	2	26	0.76	AM	F
1944	2	27	0	AM	F
1944	2	28	0	AM	F
1944	2	29	0	AM	F
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1944	3	9	0	AM	F
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1944	3	30	0.04	AM	F
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1944	4	5	0	AM	F
1944	4	6	0	AM	F
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1944	4	14	0.08	AM	F
1944	4	15	0.67	AM	F
1944	4	16	0	AM	F
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1944	4	20	0.16	AM	F

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1944	4	24 T		AM	F
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1944	4	27	0.04	AM	F
1944	4	28	0	AM	F
1944	4	29	0	AM	F
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1944	5	2	0	AM	F
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1944	5	4 T		AM	F
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1944	6	5	0	AM	F
1944	6	6	0	AM	F
1944	6	7	0	AM	F
1944	6	8 T		AM	F
1944	6	9	0.09	AM	F
1944	6	10	0	AM	F
1944	6	11	0	AM	F
1944	6	12 T		AM	F
1944	6	13	0	AM	F
1944	6	14	0.35	AM	F
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1944	6	18	0	AM	F
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1944	7	8	0	AM	F
1944	7	9	0	AM	F
1944	7	10	0	AM	F
1944	7	11	0.1	AM	F
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1944	7	14	0	AM	F
1944	7	15	0	AM	F
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1944	7	22	0	AM	F
1944	7	23	0	AM	F
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1944	7	29	0	AM	F
1944	7	30	0	AM	F
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1944	8	8	0	AM	F
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1944	8	12	0	AM	F
1944	8	13	0	AM	F

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1944	8	18 T		AM	F
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1944	8	29	0	AM	F
1944	8	30 T		AM	F
1944	8	31	1.65	AM	F
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1944	10	6	0	AM	F
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1944	12	28	0	AM	F
1944	12	29	0	AM	F
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1945	1	2	0	AM	F
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1945	1	5	0	AM	F
1945	1	6	0	AM	F
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1945	1	9	0	AM	F
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1945	1	13	0.09	AM	F
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1945	2	2 T		AM	F
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1945	2	12	0	AM	F
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1945	5	27	0	AM	F
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1945	6	2	0	AM	F
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1945	7	24	0	AM	F

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1945	9	17		0 AM	F
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1945	9	25		0 AM	F
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1945	11	24	0	AM	F
1945	11	25	0	AM	F
1945	11	26	0	AM	F
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1945	11	28	T	AM	F
1945	11	29	0	AM	F
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1945	12	10	T	AM	F
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1945	12	14	T	AM	F
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1946	2	27	0	AM	F
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1946	3	4	0.03	AM	F
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1946	3	15 T		AM	F
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1946	3	17 T		AM	F
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1946	3	19	0	AM	F
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1946	3	28	0	AM	F
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1946	4	12	0	AM	F
1946	4	13	0	AM	F
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1946	4	17	0	AM	F
1946	4	18	0	AM	F
1946	4	19	0	AM	F
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1946	5	4	0	AM	F
1946	5	5 T		AM	F
1946	5	6	0.3	AM	F
1946	5	7 T		AM	F
1946	5	8	0	AM	F
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1946	5	24 T		AM	F
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1946	7	4	0	AM	F

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1946	8	27	0	AM	F
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1946	10	4	0	AM	F
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1946	10	23	0	AM	F
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1946	10	25 T		AM	F
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1946	10	27	0	AM	F

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1946	11	18	0	AM	F
1946	11	19	0	AM	F
1946	11	20	0	AM	F
1946	11	21	0.05	AM	F
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1947	1	18	0	AM	F
1947	1	19	0	AM	F
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1947	1	22	T	AM	F
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1947	2	3	T	AM	F
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1947	2	7	T	AM	F
1947	2	8	T	AM	F
1947	2	9	0	AM	F
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1947	2	14	0	AM	F
1947	2	15	T	AM	F
1947	2	16	T	AM	F
1947	2	17	0	AM	F
1947	2	18	0	AM	F
1947	2	19	0	AM	F

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1947	2	23	T	AM	F
1947	2	24	T	AM	F
1947	2	25	T	AM	F
1947	2	26	T	AM	F
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1947	6	14	0	AM	F

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1947	10	7	0	AM	F

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1947	10	11	0	AM	F
1947	10	12	0	AM	F
1947	10	13	0	AM	F
1947	10	14	0	AM	F
1947	10	15	0	AM	F
1947	10	16	0	AM	F
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1947	10	20	0	AM	F
1947	10	21	0	AM	F
1947	10	22	0	AM	F
1947	10	23	0	AM	F
1947	10	24	T	AM	F
1947	10	25	0.3	AM	F
1947	10	26	1.5	AM	F
1947	10	27	0.9	AM	F
1947	10	28	0.45	AM	F
1947	10	29	0	AM	F
1947	10	30	0	AM	F
1947	10	31	0	AM	F
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1947	11	2	T	AM	F
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1947	11	22	0	AM	F
1947	11	23	0	AM	F
1947	11	24	0	AM	F
1947	11	25	T	AM	F
1947	11	26	T	AM	F
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1947	11	29	0	AM	F
1947	11	30	0	AM	F
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1948	1	2	0	AM	F
1948	1	3	0	AM	F
1948	1	4	T	AM	F
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1948	1	7	0	AM	F
1948	1	8	0	AM	F
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1948	1	22	0	AM	F
1948	1	23	0	AM	F
1948	1	24	0	AM	F
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1948	4	22	0	AM	F
1948	4	23	0	AM	F
1948	4	24	0	AM	F
1948	4	25	0	AM	F
1948	4	26	0.4	AM	F
1948	4	27	0	AM	F
1948	4	28	0	AM	F
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1948	5	23	0	AM	F
1948	5	24	0	AM	F

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1948	6	18	0	PM	F
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1948	6	23	1.12	PM	F
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1948	7	2	0	PM	F
1948	7	3	0	PM	F
1948	7	4	0	PM	F
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1948	7	6	0.5	PM	F
1948	7	7	0	PM	F
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1948	7	11	0.4	PM	F
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1948	7	18	0	PM	F
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1948	7	23	0	PM	F
1948	7	24	0	PM	F
1948	7	25	2.05	PM	F
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1948	7	27	0	PM	F
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1948	7	31	0	PM	F
1948	8	1	0	PM	F
1948	8	2	0	PM	F
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1948	8	15	0	PM	F
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1948	8	28	0	PM	F
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1948	9	14	0	PM	F
1948	9	15	0	PM	F
1948	9	16	0	PM	F

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1948	9	18	0	PM	F
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1948	10	3	0	PM	F
1948	10	4	0	PM	F
1948	10	5	0	PM	F
1948	10	6	0	PM	F
1948	10	7	0.4	PM	F
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1948	10	11	0	PM	F
1948	10	12	0	PM	F
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1948	12	1	0	PM	F
1948	12	2	0	PM	F
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1949	1	7	0	PM	F
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1949	1	22		0	PM	F
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1949	5	4	M		-	-

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1949	6	10	T	PM	F
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1949	6	12	0	PM	F
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1949	6	20	0	PM	F
1949	6	21	0.1	PM	F
1949	6	22	0	PM	F
1949	6	23	T	PM	F
1949	6	24	0	PM	F
1949	6	25	0	PM	F
1949	6	26	T	PM	F
1949	6	27	0	PM	F
1949	6	28	1.09	PM	F
1949	6	29	1.73	PM	F
1949	6	30	0	PM	F
1949	7	1	0	PM	F
1949	7	2	0.99	PM	F
1949	7	3	0	PM	F
1949	7	4	0	PM	F
1949	7	5	0.54	PM	F
1949	7	6	0	PM	F
1949	7	7	0.1	PM	F
1949	7	8	0.21	PM	F
1949	7	9	1.05	PM	F
1949	7	10	0.49	PM	F
1949	7	11	0	PM	F
1949	7	12	0	PM	F
1949	7	13	0	PM	F
1949	7	14	0	PM	F
1949	7	15	0	PM	F
1949	7	16	0	PM	F
1949	7	17	0	PM	F
1949	7	18	0	PM	F
1949	7	19	0	PM	F
1949	7	20	T	PM	F
1949	7	21	T	PM	F
1949	7	22	0.53	PM	F
1949	7	23	0.1	PM	F
1949	7	24	0	PM	F
1949	7	25	T	PM	F
1949	7	26	T	PM	F
1949	7	27	0	PM	F
1949	7	28	0	PM	F
1949	7	29	0.56	PM	F
1949	7	30	T	PM	F
1949	7	31	0	PM	F
1949	8	1	0	PM	F
1949	8	2	1.85	PM	F
1949	8	3	0	PM	F
1949	8	4	0	PM	F
1949	8	5	0	PM	F
1949	8	6	0	PM	F
1949	8	7	0	PM	F
1949	8	8	0	PM	F
1949	8	9	0	PM	F
1949	8	10	0	PM	F
1949	8	11	0.55	PM	F
1949	8	12	0	PM	F
1949	8	13	0	PM	F
1949	8	14	0	PM	F
1949	8	15	0	PM	F
1949	8	16	0	PM	F
1949	8	17	0.24	PM	F
1949	8	18	0.2	PM	F
1949	8	19	0.84	PM	F
1949	8	20	T	PM	F
1949	8	21	0	PM	F
1949	8	22	0	PM	F
1949	8	23	0	PM	F
1949	8	24	0	PM	F
1949	8	25	0	PM	F
1949	8	26	0	PM	F
1949	8	27	0	PM	F

1949	8	28	0.83	PM	F
1949	8	29	0	PM	F
1949	8	30 T		PM	F
1949	8	31	0.2	PM	F
1949	9	1	0	PM	F
1949	9	2	0	PM	F
1949	9	3	0	PM	F
1949	9	4	0.36	PM	F
1949	9	5	0	PM	F
1949	9	6	0	PM	F
1949	9	7	0	PM	F
1949	9	8	0	PM	F
1949	9	9	0	PM	F
1949	9	10	0.06	PM	F
1949	9	11	0.41	PM	F
1949	9	12	0.82	PM	F
1949	9	13	0	PM	F
1949	9	14 T		PM	F
1949	9	15 T		PM	F
1949	9	16	0	PM	F
1949	9	17	0	PM	F
1949	9	18	0.31	PM	F
1949	9	19	0	PM	F
1949	9	20	0	PM	F
1949	9	21	0.16	PM	F
1949	9	22	0	PM	F
1949	9	23	0	PM	F
1949	9	24	0	PM	F
1949	9	25	0	PM	F
1949	9	26	0	PM	F
1949	9	27	0	PM	F
1949	9	28	0	PM	F
1949	9	29	0	PM	F
1949	9	30	0	PM	F
1949	10	1	1.16	PM	F
1949	10	2	1.59	PM	F
1949	10	3	0	PM	F
1949	10	4 T		PM	F
1949	10	5 T		PM	F
1949	10	6	1.06	PM	F
1949	10	7	0	PM	F
1949	10	8	0	PM	F
1949	10	9	0	PM	F
1949	10	10 T		PM	F
1949	10	11	0.68	PM	F
1949	10	12	0	PM	F
1949	10	13	0	PM	F
1949	10	14	0	PM	F
1949	10	15	0	PM	F
1949	10	16	0	PM	F
1949	10	17	0	PM	F
1949	10	18	0	PM	F
1949	10	19 T		PM	F
1949	10	20	0.75	PM	F
1949	10	21	0.52	PM	F
1949	10	22 T		PM	F
1949	10	23	0	PM	F
1949	10	24	0	PM	F
1949	10	25	0	PM	F
1949	10	26	0	PM	F
1949	10	27	0	PM	F
1949	10	28	0	PM	F
1949	10	29	0	PM	F
1949	10	30	0	PM	F
1949	10	31	0	PM	F
1949	11	1	0	PM	F
1949	11	2	0	PM	F
1949	11	3	0	PM	F
1949	11	4	0	PM	F
1949	11	5	0	PM	F
1949	11	6	0	PM	F
1949	11	7	0	PM	F
1949	11	8	0	PM	F
1949	11	9	0	PM	F
1949	11	10	0	PM	F
1949	11	11	0	PM	F
1949	11	12	0.12	PM	F
1949	11	13 T		PM	F
1949	11	14	0.3	PM	F
1949	11	15	0	PM	F
1949	11	16	0	PM	F
1949	11	17	0	PM	F
1949	11	18	0	PM	F
1949	11	19	0	PM	F
1949	11	20	0	PM	F
1949	11	21	0	PM	F
1949	11	22	0	PM	F
1949	11	23 T		PM	F
1949	11	24	0.25	PM	F
1949	11	25	0	PM	F
1949	11	26	0	PM	F
1949	11	27	0	PM	F
1949	11	28	0	PM	F
1949	11	29	0	PM	F
1949	11	30	0	PM	F
1949	12	1	0	PM	F
1949	12	2	0	PM	F
1949	12	3	0.15	PM	F
1949	12	4	0	PM	F
1949	12	5	0	PM	F
1949	12	6	0	PM	F
1949	12	7	0	PM	F
1949	12	8	0	PM	F
1949	12	9	0	PM	F
1949	12	10 T		PM	F
1949	12	11	1	PM	F
1949	12	12	0	PM	F
1949	12	13	0	PM	F
1949	12	14	0	PM	F
1949	12	15	0	PM	F
1949	12	16	0	PM	F
1949	12	17	0	PM	F
1949	12	18	0.44	PM	F
1949	12	19	0	PM	F
1949	12	20	0.2	PM	F

1949	12	21		2.48	PM	F
1949	12	22		0.9	PM	F
1949	12	23		0	PM	F
1949	12	24		0	PM	F
1949	12	25		0	PM	F
1949	12	26		0.3	PM	F
1949	12	27		0	PM	F
1949	12	28		0	PM	F
1949	12	29		0	PM	F
1949	12	30		0	PM	F
1949	12	31	T		PM	F
1950	1	1		0.1	PM	F
1950	1	2		0.49	PM	F
1950	1	3		0.8	PM	F
1950	1	4		0.3	PM	F
1950	1	5		0	PM	F
1950	1	6		0	PM	F
1950	1	7		0	PM	F
1950	1	8		0	PM	F
1950	1	9		0	PM	F
1950	1	10		0.85	PM	F
1950	1	11		0	PM	F
1950	1	12	T		PM	F
1950	1	13		1.5	PM	F
1950	1	14		0.1	PM	F
1950	1	15		0.65	PM	F
1950	1	16		0	PM	F
1950	1	17		0	PM	F
1950	1	18		0	PM	F
1950	1	19		0	PM	F
1950	1	20		0	PM	F
1950	1	21		0	PM	F
1950	1	22		0	PM	F
1950	1	23	T		PM	F
1950	1	24		1.03	PM	F
1950	1	25		0.75	PM	F
1950	1	26		0	PM	F
1950	1	27		0	PM	F
1950	1	28		0	PM	F
1950	1	29	T		PM	F
1950	1	30		0	PM	F
1950	1	31	T		PM	F
1950	2	1		0	PM	F
1950	2	2		0	PM	F
1950	2	3		0	PM	F
1950	2	4		0	PM	F
1950	2	5		0	PM	F
1950	2	6	T		PM	F
1950	2	7		0	PM	F
1950	2	8		0.19	PM	F
1950	2	9		0.14	PM	F
1950	2	10		0	PM	F
1950	2	11		0	PM	F
1950	2	12		0.1	PM	F
1950	2	13		1.03	PM	F
1950	2	14		0.1	PM	F
1950	2	15	T		PM	F
1950	2	16		0	PM	F
1950	2	17		0	PM	F
1950	2	18	T		PM	F
1950	2	19		0	PM	F
1950	2	20		0	PM	F
1950	2	21		0.64	PM	F
1950	2	22		0.3	PM	F
1950	2	23		0	PM	F
1950	2	24	T		PM	F
1950	2	25		0.32	PM	F
1950	2	26		0	PM	F
1950	2	27		0	PM	F
1950	2	28		0.35	PM	F
1950	3	1	T		PM	F
1950	3	2		0	PM	F
1950	3	3		0	PM	F
1950	3	4		0	PM	F
1950	3	5		0	PM	F
1950	3	6		0	PM	F
1950	3	7	T		PM	F
1950	3	8	T		PM	F
1950	3	9		0	PM	F
1950	3	10		0	PM	F
1950	3	11		0.33	PM	F
1950	3	12		0.31	PM	F
1950	3	13	T		PM	F
1950	3	14		0	PM	F
1950	3	15		0	PM	F
1950	3	16		0.2	PM	F
1950	3	17		0	PM	F
1950	3	18		0	PM	F
1950	3	19	T		PM	F
1950	3	20		0.17	PM	F
1950	3	21		0	PM	F
1950	3	22		0.14	PM	F
1950	3	23		0	PM	F
1950	3	24		0	PM	F
1950	3	25		0	PM	F
1950	3	26	T		PM	F
1950	3	27		0.1	PM	F
1950	3	28		0	PM	F
1950	3	29		0	PM	F
1950	3	30		0	PM	F
1950	3	31		0.37	PM	F
1950	4	1		0.13	PM	F
1950	4	2		0.6	PM	F
1950	4	3		0.82	PM	F
1950	4	4		1.49	PM	F
1950	4	5		0	PM	F
1950	4	6		0	PM	F
1950	4	7		0	PM	F
1950	4	8		0	PM	F
1950	4	9	T		PM	F
1950	4	10	T		PM	F
1950	4	11		0.41	PM	F
1950	4	12		0	PM	F
1950	4	13		0	PM	F
1950	4	14		0	PM	F

1950	4	15	0	PM	F
1950	4	16	0	PM	F
1950	4	17	0	PM	F
1950	4	18	0	PM	F
1950	4	19	0.18	PM	F
1950	4	20	0	PM	F
1950	4	21	0	PM	F
1950	4	22	0	PM	F
1950	4	23	0.34	PM	F
1950	4	24	1.3	PM	F
1950	4	25	1.6	PM	F
1950	4	26	0	PM	F
1950	4	27	0	PM	F
1950	4	28	0	PM	F
1950	4	29	0	PM	F
1950	4	30 T		PM	F
1950	5	1	0	PM	F
1950	5	2	0	PM	F
1950	5	3	0	PM	F
1950	5	4	0.1	PM	F
1950	5	5	0	PM	F
1950	5	6	0	PM	F
1950	5	7	0	PM	F
1950	5	8 T		PM	F
1950	5	9	0.42	PM	F
1950	5	10	0	PM	F
1950	5	11	0	PM	F
1950	5	12	0	PM	F
1950	5	13	0	PM	F
1950	5	14	0	PM	F
1950	5	15	0	PM	F
1950	5	16	0	PM	F
1950	5	17	0	PM	F
1950	5	18	0	PM	F
1950	5	19	0	PM	F
1950	5	20	0	PM	F
1950	5	21	0.44	PM	F
1950	5	22	0	PM	F
1950	5	23	0	PM	F
1950	5	24	0	PM	F
1950	5	25 T		PM	F
1950	5	26	0	PM	F
1950	5	27	0.31	PM	F
1950	5	28	0.25	PM	F
1950	5	29	0	PM	F
1950	5	30	0	PM	F
1950	5	31 T		PM	F
1950	6	1	0	PM	F
1950	6	2 T		PM	F
1950	6	3	0.1	PM	F
1950	6	4	0	PM	F
1950	6	5	0	PM	F
1950	6	6	0	PM	F
1950	6	7	0	PM	F
1950	6	8	0	PM	F
1950	6	9	0.18	PM	F
1950	6	10	0	PM	F
1950	6	11	0	PM	F
1950	6	12	0.15	PM	F
1950	6	13	1.34	PM	F
1950	6	14 T		PM	F
1950	6	15	1.55	PM	F
1950	6	16	0.8	PM	F
1950	6	17 T		PM	F
1950	6	18	0.67	PM	F
1950	6	19	1.44	PM	F
1950	6	20 T		PM	F
1950	6	21	0	PM	F
1950	6	22	0	PM	F
1950	6	23	0	PM	F
1950	6	24 T		PM	F
1950	6	25	0.3	PM	F
1950	6	26 T		PM	F
1950	6	27	0	PM	F
1950	6	28	0	PM	F
1950	6	29 T		PM	F
1950	6	30	0.1	PM	F
1950	7	1 T		PM	F
1950	7	2	0.58	PM	F
1950	7	3	0.64	PM	F
1950	7	4	0	PM	F
1950	7	5	0	PM	F
1950	7	6	0	PM	F
1950	7	7	0	PM	F
1950	7	8	0	PM	F
1950	7	9	0	PM	F
1950	7	10	0	PM	F
1950	7	11	0	PM	F
1950	7	12	0	PM	F
1950	7	13 T		PM	F
1950	7	14	0	PM	F
1950	7	15	0	PM	F
1950	7	16	0.15	PM	F
1950	7	17	1.22	PM	F
1950	7	18	0	PM	F
1950	7	19	0.65	PM	F
1950	7	20 T		PM	F
1950	7	21	0	PM	F
1950	7	22	0	PM	F
1950	7	23	0	PM	F
1950	7	24 T		PM	F
1950	7	25 T		PM	F
1950	7	26 T		PM	F
1950	7	27 T		PM	F
1950	7	28	0	PM	F
1950	7	29	0	PM	F
1950	7	30	0	PM	F
1950	7	31 T		PM	F
1950	8	1	0	PM	F
1950	8	2	0	PM	F
1950	8	3	0	PM	F
1950	8	4 T		PM	F
1950	8	5 T		PM	F
1950	8	6	0	PM	F
1950	8	7	0	PM	F

1950	8	8	0.2	PM	F
1950	8	9	0.1	PM	F
1950	8	10	0	PM	F
1950	8	11	0.35	PM	F
1950	8	12	0	PM	F
1950	8	13	0	PM	F
1950	8	14	0	PM	F
1950	8	15	0	PM	F
1950	8	16	0	PM	F
1950	8	17	0	PM	F
1950	8	18 T		PM	F
1950	8	19	0	PM	F
1950	8	20	0	PM	F
1950	8	21	0	PM	F
1950	8	22	0	PM	F
1950	8	23	0	PM	F
1950	8	24	0	PM	F
1950	8	25	0	PM	F
1950	8	26	0	PM	F
1950	8	27	0	PM	F
1950	8	28 T		PM	F
1950	8	29	0	PM	F
1950	8	30	0.19	PM	F
1950	8	31 T		PM	F
1950	9	1 T		PM	F
1950	9	2	0.74	PM	F
1950	9	3	0	PM	F
1950	9	4	0	PM	F
1950	9	5	0	PM	F
1950	9	6	0	PM	F
1950	9	7	0	PM	F
1950	9	8 T		PM	F
1950	9	9 T		PM	F
1950	9	10	0.27	PM	F
1950	9	11 T		PM	F
1950	9	12	0.08	PM	F
1950	9	13	0	PM	F
1950	9	14	0	PM	F
1950	9	15	0	PM	F
1950	9	16	0	PM	F
1950	9	17	0	PM	F
1950	9	18	0	PM	F
1950	9	19 T		PM	F
1950	9	20	1.87	PM	F
1950	9	21	0.63	PM	F
1950	9	22	0	PM	F
1950	9	23	0	PM	F
1950	9	24	0	PM	F
1950	9	25	0	PM	F
1950	9	26	0	PM	F
1950	9	27	0	PM	F
1950	9	28	0.15	PM	F
1950	9	29	0	PM	F
1950	9	30	0	PM	F
1950	10	1	0	PM	F
1950	10	2	0	PM	F
1950	10	3	0.98	PM	F
1950	10	4	0	PM	F
1950	10	5	0	PM	F
1950	10	6	0	PM	F
1950	10	7	0.85	PM	F
1950	10	8 T		PM	F
1950	10	9	0	PM	F
1950	10	10	0	PM	F
1950	10	11	0	PM	F
1950	10	12	0	PM	F
1950	10	13	0	PM	F
1950	10	14	0	PM	F
1950	10	15	0	PM	F
1950	10	16	0	PM	F
1950	10	17	0	PM	F
1950	10	18	0	PM	F
1950	10	19	0	PM	F
1950	10	20	0	PM	F
1950	10	21	0	PM	F
1950	10	22	0	PM	F
1950	10	23	0	PM	F
1950	10	24	0	PM	F
1950	10	25	0	PM	F
1950	10	26	0.33	PM	F
1950	10	27 T		PM	F
1950	10	28	0	PM	F
1950	10	29	0	PM	F
1950	10	30	0	PM	F
1950	10	31	0	PM	F
1950	11	1	0.03	PM	F
1950	11	2	0	PM	F
1950	11	3	0	PM	F
1950	11	4	0	PM	F
1950	11	5	0	PM	F
1950	11	6	0	PM	F
1950	11	7	0.33	PM	F
1950	11	8	0.09	PM	F
1950	11	9	0.14	PM	F
1950	11	10 T		PM	F
1950	11	11	0	PM	F
1950	11	12	0	PM	F
1950	11	13	0	PM	F
1950	11	14	0	PM	F
1950	11	15	0.12	PM	F
1950	11	16	0.2	PM	F
1950	11	17	0	PM	F
1950	11	18	0	PM	F
1950	11	19	0.1	PM	F
1950	11	20	1.1	PM	F
1950	11	21	0	PM	F
1950	11	22 T		PM	F
1950	11	23	0.1	PM	F
1950	11	24 T		PM	F
1950	11	25	0	PM	F
1950	11	26	0.2	PM	F
1950	11	27 T		PM	F
1950	11	28	0	PM	F
1950	11	29	0	PM	F
1950	11	30	0	PM	F

1950	12	1		0	PM	F
1950	12	2		0	PM	F
1950	12	3		0.1	PM	F
1950	12	4		0	PM	F
1950	12	5		0	PM	F
1950	12	6		0.37	PM	F
1950	12	7		0.05	PM	F
1950	12	8		0	PM	F
1950	12	9	T		PM	F
1950	12	10	T		PM	F
1950	12	11		0.07	PM	F
1950	12	12		0.05	PM	F
1950	12	13		0	PM	F
1950	12	14		0	PM	F
1950	12	15		0	PM	F
1950	12	16		0	PM	F
1950	12	17		0	PM	F
1950	12	18		0	PM	F
1950	12	19		0.05	PM	F
1950	12	20		0	PM	F
1950	12	21		0	PM	F
1950	12	22		0	PM	F
1950	12	23		0	PM	F
1950	12	24		0	PM	F
1950	12	25		0	PM	F
1950	12	26	T		PM	F
1950	12	27		0	PM	F
1950	12	28		0	PM	F
1950	12	29		0	PM	F
1950	12	30		0	PM	F
1950	12	31		0	PM	F
1951	1	1		0	PM	F
1951	1	2		0.9	PM	F
1951	1	3		0.17	PM	F
1951	1	4		0	PM	F
1951	1	5		0	PM	F
1951	1	6		0	PM	F
1951	1	7		0	PM	F
1951	1	8		0	PM	F
1951	1	9		0	PM	F
1951	1	10	T		PM	F
1951	1	11		0	PM	F
1951	1	12		0	PM	F
1951	1	13	T		PM	F
1951	1	14		0.52	PM	F
1951	1	15	T		PM	F
1951	1	16		0	PM	F
1951	1	17		0	PM	F
1951	1	18		0	PM	F
1951	1	19		0	PM	F
1951	1	20	T		PM	F
1951	1	21	T		PM	F
1951	1	22		0	PM	F
1951	1	23		0.04	PM	F
1951	1	24		0	PM	F
1951	1	25		0	PM	F
1951	1	26		0	PM	F
1951	1	27		0	PM	F
1951	1	28	T		PM	F
1951	1	29		0	PM	F
1951	1	30		0	PM	F
1951	1	31		0.15	PM	F
1951	2	1		0.25	PM	F
1951	2	2		0	PM	F
1951	2	3		0	PM	F
1951	2	4		0	PM	F
1951	2	5		0	PM	F
1951	2	6		0.9	PM	F
1951	2	7		0	PM	F
1951	2	8		0.15	PM	F
1951	2	9		0.06	PM	F
1951	2	10		0	PM	F
1951	2	11		0	PM	F
1951	2	12		0	PM	F
1951	2	13	T		PM	F
1951	2	14		0.2	PM	F
1951	2	15	T		PM	F
1951	2	16		0.5	PM	F
1951	2	17	T		PM	F
1951	2	18		0.3	PM	F
1951	2	19		0.32	PM	F
1951	2	20		0.63	PM	F
1951	2	21		1	PM	F
1951	2	22		0	PM	F
1951	2	23		0	PM	F
1951	2	24		0	PM	F
1951	2	25		0	PM	F
1951	2	26		0	PM	F
1951	2	27		0	PM	F
1951	2	28		0.1	PM	F
1951	3	1		0.12	PM	F
1951	3	2		0.13	PM	F
1951	3	3		0.15	PM	F
1951	3	4		0	PM	F
1951	3	5		0	PM	F
1951	3	6		0	PM	F
1951	3	7		0	PM	F
1951	3	8		0	PM	F
1951	3	9		0	PM	F
1951	3	10	T		PM	F
1951	3	11		0.65	PM	F
1951	3	12		0.18	PM	F
1951	3	13		0.11	PM	F
1951	3	14		0.2	PM	F
1951	3	15	T		PM	F
1951	3	16		0	PM	F
1951	3	17		0.35	PM	F
1951	3	18		0.55	PM	F
1951	3	19		0	PM	F
1951	3	20	T		PM	F
1951	3	21		0	PM	F
1951	3	22		0	PM	F
1951	3	23		0	PM	F
1951	3	24		0	PM	F
1951	3	25		0.05	PM	F

1951	3	26	0	PM	F
1951	3	27	T	PM	F
1951	3	28	0.15	PM	F
1951	3	29	0.42	PM	F
1951	3	30	T	PM	F
1951	3	31	0	PM	F
1951	4	1	0.05	PM	F
1951	4	2	0	PM	F
1951	4	3	0	PM	F
1951	4	4	0	PM	F
1951	4	5	0	PM	F
1951	4	6	0.28	PM	F
1951	4	7	1.01	PM	F
1951	4	8	T	PM	F
1951	4	9	0.18	PM	F
1951	4	10	0.17	PM	F
1951	4	11	1.03	PM	F
1951	4	12	0.58	PM	F
1951	4	13	0.26	PM	F
1951	4	14	T	PM	F
1951	4	15	T	PM	F
1951	4	16	0	PM	F
1951	4	17	0	PM	F
1951	4	18	0	PM	F
1951	4	19	0	PM	F
1951	4	20	0	PM	F
1951	4	21	0.09	PM	F
1951	4	22	0	PM	F
1951	4	23	0	PM	F
1951	4	24	T	PM	F
1951	4	25	0.05	PM	F
1951	4	26	0.07	PM	F
1951	4	27	0	PM	F
1951	4	28	0.05	PM	F
1951	4	29	0.35	PM	F
1951	4	30	0	PM	F
1951	5	1	0	PM	F
1951	5	2	0	PM	F
1951	5	3	0.25	PM	F
1951	5	4	T	PM	F
1951	5	5	0.25	PM	F
1951	5	6	0.58	PM	F
1951	5	7	0	PM	F
1951	5	8	0	PM	F
1951	5	9	0	PM	F
1951	5	10	0.85	PM	F
1951	5	11	0.17	PM	F
1951	5	12	0	PM	F
1951	5	13	0	PM	F
1951	5	14	0	PM	F
1951	5	15	0	PM	F
1951	5	16	0	PM	F
1951	5	17	0	PM	F
1951	5	18	0	PM	F
1951	5	19	0	PM	F
1951	5	20	T	PM	F
1951	5	21	0	PM	F
1951	5	22	0.12	PM	F
1951	5	23	0	PM	F
1951	5	24	0	PM	F
1951	5	25	0	PM	F
1951	5	26	1	PM	F
1951	5	27	0.05	PM	F
1951	5	28	0	PM	F
1951	5	29	0	PM	F
1951	5	30	0	PM	F
1951	5	31	0.04	PM	F
1951	6	1	0	PM	F
1951	6	2	0	PM	F
1951	6	3	0.12	PM	F
1951	6	4	0	PM	F
1951	6	5	0	PM	F
1951	6	6	0	PM	F
1951	6	7	0.09	PM	F
1951	6	8	0.6	PM	F
1951	6	9	T	PM	F
1951	6	10	0	PM	F
1951	6	11	T	PM	F
1951	6	12	0.87	PM	F
1951	6	13	0	PM	F
1951	6	14	0	PM	F
1951	6	15	0	PM	F
1951	6	16	0.67	PM	F
1951	6	17	0	PM	F
1951	6	18	0	PM	F
1951	6	19	1.14	PM	F
1951	6	20	0	PM	F
1951	6	21	T	PM	F
1951	6	22	T	PM	F
1951	6	23	0	PM	F
1951	6	24	0.52	PM	F
1951	6	25	0	PM	F
1951	6	26	0.27	PM	F
1951	6	27	1.1	PM	F
1951	6	28	1.86	PM	F
1951	6	29	0.14	PM	F
1951	6	30	T	PM	F
1951	7	1	0	PM	F
1951	7	2	0	PM	F
1951	7	3	0	PM	F
1951	7	4	T	PM	F
1951	7	5	T	PM	F
1951	7	6	0	PM	F
1951	7	7	0	PM	F
1951	7	8	T	PM	F
1951	7	9	3.8	PM	F
1951	7	10	T	PM	F
1951	7	11	0.27	PM	F
1951	7	12	0.12	PM	F
1951	7	13	0	PM	F
1951	7	14	0	PM	F
1951	7	15	0	PM	F
1951	7	16	0	PM	F
1951	7	17	0.27	PM	F
1951	7	18	0	PM	F

