

**ATTACHMENT TO SCIENTIFIC NOTEBOOK #363
WATERSHED MODELING - FUTURE CLIMATE
PROJECT 20-01402-861**

**DAVID WOOLHISER
JUNE 6, 2000**

TO: Bruce Mabrito
FROM: R. Fedors
SUBJECT: Attachment to Scientific Notebook #363 - David Woolhiser
DATE: June 6, 2000

R Fedors 6/6/00

Prior to being issued an official bound scientific notebook, David Woolhiser was keeping notes of his work for CNWRA in a 3-ring folder. This volume contains the xeroxed and bound early work by Woolhiser on the future climate study in support of the watershed modeling; the work was continued in the official #363 notebook. The pages have been sequentially numbered and initialed. This volume is treated as a supplement to scientific notebook #363.

WATERSHED MODELING-FUTURE CLIMATE

Project 20-1402-861 Watershed Modeling

ATTACHMENT TO SCIENTIFIC NOTEBOOK 363

David A. Woolhiser, Hydrologic Consultant

TABLE OF CONTENTS

<u>Subject</u>	<u>Page</u>
Objectives and Procedures	1
Nevada Station Data Inventory, cooperative observer network	14
Nevada Daily precipitation analysis - Markov chain -mixed exponential (MCME)	24
Rerun ME with weighting parameter as regional constant	87
Computer run tables	112
Maximum and minimum temperature analysis	114
Summary of MCME runs	140
Mixed exponential program structure	144

Entire attachment was assembled 5/31/00 DW

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STOCHASTIC WEATHER SIMULATION
FOR FUTURE CLIMATE CONDITIONS AT YUCCA MOUNTAIN, NEVADA

PROPOSAL

By
David A. Woolhiser, Ph.D.

BACKGROUND

A thorough evaluation of the suitability of the Yucca Mountain site as a geologic repository for high level nuclear waste requires an estimation of percolation fluxes past the repository horizon under future climate conditions. Sources of water fluxes traversing the unsaturated zone include water that has percolated below the root zone on upland areas and water that has infiltrated into the beds of ephemeral channels within the repository footprint. Two approaches can be used to estimate fluxes under future conditions: 1) Find an analog site that has a climate similar to the expected future climate and also has similar geologic characteristics and make physical measurements of fluxes. 2) Utilize a hydrologic model that describes the appropriate infiltration mechanisms and model the Yucca Mountain conditions under a hypothesized future climate. Because of the strong relationship between precipitation and elevation in southern Nevada, it is possible to find an analog site nearby that has the hypothesized future annual precipitation. However, the seasonal distribution of precipitation may not be as hypothesized. The modeling approach requires the development of a stochastic weather simulator to provide such variables as precipitation, maximum temperature, minimum temperature and solar radiation on at least a daily time step.

The models WGEN (Richardson and Wright, 1984), CLIGEN (Nicks and Gander, 1993, 1994) and USCLIMATE (Hanson et al. 1994) are examples of stochastic weather simulation models. The latter two models have been thoroughly compared by Johnson et al. (1996). Shortcomings were identified for both models and recommendations for improvements were made. However Johnson et al. (1996) concluded "...the desired application for a climate simulation model should dictate model choice. For linkage to natural systems modeling, USCLIMATE seems superior in most respects, especially because of its daily parameterization, realistic simulations of variability and preservation of correlation among elements."

Recently some investigators have developed procedures to modify parameters in stochastic weather models, specifically WGEN, to identify climate change sensitivities and impacts (Wilks, 1992; Katz, 1996; Mearns et al., 1996). WGEN uses a monthly parameterization for the precipitation model. This stepwise parameterization was identified as a weakness of CLIGEN by Johnson et al. (1996). Because USCLIMATE utilizes the same algorithms for the generation of daily temperatures and solar radiation as WGEN, yet has daily

parameterization by means of Fourier series, it seems worthwhile to investigate methods to adjust parameters in USCLIMATE to create weather sequences for hypothesized future climates.

THE USCLIMATE MODEL

a. Daily precipitation occurrence

The precipitation occurrence or nonoccurrence on day n of year τ is represented by the random variable $X_\tau(n)$; $\tau = 1, 2, \dots, M$; $n = 1, 2, 3, \dots, 365$; where:

$$\begin{aligned} X_\tau(n) &= 0 \text{ if precipitation did not occur on day } n \\ X_\tau(n) &= 1 \text{ if precipitation occurred on day } n \end{aligned} \quad (1)$$

The dependence between wet and dry occurrences on successive days is modeled as a daily varying first order Markov chain with transition probabilities:

$$\begin{aligned} P_{ij}(n) &= P\{X_\tau(n) = j \mid X_\tau(n-1) = i\}; n = 2, 3, \dots, 365; i, j = 0, 1 \\ P_{ij}(n) &= P\{X_\tau = j \mid X_\tau(365) = i\}, n = 1 \end{aligned} \quad (2)$$

Because $P_{i1}(n) = 1 - P_{i0}(n)$; $i = 0, 1$, only two parameters are required for each day. To reduce the number of parameters that must be estimated and to insure smooth seasonal variations the daily values of the transition probabilities are described by a finite Fourier series:

$$P_{i0}(n) = \bar{P}_{i0} + \sum_{k=1}^{m_i} c_{ik} \sin(2\pi k / 365 + \Theta_{ik}); n = 1, 2, \dots, 365. \quad (3)$$

where $i = 0$ or 1 , m_i is the maximum number of harmonics required to describe the seasonal variability of the transition probability, \bar{P}_{i0} is the annual mean, c_{ik} is the amplitude, and Θ_{ik} is the phase angle in radians for the k th harmonic. The means, amplitudes and phase angles are estimated by maximum likelihood techniques (Woolhiser and Pegram, 1979; Roldan and Woolhiser, 1982).

The unconditional probability of a wet day can be closely approximated by the expression:

$$P\{X(n) = 1\} = [1 - P_{00}(n)] / [1 + P_{10}(n) - P_{00}(n)] \quad (4)$$

b. Distribution of daily precipitation

A mixed exponential distribution is used to describe the precipitation depth above a threshold, T :

$$f_n(y') = \frac{\alpha(n)\beta(n)\exp[-y'/\beta(n)]}{\beta(n)} + \frac{[1-\alpha(n)]\exp[-y'/\delta(n)]}{\delta(n)} \quad (5)$$

where $y' = y - T$; y is the daily precipitation, $\alpha(n)$ is a weighting parameter having values between 0 and 1; $\beta(n)$ and $\delta(n)$ are the means of the smaller and larger exponential distributions respectively. Let $\mu(n)$ be the mean of the mixed exponential distribution, specified by the following:

$$\mu(n) = \alpha(n)\beta(n) + [1-\alpha(n)]\delta(n) \quad (6)$$

The seasonal values of the parameters $\mu(n)$, $\delta(n)$ and $\alpha(n)$ are also described by Fourier series and the means amplitudes and phase angles are obtained by numerical optimization of the log likelihood function as described by Woolhiser et al. (1988). Significant harmonics are determined by the Akaike information criterion (AIC) (Akaike, 1974).

c. Expected precipitation accumulation on day m.

The Markov chain and the distribution of amounts are assumed independent and the precipitation amounts are assumed to be serially independent, so the expected total precipitation for m days can be written as:

$$E\{S(m)\} = \sum_{n=1}^m E\{X(n)Y(n)\} = \sum_{n=1}^m E\{X(n)\}E\{Y(n)\} \quad (7)$$

Where $Y(n)$ is the precipitation amount on day n . Thus the expectation can be written:

$$E\{S(m)\} = \sum_{n=1}^m [P\{X(n-1) = 0\}P_{01}(n) + P\{X(n-1) = 1\}P_{11}(n)][\mu(n) + T] \quad (8)$$

Expected annual precipitation is obtained when $m=365$. Leap years are not explicitly accounted for in this model although leap days can be included in the simulation mode.

d. Stochastic description of temperature and solar radiation

Daily maximum temperature (t_{\max}), minimum temperature (t_{\min}) and solar radiation (r) are described by a weakly stationary multivariate generating process based on work by Matalas (1967) and conditioned upon the precipitation occurrence process (Richardson, 1981).

The equation proposed by Richardson is:

$$t_i(n) = \chi_i(n)s_i(n) + \mu_i(n); \quad i = 1, 2, 3 \quad (9)$$

where $t_1(n)$ is the daily value of t_{\max} , $t_2(n)$ is the daily t_{\min} , $t_3(n)$ is the daily solar radiation, r , and $s_i(n)$ and $\mu_i(n)$ are the appropriate standard deviation and mean

respectively. The quantities, $s_i(n)$ and $\mu_i(n)$ are conditioned upon whether the day is dry or wet and the seasonal variation is described by Fourier series. $\chi_i(n)$ is a vector of residuals obtained from the following expression:

$$\chi_i(n) = A\chi_i(n-1) + B\varepsilon_i(n) \quad (10)$$

where $\chi_i(n)$ is a vector whose elements are the standardized residuals of t_{\max} , t_{\min} and r ; **A** and **B** are 3 by 3 matrices with elements that define the serial and cross-correlation coefficients; and ε_i is a vector of independent, normally distributed random variables with mean 0 and standard deviation of 1. The A and B matrices are:

$$\begin{aligned} A &= M_1 M_0^{-1} \quad \text{and} \\ BB^T &= M_0 - M_1 M_0^{-1} M_1^T \end{aligned} \quad (11)$$

where the superscripts -1 and T represent the inverse and transpose respectively. M_0 and M_1 are defined as:

$$M_0 = \begin{vmatrix} 1 & \rho_0(1,2) & \rho_0(1,3) \\ \rho_0(1,2) & 1 & \rho_0(2,3) \\ \rho_0(1,3) & \rho_0(2,3) & 1 \end{vmatrix} \quad (12)$$

$$M_1 = \begin{vmatrix} \rho_1(1) & \rho_1(1,2) & \rho_1(1,3) \\ \rho_1(2,1) & \rho_1(2) & \rho_1(2,3) \\ \rho_1(3,1) & \rho_1(3,2) & \rho_1(3) \end{vmatrix} \quad (13)$$

where $\rho_0(j,k)$ is the correlation coefficient between the variables j and k on the same day $\rho_1(j,k)$ is the correlation coefficient between the variables j and k with the variable k lagged one day and $\rho_1(j)$ is the lag one serial correlation coefficient for variable j . It has been found that the elements in matrices M_0 and M_1 exhibit very little spatial variability within the United States (Richardson, 1982). Average correlation coefficients given by Richardson (1982) and Richardson and Wright (1984) and the A and B matrices derived from them (Equation 11) are used in USCLIMATE (Hanson et al., 1994).

Equation 9 is utilized in the form:

$$t_j(n) = \mu_j(n)[\chi_j(n)c_j(n) + 1] \quad (14)$$

where $c_j(n)$ is the coefficient of variation. The seasonal changes in the means and coefficients of variation are specified by the expression:

$$u_j(n) = \bar{\mu}_j + c_j \cos[0.0172(n - D_j)], n = 1, 2, \dots, 365 \quad (15)$$

where $u_j(n)$ is the mean or coefficient of variation on day n , $\bar{\mu}_j$ is the annual mean, $c_j(n)$ is the amplitude of the first harmonic and D_j is the phase angle in days. Richardson and Wright (1984) presented maps of these variables determined from 31 U.S. stations. The maps in USCLIMATE are based upon 20 years of data from at least 40 stations (Hanson et al., 1994).

ADJUSTMENT OF USCLIMATE PARAMETERS FOR A CHANGED CLIMATE

a.) Markov Chain-Mixed Exponential Parameters

Woolhiser (1997) used a somewhat subjective procedure to modify the parameters in the Markov chain-mixed exponential (MCME) model in USCLIMATE to simulate precipitation sequences with a 150mm increase in annual precipitation

Possible future climate scenarios for Yucca Mountain have been proposed (DeWispelare et al., 1993). Although the conclusions by the experts were not consistent, all but one of the panelists predicted an increase in average annual precipitation during the 10,000 year time horizon. The maximum increase predicted was 150 mm greater than the present. (about a 100% increase). This estimate provides a bounding value and was adopted. No guidance was given regarding changes in the seasonal distribution of precipitation given the 150mm increase. The adjustment procedure used by Woolhiser (1997) follows.

An increase in the annual precipitation can result from an increase in the number of wet days or an increase in the mean depth of precipitation per wet day, or both. As an approximation we can write:

$$P + \Delta P = (N + \Delta N)(\mu + \Delta\mu) = N\mu + \mu\Delta N + N\Delta\mu + \Delta\mu\Delta N \quad (16)$$

Where:

P = present average annual precipitation

ΔP = Change in annual Precipitation = 150 mm. = 5.9 inches.

N = Expected present annual number of wet days = 37 (from Markov chain model).

ΔN = change in mean number of wet days.

μ = mean depth of rainfall per wet day. (0.158 inches) (from the mixed exponential model).

$\Delta\mu$ = change in mean depth of rainfall per wet day.

Substituting the above quantities in Equation 16 and simplifying:

$$\Delta P = 0.158\Delta N + 37\Delta\mu + \Delta\mu\Delta N = 5.9 \quad (17)$$

As an approximation, the first two terms on the right hand side of the equation were set equal to 2.4 inches.

Solving we obtain: $\Delta N = 15.19$ days and $\Delta \mu = 0.0649$ inches.

The first order Markov chain mean annual transition probabilities, P_{00} and P_{10} , were adjusted to achieve an increase of 15.19 wet days. If the transition probabilities were constant, the steady state probability of a wet day is:

$$P_1 = [1 - P_{00}][1 + P_{10} - P_{00}]^{-1} \quad (18)$$

Now by definition:

$$N = 365P_1 \quad \text{and} \quad \Delta N = 365\Delta P_1 = 15.19 \quad (19)$$

$$\Delta P_1 = \frac{\partial P_1}{\partial P_{00}} \Delta \bar{P}_{00} + \frac{\partial P_1}{\partial P_{10}} \Delta \bar{P}_{10} \quad (20)$$

Solving for ΔP_1 and setting $\Delta P_{00} = \Delta P_{10} = -0.0302$, we obtain estimates of the average annual transition parameters and the mean depth of rainfall per wet day.

$$\Delta \bar{P}_{00} = 0.9284 - 0.0302 = 0.8982$$

$$\Delta \bar{P}_{10} = 0.6541 - 0.0302 = 0.6239$$

$$\bar{\mu} = 0.1576 + 0.0649 = 0.2225$$

All amplitudes and phase angles for the Fourier series fit to the above parameters remained the same to preserve a similar seasonality. The above changes resulted in an increased frequency of wet days, increased persistence of rainfall and greater mean daily rainfall depths. Such changes are consistent with increased atmospheric instability for all seasons.

Although the above procedure results in simulated sequences of precipitation with an expected annual value 150mm greater than present, it is not clear that the adjustments in the mean annual values of \bar{P}_{00} , \bar{P}_{10} and $\bar{\mu}$ are realistic. If one can accept the hypothesis that a future wetter and cooler climate at Yucca Mountain would be similar to the climates presently existing at nearby locations at higher elevations, the relationships developed by Hanson et al. (1989) could be useful. Hanson et al. (1989) utilized data from a network of raingages on the Reynolds Creek Experimental Watershed in southwest Idaho to evaluate the effect of mean annual precipitation on parameters of the MCME model. They used procedures described by Woolhiser and Roldan (1986) to estimate the MCME model parameters for each of the 16 gages on Reynolds

Creek Experimental Watershed. The annual precipitation at these gages ranged from 241 to 1144mm and the mean annual number of wet days ranged from 84 to 133.9. Thus the projected annual precipitation at Yucca Mountain (165+150 = 315mm) is within the range of the Idaho stations.

Hanson et al. (1989) utilized regression techniques to determine the relationships between MCME parameters and mean annual precipitation, X. The following relationships were significant for the Markov chain:

$$\Theta_1 = \ln\left[\frac{\bar{P}_{00}}{1 - \bar{P}_{00}}\right] = 2.506 - 0.165(\ln X); (R^2 = 0.94) \quad (21)$$

$$\Theta_2 = \ln\left[\frac{\bar{P}_{10}}{1 - \bar{P}_{10}}\right] = 2.866 - 0.497(\ln X); (R^2 = 0.96) \quad (22)$$

They also found significant relationships between the amplitudes of the first harmonics of P_{00} and P_{10} and mean annual precipitation.

The following relationships were significant for the mixed exponential distribution:

$$\Theta_3 = \ln\left[\frac{\bar{\alpha}}{1 - \bar{\alpha}}\right] = -0.0449 - 0.00115X; (R^2 = 0.74) \quad (23)$$

$$\bar{\mu} = 1.644 + 0.00531X; (R^2 = 0.99) \quad (24)$$

They also found that the first phase angle of μ decreased nonlinearly with X and that the amplitude of the first phase angle of μ remained constant for stations with 55mm of annual precipitation or less and then increased linearly.

It would be unrealistic to assume that the above regression equations would provide realistic estimates of the parameters of the MCME model for Yucca Mountain under current or future climates. However, realistic adjustments to existing parameters may be made by utilizing the derivatives of the parameters with respect to annual precipitation in the regression equations.

By differentiating Equations (21), (22), (23) and (24) we obtain:

$$\frac{d\Theta_1}{dX} = -\frac{0.165}{X} \quad (25)$$

$$\frac{d\Theta_2}{dX} = -\frac{0.497}{X} \quad (26)$$

$$\frac{d\Theta_3}{dX} = -0.00115 \quad (27)$$

$$\frac{d\bar{\mu}}{dX} = 0.00531 \quad (28)$$

If we approximate the corrections to each mean parameter by the expression:

$$\Delta U = \frac{dU}{dX} \Delta X \quad (29)$$

where U is the mean of the appropriate function and ΔX is the difference in mean annual precipitation (150mm), we obtain the corrections shown in the following table.

Table 1
Comparison of corrections to MCME mean parameter values

<i>Parameter</i>	<i>Correction by Woolhiser</i>	<i>Correction by Regression</i>
$\Delta \bar{P}_{\infty}$	-0.0302	-0.0106
$\Delta \bar{P}_{10}$	-0.0302	-0.108
$\Delta \bar{\mu}$	1.65mm	0.77mm
$\Delta \bar{\alpha}$	No correction	0.07

An examination of Table 1 reveals that the arbitrary adjustments by Woolhiser are not consistent with those implied by the regression relationships found by Hanson et al. (1989). The corrections by Hanson et al. (1989) provide for an increased number of wet days by a greater increase in the persistence, a smaller increase in the dry to wet transition probability and also provide a smaller increase in the mean depth per wet day.

b.) Maximum temperature, minimum temperature and solar radiation parameters

Because Woolhiser (1997) was only interested in simulating precipitation, he did not examine the problem of adjusting the parameters in Equations (9) through (15) to reflect a cooler climate. It should be noted that when the MCME model is adjusted to reflect a wetter climate, there will be an automatic adjustment in the temperature and radiation regimes, because t_{\max} , t_{\min} and r are conditioned on whether the day is wet or dry. For example, in the Yucca Mountain vicinity the mean for t_{\max} is about ten degrees F lower on a wet day than on a dry day and the mean solar radiation on a wet day is about 180 Langleys smaller than on a dry day. Because the elements in the matrices (12) and (13) show very little variation over the continental U.S., we should not expect any change for future climate. We should also expect no change in the radiation process (although it could be adjusted to reflect the aspect of specific hillslopes). If the realizations of the t_{\max} , and t_{\min} processes, given an adjustment in the precipitation process do

not result in the hypothesized mean annual temperature, it would be easy to adjust the annual means of t_{\max} , and t_{\min} to make the required correction.

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DWS

**PROPOSED PROJECT ON DEVELOPING TECHNIQUES TO ADJUST
PARAMETERS OF THE USCLIMATE MODEL TO REFLECT CLIMATE
CHANGE**

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Objective

To develop a stochastic weather model that can simulate sequences of daily precipitation, maximum temperature, minimum temperature and solar radiation for Yucca Mountain under present and future climate conditions.

Procedures and Estimate of Professional Time

- 1) Obtain a minimum of 30 years of daily precipitation data for nearby weather stations, including Las Vegas, Beatty and a station with about 165mm of annual precipitation. (3 hrs)
- 2) Utilize the Fortran programs MCLOGIT to estimate the MCME parameters for those stations. The MCLOGIT program utilizes the logit transform of the Markov chain transition probabilities and results in a much better fit to monthly statistics for arid regions than the algorithms used by Hanson et al. (1994). (6 hrs)
- 3) Adjust the parameters obtained above to match the current annual precipitation at Yucca Mountain, using the regressions of Hanson et al. (1989). (6 hrs)
- 4) Compare precipitation statistics generated with this model to those used in the Solitario Canyon simulations and summarize the implications for the channel infiltration study. (8 hrs)
- 5) Utilize the regression relationships of Hanson et al. (1989) to adjust parameters in the MCME model for a wetter future climate and develop procedures to adjust the amplitudes and phase angles of significant harmonics to change the seasonality (i.e. a relative increase in winter precipitation. One possibility would be to postulate the expected annual accumulation of precipitation in a future climate (see Equation 8) and then to minimize a sum of squares objective function by adjusting amplitudes and phase angles of the Fourier series for the transition probabilities. (24 hrs)
- 6) Generate sequences of t_{max} , t_{min} and r and adjust mean temperature parameters to match the hypothesized mean annual temperature. (16 hrs)
- 7.) Write a technical paper describing the development of procedures to adjust parameters of a stochastic weather for future climates. (40 hrs.)

DELIVERABLES

- 1.) A stochastic weather generator to provide daily sequences that can be used as input to water balance models for modeling the runoff and infiltration regime at Yucca Mountain under present and future climate conditions.
- 2.) A technical paper describing the techniques developed to adjust weather generator parameters for future climates.

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Nevada Station Data Inventory

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NOAA/NWS cooperative observer network

From NCDC Station Historical Listing for NWS Cooperative Network
 ObsTyp: t-Temperature-1, p-Daily precip-2, w-(blank), s-(blank), e-Evap-5
 h-Hourly precip - 6 0.01" Universal, or - 7 0.10" Fisher-Porter
 U - Observed, but beginning date is uncertain

Count	Number	Station Name	Lat	Long	Elev	Start	ObsTyp	End
=====	(Coop)	(From NCDC listing)	ddmm	dddmm	ftx10	yy mm	tpwseh	yy mm
=====	=====	=====	=====	=====	=====	=====	=====	=====
1	-							
2	-							
3	260012-2	ACHURRA RANCH	4026	11535	0651	52 11		54 05
4	260012-2	ACHURRA RANCH	4026	11535	0614	54 05		56 07
5	260015-3	ACOMA	3731	11410	0553	49 12		58 12
6	260035-3	ADAMS RANCH	3618	11544	0871	66 07		76 07
7	260046-3	ADAVEN	3807	11535	0625	48 07	UU	80 06
1973 m 8	260046-3	ADAVEN	3807	11535	0625	80 12	UU	82 04
9	260099-4	ALAMO	3722	11109	-999	48 07	UU U	54 11
10	260099-4	ALAMO	3722	11510	-999	54 11	UU U	64 02
11	260109-4	ALAMO MNTC STN	3722	11509	0410	48 07		49 08
12	260150-4	AMARGOSA RANCH	3632	11630	0237	65 11		70 10
13	260150-4	AMARGOSA FARMS GAREY	3634	11628	0245	78 03	UU	86 03
14	260150-4	AMARGOSA FARMS GAREY	3634	11628	0245	86 03	12	99 99
15	260191-6	AMERICAN BEAUTY	4031	11526	0801	58 10		69 09
16	260232-2	ANGEL LAKE	4102	11506	0833	00 00		76 07
17	260282-2	ANTELOPE VALLEY FARR	3957	11725	0490	84 07	12	99 99
18	260438-2	ARTHUR 5 NW	4048	11511	0640	48 07	UU	61 12
19	260438-2	ARTHUR 5 NW	4047	11511	0628	63 07	UU	76 09
20	260438-2	ARTHUR 5 NW	4047	11511	0631	76 09	UU	86 06
21	260438-2	ARTHUR 4 NW	4047	11511	0630	86 06	12	99 99
22	260480-3	ATLANTA MINE	3827	11420	0680	81 04	UU	85 09
23	260507-2	AUSTIN	3930	11705	0661	48 07	UU U	48 12
24	260507-2	AUSTIN	3930	11705	0655	49 02	UU U	57 12
25	260507-2	AUSTIN	3930	11705	0660	58 01	UU U	59 12
26	260507-2	AUSTIN	3930	11705	0660	60 01	UU U	65 12
27	260507-2	AUSTIN	3930	11705	0660	66 01	UU U	99 99
28	260645-3	BARCLAY CROSSING	3731	11416	0551	49 12		74 03
29	260668-3	BASALT	3800	11816	0636	48 07		59 06
30	260688-W	BATTLE MOUNTAIN	4039	11656	0451	31 01		45 12
31	260691-2	BATTLE MOUNTAIN FAA AIR	4037	11652	0453	48 07	UU U	48 12
32	260691-2	BATTLE MOUNTAIN FAA AIR	4037	11652	0453	49 01	UU U	62 12
33	260691-2	BATTLE MOUNTAIN 2	4038	11656	0452	63 01		64 10
34	260691-2	BATTLE MOUNTAIN AIRPORT	4035	11654	0454	81 07	UU U	86 04
35	260691-2	BATTLE MOUNTAIN AIRPORT	4035	11654	0454	86 04	12	U 87 11
36	260691-2	BATTLE MOUNTAIN AIRPORT	4037	11652	0453	87 11	12	U 89 03
37	260691-2	BATTLE MOUNTAIN 4 SE	4037	11653	0454	89 05	12	7 99 99
38	260714-4	BEATTY	3654	11645	0331	48 07	UU U	57 01
1673 m 39	260714-4	BEATTY	3654	11645	0330	57 01	UU U	58 11
40	260714-4	BEATTY	3655	11645	0330	58 11	UU U	72 11
41	260718-4	BEATTY 8 N	3700	11643	0355	72 11	UU U	84 09
42	260718-4	BEATTY 8 N	3700	11643	0355	84 10	12	7 99 99
43	260795-2	BEOAWAWE	4036	11629	0470	49 07	UU	87 05
44	260795-2	BEOAWAWE	4036	11629	0470	87 05	U2	87 11
45	260795-2	BEOAWAWE	4036	11629	0470	87 11	12	99 99
46	260800-2	BEOAWAWE GUND RANCH	3954	11635	0575	72 06	UU U	87 12

47	260800-2	BEOWAWE U OF N RANCH	3954	11635	0574	87	12	12	5	99	99
48	260805-3	BERLIN STATE PARK	3852	11735	0694	85	07	12		88	04
49	260805-3	BERLIN STATE PARK	3852	11735	0693	88	04	12		88	04
50	260820-2	BIG BEND	4146	11541	0671	63	09			76	09
51	260840-1	BILK CREEK	4150	11825	0700	65	11			UN	KN
52	260955-3	BLUE EAGLE RANCH HANKS	3832	11533	0478	78	03	UU		85	08
53	260955-3	BLUE EAGLE RANCH HANKS	3832	11533	0478	85	08	12		86	01
54	260955-3	BLUE EAGLE RANCH HANKS	3832	11533	0478	86	01	12	7	99	99
55	260961-3	BLUE JAY HIGHWAY STN	3823	11613	0532	63	05	UU	U	85	04
56	260990-1	BLUE LAKE	4139	11843	0801	62	07			74	10
57	261071-4	BOULDER CITY	3559	11451	0252	48	07	UU	U	85	10
58	261071-4	BOULDER CITY	3559	11451	0252	85	10	12	5	99	99
59	261076-4	BOULDER CITY AIRPORT	3559	11450	-999	36	08			37	12
60	261076-4	BOULDER CITY AIRPORT	3559	11450	-999	38	04			37	12
61	261076-4	BOULDER CITY AIRPORT	3558	11450	-999	50	02			UN	KN
62	261160-1	BRINKERHOFF RANCH	4005	11740	0366	66	06	UU		81	10
63	261308-1	BUCKSKIN MOUNTAIN	4147	11733	0781	48	07			67	08
64	261311-1	BUFFALO RANCH	4023	11728	0543	66	06	UU		82	02
65	261317-2	BULL CREEK RANCH	3903	11537	0591	63	07	UU		66	09
66	261320-3	BUNKER PEAK	3727	11407	0558	49	12			76	09
67	261324-4	BUNKERVILLE	3646	11408	0154	52	03			53	11
68	261327-4	BUNKERVILLE 2 SW	3645	11409	0152	79	11	UU		83	03
69	261327-4	BUNKERVILLE	3646	11407	0155	83	03	12		99	99
70	261330-4	BUNKERVILLE MOUNTAIN	3637	11412	0325	66	07			76	07
71	261348-1	CABIN CREEK	4143	11730	0611	59	12			74	10
72	261355-4	LITTLE RED ROCK	3609	11525	0380	72	04	UU		73	07
73	261358-3	CALIENTE	3737	11431	0440	48	07	UU		84	12
74	261358-3	CALIENTE	3737	11431	0440	84	12	12		99	99
75	261371-4	CALLVILLE BAY	3609	11444	0127	89	07	12		99	99
76	261400-1	CANYON CREEK	4144	11735	0700	62	07			74	10
77	261415-2	CARLIN GOLD MINE	4058	11619	0653	66	10	UU		69	03
78	261415-2	CARLIN GOLD MINE	4058	11619	0654	69	03	UU		71	06
79	261415-2	CARLIN GOLD MINE	4058	11619	0653	71	06	UU		86	03
80	261415-2	CARLIN GOLD MINE	4058	11619	0653	86	03	12		88	03
81	261415-2	CARLIN GOLD MINE	4058	11619	0652	88	03	12		89	08
82	261415-2	CARLIN NEWMONT MINE	4058	11619	0652	89	08	12		99	99
83	261443-4	CARP	3707	11430	0300	49	05			51	09
84	261443-4	CARP	3707	11430	0260	51	09			62	11
85	261485-1	CARSON CITY	3909	11946	0465	48	07	UU		84	05
86	261485-1	CARSON CITY	3909	11946	0465	84	05	12		99	99
87	261630-2	CENTRAL NEVADA FIELD LA	3923	11719	0596	65	10	UU	U	86	11
88	261660-2	CHARLESTON	4139	11531	0600	61	07	UU		71	01
89	261680-2	CHARNAC BASIN	3919	11627	0851	54	11			76	07
90	261684-2	CHERRY CREEK	3955	11453	0613	66	12	UU	U	68	08
91	261692-1	CHICKEN CREEK	4136	11842	0640	61	01			74	10
92	261718-W	CLAY CITY	3626	11624	0219	31	01			37	12
93	261725-1	CLEAR CREEK CANYON	4044	11737	0511	59	09			74	10
94	261740-W	CLOVER VALLEY	4044	11502	0580	31	01	UU		41	12
95	261740-2	CLOVER VALLEY	4052	11502	0575	65	09	UU		86	06
96	261740-2	CLOVER VALLEY	4052	11502	0575	86	06	12		99	99
97	261755-3	COALDALE	3803	11754	0465	48	07	UU		53	05
98	261755-3	COALDALE	3802	11753	0464	53	05	UU		55	05
99	261755-3	COALDALE	3802	11753	0465	55	05	UU		58	11
100	261755-3	COALDALE	3803	11754	0460	63	07	UU		65	01
101	261790-3	COLD CREEK RANCH	3625	11544	0611	48	07			76	07
102	261889-2	CONNORS PASS	3902	11439	0733	53	10			76	07
103	261905-2	CONTACT	4147	11445	0537	48	07	UU	U	87	10
104	261905-2	CONTACT	4147	11446	0545	87	10	12	U	87	12
105	261905-2	CONTACT	4147	11445	0536	88	03	12	7	99	99
106	261925-2	COON CREEK SUMMIT	4148	11529	0831	48	11			76	07
107	261975-2	CORTEZ GOLD MINE	4011	11638	0491	68	09	UU		80	05
108	262020-2	COTTONWOOD RANCH	4006	11721	0540	48	07			49	08
109	262025-1	COW CREEK	4037	11847	0591	67	03			76	05
110	262035-3	CRESTLINE	3740	11408	0580	49	11			76	10

