



Validation of WIMS-IST

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Validation of WIMS-IST

- **What is WIMS-IST?**
- **Reactor physics phenomena**
- **Experimental data**
- **Method of comparing WIMS-IST and experiment**
- **WIMS-IST input model**
- **Comparison of WIMS-IST and experiment for different phenomena**
- **Summary of results**



What is WIMS-IST?

- **IST – Industry Standard Toolset**
- **2-dimensional collision probability solution of the neutron transport equation for a CANDU lattice cell.**
- **Calculates critical bucklings, k-effective, and cell-average parameters to use in subsequent calculations.**
- **WIMS-AECL Release 2-5d, used with the ENDF/B-VI-based NDAS library Version 1a.**



Reactor physics phenomena

- 16 phenomena, 11 simulated by WIMS-IST
- Associated with reactivity changes due to
 - Fuel, coolant, or moderator temperature changes
 - Coolant or moderator density changes
 - Moderator purity or poison-concentration change
 - Coolant purity change
 - Lattice geometry changeand
 - Flux and power distribution
 - Fuel-isotopic-composition change



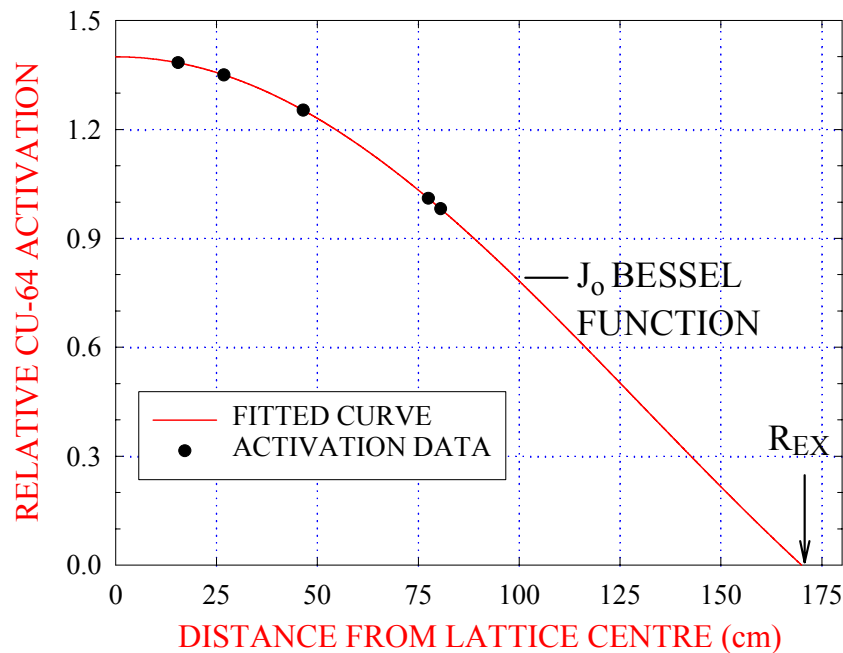
Experimental data

- **For flux distribution and fuel-isotopic-composition change, compare calculated fluxes and fuel-isotopic compositions directly to experimental quantities**
- **For reactivity effects, critical buckling is the important parameter**
- **Obtained from flux-mapped or substitution experiments**