1951	7	19		0	PM	F
1951	7	20		0	PM	F
1951	7	21		0	PM	F
1951	7	22		0.69	PM	F
1951	7	23		0.2	PM	F
1951	7	24		0	PM	F
1951	7	25		0	PM	F
1951	7	26		0	PM	F
1951	7	27		0	PM	F
1951	7	28		0	PM	F
1951	7	29		0	PM	F
1951	7	30		0	PM	F
1951	7	31		1.14	PM	F
1951	8	1		0	PM	F
1951	8	2		0	PM	F
1951	8	3		0	PM	F
1951	8	4		0	PM	F
1951	8	5		0	PM	F
1951	8	6		0.75	PM	F
1951	8	7		0	PM	F
1951	8	8		0	PM	F
1951	8	9		0.05	PM	F
1951	8	10		0	PM	F
1951	8	11		0.13	PM	F
1951	8	12		0	PM	F
1951	8	13		0	PM	F
1951	8	14		0	PM	F
1951	8	15		0.1	PM	F
1951	8	16		0	PM	F
1951	8	17	T		PM	F
1951	8	18	T		PM	F
1951	8	19		0	PM	F
1951	8	20		0.66	PM	F
1951	8	21		0.16	PM	F
1951	8	22	T		PM	F
1951	8	23		0	PM	F
1951	8	24		0	PM	F
1951	8	25		0.41	PM	F
1951	8	26		0.07	PM	F
1951	8	27		0	PM	F
1951	8	28		0	PM	F
1951	8	29		4.25	PM	F
1951	8	30		0	PM	F
1951	8	31		0	PM	F
1951	9	1		0.82	PM	F
1951	9	2		0	PM	F
1951	9	3		0	PM	F
1951	9	4		0	PM	F
1951	9	5	T		PM	F
1951	9	6	T		PM	F
1951	9	7		0	PM	F
1951	9	8		0	PM	F
1951	9	9		0.06	PM	F
1951	9	10		0.18	PM	F
1951	9	11		0	PM	F
1951	9	12	T		PM	F
1951	9	13		0.63	PM	F
1951	9	14		0	PM	F
1951	9	15		0	PM	F
1951	9	16		0	PM	F
1951	9	17		0	PM	F
1951	9	18		0	PM	F
1951	9	19		0	PM	F
1951	9	20		0	PM	F
1951	9	21		0	PM	F
1951	9	22		0.46	PM	F
1951	9	23		0	PM	F
1951	9	24		0.1	PM	F
1951	9	25		0.07	PM	F
1951	9	26		0	PM	F
1951	9	27		0.48	PM	F
1951	9	28		0	PM	F
1951	9	29		0	PM	F
1951	9	30		0.1	PM	F
1951	10	1		0	PM	F
1951	10	2		0	PM	F
1951	10	3		0	PM	F
1951	10	4		0	PM	F
1951	10	5		0	PM	F
1951	10	6		0.4	PM	F
1951	10	7		0.67	PM	F
1951	10	8		0	PM	F
1951	10	9		0	PM	F
1951	10	10		0	PM	F
1951	10	11		0	PM	F
1951	10	12		0	PM	F
1951	10	13		0	PM	F
1951	10	14		0	PM	F
1951	10	15		0	PM	F
1951	10	16		0	PM	F
1951	10	17		0	PM	F
1951	10	18		0	PM	F
1951	10	19		0	PM	F
1951	10	20		0	PM	F
1951	10	21		0	PM	F
1951	10	22		0.12	PM	F
1951	10	23		1.47	PM	F
1951	10	24		0.13	PM	F
1951	10	25		0	PM	F
1951	10	26		0	PM	F
1951	10	27		0.11	PM	F
1951	10	28		0	PM	F
1951	10	29		0.04	PM	F
1951	10	30		0	PM	F
1951	10	31		0	PM	F
1951	11	1		0	PM	F
1951	11	2	T		PM	F
1951	11	3		0.06	PM	F
1951	11	4		0	PM	F
1951	11	5		0	PM	F
1951	11	6		0.75	PM	F
1951	11	7	T		PM	F
1951	11	8		0	PM	F
1951	11	9		0	PM	F
1951	11	10		0	PM	F

1951	11	11		0	PM	F
1951	11	12		0.98	PM	F
1951	11	13		0.68	PM	F
1951	11	14		0	PM	F
1951	11	15		0	PM	F
1951	11	16	T		PM	F
1951	11	17		0.5	PM	F
1951	11	18		0	PM	F
1951	11	19		0	PM	F
1951	11	20		0	PM	F
1951	11	21		0	PM	F
1951	11	22		0.12	PM	F
1951	11	23	T		PM	F
1951	11	24		0	PM	F
1951	11	25	T		PM	F
1951	11	26	T		PM	F
1951	11	27		0	PM	F
1951	11	28		0	PM	F
1951	11	29		0	PM	F
1951	11	30		0	PM	F
1951	12	1		0	PM	F
1951	12	2		0	PM	F
1951	12	3	T		PM	F
1951	12	4		0	PM	F
1951	12	5		0	PM	F
1951	12	6	T		PM	F
1951	12	7	T		PM	F
1951	12	8		0.12	PM	F
1951	12	9	T		PM	F
1951	12	10		0	PM	F
1951	12	11	T		PM	F
1951	12	12		0	PM	F
1951	12	13		0	PM	F
1951	12	14		0.3	PM	F
1951	12	15	T		PM	F
1951	12	16		0	PM	F
1951	12	17	T		PM	F
1951	12	18		0.4	PM	F
1951	12	19		0	PM	F
1951	12	20	T		PM	F
1951	12	21		0.1	PM	F
1951	12	22		0	PM	F
1951	12	23		0	PM	F
1951	12	24		0	PM	F
1951	12	25		0.3	PM	F
1951	12	26		0	PM	F
1951	12	27		0	PM	F
1951	12	28		0	PM	F
1951	12	29		0	PM	F
1951	12	30		0	PM	F
1951	12	31	T		PM	F
1952	1	1		0	PM	F
1952	1	2		0.18	PM	F
1952	1	3		0.1	PM	F
1952	1	4		0.05	PM	F
1952	1	5	T		PM	F
1952	1	6		0	PM	F
1952	1	7		0	PM	F
1952	1	8	T		PM	F
1952	1	9		0	PM	F
1952	1	10		0	PM	F
1952	1	11	T		PM	F
1952	1	12		0.05	PM	F
1952	1	13		0	PM	F
1952	1	14	T		PM	F
1952	1	15		0.3	PM	F
1952	1	16	T		PM	F
1952	1	17		0	PM	F
1952	1	18		0	PM	F
1952	1	19		0.2	PM	F
1952	1	20		0	PM	F
1952	1	21	T		PM	F
1952	1	22	T		PM	F
1952	1	23		0	PM	F
1952	1	24	T		PM	F
1952	1	25		0.2	PM	F
1952	1	26		0.77	PM	F
1952	1	27		0	PM	F
1952	1	28		0	PM	F
1952	1	29		0	PM	F
1952	1	30		0	PM	F
1952	1	31		0	PM	F
1952	2	1		0.13	PM	F
1952	2	2		0	PM	F
1952	2	3		0.2	PM	F
1952	2	4		0.3	PM	F
1952	2	5		0	PM	F
1952	2	6	T		PM	F
1952	2	7	T		PM	F
1952	2	8		0	PM	F
1952	2	9		0	PM	F
1952	2	10		0	PM	F
1952	2	11		0	PM	F
1952	2	12		0	PM	F
1952	2	13	T		PM	F
1952	2	14		0.55	PM	F
1952	2	15		0	PM	F
1952	2	16		0	PM	F
1952	2	17		0	PM	F
1952	2	18		0	PM	F
1952	2	19		0	PM	F
1952	2	20		0	PM	F
1952	2	21		0	PM	F
1952	2	22		0	PM	F
1952	2	23		0.1	PM	F
1952	2	24	T		PM	F
1952	2	25	T		PM	F
1952	2	26		0	PM	F
1952	2	27		0	PM	F
1952	2	28		0	PM	F
1952	2	29		0.5	PM	F
1952	3	1	T		PM	F
1952	3	2		0.15	PM	F
1952	3	3		0.05	PM	F
1952	3	4		0.21	PM	F

1952	3	5	0	PM	F
1952	3	6	0	PM	F
1952	3	7	0	PM	F
1952	3	8 T		PM	F
1952	3	9	0	PM	F
1952	3	10	0.25	PM	F
1952	3	11	0.35	PM	F
1952	3	12	0	PM	F
1952	3	13	0.15	PM	F
1952	3	14	0	PM	F
1952	3	15	0	PM	F
1952	3	16	0	PM	F
1952	3	17	0	PM	F
1952	3	18	1.15	PM	F
1952	3	19	0.11	PM	F
1952	3	20	0	PM	F
1952	3	21	0	PM	F
1952	3	22	0.29	PM	F
1952	3	23 T		PM	F
1952	3	24	0	PM	F
1952	3	25 T		PM	F
1952	3	26 T		PM	F
1952	3	27	0	PM	F
1952	3	28	0	PM	F
1952	3	29	0	PM	F
1952	3	30	0	PM	F
1952	3	31	0.66	PM	F
1952	4	1	0	PM	F
1952	4	2	0	PM	F
1952	4	3	0	PM	F
1952	4	4	0.63	PM	F
1952	4	5 T		PM	F
1952	4	6 T		PM	F
1952	4	7	0	PM	F
1952	4	8	0	PM	F
1952	4	9	0	PM	F
1952	4	10	0.7	PM	F
1952	4	11 T		PM	F
1952	4	12	1.02	PM	F
1952	4	13	0.68	PM	F
1952	4	14 T		PM	F
1952	4	15	0	PM	F
1952	4	16	0	PM	F
1952	4	17	0	PM	F
1952	4	18	0	PM	F
1952	4	19	0	PM	F
1952	4	20	0	PM	F
1952	4	21 T		PM	F
1952	4	22	0.13	PM	F
1952	4	23	1.08	PM	F
1952	4	24 T		PM	F
1952	4	25	0	PM	F
1952	4	26	0	PM	F
1952	4	27	0	PM	F
1952	4	28	0	PM	F
1952	4	29	0	PM	F
1952	4	30	0	PM	F
1952	5	1	0	PM	F
1952	5	2	0	PM	F
1952	5	3	0	PM	F
1952	5	4	0	PM	F
1952	5	5	0.27	PM	F
1952	5	6	0.12	PM	F
1952	5	7	0	PM	F
1952	5	8	0	PM	F
1952	5	9	0.77	PM	F
1952	5	10	0	PM	F
1952	5	11	0.13	PM	F
1952	5	12 T		PM	F
1952	5	13	0	PM	F
1952	5	14	0	PM	F
1952	5	15 T		PM	F
1952	5	16	0.56	PM	F
1952	5	17	0.63	PM	F
1952	5	18 T		PM	F
1952	5	19 T		PM	F
1952	5	20	0	PM	F
1952	5	21	0.14	PM	F
1952	5	22 T		PM	F
1952	5	23	0	PM	F
1952	5	24	0.05	PM	F
1952	5	25	1.2	PM	F
1952	5	26	0	PM	F
1952	5	27	0	PM	F
1952	5	28	0.57	PM	F
1952	5	29	0	PM	F
1952	5	30	0	PM	F
1952	5	31	0.08	PM	F
1952	6	1	0	PM	F
1952	6	2 T		PM	F
1952	6	3	0.43	PM	F
1952	6	4	0	PM	F
1952	6	5	0	PM	F
1952	6	6	0	PM	F
1952	6	7	0	PM	F
1952	6	8	0	PM	F
1952	6	9	0.64	PM	F
1952	6	10	0	PM	F
1952	6	11	0	PM	F
1952	6	12	0.34	PM	F
1952	6	13	0	PM	F
1952	6	14	1.1	PM	F
1952	6	15	0	PM	F
1952	6	16	0	PM	F
1952	6	17 T		PM	F
1952	6	18	0	PM	F
1952	6	19	0	PM	F
1952	6	20	0.56	PM	F
1952	6	21	0.77	PM	F
1952	6	22	2.93	PM	F
1952	6	23 T		PM	F
1952	6	24	0	PM	F
1952	6	25	0	PM	F
1952	6	26	0	PM	F
1952	6	27	0	PM	F

1952	6	28	0	PM	F
1952	6	29	0	PM	F
1952	6	30	0	PM	F
1952	7	1	0	PM	F
1952	7	2	0.8	PM	F
1952	7	3	0.17	PM	F
1952	7	4	0	PM	F
1952	7	5	0	PM	F
1952	7	6	0	PM	F
1952	7	7	0	PM	F
1952	7	8	0.67	PM	F
1952	7	9	0	PM	F
1952	7	10	0	PM	F
1952	7	11	0	PM	F
1952	7	12	0	PM	F
1952	7	13	0	PM	F
1952	7	14	T	PM	F
1952	7	15	0.12	PM	F
1952	7	16	T	PM	F
1952	7	17	0.25	PM	F
1952	7	18	0	PM	F
1952	7	19	0	PM	F
1952	7	20	0	PM	F
1952	7	21	0	PM	F
1952	7	22	0	PM	F
1952	7	23	0	PM	F
1952	7	24	0	PM	F
1952	7	25	0	PM	F
1952	7	26	0	PM	F
1952	7	27	0	PM	F
1952	7	28	0	PM	F
1952	7	29	T	PM	F
1952	7	30	0	PM	F
1952	7	31	0	PM	F
1952	8	1	0	PM	F
1952	8	2	0	PM	F
1952	8	3	0	PM	F
1952	8	4	0.15	PM	F
1952	8	5	0	PM	F
1952	8	6	0	PM	F
1952	8	7	0	PM	F
1952	8	8	0	PM	F
1952	8	9	0.07	PM	F
1952	8	10	0	PM	F
1952	8	11	0.69	PM	F
1952	8	12	0	PM	F
1952	8	13	0	PM	F
1952	8	14	0	PM	F
1952	8	15	1.6	PM	F
1952	8	16	0	PM	F
1952	8	17	0	PM	F
1952	8	18	T	PM	F
1952	8	19	0	PM	F
1952	8	20	0	PM	F
1952	8	21	0.16	PM	F
1952	8	22	0	PM	F
1952	8	23	0	PM	F
1952	8	24	0	PM	F
1952	8	25	0	PM	F
1952	8	26	0	PM	F
1952	8	27	0	PM	F
1952	8	28	0	PM	F
1952	8	29	0	PM	F
1952	8	30	0	PM	F
1952	8	31	0	PM	F
1952	9	1	0.05	PM	F
1952	9	2	0	PM	F
1952	9	3	T	PM	F
1952	9	4	0	PM	F
1952	9	5	0	PM	F
1952	9	6	0	PM	F
1952	9	7	0	PM	F
1952	9	8	0	PM	F
1952	9	9	0	PM	F
1952	9	10	0	PM	F
1952	9	11	0	PM	F
1952	9	12	0	PM	F
1952	9	13	0	PM	F
1952	9	14	0.18	PM	F
1952	9	15	0	PM	F
1952	9	16	0	PM	F
1952	9	17	T	PM	F
1952	9	18	0.1	PM	F
1952	9	19	0.31	PM	F
1952	9	20	0	PM	F
1952	9	21	0	PM	F
1952	9	22	0	PM	F
1952	9	23	0	PM	F
1952	9	24	0	PM	F
1952	9	25	0	PM	F
1952	9	26	0	PM	F
1952	9	27	0	PM	F
1952	9	28	0	PM	F
1952	9	29	0	PM	F
1952	9	30	0	PM	F
1952	10	1	T	PM	F
1952	10	2	0	PM	F
1952	10	3	0	PM	F
1952	10	4	0	PM	F
1952	10	5	0	PM	F
1952	10	6	0	PM	F
1952	10	7	0	PM	F
1952	10	8	0	PM	F
1952	10	9	0	PM	F
1952	10	10	0	PM	F
1952	10	11	0	PM	F
1952	10	12	0	PM	F
1952	10	13	0	PM	F
1952	10	14	0.75	PM	F
1952	10	15	0.37	PM	F
1952	10	16	0	PM	F
1952	10	17	0	PM	F
1952	10	18	0	PM	F
1952	10	19	0	PM	F
1952	10	20	0	PM	F

1952	10	21	0	PM	F
1952	10	22	0	PM	F
1952	10	23	0	PM	F
1952	10	24	0	PM	F
1952	10	25	0	PM	F
1952	10	26	0	PM	F
1952	10	27	0	PM	F
1952	10	28	0	PM	F
1952	10	29	0	PM	F
1952	10	30	0	PM	F
1952	10	31	0	PM	F
1952	11	1	0	PM	F
1952	11	2	0.37	PM	F
1952	11	3	0	PM	F
1952	11	4	0	PM	F
1952	11	5	0	PM	F
1952	11	6	0	PM	F
1952	11	7	0	PM	F
1952	11	8	0.07	PM	F
1952	11	9	0.37	PM	F
1952	11	10	0	PM	F
1952	11	11	0	PM	F
1952	11	12	0	PM	F
1952	11	13	0	PM	F
1952	11	14	0	PM	F
1952	11	15	0	PM	F
1952	11	16	0	PM	F
1952	11	17	0	PM	F
1952	11	18	0.45	PM	F
1952	11	19	0	PM	F
1952	11	20	0	PM	F
1952	11	21	0	PM	F
1952	11	22	0	PM	F
1952	11	23	0	PM	F
1952	11	24	0.08	PM	F
1952	11	25	1.32	PM	F
1952	11	26	0.27	PM	F
1952	11	27	T	PM	F
1952	11	28	0	PM	F
1952	11	29	0.07	PM	F
1952	11	30	0	PM	F
1952	12	1	0.05	PM	F
1952	12	2	0.42	PM	F
1952	12	3	0	PM	F
1952	12	4	0.75	PM	F
1952	12	5	0	PM	F
1952	12	6	0	PM	F
1952	12	7	0	PM	F
1952	12	8	0	PM	F
1952	12	9	0	PM	F
1952	12	10	T	PM	F
1952	12	11	0	PM	F
1952	12	12	T	PM	F
1952	12	13	T	PM	F
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1952	12	15	0	PM	F
1952	12	16	0	PM	F
1952	12	17	0	PM	F
1952	12	18	0	PM	F
1952	12	19	0.25	PM	F
1952	12	20	0.6	PM	F
1952	12	21	T	PM	F
1952	12	22	0.04	PM	F
1952	12	23	0.02	PM	F
1952	12	24	0	PM	F
1952	12	25	T	PM	F
1952	12	26	0	PM	F
1952	12	27	0	PM	F
1952	12	28	0	PM	F
1952	12	29	T	PM	F
1952	12	30	0	PM	F
1952	12	31	0	PM	F
1953	1	1	0	PM	F
1953	1	2	0.13	PM	F
1953	1	3	0.03	PM	F
1953	1	4	T	PM	F
1953	1	5	T	PM	F
1953	1	6	0.4	PM	F
1953	1	7	T	PM	F
1953	1	8	0.62	PM	F
1953	1	9	0	PM	F
1953	1	10	0	PM	F
1953	1	11	0	PM	F
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1953	1	14	T	PM	F
1953	1	15	T	PM	F
1953	1	16	T	PM	F
1953	1	17	0.54	PM	F
1953	1	18	0	PM	F
1953	1	19	0	PM	F
1953	1	20	0.12	PM	F
1953	1	21	T	PM	F
1953	1	22	T	PM	F
1953	1	23	0.26	PM	F
1953	1	24	T	PM	F
1953	1	25	0	PM	F
1953	1	26	0	PM	F
1953	1	27	0	PM	F
1953	1	28	0	PM	F
1953	1	29	T	PM	F
1953	1	30	0	PM	F
1953	1	31	0	PM	F
1953	2	1	0	PM	F
1953	2	2	T	PM	F
1953	2	3	0	PM	F
1953	2	4	0	PM	F
1953	2	5	T	PM	F
1953	2	6	0.35	PM	F
1953	2	7	0	PM	F
1953	2	8	0	PM	F
1953	2	9	0	PM	F
1953	2	10	T	PM	F
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1953	2	12	0	PM	F

1953	2	13	0	PM	F
1953	2	14	0	PM	F
1953	2	15	0	PM	F
1953	2	16	T	PM	F
1953	2	17	0	PM	F
1953	2	18	0	PM	F
1953	2	19	T	PM	F
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1953	2	21	T	PM	F
1953	2	22	0	PM	F
1953	2	23	0	PM	F
1953	2	24	0	PM	F
1953	2	25	T	PM	F
1953	2	26	0	PM	F
1953	2	27	0	PM	F
1953	2	28	0	PM	F
1953	3	1	T	PM	F
1953	3	2	0.4	PM	F
1953	3	3	0.79	PM	F
1953	3	4	T	PM	F
1953	3	5	T	PM	F
1953	3	6	0	PM	F
1953	3	7	0.2	PM	F
1953	3	8	0	PM	F
1953	3	9	0	PM	F
1953	3	10	0	PM	F
1953	3	11	0.1	PM	F
1953	3	12	0.96	PM	F
1953	3	13	0	PM	F
1953	3	14	0.53	PM	F
1953	3	15	0.38	PM	F
1953	3	16	0	PM	F
1953	3	17	0	PM	F
1953	3	18	0.77	PM	F
1953	3	19	0	PM	F
1953	3	20	T	PM	F
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1953	3	22	0.03	PM	F
1953	3	23	0	PM	F
1953	3	24	T	PM	F
1953	3	25	T	PM	F
1953	3	26	0	PM	F
1953	3	27	0	PM	F
1953	3	28	0	PM	F
1953	3	29	0	PM	F
1953	3	30	1.16	PM	F
1953	3	31	1.32	PM	F
1953	4	1	0.22	PM	F
1953	4	2	T	PM	F
1953	4	3	0.11	PM	F
1953	4	4	0	PM	F
1953	4	5	0	PM	F
1953	4	6	T	PM	F
1953	4	7	0	PM	F
1953	4	8	0.29	PM	F
1953	4	9	T	PM	F
1953	4	10	0	PM	F
1953	4	11	0	PM	F
1953	4	12	T	PM	F
1953	4	13	0	PM	F
1953	4	14	T	PM	F
1953	4	15	0.14	PM	F
1953	4	16	T	PM	F
1953	4	17	0.16	PM	F
1953	4	18	T	PM	F
1953	4	19	T	PM	F
1953	4	20	0	PM	F
1953	4	21	0	PM	F
1953	4	22	0	PM	F
1953	4	23	0	PM	F
1953	4	24	0.26	PM	F
1953	4	25	0	PM	F
1953	4	26	T	PM	F
1953	4	27	0	PM	F
1953	4	28	T	PM	F
1953	4	29	0	PM	F
1953	4	30	0.27	PM	F
1953	5	1	0.1	PM	F
1953	5	2	0	PM	F
1953	5	3	0	PM	F
1953	5	4	T	PM	F
1953	5	5	0.26	PM	F
1953	5	6	0	PM	F
1953	5	7	0.22	PM	F
1953	5	8	T	PM	F
1953	5	9	0	PM	F
1953	5	10	0	PM	F
1953	5	11	0	PM	F
1953	5	12	0	PM	F
1953	5	13	T	PM	F
1953	5	14	T	PM	F
1953	5	15	0	PM	F
1953	5	16	0.35	PM	F
1953	5	17	0.5	PM	F
1953	5	18	0	PM	F
1953	5	19	0	PM	F
1953	5	20	0	PM	F
1953	5	21	0	PM	F
1953	5	22	T	PM	F
1953	5	23	0	PM	F
1953	5	24	T	PM	F
1953	5	25	0	PM	F
1953	5	26	0	PM	F
1953	5	27	0	PM	F
1953	5	28	0	PM	F
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1953	5	31	0	PM	F
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1953	6	2	0	PM	F
1953	6	3	0	PM	F
1953	6	4	0	PM	F
1953	6	5	0	PM	F
1953	6	6	1.16	PM	F
1953	6	7	0	PM	F

1953	6	8	0.36	PM	F
1953	6	9	T	PM	F
1953	6	10	0	PM	F
1953	6	11	0	PM	F
1953	6	12	0	PM	F
1953	6	13	1.3	PM	F
1953	6	14	0.3	PM	F
1953	6	15	T	PM	F
1953	6	16	0	PM	F
1953	6	17	0	PM	F
1953	6	18	0	PM	F
1953	6	19	0	PM	F
1953	6	20	0	PM	F
1953	6	21	0	PM	F
1953	6	22	0	PM	F
1953	6	23	0	PM	F
1953	6	24	0.02	PM	F
1953	6	25	0.39	PM	F
1953	6	26	2.7	PM	F
1953	6	27	T	PM	F
1953	6	28	0.87	PM	F
1953	6	29	0	PM	F
1953	6	30	0	PM	F
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1953	7	2	0.57	PM	F
1953	7	3	0	PM	F
1953	7	4	0	PM	F
1953	7	5	0.49	PM	F
1953	7	6	0.83	PM	F
1953	7	7	0	PM	F
1953	7	8	0	PM	F
1953	7	9	0	PM	F
1953	7	10	0	PM	F
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1953	7	13	0	PM	F
1953	7	14	0	PM	F
1953	7	15	0	PM	F
1953	7	16	T	PM	F
1953	7	17	1.08	PM	F
1953	7	18	0	PM	F
1953	7	19	0	PM	F
1953	7	20	0	PM	F
1953	7	21	0.07	PM	F
1953	7	22	1.2	PM	F
1953	7	23	0	PM	F
1953	7	24	0	PM	F
1953	7	25	0	PM	F
1953	7	26	0	PM	F
1953	7	27	0	PM	F
1953	7	28	0	PM	F
1953	7	29	0	PM	F
1953	7	30	T	PM	F
1953	7	31	0	PM	F
1953	8	1	0	PM	F
1953	8	2	0	PM	F
1953	8	3	T	PM	F
1953	8	4	0.11	PM	F
1953	8	5	T	PM	F
1953	8	6	0	PM	F
1953	8	7	0.32	PM	F
1953	8	8	1.56	PM	F
1953	8	9	0	PM	F
1953	8	10	0	PM	F
1953	8	11	0	PM	F
1953	8	12	0.21	PM	F
1953	8	13	0	PM	F
1953	8	14	0	PM	F
1953	8	15	0	PM	F
1953	8	16	0.03	PM	F
1953	8	17	0	PM	F
1953	8	18	0	PM	F
1953	8	19	0	PM	F
1953	8	20	0	PM	F
1953	8	21	0	PM	F
1953	8	22	0	PM	F
1953	8	23	0	PM	F
1953	8	24	0	PM	F
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1953	8	26	0	PM	F
1953	8	27	0	PM	F
1953	8	28	0	PM	F
1953	8	29	0	PM	F
1953	8	30	0	PM	F
1953	8	31	0	PM	F
1953	9	1	0	PM	F
1953	9	2	0	PM	F
1953	9	3	0	PM	F
1953	9	4	0.9	PM	F
1953	9	5	0	PM	F
1953	9	6	0.03	PM	F
1953	9	7	0	PM	F
1953	9	8	0	PM	F
1953	9	9	0	PM	F
1953	9	10	0	PM	F
1953	9	11	0	PM	F
1953	9	12	0	PM	F
1953	9	13	0	PM	F
1953	9	14	T	PM	F
1953	9	15	0	PM	F
1953	9	16	0	PM	F
1953	9	17	0	PM	F
1953	9	18	0	PM	F
1953	9	19	T	PM	F
1953	9	20	0	PM	F
1953	9	21	0	PM	F
1953	9	22	0	PM	F
1953	9	23	0	PM	F
1953	9	24	0	PM	F
1953	9	25	0	PM	F
1953	9	26	0	PM	F
1953	9	27	T	PM	F
1953	9	28	0	PM	F
1953	9	29	0	PM	F
1953	9	30	0	PM	F

1953	10	1		0 PM	F
1953	10	2		0 PM	F
1953	10	3		0 PM	F
1953	10	4		0.45 PM	F
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1953	10	22		0 PM	F
1953	10	23		0 PM	F
1953	10	24		0 PM	F
1953	10	25		0 PM	F
1953	10	26		0.1 PM	F
1953	10	27		1.45 PM	F
1953	10	28		0.04 PM	F
1953	10	29		0 PM	F
1953	10	30		0 PM	F
1953	10	31		0 PM	F
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1953	11	16		0 PM	F
1953	11	17		0 PM	F
1953	11	18	T	PM	F
1953	11	19		0 PM	F
1953	11	20		0.05 PM	F
1953	11	21		0 PM	F
1953	11	22		0.7 PM	F
1953	11	23		0 PM	F
1953	11	24	T	PM	F
1953	11	25	T	PM	F
1953	11	26	T	PM	F
1953	11	27		0.1 PM	F
1953	11	28		0 PM	F
1953	11	29		0.17 PM	F
1953	11	30		0 PM	F
1953	12	1		0 PM	F
1953	12	2		0.34 PM	F
1953	12	3		0.37 PM	F
1953	12	4		0 PM	F
1953	12	5		0 PM	F
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1953	12	7		0 PM	F
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1953	12	10	T	PM	F
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1953	12	12		0 PM	F
1953	12	13		0 PM	F
1953	12	14		0.07 PM	F
1953	12	15		0 PM	F
1953	12	16		0 PM	F
1953	12	17		0 PM	F
1953	12	18		0 PM	F
1953	12	19		0 PM	F
1953	12	20		0 PM	F
1953	12	21	T	PM	F
1953	12	22		0.37 PM	F
1953	12	23		0 PM	F
1953	12	24		0 PM	F
1953	12	25		0 PM	F
1953	12	26		0 PM	F
1953	12	27		0 PM	F
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1954	1	11	T	PM	F
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1954	1	14	T	PM	F
1954	1	15	T	PM	F
1954	1	16		0 PM	F
1954	1	17		0 PM	F
1954	1	18		0 PM	F
1954	1	19		0 PM	F
1954	1	20		1.2 PM	F
1954	1	21		0.28 PM	F
1954	1	22		0 PM	F
1954	1	23		0 PM	F

1954	1	24	T	PM	F
1954	1	25	T	PM	F
1954	1	26	0.14	PM	F
1954	1	27	0.47	PM	F
1954	1	28	0	PM	F
1954	1	29	0.06	PM	F
1954	1	30	0	PM	F
1954	1	31	0	PM	F
1954	2	1	0	PM	F
1954	2	2	0	PM	F
1954	2	3	0.08	PM	F
1954	2	4	0	PM	F
1954	2	5	0	PM	F
1954	2	6	0	PM	F
1954	2	7	0	PM	F
1954	2	8	0	PM	F
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1954	2	15	T	PM	F
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1954	2	17	0	PM	F
1954	2	18	0	PM	F
1954	2	19	0	PM	F
1954	2	20	T	PM	F
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1954	2	22	0	PM	F
1954	2	23	0.04	PM	F
1954	2	24	0	PM	F
1954	2	25	T	PM	F
1954	2	26	T	PM	F
1954	2	27	0.28	PM	F
1954	2	28	T	PM	F
1954	3	1	0	PM	F
1954	3	2	0.15	PM	F
1954	3	3	0.25	PM	F
1954	3	4	0	PM	F
1954	3	5	0	PM	F
1954	3	6	0	PM	F
1954	3	7	0	PM	F
1954	3	8	0	PM	F
1954	3	9	0	PM	F
1954	3	10	T	PM	F
1954	3	11	0.07	PM	F
1954	3	12	0.05	PM	F
1954	3	13	0.35	PM	F
1954	3	14	T	PM	F
1954	3	15	0	PM	F
1954	3	16	0	PM	F
1954	3	17	0	PM	F
1954	3	18	0	PM	F
1954	3	19	0.5	PM	F
1954	3	20	0.1	PM	F
1954	3	21	0	PM	F
1954	3	22	0	PM	F
1954	3	23	0	PM	F
1954	3	24	0.08	PM	F
1954	3	25	0.51	PM	F
1954	3	26	0	PM	F
1954	3	27	0	PM	F
1954	3	28	0	PM	F
1954	3	29	0.05	PM	F
1954	3	30	0	PM	F
1954	3	31	T	PM	F
1954	4	1	0	PM	F
1954	4	2	0	PM	F
1954	4	3	0	PM	F
1954	4	4	0	PM	F
1954	4	5	0.71	PM	F
1954	4	6	0.8	PM	F
1954	4	7	T	PM	F
1954	4	8	0	PM	F
1954	4	9	0	PM	F
1954	4	10	0.07	PM	F
1954	4	11	1.25	PM	F
1954	4	12	0	PM	F
1954	4	13	0	PM	F
1954	4	14	0	PM	F
1954	4	15	0.42	PM	F
1954	4	16	0.31	PM	F
1954	4	17	0	PM	F
1954	4	18	0	PM	F
1954	4	19	0	PM	F
1954	4	20	0	PM	F
1954	4	21	0	PM	F
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1954	4	23	T	PM	F
1954	4	24	0	PM	F
1954	4	25	0	PM	F
1954	4	26	0	PM	F
1954	4	27	0.2	PM	F
1954	4	28	0	PM	F
1954	4	29	0	PM	F
1954	4	30	0	PM	F
1954	5	1	0.2	PM	F
1954	5	2	0.36	PM	F
1954	5	3	0	PM	F
1954	5	4	0	PM	F
1954	5	5	0	PM	F
1954	5	6	0	PM	F
1954	5	7	0	PM	F
1954	5	8	0	PM	F
1954	5	9	0	PM	F
1954	5	10	0	PM	F
1954	5	11	0	PM	F
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1954	5	13	0	PM	F
1954	5	14	0	PM	F
1954	5	15	0	PM	F
1954	5	16	0.45	PM	F
1954	5	17	T	PM	F
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1954	5	20		0 PM	F
1954	5	21		0 PM	F
1954	5	22		0 PM	F
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1954	5	29		0.1 PM	F
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1954	6	4	T	PM	F
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1954	6	24		0 PM	F
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1954	7	5		0 PM	F
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1954	8	22		0 PM	F
1954	8	23		0 PM	F
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1954	8	25	T	PM	F
1954	8	26	T	PM	F
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1954	8	28		0.22 PM	F
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1954	9	9		0 PM	F
1954	9	10		0 PM	F