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111	262078-3	CURRANT	3845	11528	0518	48	07	53	11
112	262086-3	CURRANT CREEK SUMMIT	3849	11517	0682	53	10	76	07
113	262091-3	CURRANT HWY STN	3848	11521	0624	63	04	UU	78
114	262096-2	CURRIE HIGHWAY STN	4016	11443	0582	61	11	UU	74
115	262096-2	CURRIE HIGHWAY STN	4016	11445	0582	85	04	12	99
116	262119-1	DAGGET PASS	3859	11953	0733	88	11	12	99
117	262189-2	DEETH 2 SW	4104	11517	0534	51	11	UU	65
118	262189-2	DEETH 2 SW	4104	11516	0535	65	08	UU	66
119	262189-2	DEETH 2 SW	4104	11516	0534	66	11	UU	86
120	262189-2	DEETH 2 SW	4104	11516	0534	86	06	12	99
121	262229-1	DENIO JUNCTION	4159	11838	0419	51	10	UU	67
122	262229-1	DENIO JUNCTION	4158	11838	0419	67	11	UU	86
123	262229-1	DENIO JUNCTION	4158	11838	0419	86	05	12	99
124	262243-4	DESERT GAME RANGE	3626	11522	0292	48	07	UU	86
125	262243-4	DESERT GAME RANGE	3626	11522	0292	86	03	12	99
126	262251-4	DESERT ROCK WSMO	3637	11601	0330	84	04	12	99
127	262276-3	DIABLO	3755	11603	0511	59	08	UU	79
128	262296-2	DIAMOND VALLEY DUBOSE	3941	11556	0591	71	08	UU	72
129	262296-2	DIAMOND VALLEY DUBOSE	3941	11556	0597	79	07	UU	86
130	262296-2	DIAMOND VALLEY DUBOSE	3941	11556	0597	86	08	12	90
131	262296-2	DIAMOND VALLEY USDA	3941	11602	0597	90	06	12	99
132	262301-2	DIAMOND VALLEY	3942	11601	0585	63	04		64
133	262301-2	DIAMOND VALLEY	3941	11603	0591	64	12		66
134	262301-2	DIAMOND VALLEY POLLARD	3947	11555	0586	66	02	UU	68
135	262301-2	DIAMOND VALLEY POLLARD	3948	11555	0584	68	06	UU	68
136	262301-2	DIAMOND VALLEY POLLARD	3948	11556	0591	68	09	UU	71
137	262306-1	DISASTER PEAK	4157	11811	0700	61	01		74
138	262311-1	DIXIE VALLEY	4005	11740	0366	65	05	UU	66
139	262315-1	DIXIE VALLEY STARK	3943	11811	0354	71	10	UU	77
140	262315-1	DIXIE VALLEY STARK	3941	11806	0350	77	10	UU	79
141	262315-1	DIXIE VALLEY STARK	3943	11811	0354	79	04	UU	80
142	262318-1	DIXIE VALLEY BOYER	3957	11752	0360	81	12	UU	83
143	262332-2	DOBY SUMMIT	4054	11552	0660	53	09		76
144	262350-2	DOLLY VARDEN	4020	11431	0660	81	11	UU	U 82
145	262350-2	DOLLY VARDEN	4020	11431	0660	82	03	12	U 83
146	262350-2	DOLLY VARDEN	4020	11431	0661	83	01	12	U 85
147	262375-3	DONOHUE RANCH	3817	11416	0683	64	01		76
148	262380-2	DORSEY BASIN	4053	11513	0811	63	08	U	76
149	262390-3	DUCKWATER	3854	11543	0540	66	09	UU	86
150	262390-3	DUCKWATER	3854	11543	0540	86	07	12	88
151	262390-3	DUCKWATER	3857	11543	0561	88	09	12	99
152	262394-1	VIRGIN VALLEY	4152	11901	0480	59	08	UU	83
153	262394-1	VIRGIN VALLEY	4152	11901	0480	83	07	12	99
154	262406-1	DUN GLEN	4045	11753	0591	59	09		74
155	262416-1	DUTCH FLAT MINE	4110	11730	0480	59	10		74
156	262431-3	DYER	3743	11805	0495	48	07		51
157	262431-3	DYER	3740	11804	0495	51	12		53
158	262431-3	DYER 4 SE	3737	11801	0498	53	05	UU	85
159	262431-3	DYER 4 SE	3737	11801	0498	85	05	1U	86
160	262431-3	DYER 4 SE	3737	11802	0498	86	11	12	88
161	262431-3	DYER	3741	11805	0490	88	10	12	99
162	262436-3	EAGLE VALLEY STATE PARK	3802	11411	0596	73	08	UU	74
163	262477-1	EASTGATE	3918	11753	0502	48	07		69
164	262497-4	ECHO BAY	3619	11424	0125	89	07	12	99
165	262557-4	ELGIN	3721	11432	0339	51	03		68
166	262557-4	ELGIN	3721	11433	0342	85	07	12	7
167	262562-4	ELGIN 3 SE	3719	11430	0330	65	04	UU	U 85
168	262573-2	ELKO WB AIRPORT	4050	11547	0508	48	01	UU	U 63
169	262573-2	ELKO WB AIRPORT	4050	11547	0505	64	01	UU	U 64
170	262573-2	ELKO WB AIRPORT	4050	11547	0509	65	01	UU	U 66
171	262573-2	ELKO WB AIRPORT	4050	11547	0505	67	01	UU	U 99
172	262631-2	ELY WBO	3917	11451	0626	48	01	UU	U 61
173	262631-2	ELY WBO	3917	11451	0625	62	01	UU	U 99
174	262656-2	EMIGRANT PASS HWY STN	4039	11618	0576	54	08	UU	86

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175	262656-2	EMIGRANT PASS HWY STN	4039	11618	0576	86	06	12	99	99	
176	262662-1	GERLACH	4035	11920	0398	00	00	UU	57	10	
177	262662-1	GERLACH	4035	11921	0395	73	09	UU	78	02	
178	262708-2	EUREKA	3931	11558	0655	52	09	UU	85	09	
179	262708-2	EUREKA	3931	11558	0654	85	09	12	99	99	
180	262770-1	FALLON CAA AIRPORT	3925	11843	0394	48	11		55	01	
181	262780-1	FALLON EXPERIMENT STN	3927	11847	0397	48	07	UU	U	84	06
182	262780-1	FALLON EXPERIMENT STN	3927	11847	0397	84	06	12	U	99	99
183	262820-2	FERGUSON SPRINGS HMS	4025	11411	0584	72	09	UU	U	82	11
184	262820-2	FERGUSON SPRINGS HMS	4025	11411	0584	82	11	12	U	83	02
185	262840-1	FERNLEY	3936	11915	0420	49	06	UU	U	52	04
186	262840-1	FERNLEY	3937	11915	0416	54	06	UU	U	74	08
187	262849-1	FERNLEY MNTC STN	3937	11916	0416	48	07			54	07
188	262860-2	FISH CREEK RANCH	3916	11600	0605	48	07	UU	U	66	09
189	262903-1	FLEISH POWER HOUSE	3929	11959	0500	58	12			59	09
190	262948-3	GABBS	3852	11755	0463	79	05	UU		85	01
191	262984-1	GARDNERVILLE E FK CSN	3851	11942	0499	67	07			99	99
192	263090-1	GERLACH	4035	11924	0398	48	07			51	01
193	263090-1	GERLACH	4039	11921	0394	62	06	UU		72	01
194	263090-1	GERLACH	4039	11921	0395	72	01	UU		73	09
195	263090-1	GERLACH GREEN	4039	11921	0395	85	08	12		85	10
196	263090-1	GERLACH	4039	11921	0395	85	11	12		99	99
197	263095-1	GETCHELL MINE	4113	11715	0580	59	12			74	03
198	263101-3	GEYSER	3838	11438	0598	48	07	UU		60	08
199	263101-3	GEYSER RANCH	3840	11438	0602	60	08	UU		81	01
200	263101-3	GEYSER RANCH	3840	11438	0602	85	11	12		88	02
201	263114-2	GIBBS RANCH	4133	11513	0600	52	11	UU		86	06
202	263114-2	GIBBS RANCH	4133	11513	0600	86	06	12		99	99
203	263205-1	GLENBROOK	3905	11956	0640	48	07	UU		72	04
204	263205-1	GLENBROOK	3905	11956	0642	72	04	UU		75	08
205	263205-1	GLENBROOK	3905	11957	0636	75	08	UU		99	99
206	263245-1	GOLCONDA	4057	11729	0439	48	07	UU		86	04
207	263245-1	GOLCONDA	4057	11729	0439	86	04	12		99	99
208	263250-1	GOLCONDA TIPTON RANCH	4045	11730	0465	78	08	UU		83	01
209	263285-3	GOLDFIELD	3743	11713	0571	48	07	UU		50	10
210	263285-3	GOLDFIELD	3742	11714	0569	50	10	UU		84	09
211	263285-3	GOLDFIELD	3742	11714	0569	85	04	12		99	99
212	263303-2	GONCE CREEK	4118	11555	0637	48	11			61	08
213	263340-2	GREAT BASIN NATL PARK	3900	11413	0683	87	04	12		88	11
214	263340-2	GREAT BASIN NATL PARK	3900	11413	0683	88	11	12	7	99	99
215	263358-2	GREEN MOUNTAIN	4022	11531	0801	63	08			76	09
216	263450-2	HANKS CREEK	4127	11523	0671	48	11			76	07
217	263465-1	HARDSCRABBLE	4131	11722	0551	59	09			74	03
218	263498-2	HARRISON PASS	4020	11531	0731	48	07			76	10
219	263512-3	HAWTHORNE	3831	11838	0433	54	08	UU		55	08
220	263512-3	HAWTHORNE	3832	11838	0433	61	07	UU		64	11
221	263515-3	HAWTHORNE BABBITT	3832	11839	0418	48	07	UU	U	54	08
222	263515-3	HAWTHORNE BABBITT	3833	11840	0413	57	06	UU	U	74	08
223	263515-3	HAWTHORNE BABBITT	3833	11840	0417	74	08	UU	U	80	10
224	263515-3	HAWTHORNE AIRPORT	3833	11840	0422	80	10	UU	U	90	11
225	263515-3	HAWTHORNE AIRPORT	3833	11840	0422	90	11	12	7	99	99
226	263653-3	HIDDEN FOREST CAMP	3638	11512	0756	48	07			76	10
227	263671-3	HIKO	3733	11513	0394	89	07	12		99	99
228	263724-1	HINKEY SUMMIT	4140	11733	0825	52	10			72	02
229	263816-1	HUALAPAI VALLEY FITTS	4054	11918	0413	69	02	UU		71	03
230	263853-W	HUMBOLDT FIELD	4005	11809	0416	32	01			47	12
231	263940-2	I-L RANCH	4134	11624	0520	62	07	UU		70	10
232	263957-1	IMLAY	4040	11809	0421	48	07			68	05
233	263957-1	IMLAY	4039	11809	0426	68	05	12		99	99
234	263980-4	INDIAN SPRINGS	3635	11541	0312	48	07			64	11
235	263989-3	IONE 11 SE	3851	11729	0700	52	09			76	07
236	264016-2	JACKPOT	4159	11450	0529	86	03	12		99	99
237	264026-2	JACKS CREEK PASS	4133	11600	0774	48	07			76	10
238	264030-1	JACKSON CREEK	4118	11828	0620	65	10			74	10

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239	264038-2	JARBIDGE	4152	11526	0616	48	07		61	10	
240	264038-2	JARBRIDGE 4 N	4156	11526	0617	90	08	12	99	99	
241	264086-2	JIGGS	4025	11540	0520	48	07		52	08	
242	264086-2	JIGGS	4026	11540	0545	52	08	UU	U	63	08
243	264086-2	JIGGS	4025	11540	0547	63	08		70	09	
244	264086-2	JIGGS	4027	11539	0542	70	09	UU	U	72	03
245	264090-2	JIGGS 13 N	4036	11542	0540	72	03	UU	U	75	10
246	264095-2	JIGGS 3 ENE ZAGA	4028	11537	0576	78	09	UU	U	85	06
247	264095-2	JIGGS 3 ENE ZAGA	4028	11537	0576	85	06	1U	U	87	05
248	264095-2	JIGGS 8 SSE ZAGA	4021	11537	0580	87	05	12	U	89	03
249	264095-2	JIGGS 8 SSE ZAGA	4021	11537	0580	89	03	12		99	99
250	264108-1	JUNGO MEYER RANCH	4054	11826	0420	68	10	UU		69	07
251	264108-1	JUNGO MEYER RANCH	4053	11826	0420	69	07	UU		86	05
252	264128-1	KELLY CREEK RANCH	4116	11706	0511	59	09			74	03
253	264143-3	KEY PITTMAN WMA	3737	11513	0395	64	03	UU		86	07
254	264143-3	KEY PITTMAN WMA	3737	11513	0395	86	07	1U		88	05
255	264143-3	KEY PITTMAN WMA	3737	11513	0395	88	05	12		89	07
256	264199-2	KIMBERLY	3916	11502	0723	48	07			58	06
257	264226-1	KINGS RIVER CANYON	4158	11818	0580	60	12			74	10
258	264236-1	KINGS RIVER VALLEY	4146	11813	0424	56	10	UU		68	06
259	264236-1	KINGS RIVER VALLEY	4145	11814	0424	68	06	UU		85	05
260	264236-1	KINGS RIVER VALLEY	4145	11814	0424	85	05	1U		87	11
261	264236-1	KINGS RIVER VALLEY	4145	11814	0423	87	11	12		99	99
262	264255-2	KINGSTON CANYON	3912	11706	0676	55	10			76	07
263	264259-2	KINGSTON SUMMIT	3918	11707	0851	55	10			76	07
264	264268-2	KNOLL CREEK FIELD STN	4138	11444	0600	71	11	UU		79	12
265	264314-3	KYLE CANYON RANGER STN	3616	11538	0718	48	07			49	01
266	264314-3	KYLE CANYON RANGER STN	3615	11536	0721	57	10			76	07
267	264341-2	LAGES	4003	11437	0596	83	11	12		85	04
268	264341-2	LAGES	4003	11437	0596	85	04	12	7	99	99
269	264349-1	LAHONTAN	3928	11904	0416	48	07	UU		78	04
270	264349-1	LAHONTAN	3928	11904	0415	78	04	UU		88	03
271	264349-1	LAHONTAN	3928	11904	0415	88	03	12		99	99
272	264369-1	LAKE MEAD EVAPORATION	3601	11449	0172	69	03	UU	U	76	12
273	264379-3	LAKE VALLEY	3822	11437	0598	66	08	UU		72	01
274	264384-3	LAKE VALLEY STEWARD	3819	11439	0636	70	11	UU		85	08
275	264384-3	LAKE VALLEY STEWARD	3819	11439	0635	85	08	UU		89	04
276	264384-3	LAKE VALLEY STEWARD	3819	11439	0635	89	04	12		99	99
277	264390-2	LAMOILLE CANYON	4038	11521	0851	67	08			76	07
278	264392-2	LAMOILLE 3 E	4044	11526	0631	72	10	UU		75	09
279	264394-2	LAMOILLE MILLER RANCH	4042	11533	0580	75	10	UU		82	02
280	264394-2	LAMOILLE MILLER	4045	11540	0575	82	02	12		83	05
281	264394-2	LAMOILLE YOST	4043	11531	0584	83	05	12		89	08
282	264394-2	LAMOILLE YOST	4043	11531	0584	89	08	12	7	99	99
283	264395-2	LAMOILLE PH	4041	11528	0629	48	07	UU		72	07
284	264429-4	LAS VEGAS	3610	11508	0201	48	07			56	12
285	264434-4	LAS VEGAS WB AIRPORT	3614	11502	0188	48	01			49	01
286	264436-4	LAS VEGAS WSO AIRPORT	3605	11510	0217	49	01	UU	U	75	12
287	264436-4	LAS VEGAS WSO AIRPORT	3605	11510	0216	76	01	UU	U	99	99
288	264457-4	LATHROP WELLS	3638	11624	0266	48	07			52	03
289	264457-4	LATHROP WELLS	3639	11623	0267	52	03			54	07
290	264457-4	LATHROP WELLS	3639	11624	0267	54	07			64	02
291	264473-4	LATHROP WELLS 16 SSE	3625	11621	0218	70	11	UU		78	03
292	264480-4	LAUGHLIN	3510	11437	0068	83	10			87	12
293	264480-4	LAUGHLIN	3510	11437	0068	87	12	12		99	99
294	264491-2	LEE	4034	11537	0600	99	10			47	06
295	264500-3	LEE CANYON	3618	11541	0921	54	10			76	07
296	264502-3	LEE CANYON SUMMIT	3618	11541	0901	48	07			54	10
297	264514-2	LEHMAN CAVES NM	3900	11413	0683	48	07	UU		84	09
298	264514-2	LEHMAN CAVES NM	3900	11413	0683	84	09	12		87	04
299	264527-1	LEONARD CREEK RANCH	4131	11843	0423	54	12	UU	U	81	07
300	264527-1	LEONARD CREEK RANCH	4131	11843	0422	81	07	UU	U	88	07
301	264527-1	LEONARD CREEK RANCH	4131	11843	0422	88	07	12	U	99	99
302	264542-W	LEWERS RANCH	3914	11951	0520	31	01			44	12

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303	264585-1	LIMERICK PASS	4019	11810	0620	59	11		76	07
304	264600-4	LITTLE RED ROCK	3609	11525	0380	65	02	UU	71	10
305	264618-1	LITTLE VALLEY	3915	11952	0631	54	11		76	07
306	264646-W	LOGANDALE	3636	11429	0140	31	01		38	12
307	264651-4	LOGANDALE UN EXPERIMENT	3634	11428	0132	68	01	UU	U	85 02
308	264651-4	LOGANDALE UN EXPERIMENT	3634	11428	0132	85	02	1U	U	88 03
309	264651-4	LOGANDALE	3637	11429	0141	88	09	12		88 12
310	264651-4	LOGANDALE	3637	11429	0141	88	12	12	7	89 08
311	264651-4	LOGANDALE	3637	11429	0141	89	08	12	57	99 99
312	264675-3	LOVELL SUMMIT	3613	11536	0831	45	07			47 07
313	264698-1	LOVELOCK	4011	11828	0398	48	07	UU	U	82 01
314	264698-1	LOVELOCK	4011	11828	0397	82	01	UU	U	82 07
315	264698-1	LOVELOCK	4011	11828	0397	82	07	12	U	99 99
316	264700-1	LOVELOCK DERBY FIELD	4004	11833	0390	48	07	UU		50 12
317	264700-1	LOVELOCK DERBY FIELD	4004	11833	0393	51	01	UU		55 12
318	264700-1	LOVELOCK DERBY FIELD	4004	11833	0390	56	01	UU		81 12
319	264700-1	LOVELOCK FAA AIRPORT	4004	11833	0390	81	12	UU		82 02
320	264700-1	LOVELOCK FAA AIRPORT	4004	11833	0390	82	02	12		84 09
321	264700-1	LOVELOCK FAA AIRPORT	4004	11833	0390	88	03	12		99 99
322	264715-1	LOVELY VALLEY	4150	11825	0700	65	10			74 10
323	264721-2	LOWER ROBINSON	3925	11505	0757	66	10			74 03
324	264725-2	LOWER TROUT CREEK	4105	11502	0691	63	08			76 09
325	264745-2	LUND	3851	11500	0555	57	08	UU		65 11
326	264745-2	LUND	3851	11500	0557	65	11	UU		86 07
327	264745-2	LUND	3851	11500	0557	86	07	12		99 99
328	264789-2	MAJOR'S PLACE	3901	11437	0650	88	05	12		88 08
329	264804-1	MAJUBA MOUNTAIN	4041	11832	0600	63	10			74 03
330	264824-2	MALA VISTA RANCH	4119	11515	0559	48	07	UU		68 05
331	264835-3	MANHATTAN POWER HOUSE	3832	11705	0696	48	07			50 06
332	264835-3	MANHATTAN POWER HOUSE	3832	11705	0692	50	06			53 05
333	264852-3	MARK TWAIN CAMP	3811	11845	0723	50	06			56 11
334	264858-1	MARLETTE LAKE	3910	11955	0801	48	07			53 11
335	264859-1	MARLETTE LAKE 2	3909	11953	0801	54	11			76 07
336	264888-3	MATHEWS RANCH	3730	11413	-999	49	03			49 07
337	264920-1	MC CLEARYS LITTLE HMR	4129	11701	0480	59	09			74 10
338	264925-N	MCCULLOUGH PASS	3544	11510	0376	65	07			66 10
339	264925-4	MCCULLOUGH PASS	3544	11510	0376	66	10			76 07
340	264935-1	MC DERMITT	4200	11743	0443	50	03	UU	U	70 10
341	264935-1	MC DERMITT 5 W	4200	11748	0450	70	10			71 02
342	264935-1	MC DERMITT	4157	11741	0450	71	02	UU	U	77 04
343	264935-1	MC DERMITT	4200	11743	0453	77	04	UU	U	85 04
344	264935-1	MC DERMITT	4158	11748	0454	85	04	12	7	86 01
345	264935-1	MC DERMITT	4200	11743	0453	86	01	12	7	99 99
346	264939-1	MC DERMITT INDIAN RESER	4158	11738	0511	48	07			50 03
347	264950-2	MC GILL	3924	11446	0635	48	07	UU		85 09
348	264950-2	MC GILL	3924	11446	0630	85	09	12		99 99
349	265078-2	MENDIVE RANCH	4141	11545	0625	55	10			60 02
350	265085-4	MESQUITE	3648	11405	0160	42	01	UU		47 12
351	265085-4	MESQUITE	3648	11404	0157	56	03	UU		58 09
352	265085-4	MESQUITE	3648	11405	0157	58	09	UU		62 03
353	265085-4	MESQUITE	3648	11404	0157	62	03	UU		66 05
354	265092-2	METROPOLIS	4117	11501	0580	65	07	UU	U	85 06
355	265092-2	METROPOLIS	4117	11501	0580	85	06	1U	U	99 99
356	265105-2	MIDAS 4 SE	4112	11644	0520	52	11	UU		72 03
357	265120-2	MIDAS SNOW COURSE	4116	11650	0721	63	11			76 09
358	265132-1	MIDDLEGATE LOWERY	3917	11801	0460	88	04	12		99 99
359	265168-3	MINA	3823	11806	0455	48	07	UU		86 04
360	265168-3	MINA	3823	11806	0455	86	04	12		99 99
361	265191-1	MINDEN	3857	11946	0472	48	07			81 06
362	265191-1	MINDEN AIRPORT	3900	11945	0471	81	06	UU	U	83 01
363	265191-1	MINDEN AIRPORT	3900	11945	0471	83	01	12	U	84 10
364	265191-1	MINDEN	3900	11945	0471	84	10	12	U	90 07
365	265191-1	MINDEN	3858	11946	0471	90	07	12	7	99 99
366	265239-3	MINTO	3735	11422	0473	49	12			51 02

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367	265352-2	MONTELLO	4116	11412	0488	48	07	UU	86	09
368	265352-2	MONTELLO 1 SE	4115	11412	0490	86	09	12	99	99
369	265362-3	MOUNT MONTGOMERY	3758	11819	0711	60	06		U	80 11
370	265362-3	MONTGOMERY MNTC STN	3758	11819	0710	80	11		U	84 08
371	265392-2	MOUNTAIN CITY RANGER ST	4147	11557	0562	55	02			80 10
372	265392-2	MOUNTAIN CITY R S	4150	11558	0564	80	10	UU		99 99
373	265400-3	MOUNT CHARLESTON LODGE	3616	11539	0751	49	01			76 10
374	265415-3	MOUNT GRANT	3834	11849	0901	52	04			74 03
375	265436-3	MOUNT MONTGOMERY	3758	11819	0711	59	06		U	60 05
376	265440-1	MOUNT ROSE BOWL	3921	11952	0741	73	10	UU		83 02
377	265440-1	MOUNT ROSE BOWL	3921	11952	0750	83	09	12		84 11
378	265440-1	MOUNT ROSE BOWL	3921	11952	0750	85	12	12		87 12
379	265441-1	MOUNT ROSE CHRISTMAS TR	3921	11952	0724	68	04		U	87 10
380	265441-1	MOUNT ROSE CHRISTMAS TR	3921	11952	0723	87	10		U	88 10
381	265441-1	MOUNT ROSE CHRISTMAS TR	3921	11952	0724	88	10		7	99 99
382	265445-1	MOUNT ROSE HIGHWAY STN	3920	11953	0737	59	06	UU		68 05
383	265447-1	MOUNT ROSE SKY TAVERN	3921	11952	0751	70	07	UU		73 10
384	265585-1	NINE MILE PASS	4142	11817	0540	60	12			74 10
385	265605-1	NIXON	3948	11920	0391	48	07	UU		53 06
386	265605-1	NIXON	3950	11921	0390	62	07	UU		74 08
387	265683-2	NORTH FORK 10 S	4120	11546	0613	71	07	UU		72 10
388	265687-2	NORTH FORK 13 N	4141	11547	0628	72	10	UU		74 03
389	265688-2	NORTH FORK 7 NW	4134	11554	0660	74	08	UU		82 09
390	265691-2	NORTH FORK MNTC STN	4129	11549	0620	48	07	U		71 07
391	265695-2	NORTH FORK SPRING CREEK	4131	11552	0637	51	10			52 08
392	265705-4	NORTH LAS VEGAS DOXARM	3612	11505	0182	51	02	UU		61 07
393	265705-4	NORTH LAS VEGAS	3613	11508	0188	90	01	12		99 99
394	265718-2	OASIS 5 S	4057	11431	0570	85	08	12		87 05
395	265722-2	OASIS	4102	11430	0583	87	05	12		99 99
396	265760-2	OLD RUTH	3916	11459	0703	78	08	UU		85 11
397	265818-1	OROVADA	4134	11747	0430	48	07	UU	U	67 08
398	265818-1	OROVADA	4134	11747	0431	67	08	UU	U	85 05
399	265818-1	OROVADA	4134	11747	0431	85	05	1U		89 05
400	265818-1	OROVADA 4 WSW	4133	11750	0429	89	05	12		99 99
401	265819-1	OROVADA 9 SSW	4127	11750	0415	71	01	UU		75 04
402	265840-2	OVERLAND PASS	4001	11535	0679	54	07			66 09
403	265842-2	OVERLAND PASS 2	4001	11535	0675	66	10			76 07
404	265846-4	OVERTON	3633	11427	0128	48	07	UU	U	52 07
405	265846-4	OVERTON	3631	11426	0124	52	07	UU	U	54 09
406	265846-4	OVERTON	3632	11426	0122	54	09	UU	U	61 12
407	265846-4	OVERTON	3631	11425	0122	61	12	UU	U	68 01
408	265846-4	OVERTON	3632	11427	0129	88	03	12	7	88 11
409	265869-2	OWYHEE	4157	11606	0539	48	07	UU	U	82 01
410	265869-2	OWYHEE	4157	11606	0540	82	01	UU	U	83 06
411	265869-2	OWYHEE	4157	11606	0540	83	06	12	U	85 04
412	265880-4	PAHRANAGAT W L REFUGE	3716	11507	0340	64	03	UU	U	86 07
413	265880-4	PAHRANAGAT W L REFUGE	3716	11507	0340	86	07	12	U	99 99
414	265890-4	PAHRUMP 2 N	3615	11559	0285	48	10			58 06
415	265890-4	PAHRUMP	3613	11600	0283	58	06	UU		69 01
416	265890-4	PAHRUMP	3613	11601	0270	69	01	UU		80 12
417	265890-4	PAHRUMP UNIV OF NEVADA	3612	11559	0267	80	12	UU		88 09
418	265890-4	PAHRUMP	3612	11559	0267	88	09	12		99 99
419	265897-4	PAHRUMP RANCH	3612	11559	0267	48	07			52 05
420	265907-1	PAHUTE MEADOWS RANCH	4118	11856	0438	63	07	UU		79 07
421	265915-2	PALISADES	4036	11612	0483	67	05			99 99
422	265931-3	PALMETTO	3728	11746	0591	48	07			54 03
423	265990-1	PARADISE HILL	4117	11742	0450	59	12	UU		70 10
424	266000-1	PARADISE VALLEY	4130	11732	0465	48	07			51 07
425	266005-1	PARADISE VALLEY RANCH S	4130	11732	0465	48	07	UU		54 07
426	266005-1	PARADISE VALLEY 6 ENE	4131	11725	0471	54	07			54 12
427	266005-1	PARADISE VALLEY RANCH S	4130	11732	0468	54	12	UU		87 02
428	266005-1	PARADISE VALLEY RANCH S	4130	11732	0468	87	02	12		99 99
429	266055-1	PARIS RANCH	4013	11741	0414	66	06	UU		89 07
430	266055-1	PARIS RANCH	4013	11741	0414	89	07	12		99 99