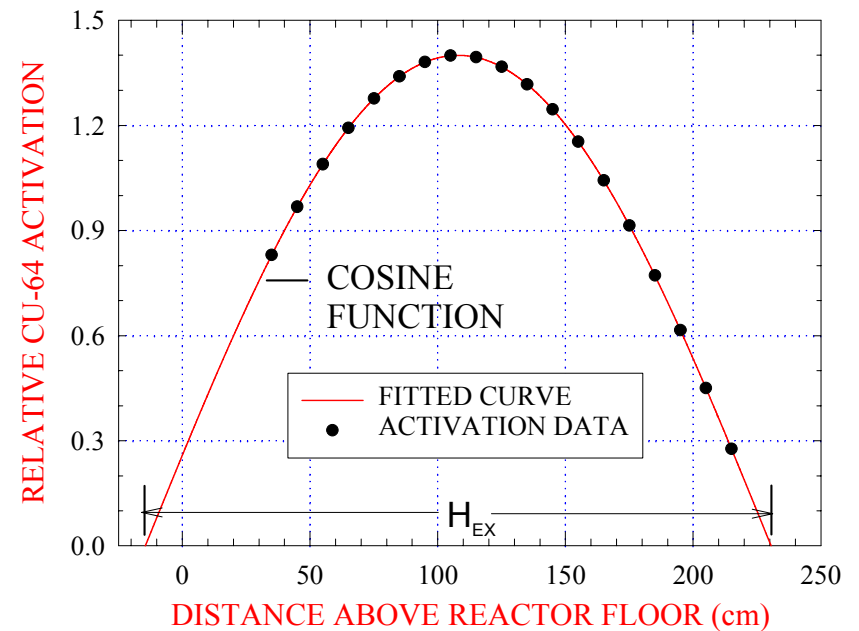


DETERMINING BUCKLING BY FLUX MAP

RADIAL FLUX SHAPE



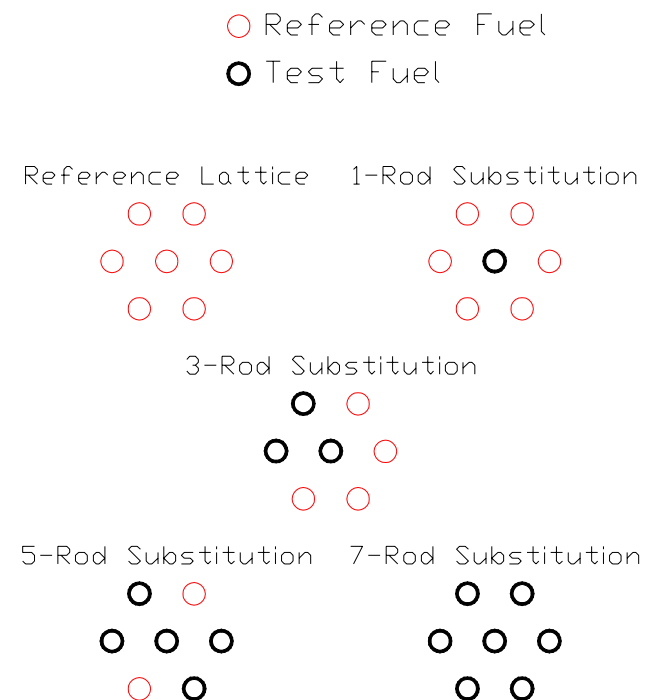
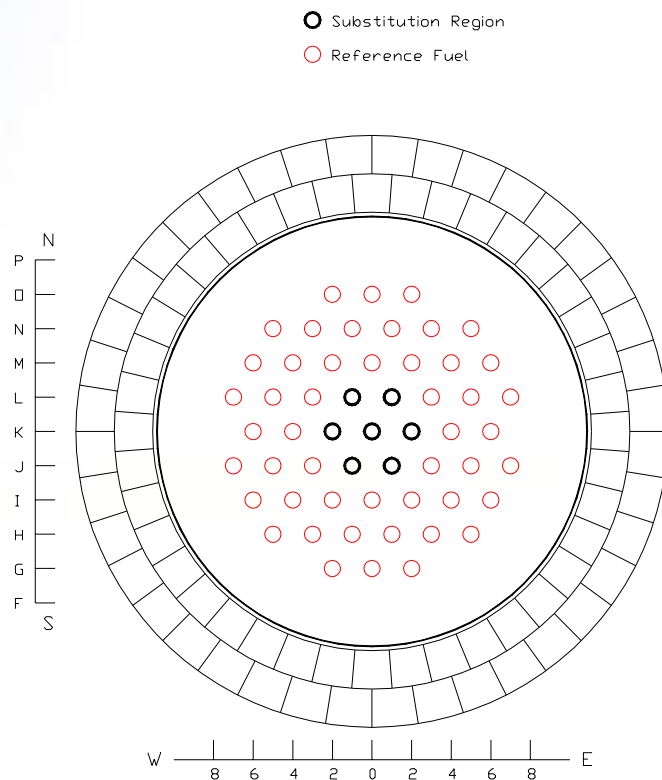
AXIAL FLUX SHAPE



$$\text{Buckling} = (2.405/R_{EX})^2 + (\pi/H_{EX})^2$$



SETUP FOR THE ROOM-TEMPERATURE SUBSTITUTION EXPERIMENTS





Method of comparing WIMS-IST and experiment for reactivity effects

- **Direct buckling method**
 - Compare calculated and measured buckling coefficients of reactivity to get bias and uncertainty.
- **K-eff method**
 - Calculate k-eff with WIMS-IST and the measured critical bucklings at different values of the parameter of interest.
 - The deviation from a constant value is a measure of the bias and the scatter is a measure of the uncertainty.
- **Both methods are essentially the same**



WIMS-IST input model

- **Compromise between accuracy and required resources**
- **For normal design and fuel management calculations**
- **Combination of 1- and 2-dimensional collision probability methods**
- **33 energy groups**
- **Shielded Zr cross-sections**
- **End regions**
- **Reasonable spatial mesh**