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1954	9	25		0 PM	F
1954	9	26		0 PM	F
1954	9	27		0 PM	F
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1954	10	22		0 PM	F
1954	10	23		0 PM	F
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1954	10	29	T	PM	F
1954	10	30	T	PM	F
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1954	11	2	T	PM	F
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1954	11	4		0.04 PM	F
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1954	11	6		0 PM	F
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1954	11	28		0.05 PM	F
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1955	1	10		0 PM	F
1955	1	11		0 PM	F
1955	1	12		0.06 PM	F
1955	1	13	T	PM	F
1955	1	14		0.06 PM	F
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1955	1	16		0 PM	F
1955	1	17		0 PM	F
1955	1	18		0 PM	F
1955	1	19		0 PM	F
1955	1	20	T	PM	F
1955	1	21		0.07 PM	F
1955	1	22	T	PM	F
1955	1	23	T	PM	F
1955	1	24		0.08 PM	F
1955	1	25	T	PM	F
1955	1	26		0 PM	F
1955	1	27		0 PM	F
1955	1	28		0.15 PM	F
1955	1	29	T	PM	F
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1955	1	31		0 PM	F
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1955	3	2		0 PM	F
1955	3	3	T	PM	F
1955	3	4	T	PM	F
1955	3	5	T	PM	F
1955	3	6	T	PM	F
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1955	3	26		0.06 PM	F
1955	3	27	T	PM	F
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1955	4	5	T	PM	F
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1955	4	16		0 PM	F
1955	4	17		0 PM	F
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1955	4	25		0.05 PM	F
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1955	4	27		0 PM	F
1955	4	28		0 PM	F

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1955	4	30	0	PM	F
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1955	5	2	0	PM	F
1955	5	3	0	PM	F
1955	5	4	0	PM	F
1955	5	5	0	PM	F
1955	5	6	0	PM	F
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1955	5	11	0	PM	F
1955	5	12	0	PM	F
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1955	5	15	0	PM	F
1955	5	16	0	PM	F
1955	5	17	0	PM	F
1955	5	18	0	PM	F
1955	5	19	0	PM	F
1955	5	20	0	PM	F
1955	5	21	T	PM	F
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1955	5	23	0.26	PM	F
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1955	5	25	0.25	PM	F
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1955	6	2	0.05	PM	F
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1955	6	16	0	PM	F
1955	6	17	0	PM	F
1955	6	18	0	PM	F
1955	6	19	0	PM	F
1955	6	20	0.11	PM	F
1955	6	21	0	PM	F
1955	6	22	T	PM	F
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1955	6	27	0	PM	F
1955	6	28	0	PM	F
1955	6	29	0	PM	F
1955	6	30	T	PM	F
1955	7	1	0	PM	F
1955	7	2	T	PM	F
1955	7	3	0	PM	F
1955	7	4	0.19	PM	F
1955	7	5	0.09	PM	F
1955	7	6	T	PM	F
1955	7	7	T	PM	F
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1955	7	9	0	PM	F
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1955	7	11	0	PM	F
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1955	7	15	0.07	PM	F
1955	7	16	T	PM	F
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1955	7	18	0.05	PM	F
1955	7	19	0.13	PM	F
1955	7	20	0	PM	F
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1955	8	3	0	PM	F
1955	8	4	0	PM	F
1955	8	5	0	PM	F
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1955	8	11	0	PM	F
1955	8	12	0	PM	F
1955	8	13	0	PM	F
1955	8	14	0	PM	F
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1955	8	18	0	PM	F
1955	8	19	0	PM	F
1955	8	20	0	PM	F
1955	8	21	0	PM	F

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1955	8	23	0	PM	F
1955	8	24	0	PM	F
1955	8	25	0	PM	F
1955	8	26	0	PM	F
1955	8	27	0	PM	F
1955	8	28	0	PM	F
1955	8	29	0.1	PM	F
1955	8	30	1.5	PM	F
1955	8	31	0	PM	F
1955	9	1	0	PM	F
1955	9	2	0	PM	F
1955	9	3	0	PM	F
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1955	9	7	0	PM	F
1955	9	8	0	PM	F
1955	9	9	0	PM	F
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1955	9	11	0.1	PM	F
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1955	9	14	0	PM	F
1955	9	15	0	PM	F
1955	9	16	0	PM	F
1955	9	17	0	PM	F
1955	9	18	0	PM	F
1955	9	19	0	PM	F
1955	9	20	0	PM	F
1955	9	21	0	PM	F
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1955	9	23	0.12	PM	F
1955	9	24	0	PM	F
1955	9	25	0	PM	F
1955	9	26	0.1	PM	F
1955	9	27	0.8	PM	F
1955	9	28	0	PM	F
1955	9	29	1	PM	F
1955	9	30	0	PM	F
1955	10	1	0	PM	F
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1955	10	6	0.5	PM	F
1955	10	7	0.38	PM	F
1955	10	8	0	PM	F
1955	10	9	0	PM	F
1955	10	10	0	PM	F
1955	10	11	0	PM	F
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1955	10	13	0	PM	F
1955	10	14	0	PM	F
1955	10	15	0	PM	F
1955	10	16	0	PM	F
1955	10	17	0.1	PM	F
1955	10	18	0	PM	F
1955	10	19	0	PM	F
1955	10	20	0	PM	F
1955	10	21	0	PM	F
1955	10	22	0	PM	F
1955	10	23	0	PM	F
1955	10	24	0.15	PM	F
1955	10	25	0	PM	F
1955	10	26	0	PM	F
1955	10	27	0	PM	F
1955	10	28	0.1	PM	F
1955	10	29	1.15	PM	F
1955	10	30	0.15	PM	F
1955	10	31	T	PM	F
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1955	11	2	0.53	PM	F
1955	11	3	0.1	PM	F
1955	11	4	0	PM	F
1955	11	5	0	PM	F
1955	11	6	0	PM	F
1955	11	7	0	PM	F
1955	11	8	0	PM	F
1955	11	9	0	PM	F
1955	11	10	T	PM	F
1955	11	11	T	PM	F
1955	11	12	0	PM	F
1955	11	13	0.16	PM	F
1955	11	14	T	PM	F
1955	11	15	T	PM	F
1955	11	16	0.17	PM	F
1955	11	17	0	PM	F
1955	11	18	0	PM	F
1955	11	19	0.18	PM	F
1955	11	20	0	PM	F
1955	11	21	0	PM	F
1955	11	22	0	PM	F
1955	11	23	0.4	PM	F
1955	11	24	0	PM	F
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1955	11	26	0	PM	F
1955	11	27	T	PM	F
1955	11	28	T	PM	F
1955	11	29	T	PM	F
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1955	12	6	0	PM	F
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1955	12	10	0	PM	F
1955	12	11	0	PM	F
1955	12	12	0	PM	F
1955	12	13	0	PM	F
1955	12	14	0.12	PM	F

1955	12	15		0	PM	F
1955	12	16		0	PM	F
1955	12	17	T		PM	F
1955	12	18		0.07	PM	F
1955	12	19		0	PM	F
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1955	12	22		0	PM	F
1955	12	23		0	PM	F
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1955	12	31		0	PM	F
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1956	1	2		0	PM	F
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1956	1	7		0	PM	F
1956	1	8		0	PM	F
1956	1	9		0	PM	F
1956	1	10		0	PM	F
1956	1	11	T		PM	F
1956	1	12		0	PM	F
1956	1	13		0	PM	F
1956	1	14		0	PM	F
1956	1	15		0	PM	F
1956	1	16		0.08	PM	F
1956	1	17		0	PM	F
1956	1	18	T		PM	F
1956	1	19		0.19	PM	F
1956	1	20	T		PM	F
1956	1	21	T		PM	F
1956	1	22	T		PM	F
1956	1	23		0	PM	F
1956	1	24		0	PM	F
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1956	1	26		0	PM	F
1956	1	27		0	PM	F
1956	1	28	T		PM	F
1956	1	29		0	PM	F
1956	1	30		0.55	PM	F
1956	1	31		0	PM	F
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1956	2	4		0	PM	F
1956	2	5		0	PM	F
1956	2	6		0.15	PM	F
1956	2	7	T		PM	F
1956	2	8	T		PM	F
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1956	2	19		0	PM	F
1956	2	20		0	PM	F
1956	2	21	T		PM	F
1956	2	22		0	PM	F
1956	2	23		0	PM	F
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1956	2	25		0.05	PM	F
1956	2	26		0	PM	F
1956	2	27		0.2	PM	F
1956	2	28		0	PM	F
1956	2	29		0	PM	F
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1956	3	3		0.1	PM	F
1956	3	4		0	PM	F
1956	3	5		0	PM	F
1956	3	6		0	PM	F
1956	3	7	T		PM	F
1956	3	8	T		PM	F
1956	3	9		0	PM	F
1956	3	10		0	PM	F
1956	3	11	T		PM	F
1956	3	12	T		PM	F
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1956	3	22		0	PM	F
1956	3	23		0	PM	F
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1956	3	26		0	PM	F
1956	3	27		0	PM	F
1956	3	28		0.11	PM	F
1956	3	29	T		PM	F
1956	3	30		0	PM	F
1956	3	31		0	PM	F
1956	4	1		0	PM	F
1956	4	2		0.1	PM	F
1956	4	3		0	PM	F
1956	4	4		0	PM	F
1956	4	5		0	PM	F
1956	4	6		0	PM	F
1956	4	7		0.22	PM	F

1956	4	8	0	PM	F
1956	4	9	0	PM	F
1956	4	10	0	PM	F
1956	4	11	0	PM	F
1956	4	12	0	PM	F
1956	4	13	0	PM	F
1956	4	14	0	PM	F
1956	4	15	0	PM	F
1956	4	16 T		PM	F
1956	4	17	0	PM	F
1956	4	18	0	PM	F
1956	4	19	0	PM	F
1956	4	20	0	PM	F
1956	4	21	0	PM	F
1956	4	22	0.01	PM	F
1956	4	23	0	PM	F
1956	4	24	0	PM	F
1956	4	25	0.33	PM	F
1956	4	26 T		PM	F
1956	4	27	0	PM	F
1956	4	28	0.35	PM	F
1956	4	29	1.52	PM	F
1956	4	30 T		PM	F
1956	5	1	0	PM	F
1956	5	2	0.07	PM	F
1956	5	3	0	PM	F
1956	5	4	0	PM	F
1956	5	5	0	PM	F
1956	5	6	0	PM	F
1956	5	7	0	PM	F
1956	5	8	0	PM	F
1956	5	9	0	PM	F
1956	5	10	0	PM	F
1956	5	11	0	PM	F
1956	5	12	0	PM	F
1956	5	13	0	PM	F
1956	5	14	0	PM	F
1956	5	15	0.33	PM	F
1956	5	16	0	PM	F
1956	5	17	0.02	PM	F
1956	5	18	0	PM	F
1956	5	19	0	PM	F
1956	5	20	0	PM	F
1956	5	21 T		PM	F
1956	5	22 T		PM	F
1956	5	23	0.58	PM	F
1956	5	24	0	PM	F
1956	5	25	0	PM	F
1956	5	26	0.92	PM	F
1956	5	27	0.72	PM	F
1956	5	28 T		PM	F
1956	5	29	0	PM	F
1956	5	30	0.47	PM	F
1956	5	31	0	PM	F
1956	6	1 T		PM	F
1956	6	2	0	PM	F
1956	6	3	0	PM	F
1956	6	4	0	PM	F
1956	6	5	0	PM	F
1956	6	6	0	PM	F
1956	6	7	0.31	PM	F
1956	6	8	0	PM	F
1956	6	9	0	PM	F
1956	6	10	0	PM	F
1956	6	11	0	PM	F
1956	6	12	0	PM	F
1956	6	13	0	PM	F
1956	6	14	0.09	PM	F
1956	6	15	0	PM	F
1956	6	16	0	PM	F
1956	6	17	0.17	PM	F
1956	6	18	0.17	PM	F
1956	6	19	0.47	PM	F
1956	6	20	0.14	PM	F
1956	6	21 T		PM	F
1956	6	22	0.6	PM	F
1956	6	23	0	PM	F
1956	6	24	0	PM	F
1956	6	25	0	PM	F
1956	6	26 T		PM	F
1956	6	27	0	PM	F
1956	6	28	0	PM	F
1956	6	29	0	PM	F
1956	6	30	0	PM	F
1956	7	1	0	PM	F
1956	7	2	0	PM	F
1956	7	3	0.9	PM	F
1956	7	4	1.05	PM	F
1956	7	5 T		PM	F
1956	7	6	0	PM	F
1956	7	7	0	PM	F
1956	7	8	1.04	PM	F
1956	7	9	0	PM	F
1956	7	10	0	PM	F
1956	7	11	0	PM	F
1956	7	12	0.22	PM	F
1956	7	13	0	PM	F
1956	7	14	0	PM	F
1956	7	15	0.63	PM	F
1956	7	16	0.1	PM	F
1956	7	17	0.04	PM	F
1956	7	18	0.1	PM	F
1956	7	19	0.14	PM	F
1956	7	20	0	PM	F
1956	7	21 T		PM	F
1956	7	22	0	PM	F
1956	7	23	0	PM	F
1956	7	24	0	PM	F
1956	7	25	0.44	PM	F
1956	7	26	0	PM	F
1956	7	27	0	PM	F
1956	7	28	0	PM	F
1956	7	29	0	PM	F
1956	7	30	0	PM	F
1956	7	31	0	PM	F

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1956	8	2		0 PM	F
1956	8	3		1.3 PM	F
1956	8	4		0 PM	F
1956	8	5		0 PM	F
1956	8	6		0 PM	F
1956	8	7		0 PM	F
1956	8	8		0.15 PM	F
1956	8	9		0.25 PM	F
1956	8	10		0 PM	F
1956	8	11		0 PM	F
1956	8	12		0 PM	F
1956	8	13		1.95 PM	F
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1956	8	15		0 PM	F
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1956	8	19		0 PM	F
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1956	8	22		0 PM	F
1956	8	23		0 PM	F
1956	8	24		0 PM	F
1956	8	25		0 PM	F
1956	8	26		0 PM	F
1956	8	27		0 PM	F
1956	8	28		0 PM	F
1956	8	29		0.27 PM	F
1956	8	30		0.28 PM	F
1956	8	31		0.15 PM	F
1956	9	1		0.5 PM	F
1956	9	2		0 PM	F
1956	9	3		0 PM	F
1956	9	4		0 PM	F
1956	9	5		0 PM	F
1956	9	6		0 PM	F
1956	9	7		0.06 PM	F
1956	9	8		0 PM	F
1956	9	9		0 PM	F
1956	9	10		0 PM	F
1956	9	11		0 PM	F
1956	9	12		0 PM	F
1956	9	13		0 PM	F
1956	9	14		0.12 PM	F
1956	9	15		0.47 PM	F
1956	9	16		0 PM	F
1956	9	17		0 PM	F
1956	9	18	T	PM	F
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1956	9	20		0 PM	F
1956	9	21		0 PM	F
1956	9	22		0 PM	F
1956	9	23		0.15 PM	F
1956	9	24		0 PM	F
1956	9	25		0 PM	F
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1956	11	2		0 PM	F
1956	11	3		0 PM	F
1956	11	4		0 PM	F
1956	11	5		0 PM	F
1956	11	6		0.53 PM	F
1956	11	7		0 PM	F
1956	11	8	T	PM	F
1956	11	9		0 PM	F
1956	11	10		0 PM	F
1956	11	11		0 PM	F
1956	11	12		0 PM	F
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1956	11	16		0 PM	F
1956	11	17		0 PM	F
1956	11	18		0 PM	F
1956	11	19		0 PM	F
1956	11	20		0.65 PM	F
1956	11	21		0.45 PM	F
1956	11	22	T	PM	F
1956	11	23		0.15 PM	F

1956	11	24	T	PM	F
1956	11	25	T	PM	F
1956	11	26	0.05	PM	F
1956	11	27	0	PM	F
1956	11	28	T	PM	F
1956	11	29	0.05	PM	F
1956	11	30	0	PM	F
1956	12	1	0	PM	F
1956	12	2	0	PM	F
1956	12	3	0	PM	F
1956	12	4	0	PM	F
1956	12	5	0.25	PM	F
1956	12	6	0.18	PM	F
1956	12	7	0.2	PM	F
1956	12	8	0.6	PM	F
1956	12	9	0.2	PM	F
1956	12	10	0	PM	F
1956	12	11	0	PM	F
1956	12	12	0	PM	F
1956	12	13	0	PM	F
1956	12	14	T	PM	F
1956	12	15	T	PM	F
1956	12	16	T	PM	F
1956	12	17	0	PM	F
1956	12	18	0	PM	F
1956	12	19	T	PM	F
1956	12	20	0.33	PM	F
1956	12	21	T	PM	F
1956	12	22	T	PM	F
1956	12	23	0.25	PM	F
1956	12	24	T	PM	F
1956	12	25	0	PM	F
1956	12	26	T	PM	F
1956	12	27	0	PM	F
1956	12	28	0.2	PM	F
1956	12	29	0	PM	F
1956	12	30	T	PM	F
1956	12	31	0	PM	F
1957	1	1	0	PM	F
1957	1	2	0	PM	F
1957	1	3	T	PM	F
1957	1	4	0	PM	F
1957	1	5	0	PM	F
1957	1	6	0.15	PM	F
1957	1	7	0	PM	F
1957	1	8	0.2	PM	F
1957	1	9	0.25	PM	F
1957	1	10	T	PM	F
1957	1	11	0	PM	F
1957	1	12	0	PM	F
1957	1	13	0.12	PM	F
1957	1	14	T	PM	F
1957	1	15	T	PM	F
1957	1	16	0	PM	F
1957	1	17	0.05	PM	F
1957	1	18	T	PM	F
1957	1	19	T	PM	F
1957	1	20	T	PM	F
1957	1	21	0	PM	F
1957	1	22	0.75	PM	F
1957	1	23	0.15	PM	F
1957	1	24	0	PM	F
1957	1	25	0	PM	F
1957	1	26	0	PM	F
1957	1	27	0	PM	F
1957	1	28	T	PM	F
1957	1	29	T	PM	F
1957	1	30	0	PM	F
1957	1	31	0.05	PM	F
1957	2	1	0	PM	F
1957	2	2	0	PM	F
1957	2	3	T	PM	F
1957	2	4	T	PM	F
1957	2	5	T	PM	F
1957	2	6	T	PM	F
1957	2	7	T	PM	F
1957	2	8	T	PM	F
1957	2	9	0.76	PM	F
1957	2	10	T	PM	F
1957	2	11	0.23	PM	F
1957	2	12	T	PM	F
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1957	2	14	0	PM	F
1957	2	15	0	PM	F
1957	2	16	0	PM	F
1957	2	17	0	PM	F
1957	2	18	0.08	PM	F
1957	2	19	0	PM	F
1957	2	20	0	PM	F
1957	2	21	0	PM	F
1957	2	22	0	PM	F
1957	2	23	T	PM	F
1957	2	24	0	PM	F
1957	2	25	0.1	PM	F
1957	2	26	0.75	PM	F
1957	2	27	0	PM	F
1957	2	28	0	PM	F
1957	3	1	0	PM	F
1957	3	2	0	PM	F
1957	3	3	0	PM	F
1957	3	4	0	PM	F
1957	3	5	0	PM	F
1957	3	6	0	PM	F
1957	3	7	T	PM	F
1957	3	8	T	PM	F
1957	3	9	T	PM	F
1957	3	10	0	PM	F
1957	3	11	0.35	PM	F
1957	3	12	0	PM	F
1957	3	13	0	PM	F
1957	3	14	0.08	PM	F
1957	3	15	0	PM	F
1957	3	16	0	PM	F
1957	3	17	0	PM	F
1957	3	18	0.1	PM	F

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1957	3	20		0 PM	F
1957	3	21		0 PM	F
1957	3	22		0.1 PM	F
1957	3	23		0 PM	F
1957	3	24	T	PM	F
1957	3	25		0.6 PM	F
1957	3	26		0 PM	F
1957	3	27	T	PM	F
1957	3	28		0 PM	F
1957	3	29		0 PM	F
1957	3	30		0 PM	F
1957	3	31		0 PM	F
1957	4	1		0.2 PM	F
1957	4	2	T	PM	F
1957	4	3		1.25 PM	F
1957	4	4		0.22 PM	F
1957	4	5		0.9 PM	F
1957	4	6		0 PM	F
1957	4	7	T	PM	F
1957	4	8		1.25 PM	F
1957	4	9		0 PM	F
1957	4	10		0 PM	F
1957	4	11		0 PM	F
1957	4	12		0.1 PM	F
1957	4	13		0 PM	F
1957	4	14		0 PM	F
1957	4	15		0 PM	F
1957	4	16	T	PM	F
1957	4	17		0.25 PM	F
1957	4	18		0.42 PM	F
1957	4	19		0.15 PM	F
1957	4	20		0.65 PM	F
1957	4	21	T	PM	F
1957	4	22		0.35 PM	F
1957	4	23		0.1 PM	F
1957	4	24		0.8 PM	F
1957	4	25		0.52 PM	F
1957	4	26		1.75 PM	F
1957	4	27		0.56 PM	F
1957	4	28		0.25 PM	F
1957	4	29		0 PM	F
1957	4	30		0 PM	F
1957	5	1		0 PM	F
1957	5	2		0 PM	F
1957	5	3		0 PM	F
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1957	5	6		0 PM	F
1957	5	7		0 PM	F
1957	5	8		0 PM	F
1957	5	9		0.05 PM	F
1957	5	10		0.53 PM	F
1957	5	11		0.63 PM	F
1957	5	12		0.22 PM	F
1957	5	13		0.53 PM	F
1957	5	14		0 PM	F
1957	5	15		0 PM	F
1957	5	16		0 PM	F
1957	5	17		0.95 PM	F
1957	5	18		0.08 PM	F
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1957	5	22		0 PM	F
1957	5	23		0.39 PM	F
1957	5	24		0 PM	F
1957	5	25		0.29 PM	F
1957	5	26		0 PM	F
1957	5	27		0 PM	F
1957	5	28		0 PM	F
1957	5	29		0 PM	F
1957	5	30		0 PM	F
1957	5	31		0.1 PM	F
1957	6	1		0.95 PM	F
1957	6	2		0 PM	F
1957	6	3		0 PM	F
1957	6	4		0 PM	F
1957	6	5		0 PM	F
1957	6	6		0 PM	F
1957	6	7		0.2 PM	F
1957	6	8	T	PM	F
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1957	6	10		0 PM	F
1957	6	11		0.1 PM	F
1957	6	12		0.33 PM	F
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1957	6	14		0.6 PM	F
1957	6	15		0 PM	F
1957	6	16	T	PM	F
1957	6	17		1.15 PM	F
1957	6	18		0 PM	F
1957	6	19		0 PM	F
1957	6	20		0 PM	F
1957	6	21		0 PM	F
1957	6	22		0 PM	F
1957	6	23		0 PM	F
1957	6	24		0 PM	F
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1957	6	26		0.2 PM	F
1957	6	27		0.66 PM	F
1957	6	28		1.64 PM	F
1957	6	29		0 PM	F
1957	6	30		0 PM	F
1957	7	1		0 PM	F
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1957	7	5		0 PM	F
1957	7	6		0 PM	F
1957	7	7		0 PM	F
1957	7	8		0 PM	F
1957	7	9		0 PM	F
1957	7	10		0 PM	F
1957	7	11		0 PM	F

1957	7	12		0 PM	F
1957	7	13		0.15 PM	F
1957	7	14	T	PM	F
1957	7	15		0 PM	F
1957	7	16		0.22 PM	F
1957	7	17		0.82 PM	F
1957	7	18		0 PM	F
1957	7	19		0 PM	F
1957	7	20		0 PM	F
1957	7	21		0 PM	F
1957	7	22	T	PM	F
1957	7	23		0.63 PM	F
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1957	7	25		0 PM	F
1957	7	26		0 PM	F
1957	7	27		0 PM	F
1957	7	28	T	PM	F
1957	7	29		0 PM	F
1957	7	30		0.3 PM	F
1957	7	31		0 PM	F
1957	8	1	T	PM	F
1957	8	2		0.13 PM	F
1957	8	3		0 PM	F
1957	8	4		0.32 PM	F
1957	8	5		0 PM	F
1957	8	6		0 PM	F
1957	8	7		0 PM	F
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1957	8	10		0 PM	F
1957	8	11		0 PM	F
1957	8	12		0 PM	F
1957	8	13		0 PM	F
1957	8	14	T	PM	F
1957	8	15		0 PM	F
1957	8	16	T	PM	F
1957	8	17		0 PM	F
1957	8	18		0 PM	F
1957	8	19		0 PM	F
1957	8	20		0 PM	F
1957	8	21		0 PM	F
1957	8	22		0 PM	F
1957	8	23		0 PM	F
1957	8	24		0.35 PM	F
1957	8	25		0 PM	F
1957	8	26		0 PM	F
1957	8	27	T	PM	F
1957	8	28		0.81 PM	F
1957	8	29		0 PM	F
1957	8	30		0 PM	F
1957	8	31		0 PM	F
1957	9	1	T	PM	F
1957	9	2		0.7 PM	F
1957	9	3		0 PM	F
1957	9	4		0 PM	F
1957	9	5		0 PM	F
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1957	9	7		0 PM	F
1957	9	8		0 PM	F
1957	9	9	T	PM	F
1957	9	10		0 PM	F
1957	9	11		0 PM	F
1957	9	12	T	PM	F
1957	9	13		0 PM	F
1957	9	14		0 PM	F
1957	9	15		0 PM	F
1957	9	16		0 PM	F
1957	9	17		0 PM	F
1957	9	18		0 PM	F
1957	9	19		0.1 PM	F
1957	9	20		0.15 PM	F
1957	9	21		0.52 PM	F
1957	9	22	T	PM	F
1957	9	23		0 PM	F
1957	9	24		0 PM	F
1957	9	25		0 PM	F
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1957	10	7		0 PM	F
1957	10	8		0 PM	F
1957	10	9	T	PM	F
1957	10	10		0 PM	F
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1957	10	12		0 PM	F
1957	10	13		0 PM	F
1957	10	14		0 PM	F
1957	10	15	T	PM	F
1957	10	16		1.1 PM	F
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1957	10	18		0 PM	F
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1957	10	26	T	PM	F
1957	10	27	T	PM	F
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1957	10	29		0 PM	F
1957	10	30		0 PM	F
1957	10	31		0 PM	F
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1957	11	3		0.02 PM	F

1957	11	4	T		PM	F
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1957	11	6		0	PM	F
1957	11	7	T		PM	F
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1957	11	14		1.7	PM	F
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1957	11	16	T		PM	F
1957	11	17	T		PM	F
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1957	11	21	T		PM	F
1957	11	22	T		PM	F
1957	11	23		0	PM	F
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1957	11	25		0	PM	F
1957	11	26		0	PM	F
1957	11	27		0	PM	F
1957	11	28		0	PM	F
1957	11	29		0	PM	F
1957	11	30	T		PM	F
1957	12	1		0	PM	F
1957	12	2		0	PM	F
1957	12	3		0.2	PM	F
1957	12	4	T		PM	F
1957	12	5		0	PM	F
1957	12	6		0	PM	F
1957	12	7		0.81	PM	F
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1957	12	10	T		PM	F
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1957	12	14		0	PM	F
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1957	12	16		0	PM	F
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1957	12	18		0.45	PM	F
1957	12	19		0.47	PM	F
1957	12	20		0.87	PM	F
1957	12	21		0	PM	F
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1957	12	25		0.46	PM	F
1957	12	26		0	PM	F
1957	12	27	T		PM	F
1957	12	28		0.3	PM	F
1957	12	29		0	PM	F
1957	12	30		0	PM	F
1957	12	31		0.25	PM	F
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1958	1	3		0	PM	F
1958	1	4		0	PM	F
1958	1	5		0	PM	F
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1958	1	7	T		PM	F
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1958	1	17	T		PM	F
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1958	1	19		0	PM	F
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1958	1	25		0	PM	F
1958	1	26	T		PM	F
1958	1	27		0.1	PM	F
1958	1	28	T		PM	F
1958	1	29	T		PM	F
1958	1	30		0	PM	F
1958	1	31		0	PM	F
1958	2	1		0	PM	F
1958	2	2	T		PM	F
1958	2	3	T		PM	F
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1958	2	11		0	PM	F
1958	2	12		0	PM	F
1958	2	13	T		PM	F
1958	2	14		0.2	PM	F
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1958	2	17		0	PM	F
1958	2	18		0	PM	F
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1958	2	23		0	PM	F
1958	2	24		0	PM	F
1958	2	25		0	PM	F
1958	2	26	T		PM	F

1958	2	27	0.33	PM	F
1958	2	28	0.08	PM	F
1958	3	1 T		PM	F
1958	3	2 T		PM	F
1958	3	3 T		PM	F
1958	3	4	0	PM	F
1958	3	5	0.12	PM	F
1958	3	6	0	PM	F
1958	3	7	0.1	PM	F
1958	3	8	0	PM	F
1958	3	9	0	PM	F
1958	3	10	0	PM	F
1958	3	11	0.15	PM	F
1958	3	12	0	PM	F
1958	3	13	0	PM	F
1958	3	14	0	PM	F
1958	3	15 T		PM	F
1958	3	16	0	PM	F
1958	3	17	0	PM	F
1958	3	18	0	PM	F
1958	3	19 T		PM	F
1958	3	20 T		PM	F
1958	3	21	0	PM	F
1958	3	22	0	PM	F
1958	3	23	0	PM	F
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1958	3	27	0	PM	F
1958	3	28	0	PM	F
1958	3	29	0	PM	F
1958	3	30 T		PM	F
1958	3	31	0	PM	F
1958	4	1	0	PM	F
1958	4	2 T		PM	F
1958	4	3	0.1	PM	F
1958	4	4	0.1	PM	F
1958	4	5	0.5	PM	F
1958	4	6	0.1	PM	F
1958	4	7	0	PM	F
1958	4	8	0	PM	F
1958	4	9	0	PM	F
1958	4	10	0	PM	F
1958	4	11	0	PM	F
1958	4	12	0	PM	F
1958	4	13	0	PM	F
1958	4	14	0	PM	F
1958	4	15 T		PM	F
1958	4	16	0	PM	F
1958	4	17	0	PM	F
1958	4	18	0	PM	F
1958	4	19	0	PM	F
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1958	4	21	0	PM	F
1958	4	22	0.54	PM	F
1958	4	23	0.42	PM	F
1958	4	24	0.2	PM	F
1958	4	25	0	PM	F
1958	4	26	0	PM	F
1958	4	27 T		PM	F
1958	4	28	0.22	PM	F
1958	4	29 T		PM	F
1958	4	30	0	PM	F
1958	5	1	0	PM	F
1958	5	2	0.17	PM	F
1958	5	3	0.05	PM	F
1958	5	4	0.75	PM	F
1958	5	5	0	PM	F
1958	5	6	0	PM	F
1958	5	7	0	PM	F
1958	5	8	0	PM	F
1958	5	9	0	PM	F
1958	5	10	0	PM	F
1958	5	11	0	PM	F
1958	5	12	0	PM	F
1958	5	13	0	PM	F
1958	5	14	0	PM	F
1958	5	15	0	PM	F
1958	5	16	0.4	PM	F
1958	5	17	0.1	PM	F
1958	5	18	0	PM	F
1958	5	19	0	PM	F
1958	5	20	0	PM	F
1958	5	21	0	PM	F
1958	5	22	0.3	PM	F
1958	5	23	0	PM	F
1958	5	24	0	PM	F
1958	5	25	0	PM	F
1958	5	26	0	PM	F
1958	5	27	0	PM	F
1958	5	28 T		PM	F
1958	5	29	0	PM	F
1958	5	30	0	PM	F
1958	5	31	0.1	PM	F
1958	6	1	1.6	PM	F
1958	6	2	0	PM	F
1958	6	3	0	PM	F
1958	6	4	0	PM	F
1958	6	5	0	PM	F
1958	6	6	0	PM	F
1958	6	7	0	PM	F
1958	6	8	0	PM	F
1958	6	9	0.4	PM	F
1958	6	10	1.6	PM	F
1958	6	11	1.25	PM	F
1958	6	12	0.25	PM	F
1958	6	13	0.27	PM	F
1958	6	14 T		PM	F
1958	6	15	0	PM	F
1958	6	16	0	PM	F
1958	6	17	0.68	PM	F
1958	6	18 T		PM	F
1958	6	19	0.1	PM	F
1958	6	20	0.32	PM	F
1958	6	21	0	PM	F

1958	6	22	0	PM	F
1958	6	23	0.25	PM	F
1958	6	24	0.1	PM	F
1958	6	25	2.18	PM	F
1958	6	26	0	PM	F
1958	6	27	0	PM	F
1958	6	28	0	PM	F
1958	6	29	0	PM	F
1958	6	30	0	PM	F
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1958	7	2	0	PM	F
1958	7	3	1.48	PM	F
1958	7	4	0	PM	F
1958	7	5	0	PM	F
1958	7	6	0	PM	F
1958	7	7	T	PM	F
1958	7	8	0	PM	F
1958	7	9	0	PM	F
1958	7	10	0.89	PM	F
1958	7	11	5.6	PM	F
1958	7	12	0	PM	F
1958	7	13	0	PM	F
1958	7	14	T	PM	F
1958	7	15	0.82	PM	F
1958	7	16	0	PM	F
1958	7	17	T	PM	F
1958	7	18	0.15	PM	F
1958	7	19	0.1	PM	F
1958	7	20	0.7	PM	F
1958	7	21	0.1	PM	F
1958	7	22	0	PM	F
1958	7	23	0	PM	F
1958	7	24	0	PM	F
1958	7	25	0.11	PM	F
1958	7	26	0	PM	F
1958	7	27	0.1	PM	F
1958	7	28	1.75	PM	F
1958	7	29	T	PM	F
1958	7	30	0.25	PM	F
1958	7	31	0.98	PM	F
1958	8	1	T	PM	F
1958	8	2	0.33	PM	F
1958	8	3	0	PM	F
1958	8	4	0	PM	F
1958	8	5	0	PM	F
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1958	8	7	0.35	PM	F
1958	8	8	0	PM	F
1958	8	9	0	PM	F
1958	8	10	0	PM	F
1958	8	11	1.3	PM	F
1958	8	12	0.1	PM	F
1958	8	13	0	PM	F
1958	8	14	0	PM	F
1958	8	15	0.35	PM	F
1958	8	16	0	PM	F
1958	8	17	T	PM	F
1958	8	18	0	PM	F
1958	8	19	0	PM	F
1958	8	20	0.12	PM	F
1958	8	21	T	PM	F
1958	8	22	0	PM	F
1958	8	23	0	PM	F
1958	8	24	0.06	PM	F
1958	8	25	0	PM	F
1958	8	26	0	PM	F
1958	8	27	0	PM	F
1958	8	28	T	PM	F
1958	8	29	T	PM	F
1958	8	30	0	PM	F
1958	8	31	0.2	PM	F
1958	9	1	0	PM	F
1958	9	2	0	PM	F
1958	9	3	0.37	PM	F
1958	9	4	0	PM	F
1958	9	5	0.62	PM	F
1958	9	6	0	PM	F
1958	9	7	0	PM	F
1958	9	8	0	PM	F
1958	9	9	0	PM	F
1958	9	10	0.32	PM	F
1958	9	11	0	PM	F
1958	9	12	0	PM	F
1958	9	13	0	PM	F
1958	9	14	0	PM	F
1958	9	15	T	PM	F
1958	9	16	0.14	PM	F
1958	9	17	0.65	PM	F
1958	9	18	0	PM	F
1958	9	19	0	PM	F
1958	9	20	0	PM	F
1958	9	21	0.05	PM	F
1958	9	22	0	PM	F
1958	9	23	0	PM	F
1958	9	24	T	PM	F
1958	9	25	0	PM	F
1958	9	26	T	PM	F
1958	9	27	0	PM	F
1958	9	28	0	PM	F
1958	9	29	0	PM	F
1958	9	30	0.6	PM	F
1958	10	1	0	PM	F
1958	10	2	0	PM	F
1958	10	3	0	PM	F
1958	10	4	0	PM	F
1958	10	5	0	PM	F
1958	10	6	0	PM	F
1958	10	7	0	PM	F
1958	10	8	0.25	PM	F
1958	10	9	0.15	PM	F
1958	10	10	0	PM	F
1958	10	11	0	PM	F
1958	10	12	0	PM	F
1958	10	13	0	PM	F
1958	10	14	0	PM	F