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431	266068-2	PARKER RANCH	4005	11437	0591	70	02	UU	U	71	10
432	266130-3	PENOYER VALLEY	3737	11547	0480	67	02	UU		72	03
433	266130-3	PENOYER VLY CASTLETON	3737	11547	0480	86	04	12		89	07
434	266130-3	PENOYER VLY CASTLETON	3737	11547	0480	90	01	12		99	99
435	266148-2	PEQUOP	4104	11432	0600	48	07	UU	U	59	04
436	266148-2	PEQUOP	4104	11432	0603	59	04	UU	U	85	07
437	266148-2	PEQUOP	4104	11432	0603	85	07		7	88	09
438	266160-2	PEQUOP SUMMIT	4105	11432	0731	64	10			66	09
439	266160-2	PEQUOP SUMMIT	4105	11432	0731	66	10			76	10
440	266235-3	PINE CANYON	3724	11414	0651	49	12			76	09
441	266242-2	PINE VALLEY BAILEY RANC	4025	11607	0505	82	05	12		99	99
442	266252-3	PIOCHE	3756	11427	0612	48	07	UU		66	05
443	266252-3	PIOCHE	3756	11427	0613	66	05	UU		71	08
444	266252-3	PIOCHE	3756	11427	0617	71	08	UU		91	02
445	266252-3	PIOCHE	3756	11427	0618	91	02	12		99	99
446	266290-1	PLEASANT VALLEY	3921	11946	0480	50	01			52	09
447	266305-1	POLE CREEK	4054	11734	0604	52	09			76	07
448	266349-2	PRIMEAUX	4040	11619	0600	48	07	UU		54	01
449	266349-2	PRIMEAUX	4040	11619	0576	54	01	UU		54	08
450	266504-1	QUINN RIVER CROSSING	4134	11826	0409	48	07			54	11
451	266574-2	RAND RANCH PALISADE	4026	11607	0505	56	10	UU		82	05
452	266630-3	RATTLESNAKE	3827	11610	0592	48	07			63	05
453	266642-2	RATTLESNAKE CANYON	4032	11531	0751	65	10			76	07
454	266691-3	RED ROCK CANYON ST PK	3605	11527	0378	77	05	UU		86	03
455	266691-3	RED ROCK CANYON ST PK	3605	11527	0378	86	03	12		99	99
456	266733-3	RED ROCK SUMMIT	3608	11532	0651	48	07			64	07
457	266742-2	REED RANCH	4126	11651	0547	60	06			74	10
458	266746-3	REESE RIVER RANGER STN	3859	11728	0665	72	03	UU		87	05
459	266746-3	REESE RIVER O'TOOLE	3904	11725	0655	87	10	12		99	99
460	266748-2	REESE VALLEY ATEN	4003	11714	0491	76	07	UU		81	04
461	266748-2	REESE VALLEY CARPER	4003	11714	0490	81	04	UU		84	07
462	266750-2	REESE VALLEY POWERS	4001	11716	0491	71	02	UU		72	04
463	266754-2	REESE VALLEY SMITH	4008	11716	0480	72	03	UU		76	07
464	266779-1	RENO WSFO AIRPORT	3930	11947	0440	48	01	UU	U	99	99
465	266784-1	RENO KIETZKE	3932	11947	0443	65	03			99	99
466	266787-1	RENO VA ST BRIDGE	3932	11949	0448	70	08			99	99
467	266905-3	ROBERTS RANCH	3610	11535	0611	48	07			76	07
468	266912-2	ROBIN RANCH	3958	11441	0624	68	08	UU	U	70	02
469	266918-2	ROBINSON SUMMIT	3925	11505	0763	53	10			66	09
470	266948-2	RODEO FLAT	4135	11557	0680	63	09			76	09
471	267123-2	RUBY LAKE	4012	11530	0601	48	07	UU	U	99	99
472	267149-1	RUCKS CABIN	4141	11733	0751	59	09			74	10
473	267175-2	RUTH	3917	11459	0683	58	06	UU		78	08
474	267175-2	RUTH	3917	11500	0686	85	12	12		88	09
475	267175-2	RUTH	3917	11459	0684	88	09	12		99	99
476	267192-1	RYE PATCH DAM	4028	11818	0416	48	07	UU	UU	52	04
477	267192-1	RYE PATCH DAM	4028	11818	0414	52	05	UU	UU	82	01
478	267192-1	RYE PATCH DAM	4028	11818	0413	82	01	UU	UU	85	04
479	267192-1	RYE PATCH DAM	4028	11818	0413	85	04	1U	UU	99	99
480	267224-2	SADLER RANCH	4012	11544	0569	54	07			76	07
481	267261-1	SAND PASS	4019	11948	0390	48	07	UU		72	07
482	267284-2	SAN JACINTO	4153	11441	0520	48	07			49	05
483	267319-3	SARCOBATUS	3716	11701	0402	48	07			61	07
484	267324-2	SAVAL RANCH	4117	11555	0637	60	07	UU		70	04
485	267330-2	SCHELLBOURNE	3948	11443	0616	48	07			58	08
486	267330-2	SCHELLBOURNE	3948	11444	0613	58	08			66	12
487	267335-2	SCHELLBOURNE PASS	3948	11439	0816	53	10			76	07
488	267358-3	SCHURZ	3857	11849	0412	48	07			57	05
489	267369-4	SEARCHLIGHT	3528	11455	0354	48	07	UU	U	84	12
490	267369-4	SEARCHLIGHT	3528	11455	0354	84	12	12	U	99	99
491	267397-2	SEVENTY ONE RANCH	4054	11519	0545	49	07		U	78	09
492	267430-1	SHEEP RANCH CANYON	4037	11733	0560	59	09			74	10
493	267443-1	SHELDON	4151	11938	0651	48	07	UU		72	02
494	267450-2	SHOSHONE 5 N	3855	11424	0593	88	10	12		99	99

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495	267463-3	SILVERPEAK	3740	11735	0426	67	09	UU	U	87	11	✓
496	267463-3	SILVERPEAK	3740	11735	0426	87	11	12	5	99	99	✓
497	267609-1	SMITH	3849	11920	0475	48	07	UU		66	11	
498	267612-1	SMITH 6 N	3857	11920	0500	73	07	UU	U	86	09	
499	267612-1	SMITH 6 N	3857	11920	0500	86	09	12	U	99	99	
500	267618-1	SMOKE CREEK ESPIL	4037	11945	0385	87	12	12		99	99	
501	267620-3	SMOKEY VALLEY	3847	11710	0562	49	06	UU	U	85	04	
502	267620-3	SMOKEY VALLEY	3847	11710	0562	85	04	1U	U	99	99	
503	267640-3	SNOWBALL RANCH	3904	11612	0716	66	09	UU	U	99	99	
504	267680-2	SOLDIER CREEK	4047	11518	0721	48	11			76	07	
505	267682-1	SOLDIERS MEADOW	4121	11910	0455	62	06	UU		68	04	
506	267686-1	SONOMA MOUNTAIN	4052	11736	0842	52	10			69	09	
507	267695-1	SPARKS TRUCKEE RIVER	3931	11944	0439	78	11			99	99	
508	267697-1	SPARKS	3933	11944	0436	88	11	12		99	99	
509	267702-1	SPAULDING CANYON	4033	11751	0591	59	09			74	10	
510	267710-1	SPOONERS STN	3906	11955	0703	51	10			81	04	
511	267750-3	SPRING VALLEY ST PK	3802	11411	0595	74	08	12		76	11	
512	267750-3	SPRING VALLEY ST PK	3802	11411	0595	76	11	12	7	99	99	
513	267806-1	STATELINE-HARRAH'S	3858	11957	0625	84	01	12		99	99	
514	267820-1	STEAD	3937	11953	0512	85	03	12		99	99	
515	267825-1	STEWART	3907	11943	0462	67	07			99	99	
516	267855-3	STONE CABIN VALLEY	3809	11635	0561	68	06	UU		71	10	✓
517	267873-1	SULPHUR	4054	11840	0404	48	07			53	01	
518	267908-3	SUNNYSIDE	3826	11501	0533	48	07	UU	U	62	07	✓
519	267908-3	SUNNYSIDE	3825	11501	0531	65	10	UU	U	85	08	
520	267908-3	SUNNYSIDE	3825	11501	0530	85	08	UU	U	86	07	✓
521	267908-3	SUNNYSIDE	3825	11501	0530	86	07	12	U	99	99	✓
522	267925-4	NORTH LAS VEGAS DOXARM	3612	11505	0182	61	08	UU		64	01	✓
523	267925-4	SUNRISE MANOR LAS VEGAS	3612	11505	0182	64	01	UU		83	07	✓
524	267925-4	SUNRISE MANOR LAS VEGAS	3612	11505	0182	84	12	12		89	11	✓
525	267953-1	SUTCLIFFE	3957	11937	0388	67	05			72	02	
526	267953-1	SUTCLIFFE	3957	11937	0400	72	02			74	03	
527	267953-1	SUTCLIFFE	3957	11937	0399	74	03			79	08	
528	267953-1	SUTCLIFFE WARRIOR POINT	4003	11938	0399	79	08	UU		85	07	
529	267953-1	SUTCLIFFE	3957	11937	0398	86	03	12		99	99	
530	267965-2	TAYLOR CANYON	4112	11606	0620	63	08			76	09	
531	267983-3	TEMPIUTE 4 NW	3741	11543	0489	70	03	UU		86	04	✓
532	268010-1	THACKER PASS	4143	11807	0500	60	12			74	10	
533	268034-3	THORNE	3836	11836	0420	48	07			50	05	
534	268160-3	TONOPAH	3804	11714	0609	48	07			50	12	✓
535	268160-3	TONOPAH	3804	11714	0602	51	01			54	06	✓
536	268165-3	TONOPAH 7 E	3804	11705	0543	75	05		U	76	05	
537	268170-3	TONOPAH AIRPORT	3804	11707	0542	51	04	UU		53	12	
538	268170-3	TONOPAH AIRPORT	3804	11705	0542	54	01	UU		82	01	
539	268170-3	TONOPAH AIRPORT	3804	11705	0543	82	01	UU		87	02	
540	268170-3	TONOPAH AP	3804	11705	0543	87	02	UU		99	99	
541	268186-1	TOPAZ LAKE	3842	11931	0502	57	07	UU	U	82	01	
542	268186-1	TOPAZ LAKE	3842	11931	0502	82	01	12	5	86	02	
543	268202-1	TOPAZ LAKE 4 N	3845	11931	0558	86	10	12		99	99	
544	268250-1	TRACY USGS	3934	11931	0424	77	11			99	99	
545	268346-2	TUSCARORA	4119	11614	0618	57	05	UU		77	04	
546	268346-2	TUSCARORA	4119	11614	0617	77	04	UU		85	06	
547	268346-2	TUSCARORA	4119	11614	0617	85	06	1U		88	06	
548	268346-2	TUSCARORA	4119	11614	0617	88	06	12		90	01	
549	268346-2	TUSCARORA	4119	11614	0617	90	05	12		99	99	
550	268349-2	TUSCARORA WILLIAMS RANC	4121	11604	0640	48	07			53	11	
551	268349-2	TUSCARORA ANDRAE RANCH	4124	11605	0586	54	05			57	04	
552	268424-3	TWIN RIVERS	3854	11715	0651	55	10			64	07	✓
553	268443-3	TWIN SPRINGS FALLINI	3812	11611	0530	85	08	12		99	99	✓
554	268500-1	UNIV OF NEVADA EXPERIME	3931	11947	0451	49	01			55	05	✓
555	268510-3	UPPER WILLIAMS RANCH	3611	11541	0580	64	07			76	07	✓
556	268538-3	URSINE	3759	11413	0576	64	04	UU		71	03	
557	268538-3	URSINE	3759	11413	0583	71	03	UU		72	12	
558	268543-3	URSINE SPRING VALLEY	3803	11410	0580	54	08			55	12	

022


Done

1575 m

559	268588-4	VALLEY OF FIRE ST PK	3626	11431	0200	72	11	UU	85	03	
560	268588-4	VALLEY OF FIRE ST PK	3626	11431	0200	85	03	UU	99	99	
561	268689-1	VERDI	3931	12000	0485	51	04		52	04	
562	268689-1	VERDI	3931	11959	0488	55	10		58	12	
563	268761-1	VIRGINIA CITY	3918	11939	0635	51	04	UU	52	04	
564	268761-1	VIRGINIA CITY	3918	11938	0600	52	04	UU	68	04	
565	268761-1	VIRGINIA CITY	3918	11938	0635	68	04	UU	84	02	
566	268761-1	VIRGINIA CITY	3918	11938	0635	84	02	UU	88	03	
567	268761-1	VIRGINIA CITY	3918	11938	0634	88	03	UU	99	99	
568	268776-1	VIRGIN VALLEY	4152	11901	0481	51	10	UU	59	08	
569	268794-1	VISTA	3931	11941	0437	60	09		99	99	
570	268810-1	VYA	4135	11955	0566	59	09	UU	80	09	
571	268822-1	WABUSKA 5 SE	3905	11907	0430	71	10	UU	U	84	03
572	268822-1	WABUSKA 5 SE	3905	11907	0430	84	03	UU	U	86	05
573	268822-1	WABUSKA 5 SE	3905	11907	0430	86	05	UU	SU	90	08
574	268822-1	WABUSKA 5 SE	3905	11907	0430	90	08	UU	U	99	99
575	268834-1	WADSWORTH	3938	11917	0408	48	07		49	05	
576	268838-1	WADSWORTH 4 N	3942	11917	0420	74	08	UU	U	86	11
577	268838-1	WADSWORTH 4 N	3942	11917	0420	86	11	UU	U	99	99
578	268842-1	WADSWORTH USGS	3938	11916	0404	75	01		86	10	
579	268977-1	WELLINGTON RANGER STN	3845	11922	0484	48	07	UU	U	73	05
580	268988-2	WELLS	4107	11458	0563	48	07	UU	U	62	11
581	268988-2	WELLS	4107	11458	0565	62	11	UU	U	86	02
582	268988-2	WELLS	4107	11458	0565	86	02	UU	U	99	99
583	269025-2	WEST FORK BEAVER CREEK	4128	11539	0620	65	10		76	07	
584	269044-3	WHEELER PASS	3623	11549	0751	63	08		76	07	
585	269055-2	WHITE HORSE PASS	4021	11414	0659	53	10		76	07	
586	269072-2	WILDHORSE RESERVOIR	4140	11547	0623	82	11	UU	85	11	
587	269072-2	WILDHORSE RESERVOIR	4140	11547	0623	85	11	UU	7	85	12
588	269072-2	WILDHORSE RESERVOIR	4140	11547	0623	85	12	UU	7	99	99
589	269122-2	WILKINS	4126	11445	0564	48	07	UU	80	05	
590	269126-2	WILKINS WINE CUP RANCH	4124	11440	0570	80	05	UU	80	09	
591	269133-2	WILLOW CREEK SUMMIT	4112	11622	0637	53	10		76	07	
592	269137-3	WILLOW SPRINGS	3826	11712	0613	48	07		49	05	
593	269154-3	WILSON CREEK SUMMIT	3821	11421	0711	53	10		76	07	
594	269159-4	WILSON TANK SUMMIT	3557	11527	0492	65	07		66	09	
595	269159-4	WILSON TANK SUMMIT	3557	11527	0492	66	10		76	07	
596	269166-2	WINNEMUCCA MEL ST BR	4058	11744	0426	75	05		86	03	
597	269166-2	WINNEMUCCA MEL ST BR	4058	11744	0425	86	03		99	99	
598	269171-1	WINNEMUCCA WB CITY	4058	11743	0429	48	01		49	09	
599	269171-1	WINNEMUCCA WSO AIRPORT	4054	11748	0430	49	09	UU	U	99	99
600	269229-1	YERINGTON	3859	11910	0438	48	07	UU	61	01	
601	269229-1	YERINGTON	3900	11910	0438	61	01	UU	67	05	
602	269229-1	YERINGTON	3859	11910	0438	67	06	UU	76	04	
603	269229-1	YERINGTON	3900	11910	0438	76	04	UU	99	99	
604	269234-1	YERINGTON SCS Y 1	3859	11910	0438	48	07		U	65	03
605	269234-1	YERINGTON SCS Y 1	3900	11910	0438	67	05		U	71	10
606	269387-3	YOMBA SCHOOL	3859	11728	0666	52	09		72	07	
607	-	-									
608	-	-									

023

Dau

 ...back to Home Page.
Western Regional Climate Center, Greg McCurdy, gmywrc@dr.edu

Jim Ashby
Dorothy Miller
11-13-98

\$ 45.00
800

ftp address
Daw 4/2/04
~~ftp://ftp.dri.edu/wrcc/wso~~

AMERIC ~ 1.0

Ordering precipitation data.

Sub direct
ftp://ftp.dri.edu/wrcc/wso

	Count	Coop No	Am. P fm Frmh			
✓ Adaveni	7	260046-3	12.75	48-07	80-06	-32 yrs
Adaveni/day	8	260046-3		80-12	82-04	

1.4 mb

Daw 4/2/04

024

~~Daw~~

? Betty-day	38	260714-4	6.27	48	57	} 24 yrs
"	39	"		57	58	
"	40	"		58	72	
✓ Betty 8N/day	41	260718-4		72	84	} ~26 yrs
"	42	"		84	98	

✓ Caliente-day	73	261358-3	8.83	48	84	36 yrs
"	74	"		84	Daw 4/2/04 98	15 yrs

✓ Goldfield-day	209	263285-3	5.70	48	50	2 yrs
"	210	"		50	84	34 yrs
"	211	"		85	Daw 4/2/04 98	13 yrs

Daw 4/2/04

✓ Las Vegas	284	264429-4	3.98	48	50	8
" WD Airport	285	264434-4		48	49	1
" WSO Airport	286	264436-4		49	75	26
" "	287	264436-4		76	98	22

Daw

✓ Tonopah Airport	537	268170-3		51	53	2
"	538	"	6.26	54	82	28
"	539	"		82	87	5
"	540	"		87	98	11

: BACKGROUND INFORMATION ON :
 : SUMMARY OF THE DAY LISTING FOR NOAA COOPERATIVE STATIONS.

:
 : 3: STATE NUMBER
 : STN: NCDC STATION NUMBER
 : YER: YEAR
 : MM: MONTH
 : DD: DAY OF MONTH
 : HH: HOUR OF OBSERVATION
 : PCPN: 24-HOUR PRECIPITATION [HUNDREDTHS OF INCHES]
 : SNFL: 24-HOUR SNOWFALL [TENTHS OF INCHES]
 : SNDP: SNOW DEPTH AT OBSERVATION [WHOLE INCHES]
 : TMAX: 24-HOUR MAXIMUM TEMPERATURE [WHOLE DEGREES F]
 : TMIN: 24-HOUR MINIMUM TEMPERATURE [WHOLE DEGREES F]

0 025

~~025~~
Daw

: IMMEDIATELY AFTER EACH OBSERVATION ARE TWO FLAGS;
 : THE FIRST IS A MEASUREMENT FLAG AND THE SECOND IS A QUALITY FLAG
 : THE FOLLOWING FLAGS ARE USED BY NCDC--->

: POSSIBLE VALUES OF MEASUREMENT FLAG:

: A: ACCUMULATED AMOUNT
 : B: ACCUMULATED AMOUNT INCLUDES ESTIMATED VALUES
 : E: ESTIMATED (SEE SECOND FLAG FOR METHOD OF ESTIMATION)
 : J: VALUE HAS BEEN MANUALLY VALIDATED
 : M: DATA IS MISSING ~ set to neg.
 : S: INCLUDED IN A SUBSEQUENT VALUE
 : T: TRACE (DATA = 00000 IN THIS CASE)
 : (: EXPERT SYSTEM EDITED VALUE, NOT VALIDATED
 : \): EXPERT SYSTEM APPROVED EDITED VALUE
 : >: OSC FLAG; ORIGINAL DATA DATA VALUE TOO HIGH TO STORE
 : <: OSC FLAG; ORIGINAL NCDC DATA VALUE TOO LOW TO STORE
 : : (BLANK) NO FLAG NEEDED

: POSSIBLE VALUES OF QUALITY FLAG:

: 0: VALID DATA ELEMENT (FOR ORIGINAL DATA ONLY)
 : 1: VALID DATA ELEMENT (FOR "UNKNOWN" SOURCE)
 : 2: INVALID DATA ELEMENT, REPLACED BY SUBSEQUENT VALUE
 : 3: INVALID DATA ELEMENT, NOT REPLACED
 : 4: VALIDITY UNKNOWN (NOT CHECKED)
 : 5: ORIGINAL NON-NUMERIC REPLACED BY DECIPHERED NUMERIC
 : A: SUBSTITUTED TOBS FOR TMAX OR TMIN
 : B: TIME SHIFTED VALUE
 : C: ESTIMATED BY 10:1 RATIO, PRECIP FROM SNOWFALL
 : D: TRANSPOSED DIGITS
 : F: ADJUSTED TMAX OR TMIN BY +- A MULTIPLE OF 10 DEGREES
 : G: CHANGED SIGN
 : H: MOVED DECIMAL POINT
 : I: OTHER RESCALING THAN F,G,H
 :
 : J: EDUCATED GUESS (SUBJECTIVELY DERIVED VALUE)
 : K: EXTRACTED FROM AN ACCUMULATED VALUE
 : L: SWITCHED TMAX AND TMIN
 : M: SWITCHED TOBS FOR TMAX OR TMIN
 : N: SUBSTITUTION OF "3 NEAREST STATION MEAN"
 :): SWITCHED SNOW AND PRECIPITATION AMOUNT
 : P: ADDED SNOWFALL TO SNOWDEPTH
 : Q: SWITCHED SNOWFALL AND SNOW ON GROUND
 : R: PRECIPITATION NOT REPORTED - ZERO ESTIMATED
 : S: MANUALLY EDITED VALUE
 : T: FAILED INTERNAL CONSISTENCY CHECK

2/2

: U: FAILED AREAL CONSISTENCY CHECK (BEGINNING OCT 1992)
:): EXPERT SYSTEM APPROVED EDITED VALUE

(026

: STATION NUMBER 260718 BEATTY 8 N
: OVERALL PERIOD CONSIDERED: 19000101-19981231
: WINDOW (START AND END) : 0101-1231
: Note: Corrected Data may follow, out of time order

DM

:YERMMDDHH	PCPN	SNFL	SNDP	TMAX	TMIN
=====	=====	=====	=====	=====	=====
1972120118	0 1	0 1	0 1	63 1	36 1
1972120218	0 1	0 1	0 1	63 1	26 1

SAMPLE

bj: **Precipitation programs**
 Date: 11/23/98 12:43:38 PM Mountain Standard Time
 From: ag1rocaj@uco.es (José_Roldán)
 To: woolhiserd@aol.com

File: Precipit.mim (149070 bytes)
 DL Time (31200 bps): < 1 minute

This message is a multi-part MIME message and will be saved with the default filename Precipit.mim

Dave: I am sending again this mail because I have found that it has not been delivered. Jose

Date: Fri, 20 Nov 1998 20:55:25 +0100

>To: Dave

>From: José Roldán <ag1rocaj@lucano.uco.es>

>Subject: Precipitation programs

>X-Attachments: C:\Fatima\MULTIPLE\Mcfo1.for; C:\Fatima\MULTIPLE\Mcso1.for;
 C:\Fatima\MULTIPLE\Mcso2.for; C:\Fatima\MULTIPLE\Tjt1.seg;
 C:\Fatima\MULTIPLE\Tjt2.seg; C:\Fatima\MULTIPLE\Tjtt1.1;
 C:\Fatima\MULTIPLE\Tjtt2.1; C:\Fatima\MULTIPLE\Tjtt3.1;
 C:\Fatima\MULTIPLE\Tjtt4.1; C:\Fatima\ALFACONS\Melsi.for;
 C:\Fatima\ALFACONS\Tjtt;

>

>Dear Dave:

>I am attaching Fortram programs we have to run Markov chain (first, MCFO1, second order, MCSO1 and MCSO2) and mixed exponential distribution, MELSI, in a PC. Also, I am including the card with input data (number of years; etc). There are two versions for the second order Markov chain because we need to change the number of periods (the most complete is MCSO2.for). The only problem is that many instructions are in spanish. Then you can ask Rosalia for the translation. If you can not run the programs or you have any other problem please tell me. Fatima is not here at the present because she has found a work in a plan devoted to modernization of traditional irrigations. However, I can contact with her in the weekend.

>I hope you have a nice pre-Thanksgiving and real Thanksgiving at Austin. Give my best regards to everybody, specially to Kay and you. Jose.

----- Headers -----

Return-Path: <ag1rocaj@lucano.uco.es>

Received: from rly-zd02.mx.aol.com (rly-zd02.mail.aol.com [172.31.33.226]) by air-zd01.mail.aol.com (v51.29) with SMTP; Mon, 23 Nov 1998 14:43:37 -0500

Received: from lucano.uco.es (lucano.uco.es [150.214.110.200])

by rly-zd02.mx.aol.com (8.8.8.8.5/AOL-4.0.0)

with SMTP id OAA20048 for <woolhiserd@aol.com>;

Mon, 23 Nov 1998 14:30:50 -0500 (EST)

X-quien: agrhid08 [150.214.116.218]

Received: from agrhid08.uco.es (agrhid08 [150.214.116.218]) by lucano.uco.es (8.6.12/8.6.12) with SMTP id UAA19014 for <woolhiserd@aol.com>; Mon, 23 Nov 1998 20:30:39 +0100

Message-Id: <3.0.1.32.19981123202804.007af200@lucano.uco.es>

X-Sender: ag1rocaj@lucano.uco.es

Mailer: Windows Eudora Light Version 3.0.1 (32)

Date: Mon, 23 Nov 1998 20:28:04 +0100

To: woolhiserd@aol.com

bj: **MIME encoding**
Date: 3/1/99 10:57:23 AM Mountain Standard Time
From: unkrich@tucson.ars.ag.gov (Carl Unkrich)
To: WOOLHISERD@aol.com (Dave Woolhiser)

028

File: mclog98.zip (566496 bytes)
DL Time (31200 bps): < 5 minutes

Daw

Dave,

I am attaching the files using a different type of encoding scheme -- there are only two choices in this e-mail utility (Netscape), so if this doesn't work, I would recomend downloading a demo copy of WinZip from www.winzip.com, which claims to be able to decode mime and uuencoded files.

Good luck,

Carl

—
Carl Unkrich
Southwest Watershed Research Center
USDA-ARS
2000 East Allen Rd
Tucson, AZ 85719
Phone: 520.670.6380 x178

*Got notice that
zip file is damaged*

----- Headers -----

Return-Path: <unkrich@tucson.ars.ag.gov>
Received: from rly-yd05.mx.aol.com (rly-yd05.mail.aol.com [172.18.150.5]) by air-yd01.mail.aol.com (v56.26) with SMTP; Mon, 01 Mar 1999 12:57:22 -0500
Received: from diablo.tucson.ars.ag.gov (diablo.tucson.ars.ag.gov [198.22.133.2])
by rly-yd05.mx.aol.com (8.8.8/8.8.5/AOL-4.0.0)
with ESMTP id MAA01579 for <WOOLHISERD@aol.com>;
Mon, 1 Mar 1999 12:57:11 -0500 (EST)
Received: from tucson.ars.ag.gov (granite-creek [198.22.133.21])
by diablo.tucson.ars.ag.gov (8.9.1a/8.9.1) with ESMTP id JAA06134
for <WOOLHISERD@aol.com>; Mon, 1 Mar 1999 09:35:15 -0700 (MST)
Message-ID: <36DAC202.84819F0F@tucson.ars.ag.gov>
Date: Mon, 01 Mar 1999 09:36:18 -0700
From: Carl Unkrich <unkrich@tucson.ars.ag.gov>
Organization: USDA-ARS
X-Mailer: Mozilla 4.02 [en] (Win95; U)
MIME-Version: 1.0
To: Dave Woolhiser <WOOLHISERD@aol.com>
Subject: MIME encoding
Content-Type: multipart/mixed; boundary="-----B468821B5F49F390A77CEDD4"

Subject: **Re: Daily Precipitation Data**
 Date: 11/29/98 10:02:01 PM Mountain Standard Time
 From: kwrcc@dri.edu
 To: WOOLHISERD@aol.com

Dave,

Read your message after I got back from a trip, sent it to the printer, and today I come across it cleaning the mess off my desk. The day is right, but the month is off by 11 instead of 10 (a mere 10 percent error).

If you have a web browser, you could take a look at the data records yourself (not the actual values, but the ****availability****).
www.wrcc.dri.edu/climsum.html, select nevada or california, select a station, then look at "metadata graphics". Every day with data in the digital historical record is indicated with a colored dot. A solid filled diagram of sufficient length indicates a good candidate. If you pick something, I can send you the record.
 Leaving soon for Portland and San Diego, back on Dec 3.

Kelly

>Dear Kelly,
 >I am working on a project to create a daily weather simulator for future
 >climate conditions at Yucca Mtn. To do that I will need to analyze long
 >records of daily precip. at different elevations near that site using the
 >logit transform for the transition probabilities for a first order Markov
 >chain. I cannot use the results of Clayton Hanson et al. because they didn't
 >use the transform (which is important for arid climates). I would like to
 >obtain data from WRCC and would appreciate your advice regarding data quality.
 >
 >Best regards Dave Woolhiser
 >woolhiserd@aol.com

----- Headers -----

Return-Path: <kwrcc@climate.dri.edu>
 Received: from rly-zd04.mx.aol.com (rly-zd04.mail.aol.com [172.31.33.228]) by air-zd02.mail.aol.com (v51.29) with SMTP;
 Mon, 30 Nov 1998 00:02:01 1900
 Received: from po.scs.unr.edu (po.scs.unr.edu [134.197.222.136])
 by rly-zd04.mx.aol.com (8.8.8/8.8.5/AOL-4.0.0)
 with ESMTP id AAA17758 for <WOOLHISERD@aol.com>;
 Mon, 30 Nov 1998 00:02:00 -0500 (EST)
 Received: from sage.dri.edu ([134.197.23.31])
 by po.scs.unr.edu (8.9.0/8.9.0) with ESMTP id VAA11489
 for <WOOLHISERD@aol.com>; Sun, 29 Nov 1998 21:03:19 -0800 (PST)
 Received: from climate.sage.dri.edu (climate [134.197.23.13])
 by sage.dri.edu (8.8.7/8.8.7) with ESMTP id VAA09168
 for <WOOLHISERD@aol.com>; Sun, 29 Nov 1998 21:01:59 -0800 (PST)
 Received: from localhost (localhost [127.0.0.1]) by climate.sage.dri.edu (8.7.1/8.7.1) with SMTP id VAA03495 for
 WOOLHISERD@aol.com>; Sun, 29 Nov 1998 21:01:59 -0800 (PST)
 Message-Id: <199811300501.VAA03495@climate.sage.dri.edu>
 X-Authentication-Warning: climate.dri.edu: Host localhost [127.0.0.1] didn't use HELO protocol

Subj: MCME program
Date: 2/23/99 1:43:59 PM Mountain Standard Time
From: ag1rocaj@uco.es (José_Roldán)
To: woolhiserd@aol.com

File: Ftn.exe (1374918 bytes)
DL Time (31200 bps): < 12 minutes

Dear Dave:

I am sorry because I have been out for several days.
I am sending you the FORTRAN 77 program . Then you can make more changes if you want. To execute that program you have to put (for first order Markov chain, for example):

```
MOVE MCFO1.FOR c:\...\FTN\BIN
CD c:\...\FTN\BIN
FL MCFO1.FOR
```

I am sending another e-mail with the executable versions of the programs. Praxedes is happy to hear you like "el dulce de membrillo". Also, we hope you have the opportunity to visit us in our new home.