Coolant-Density-Change Induced Reactivity

- **Void effect – voiding coolant causes a positive reactivity effect**
- **Leads to power pulse during a loss-of-coolant accident**
- **Uncertainties in void effect cause uncertainties in power pulse**
- **Void effect studied extensively**



Overestimate of Void Reactivity by WIMS-IST

| Fuel 22 °C, 99.75 wt% Heavy Water, 31-cm Hexagonal Pitch | Void Reactivity Discrepancy (mk) |
|---|---|
| 28-element FNU (flux mapped) | 0.57 ± 0.4 |
| 28-element FNU (AECL calibration) | 0.78 |
| 28-element FNU (OPG method) | 0.73 |
| 37-element FNU (AECL calibration) | 1.89 ± 0.64 [2] |
| 37-element FNU (OPG method) | 1.90 ± 0.45 |
| 37-element MOX (AECL calibration) | 1.68 ± 0.75 [2] |
| 37-element MOX (OPG method) | 1.29 ± 0.78 |
| 43-element CANFLEX FNU (AECL calibration) | 1.83 |



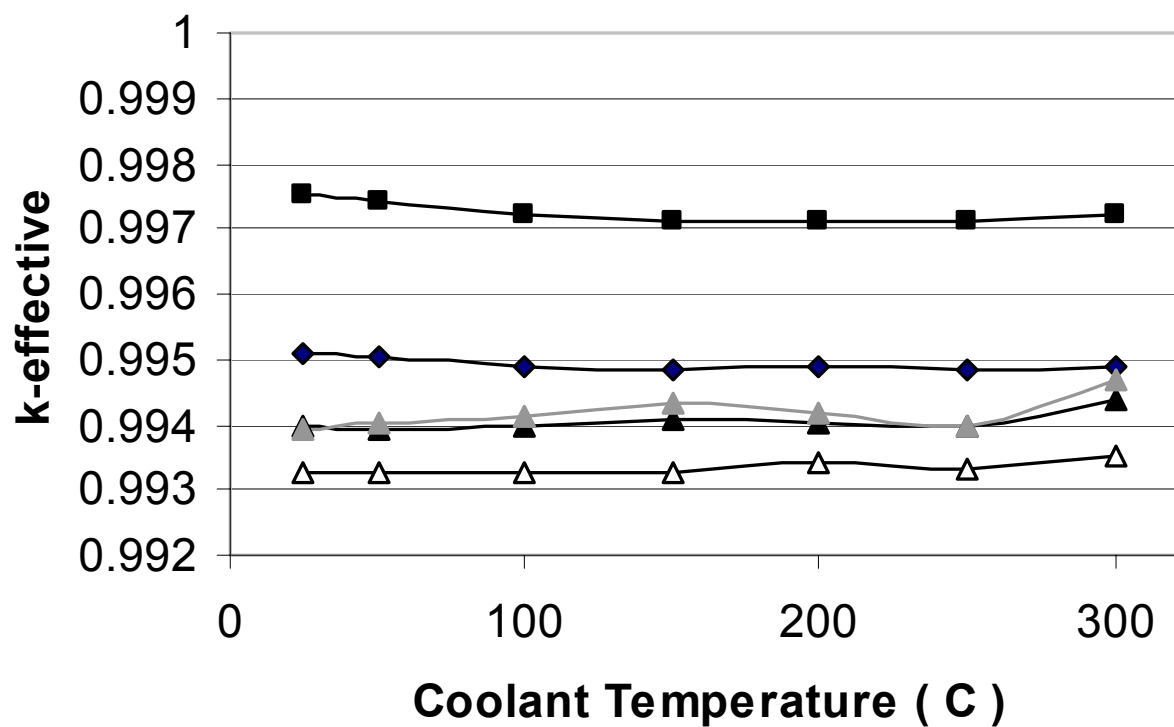
Fuel- and Coolant-temperature-change Induced Reactivity Experiments

- **37-element FNU fuel bundles**
- **37-element MOX fuel bundles**
 - 19-element boosters, room temperature extrapolation
 - 19-element boosters, measured temperature-dependant extrapolation
 - ZEEP rod boosters, room temperature extrapolation
- **43-element CANFLEX natural UO_2 fuel bundles**
- **Coolant temperature: zero bias, uncertainty $\pm 4\%$**
- **Fuel temperature: zero bias, uncertainty $\pm 10\%$**
 - Overestimate for FNU
 - Underestimate for MOX