1958	10	15	0	PM	F
1958	10	16	0	PM	F
1958	10	17	0	PM	F
1958	10	18	0	PM	F
1958	10	19	0	PM	F
1958	10	20	0	PM	F
1958	10	21	0	PM	F
1958	10	22	0.51	PM	F
1958	10	23	0	PM	F
1958	10	24	0	PM	F
1958	10	25	0	PM	F
1958	10	26	T	PM	F
1958	10	27	0	PM	F
1958	10	28	0	PM	F
1958	10	29	0	PM	F
1958	10	30	0	PM	F
1958	10	31	0	PM	F
1958	11	1	0	PM	F
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1958	11	3	0	PM	F
1958	11	4	0	PM	F
1958	11	5	0	PM	F
1958	11	6	0	PM	F
1958	11	7	0	PM	F
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1958	11	9	T	PM	F
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1958	11	11	0	PM	F
1958	11	12	0	PM	F
1958	11	13	0	PM	F
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1958	11	15	0.72	PM	F
1958	11	16	0.43	PM	F
1958	11	17	0.82	PM	F
1958	11	18	0.17	PM	F
1958	11	19	0	PM	F
1958	11	20	0	PM	F
1958	11	21	0	PM	F
1958	11	22	0	PM	F
1958	11	23	0	PM	F
1958	11	24	0	PM	F
1958	11	25	0.87	PM	F
1958	11	26	0	PM	F
1958	11	27	0	PM	F
1958	11	28	0.25	PM	F
1958	11	29	0	PM	F
1958	11	30	0	PM	F
1958	12	1	0	PM	F
1958	12	2	0	PM	F
1958	12	3	T	PM	F
1958	12	4	0	PM	F
1958	12	5	0	PM	F
1958	12	6	0	PM	F
1958	12	7	0	PM	F
1958	12	8	0.1	PM	F
1958	12	9	0	PM	F
1958	12	10	0	PM	F
1958	12	11	0	PM	F
1958	12	12	T	PM	F
1958	12	13	0	PM	F
1958	12	14	T	PM	F
1958	12	15	0	PM	F
1958	12	16	0	PM	F
1958	12	17	0	PM	F
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1958	12	25	0	PM	F
1958	12	26	0	PM	F
1958	12	27	0	PM	F
1958	12	28	0	PM	F
1958	12	29	T	PM	F
1958	12	30	0	PM	F
1958	12	31	0.2	PM	F
1959	1	1	T	PM	F
1959	1	2	0	PM	F
1959	1	3	0.15	PM	F
1959	1	4	T	PM	F
1959	1	5	0	PM	F
1959	1	6	T	PM	F
1959	1	7	0	PM	F
1959	1	8	0	PM	F
1959	1	9	0	PM	F
1959	1	10	0	PM	F
1959	1	11	0	PM	F
1959	1	12	0	PM	F
1959	1	13	T	PM	F
1959	1	14	0.2	PM	F
1959	1	15	T	PM	F
1959	1	16	0	PM	F
1959	1	17	0	PM	F
1959	1	18	0	PM	F
1959	1	19	T	PM	F
1959	1	20	0.2	PM	F
1959	1	21	0.7	PM	F
1959	1	22	0.1	PM	F
1959	1	23	0	PM	F
1959	1	24	0	PM	F
1959	1	25	T	PM	F
1959	1	26	0	PM	F
1959	1	27	0	PM	F
1959	1	28	0	PM	F
1959	1	29	T	PM	F
1959	1	30	0.15	PM	F
1959	1	31	0	PM	F
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1959	2	3	0.3	PM	F
1959	2	4	0	PM	F
1959	2	5	0	PM	F
1959	2	6	0	PM	F

1959	2	7	0	PM	F
1959	2	8	T	PM	F
1959	2	9	0.2	PM	F
1959	2	10	2.8	PM	F
1959	2	11	0	PM	F
1959	2	12	0	PM	F
1959	2	13	T	PM	F
1959	2	14	T	PM	F
1959	2	15	0	PM	F
1959	2	16	0	PM	F
1959	2	17	T	PM	F
1959	2	18	0.15	PM	F
1959	2	19	0	PM	F
1959	2	20	0	PM	F
1959	2	21	0	PM	F
1959	2	22	0	PM	F
1959	2	23	0.3	PM	F
1959	2	24	0	PM	F
1959	2	25	0	PM	F
1959	2	26	T	PM	F
1959	2	27	0	PM	F
1959	2	28	0	PM	F
1959	3	1	0	PM	F
1959	3	2	T	PM	F
1959	3	3	T	PM	F
1959	3	4	0	PM	F
1959	3	5	0.55	PM	F
1959	3	6	0.65	PM	F
1959	3	7	T	PM	F
1959	3	8	0.4	PM	F
1959	3	9	0.2	PM	F
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1959	3	11	0	PM	F
1959	3	12	T	PM	F
1959	3	13	0	PM	F
1959	3	14	0	PM	F
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1959	3	16	0	PM	F
1959	3	17	T	PM	F
1959	3	18	0	PM	F
1959	3	19	0	PM	F
1959	3	20	0	PM	F
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1959	3	22	0	PM	F
1959	3	23	0	PM	F
1959	3	24	0	PM	F
1959	3	25	0	PM	F
1959	3	26	0.65	PM	F
1959	3	27	T	PM	F
1959	3	28	0	PM	F
1959	3	29	0	PM	F
1959	3	30	T	PM	F
1959	3	31	0.35	PM	F
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1959	4	2	T	PM	F
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1959	4	4	0	PM	F
1959	4	5	0	PM	F
1959	4	6	0	PM	F
1959	4	7	0	PM	F
1959	4	8	1	PM	F
1959	4	9	0.15	PM	F
1959	4	10	T	PM	F
1959	4	11	0	PM	F
1959	4	12	0	PM	F
1959	4	13	0	PM	F
1959	4	14	0	PM	F
1959	4	15	0	PM	F
1959	4	16	0	PM	F
1959	4	17	0.1	PM	F
1959	4	18	0.1	PM	F
1959	4	19	0.85	PM	F
1959	4	20	0.25	PM	F
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1959	4	22	0	PM	F
1959	4	23	0	PM	F
1959	4	24	0	PM	F
1959	4	25	0	PM	F
1959	4	26	0.15	PM	F
1959	4	27	0.9	PM	F
1959	4	28	0.2	PM	F
1959	4	29	0	PM	F
1959	4	30	0	PM	F
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1959	5	2	0	PM	F
1959	5	3	0	PM	F
1959	5	4	0	PM	F
1959	5	5	0	PM	F
1959	5	6	0	PM	F
1959	5	7	0	PM	F
1959	5	8	0	PM	F
1959	5	9	0	PM	F
1959	5	10	0.25	PM	F
1959	5	11	0.4	PM	F
1959	5	12	0	PM	F
1959	5	13	0	PM	F
1959	5	14	0	PM	F
1959	5	15	T	PM	F
1959	5	16	0	PM	F
1959	5	17	T	PM	F
1959	5	18	0	PM	F
1959	5	19	0	PM	F
1959	5	20	0	PM	F
1959	5	21	0.15	PM	F
1959	5	22	0.62	PM	F
1959	5	23	0.15	PM	F
1959	5	24	0	PM	F
1959	5	25	T	PM	F
1959	5	26	0	PM	F
1959	5	27	0.65	PM	F
1959	5	28	0	PM	F
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1959	5	30	0	PM	F
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1959	6	1	0	PM	F

1959	6	2	0	PM	F
1959	6	3	0	PM	F
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1959	6	7	0	PM	F
1959	6	8	0	PM	F
1959	6	9	0	PM	F
1959	6	10	T	PM	F
1959	6	11	0.1	PM	F
1959	6	12	0	PM	F
1959	6	13	0	PM	F
1959	6	14	0	PM	F
1959	6	15	0	PM	F
1959	6	16	0	PM	F
1959	6	17	0	PM	F
1959	6	18	T	PM	F
1959	6	19	0	PM	F
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1959	6	21	0	PM	F
1959	6	22	0	PM	F
1959	6	23	0	PM	F
1959	6	24	0	PM	F
1959	6	25	0	PM	F
1959	6	26	T	PM	F
1959	6	27	0	PM	F
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1959	7	2	0	PM	F
1959	7	3	0	PM	F
1959	7	4	T	PM	F
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1959	7	6	0	PM	F
1959	7	7	0	PM	F
1959	7	8	0	PM	F
1959	7	9	0	PM	F
1959	7	10	0	PM	F
1959	7	11	0.08	PM	F
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1959	7	13	0	PM	F
1959	7	14	0	PM	F
1959	7	15	0	PM	F
1959	7	16	0	PM	F
1959	7	17	0.11	PM	F
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1959	7	22	0	PM	F
1959	7	23	1.7	PM	F
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1959	7	26	0	PM	F
1959	7	27	0.47	PM	F
1959	7	28	0	PM	F
1959	7	29	0	PM	F
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1959	7	31	T	PM	F
1959	8	1	0	PM	F
1959	8	2	0	PM	F
1959	8	3	T	PM	F
1959	8	4	0.03	PM	F
1959	8	5	0	PM	F
1959	8	6	0.5	PM	F
1959	8	7	0	PM	F
1959	8	8	0	PM	F
1959	8	9	0	PM	F
1959	8	10	0	PM	F
1959	8	11	0	PM	F
1959	8	12	0	PM	F
1959	8	13	0	PM	F
1959	8	14	0	PM	F
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1959	8	22	0	PM	F
1959	8	23	0	PM	F
1959	8	24	0	PM	F
1959	8	25	0	PM	F
1959	8	26	0	PM	F
1959	8	27	0.1	PM	F
1959	8	28	0	PM	F
1959	8	29	0.4	PM	F
1959	8	30	0.1	PM	F
1959	8	31	0	PM	F
1959	9	1	0.58	PM	F
1959	9	2	T	PM	F
1959	9	3	0	PM	F
1959	9	4	0	PM	F
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1959	9	7	0	PM	F
1959	9	8	0	PM	F
1959	9	9	0	PM	F
1959	9	10	0	PM	F
1959	9	11	0	PM	F
1959	9	12	0	PM	F
1959	9	13	0	PM	F
1959	9	14	0	PM	F
1959	9	15	0	PM	F
1959	9	16	T	PM	F
1959	9	17	0.1	PM	F
1959	9	18	T	PM	F
1959	9	19	0	PM	F
1959	9	20	0	PM	F
1959	9	21	T	PM	F
1959	9	22	0	PM	F
1959	9	23	T	PM	F
1959	9	24	T	PM	F

1959	9	25	T		PM	F
1959	9	26		2.3	PM	F
1959	9	27		1.52	PM	F
1959	9	28	T		PM	F
1959	9	29		0.12	PM	F
1959	9	30		0	PM	F
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1959	10	2		0	PM	F
1959	10	3		0.1	PM	F
1959	10	4		0.4	PM	F
1959	10	5		0.72	PM	F
1959	10	6		0.25	PM	F
1959	10	7	T		PM	F
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1959	10	9		0	PM	F
1959	10	10		0.53	PM	F
1959	10	11		0.89	PM	F
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1959	10	14		0	PM	F
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1959	10	17		0	PM	F
1959	10	18		0	PM	F
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1959	10	21		0	PM	F
1959	10	22		0	PM	F
1959	10	23		0.12	PM	F
1959	10	24		0.1	PM	F
1959	10	25		0.18	PM	F
1959	10	26	T		PM	F
1959	10	27		0.08	PM	F
1959	10	28		0	PM	F
1959	10	29		0	PM	F
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1959	10	31	T		PM	F
1959	11	1		0	PM	F
1959	11	2		0	PM	F
1959	11	3		0.08	PM	F
1959	11	4		0.38	PM	F
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1959	11	6	T		PM	F
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1959	11	11		0	PM	F
1959	11	12	T		PM	F
1959	11	13		1.12	PM	F
1959	11	14		0.33	PM	F
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1959	11	18		0	PM	F
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1959	11	26		0.1	PM	F
1959	11	27		0	PM	F
1959	11	28		0	PM	F
1959	11	29		0	PM	F
1959	11	30		0	PM	F
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1959	12	2		0	PM	F
1959	12	3		0	PM	F
1959	12	4		0	PM	F
1959	12	5		0.15	PM	F
1959	12	6	T		PM	F
1959	12	7		0	PM	F
1959	12	8		0	PM	F
1959	12	9		0	PM	F
1959	12	10	T		PM	F
1959	12	11		0.15	PM	F
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1959	12	14		0	PM	F
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1959	12	17		0	PM	F
1959	12	18		0	PM	F
1959	12	19		0	PM	F
1959	12	20		0.08	PM	F
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1959	12	22		0	PM	F
1959	12	23		0.2	PM	F
1959	12	24	T		PM	F
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1959	12	26		0	PM	F
1959	12	27		0.56	PM	F
1959	12	28	T		PM	F
1959	12	29	T		PM	F
1959	12	30	T		PM	F
1959	12	31	T		PM	F
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1960	1	2	T		PM	F
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1960	1	6		0	PM	F
1960	1	7		0	PM	F
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1960	1	9	T		PM	F
1960	1	10	T		PM	F
1960	1	11	T		PM	F
1960	1	12		0.75	PM	F
1960	1	13	T		PM	F
1960	1	14		0.05	PM	F
1960	1	15		0.24	PM	F
1960	1	16		0	PM	F
1960	1	17	T		PM	F

1960	1	18	0.25	PM	F
1960	1	19	T	PM	F
1960	1	20	0	PM	F
1960	1	21	0	PM	F
1960	1	22	T	PM	F
1960	1	23	0	PM	F
1960	1	24	0	PM	F
1960	1	25	0	PM	F
1960	1	26	T	PM	F
1960	1	27	0.25	PM	F
1960	1	28	0	PM	F
1960	1	29	0.03	PM	F
1960	1	30	0	PM	F
1960	1	31	0	PM	F
1960	2	1	0	PM	F
1960	2	2	0	PM	F
1960	2	3	0	PM	F
1960	2	4	0.3	PM	F
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1960	2	6	0.11	PM	F
1960	2	7	0	PM	F
1960	2	8	0.08	PM	F
1960	2	9	0.1	PM	F
1960	2	10	0.4	PM	F
1960	2	11	T	PM	F
1960	2	12	0	PM	F
1960	2	13	0	PM	F
1960	2	14	T	PM	F
1960	2	15	0	PM	F
1960	2	16	0	PM	F
1960	2	17	0	PM	F
1960	2	18	0	PM	F
1960	2	19	0	PM	F
1960	2	20	T	PM	F
1960	2	21	0.35	PM	F
1960	2	22	0	PM	F
1960	2	23	0	PM	F
1960	2	24	0.15	PM	F
1960	2	25	0.3	PM	F
1960	2	26	0	PM	F
1960	2	27	0	PM	F
1960	2	28	0.07	PM	F
1960	2	29	0	PM	F
1960	3	1	0	PM	F
1960	3	2	0	PM	F
1960	3	3	0.4	PM	F
1960	3	4	T	PM	F
1960	3	5	0	PM	F
1960	3	6	0	PM	F
1960	3	7	0.06	PM	F
1960	3	8	0	PM	F
1960	3	9	0.4	PM	F
1960	3	10	0	PM	F
1960	3	11	0.25	PM	F
1960	3	12	T	PM	F
1960	3	13	0	PM	F
1960	3	14	0	PM	F
1960	3	15	0	PM	F
1960	3	16	0.35	PM	F
1960	3	17	0.03	PM	F
1960	3	18	0	PM	F
1960	3	19	0.03	PM	F
1960	3	20	T	PM	F
1960	3	21	0.03	PM	F
1960	3	22	0	PM	F
1960	3	23	0	PM	F
1960	3	24	0	PM	F
1960	3	25	T	PM	F
1960	3	26	T	PM	F
1960	3	27	0	PM	F
1960	3	28	0	PM	F
1960	3	29	0	PM	F
1960	3	30	0.75	PM	F
1960	3	31	0	PM	F
1960	4	1	T	PM	F
1960	4	2	0	PM	F
1960	4	3	0	PM	F
1960	4	4	0.1	PM	F
1960	4	5	0	PM	F
1960	4	6	0	PM	F
1960	4	7	0	PM	F
1960	4	8	0	PM	F
1960	4	9	0	PM	F
1960	4	10	T	PM	F
1960	4	11	0.32	PM	F
1960	4	12	0	PM	F
1960	4	13	0	PM	F
1960	4	14	0.06	PM	F
1960	4	15	T	PM	F
1960	4	16	0.67	PM	F
1960	4	17	0.55	PM	F
1960	4	18	T	PM	F
1960	4	19	0	PM	F
1960	4	20	0	PM	F
1960	4	21	0.96	PM	F
1960	4	22	0	PM	F
1960	4	23	0	PM	F
1960	4	24	0	PM	F
1960	4	25	0.1	PM	F
1960	4	26	T	PM	F
1960	4	27	0	PM	F
1960	4	28	0	PM	F
1960	4	29	0.56	PM	F
1960	4	30	0.52	PM	F
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1960	5	2	0	PM	F
1960	5	3	0	PM	F
1960	5	4	0	PM	F
1960	5	5	0.22	PM	F
1960	5	6	0.42	PM	F
1960	5	7	T	PM	F
1960	5	8	0.1	PM	F
1960	5	9	0.05	PM	F
1960	5	10	T	PM	F
1960	5	11	0	PM	F

1960	5	12		0 PM	F
1960	5	13		0 PM	F
1960	5	14		0 PM	F
1960	5	15		0 PM	F
1960	5	16		0.35 PM	F
1960	5	17		0.5 PM	F
1960	5	18		0 PM	F
1960	5	19		0.1 PM	F
1960	5	20		0.05 PM	F
1960	5	21		0.15 PM	F
1960	5	22		0 PM	F
1960	5	23		0 PM	F
1960	5	24		0 PM	F
1960	5	25		1.03 PM	F
1960	5	26		0.52 PM	F
1960	5	27		0.1 PM	F
1960	5	28		0.14 PM	F
1960	5	29		0.32 PM	F
1960	5	30	T	PM	F
1960	5	31		0 PM	F
1960	6	1		0 PM	F
1960	6	2	T	PM	F
1960	6	3		0 PM	F
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1960	6	7		0 PM	F
1960	6	8		0 PM	F
1960	6	9		0 PM	F
1960	6	10		0 PM	F
1960	6	11		0.1 PM	F
1960	6	12		0.26 PM	F
1960	6	13		0.28 PM	F
1960	6	14		0.42 PM	F
1960	6	15		0 PM	F
1960	6	16		0.75 PM	F
1960	6	17		0 PM	F
1960	6	18		0 PM	F
1960	6	19		0.1 PM	F
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1960	6	21		1 PM	F
1960	6	22		0.18 PM	F
1960	6	23		1.98 PM	F
1960	6	24		0.1 PM	F
1960	6	25		0 PM	F
1960	6	26		0 PM	F
1960	6	27		0.1 PM	F
1960	6	28	T	PM	F
1960	6	29		0.15 PM	F
1960	6	30		0.3 PM	F
1960	7	1		0.38 PM	F
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1960	7	3		0 PM	F
1960	7	4		0 PM	F
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1960	7	22		0 PM	F
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1960	7	27		0.1 PM	F
1960	7	28		0 PM	F
1960	7	29		0 PM	F
1960	7	30		0 PM	F
1960	7	31		0 PM	F
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1960	8	2		0 PM	F
1960	8	3		0 PM	F
1960	8	4		0.42 PM	F
1960	8	5		0 PM	F
1960	8	6		0.32 PM	F
1960	8	7		0 PM	F
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1960	8	9		0 PM	F
1960	8	10		0 PM	F
1960	8	11		0 PM	F
1960	8	12		0 PM	F
1960	8	13		0 PM	F
1960	8	14		0.32 PM	F
1960	8	15		0 PM	F
1960	8	16		0 PM	F
1960	8	17		0 PM	F
1960	8	18	T	PM	F
1960	8	19		0.9 PM	F
1960	8	20		0.1 PM	F
1960	8	21		0 PM	F
1960	8	22		0 PM	F
1960	8	23		0 PM	F
1960	8	24		0 PM	F
1960	8	25		0 PM	F
1960	8	26		0 PM	F
1960	8	27		0 PM	F
1960	8	28		0 PM	F
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1960	8	31		0 PM	F
1960	9	1		0 PM	F
1960	9	2		0 PM	F
1960	9	3		0 PM	F

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1960	9	6	0	PM	F
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1960	9	11	0	PM	F
1960	9	12	0	PM	F
1960	9	13	0	PM	F
1960	9	14	0	PM	F
1960	9	15	0.1	PM	F
1960	9	16	0	PM	F
1960	9	17	1.12	PM	F
1960	9	18	0	PM	F
1960	9	19	0.45	PM	F
1960	9	20	T	PM	F
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1960	9	22	0	PM	F
1960	9	23	0	PM	F
1960	9	24	0	PM	F
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1960	9	28	0	PM	F
1960	9	29	0	PM	F
1960	9	30	T	PM	F
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1960	10	2	0	PM	F
1960	10	3	T	PM	F
1960	10	4	0	PM	F
1960	10	5	T	PM	F
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1960	10	7	0	PM	F
1960	10	8	0	PM	F
1960	10	9	0	PM	F
1960	10	10	0	PM	F
1960	10	11	0	PM	F
1960	10	12	0	PM	F
1960	10	13	0	PM	F
1960	10	14	0.4	PM	F
1960	10	15	T	PM	F
1960	10	16	0	PM	F
1960	10	17	0	PM	F
1960	10	18	0	PM	F
1960	10	19	T	PM	F
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1960	10	22	0	PM	F
1960	10	23	0	PM	F
1960	10	24	0	PM	F
1960	10	25	T	PM	F
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1960	10	27	0	PM	F
1960	10	28	0	PM	F
1960	10	29	0	PM	F
1960	10	30	0	PM	F
1960	10	31	0.9	PM	F
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1960	11	4	0	PM	F
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1960	11	12	0	PM	F
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1960	11	20	0	PM	F
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1960	11	29	T	PM	F
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1962	7	26		0 PM	F
1962	7	27		0 PM	F
1962	7	28		0.04 PM	F
1962	7	29		0 PM	F
1962	7	30		0 PM	F
1962	7	31		0 PM	F
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1962	8	2		0 PM	F
1962	8	3		0 PM	F
1962	8	4		0 PM	F
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1962	8	6		0.44 PM	F
1962	8	7		0 PM	F
1962	8	8		0 PM	F
1962	8	9		0.25 PM	F
1962	8	10		0 PM	F
1962	8	11		0 PM	F
1962	8	12		0 PM	F
1962	8	13		0 PM	F
1962	8	14		0 PM	F
1962	8	15		0 PM	F
1962	8	16		0 PM	F
1962	8	17		0 PM	F
1962	8	18		0 PM	F
1962	8	19	T	PM	F
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1962	8	24	T	PM	F
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1962	8	31	T	PM	F
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1962	9	2		0 PM	F
1962	9	3	T	PM	F
1962	9	4	T	PM	F
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1962	9	21		0 PM	F
1962	9	22		0 PM	F
1962	9	23		0 PM	F
1962	9	24		0.62 PM	F
1962	9	25		0.03 PM	F
1962	9	26		0 PM	F
1962	9	27		0.03 PM	F
1962	9	28		0 PM	F
1962	9	29		0 PM	F
1962	9	30		0 PM	F
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1962	10	11		0 PM	F
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1962	10	21		0 PM	F
1962	10	22		0 PM	F
1962	10	23		0 PM	F
1962	10	24		0 PM	F
1962	10	25		0.03 PM	F
1962	10	26		0 PM	F
1962	10	27		0 PM	F
1962	10	28		0 PM	F
1962	10	29		0 PM	F
1962	10	30		0 PM	F
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1962	11	15	T	PM	F
1962	11	16		0.48 PM	F
1962	11	17	T	PM	F

1962	11	18	0	PM	F
1962	11	19	T	PM	F
1962	11	20	0	PM	F
1962	11	21	0	PM	F
1962	11	22	0	PM	F
1962	11	23	0	PM	F
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1962	11	29	0	PM	F
1962	11	30	0	PM	F
1962	12	1	0	PM	F
1962	12	2	0	PM	F
1962	12	3	0	PM	F
1962	12	4	0.04	PM	F
1962	12	5	T	PM	F
1962	12	6	0	PM	F
1962	12	7	0	PM	F
1962	12	8	0	PM	F
1962	12	9	0.01	PM	F
1962	12	10	0.02	PM	F
1962	12	11	T	PM	F
1962	12	12	0	PM	F
1962	12	13	0	PM	F
1962	12	14	0	PM	F
1962	12	15	0	PM	F
1962	12	16	0	PM	F
1962	12	17	0	PM	F
1962	12	18	0	PM	F
1962	12	19	0	PM	F
1962	12	20	0.19	PM	F
1962	12	21	T	PM	F
1962	12	22	0	PM	F
1962	12	23	0	PM	F
1962	12	24	0	PM	F
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1962	12	26	0	PM	F
1962	12	27	0	PM	F
1962	12	28	0	PM	F
1962	12	29	0	PM	F
1962	12	30	0	PM	F
1962	12	31	0	PM	F
1963	1	1	0	PM	F
1963	1	2	0.02	PM	F
1963	1	3	0	PM	F
1963	1	4	0	PM	F
1963	1	5	0	PM	F
1963	1	6	T	PM	F
1963	1	7	0.05	PM	F
1963	1	8	0	PM	F
1963	1	9	0	PM	F
1963	1	10	0	PM	F
1963	1	11	T	PM	F
1963	1	12	0.02	PM	F
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1963	1	15	0	PM	F
1963	1	16	0	PM	F
1963	1	17	0	PM	F
1963	1	18	0	PM	F
1963	1	19	0.25	PM	F
1963	1	20	0	PM	F
1963	1	21	0	PM	F
1963	1	22	0.15	PM	F
1963	1	23	0.06	PM	F
1963	1	24	T	PM	F
1963	1	25	T	PM	F
1963	1	26	0	PM	F
1963	1	27	0.03	PM	F
1963	1	28	0	PM	F
1963	1	29	0	PM	F
1963	1	30	0	PM	F
1963	1	31	0	PM	F
1963	2	1	0.02	PM	F
1963	2	2	0	PM	F
1963	2	3	0	PM	F
1963	2	4	0	PM	F
1963	2	5	0	PM	F
1963	2	6	0	PM	F
1963	2	7	0	PM	F
1963	2	8	0	PM	F
1963	2	9	0.02	PM	F
1963	2	10	0.03	PM	F
1963	2	11	T	PM	F
1963	2	12	T	PM	F
1963	2	13	0.01	PM	F
1963	2	14	0	PM	F
1963	2	15	0	PM	F
1963	2	16	0	PM	F
1963	2	17	0	PM	F
1963	2	18	0	PM	F
1963	2	19	0	PM	F
1963	2	20	0.02	PM	F
1963	2	21	0	PM	F
1963	2	22	0	PM	F
1963	2	23	0.4	PM	F
1963	2	24	0.09	PM	F
1963	2	25	0.16	PM	F
1963	2	26	0	PM	F
1963	2	27	T	PM	F
1963	2	28	0.01	PM	F
1963	3	1	0	PM	F
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1963	3	7	0	PM	F
1963	3	8	0.01	PM	F
1963	3	9	0.16	PM	F
1963	3	10	0	PM	F
1963	3	11	0.11	PM	F
1963	3	12	0	PM	F

1963	3	13	0	PM	F
1963	3	14	0	PM	F
1963	3	15	0	PM	F
1963	3	16	0.34	PM	F
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1963	3	21	0	PM	F
1963	3	22	0	PM	F
1963	3	23	0	PM	F
1963	3	24	0	PM	F
1963	3	25	0.57	PM	F
1963	3	26	0.6	PM	F
1963	3	27	0	PM	F
1963	3	28	0	PM	F
1963	3	29	0	PM	F
1963	3	30	0.32	PM	F
1963	3	31	1.04	PM	F
1963	4	1	T	PM	F
1963	4	2	0	PM	F
1963	4	3	T	PM	F
1963	4	4	0	PM	F
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1963	4	6	0	PM	F
1963	4	7	0	PM	F
1963	4	8	T	PM	F
1963	4	9	0	PM	F
1963	4	10	0	PM	F
1963	4	11	0	PM	F
1963	4	12	T	PM	F
1963	4	13	0	PM	F
1963	4	14	0	PM	F
1963	4	15	0	PM	F
1963	4	16	0.15	PM	F
1963	4	17	0.16	PM	F
1963	4	18	0.1	PM	F
1963	4	19	0.2	PM	F
1963	4	20	T	PM	F
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1963	4	22	0.01	PM	F
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1963	4	24	0	PM	F
1963	4	25	0	PM	F
1963	4	26	0	PM	F
1963	4	27	0	PM	F
1963	4	28	0	PM	F
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1963	5	2	0	PM	F
1963	5	3	0	PM	F
1963	5	4	0	PM	F
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1963	5	7	0	PM	F
1963	5	8	0	PM	F
1963	5	9	0	PM	F
1963	5	10	0	PM	F
1963	5	11	0	PM	F
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1963	5	14	0	PM	F
1963	5	15	0.18	PM	F
1963	5	16	0	PM	F
1963	5	17	0.1	PM	F
1963	5	18	0	PM	F
1963	5	19	0.12	PM	F
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1963	5	22	0	PM	F
1963	5	23	0	PM	F
1963	5	24	0	PM	F
1963	5	25	0	PM	F
1963	5	26	0.27	PM	F
1963	5	27	0.11	PM	F
1963	5	28	0.1	PM	F
1963	5	29	0	PM	F
1963	5	30	0	PM	F
1963	5	31	0	PM	F
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1963	6	3	0	PM	F
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1963	6	7	0	PM	F
1963	6	8	0	PM	F
1963	6	9	0	PM	F
1963	6	10	T	PM	F
1963	6	11	0.03	PM	F
1963	6	12	0.01	PM	F
1963	6	13	0.07	PM	F
1963	6	14	0	PM	F
1963	6	15	0	PM	F
1963	6	16	0	PM	F
1963	6	17	0	PM	F
1963	6	18	0	PM	F
1963	6	19	0	PM	F
1963	6	20	0.14	PM	F
1963	6	21	0	PM	F
1963	6	22	0	PM	F
1963	6	23	0	PM	F
1963	6	24	0	PM	F
1963	6	25	0	PM	F
1963	6	26	0	PM	F
1963	6	27	0	PM	F
1963	6	28	0	PM	F
1963	6	29	0	PM	F
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1963	7	1	0.48	PM	F
1963	7	2	0.34	PM	F
1963	7	3	0	PM	F
1963	7	4	T	PM	F
1963	7	5	T	PM	F