Juan Vicente was last week in Arizona. He tried to call you but he couldn't. Write me if you have any problem. Best regards to Kay. Jose

Jose Roldan
Profesor de Hidraulica y Riegos
Editor Cientifico "Ingeniería del Agua"
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Headers

Return-Path: <ag1rocaj@uco.es>
Received: from rly-ya01.mx.aol.com (rly-ya01.mail.aol.com [172.18.144.193]) by air-ya05.mx.aol.com (v56.26) with SMTP; Tue, 23 Feb 1999 15:43:55 -0500
Received: from lucano.uco.es (lucano.uco.es [150.214.110.200]) by rly-ya01.mx.aol.com (8.8/8.8.5/AOL-4.0.0) with ESMTP id OAA13638 for <woolhiserd@aol.com>; Tue, 23 Feb 1999 14:28:16 -0500 (EST)
Received: from agrhid08.uco.es (agrhid08.uco.es [150.214.115.123]) by lucano.uco.es (8.9.2/8.9.1) with SMTP id UAA00272 for <woolhiserd@aol.com>; Tue, 23 Feb 1999 20:25:25 +0100 (MET)
X-quien: agrhid08.uco.es [150.214.115.123]
Message-Id: <3.0.1.32.19990223202235.007a6310@lucano.uco.es>
Sender: ag1rocaj@lucano.uco.es (Unverified)
X-Mailer: Windows Eudora Light Version 3.0.1 (32)

Preparation of Nat. Weather service data for input to Fortran programs for MCMF model with logit transform.

031

1. Copy to a new file with extension .TXT

2. With MSDOS editor at beginning + end of record, start at Mar 1 and end at Feb 28

3. Remove leap year days

Note time of day that depth is observed - may affect transition probabilities.

4. Write BASIC program to prepare output file

Daily precip (in)	TMAX	TMIN
	"F + 100	"F + 100
XX.XX	XXX.	XXX.

5. Modify Analysis programs for precipitation to accept this input.

6. Write a BASIC program to estimate: (obtained FORTRAN program from C. Richardson)

W(1) annual mean of t_{max} for dry days

W(2) amplitude of t_{max} for wet and dry days

W(3) annual mean of the CV of t_{max} for wet or dry days

W(4) amplitude of the CV " " " " "

W(5) annual mean of t_{max} for wet days

W(6) annual mean of t_{min} for wet or dry days

W(7) amplitude of t_{min} for wet or dry days

W(8) annual mean of CV of t_{min} for wet or dry days

W(9) amplitude of CV of t_{min} " " "

7. Lag and cross-correlation coefficients - we will use the values used in USCLIMATE p 5 & 6.

1. Identify parameters for Markov Chain - mixed exponential model for nearby stations.

032

A. Programs

1. MCF01.EXE Uses the logit transformation & fits Fourier series to logits of y_{00} and y_{10} .

Revised input MCF01R.FOR

DW

2. MELST.EXE Fits Fourier series to parameters of the mixed exponential model and the first order MC model.

5/20/99 DW

1. Create file TTJJTT with the following

DW 4/2/04

Line 1 11 I5 LMAXH = maximum number of ^{parameters} ~~harmonics~~ 2X Harmonics + 1

2. 12 THRES, NRE, NCOUNT, SCREEN, NLU, INIC

EG. 4, 2I5, F6.3, I4, I5 THRES = THRESHOLD in inches = 0.008

NRE = Number in matrix = 1301

NCOUNT = Number of years in analysis

SCREEN = CRITICAL STAT VALUE = 5.990 (chi square)

NLU = Number of years to skip

INIC = YEAR THAT ^{ANALYSIS} ~~ANALYSIS~~ BEGINS

DW 4/2/04

3. 9 A ONAME OUTPUT FILE NAME (alpha numeric)

4. 1515 I2 NUMEST Number of stations in data list

5. 9 PNAME Name of data file # 1

6. 9 " " # 2

etc

!

NUMEST

8. For radiation we will use values interpolated from Figs A10 - A17 in USCLIMATE.

033

Daw

BASIC Program will be called DAYREAD.BAS

This program will convert the daily NWS data to

and will calculate the mean, amplitude and phase angles listed in step 6.

Suppose we represent each (or any) of these series as

$$F(I) \quad I=1, 365$$

If $F(I)$ is represented by the Fourier Series

$$F(I) = \frac{a_0}{2} + \sum_{n=1}^m \left(a_n \cos \frac{n\pi I}{L} + b_n \sin \frac{n\pi I}{L} \right)$$

$$a_n = \frac{2}{m} \sum_{i=0}^{m-1} F(I) \cos \frac{n\pi I}{L} \quad n=0, 1, 2, \dots$$

$$b_n = \frac{2}{m} \sum F(I) \sin \frac{n\pi I}{L} \quad n=1, 2, 3, \dots$$

We read in $T_{MAX}^{(I,J)}$ and $T_{MIN}^{(I,J)}$ for each day for each year

Get $SUMT_{MAX}(J)$ and $SUMT_{MIN}(J)$ $J=1, 365$

Then Get $STD_{T_{MAX}} = \sqrt{\frac{\sum (T_{MAX} - T_{MAXBAR})^2}{NYR}}$

$$STD_{T_{MIN}} = \sqrt{\frac{\sum (T_{MIN} - T_{MINBAR})^2}{NYR}}$$

$$CVT_{MAX}(J) = STD_{T_{MAX}}(J) / T_{MAXBAR}(J)$$

$$CVT_{MIN}(J) = STD_{T_{MIN}}(J) / T_{MINBAR}(J)$$

5/19/99 Received word from Clarence Richardson that he will send the P.C. version of his FORTRAN program to calculate means, amplitudes etc for T_{max} & T_{min} \therefore will abandon the BASIC program for this analysis

must be
conditional
or
wet or
dry days

Continuing with step 4.

034

Test Program

a) Copy BEATTY^{1.009} to BEATTY¹.TXT

b) Edit as shown in 2. + 3.

data starts Mar. 1, 1949
data ends Feb 28, 1953
skip 5 lines

No. 5505
Engineer's Computation Pad
ADIN

Beatty 8N.DAT	1973072818	Line 161	365	
	73	526	365	
	74	891	365	
	1976	1252	366	(leap)
	1977	1622	365	
	78	1987	365	
	79	2352	365	
	80	2717	366	Leap
	81	3083	365	
	82	3448	365	
	83	3813	365	Leap
	84	4178	274	2 skips 8/1 to 10/31
	85	4452	365	
	86	4817	365	
	87	5182	365	
	88	5547	366	Leap
	89	5913	365	
	90	6278	365	
	91	6643	365	
	92	7008	366	Leap
	93	7374	365	
	94	7739	365	
	95	8104	365	
	96	8469	366	Leap
	97	8835	365	
		9200		
	98	2-28		
BEATTY8N.TXT	84	3965	273	
	85	4238		

Will remove 1984 data

starts in 1973 ends in 1997 24-1 = 24 yrs
8760 - 8 = 8760 8760 / 365 = 24

BEATTY8N.PTT has 8760 lines ✓

The File Beatty 8N.PTT should start with the station name
(one line)

5/21/99 Revised MCFOIR.FOR RVD BEATTY 8N. OUT

035

Prepare files for Caliente

DW

1. Copy Caliente.day to Caliente.TXT ✓

2. Edit Caliente.TXT

remove leap days ✓

start @ Mar 1 ✓

end @ Feb 28 - not critical

check to make sure no missing data

Note: Following yrs were omitted 1930, 38, 42, 43, 44, 46, 56, 66, 69, 75, 76, 78, 86
because they were incomplete

5/24/99 Ran Beatty 8N with MCFOIR with 3 harmonics
results look o.k.

Ran Caliente with MCFOIR with 3 harmonics ✓
results look o.k.

CALIENTE.OUT

Prepare files for Adaven

1. Copy Adaven.day to Adaven.TXT ✓

2. Edit Adaven.txt ✓

start at Mar 1 ✓

remove leap days ✓

5/25/99

Finished editing Adaven¹.TXT

.PTT - Total of 32 years.

Years omitted: '28, 29, 31, 35-38, 42, 43, 45-47, 49, 50, 53, 56, 57
71, 72

Ran Adaven ✓

ADAVEN.OUT

DW 4/21/04

Prepare files for Las Vegas

1. Copy VEGAS.DAY to VEGAS.TXT ✓

2. Edit VEGAS.TXT

start at Mar 1, 1949 ✓

remove leap days ✓

Years omitted: 38, 48, 52,

Note: Read at both 24:00 & 18:00

Ran Vegas ✓ ✓

VEGAS.OUT

Analyses of nearby rainfall data (con't.)

Prepare a spreadsheet PSIPLLOT to explore the relationships between: \bar{G}_{00} and annual precip

 \bar{G}_{10} C_{100} C_{200} C_{110} C_{210} $\bar{\alpha}$ $\bar{\beta}$ $\bar{\mu}$

037

~~DW~~

No. 5505
Engineer's Computation Pad



File is MCMEPAR.IDW in SWRI\CLIMATE

Create Plot of \bar{G}_{00} and \bar{G}_{10} vs annual precip

Add regression lines

$$\bar{G}_{00} = 3.07 - 0.00248 \bar{p} \quad r^2 = 0.719$$

$$\bar{G}_{10} = 0.932 - 0.00161 \bar{p} \quad r^2 = 0.463$$

where \bar{p} is in mm

This compares with the following equations from Hanson and Woolhiser (1990)

$$\theta_1 = 2.046 - 0.0011 X \quad r^2 = 0.664$$

$$\theta_2 = 0.648 - 0.0013 X \quad r^2 = 0.859$$

$$\text{where } \theta_1 = \ln(\bar{P}_{10}/1 - \bar{p}_{10})$$

$$\theta_2 = \ln(\bar{P}_{00}/1 - \bar{p}_{00})$$

and X is the mean annual precipitation

Hanson & Woolhiser used data from 22 NWS stations in Idaho. Record lengths were approximately 40 yrs. The logits were also estimated differently. Hanson & Woolhiser transformed the probabilities obtained by direct optimization, whereas in this study the logits were estimated directly.

Hanson, C.L. and D.A. Woolhiser, 1990. Precipitation Simulation Model for Mountainous Areas. in *Hydraulics and Hydrology of Arid Lands*. Proc. of Int'l Symposium, HY and IR Div. / ASCE. San Diego CA. 578-583

There are some problems with the data used in this study for example: some of the records are intermittent and the reading times at some stations changed during the period of record. Also there were different times of reading ie some at 24:00 some at 08:00 and some at 18:00.

038

When the amplitudes of the first and second harmonics of G_{00} and G_{10} are plotted against annual precip., there is no obvious trends.

No. 5505
Engineer's Computation Pad



When α , $\bar{\beta}$ and $\bar{\mu}$ are plotted against annual.P, there is some trend if Las Vegas is omitted. For $\bar{\mu}$, there is a weak increasing trend for $\bar{\beta}$. It might be worthwhile to use a regional α . It also may be a good idea to increase the number of harmonics for μ .

: STATION NUMBER 260718 BEATTY 8 N
 : OVERALL PERIOD CONSIDERED: 19000101-19981231
 : WINDOW (START AND END) : 0101-1231
 Note: Corrected Data may follow, out of time order

039

: YERMMDDHH	PCPN	SNFL	SNDP	TMAX	TMIN
1972120118	0 1	0 1	0 1	63 1	36 1
1972120218	0 1	0 1	0 1	63 1	26 1
1972120318	0 1	0 1	0 1	60 1	27 1
1972120418	OT1	OT1	OT1	56 1	26 1
1972120518	0 1	0 1	0 1	54 1	22 1
1972120618	0 1	0 1	0 1	39 1	15 1
1972120718	OT1	OT1	OT1	44 1	22 1
1972120818	0 1	0 1	0 1	47 1	26 1
1972120918	0 1	0 1	0 1	41 1	12 1
1972121018	0 1	0 1	0 1	27 1	14 1
1972121118	0 1	0 1	0 1	27 1	13 1
1972121218	0 1	0 1	0 1	30 1	10 1
1972121318	0 1	0 1	0 1	30 1	15 1
1972121418	0 1	0 1	0 1	41 1	18 1
1972121518	0 1	0 1	0 1	46 1	22 1
1972121618	0 1	0 1	0 1	41 1	22 1
1972121718	0 1	0 1	0 1	43 1	28 1
1972121818	0 1	0 1	0 1	47 1	30 1
1972121918	0 1	0 1	0 1	60 1	27 1
1972122018	0 1	0 1	0 1	62 1	34 1
1972122118	0 1	0 1	0 1	62 1	29 1
1972122218	0 1	0 1	0 1	62 1	25 1
1972122318	0 1	0 1	0 1	60 1	33 1
1972122418	0 1	0 1	0 1	61 1	26 1
1972122518	0 1	0 1	0 1	57 1	32 1
1972122618	0 1	0 1	0 1	56 1	31 1
1972122718	0 1	0 1	0 1	61 1	25 1
1972122818	OT1	OT1	0 1	56 1	27 1
1972122918	0 1	0 1	0 1	41 1	26 1
1972123018	0 1	0 1	0 1	41 1	22 1
1972123118	0 1	0 1	0 1	48 1	19 1
1973010118	0 1	0 1	0 1	46 1	28 1
1973010218	0 1	0 1	0 1	44 1	24 1
1973010318	0 1	0 1	0 1	48 1	17 1
1973010418	1 1	3 1	OT1	46 1	20 1
1973010518	0 1	0 1	0 1	38 1	13 1
1973010618	0 1	0 1	0 1	41 1	14 1
1973010718	0 1	0 1	0 1	45 1	15 1
1973010818	0 1	0 1	0 1	43 1	15 1
1973010918	5 1	5 1	1 1	41 1	22 1
1973011018	OT1	0 1	OT1	35 1	30 1
1973011118	0 1	0 1	0 1	50 1	22 1
1973011218	0 1	0 1	0 1	53 1	22 1

measurement flag

quality flag

DAW

1-10

13-15
 16-17
 depth in hundredths of inches
 34-36
 TMAX
 41-43

ADAVEN

5/24/99

DWJ

WORK SHEET

EDITING ADAVEN.TXT
To find missing data

040

~~DWJ~~

Line					
1928	9	1456	40-4374	365	
32	1465	1458	41-4739	365	
36	2923	1451	42-5104	334	X on 4/1/04
40	4374	1527	43-5438	605	X
44	5801	1456	44-6043	5801	363 X 3/01 missing added
48	7257	1457	45-6166	364	X 66-13791 365
52	8714		46-6530	364	X on 67-14150 365
56	10173		47-6894	364	X on 68-14521 365
60	11600	1460	48-7258	365	69-14886 365
64	13060	1460	49-7623	363	X 70-15251 365
68	14520		50-7986	364	X 71-15616 X
			51-8350	365	72 Missing 1/1/72-3/10/72 X
76	17324		52-8715	365	73-16230 365
Annual			53-9080	364	X 74-16595 365
28-9	363	X	54-9444	365	75-16960 365
29-372	364	X	55-9809	365	76-17325 365
30-736	365		56-10174	363	X 77-17690 365
31-1101	364	X	57-10537	334	X 78-18055 365 ✓
32-1465	365		58-10871	365	79-18420
33-1830	365		59-11236	365	80
34-2195	365		60-11601	365	Terminated @ 03/01/79
35-2560	363	X	61-11966	365	32 full years
36-2923	361	X	62-12331	365	Begin 1930 - 365 - check!
37-3284	362	X	63-12696	365	11680 - 32 yrs - check!
38-3646	363	X	64-13061	365	
39-4009	365		65-13426	365	
40-4374			66-13791		

PROGRAM MCFO VER. 2.0 (FORTRAN 77)

5/28/99

1/2

$\bar{p} = 12.75$

$\ln \bar{p} = 2.546$

SCREEN = 5.990 WHICH IS THE 0.05 SIGNIFICANCE LEVEL
;: STATION NUMBER 260046 ADAVEN
RAINGAGE= 1 : STATION NUMBER 260046 ADAVEN
YEARS = 32 (SINCE 1930 TO 1961)

\bar{p} from this sample
= 12.79"

0.11

OCCURRENCE PROCESS

32 NDD NDW NWD NWW ND NW; # OF PERIODS= 26

309	50	49	38	359	87
350	37	38	23	387	61
326	47	48	27	373	75
346	44	40	18	390	58
344	33	38	33	377	71
379	29	28	12	408	40
373	29	29	17	402	46
373	30	32	13	403	45
412	16	14	6	428	20
372	30	30	16	402	46
315	52	50	31	367	81
332	41	45	30	373	75
373	28	28	19	401	47
387	24	22	15	411	37
388	26	26	8	414	34
400	20	21	7	420	28
408	18	18	4	426	22
396	19	18	15	415	33
366	32	31	19	398	50
363	32	34	19	395	53
370	33	29	16	403	45
339	39	41	27	378	68
317	41	40	36	358	76
318	41	44	30	359	74
305	46	43	33	351	76
324	52	54	30	376	84

NUMBER OF PARAMETERS CONSIDERED= 7

~~DAW~~

DRY-DRY SITUATION:

Number of Periods= 26

Initial Parameter Estimates:

2.3924	-.89921E-01	-.37374	0.12667	-.14657
-.12660	0.31321E-01			

Likelihood Function = -2977.34473

Optimum Parameter Estimates:

2.3793	-.18616E-01	-.35400	0.27332	-.27123
-.25734	0.18347			

Adaven

Corresponding Amplitudes:

2.3793 0.35449 0.38505 0.31605

Corresponding Phase Angles:

0.0000 -1.6233 -.78157 2.5222

Likelihood Function = -2969.66187

042

~~-----~~ DAW

WET-DRY SITUATION:

Number of Periods= 26

Initial Parameter Estimates:

0.57969 0.46737E-02 -.16673 0.14140 -.11991E-01
-.80632E-01 0.48191E-01
Likelihood Function = -947.470703

Optimum Parameter Estimates:

0.54422 0.42520E-01 -.14912 0.15500 -.93820E-01
-.13115 0.14542

Corresponding Amplitudes:

0.54422 0.15506 0.18118 0.19582

Corresponding Phase Angles:

0.0000 -1.2930 -.54431 2.3046

Likelihood Function = -946.338013

FINAL LOG LIKELIHOOD FUNCTION: -3916.00000

26; -3916.000000

DAW 4/2/04
~~5x~~ 3x, 5(2x, 611.5)

5/28/99 11/2

PROGRAM MCFO VER. 2.0 (FORTRAN 77)

$\bar{p} = 6.27$
 $\ln \bar{p} = 1.836$

043

SCREEN = 5.990 WHICH IS THE 0.05 SIGNIFICANCE LEVEL
: STATION NUMBER 260718 BEATTY8N
RAINGAGE= 1 : STATION NUMBER 260718 BEATTY8N
YEARS = 24 (SINCE 1973 TO 1996)

OCCURRENCE PROCESS

\bar{p} from this sample
= 6.16"

24 NDD NDW NWD NWW ND NW; # OF PERIODS= 26

228	37	36	34	265	70
241	33	37	22	274	59
298	16	16	6	314	22
295	15	17	9	310	26
277	24	22	13	301	35
279	23	23	11	302	34
290	16	17	13	306	30
312	11	11	2	323	13
326	3	5	2	329	7
312	10	8	6	322	14
282	22	23	9	304	32
289	21	19	7	310	26
299	13	16	8	312	24
299	16	14	7	315	21
300	16	15	5	316	20
294	15	17	10	309	27
317	10	9	0	327	9
293	16	18	9	309	27
298	16	15	7	314	22
296	19	18	3	315	21
294	15	16	8	309	24
283	22	21	10	305	31
250	30	28	28	280	56
272	24	26	14	296	40
253	31	28	22	284	50
282	28	29	15	310	44

NUMBER OF PARAMETERS CONSIDERED= 7

DRY-DRY SITUATION:

Number of Periods= 26

Initial Parameter Estimates:

2.7957 0.10169 -.44087 -.88447E-01 -.27936
0.41542E-01 0.14732
Likelihood Function = -1846.42664

Optimum Parameter Estimates:

2.7447 0.14576 -.45273 0.10679 -.29028
-.61791E-01 0.10873

Corresponding Amplitudes:

044

2.7447 0.47562 0.30930 0.12506

Corresponding Phase Angles:

0.0000 -1.2593 -1.2183 2.0876

DAW

Likelihood Function = -1840.30237

WET-DRY SITUATION:

Number of Periods= 26

Initial Parameter Estimates:

0.87648 -.29210 -.43405 0.29549 -.10890
0.37111E-01 0.23426
Likelihood Function = -514.350464

Optimum Parameter Estimates:

0.67661 -.18847E-01 -.25681 0.12436 -.14940
0.11662 -.11219E-01

Corresponding Amplitudes:

0.67661 0.25750 0.19439 0.11715

Corresponding Phase Angles:

0.0000 -1.6441 -.87659 -.95906E-01

Likelihood Function = -506.033905

FINAL LOG LIKELIHOOD FUNCTION: -2346.33618
26; -2346.336180

Editing Work sheet Line CALIENTE

54 yrs
use 40

1932	0229	888	1460	1429	9	
1936	2348	1292		(30)	252	- March is missing
1940	3640	1458		31	523	365
1944	5098	1457		32	888	
1948	6555	1460		33	1253	365
1952	8015	1460		34	1618	365
1956	9475	1448?		35	1983	365
1960	10,923	1460		36	2348	365
1964	12,383	1432?		37	2713	365
1968	13,865	1399?		(38)	3078	298
1972	15,214	1430?		39	3276	364
1976	16,644	1398?		40	3640	365
1980	18,042	1460		41	4005	365
1984	19,502	1430?		(42)	4370	364
1988	20,932	1460		43	4734	364
1992	22,392	1460		(44)	5098	363
1996	23,852			45	5461	365
Thru 1998		215		(46)	5826	364

~~DAW~~

67 days missing
1 day missing
added Aug 31 = 30

1 day
1 day
2 days

Detecting missing data

48	6555	365
49	6920	365
50	7285	365
51	7650	365
52	8015	365
53	8380	365
54	8745	365
55	9110	365
(56)	9475	353
57	9828	

CALIENTE, CONT

57 9828 365
 58 10193 365
 59 10558 365
 60 10923 365
 61 11288 365
 62 11653 365
 63 12018 365
 64 12383 365
 65 12748 365
 (66) 13113 337]
 67 13450 365
 68 13815 365
 (69) 14180 304]
 70 14484 365
 71 14849 365
 72 15214 365
 73 15579 365
 74 15944 365
 (75) 16309 335 -30
 (76) 16644 334 -31
 77 16978 365
 (78) 17343 334 -31
 79 17677 365
 80 18042 365
 81 18407 365
 82 18772 365
 83 19137 365
 84 19502

84 19502 365
 85 19867 16068
 (86) 16433 365
 335]
 87 16768 365
 88 17133 365
 89 17498 365
 90 17863 365
 91 18228 365
 92 18593 365
 93 18958 365
 94 19323 365
 95 19688 365
 96 20053 365
 97 20418 365
 98 20783

changed to
 8:00 reading
 045A

~~DAW~~

PROGRAM MCFO VER. 2.0 (FORTRAN 77)

5/28/99
 $\bar{p} = 8.83$
 $\ln \bar{p} = 2.178$

1/2

SCREEN = 5.990 WHICH IS THE 0.05 SIGNIFICANCE LEVEL
;: STATION NUMBER 261358 CALIENTE
RAINGAGE= 1 : STATION NUMBER 261358 CALIENTE
YEARS = 40 (SINCE 1929 TO 1968)

\bar{p} from this sample
= 8.80 " (046

OCCURRENCE PROCESS

40 NDD NDW NWD NWW ND NW; # OF PERIODS= 26

415	43	43	44	458	87
390	58	57	41	448	98
431	41	46	39	472	85
467	39	32	22	506	54
408	49	56	47	457	103
446	44	42	28	490	70
445	46	42	27	491	69
513	16	23	8	529	31
503	23	20	9	526	29
433	47	43	35	480	78
375	69	74	42	444	116
380	65	64	51	445	115
439	45	47	29	484	76
479	32	29	20	511	49
78	28	29	25	506	54
465	30	30	30	495	60
456	37	39	28	493	67
484	28	30	18	512	48
445	44	43	28	489	71
459	36	37	18	495	55
430	38	34	30	468	64
399	52	52	33	451	85
416	55	55	34	471	89
407	59	61	33	466	94
399	61	56	44	460	100
421	66	67	43	487	110

~~DAW~~

NUMBER OF PARAMETERS CONSIDERED= 7

DRY-DRY SITUATION:

Number of Periods= 26

Initial Parameter Estimates:

2.3414	0.42186E-02	-.22307	0.12341	-.16401
-.10224	0.52824E-01			

Likelihood Function = -3814.76025

Optimum Parameter Estimates:

-.22243146	0.10998304E-01	-.21185	0.29937	-.28570
------------	----------------	---------	---------	---------

Daw Calibrate

Corresponding Amplitudes:

2.3146 0.21264 0.41382 0.28610

Corresponding Phase Angles:

0.0000 -1.4846 -0.76204 2.4614

047

Likelihood Function = -3805.12402

WET-DRY SITUATION:

Number of Periods= 26

Initial Parameter Estimates:

0.38758 0.35862E-01 -.26183E-01 -.15927 -.16506
-.10063E-01 0.38011E-01

Likelihood Function = -1324.93958

Optimum Parameter Estimates:

0.36420 0.77022E-02 -.18233E-01 -.10151 -.81055E-01
-.40240E-01 0.47511E-01

Corresponding Amplitudes:

0.36420 0.19793E-01 0.12990 0.62262E-01

Corresponding Phase Angles:

0.0000 -1.1711 -2.4678 2.2735

Likelihood Function = -1323.22754

FINAL LOG LIKELIHOOD FUNCTION: -5128.35156
26; -5128.351560

~~DAW~~

GOLDFIELD.TXT Reading of 18700 until '82 then 2:05 time 17500 n. 53

1949		63-3221	310 X	
52	1060	64-3531	246 X	89-11483 365
		65-3777	326 X	90 11848 365
60	2127,1404	66-4103	365	91 12213 365
64	3531,1302	67 4468	365	92 12578 335 ? X
68	4833,1460	68 4833	365	93 12913 365
72	6293,1004	69 5198	365	94 13278 365
76	7297,1460	70 5563	365	95 13643 366 ??
80	8757,1358	71 5928	365	96 14008 365
84	10115,1034	72 6293	335 X	97 14374 365
88	11149,1429	73 6628	304 X	98 14739
92	12578,1430	75 6932	365	?
96	14008	76 7297	365	98 14859
		77 7662	365	
99-9	365	78 8027	365	
50-374	248	79 8392	365	
51-722	338	80 8757	365	
52-1060	X	81 9122	335 X	
52/19/50-53/6/10	53 X	82 9487	365	
54	1539 X	83 9722	X	
	X	84	X	
59	1762 365	85	X	
60	2127 365	86 10412	365	
61	2492 364 ??	87 10784	365	
62	2856 365	88 11149	334 X	
63	3221	89 11483		

remove page check

27 10015

1104
1462

10563
- 8
10555

÷ 365 = 28.91

10229
- 9

10220
÷ 365 = 28 ✓

1949 -

check
add idny
missed 31

PROGRAM MCFO VER. 2.0 (FORTRAN 77)

Daw 5/28/99
 $\bar{p} = 5.70$
 $1/n \bar{p} =$

049

SCREEN = 5.990 WHICH IS THE 0.05 SIGNIFICANCE LEVEL
;: STATION NUMBER 263285 GOLD
RAINGAGE= 1 : STATION NUMBER 263285 GOLDFIELD
YEARS = 28 (SINCE 1949 TO 1976)

\bar{p} from this sample
= 6.49"

OCCURRENCE PROCESS

28	NDD	NDW	NWD	NWW	ND NW;	# OF PERIODS=	26
287	38	43	18	325	61		
308	30	30	13	338	43		
330	25	25	9	355	34		
325	29	29	9	354	38		
326	29	27	9	355	36		
314	26	32	16	340	48		
338	22	20	10	360	30		
342	17	17	16	359	33		
362	11	14	5	373	19		
344	18	18	12	362	30		
315	30	27	20	345	47		
340	21	24	7	361	31		
335	23	23	11	358	34		
344	19	18	11	363	29		
349	20	17	6	369	23		
368	9	12	3	377	15		
370	9	11	2	379	13		
343	17	15	10	360	25		
337	17	17	7	354	24		
330	18	17	8	348	25		
322	17	14	9	339	23		
314	22	24	4	336	28		
312	25	30	22	337	52		
318	29	27	15	347	42		
320	23	24	22	343	46		
327	36	32	14	363	46		

NUMBER OF PARAMETERS CONSIDERED= 7

DRY-DRY SITUATION:

Number of Periods= 26

Initial Parameter Estimates:

2.7574	-.18822	-.38450	0.41663E-01	-.15516
-.66721E-01	0.90660E-01			

likelihood Function = -2141.05981

Optimum Parameter Estimates:

-.17267364	0.18540885	-.33692	0.15112	-.23371
------------	------------	---------	---------	---------

~~DAW~~

Goldfield

72

Corresponding Amplitudes:

2.7364	0.35407	0.27831	0.25333
--------	---------	---------	---------

050

Corresponding Phase Angles:

0.0000	-1.8833	-.99680	2.3204
--------	---------	---------	--------

Likelihood Function = -2137.35986

WET-DRY SITUATION:

Number of Periods= 26

Initial Parameter Estimates:

0.80254	-.82429E-01	-.52035E-01	0.25086	0.77472E-01
0.63243E-02	-.72870E-01			

Likelihood Function = -551.646545

Optimum Parameter Estimates:

0.73231	-.43930E-01	0.15542E-01	0.27687	-.34918E-01
0.18864	-.19431			

Corresponding Amplitudes:

0.73231	0.46598E-01	0.27906	0.27081
---------	-------------	---------	---------

Corresponding Phase Angles:

0.0000	2.8016	-.12546	-.80019
--------	--------	---------	---------

Likelihood Function = -549.849548

FINAL LOG LIKELIHOOD FUNCTION: -2687.20947
 26; -2687.209470

WORKSHEET

VEGAS.TXT

serviced at 24:00

Daw

5		37	9 365	74	12774 365
52	1104 1459	38	3743 56 X	75	13139 365
56	2563 1460	39	730 365	76	13504 365
60	4023 1460	40	1095 365	77	13869 365
64	5483 1460	41	1460 365	78	14234 365
68	6943 1460	42	1825 365	79	14599 365
72	8403 1460	43	2190 365	80	14964 365
76	9863 1460	44	2555 365	81	15329 365
80	11323 730	? 45	2920 365	82	15694 369 ?? OK
82	12053 24:00	46	3285 365	83	16063 369 ?? OK
83	12422	47	3650	84	16432 365
84	12791 1,461 ?	48	missing	85	16797 365
88	14252 1,460	49	3650 365	86	17162 365
92	15712 1,460	50	4015 365	87	17527 366 16799 366 OK
96	17172	51	4380	88	17893 365 17105
98	17902	0731	then goes to 96/	89	18258 365
1940	19169 1460	52	4745 365	90	18623 365
47	20629	53	5109 365	91	18988 365
		54	5474 365	92	19353 365
47-12/31		55	5839 365	93	19718 365
have	1946, 45, 44, 43, 42, 41	56	6204 365	94	20083 365
	40, 39, 38, 37	57	6569 365	95	20448 365
		58	6934 365	96	20813 365
		59	7299 365	97	21178 365
		60	7664 365	98	21543 X
		61	8029		

$$\frac{20813}{8} = 2601.625 \approx 2605 \div 365 = 57 \text{ yrs}$$

PROGRAM MCFO VER. 2.0 (FORTRAN 77)