Coolant-temperature-change Induced Reactivity

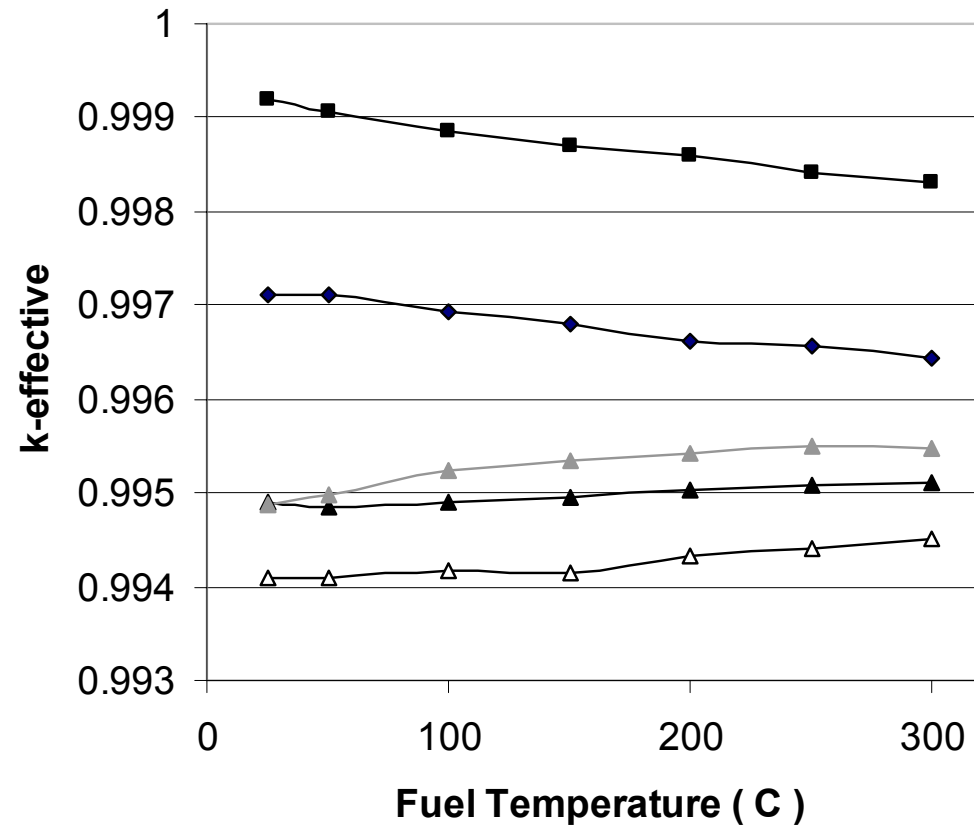
Accuracy of WIMS-IST Coolant Temperature Coefficient





Fuel-temperature-change Induced Reactivity

Accuracy of WIMS-IST Fuel Temperature Coefficient





Moderator-density- and moderator-temperature-change induced reactivity

- **Flux-mapped 19-element fuel**
- **11 to 82°C (uniform reactor temperature)**
- **Comparing buckling coefficients leads to zero bias with uncertainty of $\pm 2.6\%$**



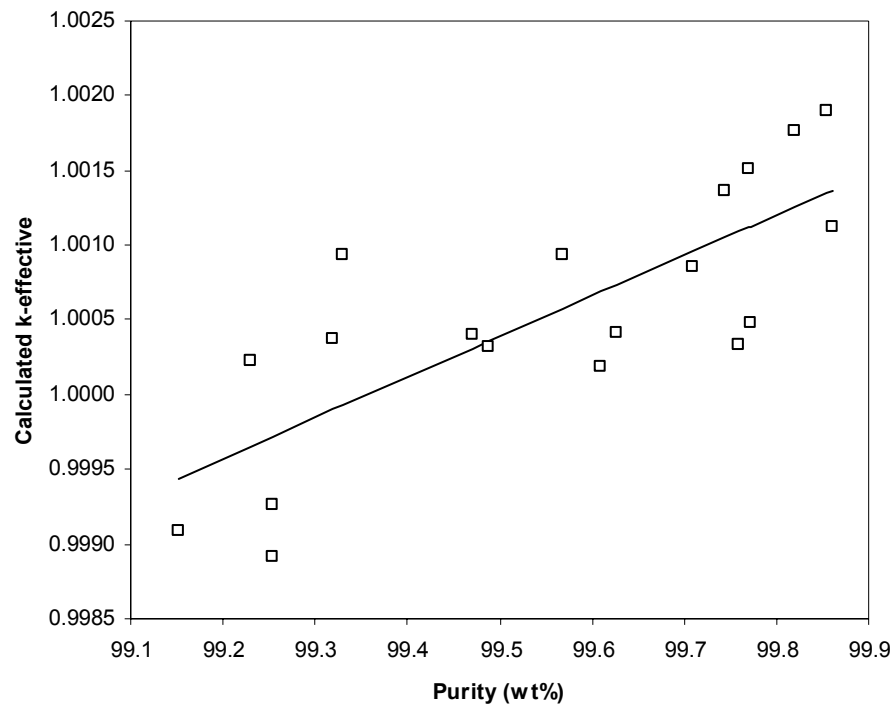
Difference between Moderator-Poison (Boron) Buckling Coefficients