1963	7	6		1.84 PM	F
1963	7	7		0.01 PM	F
1963	7	8		0 PM	F
1963	7	9		0 PM	F
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1963	7	16		0 PM	F
1963	7	17		0.01 PM	F
1963	7	18		0 PM	F
1963	7	19		0 PM	F
1963	7	20		0.16 PM	F
1963	7	21		0 PM	F
1963	7	22		0 PM	F
1963	7	23		0 PM	F
1963	7	24		0 PM	F
1963	7	25		0 PM	F
1963	7	26		0 PM	F
1963	7	27	T	PM	F
1963	7	28		0.09 PM	F
1963	7	29		0 PM	F
1963	7	30		0 PM	F
1963	7	31		0.43 PM	F
1963	8	1		0 PM	F
1963	8	2		0 PM	F
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1963	8	11		0 PM	F
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1963	8	15		0 PM	F
1963	8	16		0 PM	F
1963	8	17		0 PM	F
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1963	8	20		0 PM	F
1963	8	21		0 PM	F
1963	8	22		0 PM	F
1963	8	23		0 PM	F
1963	8	24		0.14 PM	F
1963	8	25		0 PM	F
1963	8	26		0 PM	F
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1963	8	29		0 PM	F
1963	8	30		0 PM	F
1963	8	31		0 PM	F
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1963	9	2		0.22 PM	F
1963	9	3		0.26 PM	F
1963	9	4		0 PM	F
1963	9	5		0 PM	F
1963	9	6		0 PM	F
1963	9	7		0 PM	F
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1963	9	12		0 PM	F
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1963	9	16		0 PM	F
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1963	9	18		0 PM	F
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1963	9	23		0 PM	F
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1963	9	25		0 PM	F
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1963	9	27		0 PM	F
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1963	9	29		0.05 PM	F
1963	9	30		0 PM	F
1963	10	1		0 PM	F
1963	10	2		0 PM	F
1963	10	3		0 PM	F
1963	10	4		0 PM	F
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1963	10	31		0 PM	F
1963	11	1		0.07 PM	F
1963	11	2		0 PM	F
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1963	11	5		0.56 PM	F
1963	11	6		0 PM	F
1963	11	7		0 PM	F
1963	11	8		0 PM	F
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1963	11	16		0 PM	F
1963	11	17		0 PM	F
1963	11	18		0.02 PM	F
1963	11	19		0 PM	F
1963	11	20		0.12 PM	F
1963	11	21		0 PM	F
1963	11	22		0.63 PM	F
1963	11	23		0.68 PM	F
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1963	11	25		0 PM	F
1963	11	26		0 PM	F
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1963	11	28		0 PM	F
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1963	11	30		0.08 PM	F
1963	12	1		0 PM	F
1963	12	2		0 PM	F
1963	12	3		0.01 PM	F
1963	12	4		0 PM	F
1963	12	5		0.07 PM	F
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1963	12	10		0 PM	F
1963	12	11		0.05 PM	F
1963	12	12		0.06 PM	F
1963	12	13		0 PM	F
1963	12	14		0 PM	F
1963	12	15		0 PM	F
1963	12	16		0 PM	F
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1963	12	20		0 PM	F
1963	12	21		0 PM	F
1963	12	22		0 PM	F
1963	12	23		0 PM	F
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1964	1	8		0 PM	F
1964	1	9		0 PM	F
1964	1	10		0 PM	F
1964	1	11	T	PM	F
1964	1	12		0.4 PM	F
1964	1	13		0.31 PM	F
1964	1	14		0 PM	F
1964	1	15		0 PM	F
1964	1	16	T	PM	F
1964	1	17		0 PM	F
1964	1	18		0 PM	F
1964	1	19	T	PM	F
1964	1	20		0.1 PM	F
1964	1	21		0 PM	F
1964	1	22		0 PM	F
1964	1	23		0 PM	F
1964	1	24		0.04 PM	F
1964	1	25		0.01 PM	F
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1964	2	3		0 PM	F
1964	2	4		0 PM	F
1964	2	5		0 PM	F
1964	2	6		0.02 PM	F
1964	2	7	T	PM	F
1964	2	8		0.01 PM	F
1964	2	9	T	PM	F
1964	2	10		0.04 PM	F
1964	2	11		0 PM	F
1964	2	12		0.08 PM	F
1964	2	13		0.48 PM	F
1964	2	14		0 PM	F
1964	2	15		0.06 PM	F
1964	2	16		0.22 PM	F
1964	2	17		0 PM	F
1964	2	18		0 PM	F
1964	2	19		0.12 PM	F
1964	2	20		0.01 PM	F

1964	2	21	T		PM	F
1964	2	22		0	PM	F
1964	2	23		0	PM	F
1964	2	24		0	PM	F
1964	2	25		0	PM	F
1964	2	26		0.24	PM	F
1964	2	27		0	PM	F
1964	2	28		0	PM	F
1964	2	29		0	PM	F
1964	3	1		0	PM	F
1964	3	2		0	PM	F
1964	3	3		0	PM	F
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1964	3	5		0.1	PM	F
1964	3	6		0	PM	F
1964	3	7		0	PM	F
1964	3	8		0.09	PM	F
1964	3	9		0.23	PM	F
1964	3	10		0.18	PM	F
1964	3	11		0.2	PM	F
1964	3	12		0.18	PM	F
1964	3	13		0	PM	F
1964	3	14		0.15	PM	F
1964	3	15		0	PM	F
1964	3	16		0	PM	F
1964	3	17		0	PM	F
1964	3	18		0	PM	F
1964	3	19		0	PM	F
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1964	3	21		0.2	PM	F
1964	3	22		0	PM	F
1964	3	23		0	PM	F
1964	3	24		0	PM	F
1964	3	25		1.19	PM	F
1964	3	26	T		PM	F
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1964	3	28		0.37	PM	F
1964	3	29		0.02	PM	F
1964	3	30		0.02	PM	F
1964	3	31		0	PM	F
1964	4	1		0	PM	F
1964	4	2		0.65	PM	F
1964	4	3		0.14	PM	F
1964	4	4		0	PM	F
1964	4	5		0.88	PM	F
1964	4	6		0.52	PM	F
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1964	4	9		0	PM	F
1964	4	10		0	PM	F
1964	4	11		0	PM	F
1964	4	12		0.27	PM	F
1964	4	13		0	PM	F
1964	4	14		0	PM	F
1964	4	15		0	PM	F
1964	4	16		0	PM	F
1964	4	17		0	PM	F
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1964	4	23		0.51	PM	F
1964	4	24		0	PM	F
1964	4	25		0	PM	F
1964	4	26		0.23	PM	F
1964	4	27		0.82	PM	F
1964	4	28		0.05	PM	F
1964	4	29		0.02	PM	F
1964	4	30		0	PM	F
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1964	5	3		0	PM	F
1964	5	4		0	PM	F
1964	5	5		0	PM	F
1964	5	6		0.09	PM	F
1964	5	7		0	PM	F
1964	5	8		0.02	PM	F
1964	5	9		0.13	PM	F
1964	5	10		0	PM	F
1964	5	11		0	PM	F
1964	5	12		0.56	PM	F
1964	5	13		0.08	PM	F
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1964	5	18		0	PM	F
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1964	5	24		0	PM	F
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1964	5	26	T		PM	F
1964	5	27	T		PM	F
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1964	5	30		0	PM	F
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1964	6	2		0.27	PM	F
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1964	6	4		0	PM	F
1964	6	5		1.01	PM	F
1964	6	6		0	PM	F
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1964	6	12		1.03	PM	F
1964	6	13		0	PM	F
1964	6	14	T		PM	F

1964	6	15	0.14	PM	F
1964	6	16	0	PM	F
1964	6	17	0	PM	F
1964	6	18	0.09	PM	F
1964	6	19	0	PM	F
1964	6	20	2.22	PM	F
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1964	6	22	0	PM	F
1964	6	23	0	PM	F
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1964	6	29	0	PM	F
1964	6	30	0	PM	F
1964	7	1	0	PM	F
1964	7	2	0	PM	F
1964	7	3	0.05	PM	F
1964	7	4	0	PM	F
1964	7	5	0	PM	F
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1964	7	7	0.1	PM	F
1964	7	8	0.27	PM	F
1964	7	9	0	PM	F
1964	7	10	0	PM	F
1964	7	11	T	PM	F
1964	7	12	0.32	PM	F
1964	7	13	0	PM	F
1964	7	14	0.04	PM	F
1964	7	15	0.57	PM	F
1964	7	16	0	PM	F
1964	7	17	0	PM	F
1964	7	18	0.31	PM	F
1964	7	19	0	PM	F
1964	7	20	0	PM	F
1964	7	21	T	PM	F
1964	7	22	0	PM	F
1964	7	23	0	PM	F
1964	7	24	0	PM	F
1964	7	25	0.1	PM	F
1964	7	26	0	PM	F
1964	7	27	0	PM	F
1964	7	28	0	PM	F
1964	7	29	0	PM	F
1964	7	30	0	PM	F
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1964	8	6	0	PM	F
1964	8	7	0	PM	F
1964	8	8	0	PM	F
1964	8	9	0	PM	F
1964	8	10	0	PM	F
1964	8	11	0.03	PM	F
1964	8	12	0	PM	F
1964	8	13	0	PM	F
1964	8	14	0	PM	F
1964	8	15	0	PM	F
1964	8	16	0	PM	F
1964	8	17	0	PM	F
1964	8	18	0	PM	F
1964	8	19	0.03	PM	F
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1964	8	21	0.97	PM	F
1964	8	22	0	PM	F
1964	8	23	0	PM	F
1964	8	24	0	PM	F
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1964	8	26	0	PM	F
1964	8	27	0	PM	F
1964	8	28	0	PM	F
1964	8	29	0	PM	F
1964	8	30	0.5	PM	F
1964	8	31	0	PM	F
1964	9	1	0	PM	F
1964	9	2	0	PM	F
1964	9	3	0	PM	F
1964	9	4	0	PM	F
1964	9	5	0	PM	F
1964	9	6	0	PM	F
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1964	9	12	0	PM	F
1964	9	13	0	PM	F
1964	9	14	0	PM	F
1964	9	15	0	PM	F
1964	9	16	0.09	PM	F
1964	9	17	0	PM	F
1964	9	18	0.78	PM	F
1964	9	19	0	PM	F
1964	9	20	0.12	PM	F
1964	9	21	0.07	PM	F
1964	9	22	1.25	PM	F
1964	9	23	0.17	PM	F
1964	9	24	0	PM	F
1964	9	25	0	PM	F
1964	9	26	0.34	PM	F
1964	9	27	0.7	PM	F
1964	9	28	0	PM	F
1964	9	29	0	PM	F
1964	9	30	0	PM	F
1964	10	1	0	PM	F
1964	10	2	0	PM	F
1964	10	3	0	PM	F
1964	10	4	0	PM	F
1964	10	5	0	PM	F
1964	10	6	0	PM	F
1964	10	7	0	PM	F

1964	10	8	0.05	PM	F
1964	10	9	0	PM	F
1964	10	10	0	PM	F
1964	10	11	0	PM	F
1964	10	12	0	PM	F
1964	10	13	0	PM	F
1964	10	14	0	PM	F
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1964	10	22	0	PM	F
1964	10	23	0	PM	F
1964	10	24	0	PM	F
1964	10	25	0	PM	F
1964	10	26	0	PM	F
1964	10	27	0.07	PM	F
1964	10	28	0	PM	F
1964	10	29	0	PM	F
1964	10	30	0	PM	F
1964	10	31	0	PM	F
1964	11	1	0	PM	F
1964	11	2	0.05	PM	F
1964	11	3	0	PM	F
1964	11	4	0	PM	F
1964	11	5	0	PM	F
1964	11	6	0	PM	F
1964	11	7	0	PM	F
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1964	11	11	0	PM	F
1964	11	12	0	PM	F
1964	11	13	0	PM	F
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1964	11	15	0.75	PM	F
1964	11	16	1	PM	F
1964	11	17	0	PM	F
1964	11	18	0	PM	F
1964	11	19	0.22	PM	F
1964	11	20	0	PM	F
1964	11	21	0	PM	F
1964	11	22	0	PM	F
1964	11	23	0	PM	F
1964	11	24	0	PM	F
1964	11	25	0	PM	F
1964	11	26	0	PM	F
1964	11	27	0	PM	F
1964	11	28	1.91	PM	F
1964	11	29	0.13	PM	F
1964	11	30	0	PM	F
1964	12	1	0	PM	F
1964	12	2	0.08	PM	F
1964	12	3	0.02	PM	F
1964	12	4	0.5	PM	F
1964	12	5	0	PM	F
1964	12	6	0	PM	F
1964	12	7	0	PM	F
1964	12	8	0.03	PM	F
1964	12	9	0	PM	F
1964	12	10	0.01	PM	F
1964	12	11	0.29	PM	F
1964	12	12	0	PM	F
1964	12	13	0.05	PM	F
1964	12	14	0	PM	F
1964	12	15	0	PM	F
1964	12	16	0	PM	F
1964	12	17	0	PM	F
1964	12	18	0	PM	F
1964	12	19	0	PM	F
1964	12	20	0	PM	F
1964	12	21	0	PM	F
1964	12	22	0	PM	F
1964	12	23	0	PM	F
1964	12	24	0.08	PM	F
1964	12	25	0.21	PM	F
1964	12	26	0	PM	F
1964	12	27	0	PM	F
1964	12	28	0	PM	F
1964	12	29	0	PM	F
1964	12	30	0	PM	F
1964	12	31	0.14	PM	F
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1965	1	2	0	PM	F
1965	1	3	0	PM	F
1965	1	4	0	PM	F
1965	1	5	0	PM	F
1965	1	6	0	PM	F
1965	1	7	0	PM	F
1965	1	8	0.4	PM	F
1965	1	9	0.11	PM	F
1965	1	10	0	PM	F
1965	1	11	0	PM	F
1965	1	12	0	PM	F
1965	1	13	T	PM	F
1965	1	14	0	PM	F
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1965	1	20	0	PM	F
1965	1	21	0	PM	F
1965	1	22	1.12	PM	F
1965	1	23	0.71	PM	F
1965	1	24	0.03	PM	F
1965	1	25	0	PM	F
1965	1	26	0.05	PM	F
1965	1	27	0	PM	F
1965	1	28	0.02	PM	F
1965	1	29	0	PM	F
1965	1	30	0.02	PM	F

1965	1	31	0	PM	F
1965	2	1	0.1	PM	F
1965	2	2	0	PM	F
1965	2	3	0	PM	F
1965	2	4	0	PM	F
1965	2	5	0	PM	F
1965	2	6	0	PM	F
1965	2	7	T	PM	F
1965	2	8	0.05	PM	F
1965	2	9	0.48	PM	F
1965	2	10	0.12	PM	F
1965	2	11	0.01	PM	F
1965	2	12	0.03	PM	F
1965	2	13	0	PM	F
1965	2	14	0	PM	F
1965	2	15	0	PM	F
1965	2	16	0	PM	F
1965	2	17	0	PM	F
1965	2	18	0	PM	F
1965	2	19	0	PM	F
1965	2	20	0	PM	F
1965	2	21	0	PM	F
1965	2	22	0	PM	F
1965	2	23	T	PM	F
1965	2	24	0.6	PM	F
1965	2	25	0.09	PM	F
1965	2	26	0	PM	F
1965	2	27	0	PM	F
1965	2	28	0	PM	F
1965	3	1	0.03	PM	F
1965	3	2	0.44	PM	F
1965	3	3	T	PM	F
1965	3	4	0.64	PM	F
1965	3	5	T	PM	F
1965	3	6	0.05	PM	F
1965	3	7	0.01	PM	F
1965	3	8	0	PM	F
1965	3	9	0.02	PM	F
1965	3	10	0	PM	F
1965	3	11	0	PM	F
1965	3	12	T	PM	F
1965	3	13	0	PM	F
1965	3	14	0.09	PM	F
1965	3	15	0	PM	F
1965	3	16	0	PM	F
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1965	3	18	0	PM	F
1965	3	19	0	PM	F
1965	3	20	0	PM	F
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1965	3	22	0	PM	F
1965	3	23	0.74	PM	F
1965	3	24	0.11	PM	F
1965	3	25	0.07	PM	F
1965	3	26	T	PM	F
1965	3	27	0	PM	F
1965	3	28	T	PM	F
1965	3	29	0	PM	F
1965	3	30	0	PM	F
1965	3	31	0	PM	F
1965	4	1	0	PM	F
1965	4	2	0	PM	F
1965	4	3	0.02	PM	F
1965	4	4	0.02	PM	F
1965	4	5	0.74	PM	F
1965	4	6	0.81	PM	F
1965	4	7	0	PM	F
1965	4	8	0.05	PM	F
1965	4	9	0	PM	F
1965	4	10	0.24	PM	F
1965	4	11	0.4	PM	F
1965	4	12	0	PM	F
1965	4	13	0	PM	F
1965	4	14	0.1	PM	F
1965	4	15	1.2	PM	F
1965	4	16	0.03	PM	F
1965	4	17	0	PM	F
1965	4	18	0.01	PM	F
1965	4	19	0	PM	F
1965	4	20	0	PM	F
1965	4	21	T	PM	F
1965	4	22	0	PM	F
1965	4	23	0.32	PM	F
1965	4	24	0.14	PM	F
1965	4	25	0.86	PM	F
1965	4	26	0.02	PM	F
1965	4	27	0	PM	F
1965	4	28	0.78	PM	F
1965	4	29	0	PM	F
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1965	5	1	0	PM	F
1965	5	2	0	PM	F
1965	5	3	0	PM	F
1965	5	4	0	PM	F
1965	5	5	0.74	PM	F
1965	5	6	0.13	PM	F
1965	5	7	0	PM	F
1965	5	8	0	PM	F
1965	5	9	0.02	PM	F
1965	5	10	0	PM	F
1965	5	11	0	PM	F
1965	5	12	0	PM	F
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1965	5	14	0	PM	F
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1965	5	18	1.32	PM	F
1965	5	19	0.04	PM	F
1965	5	20	0	PM	F
1965	5	21	0	PM	F
1965	5	22	0.22	PM	F
1965	5	23	0.1	PM	F
1965	5	24	T	PM	F
1965	5	25	0.13	PM	F

1965	5	26	0.78	PM	F
1965	5	27	0.15	PM	F
1965	5	28	0	PM	F
1965	5	29	0	PM	F
1965	5	30	0.1	PM	F
1965	5	31	0	PM	F
1965	6	1	0.19	PM	F
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1965	6	3	0	PM	F
1965	6	4	0	PM	F
1965	6	5	0	PM	F
1965	6	6	0.02	PM	F
1965	6	7	0.19	PM	F
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1965	6	9	0	PM	F
1965	6	10	0	PM	F
1965	6	11	0	PM	F
1965	6	12	0	PM	F
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1965	6	14	0	PM	F
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1965	6	17	0	PM	F
1965	6	18	0	PM	F
1965	6	19	0	PM	F
1965	6	20	0	PM	F
1965	6	21	0.33	PM	F
1965	6	22	0	PM	F
1965	6	23	0	PM	F
1965	6	24 T		PM	F
1965	6	25	0	PM	F
1965	6	26	0	PM	F
1965	6	27	0	PM	F
1965	6	28	0	PM	F
1965	6	29	0.6	PM	F
1965	6	30	0	PM	F
1965	7	1	0	PM	F
1965	7	2	0.75	PM	F
1965	7	3	0	PM	F
1965	7	4	0	PM	F
1965	7	5	0	PM	F
1965	7	6 T		PM	F
1965	7	7	0.57	PM	F
1965	7	8	0	PM	F
1965	7	9	0.17	PM	F
1965	7	10	0	PM	F
1965	7	11	0	PM	F
1965	7	12	0	PM	F
1965	7	13	0	PM	F
1965	7	14 T		PM	F
1965	7	15	0	PM	F
1965	7	16	0	PM	F
1965	7	17	0.14	PM	F
1965	7	18	0	PM	F
1965	7	19	0	PM	F
1965	7	20	0.02	PM	F
1965	7	21	0	PM	F
1965	7	22	0	PM	F
1965	7	23	0	PM	F
1965	7	24	0	PM	F
1965	7	25	0	PM	F
1965	7	26	0	PM	F
1965	7	27	0	PM	F
1965	7	28	0	PM	F
1965	7	29	0	PM	F
1965	7	30	0	PM	F
1965	7	31	0.06	PM	F
1965	8	1	1.02	PM	F
1965	8	2	0.12	PM	F
1965	8	3	0.02	PM	F
1965	8	4	1.59	PM	F
1965	8	5	0	PM	F
1965	8	6	0	PM	F
1965	8	7	0.2	PM	F
1965	8	8	0	PM	F
1965	8	9	0.03	PM	F
1965	8	10	0	PM	F
1965	8	11	0	PM	F
1965	8	12	0	PM	F
1965	8	13	0	PM	F
1965	8	14	0	PM	F
1965	8	15	0	PM	F
1965	8	16	0.6	PM	F
1965	8	17	0.53	PM	F
1965	8	18	0	PM	F
1965	8	19	0	PM	F
1965	8	20	0	PM	F
1965	8	21	0	PM	F
1965	8	22	0.1	PM	F
1965	8	23	0	PM	F
1965	8	24	0	PM	F
1965	8	25	0.1	PM	F
1965	8	26	2.44	PM	F
1965	8	27	0	PM	F
1965	8	28	0	PM	F
1965	8	29	0	PM	F
1965	8	30	0.62	PM	F
1965	8	31	1.73	PM	F
1965	9	1	0	PM	F
1965	9	2	0	PM	F
1965	9	3	0	PM	F
1965	9	4	0.31	PM	F
1965	9	5	0	PM	F
1965	9	6	0	PM	F
1965	9	7	0.15	PM	F
1965	9	8	0.03	PM	F
1965	9	9	0	PM	F
1965	9	10	0	PM	F
1965	9	11	0	PM	F
1965	9	12	0	PM	F
1965	9	13	0	PM	F
1965	9	14	0	PM	F
1965	9	15	1.55	PM	F
1965	9	16	2.7	PM	F
1965	9	17	0	PM	F

1965	9	18	0	PM	F
1965	9	19	0	PM	F
1965	9	20	0.49	PM	F
1965	9	21	0.05	PM	F
1965	9	22	1.42	PM	F
1965	9	23	0.2	PM	F
1965	9	24	0	PM	F
1965	9	25	0	PM	F
1965	9	26	0	PM	F
1965	9	27	0	PM	F
1965	9	28	0	PM	F
1965	9	29	0	PM	F
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1965	10	3	0	PM	F
1965	10	4	0	PM	F
1965	10	5	0	PM	F
1965	10	6	0	PM	F
1965	10	7	0.66	PM	F
1965	10	8	0	PM	F
1965	10	9	0	PM	F
1965	10	10	0	PM	F
1965	10	11	0.35	PM	F
1965	10	12	0	PM	F
1965	10	13	0	PM	F
1965	10	14	0	PM	F
1965	10	15	0	PM	F
1965	10	16	0	PM	F
1965	10	17	0	PM	F
1965	10	18	0	PM	F
1965	10	19	0	PM	F
1965	10	20	0.05	PM	F
1965	10	21	0.02	PM	F
1965	10	22	0.04	PM	F
1965	10	23	0	PM	F
1965	10	24	0	PM	F
1965	10	25	0	PM	F
1965	10	26	0	PM	F
1965	10	27	0	PM	F
1965	10	28	0	PM	F
1965	10	29	0	PM	F
1965	10	30	0	PM	F
1965	10	31	0	PM	F
1965	11	1	0	PM	F
1965	11	2	0	PM	F
1965	11	3	0	PM	F
1965	11	4	0	PM	F
1965	11	5	0	PM	F
1965	11	6 T		PM	F
1965	11	7 T		PM	F
1965	11	8	0.33	PM	F
1965	11	9	0	PM	F
1965	11	10	0	PM	F
1965	11	11	0	PM	F
1965	11	12	0.16	PM	F
1965	11	13	0	PM	F
1965	11	14	0	PM	F
1965	11	15	0	PM	F
1965	11	16	0.02	PM	F
1965	11	17	0	PM	F
1965	11	18 T		PM	F
1965	11	19	0	PM	F
1965	11	20	0	PM	F
1965	11	21	0.1	PM	F
1965	11	22	0	PM	F
1965	11	23	0	PM	F
1965	11	24	0.01	PM	F
1965	11	25	0	PM	F
1965	11	26	0.37	PM	F
1965	11	27	0	PM	F
1965	11	28	0	PM	F
1965	11	29	0	PM	F
1965	11	30 T		PM	F
1965	12	1	0	PM	F
1965	12	2	0.07	PM	F
1965	12	3	0.02	PM	F
1965	12	4	0	PM	F
1965	12	5	0	PM	F
1965	12	6	0	PM	F
1965	12	7	0	PM	F
1965	12	8	0	PM	F
1965	12	9	0	PM	F
1965	12	10	0.14	PM	F
1965	12	11	0.13	PM	F
1965	12	12	0.18	PM	F
1965	12	13	0	PM	F
1965	12	14	0	PM	F
1965	12	15	0	PM	F
1965	12	16	0.01	PM	F
1965	12	17	0	PM	F
1965	12	18	0	PM	F
1965	12	19	0	PM	F
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1965	12	23	0.02	PM	F
1965	12	24	0.97	PM	F
1965	12	25	1.43	PM	F
1965	12	26	0	PM	F
1965	12	27	0	PM	F
1965	12	28	0	PM	F
1965	12	29	0	PM	F
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1966	1	2	0	PM	F
1966	1	3	0	PM	F
1966	1	4	0	PM	F
1966	1	5	0	PM	F
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1966	1	8	0	PM	F
1966	1	9	0	PM	F
1966	1	10	0	PM	F

1966	1	11	0	PM	F
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1966	1	13	0.14	PM	F
1966	1	14	0	PM	F
1966	1	15	0	PM	F
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1966	1	17	0	PM	F
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1966	1	27	0	PM	F
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1966	1	29	T	PM	F
1966	1	30	0	PM	F
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1966	2	5	0	PM	F
1966	2	6	0	PM	F
1966	2	7	0	PM	F
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1966	2	12	0	PM	F
1966	2	13	0	PM	F
1966	2	14	0.02	PM	F
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1966	2	25	0	PM	F
1966	2	26	0	PM	F
1966	2	27	0.02	PM	F
1966	2	28	0.56	PM	F
1966	3	1	0.13	PM	F
1966	3	2	0	PM	F
1966	3	3	0.23	PM	F
1966	3	4	1.07	PM	F
1966	3	5	0.02	PM	F
1966	3	6	T	PM	F
1966	3	7	0	PM	F
1966	3	8	0	PM	F
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1966	3	11	0.12	PM	F
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1966	3	14	0	PM	F
1966	3	15	0	PM	F
1966	3	16	0	PM	F
1966	3	17	0	PM	F
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1966	3	23	0.14	PM	F
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1966	4	5	0.01	PM	F
1966	4	6	0	PM	F
1966	4	7	0	PM	F
1966	4	8	0.01	PM	F
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1966	4	12	0	PM	F
1966	4	13	0	PM	F
1966	4	14	0	PM	F
1966	4	15	T	PM	F
1966	4	16	0	PM	F
1966	4	17	T	PM	F
1966	4	18	T	PM	F
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1966	4	23	1.23	PM	F
1966	4	24	0.23	PM	F
1966	4	25	0	PM	F
1966	4	26	0	PM	F
1966	4	27	0.45	PM	F
1966	4	28	0.61	PM	F
1966	4	29	0	PM	F
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1966	5	1	0	PM	F
1966	5	2	0	PM	F
1966	5	3	0	PM	F
1966	5	4	0	PM	F
1966	5	5	0	PM	F

1966	5	6	0	PM	F
1966	5	7	0	PM	F
1966	5	8	0	PM	F
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1966	5	11	0.62	PM	F
1966	5	12	0.04	PM	F
1966	5	13	0.14	PM	F
1966	5	14	0	PM	F
1966	5	15	0.05	PM	F
1966	5	16	0.02	PM	F
1966	5	17	0.28	PM	F
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1966	5	22	0	PM	F
1966	5	23	0	PM	F
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1966	6	4	0	PM	F
1966	6	5	0	PM	F
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1966	6	11	0	PM	F
1966	6	12	0	PM	F
1966	6	13	0.04	PM	F
1966	6	14	0.06	PM	F
1966	6	15	0.02	PM	F
1966	6	16	0.8	PM	F
1966	6	17	0	PM	F
1966	6	18	0	PM	F
1966	6	19	0	PM	F
1966	6	20	0	PM	F
1966	6	21	0	PM	F
1966	6	22	0	PM	F
1966	6	23	0	PM	F
1966	6	24	0	PM	F
1966	6	25	0	PM	F
1966	6	26	0	PM	F
1966	6	27	0	PM	F
1966	6	28	0.11	PM	F
1966	6	29	0.03	PM	F
1966	6	30	0	PM	F
1966	7	1	0	PM	F
1966	7	2	0	PM	F
1966	7	3	0	PM	F
1966	7	4	0	PM	F
1966	7	5	0	PM	F
1966	7	6	0.15	PM	F
1966	7	7	0	PM	F
1966	7	8	0	PM	F
1966	7	9	0	PM	F
1966	7	10	0.05	PM	F
1966	7	11	0	PM	F
1966	7	12	0	PM	F
1966	7	13	0	PM	F
1966	7	14	0	PM	F
1966	7	15	T	PM	F
1966	7	16	0	PM	F
1966	7	17	0	PM	F
1966	7	18	0	PM	F
1966	7	19	0.03	PM	F
1966	7	20	0	PM	F
1966	7	21	0	PM	F
1966	7	22	0	PM	F
1966	7	23	0	PM	F
1966	7	24	T	PM	F
1966	7	25	0	PM	F
1966	7	26	0	PM	F
1966	7	27	0.22	PM	F
1966	7	28	2.03	PM	F
1966	7	29	0	PM	F
1966	7	30	0	PM	F
1966	7	31	0	PM	F
1966	8	1	0	PM	F
1966	8	2	0.2	PM	F
1966	8	3	0	PM	F
1966	8	4	0	PM	F
1966	8	5	0	PM	F
1966	8	6	0	PM	F
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1966	8	11	0.13	PM	F
1966	8	12	0	PM	F
1966	8	13	0	PM	F
1966	8	14	0	PM	F
1966	8	15	0.02	PM	F
1966	8	16	0	PM	F
1966	8	17	0	PM	F
1966	8	18	0	PM	F
1966	8	19	0.05	PM	F
1966	8	20	0	PM	F
1966	8	21	0	PM	F
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1966	8	23	0	PM	F
1966	8	24	0	PM	F
1966	8	25	0	PM	F
1966	8	26	0	PM	F
1966	8	27	0	PM	F
1966	8	28	0	PM	F

1966	8	29	0	PM	F
1966	8	30	0	PM	F
1966	8	31	0	PM	F
1966	9	1	0	PM	F
1966	9	2	0	PM	F
1966	9	3	0.45	PM	F
1966	9	4	0	PM	F
1966	9	5	0	PM	F
1966	9	6	0	PM	F
1966	9	7	0	PM	F
1966	9	8	0	PM	F
1966	9	9	0	PM	F
1966	9	10	0	PM	F
1966	9	11	0	PM	F
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1966	9	16	0	PM	F
1966	9	17	0	PM	F
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1966	9	22	0	PM	F
1966	9	23	0	PM	F
1966	9	24	0	PM	F
1966	9	25	0.15	PM	F
1966	9	26	0	PM	F
1966	9	27	0.09	PM	F
1966	9	28	0	PM	F
1966	9	29	0.09	PM	F
1966	9	30	0.07	PM	F
1966	10	1	0	PM	F
1966	10	2	0	PM	F
1966	10	3	0	PM	F
1966	10	4	0	PM	F
1966	10	5	0	PM	F
1966	10	6	0	PM	F
1966	10	7	0	PM	F
1966	10	8	0	PM	F
1966	10	9	0	PM	F
1966	10	10	0.16	PM	F
1966	10	11	0	PM	F
1966	10	12	0	PM	F
1966	10	13	0.19	PM	F
1966	10	14	0.01	PM	F
1966	10	15	1	PM	F
1966	10	16	0	PM	F
1966	10	17	0	PM	F
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1966	10	20	0	PM	F
1966	10	21	0	PM	F
1966	10	22	0	PM	F
1966	10	23	0	PM	F
1966	10	24	0	PM	F
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1966	11	1	0	PM	F
1966	11	2	T	PM	F
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1966	11	7	0.06	PM	F
1966	11	8	0.04	PM	F
1966	11	9	0.27	PM	F
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1966	11	11	0	PM	F
1966	11	12	0	PM	F
1966	11	13	0	PM	F
1966	11	14	0	PM	F
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1966	11	18	0	PM	F
1966	11	19	0	PM	F
1966	11	20	0	PM	F
1966	11	21	0	PM	F
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1966	11	23	0	PM	F
1966	11	24	0	PM	F
1966	11	25	0.8	PM	F
1966	11	26	0.08	PM	F
1966	11	27	2.43	PM	F
1966	11	28	0	PM	F
1966	11	29	0	PM	F
1966	11	30	0	PM	F
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1966	12	2	0	PM	F
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1966	12	5	0.2	PM	F
1966	12	6	0.29	PM	F
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1966	12	10	0	PM	F
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1966	12	12	0	PM	F
1966	12	13	0	PM	F
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1966	12	18	0	PM	F
1966	12	19	0	PM	F
1966	12	20	0	PM	F
1966	12	21	0	PM	F

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1966	12	24	0	PM	F
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1966	12	26	0	PM	F
1966	12	27	0	PM	F
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1966	12	29	T	PM	F
1966	12	30	T	PM	F
1966	12	31	T	PM	F
1967	1	1	T	PM	F
1967	1	2	0	PM	F
1967	1	3	0	PM	F
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1967	1	5	0.01	PM	F
1967	1	6	0	PM	F
1967	1	7	0.2	PM	F
1967	1	8	T	PM	F
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1967	1	10	0	PM	F
1967	1	11	0	PM	F
1967	1	12	0	PM	F
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1967	1	21	0	PM	F
1967	1	22	0	PM	F
1967	1	23	0	PM	F
1967	1	24	0	PM	F
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1967	1	26	1.32	PM	F
1967	1	27	0.53	PM	F
1967	1	28	0	PM	F
1967	1	29	0	PM	F
1967	1	30	0	PM	F
1967	1	31	0	PM	F
1967	2	1	0.02	PM	F
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1967	2	4	0	PM	F
1967	2	5	0.18	PM	F
1967	2	6	0	PM	F
1967	2	7	0	PM	F
1967	2	8	0	PM	F
1967	2	9	0	PM	F
1967	2	10	0	PM	F
1967	2	11	0	PM	F
1967	2	12	0	PM	F
1967	2	13	0	PM	F
1967	2	14	0	PM	F
1967	2	15	T	PM	F
1967	2	16	0	PM	F
1967	2	17	0	PM	F
1967	2	18	0.02	PM	F
1967	2	19	0	PM	F
1967	2	20	T	PM	F
1967	2	21	T	PM	F
1967	2	22	0.02	PM	F
1967	2	23	0.12	PM	F
1967	2	24	T	PM	F
1967	2	25	0	PM	F
1967	2	26	0	PM	F
1967	2	27	0.18	PM	F
1967	2	28	0	PM	F
1967	3	1	0	PM	F
1967	3	2	0	PM	F
1967	3	3	0	PM	F
1967	3	4	0.08	PM	F
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1967	3	10	0	PM	F
1967	3	11	0	PM	F
1967	3	12	0	PM	F
1967	3	13	0.01	PM	F
1967	3	14	0	PM	F
1967	3	15	0.04	PM	F
1967	3	16	0	PM	F
1967	3	17	0	PM	F
1967	3	18	0	PM	F
1967	3	19	0	PM	F
1967	3	20	1.5	PM	F
1967	3	21	0.05	PM	F
1967	3	22	0	PM	F
1967	3	23	0	PM	F
1967	3	24	0.01	PM	F
1967	3	25	0.02	PM	F
1967	3	26	0.15	PM	F
1967	3	27	0.04	PM	F
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1967	3	29	0	PM	F
1967	3	30	0	PM	F
1967	3	31	0	PM	F
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1967	4	6	0	PM	F
1967	4	7	0	PM	F
1967	4	8	0.04	PM	F
1967	4	9	0.08	PM	F
1967	4	10	0	PM	F
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1967	4	13	0.52	PM	F
1967	4	14	0	PM	F
1967	4	15	0	PM	F