DAW

$\bar{p} = 3.98$

$\ln \bar{p} = 1.381$

052

SCREEN = 5.990 WHICH IS THE 0.05 SIGNIFICANCE LEVEL
; 264436 LAS VEGAS WSO AIRPOR
RAINGAGE= 1 264436 LAS VEGAS WSO AIRPORT
YEARS = 57 (SINCE 1937 TO 1993)

\bar{p} from this sample
= 4.15

OCCURRENCE PROCESS

57 NDD NDW NWD NWW ND NW; # OF PERIODS= 26

642	61	61	33	703	94	<i>Period 1</i>
666	53	55	24	719	79	<i>" 2</i>
704	35	38	21	739	59	
727	30	31	10	757	41	
734	27	29	8	761	37	
738	30	26	4	768	30	
731	27	29	11	758	40	
771	11	14	2	782	16	
775	10	8	5	785	13	
715	38	33	12	753	45	
644	64	67	23	708	90	
645	64	63	26	709	89	
698	42	43	15	740	58	
703	38	40	17	741	57	
734	28	27	9	762	36	
714	36	34	14	750	48	
739	26	26	7	765	33	
705	36	39	18	741	57	
693	47	42	16	740	58	
711	37	39	11	748	50	
680	46	44	28	726	72	
697	37	42	22	734	64	
644	61	56	37	705	93	
676	46	50	26	722	76	
652	58	54	34	710	88	
699	65	63	28	764	91	<i>Period 26</i>

NUMBER OF PARAMETERS CONSIDERED= 7

DRY-DRY SITUATION:

Number of Periods= 26

Initial Parameter Estimates:

 2.9404 0.25822 -.15658 0.28670E-01 -.33125
 -.18767 -.59885E-02
 Likelihood Function = -4040.54907

Optimum Parameter Estimates:

 -.29229063 0.10628748 -.18562 0.31080 -.44689

DWS

Corresponding Amplitudes:

2.9063	0.32558	0.54435	0.32009
--------	---------	---------	---------

053

Corresponding Phase Angles:

0.0000	-.60665	-.96311	2.7698
--------	---------	---------	--------

Likelihood Function = -4021.83691

WET-DRY SITUATION:

Number of Periods= 26

Initial Parameter Estimates:

0.93578	0.19246	-.13055	0.11082	-.13521
-.82729E-01	-.47410E-01			

Likelihood Function = -925.227295

Optimum Parameter Estimates:

0.91045	0.23493	-.20403	0.15996	-.17063
-.72529E-01	0.62259E-01			

Corresponding Amplitudes:

0.91045	0.31115	0.23388	0.95586E-01
---------	---------	---------	-------------

Corresponding Phase Angles:

0.0000	-.71512	-.81766	2.4322
--------	---------	---------	--------

Likelihood Function = -923.080200

FINAL LOG LIKELIHOOD FUNCTION: -4944.91699
 26; -4944.916990

TANORAH.TXT

5/17/98

~~DATA~~

- 58 9 365 ✓
- 56 374,460 ✓
- 60 1834,460 ✓
- 64 3294,460 ✓
- 68 4754,460 ✓
- 72 6214,460 ✓
- 76 7674,460 ✓
- 80 9134,460 ✓
- 84 10594,460 ✓
- 88 12054,429
- 92 13483,460 ✓
- 96 14943

- 84 10594 365 ✓
- 85 19959 365 ✓
- 86 11324 365 ✓
- 87 11689 365 ✓
- 88 12054 365 ✓
- 89 12419 334 - 31 ✓
- 90 12753 365 ✓
- 91 13118 365 ✓
- 92 13483

$$\begin{array}{r}
 15,338 \\
 - 8 \\
 \hline
 15,330 = 42 \text{ yrs from } 1955
 \end{array}$$

PROGRAM MCFO VER. 2.0 (FORTRAN 77)

5/28/99

1/2

DWS
 $\bar{p} = 6.26''$

055

$\ln \bar{p} = 1.834$

SCREEN = 5.990 WHICH IS THE 0.05 SIGNIFICANCE LEVEL
;: STATION NUMBER 268170 TONO PAK
RAINGAGE= 1 : STATION NUMBER 268170 TONO
YEARS = 42 (SINCE 1955 TO 1996)

\bar{p} from this sample
= 5.32''

OCCURRENCE PROCESS

42 NDD NDW NWD NWW ND NW; # OF PERIODS= 26

426	59	64	38	485	102
471	48	45	24	519	69
496	35	38	19	531	57
487	43	43	15	530	58
490	41	37	20	531	57
484	36	39	29	520	68
483	43	42	20	526	62
498	33	36	21	531	57
551	14	16	7	565	23
516	29	26	17	545	43
451	50	52	35	501	87
465	54	51	18	519	69
497	34	37	20	531	57
500	33	30	25	533	55
511	30	31	16	541	47
515	27	28	18	542	46
532	24	23	9	556	32
519	26	27	16	545	43
495	36	35	22	531	57
497	39	39	13	536	52
513	31	30	12	544	42
490	37	39	22	527	61
462	44	42	40	506	82
471	49	48	20	520	68
474	39	38	37	513	75
504	49	47	30	553	77

NUMBER OF PARAMETERS CONSIDERED= 7

DRY-DRY SITUATION:

Number of Periods= 26

Initial Parameter Estimates:

2.6050 -.58667E-01 -.23233 0.21174E-01 -.14402
-.47759E-01 0.72349E-01
Likelihood Function = -3525.77734

Optimum Parameter Estimates:

2.5834 -.30709E-01 -.20856 0.14625 -.20366
-.15945 0.14712

DAN

Tonopah

(056

Corresponding Amplitudes:

2.5834 0.21081 0.25073 0.21695

Corresponding Phase Angles:

0.0000 -1.7170 -0.94803 2.3964

Likelihood Function = -3521.00806

4 harmonics -3515.34

$AIC = -2(-3521.008 + 7) = 7028.04$
 $AIC = -2(-3515.36 + 9) = 7012.72$
7056.0
7048.72 *

WET-DRY SITUATION:

* MIN

Number of Periods= 26

Initial Parameter Estimates:

0.59967 0.13792E-02 -0.30306E-01 0.45200E-01

0.12438 0.30978E-01
Likelihood Function = -1011.80634

4 harmonics -1010.39

$AIC = -2(-1011.8 + 7) = 2009.6$
 $AIC = -2(-1010.39 + 9) = 2002.78$
-0.73495E-01
2037.6 * min
2,038.78
DAN 4/2/04

Optimum Parameter Estimates:

0.56979 0.15363E-01 -0.26668E-01 0.11143 -0.10498
0.19586 -0.10169

Corresponding Amplitudes:

0.56979 0.30777E-01 0.15309 0.22068

Corresponding Phase Angles:

0.0000 -1.0481 -0.75559 -0.47891

Likelihood Function = -1010.42798

FINAL LOG LIKELIHOOD FUNCTION: -4531.43604

26; -4531.43604

-4525.75

Note: Min AIC for p00 is for 4 harmonics
" " " p10 is for 3 "

2nd printout / same data 5/27/99

1/2

: STATION NUMBER 260046 ADAVEN

$\bar{p} = 12.79'' = 324.9 \text{ mm}$ *DM*

057

VALOR MEDIO DE ALFA ANTES DE OPTIMIZAR = .317868

~~DAW~~ DAW

FINAL LOG-LIKELIHOOD VALUE=-F= 441.88730

PARAMETER	MEAN	AMP	PAN	AMP	PAN
ALFA	.24080				
BETA	.85445E-01	.63701E-01	-2.0522	.19907E-01	-2.4440
MEAN	.25822	.49695E-01	-2.7854	.20414E-01	.26296

: STATION NUMBER 260718

BEATTY8N

$\bar{p} = 6.16'' = 156.5 \text{ mm}$

ME
BEATTY-8N, 0.1
DAW 4/27/04

VALOR MEDIO DE ALFA ANTES DE OPTIMIZAR = .350336

FINAL LOG-LIKELIHOOD VALUE=-F= 630.17640

PARAMETER	MEAN	AMP	PAN	AMP	PAN
ALFA	.34495				
BETA	.30627E-01	.19786E-01	-.88589	.15530E-02	2.8120
MEAN	.19229	.32308E-01	3.2380	.39253E-01	1.4996

: STATION NUMBER 263285

GOLDFIELD

$\bar{p} = 6.49'' = 164.8 \text{ mm}$

VALOR MEDIO DE ALFA ANTES DE OPTIMIZAR = .355947

FINAL LOG-LIKELIHOOD VALUE=-F= 600.59920

PARAMETER	MEAN	AMP	PAN	AMP	PAN
ALFA	.34419				
BETA	.50262E-01	.11991E-01	1.8903	.36913E-01	-.11324E-01
MEAN	.20673	.14774E-01	-2.0505	.29507E-01	.39428

: STATION NUMBER 268170

TONOPAH

$\bar{p} = 5.32'' = 135.1 \text{ mm}$

VALOR MEDIO DE ALFA ANTES DE OPTIMIZAR = .322061

FINAL LOG-LIKELIHOOD VALUE=-F= 1708.79700

PARAMETER	MEAN	AMP	PAN	AMP	PAN
ALFA	.29003				
BETA	.17398E-01	.30058E-02	-4.1570	.67835E-02	-1.7148
MEAN	.16362	.32569E-01	-1.4532	.18968E-01	.51151

264436

LAS VEGAS WSO AIRPORT

$\bar{p} = 4.15'' = 105.4 \text{ mm}$

~~DAW~~

5777184

1/2

VALOR MEDIO DE ALFA ANTES DE OPTIMIZAR = .328296

058

FINAL LOG-LIKELIHOOD VALUE=-F= 1119.28100

PARAMETER	MEAN	AMP	PAN	AMP	PAN
ALFA	.29226				
BETA	.10731E-01	.31424E-02	.77606	.68334E-02	.61722
MEAN	.27777	.20483E-01	-1.8802	.16194E-01	2.5463

: STATION NUMBER 261358 CALIENTE $\bar{p} = 8.80'' = 223.5 \text{ mm}$

VALOR MEDIO DE ALFA ANTES DE OPTIMIZAR = .213799

FINAL LOG-LIKELIHOOD VALUE=-F= 1648.98400

PARAMETER	MEAN	AMP	PAN	AMP	PAN
ALFA	.20398				
BETA	.15845E-01	.11005E-01	-.46130	.52284E-02	-.95156
MEAN	.18461	.39613E-01	-2.3523	.17429E-01	.22275

77105T 5/20/73

~~Dist~~

(059

5
0.0080 1301 24 5.990 0 1973
BEATTY8N.OUT
BEATTY8N.PTT

UNIT 19

~~DAW~~

FOR MELSI REV

See ATTACHED ME

SAL - OFIL - unit 17
 DAT - PNAME - out file
 BOR.1 - ONAME - unit 17
 BOR.2 - FNAME - unit 18
 Name

precip file
 output file

1 -NSTA CORDOBA 0.1000 5 401 44 5.990 0 2 2 2 2 1953
 0.0000001 0.00000002 9.99

0.2600
 PAREPS
 FNEPS
 ZMIS

CALFA, KPER, KALFA, NUMSAV

To put in a logistic mean &

SAMPLE INPUT FILE

060

MAX A
 MAX B
 MAX T
 INIC
 MAXH

Parameters averaged for
Las Vegas + St. George, VT 061

~~DAW~~

AVERAGE PARAMETERS FOR STATION

0.9284E+00	0.1765E-01	-.5562E+00	0.2285E-01	-.1179E+01
0.1340E-01	-.5669E+00	0.1415E-01	0.9458E-01	0.9728E-02
-.2110E+01	0.2510E-02	0.1652E+01		
P10				
0.6541E+00	0.3345E-01	-.8096E+00	0.0000E+00	0.0000E+00
0.2687E-01	-.7619E+00	0.0000E+00	0.0000E+00	0.0000E+00
0.0000E+00	0.0000E+00	0.0000E+00		
BETA				
0.3321E-01	0.2026E-01	0.1288E+01	0.0000E+00	0.0000E+00
0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00
0.0000E+00	0.0000E+00	0.0000E+00		
MEAN				
0.1576E+00	0.3077E-01	-.2632E+01	0.0000E+00	0.0000E+00
0.0000E+00	0.0000E+00	0.1410E-01	0.2814E+01	0.0000E+00
0.0000E+00	0.0000E+00	0.0000E+00		
ALPHA =	.31303			

PRESS RETURN TO CONTINUE

DAW \bar{G}_{00} vs \bar{P}

1/2

0 062

=====
Linear Fitting Report

Data File Name: C:\consult\swri\CLIMATE\MCMEPAR.PDW
=====

Model Equation(s):
G00=B+A*PMM

Initial Parameters:

A= -0.0024775095
B= 3.07017494

Save Options:

Save Data

Number of Function Calls: 2

Parameters After Fitting:

A= -0.0024775095
B= 3.07017494

SumSqr: 0.073782166
StdDev: 0.067907182

Covariance Matrix:

cvm[1,1]: 0.00003244837
cvm[2,1]: -0.0060152038
cvm[2,2]: 1.28175111

Goodness of Fit Statistics ...

___ C O D: 0.71940166
___ Corrl: 0.84817549
___ M S C: 0.60416436

Parameter Statistics...

Parameter: A= -0.0024775095

StdDev: 0.00077364580
Coeff. of Variance: -31.22675346

___ 95 % Confidence Interval

___ Uninvariant ...

LOW: -0.0046254945
HIGH: -0.00032952463

___ Supporting Plane ...

LOW: -0.0053606814
HIGH: 0.00040566229

Parameter: B= 3.07017494

DAW

\bar{G}_0 vs \bar{P}

2/2

StdDev: 0.15376148
Coeff. of Variance: 5.00823193

063

___ 95 % Confidence Interval

___ Uninvariant ...

LOW: 2.64326466
HIGH: 3.49708522

___ Supporting Plane ...

LOW: 2.49714685
HIGH: 3.64320303

=====
----Created by David A. Woolhiser with PSI-Plot
----Fri May 28 09:15:42 1999
=====

~~DAW~~

\bar{G}_{10} vs \bar{P}

1/2

=====
Linear Fitting Report

064

Data File Name: C:\consult\swri\CLIMATE\MCMEPAR.PDW
=====

Model Equation(s):
G10=B+A*PMM

Initial Parameters:

A= -0.0016109222
B= 0.93161567

Save Options:

Save Data

Number of Function Calls:

4

Parameters After Fitting:

A= -0.0016109222
B= 0.93161567

SumSqr: 0.092901455
StdDev: 0.076199350

Covariance Matrix:

cvm[1,1]: 0.00003244837
cvm[2,1]: -0.0060152038
cvm[2,2]: 1.28175111

Goodness of Fit Statistics ...

___ C O D: 0.46261473
___ Corrl: 0.68015787
___ M S C: -0.045626672

Parameter Statistics...

Parameter: A= -0.0016109222

StdDev: 0.00086811594
Coeff. of Variance: -53.88937589

___ 95 % Confidence Interval

___ Uninvariant ...

LOW: -0.0040211983
HIGH: 0.00079935382

___ Supporting Plane ...

LOW: -0.0048461591
HIGH: 0.0016243147

Parameter: B= 0.93161567

~~DAW~~ DAW

G_{10} vs. \bar{P}

2/2

0 065

StdDev: 0.17253735
Coeff. of Variance: 18.52022794

___ 95 % Confidence Interval

___ Uninvariant ...

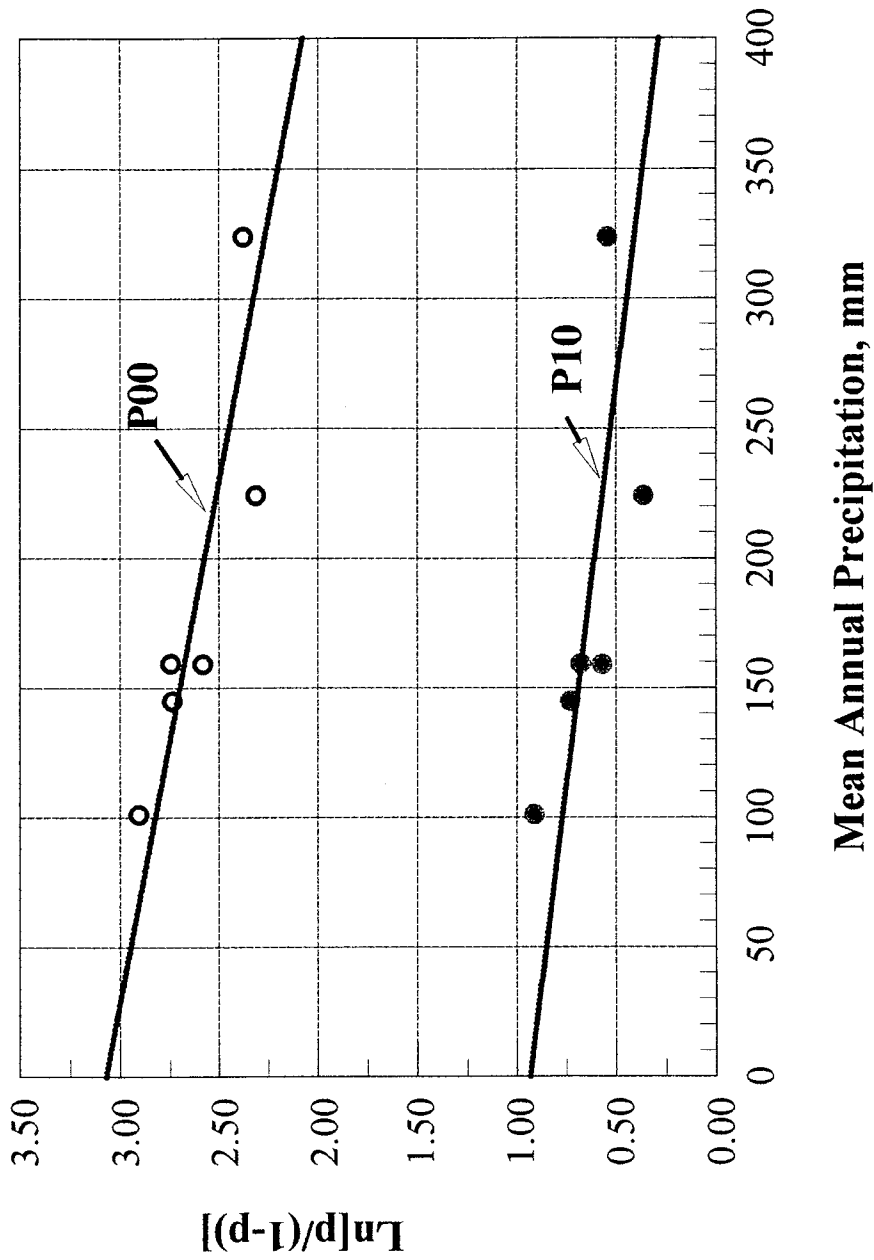
LOW: 0.45257524
HIGH: 1.41065610

___ Supporting Plane ...

LOW: 0.28861494
HIGH: 1.57461641

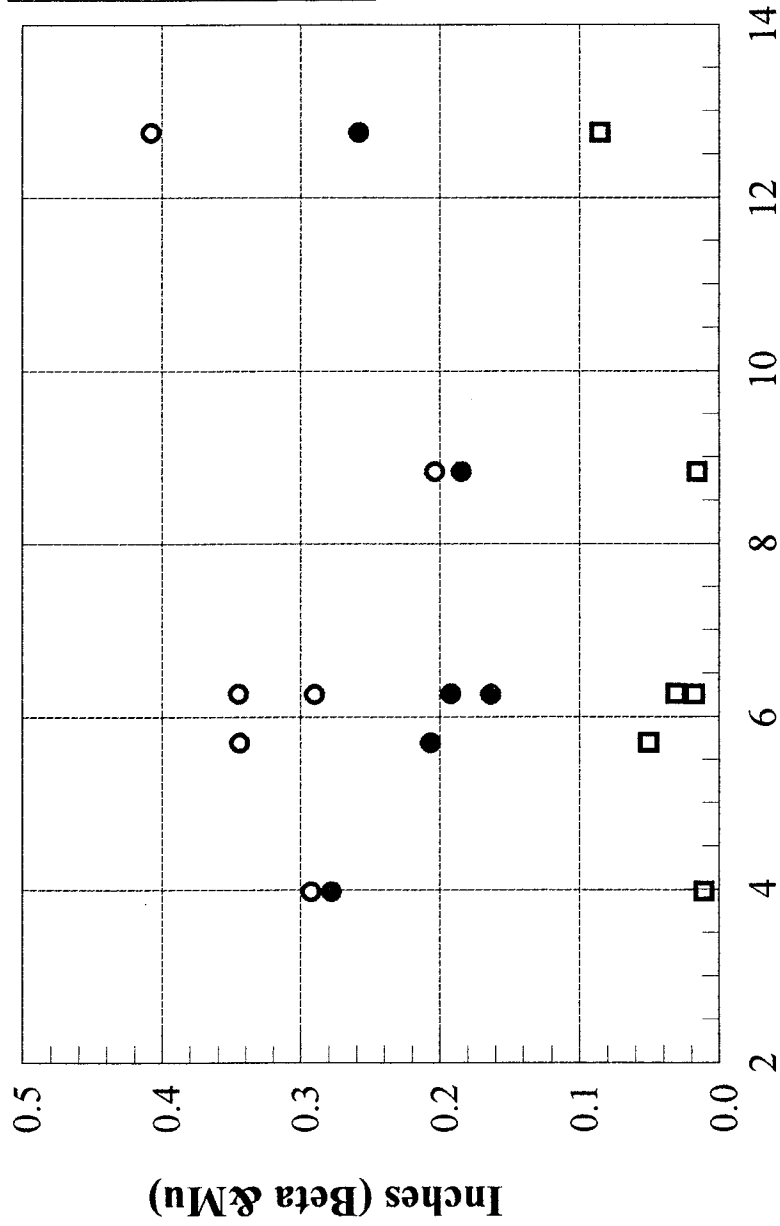
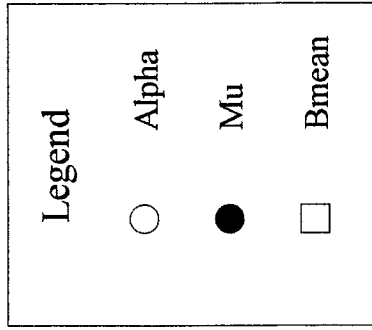
=====
----Created by David A. Woolhiser with PSI-Plot
----Fri May 28 09:22:05 1999
=====

DAW



Relations between the mean logits and Annual Precipitation

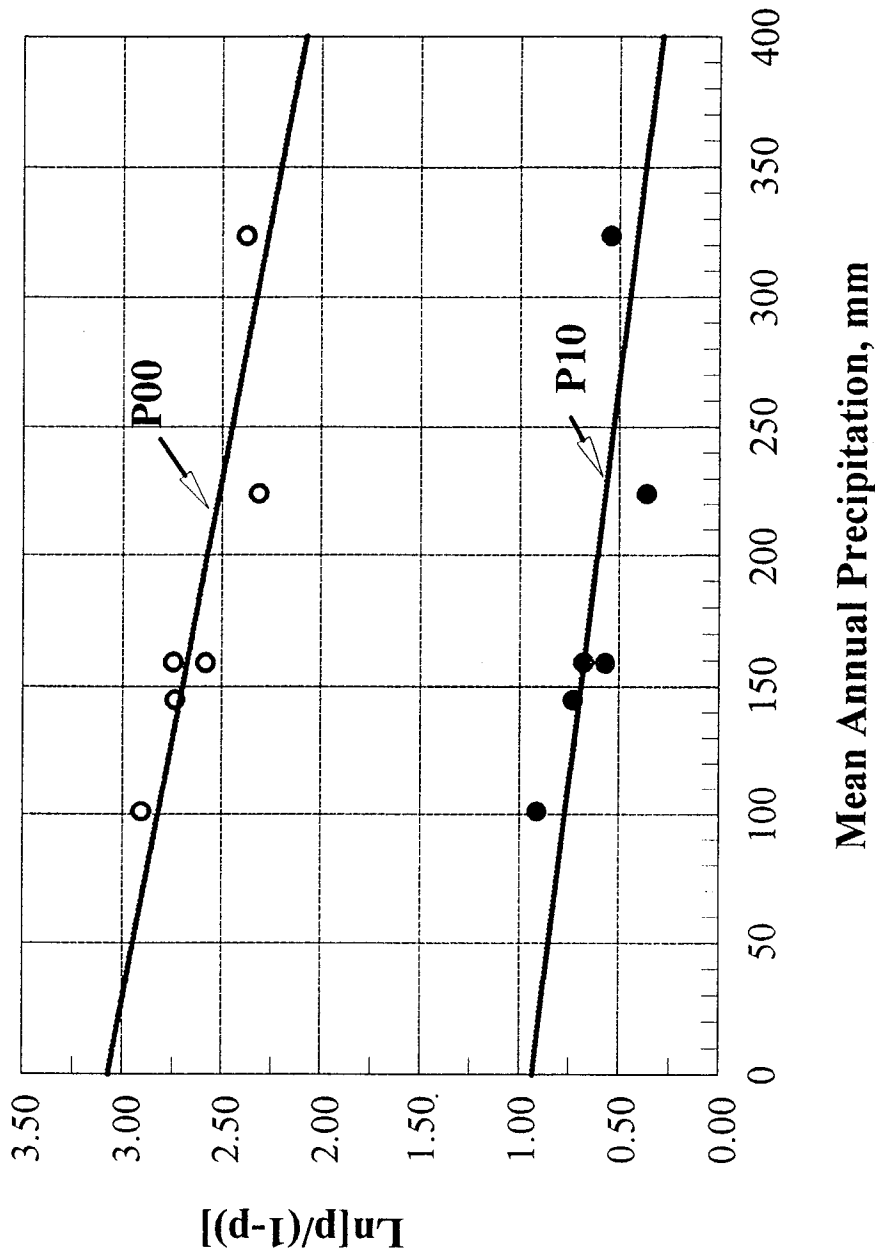
MEPAR.PGW
DAW 5/28/99



Mean Annual Precipitation, in.

DAW

DAW



Relations between the mean logits and Annual Precipitation

C:\CONSULT\SWR\CLIMATE\THETA.PDW

Station	AnPmm	MUAve	C1	Phi1	C2	Phi2	C3	Phi3
Adaven	324.9000	0.2293	0.0635	-2.6941	0.0204	0.3731	0.0081	-3.2667
Beatty8n	156.5000	0.1843	0.0217	2.9537	0.0241	1.7642	0.0143	0.6063
Goldfield	164.8000	0.1652	0.0402	-1.9533	0.0352	0.6328	0.0559	-3.3626
Tonopah	135.1000	0.1045	0.0303	-1.4535	0.0168	0.4261	0.0054	-3.9021
Las Vegas	105.4000	0.1916	0.0161	-1.9924	0.0187	2.4895	0.0070	-0.5475
Caliente	223.5000	0.2134	0.0360	-2.3082	0.0140	0.2298	0.0011	2.5127

$\bar{T}_a = 0.1147 + 0.000360 P$ $R = 0.648$ $R^2 = 0.420$ *DMW 8/6/99*

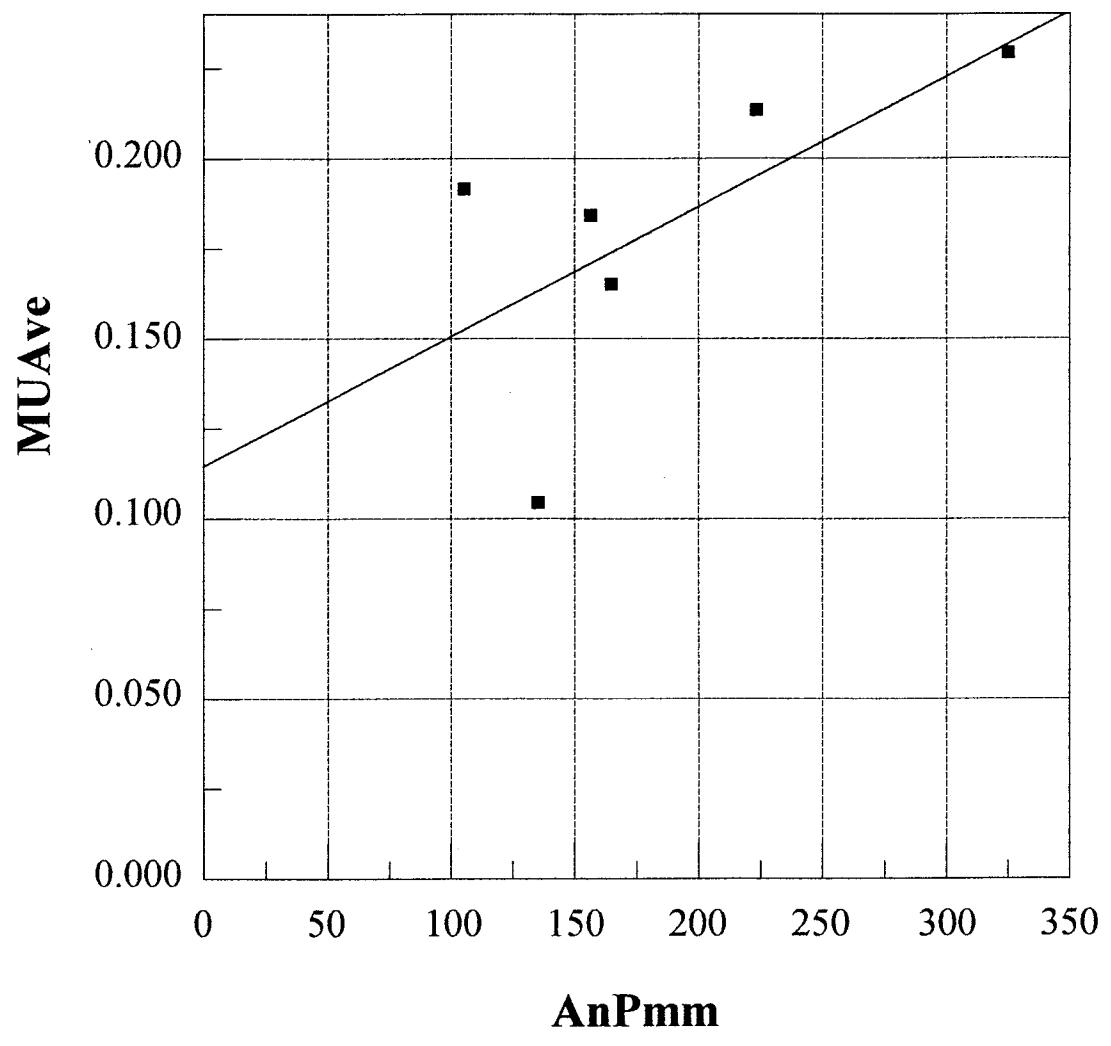
MIXED EXPERIMENTAL PARAMETERS

DMW

DAW

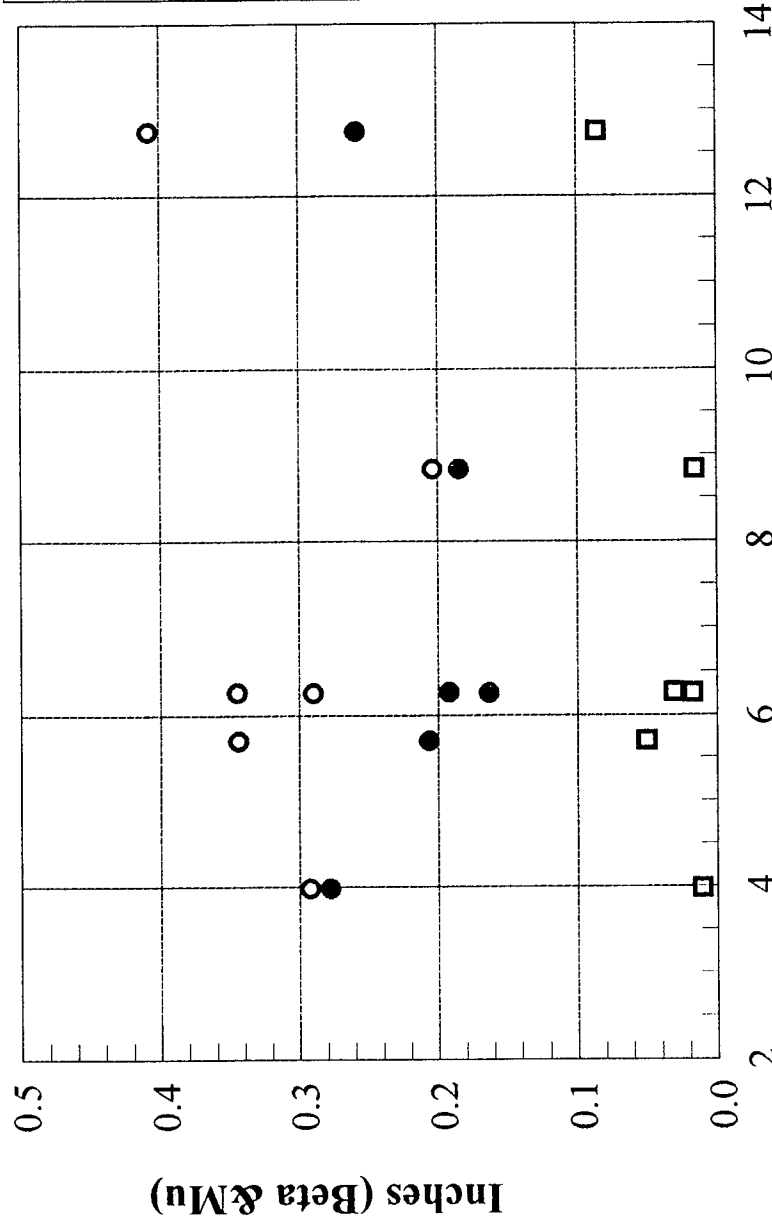
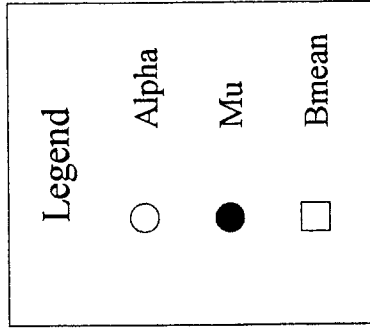
0 070

THETA.PDW



MuVSP.pgw DAW 8-6-99

MEPAR.PGW
DAW 5/28/99



Mean Annual Precipitation, in.