| Experiment | Coolant | Relative Difference in Coefficient |
|---------------------------|------------------|------------------------------------|
| | | |
| 28-element air-cooled FNU | Air | -1.3% |
| 37-element FNU | Air | 1.7% |
| | D ₂ O | 0.0% |
| 37-element MOX | Air | -2.6% |
| | D ₂ O | -3.0% |



Moderator-purity-change induced reactivity

- 28-element UO_2 fuel
- Moderator purity reactivity coefficient overestimated by 8% with uncertainty of $\pm 3\%$





Coolant-purity-change induced reactivity

- 37-element FNU and MOX substitution experiments
- 31-cm hexagonal lattice pitch
- 3 purities from 99.76 to 95.1 wt% D₂O
- FNU bias and uncertainty $8\% \pm 11\%$
- MOX bias and uncertainty $-10\% \pm 8\%$
- Overall assign a bias and uncertainty of $0 \pm 12\%$



Lattice geometry distortion effects

- **Only channel sag**
- **Change in lattice pitch**
- **19-element and 28-element UO_2 fuels**
- **Hexagonal pitches from 24 to 40 cm**
- **No bias with varying lattice pitch**



Flux distribution within bundle

- **8 zero-power experiments with foils or other flux indicators**
- **28, 31, 36, 37 and 43-element fuel**
- **Pitch mostly 31-cm hexagonal although 2 measurements with pitches of 24-cm hexagonal**
- **Number of different foil materials**
- **Flux depression through a fuel bundle calculated to an accuracy of about 1%**



Fuel-isotopic-composition change

- **19-element NPD bundle – half elements from each ring**
- **28-element Pickering-A bundle – outer element**
- **37-element Bruce-A bundle half elements from each ring**
- **No or small bias and an uncertainty of $\pm 2\%$**



Bias and uncertainty using element data (all bundles)

| Atom Ratio | Average C/M | Standard Deviation C/M | Bias | Uncertainty |
|-----------------------------|-------------|------------------------|-------|-------------|
| $^{235}\text{U}/\text{U}$ | 1.005 | 0.016 | 0.5% | $\pm 2\%$ |
| $^{236}\text{U}/\text{U}$ | 0.961 | 0.040 | -4% | $\pm 4\%$ |
| $^{238}\text{U}/\text{U}$ | 1.000 | 0.000 | 0 | 0 |
| $^{239}\text{Pu}/\text{Pu}$ | 0.996 | 0.004 | -0.4% | $\pm 0.4\%$ |
| $^{240}\text{Pu}/\text{Pu}$ | 1.006 | 0.008 | 0.6% | $\pm 0.8\%$ |
| $^{241}\text{Pu}/\text{Pu}$ | 1.037 | 0.023 | 4% | $\pm 2\%$ |
| $^{242}\text{Pu}/\text{Pu}$ | 1.001 | 0.024 | 0.1% | $\pm 2\%$ |
| Pu/U | 1.017 | 0.021 | 2% | $\pm 2\%$ |



Summary of bias and uncertainty

| Description of Phenomenon | Bias | Uncertainty |
|---|---|--------------------------------|
| Coolant void reactivity | Overestimate +1.9 mk (37-element FNU) | ± 0.8 mk |
| Coolant-temperature coefficient | No bias | $\pm 4\%$ |
| Moderator-density and moderator-temperature coefficient | No bias | $\pm 3\%$ |
| Moderator-poison coefficient | No bias | $\pm 2\%$ |
| Moderator-purity coefficient | Overestimate +8% | $\pm 3\%$ |
| Fuel-temperature coefficient | Overestimate for FNU Underestimate for simulated mid-burnup fuel | $\pm 10\%$ |
| Fuel isotopic change | No or small bias for actinides | $\pm 2\%$ |
| Flux-power distributions | No bias in bundle flux shape | $\pm 1\%$ in bundle flux shape |
| Lattice distortion reactivity | No bias in lattice cell with varying pitch | — |
| Coolant-purity coefficient | No bias | $\pm 12\%$ |