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1967	4	21	0.42	PM	F
1967	4	22	0.4	PM	F
1967	4	23	0.18	PM	F
1967	4	24	0.18	PM	F
1967	4	25	0	PM	F
1967	4	26	0.29	PM	F
1967	4	27	0.02	PM	F
1967	4	28	0	PM	F
1967	4	29	0.28	PM	F
1967	4	30	0.12	PM	F
1967	5	1	0.08	PM	F
1967	5	2	0	PM	F
1967	5	3	0	PM	F
1967	5	4	0.02	PM	F
1967	5	5	0.16	PM	F
1967	5	6	1	PM	F
1967	5	7	1.5	PM	F
1967	5	8	0.01	PM	F
1967	5	9	0	PM	F
1967	5	10	0	PM	F
1967	5	11	0.34	PM	F
1967	5	12	0	PM	F
1967	5	13	0	PM	F
1967	5	14	0.11	PM	F
1967	5	15	0	PM	F
1967	5	16	0	PM	F
1967	5	17	0	PM	F
1967	5	18	0	PM	F
1967	5	19	0.07	PM	F
1967	5	20	0	PM	F
1967	5	21	0	PM	F
1967	5	22	0	PM	F
1967	5	23	0	PM	F
1967	5	24	0	PM	F
1967	5	25	0	PM	F
1967	5	26	0	PM	F
1967	5	27	0	PM	F
1967	5	28	1.6	PM	F
1967	5	29	0.04	PM	F
1967	5	30	1.05	PM	F
1967	5	31	0.11	PM	F
1967	6	1	0.04	PM	F
1967	6	2	0	PM	F
1967	6	3	0	PM	F
1967	6	4	0	PM	F
1967	6	5	0	PM	F
1967	6	6	0.31	PM	F
1967	6	7	0.08	PM	F
1967	6	8	0.07	PM	F
1967	6	9	0.1	PM	F
1967	6	10	0	PM	F
1967	6	11	0.7	PM	F
1967	6	12	1.17	PM	F
1967	6	13	0	PM	F
1967	6	14	0	PM	F
1967	6	15	0	PM	F
1967	6	16	0	PM	F
1967	6	17	0.06	PM	F
1967	6	18	0	PM	F
1967	6	19	0	PM	F
1967	6	20	0	PM	F
1967	6	21	0.85	PM	F
1967	6	22	0	PM	F
1967	6	23	0	PM	F
1967	6	24	0.02	PM	F
1967	6	25	0	PM	F
1967	6	26	0	PM	F
1967	6	27	0	PM	F
1967	6	28	0	PM	F
1967	6	29	0	PM	F
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1967	7	2	0.08	PM	F
1967	7	3	0	PM	F
1967	7	4	0	PM	F
1967	7	5	0	PM	F
1967	7	6	0	PM	F
1967	7	7	0	PM	F
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1967	7	9	0.12	PM	F
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1967	7	11	0	PM	F
1967	7	12	0	PM	F
1967	7	13	0	PM	F
1967	7	14	0	PM	F
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1967	7	22	0	PM	F
1967	7	23	0	PM	F
1967	7	24	1.74	PM	F
1967	7	25	0	PM	F
1967	7	26	0	PM	F
1967	7	27	0.56	PM	F
1967	7	28	0	PM	F
1967	7	29	0	PM	F
1967	7	30	0	PM	F
1967	7	31	0.32	PM	F
1967	8	1	0	PM	F
1967	8	2	0	PM	F
1967	8	3	T	PM	F
1967	8	4	0	PM	F
1967	8	5	0	PM	F
1967	8	6	0	PM	F
1967	8	7	0.07	PM	F
1967	8	8	0.6	PM	F

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1967	8	10		0 PM	F
1967	8	11		0 PM	F
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1967	8	28		0 PM	F
1967	8	29		0 PM	F
1967	8	30	T	PM	F
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1967	9	5		0 PM	F
1967	9	6		0 PM	F
1967	9	7		0 PM	F
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1967	9	16		0.03 PM	F
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1967	9	23		0 PM	F
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1967	10	1		0 PM	F
1967	10	2		0 PM	F
1967	10	3		0 PM	F
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1967	10	8		0.54 PM	F
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1967	10	11		0 PM	F
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1967	10	14		0 PM	F
1967	10	15		1.2 PM	F
1967	10	16		2.09 PM	F
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1967	10	28		0.04 PM	F
1967	10	29		0.11 PM	F
1967	10	30		0.17 PM	F
1967	10	31		0.68 PM	F
1967	11	1		0.25 PM	F
1967	11	2		0.08 PM	F
1967	11	3		0.54 PM	F
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1967	11	16		0 PM	F
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1967	11	26		0 PM	F
1967	11	27		0 PM	F
1967	11	28		0 PM	F
1967	11	29		0 PM	F
1967	11	30		0.25 PM	F
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1967	12	13		0 PM	F
1967	12	14		0 PM	F
1967	12	15		0 PM	F
1967	12	16		0 PM	F
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1967	12	22		0 PM	F
1967	12	23		0 PM	F
1967	12	24		0 PM	F
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1967	12	26		0 PM	F
1967	12	27	T	PM	F
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1967	12	29		0 PM	F
1967	12	30		0 PM	F
1967	12	31		0.09 PM	F
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1968	1	2		0.02 PM	F
1968	1	3		0 PM	F
1968	1	4		0 PM	F
1968	1	5		0 PM	F
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1968	1	10		0 PM	F
1968	1	11		0 PM	F
1968	1	12		0 PM	F
1968	1	13		0.3 PM	F
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1968	1	15		0 PM	F
1968	1	16		0 PM	F
1968	1	17		0 PM	F
1968	1	18		0 PM	F
1968	1	19		0.01 PM	F
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1968	1	23		0 PM	F
1968	1	24		0 PM	F
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1968	1	27		0.18 PM	F
1968	1	28		0 PM	F
1968	1	29		0.33 PM	F
1968	1	30		0.02 PM	F
1968	1	31		0.01 PM	F
1968	2	1		1.4 PM	F
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1968	2	4		0 PM	F
1968	2	5		0 PM	F
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1968	2	7		0.11 PM	F
1968	2	8		0 PM	F
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1968	2	23		0 PM	F
1968	2	24		0 PM	F
1968	2	25		0 PM	F
1968	2	26	T	PM	F
1968	2	27		0.02 PM	F
1968	2	28		0.04 PM	F
1968	2	29	T	PM	F
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1968	3	2		0 PM	F
1968	3	3		0 PM	F
1968	3	4		0 PM	F
1968	3	5		0 PM	F
1968	3	6		0 PM	F
1968	3	7		0 PM	F
1968	3	8		0.01 PM	F
1968	3	9		0.03 PM	F
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1968	3	17		0 PM	F
1968	3	18		0.01 PM	F
1968	3	19		0.16 PM	F
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1968	3	23		0 PM	F
1968	3	24		0 PM	F
1968	3	25		0 PM	F

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1968	3	29 T		PM	F
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1968	4	4	2.03	PM	F
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1968	4	7	0	PM	F
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1968	4	18	0	PM	F
1968	4	19	0	PM	F
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1968	4	21	0	PM	F
1968	4	22	0	PM	F
1968	4	23	0	PM	F
1968	4	24	0	PM	F
1968	4	25	0	PM	F
1968	4	26	0.11	PM	F
1968	4	27	0	PM	F
1968	4	28	0	PM	F
1968	4	29	0.03	PM	F
1968	4	30	0	PM	F
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1968	5	2	0	PM	F
1968	5	3	0	PM	F
1968	5	4	0	PM	F
1968	5	5	0	PM	F
1968	5	6	0	PM	F
1968	5	7	0	PM	F
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1968	5	9	0.08	PM	F
1968	5	10	0	PM	F
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1968	5	12	0	PM	F
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1968	5	15 M		-	F
1968	5	16	0	PM	F
1968	5	17	0	PM	F
1968	5	18	0.52	PM	F
1968	5	19	0.05	PM	F
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1968	5	22 T		PM	F
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1968	5	26	0	PM	F
1968	5	27 T		PM	F
1968	5	28	0.02	PM	F
1968	5	29	0.69	PM	F
1968	5	30	0	PM	F
1968	5	31	0	PM	F
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1968	6	2	0	PM	F
1968	6	3	0	PM	F
1968	6	4	0	PM	F
1968	6	5	0	PM	F
1968	6	6	0	PM	F
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1968	6	9	0	PM	F
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1968	6	12	0	PM	F
1968	6	13	0	PM	F
1968	6	14 T		PM	F
1968	6	15	2.62	PM	F
1968	6	16	0.1	PM	F
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1968	6	18	0	PM	F
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1968	6	24	0.05	PM	F
1968	6	25	1.15	PM	F
1968	6	26	0.48	PM	F
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1968	7	2	0	PM	F
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1968	7	6	0	PM	F
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1968	7	11	0	PM	F
1968	7	12	0	PM	F
1968	7	13	0	PM	F
1968	7	14 T		PM	F
1968	7	15	0.07	PM	F
1968	7	16	0	PM	F
1968	7	17	0	PM	F
1968	7	18	0.96	PM	F

1968	7	19		0 PM	F
1968	7	20		0 PM	F
1968	7	21		0 PM	F
1968	7	22		0 PM	F
1968	7	23		0.07 PM	F
1968	7	24		0.25 PM	F
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1968	7	27		0.34 PM	F
1968	7	28		0 PM	F
1968	7	29		0 PM	F
1968	7	30		0 PM	F
1968	7	31		0 PM	F
1968	8	1		0.1 PM	F
1968	8	2		0 PM	F
1968	8	3		0 PM	F
1968	8	4		4.25 PM	F
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1968	8	6		0 PM	F
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1968	8	27		0 PM	F
1968	8	28		0 PM	F
1968	8	29		0 PM	F
1968	8	30		0 PM	F
1968	8	31		0.06 PM	F
1968	9	1		0.08 PM	F
1968	9	2		0 PM	F
1968	9	3		0 PM	F
1968	9	4		0.01 PM	F
1968	9	5		0 PM	F
1968	9	6		0 PM	F
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1968	9	12		0 PM	F
1968	9	13		0 PM	F
1968	9	14		0 PM	F
1968	9	15		0 PM	F
1968	9	16		0.07 PM	F
1968	9	17		0.04 PM	F
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1968	9	21		0 PM	F
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1968	9	25		0 PM	F
1968	9	26		0 PM	F
1968	9	27		0 PM	F
1968	9	28		0 PM	F
1968	9	29	T	PM	F
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1968	10	1		0 PM	F
1968	10	2		0.03 PM	F
1968	10	3		0.1 PM	F
1968	10	4		0 PM	F
1968	10	5		0 PM	F
1968	10	6		0.03 PM	F
1968	10	7		0 PM	F
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1968	10	11		0 PM	F
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1968	10	18		0 PM	F
1968	10	19		0 PM	F
1968	10	20		0 PM	F
1968	10	21		0 PM	F
1968	10	22		0.05 PM	F
1968	10	23		0 PM	F
1968	10	24		0.04 PM	F
1968	10	25		0 PM	F
1968	10	26		0 PM	F
1968	10	27		0 PM	F
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1968	10	30		0 PM	F
1968	10	31		0 PM	F
1968	11	1		0 PM	F
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1968	11	4		0 PM	F
1968	11	5		0 PM	F
1968	11	6		0.01 PM	F
1968	11	7		0.13 PM	F
1968	11	8		0 PM	F
1968	11	9	T	PM	F
1968	11	10		0 PM	F

1968	11	11	0.05	PM	F
1968	11	12	0	PM	F
1968	11	13	0	PM	F
1968	11	14	0.06	PM	F
1968	11	15	0.45	PM	F
1968	11	16	0.72	PM	F
1968	11	17	0.03	PM	F
1968	11	18	1.07	PM	F
1968	11	19	0.02	PM	F
1968	11	20	0	PM	F
1968	11	21	0	PM	F
1968	11	22	0	PM	F
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1968	11	27	0	PM	F
1968	11	28	1.44	PM	F
1968	11	29	0	PM	F
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1968	12	1	0.22	PM	F
1968	12	2	0	PM	F
1968	12	3	0	PM	F
1968	12	4	0	PM	F
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1968	12	6	0	PM	F
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1968	12	14	0	PM	F
1968	12	15	0	PM	F
1968	12	16	0	PM	F
1968	12	17	0	PM	F
1968	12	18	0.03	PM	F
1968	12	19	0.29	PM	F
1968	12	20	0	PM	F
1968	12	21	0	PM	F
1968	12	22	0.45	PM	F
1968	12	23	0.06	PM	F
1968	12	24	0	PM	F
1968	12	25 T		PM	F
1968	12	26 T		PM	F
1968	12	27	0.63	PM	F
1968	12	28	0.92	PM	F
1968	12	29	0	PM	F
1968	12	30	0.14	PM	F
1968	12	31	0.04	PM	F
1969	1	1	0	PM	F
1969	1	2	0	PM	F
1969	1	3	0	PM	F
1969	1	4	0	PM	F
1969	1	5	0.04	PM	F
1969	1	6	0.37	PM	F
1969	1	7	0	PM	F
1969	1	8	0	PM	F
1969	1	9	0.01	PM	F
1969	1	10	0	PM	F
1969	1	11	0	PM	F
1969	1	12	0	PM	F
1969	1	13	0	PM	F
1969	1	14	0	PM	F
1969	1	15	0.04	PM	F
1969	1	16	0.43	PM	F
1969	1	17	0.4	PM	F
1969	1	18	0	PM	F
1969	1	19	0	PM	F
1969	1	20	0	PM	F
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1969	1	22	0.05	PM	F
1969	1	23	0.3	PM	F
1969	1	24 T		PM	F
1969	1	25	0	PM	F
1969	1	26	0.08	PM	F
1969	1	27	0	PM	F
1969	1	28	0.67	PM	F
1969	1	29	0.63	PM	F
1969	1	30	0.07	PM	F
1969	1	31	0	PM	F
1969	2	1	0	PM	F
1969	2	2	0	PM	F
1969	2	3	0.07	PM	F
1969	2	4	0	PM	F
1969	2	5	0	PM	F
1969	2	6	0.08	PM	F
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1969	2	8	0.79	PM	F
1969	2	9 T		PM	F
1969	2	10	0	PM	F
1969	2	11	0	PM	F
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1969	2	15	0	PM	F
1969	2	16	0	PM	F
1969	2	17	0	PM	F
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1969	3	4	0	PM	F
1969	3	5	0	PM	F

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1970	2	13	T	PM	F

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1970	2	19 T		PM	F
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1970	10	11	0	PM	F
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1970	10	23	0.18	PM	F
1970	10	24	0	PM	F
1970	10	25	0	PM	F
1970	10	26	0	PM	F
1970	10	27	0.02	PM	F
1970	10	28	0.51	PM	F
1970	10	29	0	PM	F
1970	10	30	0	PM	F
1970	10	31	0	PM	F
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1970	11	2	0.03	PM	F
1970	11	3	0.05	PM	F
1970	11	4	0.08	PM	F
1970	11	5	0	PM	F
1970	11	6	0	PM	F
1970	11	7	0	PM	F
1970	11	8	0	PM	F
1970	11	9	0.34	PM	F
1970	11	10	0.18	PM	F
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1970	11	12	0	PM	F
1970	11	13	0	PM	F
1970	11	14	0.04	PM	F
1970	11	15	0	PM	F
1970	11	16	0	PM	F
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1970	11	24	0.02	PM	F
1970	11	25	0	PM	F
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1970	11	27	0.02	PM	F
1970	11	28	0.03	PM	F
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1970	12	15	0	PM	F
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1970	12	24	0	PM	F
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1970	12	26	0	PM	F
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1971	1	9	0	PM	F
1971	1	10	0	PM	F
1971	1	11	0	PM	F
1971	1	12	0	PM	F
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1971	1	14	0	PM	F
1971	1	15	0	PM	F
1971	1	16	0	PM	F
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1971	1	21	0	PM	F
1971	1	22	0	PM	F
1971	1	23	0	PM	F
1971	1	24	0	PM	F

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1971	6	27	0	PM	F
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1971	8	13	0	PM	F
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1971	8	18	0	PM	F
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1971	8	31	0	PM	F
1971	9	1	0	PM	F
1971	9	2	0	PM	F
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1971	9	13	0	PM	F
1971	9	14	0	PM	F
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1971	10	5	0	PM	F
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1971	10	14	0	PM	F
1971	10	15	0	PM	F
1971	10	16	0	PM	F
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1971	10	18	0	PM	F
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1971	10	24	0.05	PM	F
1971	10	25	0	PM	F
1971	10	26	0	PM	F
1971	10	27	0	PM	F
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1971	10	29	0	PM	F
1971	10	30	0	PM	F
1971	10	31	0	PM	F
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1971	11	4	0	PM	F
1971	11	5	0	PM	F
1971	11	6	0	PM	F
1971	11	7	0	PM	F
1971	11	8	0	PM	F
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1971	11	10	0	PM	F
1971	11	11	0	PM	F
1971	11	12	0	PM	F
1971	11	13	0	PM	F
1971	11	14	0	PM	F
1971	11	15	0	PM	F
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1971	11	21	0	PM	F
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1971	11	25	0	PM	F
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1971	11	30	0	PM	F
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1971	12	16	0	PM	F
1971	12	17	0	PM	F
1971	12	18	0	PM	F
1971	12	19	0.04	PM	F
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1971	12	22	0	PM	F
1971	12	23	0	PM	F
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1971	12	27	0.01	PM	F
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1972	1	4	0	PM	F

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1972	1	6	0	PM	F
1972	1	7	0	PM	F
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1972	1	9	0	PM	F
1972	1	10	0	PM	F
1972	1	11	T	PM	F
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1972	1	13	0.16	PM	F
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1972	1	15	0	PM	F
1972	1	16	0	PM	F
1972	1	17	0	PM	F
1972	1	18	0	PM	F
1972	1	19	0	PM	F
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1972	1	21	0	PM	F
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1972	1	24	0	PM	F
1972	1	25	0	PM	F
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1972	1	30	0	PM	F
1972	1	31	0	PM	F
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1972	2	4	0	PM	F
1972	2	5	0	PM	F
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1972	2	20	0	PM	F
1972	2	21	0	PM	F
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1972	2	24	0	PM	F
1972	2	25	T	PM	F
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1972	2	27	0	PM	F
1972	2	28	0	PM	F
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1972	3	11	0	PM	F
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1972	4	5	0	PM	F
1972	4	6	0	PM	F
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1972	4	8	0	PM	F
1972	4	9	0	PM	F
1972	4	10	0	PM	F
1972	4	11	0	PM	F
1972	4	12	0.69	PM	F
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1972	4	14	0.04	PM	F
1972	4	15	0	PM	F
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1972	4	23	0	PM	F
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1972	4	26	0	PM	F
1972	4	27	0	PM	F
1972	4	28	0.12	PM	F

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1972	5	3	0	PM	F
1972	5	4	0	PM	F
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1972	5	11	0	PM	F
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1972	5	25	0	PM	F
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1972	5	31	0	PM	F
1972	6	1	0	PM	F
1972	6	2	0	PM	F
1972	6	3	0	PM	F
1972	6	4	0	PM	F
1972	6	5	0	PM	F
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1972	6	7	0	PM	F
1972	6	8	0.5	PM	F
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1972	6	11	0	PM	F
1972	6	12	0	PM	F
1972	6	13	0.06	PM	F
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1972	6	16	0	PM	F
1972	6	17	0	PM	F
1972	6	18	0	PM	F
1972	6	19	0	PM	F
1972	6	20	0.07	PM	F
1972	6	21	0.06	PM	F
1972	6	22	0	PM	F
1972	6	23	0	PM	F
1972	6	24	0	PM	F
1972	6	25	0	PM	F
1972	6	26	0	PM	F
1972	6	27	0	PM	F
1972	6	28	1.17	PM	F
1972	6	29	0.12	PM	F
1972	6	30	0	PM	F
1972	7	1	0	PM	F
1972	7	2	0.65	PM	F
1972	7	3	0.17	PM	F
1972	7	4	0	PM	F
1972	7	5	0	PM	F
1972	7	6	0	PM	F
1972	7	7	0.31	PM	F
1972	7	8	0	PM	F
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1972	7	10	0	PM	F
1972	7	11	0	PM	F
1972	7	12	0	PM	F
1972	7	13	0	PM	F
1972	7	14	0	PM	F
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1972	7	16	0	PM	F
1972	7	17	0	PM	F
1972	7	18	0.21	PM	F
1972	7	19	T	PM	F
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1972	7	21	0	PM	F
1972	7	22	0	PM	F
1972	7	23	0	PM	F
1972	7	24	0	PM	F
1972	7	25	0	PM	F
1972	7	26	0.03	PM	F
1972	7	27	0	PM	F
1972	7	28	0	PM	F
1972	7	29	0	PM	F
1972	7	30	0	PM	F
1972	7	31	0	PM	F
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1972	8	7	0.02	PM	F
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1972	8	12	0.79	PM	F
1972	8	13	0	PM	F
1972	8	14	0	PM	F
1972	8	15	0.16	PM	F
1972	8	16	0	PM	F
1972	8	17	0	PM	F
1972	8	18	0	PM	F
1972	8	19	0	PM	F
1972	8	20	0	PM	F
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1972	9	23		0.67 PM	F
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1972	9	25		0.45 PM	F
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1972	10	5		0.05 PM	F
1972	10	6		0.1 PM	F
1972	10	7		0.04 PM	F
1972	10	8		0 PM	F
1972	10	9		0 PM	F
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1972	10	19		0 PM	F
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1972	10	21		0.46 PM	F
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1972	10	23		0.16 PM	F
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1972	11	15		0 PM	F
1972	11	16		0 PM	F
1972	11	17		0 PM	F
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1972	11	24		0 PM	F
1972	11	25		0.04 PM	F
1972	11	26		0.02 PM	F
1972	11	27		0.23 PM	F
1972	11	28		0 PM	F
1972	11	29		0 PM	F
1972	11	30		0 PM	F
1972	12	1		0 PM	F
1972	12	2		0 PM	F
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1972	12	9	T	PM	F
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1972	12	11		0 PM	F
1972	12	12		1.82 PM	F
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1972	12	14		0 PM	F

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1972	12	16		0 PM	F
1972	12	17		0 PM	F
1972	12	18		0 PM	F
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1973	1	14		0 PM	F
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1973	1	18		0.29 PM	F
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1973	1	20	T	PM	F
1973	1	21	T	PM	F
1973	1	22		0.06 PM	F
1973	1	23		0.03 PM	F
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1973	1	26		0 PM	F
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1973	1	30		0 PM	F
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1973	2	2		0.05 PM	F
1973	2	3		0 PM	F
1973	2	4		0 PM	F
1973	2	5		0 PM	F
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1973	2	9		0 PM	F
1973	2	10		0 PM	F
1973	2	11		0 PM	F
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1973	2	13		0.15 PM	F
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1973	2	18		0.01 PM	F
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1973	3	1	T	PM	F
1973	3	2		0.07 PM	F
1973	3	3		0.02 PM	F
1973	3	4		0.03 PM	F
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1973	3	7		1.27 PM	F
1973	3	8		0 PM	F
1973	3	9		0.31 PM	F
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1973	3	11		2.01 PM	F
1973	3	12		0 PM	F
1973	3	13		0 PM	F
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1973	3	15		0 PM	F
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1973	3	22		0 PM	F
1973	3	23		0 PM	F
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1973	3	30		0 PM	F
1973	3	31		0.42 PM	F
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1973	4	2		0.2 PM	F
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1973	4	4		0.03 PM	F
1973	4	5		0 PM	F
1973	4	6		0 PM	F
1973	4	7		0 PM	F
1973	4	8		0 PM	F

1973	4	9		0.85 PM	F
1973	4	10		0.1 PM	F
1973	4	11		0 PM	F
1973	4	12		0.03 PM	F
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1973	4	16		0.58 PM	F
1973	4	17		0 PM	F
1973	4	18		0.02 PM	F
1973	4	19		0.17 PM	F
1973	4	20		0.07 PM	F
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1973	4	24		0 PM	F
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1973	5	4		0 PM	F
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1973	5	6		0.27 PM	F
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1973	5	10		0 PM	F
1973	5	11		0 PM	F
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1973	5	25		0.04 PM	F
1973	5	26		0.4 PM	F
1973	5	27		0.65 PM	F
1973	5	28		0.15 PM	F
1973	5	29		0.15 PM	F
1973	5	30		0.06 PM	F
1973	5	31		0 PM	F
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1973	6	2		0.6 PM	F
1973	6	3		0.45 PM	F
1973	6	4		1.52 PM	F
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1973	6	8		0 PM	F
1973	6	9		0 PM	F
1973	6	10		0 PM	F
1973	6	11		0 PM	F
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1973	6	14		0 PM	F
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1973	6	16		0 PM	F
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1973	6	21		0 PM	F
1973	6	22		0 PM	F
1973	6	23		0 PM	F
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1973	6	26		0.72 PM	F
1973	6	27		0 PM	F
1973	6	28		0 PM	F
1973	6	29		0 PM	F
1973	6	30		0 PM	F
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1973	7	6		0 PM	F
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1973	7	16		0 PM	F
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1973	7	20		1.67 PM	F
1973	7	21		1.02 PM	F
1973	7	22		0.1 PM	F
1973	7	23		0.2 PM	F
1973	7	24		0.13 PM	F
1973	7	25		0.08 PM	F
1973	7	26		0.08 PM	F
1973	7	27		0 PM	F
1973	7	28		0 PM	F
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1973	8	2	0	PM	F
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1973	8	4	0	PM	F
1973	8	5	0	PM	F
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1973	8	7	0	PM	F
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1973	8	10	0	PM	F
1973	8	11	0	PM	F
1973	8	12	0.92	PM	F
1973	8	13	0.82	PM	F
1973	8	14	0.18	PM	F
1973	8	15	0	PM	F
1973	8	16	0	PM	F
1973	8	17	0	PM	F
1973	8	18	0	PM	F
1973	8	19	0	PM	F
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1973	8	26	0	PM	F
1973	8	27	0	PM	F
1973	8	28	0	PM	F
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1973	8	31	0	PM	F
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1973	9	11	0	PM	F
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1973	9	13	0	PM	F
1973	9	14	0.32	PM	F
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1973	10	8	0	PM	F
1973	10	9	0	PM	F
1973	10	10	0	PM	F
1973	10	11	0	PM	F
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1973	10	14	0	PM	F
1973	10	15	0	PM	F
1973	10	16	0	PM	F
1973	10	17	0	PM	F
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1973	10	25	0	PM	F
1973	10	26	0	PM	F
1973	10	27	0.45	PM	F
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1973	11	1	0	PM	F
1973	11	2	0	PM	F
1973	11	3	0	PM	F
1973	11	4	0	PM	F
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1973	11	6	0	PM	F
1973	11	7	0	PM	F
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1973	11	10	0	PM	F
1973	11	11	0	PM	F
1973	11	12	0	PM	F
1973	11	13	0	PM	F
1973	11	14	0	PM	F
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1973	11	16	0	PM	F
1973	11	17	0	PM	F
1973	11	18	T	PM	F
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1973	11	20	0	PM	F
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1973	11	22	0	PM	F
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1973	11	24	0.38	PM	F

1973	11	25	0.55	PM	F
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1973	11	27	0	PM	F
1973	11	28	0.38	PM	F
1973	11	29	0	PM	F
1973	11	30	0	PM	F
1973	12	1	0	PM	F
1973	12	2	0	PM	F
1973	12	3	0	PM	F
1973	12	4	1.11	PM	F
1973	12	5	0.17	PM	F
1973	12	6	0	PM	F
1973	12	7	0	PM	F
1973	12	8	0	PM	F
1973	12	9	0.02	PM	F
1973	12	10	0	PM	F
1973	12	11	0	PM	F
1973	12	12	0	PM	F
1973	12	13	0.1	PM	F
1973	12	14	T	PM	F
1973	12	15	0.13	PM	F
1973	12	16	0	PM	F
1973	12	17	0	PM	F
1973	12	18	0.09	PM	F
1973	12	19	0.67	PM	F
1973	12	20	0.48	PM	F
1973	12	21	0	PM	F
1973	12	22	0	PM	F
1973	12	23	0	PM	F
1973	12	24	0.13	PM	F
1973	12	25	0	PM	F
1973	12	26	0.08	PM	F
1973	12	27	T	PM	F
1973	12	28	T	PM	F
1973	12	29	0.06	PM	F
1973	12	30	0	PM	F
1973	12	31	0.26	PM	F
1974	1	1	0	PM	F
1974	1	2	0	PM	F
1974	1	3	0	PM	F
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1974	1	5	0	PM	F
1974	1	6	0	PM	F
1974	1	7	0	PM	F
1974	1	8	0.06	PM	F
1974	1	9	0.29	PM	F
1974	1	10	0.2	PM	F
1974	1	11	0	PM	F
1974	1	12	0	PM	F
1974	1	13	0	PM	F
1974	1	14	0	PM	F
1974	1	15	0	PM	F
1974	1	16	0	PM	F
1974	1	17	0	PM	F
1974	1	18	0.02	PM	F
1974	1	19	0.15	PM	F
1974	1	20	1	PM	F
1974	1	21	0.06	PM	F
1974	1	22	0.28	PM	F
1974	1	23	0	PM	F
1974	1	24	0	PM	F
1974	1	25	0.05	PM	F
1974	1	26	0.15	PM	F
1974	1	27	0.63	PM	F
1974	1	28	0.32	PM	F
1974	1	29	0	PM	F
1974	1	30	0	PM	F
1974	1	31	0	PM	F
1974	2	1	0	PM	F
1974	2	2	0	PM	F
1974	2	3	0	PM	F
1974	2	4	0	PM	F
1974	2	5	0	PM	F
1974	2	6	0.46	PM	F
1974	2	7	0	PM	F
1974	2	8	0.01	PM	F
1974	2	9	0	PM	F
1974	2	10	T	PM	F
1974	2	11	0	PM	F
1974	2	12	0	PM	F
1974	2	13	0	PM	F
1974	2	14	0	PM	F
1974	2	15	0	PM	F
1974	2	16	0	PM	F
1974	2	17	0	PM	F
1974	2	18	0.25	PM	F
1974	2	19	0.37	PM	F
1974	2	20	0	PM	F
1974	2	21	0.33	PM	F
1974	2	22	0.04	PM	F
1974	2	23	0	PM	F
1974	2	24	0.22	PM	F
1974	2	25	0	PM	F
1974	2	26	0	PM	F
1974	2	27	0	PM	F
1974	2	28	0	PM	F
1974	3	1	0	PM	F
1974	3	2	0	PM	F
1974	3	3	0	PM	F
1974	3	4	0.6	PM	F
1974	3	5	0.2	PM	F
1974	3	6	0	PM	F
1974	3	7	0	PM	F
1974	3	8	0	PM	F
1974	3	9	0.49	PM	F
1974	3	10	0	PM	F
1974	3	11	0.85	PM	F
1974	3	12	0.53	PM	F
1974	3	13	0	PM	F
1974	3	14	0	PM	F
1974	3	15	0.4	PM	F
1974	3	16	0	PM	F
1974	3	17	0	PM	F
1974	3	18	0	PM	F
1974	3	19	0	PM	F

1974	3	20		0 PM	F
1974	3	21		0.15 PM	F
1974	3	22		0 PM	F
1974	3	23		0.14 PM	F
1974	3	24		0 PM	F
1974	3	25		0 PM	F
1974	3	26		0 PM	F
1974	3	27		0 PM	F
1974	3	28		0 PM	F
1974	3	29		0.18 PM	F
1974	3	30		0.67 PM	F
1974	3	31		0 PM	F
1974	4	1		0 PM	F
1974	4	2		0 PM	F
1974	4	3		0.35 PM	F
1974	4	4		0.12 PM	F
1974	4	5		0.1 PM	F
1974	4	6		0 PM	F
1974	4	7		0.12 PM	F
1974	4	8		0.58 PM	F
1974	4	9		0 PM	F
1974	4	10		0 PM	F
1974	4	11		0.25 PM	F
1974	4	12		0.18 PM	F
1974	4	13		0.08 PM	F
1974	4	14	T	PM	F
1974	4	15		0 PM	F
1974	4	16		0 PM	F
1974	4	17		0 PM	F
1974	4	18		0 PM	F
1974	4	19		0.05 PM	F
1974	4	20		0 PM	F
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1974	4	24		0 PM	F
1974	4	25		0 PM	F
1974	4	26		0 PM	F
1974	4	27		0 PM	F
1974	4	28		0.11 PM	F
1974	4	29		0.28 PM	F
1974	4	30		0.04 PM	F
1974	5	1		0 PM	F
1974	5	2		0.23 PM	F
1974	5	3		0 PM	F
1974	5	4		0 PM	F
1974	5	5		0 PM	F
1974	5	6		0 PM	F
1974	5	7		0.03 PM	F
1974	5	8		0.77 PM	F
1974	5	9		0 PM	F
1974	5	10		0 PM	F
1974	5	11		0.11 PM	F
1974	5	12		0 PM	F
1974	5	13		0.19 PM	F
1974	5	14		0.73 PM	F
1974	5	15		0 PM	F
1974	5	16		0 PM	F
1974	5	17		1.01 PM	F
1974	5	18		0.05 PM	F
1974	5	19		0.83 PM	F
1974	5	20		0.55 PM	F
1974	5	21		0.03 PM	F
1974	5	22		0.43 PM	F
1974	5	23		0 PM	F
1974	5	24		0.55 PM	F
1974	5	25		0 PM	F
1974	5	26		0 PM	F
1974	5	27		0 PM	F
1974	5	28	T	PM	F
1974	5	29		0.52 PM	F
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1974	6	1		0 PM	F
1974	6	2		0 PM	F
1974	6	3		0 PM	F
1974	6	4		0 PM	F
1974	6	5		0.22 PM	F
1974	6	6		0.78 PM	F
1974	6	7		0.08 PM	F
1974	6	8		0.07 PM	F
1974	6	9		0 PM	F
1974	6	10		0.12 PM	F
1974	6	11		0.05 PM	F
1974	6	12		0.05 PM	F
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1974	6	14		0.63 PM	F
1974	6	15		0.1 PM	F
1974	6	16		0 PM	F
1974	6	17		0 PM	F
1974	6	18		0 PM	F
1974	6	19		0.66 PM	F
1974	6	20		0.58 PM	F
1974	6	21		1 PM	F
1974	6	22		3.08 PM	F
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1974	6	30		0 PM	F
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1974	7	3		0 PM	F
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1974	7	5		0 PM	F
1974	7	6		0 PM	F
1974	7	7		0 PM	F
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1974	7	9		0.13 PM	F
1974	7	10		0.2 PM	F
1974	7	11		0.24 PM	F
1974	7	12		0 PM	F