PROGRAM MCFO

C
 C PROGRAM: MCFO (MCMELOG) *DAW DAW 8/3/99*
 C VERSION: 2.1
 C DATE : 3, OCT, 1997
 C WRITTEN: DR. WOOLHEISER (MODIFICADO POR GIL), REV. DAW 5/21/99
 C LANGUAGE: FORTRAN 77

0. 072

C La versi=A2n 2.1 calcula lo mismo que la 2.0 pero para todas las
 C estaciones indicadas en la tarjeta y para los 21 per=A1odos
 C seleccionados.

C DESCRIPTION:

C -----

C *
 C * A FIRST ORDER MARKOV CHAIN WITH TWO STATES
 C * IS USED TO DESCRIBE WET AND DRY DAY OCCURRENCE
 C * THE PROBABILITIES ARE TRANSFORMED TO LOGITS.
 C * THE PARAMETERS ARE DETERMINED BY USING A NEWTON
 C * RAPHSON METHOD.
 C *
 C * CONSTRAINTS
 C * *****
 C *
 C** * MAXIMUM NUMBER OF YEARS = 120 (NCOUNT AND NLU)
 C * MAXIMUM NUMBER OF HARMONICS = (LMAXH) FOR MC.
 C * MAXIMUM NUMBER IN REAL MATRIX (*B* MATRIX) = 1301 (NRE)
 C** * MAXIMUM NUMBER OF WET DAYS IN A 14-DAY PERIOD = 1300 (PROGRAM
 C * WILL STOP *STOP1* AT SUBROUTINE *CALCUL* IF THAT NUMBER IS
 C * EXCEEDED)
 C** * MAXIMUM NUMBER OF WET DAYS ON A CALENDAR DAY = 120 (PROGRAM
 C * WILL STOP *STOP2* AT SUBROUTINE *CALCUL* IF THAT NUMBER IS
 C * EXCEEDED)
 C * PROGRAM CAN WORK WITH ONLY ONE STATION AT EACH TIME

C *****

C DESCRIPCION DEL FICHERO DE ENTRADA DE DATOS

C RECORD 1: PNAME : FICHERO CON LOS DATOS DE PRECIPITACION

C RECORD 2: ONAME : FICHERO CON LA SALIDA DE LOS RESULTADOS DE LA
 C CADENA DE MARKOV DE PRIMER ORDEN.

C RECORD 3: NAME : A30 NOMBRE DE LA ESTACION

C RECORD 4: LMAXH : 00 - 05 I5 NUMERO DE ARMONICOS A CONSIDERAR EN EL
 C PROCESO DE OCURRENCIA

C RECORD 5: THRES : 00 - 06 F6.4 UMBRAL DE PREC. PARA LOS DIAS LLUVIOSOS

C NRE : 07 - 11 I5 NUMERO DE VALORES EN LA MATRIZ REAL

C NCOUNT: 12 - 16 I5 NUMERO DE A=A5OS EN EL FICHERO A USAR

C SCREEN: 17 - 22 F6.3 CHI-SQUARE VALUE WITH TWO DEGREES OF
 C FREEDOM RECOMMENDED LEVEL = 0.05

C NLU : 23 - 27 I4 NUMERO DE A=A5OS DEL FICHERO QUE SE= SALTAN

C INIC : 28 - 32 I5 PRIMER A=A50 DEL REGISTRO CONSIDERADO

C RECORD 7: NPER : 10 - 11 I2 NUMERO DE PERIODOS (13 o 52)

INTEGER IHMC

Daw

```

COMMON /UNO/PRE(120,365),NCOUNT,THRES,NLU,INIC
COMMON /DOS/PDD(52),PWD(52),ALFA(52),BETA(52),TETA(52),
1 DMEAN(52)
COMMON /SEIS/B(1301),AMP(6,6),PAN(6,6),
1 MAXH,SCREEN,ALMEAN,BEMEAN,TEMEAN,
2 XMUMEAN
COMMON /ONE/NPER,NPER
COMMON /OBS52/NDD(52),NWD(52),NDW(52),NWW(52),ND(52),NW(52),
1 PDD52(52),PWD52(52),PW52(52)
COMMON /OBS365/N11(365),N21(365),N12(365),N22(365),
1 N1(365),N2(365),
1 PDD365(365),PWD365(365),PW365(365)
COMMON /CNTM/NMD(52),N31(365),NMW(52),N32(365),
1 NDM(52),N13(365),NWM(52),N23(365),NMM(52),N33(365),
2 NTD(52),NT1(365),NTW(52),NT2(365),NTM(52),NT3(365),
3 NMDT,NMWT,NMMT,NDMT,NWMT,NDDT,NWDT,NDWT,NWWT,
4 MNTM(52),MNAM(52)
COMMON /PRED52 /TPDD52(52),TPWD52(52),TPW52(52),
1 TAMT52(52),TDWA52(52)
COMMON /PRED365/TPDD365(365),TPWD365(365),TPW365(365),
1 TAMT365(365),TDWA365(365)
COMMON /MCL/PARMCL(12,4,5),FLIKE(4,5),AMCAMP(0:12,4,5),
1 AMCPHS(12,4,5)
COMMON /ALL/LMAXH,LNPER,PHI(12,365)
LOGICAL COMP
COMMON /JALG/COMP

```

```

CHARACTER ONAME*30,PNAME*30,NAME*30
INTEGER NNPP(21),NUMEST

```

```

DATA NNPP/52,40,36,30,26,24,22,21,20,19,18,
117,16,15,14,13,12,10,8,7,6/

```

C
C
C
C

THE FOLLOWING ARRAYS WERE ADDED TO GENERATE DAILY PRECIPITATION FOR OBSERVED AND PREDICTED.

C
C
C
C

```

PROMPT USER FOR INPUT PARAMETER FILE NAME
=====

```

C
C

```

OPEN(UNIT=19,FILE='TTJJTT',STATUS='OLD')
READ INPUT AND OUTPUT FILENAMES FROM PARAMETER FILE
=====

```

1515

```

READ(19,11,END=4)LMAXH
READ(19,12,END=4)THRES,NRE,NCOUNT,SCREEN,NLU,INIC
READ(19,9) ONAME
OPEN(UNIT=17,FILE=ONAME,STATUS='NEW')
READ(19,1515)NUMEST
FORMAT(I2)
DATA NSTA/0001/
WRITE(17,900)
III =IFIX(SCREEN)

IHMC=LMAXH
IF (IHMC.EQ.0)IHMC=5

IF(5-III.LT.0)THEN

```

DAW

```

WRITE(17,52)SCREEN,0.01
ELSE IF(5-III.EQ.0)THEN
WRITE(17,52)SCREEN,0.05
ELSE
WRITE(17,52)SCREEN,0.1
ENDIF
C Begin loop for multiple stations

```

```

DO KKK=1,NUMEST
READ(19,9) PNAME
OPEN(UNIT=16,FILE=PNAME,STATUS='OLD')
IJ =INIC+NLU
JI =IJ+NCOUNT-1

```

```

C READ PRECIPITATION DATA
C =====

```

```

READ(16,10,END=4)NAME
WRITE(17,2222)NAME
2222 FORMAT (' ;',A)
WRITE(17,40)NSTA,NAME,NCOUNT,IJ,JI

```

```

C NEED TO SKIP FILES
C -----

```

```

C Revision of reading format DAW 5/18/99 TMAX and TMIN read but not used
C IF(NLU.NE.0)THEN
C DO I=1,NLU
C READ(16,30)(PRE(I,J),J=1,365)
C ENDDO
C DO I=1,NLU
C DO J=1,365
C READ(16,30) PRE(I,J), TMAX, TMIN
C ENDDO
C ENDDO
C ENDIF

```

```

C READ PRECIPITATION DATA Revised format by DAW 5/18/99
C -----

```

```

DO I=1,NCOUNT
DO J=1,365
C READ(16,30)(PRE(I,J),J=1,365)
C READ(16,30) PRE(I,J), TMAX, TMIN
C ENDDO
C ENDDO

```

```

C DO IJI=1,21 Took out DO loop on multiple periods, DAW 5/21/99
C IJI=5

```

RUN C2 ~~DAW~~

1/2

PROGRAM MCFO VER. 2.0 (FORTRAN 77)

DAW 8/3/99

SCREEN = 5.990 WHICH IS THE 0.05 SIGNIFICANCE LEVEL
;: STATION NUMBER 268170 TONO
RAINGAGE= 1 : STATION NUMBER 268170 TONO
YEARS = 42 (SINCE 1955 TO 1996)

TONOPAH4.OUT 6 075
TONOPAHMC.CON

OCCURRENCE PROCESS

42 NDD NDW NWD NWW ND NW; # OF PERIODS= 26

426	59	64	38	485	102
471	48	45	24	519	69
496	35	38	19	531	57
487	43	43	15	530	58
490	41	37	20	531	57
484	36	39	29	520	68
483	43	42	20	526	62
498	33	36	21	531	57
551	14	16	7	565	23
516	29	26	17	545	43
451	50	52	35	501	87
465	54	51	18	519	69
497	34	37	20	531	57
500	33	30	25	533	55
511	30	31	16	541	47
515	27	28	18	542	46
532	24	23	9	556	32
519	26	27	16	545	43
495	36	35	22	531	57
497	39	39	13	536	52
513	31	30	12	544	42
490	37	39	22	527	61
462	44	42	40	506	82
471	49	48	20	520	68
474	39	38	37	513	75
504	49	47	30	553	77

NUMBER OF PARAMETERS CONSIDERED= 9

DRY-DRY SITUATION:

Number of Periods= 26

Initial Parameter Estimates:

2.6050	-.58667E-01	-.23233	0.21174E-01	-.14402
-.47759E-01	0.72349E-01	0.88425E-01	-.17559E-01	

likelihood Function = -3523.88770

Optimum Parameter Estimates:

2.5885	-.29964E-01	-.21697	0.13916	-.19069
-.17892	0.15912	0.27765	-.24554	

RUN C3

CALIEN4.OUT

1/2

Draw 8/4/99

PROGRAM MCFO VER. 2.0 (FORTRAN 77)

077

SCREEN = 5.990 WHICH IS THE 0.05 SIGNIFICANCE LEVEL
 ;: STATION NUMBER 261358 CALI
 RAINGAGE= 1 : STATION NUMBER 261358 CALI
 YEARS = 40 (SINCE 1929 TO 1968)

OCCURRENCE PROCESS

40 NDD NDW NWD NWW ND NW; # OF PERIODS= 26

415	43	43	44	458	87
390	58	57	41	448	98
431	41	46	39	472	85
467	39	32	22	506	54
408	49	56	47	457	103
446	44	42	28	490	70
445	46	42	27	491	69
513	16	23	8	529	31
503	23	20	9	526	29
433	47	43	35	480	78
375	69	74	42	444	116
380	65	64	51	445	115
439	45	47	29	484	76
479	32	29	20	511	49
478	28	29	25	506	54
465	30	30	30	495	60
456	37	39	28	493	67
484	28	30	18	512	48
445	44	43	28	489	71
459	36	37	18	495	55
430	38	34	30	468	64
399	52	52	33	451	85
416	55	55	34	471	89
407	59	61	33	466	94
399	61	56	44	460	100
421	66	67	43	487	110

NUMBER OF PARAMETERS CONSIDERED= 9

DRY-DRY SITUATION:

Number of Periods= 26

Initial Parameter Estimates:

2.3414	0.42186E-02	-.22307	0.12341	-.16401
-.10224	0.52824E-01	0.26403	0.17764	

likelihood Function = -3812.15601

Optimum Parameter Estimates:

-.24220	0.27522E-01	-.22118	0.27726	-.26539
2.3243	0.18315	0.33879	-.12306	

Call 4.0V

2/2

~~DAW~~

078

Corresponding Amplitudes:

2.3243	0.22288	0.38381	0.30365	0.36045
--------	---------	---------	---------	---------

Corresponding Phase Angles:

0.0000	-1.4470	-0.76353	2.4941	-0.34840
--------	---------	----------	--------	----------

Likelihood Function = -3789.72095 with 4 harmonics - 4
 -3805.12 " 3 " - 7

WET-DRY SITUATION:

Number of Periods= 26

Initial Parameter Estimates:

0.38758	0.35862E-01	-0.26183E-01	-0.15927	-0.16506
-0.10063E-01	0.38011E-01	0.97160E-02	0.29917E-01	

Likelihood Function = -1324.90662

Optimum Parameter Estimates:

0.36226	0.40061E-02	-0.15927E-01	-0.98816E-01	-0.82958E-01
-0.35390E-01	0.43169E-01	-0.55079E-01	0.52161E-01	

Corresponding Amplitudes:

0.36226	0.16423E-01	0.12902	0.55821E-01	0.75858E-01
---------	-------------	---------	-------------	-------------

Corresponding Phase Angles:

0.0000	-1.3244	-2.4432	2.2575	2.3834
--------	---------	---------	--------	--------

Likelihood Function = -1323.10815 with 9
 -1323.22 with 7
 FINAL LOG LIKELIHOOD FUNCTION: -5112.82910
 26; -5112.829100

4 harmonics for pi
 3 " for pi

RUNC4

ADAVEN4.OUT

1/2

PROGRAM MCFO VER. 2.0 (FORTRAN 77)

DAW 8/4/99

~~DAW~~

079

SCREEN = 5.990 WHICH IS THE 0.05 SIGNIFICANCE LEVEL
;: STATION NUMBER 260046 ADAV
RAINGAGE= 1 : STATION NUMBER 260046 ADAV
YEARS = 32 (SINCE 1930 TO 1961)

OCCURRENCE PROCESS

32 NDD NDW NWD NWW ND NW; # OF PERIODS= 26

309	50	49	38	359	87
350	37	38	23	387	61
326	47	48	27	373	75
346	44	40	18	390	58
344	33	38	33	377	71
379	29	28	12	408	40
373	29	29	17	402	46
373	30	32	13	403	45
412	16	14	6	428	20
372	30	30	16	402	46
315	52	50	31	367	81
332	41	45	30	373	75
373	28	28	19	401	47
387	24	22	15	411	37
388	26	26	8	414	34
400	20	21	7	420	28
408	18	18	4	426	22
396	19	18	15	415	33
366	32	31	19	398	50
363	32	34	19	395	53
370	33	29	16	403	45
339	39	41	27	378	68
317	41	40	36	358	76
318	41	44	30	359	74
305	46	43	33	351	76
324	52	54	30	376	84

NUMBER OF PARAMETERS CONSIDERED= 9

DRY-DRY SITUATION:

Number of Periods= 26

Initial Parameter Estimates:

2.3924	-.89921E-01	-.37374	0.12667	-.14657
-.12660	0.31321E-01	0.10195	0.45248E-01	

Likelihood Function = -2975.11523

Optimum Parameter Estimates:

-.27708819	0.18687959E-01	0.20186397	-.10286419	-.25978
------------	----------------	------------	------------	---------

Corresponding Amplitudes:

~~DAW~~

2.3819 0.36420 0.37052 0.33419 0.22590

Corresponding Phase Angles:

0.0000 -1.6064 -0.77698 2.5482 -0.47310

Likelihood Function = -2966.36182 for 4 AIC = 5950.72 * min
 -2969.66 for 3 AIC = 5953.32

WET-DRY SITUATION:

Number of Periods= 26

Initial Parameter Estimates:

0.57969 0.46737E-02 -0.16673 0.14140 -0.11991E-01
-.80632E-01 0.48191E-01 0.10286 0.59837E-02
Likelihood Function = -946.595947

Optimum Parameter Estimates:

0.55822 0.53863E-01 -0.17164 0.14495 -0.79952E-01
-.16200 0.17071 0.24001 -0.17099

Corresponding Amplitudes:

0.55822 0.17989 0.16553 0.23534 0.29469

Corresponding Phase Angles:

0.0000 -1.2667 -0.50407 2.3300 -0.61901

Likelihood Function = -944.853760 AIC = 1907.7
 -946.33 for 3 harmonics AIC = 1906.66 * min

FINAL LOG LIKELIHOOD FUNCTION: -3911.21558
26; -3911.215580

Run C5

BEATEN 4. OUT

1/2

PROGRAM MCFO VER. 2.0 (FORTRAN 77)

DAW 8/4/99

081

 SCREEN = 5.990 WHICH IS THE 0.05 SIGNIFICANCE LEVEL
 ;: STATION NUMBER 260718 BEAT
 RAINGAGE= 1 : STATION NUMBER 260718 BEAT
 YEARS = 24 (SINCE 1973 TO 1996)

DAW

OCCURRENCE PROCESS

24	NDD	NDW	NWD	NWW	ND	NW;	# OF PERIODS=	26
228	37	36	34	265	70			
241	33	37	22	274	59			
298	16	16	6	314	22			
295	15	17	9	310	26			
277	24	22	13	301	35			
279	23	23	11	302	34			
290	16	17	13	306	30			
312	11	11	2	323	13			
326	3	5	2	329	7			
312	10	8	6	322	14			
282	22	23	9	304	32			
289	21	19	7	310	26			
299	13	16	8	312	24			
299	16	14	7	315	21			
300	16	15	5	316	20			
294	15	17	10	309	27			
317	10	9	0	327	9			
293	16	18	9	309	27			
298	16	15	7	314	22			
296	19	18	3	315	21			
294	15	16	8	309	24			
283	22	21	10	305	31			
250	30	28	28	280	56			
272	24	26	14	296	40			
253	31	28	22	284	50			
282	28	29	15	310	44			

NUMBER OF PARAMETERS CONSIDERED= 9

DRY-DRY SITUATION:

Number of Periods= 26

Initial Parameter Estimates:

 2.7957 0.10169 -.44087 -.88447E-01 -.27936
 0.41542E-01 0.14732 0.12658 -.20314E-01
 Likelihood Function = -1845.98596

Optimum Parameter Estimates:

 -.94573E-01 0.14676 0.28712 0.92034E-01 -.27592

Corresponding Amplitudes:

2.7511	0.48574	0.29087	0.17459	0.39786
--------	---------	---------	---------	---------

Corresponding Phase Angles:

0.0000	-1.2549	-1.2489	2.1432	-.76458
--------	---------	---------	--------	---------

Likelihood Function = -1837.15564 * Min AIC
 -1840.30 for 3 harmonics

WET-DRY SITUATION:

Number of Periods= 26

Initial Parameter Estimates:

0.87648	-.29210	-.43405	0.29549	-.10890
0.37111E-01	0.23426	-.96922E-01	-.17861	

Likelihood Function = -514.907898

Optimum Parameter Estimates:

0.67330	-.28762E-01	-.25101	0.13162	-.14812
0.13256	-.24163E-01	-.77544E-01	0.51912E-01	

Corresponding Amplitudes:

0.67330	0.25265	0.19815	0.13475	0.93316E-01
---------	---------	---------	---------	-------------

Corresponding Phase Angles:

0.0000	-1.6849	-.84431	-.18030	2.5517
--------	---------	---------	---------	--------

Likelihood Function = -505.952240
 -506.03 * MIN AIC - 3 harmonics

FINAL LOG LIKELIHOOD FUNCTION: -2343.10791
 26; -2343.107910

RUNCG

GOLD4.00T

1/2

PROGRAM MCFO VER. 2.0 (FORTRAN 77)

D W W 8/4/99

~~DAW~~

083

SCREEN = 5.990 WHICH IS THE 0.05 SIGNIFICANCE LEVEL
 ;: STATION NUMBER 263285 GOLD
 RAINGAGE= 1 : STATION NUMBER 263285 GOLD
 YEARS = 28 (SINCE 1949 TO 1976)

OCCURRENCE PROCESS

28 NDD NDW NWD NWW ND NW; # OF PERIODS= 26

287	38	43	18	325	61
308	30	30	13	338	43
330	25	25	9	355	34
325	29	29	9	354	38
326	29	27	9	355	36
314	26	32	16	340	48
338	22	20	10	360	30
342	17	17	16	359	33
362	11	14	5	373	19
344	18	18	12	362	30
315	30	27	20	345	47
340	21	24	7	361	31
335	23	23	11	358	34
344	19	18	11	363	29
349	20	17	6	369	23
368	9	12	3	377	15
370	9	11	2	379	13
343	17	15	10	360	25
337	17	17	7	354	24
330	18	17	8	348	25
322	17	14	9	339	23
314	22	24	4	336	28
312	25	30	22	337	52
318	29	27	15	347	42
320	23	24	22	343	46
327	36	32	14	363	46

NUMBER OF PARAMETERS CONSIDERED= 9

DRY-DRY SITUATION:

Number of Periods= 26

Initial Parameter Estimates:

2.7574 -.18822 -.38450 0.41663E-01 -.15516
 -.66721E-01 0.90660E-01 0.61647E-01 -.44093E-01
 Likelihood Function = -2139.95459

Optimum Parameter Estimates:

2.7418 -.10657 -.34767 0.14350 -.21882
 -.20408 0.20483 0.25967 -.25412

Corresponding Amplitudes:

2.7418	0.36363	0.26168	0.28914	0.36333
--------	---------	---------	---------	---------

Corresponding Phase Angles:

0.0000	-1.8682	-.99035	2.3544	-.77460
--------	---------	---------	--------	---------

Likelihood Function = -2134.30225 * min AIC
 -2137.36 with 3

WET-DRY SITUATION:

Number of Periods= 26

Initial Parameter Estimates:

0.80254	-.82429E-01	-.52035E-01	0.25086	0.77472E-01
0.63243E-02	-.72870E-01	0.21155E-01	-.81634E-01	

Likelihood Function = -551.649963

Optimum Parameter Estimates:

0.73884	-.40275E-01	0.95444E-02	0.28077	-.29131E-01
0.17062	-.18365	0.13994	-.11812	

Corresponding Amplitudes:

0.73884	0.41390E-01	0.28228	0.25068	0.18313
---------	-------------	---------	---------	---------

Corresponding Phase Angles:

0.0000	2.9089	-.10338	-.82215	-.70106
--------	--------	---------	---------	---------

Likelihood Function = -549.572693
 -549.85 with 3 * min AIC

FINAL LOG LIKELIHOOD FUNCTION: -2683.87500
 26; -2683.875000

PROGRAM MCFO VER. 2.0 (FORTRAN 77)

8/14/99

DAW

085

SCREEN = 5.990 WHICH IS THE 0.05 SIGNIFICANCE LEVEL
; 264436 LAS VEGAS WSO AIRPOR
RAINGAGE= 1 264436 LAS VEGAS WSO AIRPOR
YEARS = 57 (SINCE 1937 TO 1993)

OCCURRENCE PROCESS

57 NDD NDW NWD NWW ND NW; # OF PERIODS= 26

642	61	61	33	703	94
666	53	55	24	719	79
704	35	38	21	739	59
727	30	31	10	757	41
734	27	29	8	761	37
738	30	26	4	768	30
731	27	29	11	758	40
771	11	14	2	782	16
775	10	8	5	785	13
715	38	33	12	753	45
644	64	67	23	708	90
645	64	63	26	709	89
698	42	43	15	740	58
703	38	40	17	741	57
734	28	27	9	762	36
714	36	34	14	750	48
739	26	26	7	765	33
705	36	39	18	741	57
693	47	42	16	740	58
711	37	39	11	748	50
680	46	44	28	726	72
697	37	42	22	734	64
644	61	56	37	705	93
676	46	50	26	722	76
652	58	54	34	710	88
699	65	63	28	764	91

NUMBER OF PARAMETERS CONSIDERED= 9

DRY-DRY SITUATION:

Number of Periods= 26

Initial Parameter Estimates:

2.9404	0.25822	-.15658	0.28670E-01	-.33125
-.18767	-.59885E-02	0.20679	0.86812E-01	

Likelihood Function = -4037.90723

Optimum Parameter Estimates:

-.32329	0.14635	0.26963	0.25539	-.18758	-.42625
---------	---------	---------	---------	---------	---------

Corresponding Amplitudes:

~~DAW~~

 2.9128 0.33880 0.50975 0.35487 0.33495

086

Corresponding Phase Angles:

 0.0000 -.65039 -.99029 2.7165 -.48979

Likelihood Function = -4013.51318 * min AIC
 -4021.84 for 3 harmonics

WET-DRY SITUATION:

 Number of Periods= 26

Initial Parameter Estimates:

 0.93578 0.19246 -.13055 0.11082 -.13521
 -.82729E-01 -.47410E-01 -.40004E-01 0.41874E-01
 Likelihood Function = -924.843628

Optimum Parameter Estimates:

 0.90554 0.23128 -.18748 0.17627 -.18538
 -.52110E-01 0.23725E-01 -.17913 0.16474

Corresponding Amplitudes:

 0.90554 0.29772 0.25580 0.57257E-01 0.24337

Corresponding Phase Angles:

 0.0000 -.68118 -.81057 2.7144 2.3980

Likelihood Function = -922.343994
 -923.08 for 3 harmonics * min AIC

FINAL LOG LIKELIHOOD FUNCTION: -4935.85742
 26; -4935.857420

Rerun the mixed exponential analysis with α = a regional constant.

Average α from 6 stations

~~Daw~~

First check to see if more harmonics are appropriate (i.e. lead to a lower Akaike Information Criterion (AIC))

Run Caliente with 4 harmonics - 2 harmonics gave a lower AIC for Mixed exponential. 40 yrs

Try Caliente with 3 harmonics - 2 harmonics still gives minimum AIC

Run C2 - Tonopah with 4 harmonics MC $\left\{ \begin{array}{l} 4 \text{ harmonics for } p_{00} \\ 3 \text{ " " " " " " " " } \\ 3 \text{ " " " " " " " " } \end{array} \right.$ Min AIC $\left\{ \begin{array}{l} p_{10} \\ p_{10} \\ p_{10} \end{array} \right.$
 8/14/99 Continue computer runs with MCFOIR.

Run C3 - Caliente 4 harmonics give lowest AIC for p_{00}
 3 " " " " " " for p_{10}

Run C4 - Adaven 4 harmonics for p_{00}
 3 " " for p_{10}

Run C5 - BEATTY8N 4 harmonics for p_{00}
 3 " " for p_{10}

Run C6 - GOLDFIELD " "

Run C7 - Las Vegas " "

CONCLUSION: Require 4 harmonics for p_{00} } all stations
 " 3 " " " " } p_{10}

Now make computer runs with ~~MCFOIR~~ ^{Daw 4/2/04} MELSIREV - 3 harmonics

Run C8 - Las Vegas 3 harmonics - minimum AIC 40 yrs

Run C9 - Adaven 3 harmonics - min. AIC 32 "

Run C10 - BEATTY8N 2 harmonics - min AIC 24 "

Run C11 - Goldfield 3 harmonics - min AIC 28 "

Run C12 - Tonopah 2 harmonics - min AIC 42 "

CONCLUSION: 3 have 3 harmonics, 3 have 2 harmonics. Not directly related to record length. For consistency use the 3 harmonic cases to get an average α .

13-782 50 SHEETS, FILER, 5 SQUARE
 42-381 100 SHEETS, FOLDER, 5 SQUARE
 42-382 100 SHEETS, FOLDER, 5 SQUARE
 42-383 200 SHEETS, FOLDER, 5 SQUARE
 42-384 200 SHEETS, FOLDER, 5 SQUARE
 42-385 100 RECYCLED WHITE 5 SQUARE
 42-386 200 RECYCLED WHITE 5 SQUARE
 Made in U.S.A.



