

~~#~~ 6

**From:** Michelle Honcharik  
**To:** Jerry Holm  
**Date:** 3/9/04 4:13PM  
**Subject:** RAI on BAW-10244

Jerry,  
Please see attached.  
Michelle

**CC:** Jim Mallay

---

Framatome  
ANP  
Proj. 728  
Michelle  
Honcharik

**Mail Envelope Properties** (404E336D.F5C : 11 : 19583)

**Subject:** RAI on BAW-10244  
**Creation Date:** 3/9/04 4:13PM  
**From:** Michelle Honcharik

**Created By:** MCH3@nrc.gov

<b>Recipients</b>	<b>Action</b>	<b>Date &amp; Time</b>
framatome-anp.com	Transferred	03/09/04 04:13PM
gerald.holm (Jerald Holm)		
jim.mallay CC (James Mallay)		

<b>Post Office</b>	<b>Delivered</b>	<b>Route</b>
		framatome-anp.com

<b>Files</b>	<b>Size</b>	<b>Date &amp; Time</b>
BAW 10244_RAI.wpd	6393	03/09/04 04:11PM
MESSAGE	607	03/09/04 04:13PM

**Options**

**Auto Delete:** No  
**Expiration Date:** None  
**Notify Recipients:** Yes  
**Priority:** Standard  
**Reply Requested:** No  
**Return Notification:**  
Send Notification when Opened

**Concealed Subject:** No  
**Security:** Standard

**To Be Delivered:** Immediate  
**Status Tracking:** Delivered & Opened

REQUEST FOR ADDITIONAL INFORMATION

BAW-10244P, "MARK-BW CHF CORRELATIONS APPLIED WITH XCOBRA-IIIC"

FRAMATOME ANP

PROJECT NO. 728

1. Provide rationale for the need to use XCOBRA-IIIC code for the proposed licensing topical report (TR), BAW-10244P, "Mark-BW CHF [Critical Heat Flux] Correlations Applied with XCOBRA-IIIC" relative to LYNXT code.
2. Provide evaluation for satisfying the limitations imposed on the application of the approved BWU CHF correlation to the proposed TR with a different thermal hydraulic safety analysis code.
3. Please identify any differences in relation to the data bases to support the code development and verification, assumptions, ranges of the application, and expected results of the analysis under same conditions between the proposed licensing TRs using XCOBRA-IIIC code and the BWU CHF correlation using LYNXT.
4. Provide in details the reasons causing the different results of the departure from nucleate boiling ratio (DNBR) design limits and quantify their impact on the plant-specific applications with respect to the safety margin for the plant operation.
5. It appears that the DNBR design limit of 1.22 for BWU-N with non-mixing vane when the pressure is above 1500 psia stated in Table 4.3 is inconsistent with the DNBR design limit of 1.23 stated on Page 1-1. Please clarify the difference.
6. Please clarify that the performance factor as shown in the equation  $Q_{CHF, and}$  and Table 3.1 indicates that the proposed TR is only applied to the Mark-BW17 fuel design.
7. Provide uncertainties, confidence level, and ranges of application in a table for BWU CHF correlation in the code LYNXT versus COBRA-IIIC code, and identify the impact on the DNBR design limit due to the different uncertainties.