1974	7	13	0	PM	F
1974	7	14	0	PM	F
1974	7	15	0	PM	F
1974	7	16	0	PM	F
1974	7	17	0	PM	F
1974	7	18	0	PM	F
1974	7	19	0	PM	F
1974	7	20	0	PM	F
1974	7	21	0	PM	F
1974	7	22	0.95	PM	F
1974	7	23	0	PM	F
1974	7	24	0	PM	F
1974	7	25	0	PM	F
1974	7	26	0	PM	F
1974	7	27	0	PM	F
1974	7	28	0.42	PM	F
1974	7	29	0	PM	F
1974	7	30	0	PM	F
1974	7	31	0	PM	F
1974	8	1	0	PM	F
1974	8	2	0.9	PM	F
1974	8	3	0	PM	F
1974	8	4	0	PM	F
1974	8	5	0	PM	F
1974	8	6	0	PM	F
1974	8	7	0	PM	F
1974	8	8	0	PM	F
1974	8	9	0	PM	F
1974	8	10	1.2	PM	F
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1974	8	13	0	PM	F
1974	8	14	0	PM	F
1974	8	15	0	PM	F
1974	8	16	0	PM	F
1974	8	17	0	PM	F
1974	8	18	0	PM	F
1974	8	19	0	PM	F
1974	8	20	0	PM	F
1974	8	21	0	PM	F
1974	8	22	T	PM	F
1974	8	23	0.02	PM	F
1974	8	24	0	PM	F
1974	8	25	0	PM	F
1974	8	26	0	PM	F
1974	8	27	0	PM	F
1974	8	28	0.53	PM	F
1974	8	29	0	PM	F
1974	8	30	0	PM	F
1974	8	31	0	PM	F
1974	9	1	0.15	PM	F
1974	9	2	0.11	PM	F
1974	9	3	0.2	PM	F
1974	9	4	0	PM	F
1974	9	5	0	PM	F
1974	9	6	0	PM	F
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1974	9	8	0	PM	F
1974	9	9	0	PM	F
1974	9	10	0	PM	F
1974	9	11	0.48	PM	F
1974	9	12	0.18	PM	F
1974	9	13	0.56	PM	F
1974	9	14	0	PM	F
1974	9	15	0	PM	F
1974	9	16	0	PM	F
1974	9	17	0	PM	F
1974	9	18	0	PM	F
1974	9	19	0	PM	F
1974	9	20	0	PM	F
1974	9	21	0	PM	F
1974	9	22	0	PM	F
1974	9	23	0	PM	F
1974	9	24	0	PM	F
1974	9	25	0	PM	F
1974	9	26	0	PM	F
1974	9	27	0	PM	F
1974	9	28	T	PM	F
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1974	10	5	0	PM	F
1974	10	6	0	PM	F
1974	10	7	0	PM	F
1974	10	8	0	PM	F
1974	10	9	0	PM	F
1974	10	10	0	PM	F
1974	10	11	0	PM	F
1974	10	12	0.02	PM	F
1974	10	13	0.31	PM	F
1974	10	14	0.66	PM	F
1974	10	15	0	PM	F
1974	10	16	0	PM	F
1974	10	17	0	PM	F
1974	10	18	0.1	PM	F
1974	10	19	0	PM	F
1974	10	20	0	PM	F
1974	10	21	0	PM	F
1974	10	22	0	PM	F
1974	10	23	T	PM	F
1974	10	24	0	PM	F
1974	10	25	0.27	PM	F
1974	10	26	0	PM	F
1974	10	27	0	PM	F
1974	10	28	0	PM	F
1974	10	29	0.4	PM	F
1974	10	30	0	PM	F
1974	10	31	0	PM	F
1974	11	1	0.02	PM	F
1974	11	2	0	PM	F
1974	11	3	1.1	PM	F
1974	11	4	0.36	PM	F

1974	11	5		0.28 PM	F
1974	11	6		0 PM	F
1974	11	7		0 PM	F
1974	11	8		0 PM	F
1974	11	9		0 PM	F
1974	11	10		1.1 PM	F
1974	11	11		0.28 PM	F
1974	11	12		0 PM	F
1974	11	13		0.55 PM	F
1974	11	14		0.15 PM	F
1974	11	15		0 PM	F
1974	11	16		0 PM	F
1974	11	17		0 PM	F
1974	11	18		0 PM	F
1974	11	19		0 PM	F
1974	11	20		0 PM	F
1974	11	21		0 PM	F
1974	11	22		0 PM	F
1974	11	23		0 PM	F
1974	11	24		0 PM	F
1974	11	25		0 PM	F
1974	11	26		0 PM	F
1974	11	27		0 PM	F
1974	11	28		0 PM	F
1974	11	29		0 PM	F
1974	11	30		0.15 PM	F
1974	12	1		0.29 PM	F
1974	12	2		0 PM	F
1974	12	3		0 PM	F
1974	12	4		0 PM	F
1974	12	5		0 PM	F
1974	12	6		0 PM	F
1974	12	7		0.28 PM	F
1974	12	8		0.03 PM	F
1974	12	9		0 PM	F
1974	12	10		0 PM	F
1974	12	11		0.07 PM	F
1974	12	12		0.12 PM	F
1974	12	13		0 PM	F
1974	12	14		0 PM	F
1974	12	15		0.2 PM	F
1974	12	16	T	PM	F
1974	12	17	T	PM	F
1974	12	18		0 PM	F
1974	12	19		0.21 PM	F
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1974	12	21		0 PM	F
1974	12	22		0 PM	F
1974	12	23		0.2 PM	F
1974	12	24		0.21 PM	F
1974	12	25		0 PM	F
1974	12	26		0 PM	F
1974	12	27	T	PM	F
1974	12	28		0 PM	F
1974	12	29		0.02 PM	F
1974	12	30		0.11 PM	F
1974	12	31		0.1 PM	F
1975	1	1		0 PM	F
1975	1	2		0 PM	F
1975	1	3		0.16 PM	F
1975	1	4		0 PM	F
1975	1	5		0 PM	F
1975	1	6		0.15 PM	F
1975	1	7		0 PM	F
1975	1	8		0.04 PM	F
1975	1	9		0 PM	F
1975	1	10		2.75 PM	F
1975	1	11		0.14 PM	F
1975	1	12		0 PM	F
1975	1	13		0 PM	F
1975	1	14		0 PM	F
1975	1	15		0.06 PM	F
1975	1	16		0 PM	F
1975	1	17		0.07 PM	F
1975	1	18		0 PM	F
1975	1	19		0.27 PM	F
1975	1	20		0 PM	F
1975	1	21		0 PM	F
1975	1	22		0 PM	F
1975	1	23		0 PM	F
1975	1	24		0.12 PM	F
1975	1	25		0.37 PM	F
1975	1	26		0 PM	F
1975	1	27		0 PM	F
1975	1	28		0 PM	F
1975	1	29		0.47 PM	F
1975	1	30	T	PM	F
1975	1	31		0.15 PM	F
1975	2	1		0 PM	F
1975	2	2		0 PM	F
1975	2	3		0 PM	F
1975	2	4		0.05 PM	F
1975	2	5		0.1 PM	F
1975	2	6		0.06 PM	F
1975	2	7		0 PM	F
1975	2	8		0.07 PM	F
1975	2	9		0.12 PM	F
1975	2	10		0 PM	F
1975	2	11		0 PM	F
1975	2	12		0.83 PM	F
1975	2	13		0 PM	F
1975	2	14		0 PM	F
1975	2	15		0.06 PM	F
1975	2	16		0 PM	F
1975	2	17		0.15 PM	F
1975	2	18		0.03 PM	F
1975	2	19		0 PM	F
1975	2	20		0 PM	F
1975	2	21		0.05 PM	F
1975	2	22		0.88 PM	F
1975	2	23		0.55 PM	F
1975	2	24		0.28 PM	F
1975	2	25		0.06 PM	F
1975	2	26		0 PM	F
1975	2	27		0 PM	F

1975	2	28	0	PM	F
1975	3	1	0	PM	F
1975	3	2	0	PM	F
1975	3	3	0	PM	F
1975	3	4	0	PM	F
1975	3	5	0	PM	F
1975	3	6	0	PM	F
1975	3	7	0.18	PM	F
1975	3	8	0	PM	F
1975	3	9	0	PM	F
1975	3	10	0.2	PM	F
1975	3	11	0	PM	F
1975	3	12	0.02	PM	F
1975	3	13	0	PM	F
1975	3	14	0	PM	F
1975	3	15	0	PM	F
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1975	3	17	0	PM	F
1975	3	18	0	PM	F
1975	3	19	0	PM	F
1975	3	20	0	PM	F
1975	3	21	0	PM	F
1975	3	22	0	PM	F
1975	3	23	0	PM	F
1975	3	24	0	PM	F
1975	3	25	0.03	PM	F
1975	3	26	0	PM	F
1975	3	27	0.44	PM	F
1975	3	28	0.59	PM	F
1975	3	29	0.29	PM	F
1975	3	30	0	PM	F
1975	3	31	0	PM	F
1975	4	1	0	PM	F
1975	4	2	0.08	PM	F
1975	4	3	0.36	PM	F
1975	4	4	0	PM	F
1975	4	5	0	PM	F
1975	4	6	0	PM	F
1975	4	7	0	PM	F
1975	4	8	0	PM	F
1975	4	9	0.08	PM	F
1975	4	10	0	PM	F
1975	4	11	0	PM	F
1975	4	12	0	PM	F
1975	4	13	0	PM	F
1975	4	14	0.12	PM	F
1975	4	15	0	PM	F
1975	4	16	0	PM	F
1975	4	17	0	PM	F
1975	4	18	0.09	PM	F
1975	4	19	0.15	PM	F
1975	4	20	0	PM	F
1975	4	21	0	PM	F
1975	4	22	0	PM	F
1975	4	23	0.65	PM	F
1975	4	24	1.15	PM	F
1975	4	25	0.07	PM	F
1975	4	26	0	PM	F
1975	4	27	0.28	PM	F
1975	4	28	0	PM	F
1975	4	29	0	PM	F
1975	4	30	0.31	PM	F
1975	5	1	0.3	PM	F
1975	5	2	0	PM	F
1975	5	3	0	PM	F
1975	5	4	0	PM	F
1975	5	5	0	PM	F
1975	5	6	0	PM	F
1975	5	7	0	PM	F
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1975	5	11	0	PM	F
1975	5	12	0	PM	F
1975	5	13	0	PM	F
1975	5	14	0	PM	F
1975	5	15	0	PM	F
1975	5	16	0	PM	F
1975	5	17	0	PM	F
1975	5	18	0	PM	F
1975	5	19	0	PM	F
1975	5	20	0.05	PM	F
1975	5	21	0.1	PM	F
1975	5	22	0	PM	F
1975	5	23	0	PM	F
1975	5	24	0.05	PM	F
1975	5	25	0.1	PM	F
1975	5	26	0.34	PM	F
1975	5	27	0	PM	F
1975	5	28	0	PM	F
1975	5	29	0.13	PM	F
1975	5	30	0.5	PM	F
1975	5	31	0	PM	F
1975	6	1	0.15	PM	F
1975	6	2	0	PM	F
1975	6	3	0.04	PM	F
1975	6	4	0	PM	F
1975	6	5	0.72	PM	F
1975	6	6	0	PM	F
1975	6	7	0	PM	F
1975	6	8	0	PM	F
1975	6	9	0	PM	F
1975	6	10	0	PM	F
1975	6	11	0	PM	F
1975	6	12	0	PM	F
1975	6	13	0.02	PM	F
1975	6	14	0.55	PM	F
1975	6	15	2.25	PM	F
1975	6	16	0	PM	F
1975	6	17	0.07	PM	F
1975	6	18	0	PM	F
1975	6	19	0	PM	F
1975	6	20	0	PM	F
1975	6	21	0.2	PM	F
1975	6	22	0	PM	F

1975	6	23	0.65	PM	F
1975	6	24	0	PM	F
1975	6	25	0.65	PM	F
1975	6	26	0.61	PM	F
1975	6	27	0	PM	F
1975	6	28	0	PM	F
1975	6	29	0	PM	F
1975	6	30	0	PM	F
1975	7	1	0	PM	F
1975	7	2	0	PM	F
1975	7	3	0	PM	F
1975	7	4	0	PM	F
1975	7	5	0.61	PM	F
1975	7	6	0.27	PM	F
1975	7	7	0.4	PM	F
1975	7	8	0	PM	F
1975	7	9	0.84	PM	F
1975	7	10	0.11	PM	F
1975	7	11	0	PM	F
1975	7	12	0	PM	F
1975	7	13	0	PM	F
1975	7	14	0	PM	F
1975	7	15	0	PM	F
1975	7	16	0	PM	F
1975	7	17	0	PM	F
1975	7	18	0	PM	F
1975	7	19	2	PM	F
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1975	7	22	0	PM	F
1975	7	23	1	PM	F
1975	7	24	0	PM	F
1975	7	25	0	PM	F
1975	7	26	0	PM	F
1975	7	27	0	PM	F
1975	7	28	0	PM	F
1975	7	29	0	PM	F
1975	7	30	0	PM	F
1975	7	31	0	PM	F
1975	8	1	0.12	PM	F
1975	8	2	0.45	PM	F
1975	8	3	0	PM	F
1975	8	4	0	PM	F
1975	8	5	0.73	PM	F
1975	8	6	0	PM	F
1975	8	7	0	PM	F
1975	8	8	0	PM	F
1975	8	9	0	PM	F
1975	8	10	0	PM	F
1975	8	11	0.32	PM	F
1975	8	12	0	PM	F
1975	8	13	0.12	PM	F
1975	8	14	0.26	PM	F
1975	8	15	1.5	PM	F
1975	8	16	0	PM	F
1975	8	17	0	PM	F
1975	8	18	0	PM	F
1975	8	19	1.35	PM	F
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1975	8	22	0	PM	F
1975	8	23	0	PM	F
1975	8	24	0	PM	F
1975	8	25	0	PM	F
1975	8	26	3.33	PM	F
1975	8	27	0	PM	F
1975	8	28	0	PM	F
1975	8	29	0.9	PM	F
1975	8	30	0.64	PM	F
1975	8	31	0	PM	F
1975	9	1	0	PM	F
1975	9	2	0	PM	F
1975	9	3	0	PM	F
1975	9	4	0.52	PM	F
1975	9	5	0.15	PM	F
1975	9	6	0	PM	F
1975	9	7	0	PM	F
1975	9	8	0	PM	F
1975	9	9	0	PM	F
1975	9	10	0	PM	F
1975	9	11	0.15	PM	F
1975	9	12	0.58	PM	F
1975	9	13	0	PM	F
1975	9	14	0	PM	F
1975	9	15	0	PM	F
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1975	10	10	0	PM	F
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1975	10	13	0	PM	F
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1975	10	15	0.08	PM	F

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1975	11	2	0.12 PM	F
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1975	11	6	0 PM	F
1975	11	7	0.07 PM	F
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1975	11	22	0 PM	F
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1975	12	11	0 PM	F
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1975	12	22	0 PM	F
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1975	12	24	0 PM	F
1975	12	25	0.11 PM	F
1975	12	26	0.03 PM	F
1975	12	27	0 PM	F
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1976	1	2	0.13 PM	F
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1976	1	4	0 PM	F
1976	1	5	0 PM	F
1976	1	6	0 PM	F
1976	1	7	0.25 PM	F
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1976	1	9	0 PM	F
1976	1	10	0 PM	F
1976	1	11	0 PM	F
1976	1	12	0 PM	F
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1976	1	28	0 PM	F
1976	1	29	0 PM	F
1976	1	30	0 PM	F
1976	1	31	0 PM	F
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1976	2	2	0 PM	F
1976	2	3	0 PM	F
1976	2	4	0 PM	F
1976	2	5	0.2 PM	F
1976	2	6	0.29 PM	F
1976	2	7	0 PM	F

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1976	2	11	0	PM	F
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1976	2	26	0	PM	F
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1976	2	28	0	PM	F
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1976	3	2	0.08	PM	F
1976	3	3	0.07	PM	F
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1976	3	12	0.37	PM	F
1976	3	13	T	PM	F
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1976	3	15	0	PM	F
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1976	3	17	0	PM	F
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1976	3	21	0	PM	F
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1976	3	26	0	PM	F
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1976	3	31	0	PM	F
1976	4	1	0	PM	F
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1976	4	3	0	PM	F
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1976	4	30	0	PM	F
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1976	5	3	0	PM	F
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1976	5	10	0	PM	F
1976	5	11	0	PM	F
1976	5	12	0	PM	F
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1976	5	15	0.35	PM	F
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1976	5	25	0	PM	F
1976	5	26	0	PM	F
1976	5	27	0	PM	F
1976	5	28	0.14	PM	F
1976	5	29	0.21	PM	F
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1976	5	31	0.05	PM	F
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1976	6	2	0	PM	F
1976	6	3	0	PM	F
1976	6	4	0	PM	F
1976	6	5	0	PM	F
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1976	6	11	0	PM	F
1976	6	12	0.02	PM	F
1976	6	13	0	PM	F
1976	6	14	0	PM	F
1976	6	15	0.08	PM	F
1976	6	16	0	PM	F
1976	6	17	0	PM	F
1976	6	18	0	PM	F
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1976	6	20	0	PM	F
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1976	6	27	0	PM	F
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1976	7	4	0	PM	F
1976	7	5	0	PM	F
1976	7	6	0	PM	F
1976	7	7	0.3	PM	F
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1976	7	11	0	PM	F
1976	7	12	0	PM	F
1976	7	13	0	PM	F
1976	7	14	0	PM	F
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1976	7	16	0	PM	F
1976	7	17	0	PM	F
1976	7	18	0	PM	F
1976	7	19	0	PM	F
1976	7	20	0	PM	F
1976	7	21	0.54	PM	F
1976	7	22	0.51	PM	F
1976	7	23	0	PM	F
1976	7	24	0	PM	F
1976	7	25	0	PM	F
1976	7	26	0	PM	F
1976	7	27	0.71	PM	F
1976	7	28	0.44	PM	F
1976	7	29	0	PM	F
1976	7	30	0	PM	F
1976	7	31	0	PM	F
1976	8	1	0	PM	F
1976	8	2	0	PM	F
1976	8	3	0	PM	F
1976	8	4	0	PM	F
1976	8	5	0.04	PM	F
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1976	8	7	0.14	PM	F
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1976	8	11	0	PM	F
1976	8	12	0	PM	F
1976	8	13	0	PM	F
1976	8	14	0	PM	F
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1976	9	23	0	PM	F
1976	9	24	0	PM	F

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1976	11	28		0 PM	F
1976	11	29		0 PM	F
1976	11	30		0 PM	F
1976	12	1	T	PM	F
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1977	1	1		0 PM	F
1977	1	2	T	PM	F
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1977	1	10		0.35 PM	F
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1977	1	16		0 PM	F
1977	1	17		0 PM	F

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1977	1	19	T	PM	F
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1977	2	19		0.16 PM	F
1977	2	20		0 PM	F
1977	2	21		0 PM	F
1977	2	22	T	PM	F
1977	2	23		0 PM	F
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1977	3	22	M	-	F
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1977	3	29		1.56 PM	F
1977	3	30		0 PM	F
1977	3	31		0 PM	F
1977	4	1		0 PM	F
1977	4	2		0.8 PM	F
1977	4	3		0 PM	F
1977	4	4		0.08 PM	F
1977	4	5		0.23 PM	F
1977	4	6		0 PM	F
1977	4	7		0.02 PM	F
1977	4	8		0 PM	F
1977	4	9		0 PM	F
1977	4	10		0 PM	F
1977	4	11		0 PM	F
1977	4	12		0 PM	F
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1977	4	16		0 PM	F
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1977	4	21		0.66 PM	F
1977	4	22		0.01 PM	F
1977	4	23		0.46 PM	F
1977	4	24		0 PM	F
1977	4	25		0 PM	F
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1977	5	10		0 PM	F
1977	5	11		0 PM	F
1977	5	12		0 PM	F

1977	5	13	0	PM	F
1977	5	14	0	PM	F
1977	5	15	0	PM	F
1977	5	16	0	PM	F
1977	5	17	0	PM	F
1977	5	18	0	PM	F
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1977	5	22	0	PM	F
1977	5	23	0	PM	F
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1977	5	25	T	PM	F
1977	5	26	0	PM	F
1977	5	27	0	PM	F
1977	5	28	0.02	PM	F
1977	5	29	0.22	PM	F
1977	5	30	0	PM	F
1977	5	31	0	PM	F
1977	6	1	0	PM	F
1977	6	2	0	PM	F
1977	6	3	0	PM	F
1977	6	4	0	PM	F
1977	6	5	0	PM	F
1977	6	6	0	PM	F
1977	6	7	0	PM	F
1977	6	8	0.32	PM	F
1977	6	9	0	PM	F
1977	6	10	0.23	PM	F
1977	6	11	0.31	PM	F
1977	6	12	0	PM	F
1977	6	13	0	PM	F
1977	6	14	0	PM	F
1977	6	15	0	PM	F
1977	6	16	0	PM	F
1977	6	17	0	PM	F
1977	6	18	0	PM	F
1977	6	19	0	PM	F
1977	6	20	0	PM	F
1977	6	21	0	PM	F
1977	6	22	0.15	PM	F
1977	6	23	0.15	PM	F
1977	6	24	0.18	PM	F
1977	6	25	0	PM	F
1977	6	26	0.59	PM	F
1977	6	27	0.83	PM	F
1977	6	28	0	PM	F
1977	6	29	1.08	PM	F
1977	6	30	0	PM	F
1977	7	1	0.06	PM	F
1977	7	2	0	PM	F
1977	7	3	0	PM	F
1977	7	4	0	PM	F
1977	7	5	0	PM	F
1977	7	6	0	PM	F
1977	7	7	0	PM	F
1977	7	8	0.32	PM	F
1977	7	9	0	PM	F
1977	7	10	0	PM	F
1977	7	11	0	PM	F
1977	7	12	0.88	PM	F
1977	7	13	0	PM	F
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1977	7	15	0	PM	F
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1977	7	19	0	PM	F
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1977	7	24	0	PM	F
1977	7	25	0	PM	F
1977	7	26	0	PM	F
1977	7	27	0	PM	F
1977	7	28	0	PM	F
1977	7	29	0	PM	F
1977	7	30	1.1	PM	F
1977	7	31	0.93	PM	F
1977	8	1	0	PM	F
1977	8	2	0.09	PM	F
1977	8	3	0	PM	F
1977	8	4	0	PM	F
1977	8	5	0.56	PM	F
1977	8	6	2.32	PM	F
1977	8	7	1.77	PM	F
1977	8	8	0.44	PM	F
1977	8	9	0.55	PM	F
1977	8	10	0.05	PM	F
1977	8	11	0	PM	F
1977	8	12	0.32	PM	F
1977	8	13	0	PM	F
1977	8	14	0	PM	F
1977	8	15	0	PM	F
1977	8	16	0	PM	F
1977	8	17	0.6	PM	F
1977	8	18	0	PM	F
1977	8	19	0	PM	F
1977	8	20	0.01	PM	F
1977	8	21	0.15	PM	F
1977	8	22	0.46	PM	F
1977	8	23	T	PM	F
1977	8	24	0	PM	F
1977	8	25	0	PM	F
1977	8	26	0	PM	F
1977	8	27	0	PM	F
1977	8	28	0	PM	F
1977	8	29	0.55	PM	F
1977	8	30	0	PM	F
1977	8	31	0	PM	F
1977	9	1	T	PM	F
1977	9	2	0	PM	F
1977	9	3	0	PM	F
1977	9	4	0.05	PM	F

1977	9	5	T	PM	F
1977	9	6		0 PM	F
1977	9	7		0 PM	F
1977	9	8		0.1 PM	F
1977	9	9		0 PM	F
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1977	9	15		0 PM	F
1977	9	16		0 PM	F
1977	9	17		0.01 PM	F
1977	9	18		0.21 PM	F
1977	9	19		0.1 PM	F
1977	9	20		0 PM	F
1977	9	21		0 PM	F
1977	9	22		0 PM	F
1977	9	23		0 PM	F
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1977	9	25		0 PM	F
1977	9	26		0.04 PM	F
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1977	9	28		0 PM	F
1977	9	29		0 PM	F
1977	9	30		0 PM	F
1977	10	1		3.94 PM	F
1977	10	2		0.13 PM	F
1977	10	3		0 PM	F
1977	10	4	T	PM	F
1977	10	5		0.03 PM	F
1977	10	6	T	PM	F
1977	10	7		0 PM	F
1977	10	8		1.45 PM	F
1977	10	9	T	PM	F
1977	10	10		0 PM	F
1977	10	11		0.11 PM	F
1977	10	12		0.01 PM	F
1977	10	13		0 PM	F
1977	10	14		0 PM	F
1977	10	15		0 PM	F
1977	10	16	T	PM	F
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1977	10	18		0 PM	F
1977	10	19		0 PM	F
1977	10	20		0 PM	F
1977	10	21		0 PM	F
1977	10	22		0 PM	F
1977	10	23		0.86 PM	F
1977	10	24		0.09 PM	F
1977	10	25		0.93 PM	F
1977	10	26		0.07 PM	F
1977	10	27		0 PM	F
1977	10	28		0 PM	F
1977	10	29		0 PM	F
1977	10	30		0 PM	F
1977	10	31		0.17 PM	F
1977	11	1		0.11 PM	F
1977	11	2		0 PM	F
1977	11	3		0 PM	F
1977	11	4		0 PM	F
1977	11	5		0 PM	F
1977	11	6		0 PM	F
1977	11	7		0.13 PM	F
1977	11	8		0.35 PM	F
1977	11	9		0.07 PM	F
1977	11	10	T	PM	F
1977	11	11	T	PM	F
1977	11	12		0 PM	F
1977	11	13		0 PM	F
1977	11	14		0 PM	F
1977	11	15	T	PM	F
1977	11	16		0 PM	F
1977	11	17		0 PM	F
1977	11	18		0 PM	F
1977	11	19		0.05 PM	F
1977	11	20		0.05 PM	F
1977	11	21		0.05 PM	F
1977	11	22		0 PM	F
1977	11	23		0.02 PM	F
1977	11	24	T	PM	F
1977	11	25	T	PM	F
1977	11	26		0.04 PM	F
1977	11	27		0.26 PM	F
1977	11	28		0.04 PM	F
1977	11	29		0 PM	F
1977	11	30		0 PM	F
1977	12	1		1.06 PM	F
1977	12	2		0 PM	F
1977	12	3		0.4 PM	F
1977	12	4		0 PM	F
1977	12	5		0.3 PM	F
1977	12	6		0.47 PM	F
1977	12	7		0 PM	F
1977	12	8		0 PM	F
1977	12	9		0.33 PM	F
1977	12	10		0 PM	F
1977	12	11		0 PM	F
1977	12	12		0 PM	F
1977	12	13		0 PM	F
1977	12	14		0.07 PM	F
1977	12	15		0 PM	F
1977	12	16		0 PM	F
1977	12	17		0.02 PM	F
1977	12	18		0 PM	F
1977	12	19		0 PM	F
1977	12	20		0.19 PM	F
1977	12	21		0.03 PM	F
1977	12	22		0 PM	F
1977	12	23		0 PM	F
1977	12	24		0 PM	F
1977	12	25	T	PM	F
1977	12	26		0 PM	F
1977	12	27		0 PM	F
1977	12	28		0 PM	F

1977	12	29	T		PM	F
1977	12	30		0	PM	F
1977	12	31		0	PM	F
1978	1	1		0.02	PM	F
1978	1	2		0	PM	F
1978	1	3		0	PM	F
1978	1	4		0	PM	F
1978	1	5	T		PM	F
1978	1	6		0	PM	F
1978	1	7	T		PM	F
1978	1	8		0	PM	F
1978	1	9	T		PM	F
1978	1	10		0	PM	F
1978	1	11		0	PM	F
1978	1	12	T		PM	F
1978	1	13		0.12	PM	F
1978	1	14		0.1	PM	F
1978	1	15	T		PM	F
1978	1	16		0.08	PM	F
1978	1	17		0.12	PM	F
1978	1	18		0	PM	F
1978	1	19		0	PM	F
1978	1	20	T		PM	F
1978	1	21		0.01	PM	F
1978	1	22		0	PM	F
1978	1	23		0	PM	F
1978	1	24	T		PM	F
1978	1	25		0.03	PM	F
1978	1	26		0.04	PM	F
1978	1	27	T		PM	F
1978	1	28		0	PM	F
1978	1	29		0	PM	F
1978	1	30		0	PM	F
1978	1	31		0.03	PM	F
1978	2	1	T		PM	F
1978	2	2		0	PM	F
1978	2	3	T		PM	F
1978	2	4		0.02	PM	F
1978	2	5		0	PM	F
1978	2	6		0	PM	F
1978	2	7		0	PM	F
1978	2	8		0	PM	F
1978	2	9		0	PM	F
1978	2	10		0	PM	F
1978	2	11		0	PM	F
1978	2	12		0	PM	F
1978	2	13		0.12	PM	F
1978	2	14		0.22	PM	F
1978	2	15		0.09	PM	F
1978	2	16		0	PM	F
1978	2	17		0	PM	F
1978	2	18	T		PM	F
1978	2	19		0.02	PM	F
1978	2	20	T		PM	F
1978	2	21	T		PM	F
1978	2	22		0.02	PM	F
1978	2	23		0	PM	F
1978	2	24		0	PM	F
1978	2	25		0	PM	F
1978	2	26		0	PM	F
1978	2	27		0.06	PM	F
1978	2	28		0.04	PM	F
1978	3	1		0	PM	F
1978	3	2		0.04	PM	F
1978	3	3		0.14	PM	F
1978	3	4	T		PM	F
1978	3	5		0	PM	F
1978	3	6	T		PM	F
1978	3	7	T		PM	F
1978	3	8		0.31	PM	F
1978	3	9		0	PM	F
1978	3	10		0	PM	F
1978	3	11		0	PM	F
1978	3	12		0.04	PM	F
1978	3	13		0	PM	F
1978	3	14		0.27	PM	F
1978	3	15	T		PM	F
1978	3	16		0	PM	F
1978	3	17	T		PM	F
1978	3	18	T		PM	F
1978	3	19		0	PM	F
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1978	3	22		0	PM	F
1978	3	23		0.31	PM	F
1978	3	24	T		PM	F
1978	3	25		0.78	PM	F
1978	3	26		0.4	PM	F
1978	3	27	T		PM	F
1978	3	28		0	PM	F
1978	3	29		0	PM	F
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1978	4	3	M		-	-
1978	4	4	M		-	-
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1978	4	18	M		-	-
1978	4	19	M		-	-
1978	4	20	M		-	-
1978	4	21	M		-	-
1978	4	22	M		-	-