Set up a spreadsheet for each parameter estimated as a Fourier Series. Use

1. G_{00} G00.PDW four harmonics ✓ — DAW

2. G_{10} G10.PDW three harmonics (088

3. $\beta + \alpha$ ALBETA.PDW Three harmonics $\bar{\alpha} = 0.298$

4. ~~Theta~~ ^{THETA} THETA.PDW Three harmonics (α variable)

5. β with α constant
Col. 1 Col. 2.

Station An. Precip
(mm)

6. μ . PDW with α constant.

8/6/99

Complete 6 runs with $\bar{\alpha} = 0.298$

Attempted runs with α input. The revisions in Spain seem to have created a problem with this option - no results for 2 stations (Runs C13 + C14)

Entered data in spreadsheets G10.PDW and ALBETA.PDW

Findings:

1. There is a weak correlation between $\ln\left(\frac{\alpha}{1-\alpha}\right)$ and mean annual P . $R = 0.356$ $R^2 = 0.127$

$$\ln\left(\frac{\alpha}{1-\alpha}\right) = -0.5695 - 0.00168 P$$

2. There is a stronger correlation between β and mean annual P . $R = 0.723$ $R^2 = 0.522$

$$\bar{\beta} = -0.01534 + 0.000286 \bar{P} \quad (\beta \text{ in inches, } \bar{P} \text{ in mm.})$$

$$= -0.3896 + 0.0073 \bar{P} \quad (\beta \text{ in mm, } \bar{P} \text{ in mm.})$$

(Gradient in Idaho was 0.0021 so there is a stronger relation in Nevada.)

PROGRAM MCMELOG

DAW 8/6/99

089

C
 C PROGRAM: MELSI (MCMELOG + AGUA53)
 C VERSION: 2.0
 C DATE : 16, OCT, 1997
 C WRITTEN: DR. WOOLHEISER (MODIFICADO POR GIL) Rev. by DAW 5/21/99
 C LANGUAGE: FORTRAN 77

C DESCRIPTION:

C *
 C * A MIXED EXPONENTIAL DISTRIBUTION IS USED TO
 C * DESCRIBE THE PRECIPITATION DEPTH ON WET DAYS.
 C * THE SIMPLEX METHOD IS USED TO OPTIMIZE PARAMETERS.
 C * LA OPTIMIZACION QUE SE REALIZA ES SIMULTANEA.
 C *
 C * CONSTRAINTS
 C * *****
 C *
 C** * MAXIMUM NUMBER OF YEARS = 50 (NCOUNT AND NLU)
 C * MAXIMUM NUMBER OF HARMONICS = 6(MAXH AND MAXH1) FOR MIX-EXP
 C * MAXIMUM NUMBER IN REAL MATRIX (*B* MATRIX) = 1301 (NRE)
 C** * MAXIMUM NUMBER OF WET DAYS IN A 14-DAY PERIOD = 1300 (PROGRAM
 C * WILL STOP *STOP1* AT SUBROUTINE *CALCUL* IF THAT NUMBER IS
 C * EXCEEDED)
 C** * MAXIMUM NUMBER OF WET DAYS ON A CALENDAR DAY = 120 (PROGRAM
 C * WILL STOP *STOP2* AT SUBROUTINE *CALCUL* IF THAT NUMBER IS
 C * EXCEEDED)
 C * PROGRAM CAN WORK WITH ONLY ONE STATION AT EACH TIME

REAL*8 PAREPS,FNEPS
 INTEGER IHMC
 COMMON/UNO/PRE(50,365),NCOUNT,THRES,NLU,INIC,NUMSAV,MOR(26)
 COMMON/DOS/PDD(26),PWD(26),ALFA(26),BETA(26),TETA(26),DIB(26),
 1 DMEAN(26)
 COMMON/NUEVE/ALF1(365),BET1(365),TET1(365),UNITX,AMAX,AMIN,BMIN,
 1 TMIN,QLIKX,NCX(6,3),NC1X(6,3),XMU(365)
 COMMON/SEIS/B(1301),SENO(6,365),COSE(6,365),AMP(6,6),PAN(6,6),
 1 MAXH,SCREEN,ALMEAN,BEMEAN,TEMEAN,MAXA,MAXB,MAXT,CALFA,
 2 KALFA,XMUMEAN
 COMMON/OCHO/PR(50,1300),MX(26),LX(365),MM,IPER,ORMOM1(26),
 1 MSD(26)
 COMMON/DIEZ/SECO(53),HUM(53),PLO(53),PAR1(53),PAR2(53),PAR3(53),
 1 ZMEDIA(53)
 COMMON/ONE/NPER,NNPER,PAREPS,FNEPS,ZMIS
 COMMON/PRED365/TPDD365(365),TPWD365(365),TPW365(365),
 1 TAMT365(365),TDWA365(365)
 COMMON/ACCUM26/ACOBNSU(26),ACPRENU(26),ACOBNSAM(26),ACPREAM(26),
 1 ACOBSMS(26)
 COMMON/ALL/LMAXH,LNPER,PHI(12,365)
 CHARACTER FNAME*30,INAME*30,ONAME*30,PNAME*30,NAME*30,
 1 ZL(9)*4,OFIL*30

C
 C THE FOLLOWING ARRAYS WERE ADDED TO GENERATE DAILY PRECIPITATION FOR
 C OBSERVED AND PREDICTED.
 C

DATA CALFA/0./,KALFA,NUMSAV/2*0/

Daw

```

C   FORMATS
C   -----
9   FORMAT(A)
   FORMAT(I4,A,F6.4,3I5,F6.3,2I4,3I2,I5)
33  FORMAT(F6.2, 2X,F6.0,2X,F6.0)
25  FORMAT(//,' DISTRIBUTION OF PRECIPITATION DEPTH',/
1    ' -----',//)
35  FORMAT(1H1)
40  FORMAT(' RAINGAGE=',I5,2X,A30,/
1    ' YEARS   =',I5,2X,'(SINCE',1X,I5,2X,'TO',1X,I5,')')
50  FORMAT(' WET DAY THRESHOLD   =',F6.4/
1    ' TABLE OF REAL VALUES=',I5/
1    ' HARMS(MARKOV)           =',I2/
1    ' HARMS(MIX.EXP)         =',I2)
52  FORMAT(' SCREEN =',F6.3,2X,'WHICH IS THE',F5.2,
1    ' SIGNIFICANCE LEVEL')
690 FORMAT(' PARAMETER CONVERGENCE TOLERANCE = 'G12.5,/,
1    ' FUNCTION CONVERGENCE TOLERANCE = 'G12.5,/,/,
2    ' MISSING PRECIPITATION CODE = 'G12.5)
700 FORMAT(F9.0,3I2)
710 FORMAT(' CONSTANT VALUE FOR ALFA HAS BEEN INPUTTED ',5X,
1 'INPUT VALUE = 'F8.4,' ONLY BETA AND TETA WILL BE OPTIMIZED')
720 FORMAT(' CONSTANT ALFA WILL BE OBTAINED FROM THE MEANS OF '
1    'ALFAS OPTIMIZED OVER 26 BIWEEKLY PERIODS')
725 FORMAT(1X,8I5)
730 FORMAT(1X,I5,' PERIODS WILL BE SAVED ',5X,'THEY ARE:'(10I5))
731 FORMAT(' NUMBER OF PERIODS CONSIDERED IN ANALYSIS = ',I2)
770 FORMAT(// OBSERVED NUMBER OF ACCUMULATED WET DAYS//)
777 FORMAT(// THEORETICAL NUMBER OF ACCUMULATED WET DAYS//)
778 FORMAT(// OBSERVED NUMBER OF ACCUMULATED MISSING DAYS//)
800 FORMAT(// OBSERVED ACCUMULATED PRECIPITATION DEPTH PER ',
1    I2, '-DAY PERIODS'//)
810 FORMAT(10X,13F8.2)
820 FORMAT(// THEORETICAL ACCUMULATED PRECIPITATION DEPTH PER ',
1    I2, '-DAY PERIODS'//)
830 FORMAT('1COMPUTED PARAMETER VALUES'/
1    ' -----'//)
831 FORMAT(' PARAMETER',4X,'MEAN',2(10X,'AMP',10X,'PAN'))
832 FORMAT(/,3X,A,3X,G12.5,(T26,8(G12.5,1X)))
C833 FORMAT(/,1X,A,F10.6)
900 FORMAT('1'/ ' -----'/

```


RUN # C1 ~~DAW~~

8/3/99

CALIEME.CON

1/1

: STATION NUMBER 261358 CALI

4 harmonics

093

VALOR MEDIO DE ALFA ANTES DE OPTIMIZAR = .213799

FINAL LOG-LIKELIHOOD VALUE=-F= 1649.58100

PARAMETER	MEAN	AMP	PAN	AMP	PAN
ALFA	.19191				
BETA	.14011E-01	.10685E-01	-.35809	.57319E-02	-1.4164
.28202E-02	2.0365	.18590E-02	-.54420E-01		
MEAN	.15435	.38497E-01	-2.3368	.16049E-01	.20036
.98617E-03	2.4613	.90649E-02	-3.1416		

Note: Akaike Information Criterion $AIC = -2 \log(\text{max likelihood}) + 2m$
 where $m = \text{number of parameters}$

For 26 periods, 3 parameters/period $m = 78$ $ML = 1691.31$ $\frac{AIC}{-3226.63}$
 For 1 per for α , 9 parameters each for $\beta + \mu$ $m = 19$ $ML = 1649.58$ -3261.14
 For 1 per for α , 5 parameters each for $\beta + \mu$ $m = 11$ $ML = 1648.98$ -3275.96 *

MIN. AIC is for 2 harmonics for $\beta + \mu$

For 1 per for α 7 parameters each for $\beta + \mu$ $m = 15$ $ML = 1649.55$ -3269.10

DMV 8/3/99

11

: STATION NUMBER 261358 CALIENTE 3 hammils

VALOR MEDIO DE ALFA ANTES DE OPTIMIZAR = .213799

~~DMV~~

094

FINAL LOG-LIKELIHOOD VALUE=-F= 1649.55900

PARAMETER	MEAN	AMP	PAN	AMP	PAN
ALFA	.18590				
BETA	.13123E-01 .22477E-02	.90114E-02 1.5933	-.42364	.66599E-02	-1.4855
MEAN	.21343 .11437E-02	.35974E-01 2.5127	-2.3082	.14024E-01	.22980

264436 LAS VEGAS WSO AIRPOR

Run # C8

Daw VEGASME.D4

Daw 8/4/99

VALOR MEDIO DE ALFA ANTES DE OPTIMIZAR = .328296

FINAL LOG-LIKELIHOOD VALUE=-F= 1127.32200 for 3 - min AIC (

1119.28 for 2 harmonics

095

PARAMETER	MEAN	AMP	PAN	AMP	PAN
ALFA	.28203				
BETA	.97436E-02 .47770E-02	.37570E-02 .25259	.80341	.65693E-02	1.0253
MEAN	.19160 .70230E-02	.16148E-01 -.54753	-1.9924	.18710E-01	2.4895

: STATION NUMBER 260046

RUN # C9

ADAV3ME.04

ADAV

DAW

8/14/49

VALOR MEDIO DE ALFA ANTES DE OPTIMIZAR = .317868

096

FINAL LOG-LIKELIHOOD VALUE=-F= 446.55910 * Min MIC
441.89 for 2 harmonics

PARAMETER	MEAN	AMP	PAN	AMP	PAN
ALFA	.26983				
BETA	.88066E-01 .64334E-01	.42300E-01 1.1824	-1.6823	.10282E-01	-2.1371
MEAN	.22935 .80856E-02	.63529E-01 -3.2667	-2.6941	.20371E-01	.37309

RUN C10
STATION NUMBER 260718 BEATTY8N BEAT 3 ME. 04

DAW 814/00

1/1

VALOR MEDIO DE ALFA ANTES DE OPTIMIZAR = .350336

DAW

097

FINAL LOG-LIKELIHOOD VALUE=-F= 631.07320

630.18 with 2 harmonics * min AIC

PARAMETER	MEAN	AMP	PAN	AMP	PAN
ALFA	.35344				
BETA	.36569E-01 .12038E-01	.16671E-01 -3.4876	-.58350	.14594E-01	2.5251
MEAN	.18434 .14274E-01	.21729E-01 .60635	2.9537	.24144E-01	1.7642

: STATION NUMBER 263285 GOLDFIELD

DAW *DAW 8/9/99*

VALOR MEDIO DE ALFA ANTES DE OPTIMIZAR = .355947

098

FINAL LOG-LIKELIHOOD VALUE=-F⇒ 614.06380 * MIN AIC
600.60 for 2 HARMONICS

PARAMETER	MEAN	AMP	PAN	AMP	PAN
ALFA	.40497				
BETA	.60929E-01 .18533E-01	.12924E-01 .62237	1.1661	.27927E-01	-.27251E-01
MEAN	.16520 .55931E-01	.40235E-01 -3.3626	-1.9533	.35153E-01	.63275

RUN # C.12 TONOPAH ME.04

: STATION NUMBER 268170 TONOPAH

DWD 8/4/99

0 099

VALOR MEDIO DE ALFA ANTES DE OPTIMIZAR = .322061

FINAL LOG-LIKELIHOOD VALUE=-F= 1709.63500

*1708.80 with 2 harmonics * Min AIC*

PARAMETER	MEAN	AMP	PAN	AMP	PAN
ALFA	.29153				
BETA	.17381E-01 .71435E-02	.71402E-02 -1.0172	-4.3429	.75322E-02	-2.1360
MEAN	.10451 .54533E-02	.30350E-01 -3.9021	-1.4535	.16841E-01	.42614

DAW

1/2

Linear Fitting Report

Data File Name: C:\consult\swri\CLIMATE\G00.PDW

100

Model Equation(s):
MEAN=B+A*ANPMM

Initial Parameters:

A= -0.0023351788
B= 3.04881925

Save Options:

Number of Function Calls: 9

Parameters After Fitting:

A= -0.0023351788
B= 3.04881925

SumSqr: 0.093218556
StdDev: 0.076329285

Covariance Matrix:

cvm[1,1]: 0.00003215360
cvm[2,1]: -0.0059494884
cvm[2,2]: 1.26752034

Goodness of Fit Statistics ...

___ C O D: 0.64530410
___ Corrl: 0.80330822
___ M S C: 0.36982782

Parameter Statistics...

Parameter: A= -0.0023351788

StdDev: 0.00086563740
Coeff. of Variance: -37.06942702

___ 95 % Confidence Interval

___ Uninvariant ...

LOW: -0.0047385734
HIGH: 0.00006821574

___ Supporting Plane ...

LOW: -0.0055611789
HIGH: 0.00089082125

Parameter: R= 3.04881925

StdDev: 0.17186944
Coeff. of Variance: 5.63724589

Daw

_95 % Confidence Interval

___ Uninvariant ...

LOW: 2.57163323
HIGH: 3.52600527

___ Supporting Plane ...

LOW: 2.40830763
HIGH: 3.68933087

=====
----Created by D. A. Woolhiser with ProStat
----Wed Aug 04 16:29:04 1999
=====

CI - no correlation
 $\Phi_1 - R^2 = .166 \quad R = .407 \quad \Phi_1 = -1.008 - 0.00224 \bar{P}$
C₂ - no correlation n.s.
 $\Phi_2 - R^2 = .386 \quad R = .621 \quad \Phi_2 = -1.21 + .001396 \bar{P}$
C₃ - n.s.
 $\Phi_3 - n.s.$
C₄ - R² = 0.598, R = .773, C₄ = 0.4518 - 0.000592 \bar{P}
 $\Phi_4 - R^2 = 0.214, R = 0.463 \quad \Phi_4 = -0.792 + 0.00106 \bar{P}$

DATA

41

=====
Column Information Report

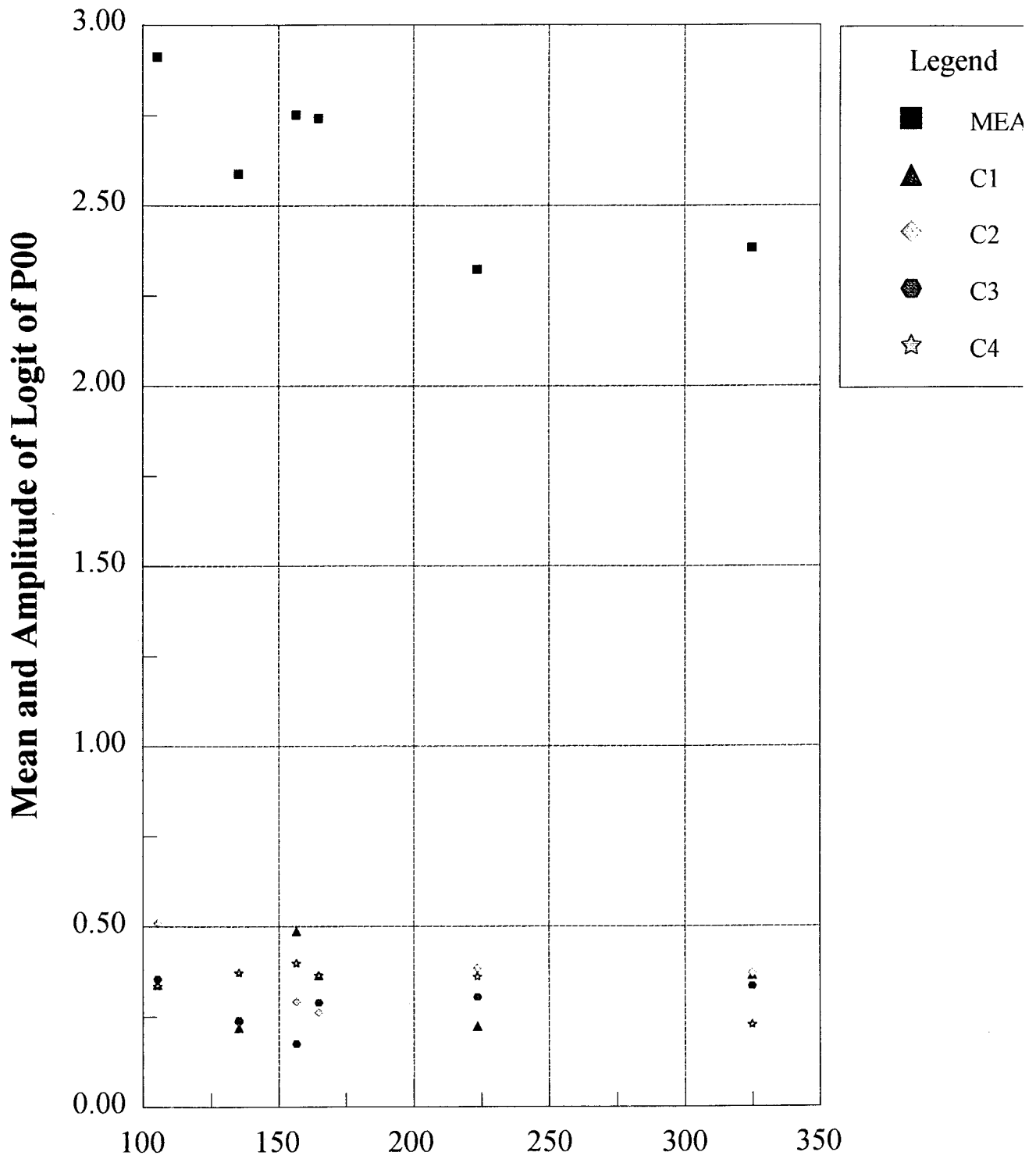
Data File Name: C:\consult\swri\CLIMATE\G00.PDW

102

=====
Current Sheet Name: C:\CONSULT\SWRI\CLIMATE\G00.PDW
Number of Columns: 11
Current Column Index: 2
Current Column Name: ANPMM *→ mean annual precip.*
Number of Points: 6
Current Column Type: Number
Maximum Value: 324.90000000
Minimum Value: 105.40000000
Sum of Column: 1110.20000000
Mean Value: 185.03333333
Number of Missing Points: 0

=====
----Created by D. A. Woolhiser with ProStat
----Wed Aug 04 16:13:20 1999
=====

DWS



Column Information Report

Data File Name: C:\CONSULT\SWRI\CLIMATE\ALBETA.PDW

```

Current Sheet Name:C:\CONSULT\SWRI\CLIMATE\ALBETA.PDW
Number of Columns:      3
Current Column Index:   3
Current Column Name:    ALPHA
Number of Points:       6
Current Column Type:    Number
Maximum Value:          0.40497000
Minimum Value:          0.18590000
Sum of Column:          1.78770000
Mean Value:             0.29795000
Number of Missing Points: 0

```

----Created by D. A. Woolhiser with ProStat
 ----Thu Aug 05 11:14:33 1999

These are from the α values obtained from runs C8-C12 and an unnumbered run for Caliente. All were run with 3 harmonics for β and μ .

The average of α , $\bar{\alpha} = 0.298$ will be used as a constant for repeat runs. The objective of the repeat runs is to see if by using a regional value for α , there will be a more clear cut relation between the Fourier coefficients for β and μ and mean annual precipitation.

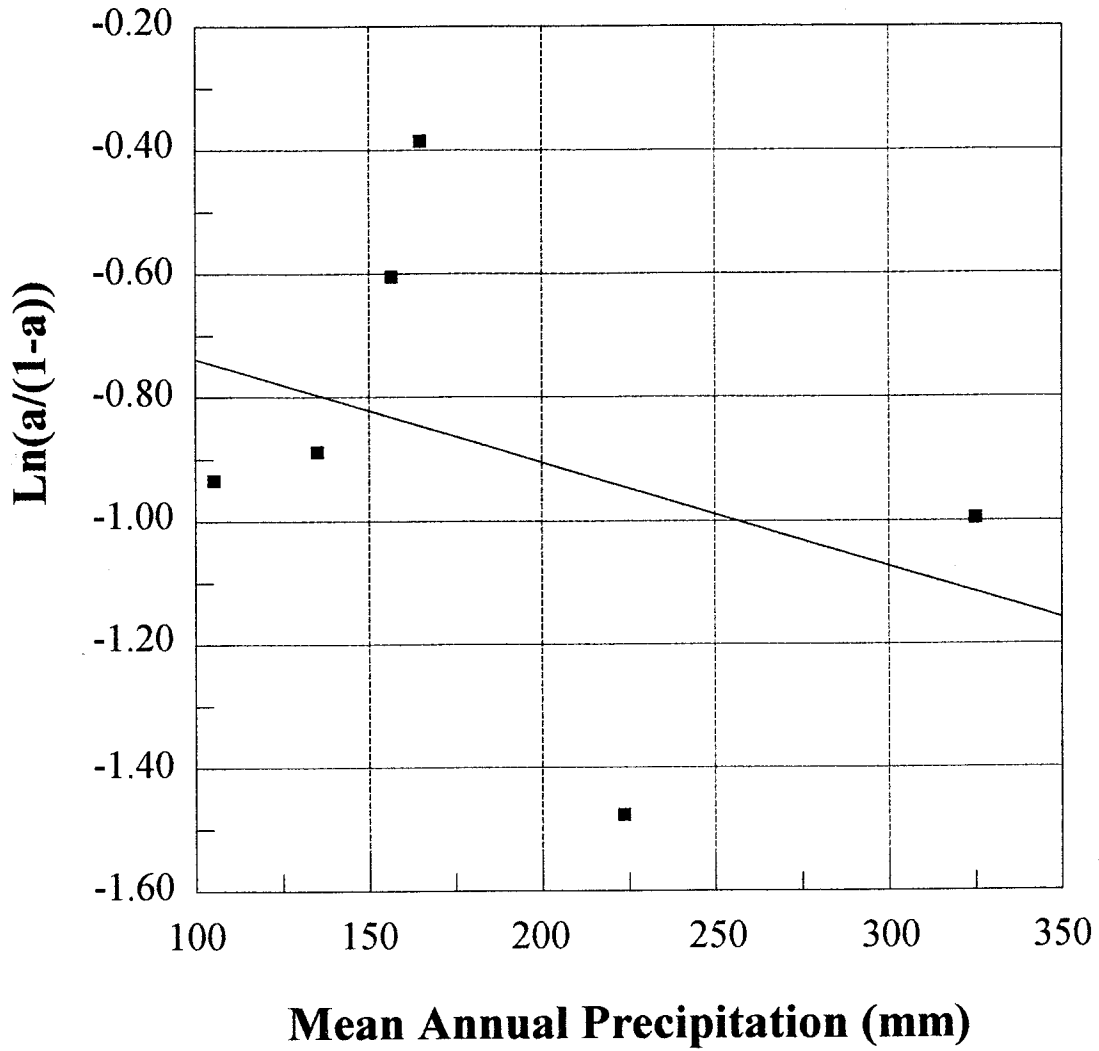
Note: There is a weak correlation between α and an. precip

$$\alpha = 0.3598 - 0.000345P \quad R^2 = 0.123 \quad R = 0.351$$

Scatter diagram: Alpha VS P, PGW

DAW

ALBETA.PDW



$$\ln\left(\frac{a}{1-a}\right) = -0.5695 + 0.00168 P \quad R=0.356 \quad R^2=0.127$$

CLIMATE \ Logit vs P. PGW DAW 8/6/99

Linear Fitting Report

Data File Name: C:\CONSULT\SWRI\CLIMATE\ALBETA.PDW

106

Model Equation(s):
LOGIT=B+A*ANPMM

Initial Parameters:

A= -0.0016809110
B= -0.56955707

Save Options:

Save Data

Number of Function Calls: 2

Parameters After Fitting:

A= -0.0016809110
B= -0.56955707

SumSqr: 0.60617079
StdDev: 0.19464243

Covariance Matrix:

cvm[1,1]: 0.00003215360
cvm[2,1]: -0.0059494884
cvm[2,2]: 1.26752034

Goodness of Fit Statistics ...

___ C O D: 0.12661127
___ Corrl: 0.35582477
___ M S C: -0.53129213

Parameter Statistics...

Parameter: A= -0.0016809110

StdDev: 0.0022074066
Coeff. of Variance: -131.32203794

___ 95 % Confidence Interval

___ Uninvariant ...

LOW: -0.0078096537
HIGH: 0.0044478317

___ Supporting Plane ...

LOW: -0.0099073274
HIGH: 0.0065455054

Parameter: B= -0.56955707

DW

StdDev: 0.43827326
Coeff. of Variance: -76.94984139

107

_95 % Confidence Interval

___ Uninvariant ...

LOW: -1.78639862
HIGH: 0.64728449

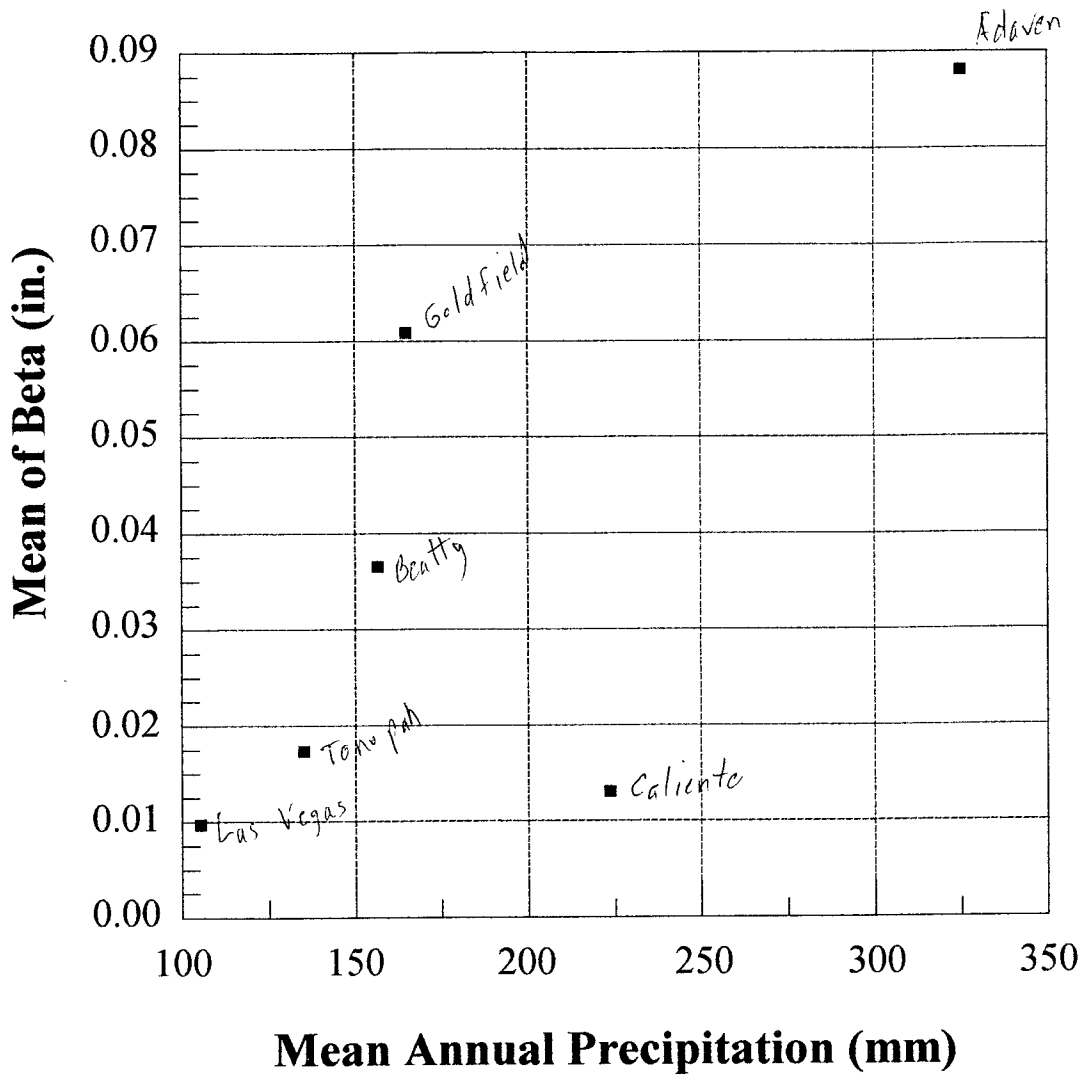
___ Supporting Plane ...