1978	4	23	M	-		-
1978	4	24	M	-		-
1978	4	25	M	-		-
1978	4	26	M	-		-
1978	4	27	M	-		-
1978	4	28	M	-		-
1978	4	29	M	-		-
1978	4	30	M	-		-
1978	5	1		0	PM	F
1978	5	2		0	PM	F
1978	5	3		0	PM	F
1978	5	4		0.19	PM	F
1978	5	5		0.62	PM	F
1978	5	6		0.02	PM	F
1978	5	7		0.31	PM	F
1978	5	8		0.59	PM	F
1978	5	9		0	PM	F
1978	5	10		0	PM	F
1978	5	11		0.09	PM	F
1978	5	12		0.68	PM	F
1978	5	13		0.98	PM	F
1978	5	14		0.67	PM	F
1978	5	15		0.03	PM	F
1978	5	16	T		PM	F
1978	5	17		0	PM	F
1978	5	18		0	PM	F
1978	5	19		0	PM	F
1978	5	20		0	PM	F
1978	5	21		0	PM	F
1978	5	22		0	PM	F
1978	5	23		0.25	PM	F
1978	5	24		0.25	PM	F
1978	5	25		0	PM	F
1978	5	26		0	PM	F
1978	5	27		0	PM	F
1978	5	28		0	PM	F
1978	5	29		0	PM	F
1978	5	30	T		PM	F
1978	5	31		0	PM	F
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1978	6	2	T		PM	F
1978	6	3	T		PM	F
1978	6	4		0	PM	F
1978	6	5		0	PM	F
1978	6	6		0	PM	F
1978	6	7		0.28	PM	F
1978	6	8		0.17	PM	F
1978	6	9		0	PM	F
1978	6	10		0	PM	F
1978	6	11		0	PM	F
1978	6	12		0	PM	F
1978	6	13		0	PM	F
1978	6	14		0.01	PM	F
1978	6	15		0	PM	F
1978	6	16		0.12	PM	F
1978	6	17		0.26	PM	F
1978	6	18	T		PM	F
1978	6	19		0	PM	F
1978	6	20		0.25	PM	F
1978	6	21		0	PM	F
1978	6	22		0	PM	F
1978	6	23		0	PM	F
1978	6	24		0	PM	F
1978	6	25		0	PM	F
1978	6	26		0.02	PM	F
1978	6	27		0	PM	F
1978	6	28		0.01	PM	F
1978	6	29		0	PM	F
1978	6	30		0	PM	F
1978	7	1		0.5	PM	F
1978	7	2		1.87	PM	F
1978	7	3		0.08	PM	F
1978	7	4		0	PM	F
1978	7	5		0	PM	F
1978	7	6		0	PM	F
1978	7	7		0	PM	F
1978	7	8		0.03	PM	F
1978	7	9		1.18	PM	F
1978	7	10		0	PM	F
1978	7	11		0	PM	F
1978	7	12		0	PM	F
1978	7	13		0.07	PM	F
1978	7	14		0	PM	F
1978	7	15		0	PM	F
1978	7	16		0	PM	F
1978	7	17		0	PM	F
1978	7	18		0	PM	F
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1978	7	20		0	PM	F
1978	7	21		0	PM	F
1978	7	22		0	PM	F
1978	7	23		0.65	PM	F
1978	7	24		0.26	PM	F
1978	7	25		0	PM	F
1978	7	26		0	PM	F
1978	7	27		0.93	PM	F
1978	7	28		0	PM	F
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1978	7	30		0	PM	F
1978	7	31		0	PM	F
1978	8	1		0.47	PM	F
1978	8	2		0.09	PM	F
1978	8	3		0	PM	F
1978	8	4		0	PM	F
1978	8	5		0	PM	F
1978	8	6		0.06	PM	F
1978	8	7		0	PM	F
1978	8	8		0	PM	F
1978	8	9		0	PM	F
1978	8	10		0.01	PM	F
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1978	8	12		0	PM	F
1978	8	13		0	PM	F
1978	8	14		0	PM	F
1978	8	15		0.05	PM	F

1978	8	16		0 PM	F
1978	8	17		0.7 PM	F
1978	8	18		0.04 PM	F
1978	8	19		0 PM	F
1978	8	20		0 PM	F
1978	8	21		0 PM	F
1978	8	22		0 PM	F
1978	8	23		0 PM	F
1978	8	24		0 PM	F
1978	8	25		0.38 PM	F
1978	8	26		0.08 PM	F
1978	8	27		0.84 PM	F
1978	8	28		0 PM	F
1978	8	29		0 PM	F
1978	8	30		0 PM	F
1978	8	31		0 PM	F
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1978	9	10		0 PM	F
1978	9	11		0 PM	F
1978	9	12		0 PM	F
1978	9	13	T	PM	F
1978	9	14		0.15 PM	F
1978	9	15		0 PM	F
1978	9	16		0.49 PM	F
1978	9	17		0.96 PM	F
1978	9	18		0.01 PM	F
1978	9	19		0.05 PM	F
1978	9	20		0 PM	F
1978	9	21		0.86 PM	F
1978	9	22		0 PM	F
1978	9	23		0 PM	F
1978	9	24		0 PM	F
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1978	9	26		0 PM	F
1978	9	27		0 PM	F
1978	9	28		0 PM	F
1978	9	29		0 PM	F
1978	9	30		0.24 PM	F
1978	10	1	M	-	F
1978	10	2	M	-	F
1978	10	3	M	-	F
1978	10	4	M	-	F
1978	10	5	M	-	F
1978	10	6	M	-	F
1978	10	7	M	-	F
1978	10	8	M	-	F
1978	10	9	M	-	F
1978	10	10	M	-	F
1978	10	11	M	-	F
1978	10	12	M	-	F
1978	10	13	M	-	F
1978	10	14	M	-	F
1978	10	15	M	-	F
1978	10	16	M	-	F
1978	10	17	M	-	F
1978	10	18	M	-	F
1978	10	19	M	-	F
1978	10	20	M	-	F
1978	10	21	M	-	F
1978	10	22	M	-	F
1978	10	23	M	-	F
1978	10	24	M	-	F
1978	10	25	M	-	F
1978	10	26	M	-	F
1978	10	27	M	-	F
1978	10	28	M	-	F
1978	10	29	M	-	F
1978	10	30	M	-	F
1978	10	31	M	-	F
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1978	11	3		0 PM	F
1978	11	4	T	PM	F
1978	11	5		0 PM	F
1978	11	6	T	PM	F
1978	11	7		0.37 PM	F
1978	11	8		0 PM	F
1978	11	9		0 PM	F
1978	11	10		0 PM	F
1978	11	11		0 PM	F
1978	11	12	T	PM	F
1978	11	13		0.03 PM	F
1978	11	14	T	PM	F
1978	11	15		0.4 PM	F
1978	11	16		0.03 PM	F
1978	11	17		0.63 PM	F
1978	11	18		0 PM	F
1978	11	19		0.02 PM	F
1978	11	20	T	PM	F
1978	11	21		0 PM	F
1978	11	22		0 PM	F
1978	11	23		0.38 PM	F
1978	11	24		0 PM	F
1978	11	25		0 PM	F
1978	11	26		0.07 PM	F
1978	11	27		0.4 PM	F
1978	11	28		0 PM	F
1978	11	29		0 PM	F
1978	11	30		0 PM	F
1978	12	1		0 PM	F
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1978	12	4	T	PM	F
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1978	12	6		0 PM	F
1978	12	7		0.74 PM	F
1978	12	8		0.07 PM	F

1978	12	9	T	PM	F
1978	12	10	0	PM	F
1978	12	11	0	PM	F
1978	12	12	0	PM	F
1978	12	13	0	PM	F
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1978	12	19	T	PM	F
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1978	12	25	0	PM	F
1978	12	26	0	PM	F
1978	12	27	0	PM	F
1978	12	28	0	PM	F
1978	12	29	0.27	PM	F
1978	12	30	0.77	PM	F
1978	12	31	0.25	PM	F
1979	1	1	0.92	PM	F
1979	1	2	0.2	PM	F
1979	1	3	0	PM	F
1979	1	4	0.04	PM	F
1979	1	5	0.07	PM	F
1979	1	6	0.05	PM	F
1979	1	7	T	PM	F
1979	1	8	T	PM	F
1979	1	9	0	PM	F
1979	1	10	0	PM	F
1979	1	11	0	PM	F
1979	1	12	0.07	PM	F
1979	1	13	0.25	PM	F
1979	1	14	0.96	PM	F
1979	1	15	0	PM	F
1979	1	16	0	PM	F
1979	1	17	T	PM	F
1979	1	18	0	PM	F
1979	1	19	0.26	PM	F
1979	1	20	0	PM	F
1979	1	21	0.04	PM	F
1979	1	22	T	PM	F
1979	1	23	0.05	PM	F
1979	1	24	0.7	PM	F
1979	1	25	0.14	PM	F
1979	1	26	T	PM	F
1979	1	27	0.36	PM	F
1979	1	28	T	PM	F
1979	1	29	T	PM	F
1979	1	30	0.11	PM	F
1979	1	31	0	PM	F
1979	2	1	0	PM	F
1979	2	2	0.07	PM	F
1979	2	3	T	PM	F
1979	2	4	0	PM	F
1979	2	5	0	PM	F
1979	2	6	0	PM	F
1979	2	7	0.03	PM	F
1979	2	8	0.12	PM	F
1979	2	9	0	PM	F
1979	2	10	T	PM	F
1979	2	11	0	PM	F
1979	2	12	T	PM	F
1979	2	13	0	PM	F
1979	2	14	T	PM	F
1979	2	15	T	PM	F
1979	2	16	0.03	PM	F
1979	2	17	T	PM	F
1979	2	18	0.11	PM	F
1979	2	19	0	PM	F
1979	2	20	0	PM	F
1979	2	21	0.48	PM	F
1979	2	22	0	PM	F
1979	2	23	0.05	PM	F
1979	2	24	0	PM	F
1979	2	25	0	PM	F
1979	2	26	0	PM	F
1979	2	27	0	PM	F
1979	2	28	0.22	PM	F
1979	3	1	0.22	PM	F
1979	3	2	0	PM	F
1979	3	3	0.01	PM	F
1979	3	4	2.27	PM	F
1979	3	5	T	PM	F
1979	3	6	0	PM	F
1979	3	7	0.02	PM	F
1979	3	8	0.06	PM	F
1979	3	9	0.08	PM	F
1979	3	10	0.35	PM	F
1979	3	11	0	PM	F
1979	3	12	0	PM	F
1979	3	13	0	PM	F
1979	3	14	0	PM	F
1979	3	15	0	PM	F
1979	3	16	0	PM	F
1979	3	17	0	PM	F
1979	3	18	0.06	PM	F
1979	3	19	1.23	PM	F
1979	3	20	0.06	PM	F
1979	3	21	0	PM	F
1979	3	22	0	PM	F
1979	3	23	0.33	PM	F
1979	3	24	1.08	PM	F
1979	3	25	0.3	PM	F
1979	3	26	T	PM	F
1979	3	27	0	PM	F
1979	3	28	0.02	PM	F
1979	3	29	0.68	PM	F
1979	3	30	0.22	PM	F
1979	3	31	0.61	PM	F
1979	4	1	0	PM	F
1979	4	2	0.25	PM	F

1979	4	3	T		PM	F
1979	4	4	T		PM	F
1979	4	5		0.14	PM	F
1979	4	6		0	PM	F
1979	4	7	T		PM	F
1979	4	8		0	PM	F
1979	4	9		0.45	PM	F
1979	4	10		0	PM	F
1979	4	11		0.94	PM	F
1979	4	12		3.5	PM	F
1979	4	13		0.08	PM	F
1979	4	14		0	PM	F
1979	4	15		0	PM	F
1979	4	16		0	PM	F
1979	4	17		0	PM	F
1979	4	18		0	PM	F
1979	4	19		0	PM	F
1979	4	20	T		PM	F
1979	4	21		0.3	PM	F
1979	4	22		0.16	PM	F
1979	4	23		0	PM	F
1979	4	24		0.63	PM	F
1979	4	25		0.37	PM	F
1979	4	26		0.78	PM	F
1979	4	27		0.01	PM	F
1979	4	28		0.12	PM	F
1979	4	29		0	PM	F
1979	4	30		0.15	PM	F
1979	5	1		0	PM	F
1979	5	2		0	PM	F
1979	5	3		0.82	PM	F
1979	5	4		0.03	PM	F
1979	5	5		0	PM	F
1979	5	6		0	PM	F
1979	5	7		0	PM	F
1979	5	8		0	PM	F
1979	5	9		0	PM	F
1979	5	10		0	PM	F
1979	5	11		0	PM	F
1979	5	12		0.22	PM	F
1979	5	13		0.03	PM	F
1979	5	14		0.14	PM	F
1979	5	15		0.2	PM	F
1979	5	16		0	PM	F
1979	5	17		0	PM	F
1979	5	18		0	PM	F
1979	5	19	T		PM	F
1979	5	20		0	PM	F
1979	5	21		0	PM	F
1979	5	22		0	PM	F
1979	5	23		0	PM	F
1979	5	24		0	PM	F
1979	5	25		0.02	PM	F
1979	5	26		0	PM	F
1979	5	27		0.27	PM	F
1979	5	28		0	PM	F
1979	5	29		0	PM	F
1979	5	30		0	PM	F
1979	5	31		0	PM	F
1979	6	1		0	PM	F
1979	6	2		0	PM	F
1979	6	3		0	PM	F
1979	6	4		0	PM	F
1979	6	5		0	PM	F
1979	6	6		0	PM	F
1979	6	7		0.03	PM	F
1979	6	8		0.36	PM	F
1979	6	9		0.04	PM	F
1979	6	10		0.36	PM	F
1979	6	11		0	PM	F
1979	6	12		0	PM	F
1979	6	13		0.16	PM	F
1979	6	14		0.13	PM	F
1979	6	15		0	PM	F
1979	6	16		0	PM	F
1979	6	17		0	PM	F
1979	6	18		0	PM	F
1979	6	19		0	PM	F
1979	6	20		0.03	PM	F
1979	6	21		0	PM	F
1979	6	22		0	PM	F
1979	6	23		0	PM	F
1979	6	24		0.06	PM	F
1979	6	25		0	PM	F
1979	6	26		0	PM	F
1979	6	27		0	PM	F
1979	6	28	T		PM	F
1979	6	29		0	PM	F
1979	6	30		0.04	PM	F
1979	7	1		0	PM	F
1979	7	2		0	PM	F
1979	7	3		0	PM	F
1979	7	4		0.3	PM	F
1979	7	5		0	PM	F
1979	7	6		0	PM	F
1979	7	7		0	PM	F
1979	7	8	T		PM	F
1979	7	9		0	PM	F
1979	7	10		0	PM	F
1979	7	11		0	PM	F
1979	7	12		0	PM	F
1979	7	13	T		PM	F
1979	7	14		0.33	PM	F
1979	7	15		0	PM	F
1979	7	16		0	PM	F
1979	7	17		0	PM	F
1979	7	18		0	PM	F
1979	7	19		0	PM	F
1979	7	20		0	PM	F
1979	7	21		0	PM	F
1979	7	22		0	PM	F
1979	7	23		0.2	PM	F
1979	7	24	T		PM	F
1979	7	25		2.84	PM	F
1979	7	26		0	PM	F

1979	7	27	0.1	PM	F
1979	7	28	0.02	PM	F
1979	7	29	0.12	PM	F
1979	7	30	0.87	PM	F
1979	7	31	0.34	PM	F
1979	8	1	1.12	PM	F
1979	8	2	0	PM	F
1979	8	3	0	PM	F
1979	8	4	0	PM	F
1979	8	5	0	PM	F
1979	8	6	0	PM	F
1979	8	7	0	PM	F
1979	8	8	0	PM	F
1979	8	9	0	PM	F
1979	8	10	0.29	PM	F
1979	8	11	0	PM	F
1979	8	12	0	PM	F
1979	8	13	0	PM	F
1979	8	14	0	PM	F
1979	8	15	0	PM	F
1979	8	16	0	PM	F
1979	8	17	0	PM	F
1979	8	18	0.59	PM	F
1979	8	19	T	PM	F
1979	8	20	0.05	PM	F
1979	8	21	T	PM	F
1979	8	22	0.11	PM	F
1979	8	23	0.03	PM	F
1979	8	24	0	PM	F
1979	8	25	0	PM	F
1979	8	26	0.12	PM	F
1979	8	27	T	PM	F
1979	8	28	0.01	PM	F
1979	8	29	0.01	PM	F
1979	8	30	0	PM	F
1979	8	31	0	PM	F
1979	9	1	0.07	PM	F
1979	9	2	T	PM	F
1979	9	3	0	PM	F
1979	9	4	0	PM	F
1979	9	5	0	PM	F
1979	9	6	0	PM	F
1979	9	7	0	PM	F
1979	9	8	0	PM	F
1979	9	9	0	PM	F
1979	9	10	0	PM	F
1979	9	11	0	PM	F
1979	9	12	0	PM	F
1979	9	13	0	PM	F
1979	9	14	0	PM	F
1979	9	15	0	PM	F
1979	9	16	0	PM	F
1979	9	17	0	PM	F
1979	9	18	0	PM	F
1979	9	19	0	PM	F
1979	9	20	0	PM	F
1979	9	21	0	PM	F
1979	9	22	0	PM	F
1979	9	23	0	PM	F
1979	9	24	0	PM	F
1979	9	25	0	PM	F
1979	9	26	0	PM	F
1979	9	27	0	PM	F
1979	9	28	0	PM	F
1979	9	29	0.08	PM	F
1979	9	30	0	PM	F
1979	10	1	0.29	PM	F
1979	10	2	0.02	PM	F
1979	10	3	0.01	PM	F
1979	10	4	0	PM	F
1979	10	5	0.03	PM	F
1979	10	6	0	PM	F
1979	10	7	0	PM	F
1979	10	8	0.01	PM	F
1979	10	9	T	PM	F
1979	10	10	0	PM	F
1979	10	11	0.08	PM	F
1979	10	12	0	PM	F
1979	10	13	0	PM	F
1979	10	14	T	PM	F
1979	10	15	0.01	PM	F
1979	10	16	0.19	PM	F
1979	10	17	0.01	PM	F
1979	10	18	0	PM	F
1979	10	19	T	PM	F
1979	10	20	0	PM	F
1979	10	21	0	PM	F
1979	10	22	0	PM	F
1979	10	23	0.53	PM	F
1979	10	24	0	PM	F
1979	10	25	0	PM	F
1979	10	26	0	PM	F
1979	10	27	0	PM	F
1979	10	28	0	PM	F
1979	10	29	0	PM	F
1979	10	30	0	PM	F
1979	10	31	0.16	PM	F
1979	11	1	0	PM	F
1979	11	2	0	PM	F
1979	11	3	0	PM	F
1979	11	4	0	PM	F
1979	11	5	0	PM	F
1979	11	6	T	PM	F
1979	11	7	0	PM	F
1979	11	8	0.16	PM	F
1979	11	9	0.17	PM	F
1979	11	10	0.18	PM	F
1979	11	11	T	PM	F
1979	11	12	0	PM	F
1979	11	13	0	PM	F
1979	11	14	0	PM	F
1979	11	15	0	PM	F
1979	11	16	0	PM	F
1979	11	17	0	PM	F
1979	11	18	0	PM	F

1979	11	19		0 PM	F
1979	11	20		0 PM	F
1979	11	21		0.33 PM	F
1979	11	22		0.14 PM	F
1979	11	23		0.02 PM	F
1979	11	24		0 PM	F
1979	11	25		0 PM	F
1979	11	26		1.02 PM	F
1979	11	27		0.03 PM	F
1979	11	28		0.13 PM	F
1979	11	29		0.02 PM	F
1979	11	30	T	PM	F
1979	12	1		0 PM	F
1979	12	2		0 PM	F
1979	12	3		0 PM	F
1979	12	4		0 PM	F
1979	12	5		0 PM	F
1979	12	6		0 PM	F
1979	12	7		0.01 PM	F
1979	12	8		0 PM	F
1979	12	9		0 PM	F
1979	12	10		0 PM	F
1979	12	11		0 PM	F
1979	12	12		0.06 PM	F
1979	12	13		0 PM	F
1979	12	14		0 PM	F
1979	12	15		0 PM	F
1979	12	16		0 PM	F
1979	12	17	T	PM	F
1979	12	18		0 PM	F
1979	12	19		0 PM	F
1979	12	20		0 PM	F
1979	12	21		0 PM	F
1979	12	22		0.22 PM	F
1979	12	23		0.12 PM	F
1979	12	24		0.58 PM	F
1979	12	25		0.9 PM	F
1979	12	26		0 PM	F
1979	12	27		0 PM	F
1979	12	28		0 PM	F
1979	12	29		0 PM	F
1979	12	30		0 PM	F
1979	12	31		0 PM	F
1980	1	1		0 PM	F
1980	1	2		0 PM	F
1980	1	3	T	PM	F
1980	1	4	T	PM	F
1980	1	5		0 PM	F
1980	1	6		0.06 PM	F
1980	1	7		0 PM	F
1980	1	8		0 PM	F
1980	1	9		0 PM	F
1980	1	10		0.02 PM	F
1980	1	11		0 PM	F
1980	1	12		0 PM	F
1980	1	13		0.03 PM	F
1980	1	14		0 PM	F
1980	1	15		0.01 PM	F
1980	1	16		0.1 PM	F
1980	1	17		0 PM	F
1980	1	18		0 PM	F
1980	1	19		0.03 PM	F
1980	1	20		0 PM	F
1980	1	21	T	PM	F
1980	1	22	T	PM	F
1980	1	23	T	PM	F
1980	1	24		0.11 PM	F
1980	1	25		0 PM	F
1980	1	26		0 PM	F
1980	1	27	T	PM	F
1980	1	28		0 PM	F
1980	1	29		0.08 PM	F
1980	1	30		0.06 PM	F
1980	1	31		0 PM	F
1980	2	1		0 PM	F
1980	2	2		0 PM	F
1980	2	3		0 PM	F
1980	2	4		0 PM	F
1980	2	5		0.06 PM	F
1980	2	6		0.17 PM	F
1980	2	7		0.03 PM	F
1980	2	8		0 PM	F
1980	2	9		0.05 PM	F
1980	2	10		0 PM	F
1980	2	11		0 PM	F
1980	2	12	T	PM	F
1980	2	13		0 PM	F
1980	2	14		0 PM	F
1980	2	15		0.43 PM	F
1980	2	16		0.12 PM	F
1980	2	17		0 PM	F
1980	2	18		0 PM	F
1980	2	19		0 PM	F
1980	2	20	T	PM	F
1980	2	21	T	PM	F
1980	2	22		0.07 PM	F
1980	2	23		0 PM	F
1980	2	24		0 PM	F
1980	2	25		0.12 PM	F
1980	2	26		0.11 PM	F
1980	2	27		0 PM	F
1980	2	28		0.01 PM	F
1980	2	29		0 PM	F
1980	3	1		0.1 PM	F
1980	3	2		0 PM	F
1980	3	3		0 PM	F
1980	3	4		0 PM	F
1980	3	5		0.09 PM	F
1980	3	6		0 PM	F
1980	3	7		0 PM	F
1980	3	8		0.7 PM	F
1980	3	9	T	PM	F
1980	3	10		0.03 PM	F
1980	3	11		0 PM	F
1980	3	12		0 PM	F

1980	3	13	0.08	PM	F
1980	3	14	0	PM	F
1980	3	15	0	PM	F
1980	3	16	0	PM	F
1980	3	17	0.77	PM	F
1980	3	18 T		PM	F
1980	3	19	0	PM	F
1980	3	20	0	PM	F
1980	3	21	0.28	PM	F
1980	3	22	0	PM	F
1980	3	23	0	PM	F
1980	3	24	0.25	PM	F
1980	3	25	0.52	PM	F
1980	3	26	0	PM	F
1980	3	27	0	PM	F
1980	3	28	0	PM	F
1980	3	29	0.45	PM	F
1980	3	30 T		PM	F
1980	3	31	1.32	PM	F
1980	4	1	0	PM	F
1980	4	2 T		PM	F
1980	4	3	0.05	PM	F
1980	4	4	0.03	PM	F
1980	4	5	0.01	PM	F
1980	4	6	0	PM	F
1980	4	7	0.01	PM	F
1980	4	8	0.45	PM	F
1980	4	9	0.2	PM	F
1980	4	10	0.15	PM	F
1980	4	11	0	PM	F
1980	4	12 T		PM	F
1980	4	13	0	PM	F
1980	4	14	0.57	PM	F
1980	4	15	0.48	PM	F
1980	4	16	0	PM	F
1980	4	17	0	PM	F
1980	4	18 T		PM	F
1980	4	19	0	PM	F
1980	4	20	0	PM	F
1980	4	21	0	PM	F
1980	4	22	0	PM	F
1980	4	23	0	PM	F
1980	4	24	0	PM	F
1980	4	25	0	PM	F
1980	4	26	0	PM	F
1980	4	27	0.04	PM	F
1980	4	28	0.08	PM	F
1980	4	29	0.14	PM	F
1980	4	30 T		PM	F
1980	5	1	0	PM	F
1980	5	2	0	PM	F
1980	5	3	0	PM	F
1980	5	4	0	PM	F
1980	5	5	0	PM	F
1980	5	6 T		PM	F
1980	5	7	0	PM	F
1980	5	8	0	PM	F
1980	5	9	0	PM	F
1980	5	10 T		PM	F
1980	5	11	0.02	PM	F
1980	5	12	0.33	PM	F
1980	5	13	0.74	PM	F
1980	5	14	0	PM	F
1980	5	15	0	PM	F
1980	5	16	0	PM	F
1980	5	17	0.33	PM	F
1980	5	18	0.75	PM	F
1980	5	19	0.02	PM	F
1980	5	20	0.17	PM	F
1980	5	21	0	PM	F
1980	5	22	0	PM	F
1980	5	23	0.07	PM	F
1980	5	24	0.15	PM	F
1980	5	25	0.01	PM	F
1980	5	26	0	PM	F
1980	5	27	0	PM	F
1980	5	28	0	PM	F
1980	5	29	0	PM	F
1980	5	30	0	PM	F
1980	5	31	0.31	PM	F
1980	6	1	1.45	PM	F
1980	6	2	1.04	PM	F
1980	6	3	0.02	PM	F
1980	6	4	0.03	PM	F
1980	6	5 T		PM	F
1980	6	6	0	PM	F
1980	6	7	0.03	PM	F
1980	6	8	0	PM	F
1980	6	9 T		PM	F
1980	6	10	0	PM	F
1980	6	11	0	PM	F
1980	6	12	0	PM	F
1980	6	13	0	PM	F
1980	6	14 T		PM	F
1980	6	15	1.07	PM	F
1980	6	16	0.42	PM	F
1980	6	17	0	PM	F
1980	6	18	0	PM	F
1980	6	19 T		PM	F
1980	6	20	0	PM	F
1980	6	21	0	PM	F
1980	6	22	0	PM	F
1980	6	23	0.06	PM	F
1980	6	24	0.06	PM	F
1980	6	25	0	PM	F
1980	6	26	0	PM	F
1980	6	27	0	PM	F
1980	6	28	0.16	PM	F
1980	6	29 T		PM	F
1980	6	30	0	PM	F
1980	7	1	0	PM	F
1980	7	2	0	PM	F
1980	7	3	0.05	PM	F
1980	7	4	0.23	PM	F
1980	7	5	0.15	PM	F

1980	7	6	0	PM	F
1980	7	7	0	PM	F
1980	7	8	0	PM	F
1980	7	9	0	PM	F
1980	7	10	0.02	PM	F
1980	7	11	T	PM	F
1980	7	12	T	PM	F
1980	7	13	0	PM	F
1980	7	14	0	PM	F
1980	7	15	0	PM	F
1980	7	16	0	PM	F
1980	7	17	0	PM	F
1980	7	18	0	PM	F
1980	7	19	0.02	PM	F
1980	7	20	0	PM	F
1980	7	21	0	PM	F
1980	7	22	0.08	PM	F
1980	7	23	0	PM	F
1980	7	24	0	PM	F
1980	7	25	0	PM	F
1980	7	26	0	PM	F
1980	7	27	0.14	PM	F
1980	7	28	0.12	PM	F
1980	7	29	0	PM	F
1980	7	30	0	PM	F
1980	7	31	0.13	PM	F
1980	8	1	0	PM	F
1980	8	2	0	PM	F
1980	8	3	0.06	PM	F
1980	8	4	0	PM	F
1980	8	5	0.66	PM	F
1980	8	6	0.03	PM	F
1980	8	7	0.01	PM	F
1980	8	8	0.01	PM	F
1980	8	9	0	PM	F
1980	8	10	0	PM	F
1980	8	11	0.53	PM	F
1980	8	12	0.03	PM	F
1980	8	13	0	PM	F
1980	8	14	1.65	PM	F
1980	8	15	0.94	PM	F
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1980	8	18	0.13	PM	F
1980	8	19	0.16	PM	F
1980	8	20	T	PM	F
1980	8	21	T	PM	F
1980	8	22	0	PM	F
1980	8	23	0	PM	F
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1980	8	26	0	PM	F
1980	8	27	0	PM	F
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1980	8	30	0.08	PM	F
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1980	9	3	0.01	PM	F
1980	9	4	0	PM	F
1980	9	5	T	PM	F
1980	9	6	0.2	PM	F
1980	9	7	0.01	PM	F
1980	9	8	T	PM	F
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1980	9	10	0.02	PM	F
1980	9	11	0	PM	F
1980	9	12	0.03	PM	F
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1980	9	16	0.7	PM	F
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1980	9	29	0	PM	F
1980	9	30	0	PM	F
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1980	10	2	0.12	PM	F
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1980	10	5	0	PM	F
1980	10	6	0	PM	F
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1980	10	11	0	PM	F
1980	10	12	0	PM	F
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1980	10	14	0.08	PM	F
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1981	5	22	0	PM	F
1981	5	23 T		PM	F
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1981	5	25 T		PM	F
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1981	8	28	0.25	PM	F
1981	8	29 T		PM	F
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1982	1	25	0	AM	F
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1982	2	26		0 AM	F
1982	2	27		0 AM	F
1982	2	28		0 AM	F
1982	3	1	T	AM	F
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2001	11	4	0	AM	F
2001	11	5	0	AM	F
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2001	11	7	0	AM	F
2001	11	8	0	AM	F
2001	11	9	0.03	AM	F
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2001	11	14	0	AM	F
2001	11	15	0	AM	F
2001	11	16	0	AM	F
2001	11	17	0	AM	F
2001	11	18	0.01	AM	F
2001	11	19	0.08	AM	F
2001	11	20	0	AM	F
2001	11	21	0	AM	F
2001	11	22	0	AM	F
2001	11	23	0	AM	F
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2001	11	25	0.25	AM	F
2001	11	26	0	AM	F
2001	11	27	0.07	AM	F
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2001	12	2	0	AM	F

2001	12	3	0	AM	F
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2002	7	4		0 AM	P
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2002	7	6		0 AM	P
2002	7	7	M	-	-
2002	7	8		0 AM	P
2002	7	9	M	-	-
2002	7	10	M	-	-
2002	7	11	M	-	-
2002	7	12		0.01 AM	P
2002	7	13	M	-	-
2002	7	14	M	-	-
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2002	7	16	M	-	-
2002	7	17	M	-	-
2002	7	18	M	-	-
2002	7	19	M	-	-
2002	7	20	M	-	-

2002	7	21	M	-	-
2002	7	22	M	-	-
2002	7	23	M	-	-
2002	7	24	0	AM	P
2002	7	25	M	-	-
2002	7	26	0	AM	P
2002	7	27	0.4	AM	P
2002	7	28	M	-	-
2002	7	29	0.01	AM	P
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2002	8	1	0	AM	P
2002	8	2	M	-	-
2002	8	3	0.01	AM	P
2002	8	4	M	-	-
2002	8	5	M	-	-
2002	8	6	M	-	-
2002	8	7	M	-	-
2002	8	8	M	-	-

M = missing, e = estimated, T = trace
P = preliminary data, F = final data from NCDC

RAI ATTACHMENT

RAI 3.2.2-1 Attachment (New Figure 3.2-1)

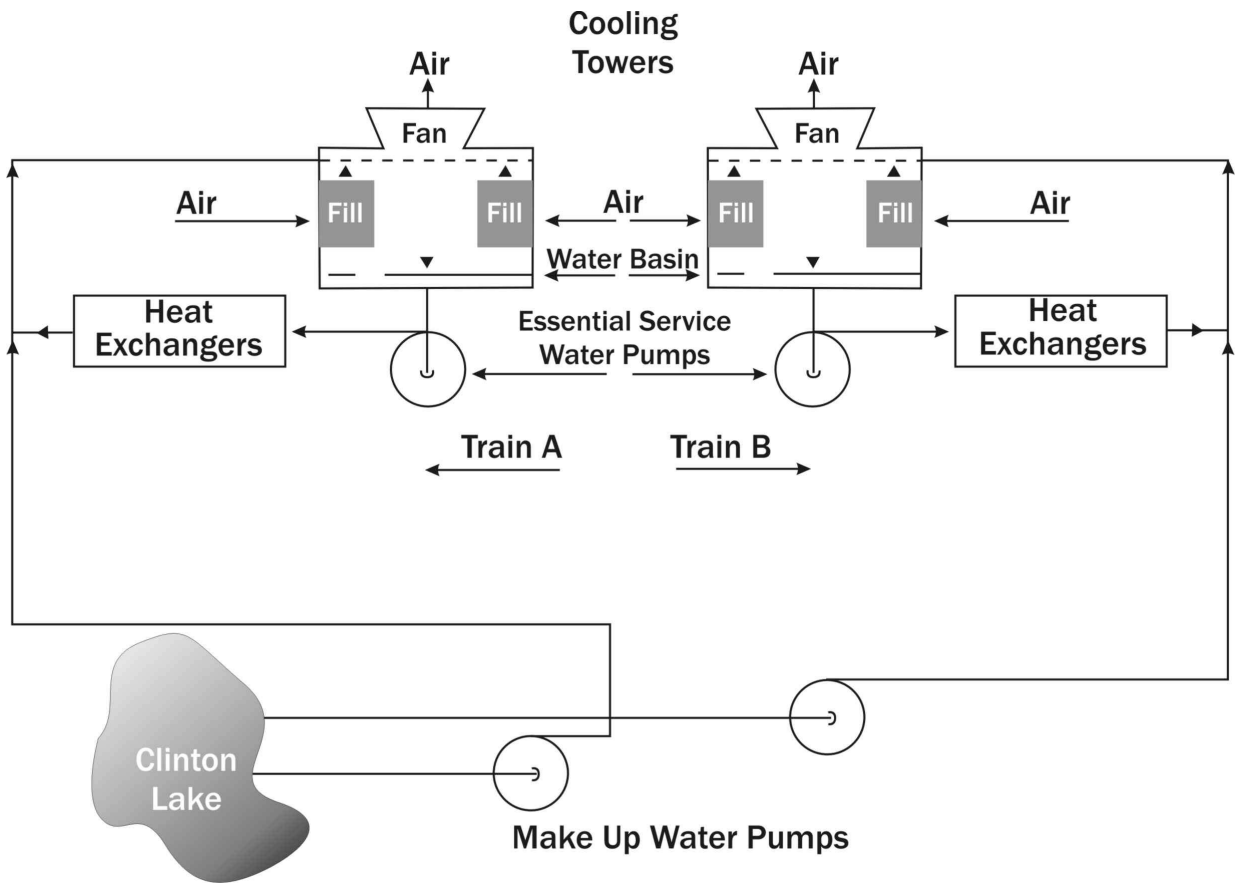
(Note – This attachment provided on the enclosed CD-ROM.)

See file: RAI 3.2.2-1 Attachment (New Figure 3.2-1).pdf

Site Safety Analysis Report for the EGC Early Site Permit

Figure 3.2-1

Ultimate Heat Sink Schematic



Not to Scale