LOW: -2.20288478
HIGH: 1.06377065

=====
----Created by D. A. Woolhiser with ProStat
----Fri Aug 06 11:21:25 1999
=====

DAW

ALBETA.PDW



$$\bar{\beta} = -0.00823 + 0.1538 \alpha \quad R^2 = 0.137$$

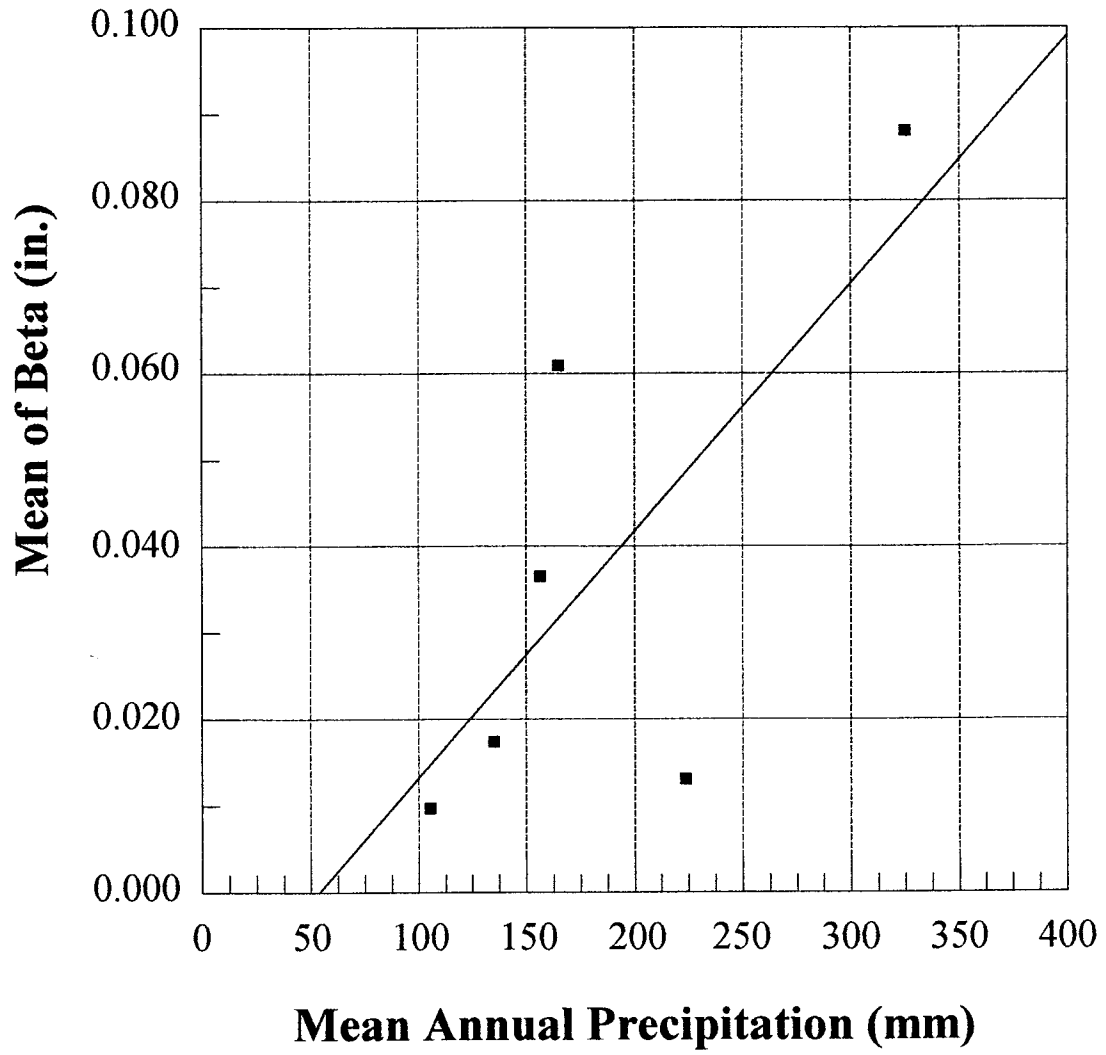
$$\bar{\beta} = -0.01534 + 0.000286 \bar{p} \quad R^2 = 0.521 \quad R = 0.723$$

\bar{p} in mm.

Large variation in amplitudes and phase $\angle s$

DAW 8/6/99

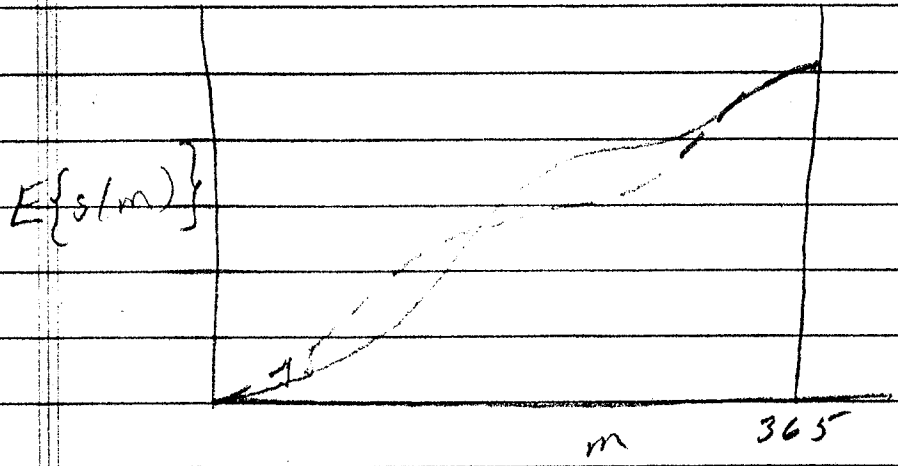
ALBETA.PDW



DWS

$$E\{s(m)\} = \sum_{n=1}^{365} [P\{X(n-1)=0\} \rho_{01}(n) + P\{X(n-1)=1\} \rho_{11}(n)]$$

$$\underbrace{\alpha(n)\beta(n) + [1-\alpha(n)]\delta(n)}_{\mu(n)} + T$$



Suppose that the seasonality changes as indicated by the dotted line, but the annual mean precip. doesn't change. Let this series be $E'\{s(m)\}$

We wish to minimize $\sum_{m=1}^{365} (E\{s(m)\} - E'\{s(m)\})^2 = F$

under the constraint that $E\{s(365)\} = E'\{s(365)\}$
 changes can be made in phase ϕ and amplitude of G_{00}, G_{10}, \dots

First assume that $\bar{G}_{00}, \bar{G}_{10}$ and $\bar{\mu}$ do not change

Parameters that could change:

- $C_{100}, \phi_{100}, C_{200}, \phi_{200}, C_{300}, \phi_{300}, C_{400}, \phi_{400}$
- $C_{110}, \phi_{110}, C_{210}, \phi_{210}, C_{310}, \phi_{310}$
- $C_{120}, \phi_{120}, C_{220}, \phi_{220}, C_{320}, \phi_{320}$

DMS

This brings up an interesting question. Is there a correlation between phase angles and amplitudes of $G_{00} + G_{10}$ and μ ?

$$dF = \frac{\partial F}{\partial G_{100}} \Delta G_{100} + \frac{\partial F}{\partial \phi_{100}} \Delta \phi_{100} + \dots + \frac{\partial F}{\partial G_{\mu 1}} \Delta G_{\mu 1} + \frac{\partial F}{\partial \phi_{\mu 1}} \Delta \phi_{\mu 1}$$

$$\frac{\partial F}{\partial G_{100}} = 0$$

$$\frac{\partial F}{\partial \phi_{100}} = 0$$

$$|$$

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TABLE OF COMPUTER RUNS FOR FUTURE CLIMATE STUDIES

Run # & Date	Program	CON File	Input File	Output Files	No. Of Harmonics	Comments
C1 8/3/99	MELSIREV	CALLENME	CALIENTE.PTT		4	2 HARMONICS gave lower AIC
C2 8/3/99	MCFOIR	TONOPAH	TONOPAH.PTT	TONOPAH.OUT	4	
C3 8/4/99	"	CALLENMC	CALIENTE	CALLEN4.OUT	4	N=40, 1929-68
C4 "	"	ADAVENMC	ADAVENI	ADAVEN4.OUT	4	N=70, N=32, 1930
C5 "	"	BEATNMC	BEATTY8N	BEAT8N4.OUT	4	N=24, 1973
C6 "	"	GOLD4MC	GOLDFIEL	GOLD4.OUT	4	N=28, 1949
C7 "	MCFOIR	VEGAS4MC	VEGAS	VEGAS4.OUT	4	N=57, 1937
C8 "	MELSIREV	VEGAS3ME	VEGAS	VEGAS4, 04, 05, 06	3	N=32, 1937
C9 "	"	ADAV3ME	ADAVENI	ADAV3ME, 04, 05, 06	3	N=32, 1930
C10 "	"	BEAT3ME	BEATTY8N	BEAT3ME, 04, 05, 06	3	N=24, 1973
C11 "	"	GOLD3ME	GOLDFIEL	GOLD3ME, 04, 05, 06	3	N=28, 1949
C12 "	"	TONO3ME	TONOPAH	TONO3ME, 04, 05, 06	3	N=42, 1955
C13 8/6/99	MELSIREV	ADA3MEA	ADAVENI	ADA3MEA, 01, 02, 03	3	$\alpha = 0.298$ } computer program error
C14 "	"	BEA3MEA	BEATTY8N	BEA3MEA, 01, 02, 03	3	$\alpha = 0.298$ } constant α as input doesn't work
C15 1/12/00	MIXEX 2000	CAL3MEA	CALIENTE	CAL3MEA, 01, 02, 03	$\beta = 2$, $\mu = 3$	CAL 5000 MEAS MCP DOW 4/2/04
C16 1/19/00	"	GOLD3MEA	GOLDFIEL	GOLD3MEA, 01, 02, 03	$\beta = 2$, $\mu = 3$	GOLD 5000 MCP 171273
C17 "	"	TONO3MEA	TONOPAH	TONO3MEA, 01, 02, 03	$\beta = 2$, $\mu = 3$	13 per. L=1753.33, 4698664 1500 eval.
C18 "	"	VEG3MEA	VEGAS	VEG3MEA, 01, 02, 03	$\beta = 2$, $\mu = 3$	13 per. L=114.87, 117.51, 24 p 1179.8
C19 "	"	BEA3MEA	BEATTY8N	BEA3MEA, 01, 02, 03	$\beta = 2$, $\mu = 3$	13 per. L=665.03, 618739, 620.781
C20 1/19/00	MIXEX 2000	BEACALC80	CALIENTE	CAL3MEA, 01, 02, 03	$\beta = 2$, $\mu = 3$	13 per. L=1441.54 GETH MEAS MCP
C21 1/19/00	"	ADAC21	ADAVENI	ADAC21, 01, 02, 03	$\beta = 2$, $\mu = 3$	13 per. 483.787, 430.618, 436.098
C16 1/21/00	"	GOLC16	GOLDFIEL	GOLC16, 01, 02, 03	$\beta = 2$, $\mu = 3$	648.09, 603.09, 613.81

DOW 4/2/04

DOW 4/2/04
DOW

The program WGENPAR.FOR can be used for the analysis
Procedure: ~~Dow~~

1. Write a BASIC program to convert *.TXT files to
input file for WGENPAR ie

t_{max} t_{min} N $precip$ N $rad.$

IMO IDA IYR V1 V2 V3 V4
 I2 I2 I2 FG.1 FG.1 FG.2 CX FG.2

114

Note: Code for missing data is 99.99

WGENPAR assumes that data starts on Jan 1 and ends Dec 31

Program Name is DAYREADT.BAS modified from DAYREAD.BAS
output file extension is ~~TAR~~ ^{TPR} (Temperature ^{Precipitation} and Radiation)

Dow 4/1/04

Dow 4/2/04

6/3/99

Run WGENPAR2 with BEATTY~1.TPR as input

output file 1 = " .FIL
" 2 = " .DAT

Did not run. Got message "DOSXMSF.EXE must be in path."

sent e-mail to C. Richardson asking for suggestions.

Set up input file for WGENPAR2

BEATTY8N:

1. Copy BEATTY8N.TXT to BEATTY8N.IN
2. Edit .IN to begin at 1/1 and end at 12/31
starts at 1974 ends 12/31/97 84 missing
97-74 = 23 yrs.
3. RUN DAYREADT.BAS - Get BEATTY8N.TPR ←

Got message that DOSXMSF.EXE required to run program.
sent e-mail to C. Richardson. He attached that file. Downloaded
to Climate

6/4/99 Run BEATTY8N.TPR run successful
output BEATTY23.FIL
" " .DAT

CALIENTE

Daw

1. Copy CALIENTE.TXT to CALIENTE.IN
2. Edit to begin Jan 1 and end Dec. 31 ✓
3. Run DAYREADT.BAS - Get CALIENT.TPR ✓
 $20,083 - 9 = 20,074 = 55 \text{ yrs. took off } 2 \text{ yrs}$
4. Run WGENPAR2 run with 55 yrs.

115

1937

No. 5505
Engineer's Computation Pad

CALIENTE.TPR
 CALIENTE.FIL ✓
 CALIENTE.DAT

TONOPAH

1. Copy TONOPAH.TVT to TONOPAH.INE ✓
2. Edit $14973 - 9 = 14964 \div 365 = 41 \text{ yrs}$ ✓
3. Run DAYREADT.BAS GET TONOPAH.TPR ✓
4. Run WGENPAR2 40 yrs. ✓
 TONOPAH.FIL ✓
 " .DAT

ADAVEN^{~1}

1. Copy ADAVEN^{~1}.TXT TO ADAVEN.INE ✓
2. Edit $11323 - 9 + 1 = 11315 = 31 \text{ yrs}$ ✓
3. Run DAYREADT.BAS ✓
4. Run WGENPAR2 30 yrs ✓ GET ADAVEN.TPR
 ADAVEN.FIL
 " .DAT

LAS VEGAS 37-

1. Copy VEGAS.TXT to VEGAS.INE ✓
2. Edit ✓ $20448 - 9 + 1 = 20440 \div 365 = 56 \text{ yrs.}$ ✓
3. Run DAYREADT.BAS ✓ GET VEGAS.TPR
4. Run WGENPAR2 35 yrs
 VEGAS.FIL
 " .DAT

Create a spreadsheet file (PSI PLOT) with temperature statistics.

FILE NAME: TEMPSTAT.PDW ~~DWA~~

Column Statistics: TEMPCOLSTAT.TXT

116

Column Headings:

- 1 STATION
- 2 Ann P - Av. annual precip. from record analysed
- 3 TXMD - Mean of T_{max} for dry days
- 4 ATX - Amplitude " " " "
- 5 CVTZ - Coefficient of variation of T_{max} for wet + dry days (unadjusted)
- 6 CVTX - " " " " (adjusted)
- 7 ACVTZ - amplitude of CV of T_{max} w+d (unadjusted)
- 8 ACVTX - amplitude of coef. of variation of T_{max} w+d (adjusted)
- 9 TXMW - mean of T_{max} for wet days
- 10 TN - mean of T_{min} for wet or dry days
- 11 ATN - amplitude of T_{min} for wet or dry days
- 12 CVTNZ - coefficient of variation of T_{min} for wet or dry days (unadjusted)
- 13 CVTN - " " " " (adjusted)
- 14 ACVTNZ - Amplitude of the coefficient of variation of T_{min} w+d (unadjusted)
- 15 ACVTN - " " " " (adjusted)

$$CVTX = \frac{CVTZ * TXMD}{(100 + TXMD)}$$

$$ACVTX = \frac{ACVTZ * TXMD}{(100 + TXMD)}$$

$$CVTN = \frac{CVTNZ * TN}{(100 + TN)}$$

$$ACVTN = \frac{ACVTNZ * TN}{(100 + TN)}$$

7/8/99

Exploratory statistics

1. Relation between mean annual rainfall and elevation + Latitude

Elev. is highly correlated with latitude

$$E = -66241.8 + 1892 * L$$

$$R^2 = 0.917$$

So a multiple regression; $P = a + b_1 E + b_2 L$ would give spurious results.

$$P = 1.365 + 0.00129 E$$

$$R^2 = 0.41$$

GOLDFIELD

-1997

DWW

1. COPY GOLDFIEL.TXT to GOLDFIEL.INE ✓
2. Edit. ✓ $9843 - 8 = 9855 \div 365 = 27$ yrs ✓
3. RUN DAYREADT.BAS. Get GOLDFIEL.TPR ✓
4. RUN WGENPAR2. 27 yrs ✓

117

GOLDFIEL.FIL ✓
" " ,DAT

6/7/99 Adjustment of Coefficients of variation means
and amplitudes. DWW 4/2/04

CVTX = ~~coeff.~~ mean of CV of T_{max} for wet or dry days

ACVTX = amplitude of CV of T_{max} " " "

CVTN = mean of CV of T_{min} for wet or dry days

ACVTN = amplitude of CV " " " "

Hanson, et al. (1994) corrected a problem with WGEN by adding $100^{\circ}F$ to all daily maximum and minimum temperature values. The coefficients of variation were adjusted to reflect this transformation

Adjustment of CVs

let x = a random variable with mean \bar{x} , $var = s^2$

let $z = x + 100$

The coefficient of variation $CV_x = s/\bar{x}$ what is CV_z

$$Var\{z\} = Var\{x + 100\} = Var\{x\}$$

$$\bar{z} = 100 + E\{x\} = 100 + \bar{x}$$

$$CV_z = \frac{\sqrt{Var\{z\}}}{\bar{z}} = \frac{\sqrt{Var\{x\}}}{100 + \bar{x}} = \frac{s_x}{100 + \bar{x}}$$

$$(100 + \bar{x}) CV_z = s_x$$

$$s_x = \bar{x} CV_x$$

$$(100 + \bar{x}) CV_z = \bar{x} CV_x$$

$$CV_z = \frac{CV_x \bar{x}}{(100 + \bar{x})}$$

 CV_z

2. Are there any relationships between Temperature model parameters and elevation.

DAW

~~TXMD = 78.44 - 0.00419 E R² = 0.358~~ } DAW 4/4/04 118

~~TXMD = 87.46 - 0.00374 E R² = 0.98~~ DAW 4/2/04

TXMD = 87.46 - 0.00374 E R² = .98 O.K.

This makes sense 3.74°/1000 ft

Try TN vs Elew

TN = 59.62 - 0.004084 E R² = 0.82 O.K.

6/9/99 4.084°/1000 ft

TEMP COL STAS, TX1
Try TXMW vs Elew.

TXMW = 77.756 - 0.003408 E R² = 0.965 O.K.

MSC: = 2.69 3.408°/1000 ft

CVTX

CVTX = 0.10645 - 0.00000884 E R² = 0.474

ACVTX

ACVTX = -0.01933 - 0.000001906 E R² = 0.272

ATN

ATN = 20.003 - 0.0004374 E R² = 0.202

CVTN R² = 0.003

ACVTN R² = 0.049

Normal Lapse Rate = 3.6° F / 1000 ft Trewartha p 28
vertical temp. gradient is ~ 1,000 x the rate of temp change due to latitude.

? Are the gradients from the analysis significantly different from the average normal lapse rate? DAW 4/2/04

Dry adiabatic lapse rate = 5.54° F / 1000 ft p 126 Trewartha
Retarded or wet adiabatic rate { at low temperatures ~ to dry adiabatic
at high temperatures ~ 1/2 dry adiabatic



TEMP COL STAS, TX1

DAW

120

```

'PROGRAM PDISPLAY.BAS by DAW 10/28/99
'This program creates a file of daily values of Markov chain
'parameters, 'Poo, P1o, and mixed exponential parameters, alpha,
'beta and mu. It also computes the expected accumulated
'precipitation.
' Input consists of the mean, amplitudes and phase angles of the
'finite Fourier series of the logits of Poo and P1o and also the
'Fourier series of alpha, beta and mu of the mixed exponential
'distribution of daily precipitation.
'*****
'GOOPAR(I)=Fourier coefficients of G00 (mean, amplitudes & phase angles)
'G1OPAR(I)=Fourier coefficients of G10
'ALPHAPAR(I)=Fourier coefficients of ALPHA
'BETAPAR(I)= Fourier coefficients of BETA
'MUPAR(I)= Fourier coefficients of MU
'G00(I)=logit of dry-dry transition probability. Goo=log(p/1-p)
'G10(I)=logit of wet-dry transition probability.
'ALPHA(I)=daily weighting factor in mixed exponential distribution
'P00(I)=Probability that day I was dry given day I-1 was dry
'P10(I)=Probability that day I was dry given that day I-1 was wet.
'BETA(I)=daily mean of the smallest exponential distribution, mm.
'MU(I)=daily mean of the mixed exponential distribution, mm.
'THETA(I)= mean of the largest of the mixed exponential
'T= Threshold subtracted from precipitation depth to enable a mixed
'exponential fit in interval 0 to infinity. 0.008 inches
'PWET= unconditional probability of a wet day
'SUM(I)=Expected total precipitation including day I. See Hanson
'et al. "Microcomputer Program for Daily Weather Simulation in the
'Contiguous United States" ARS - 114, 1994.

```

```

OPTION BASE 1
DIM G00(365), G10(365), ALPHA(365), BETA(365), MU(365)
DIM GOOPAR(10), G1OPAR(10), ALPHAPAR(9), BETAPAR(9), MUPAR(9)
T = .008
INPUT "ENTER INPUT FILE NAME, EXTENSION WILL BE .ME ", INFILE$
OPEN INFILE$ FOR INPUT AS #1
'Create name for output file. Name will be the same except the
'extension will be .DAT.
N% = LEN(INFILE$) - 3
OUTFILE$ = LEFT$(INFILE$, N%) + "DAT"
OPEN OUTFILE$ FOR OUTPUT AS #2
'Read parameters for Markov chain. The format is set up so that
'parameter values can be created easily from output files of MCFOUR
'and MIXEX
'Mean and amplitudes
INPUT #1, GOOPAR(1), GOOPAR(2), GOOPAR(3), GOOPAR(4), GOOPAR(5)
'Phase angles (6) will always be zero
INPUT #1, GOOPAR(6), GOOPAR(7), GOOPAR(8), GOOPAR(9), GOOPAR(10)
INPUT #1, G1OPAR(1), G1OPAR(2), G1OPAR(3), G1OPAR(4), G1OPAR(5)
INPUT #1, G1OPAR(6), G1OPAR(7), G1OPAR(8), G1OPAR(9), G1OPAR(10)

'Read parameters for mixed exponential
'mean, 1st amplitude, 1st phase angle, 2nd amplitude, 2nd phase angle, e
INPUT #1, ALPHAPAR(1), ALPHAPAR(2), ALPHAPAR(3), ALPHAPAR(4), ALPHAPAR(5)
INPUT #1, BETAPAR(1), BETAPAR(2), BETAPAR(3), BETAPAR(4), BETAPAR(5), BE
INPUT #1, MUPAR(1), MUPAR(2), MUPAR(3), MUPAR(4), MUPAR(5), MUPAR(6), MU

'Calculate Fourier series for each day
'Markov chain
FOR I = 1 TO 365

```

```

G00(I) = 0, G10(I) = 0
FOR J = 1 TO 4
  G00(I) = G00(I) + G00PAR(J + 1) * SIN(.017214 * J * I + G00PAR(J + 6))
  G10(I) = G10(I) + G10PAR(J + 1) * SIN(.017214 * J * I + G10PAR(J + 6))
NEXT J

```

~~Daw~~

```

G00(I) = G00(I) + G00PAR(1) ' Add mean
G10(I) = G10(I) + G10PAR(1)
' Transform to probabilities
P00(I) = EXP(G00(I)) / (1! + EXP(G00(I)))
P10(I) = EXP(G10(I)) / (1! + EXP(G10(I)))

```

(121

```

NEXT I
' Mixed exponential
FOR I = 1 TO 365
  FOR J = 1 TO 9
    ALPHA(I) = ALPHAPAR(J + 1) * SIN(.017217 * J * I + ALPHAPAR(J + 2))
    BETA(I) = BETAPAR(J + 1) * SIN(.017217 * J * I + BETAPAR(J + 2))
    MU(I) = MUPAR(J + 1) * SIN(.017217 * J * I + MUPAR(J + 2))
  NEXT J
  ALPHA(I) = ALPHA(I) + ALPHAPAR(1) ' Add means
  BETA(I) = BETA(I) + BETAPAR(1)
  MU(I) = MU(I) + MUPAR(1)
  ' Compute theta
  THETA(I) = (MU(I) - ALPHA(I) * BETA(I)) / (1! - ALPHA(I))

```

Daw 4/2/04
 $\alpha(I) = 0, \beta(I) = 0, \mu(I) = 0$
 $\alpha(I) = \alpha(I) + \alpha(I)$
 $\beta(I) = \beta(I) + \beta(I)$
 $\mu(I) = \mu(I) + \mu(I)$
K
1/muse

```

NEXT I
' Compute expected sum of precipitation on day I
' Approximate probability of a wet day 365
PSTART = (1! - P00(365)) / (1! + P10(365) - P00(365))
PWET = PSTART
PDRY = 1! - PSTART
SUM(1) = (PDRY * P01(1) + PWET * (1! - P10(1))) * (MU(1) + T)
PWET = (PDRY * P01(1) + PWET * (1! - P10(1)))
FOR I = 2 TO 365
  PWET = (1 - PWET) * (P01(I) + PWET * (1 - P10(I)))
  SUM(I) = SUM(I - 1) + PWET * (MU(I) + T)
NEXT I

```

```

' Print to file
FOR I = 1 TO 365
  PRINT #2, USING "### #.### #.### #.### #.### ##.### ####.#"
NEXT I
CLOSE #1
CLOSE #2
END

```

*J=1 ALPHA(I) = AMP(I) * sin(...) + phi(I)*
J=3 ALPHA(I) + AMP(phi)
J=5
J=7

J+1

8

9

DAW

```
'PROGRAM DAYREADT.BAS By DAW 6/2/99
'This program will read a line from the National Weather Service
'daily data format and will write the month, day, year, daily rainfall
 amount in inches,'the maximum daily temperature and the minimum daily temperatu
e degrees F to a file in a format readable by WGENPAR.FOR. Missing data will
'be coded as 99.99. Output format will be
' in the FORTRAN form 3I2, 2F6.1, F6.2, 6x, F6.2
,
```

122

```
OPTION BASE 1
  INPUT "ENTER INPUT FILE NAME", INFILE$
  OPEN INFILE$ FOR INPUT AS #1
'Create output file name
  N% = LEN(INFILE$) - 3
  OUTFILE$ = LEFT$(INFILE$, N%) + "TPAR" 'Add extension TPAR to infile
  name.
  OPEN OUTFILE$ FOR OUTPUT AS #2

  Read heading information
  INPUT #1, A$
  PRINT #2, A$ ' Print title
  FOR I% = 1 TO 8
    INPUT #1, A$
    PRINT , A$
  NEXT I%
  INPUT "ENTER STATION LATITUDE IN DEGREES", ALAT
  KSD = 1

  PRINT #2, USING "          #####.      #####"; ALAT; KSD
  RAD = 99.99
  DO WHILE NOT EOF(1) ' Begin reading loop
    INPUT #1, A$
    PRINT , A$
    YR$ = MID$(A$, 3, 2) ' Read last 2 digits of year
    MO$ = MID$(A$, 5, 2) ' Read month

    DAY$ = MID$(A$, 7, 2) 'Read day
    MODAYR$ = MO$ + DAY$ + YR$
    DATE = VAL(MODAYR$)
    PRECIP$ = MID$(A$, 12, 4)
    P = VAL(PRECIP$) / 100! 'Convert string to decimal inches
    PCODE$ = MID$(A$, 16, 1) ' Measurement flag
    IF PCODE$ = "M" THEN P = 99.99 ' Missing data
    TMAX$ = MID$(A$, 34, 3)
    TMAX = VAL(TMAX$)
    TMAXCOD$ = MID$(A$, 38, 1) ' Measurement flag
    IF TMAXCOD$ = "M" THEN TMAX = 99.99

    TMIN$ = MID$(A$, 41, 3)
    TMIN = VAL(TMIN$)
    TMINCOD$ = MID$(A$, 44, 1)
    IF TMINCOD$ = "M" THEN TMIN = 99.99
  PRINT #2, USING "##### ##.# ##.# ##.##      ##.##"; DATE; TMAX; TMIN; P;

  LOOP

  CLOSE #1
  CLOSE #2

  END
```

Times used
AD

C:\consult\swr\CLIMATE\TEMPSTAT.PDW

Station	Annual P	TXMD	ATX	CVTZ	CVTX	ACVTZ	ACVTX	TXMW
Adaven	12.79	64.483	21.938	0.157		-0.099	7/2/04	66.55.748
Beatty8n	0.16	75.945	20.812	0.109		-0.049		66.735
Caliente	8.80	70.764	23.584	0.179		-0.056		64.023
Goldfield	6.49	65.148	22.167	0.139		-0.072		58.015
Las Vegas	4.15	78.743	23.906	0.236		-0.067		69.171
Tonopah	5.37	67.348	22.887	0.135		-0.068		59.193

Daw

Worksheet
Daw 7/7/99

C:\consult\swri\CLIMATE\TEMPSTAT.PDW

MISS
 2.13
 0.33
 2.53
 4.32
 0
 0.02

NW
 44.75
 37.47
 48.97
 31.36
 25.83
 36.81

Adavon
 Beatty
 Caliente
 Goldfield
 Las Vegas
 Tonopah

TN	ATN	CVTNZ	CVTN	ACVTNZ	ACVTN	Column16
35.54	16.578	0.300		-1.241		1.0000
43.847	16.055	0.174		-1.064		
36.888	18.568	0.358		-1.275		
39.067	18.373	0.225		-1.136		
53.611	20.176	0.221		-1.138		
36.552	18.248	0.221		-1.153		1.0000

TXMD = 72.61 + 0.412 LAT - 0.00382 ELEV

Dave

C:\CONSULT\ISWR\CLIMATE\TEMPSTAT.PDW

Station	Annual P*	TXMD	ATX	CVTZ	CVTX	ACVTZ	ACVTX	TKMW
Adaven	12.7900	64.4830	21.9380	0.1570	0.0615	-0.0990	-0.0388	55.743
Beatty8n	6.1600	75.4450	20.8120	0.1090	0.0469	-0.0490	-0.0211	66.735
Caliente	8.8000	70.7640	23.5840	0.1790	0.0742	-0.0560	-0.0232	64.023
Goldfield	6.4900	65.1480	22.1670	0.1390	0.0548	-0.0720	-0.0284	58.015
Las Vegas	4.1500	78.7430	23.2060	0.2360	0.1040	-0.0670	-0.0295	69.171
Tonopah	5.3200	67.3480	22.8870	0.1350	0.0543	-0.0680	-0.0274	59.193

Mean 70.32 22.43 0.06595 -0.02806 62.15

std dev 5.78 1.01 0.0207 0.00617 5.305

CV 0.082 0.0456 0.3139 0.2199 0.0854

R² reg. w/dec. 0.98 N5 R² 6.424 0.223 0.965

* Annual P is from these data files. French shows different values.
 * French (1953) Probably due to different periods of record.

Daw

Daw 7/8/99

C:\CONSULT\SWR\CLIMATE\TEMPSTAT.PDW

TN	ATN	CVTNZ	CVTN	ACVTNZ	ACVTN	Latitude	Elevation	Wet Days	Av
35.5400	16.5780	0.3000	0.0787	-0.2410	-0.0632	38.1170	6250.0000	44.7500	
43.8470	16.0550	0.1740	0.0530	-0.0640	-0.0195	37.0000	3550.0000	32.6700	
36.8880	18.5680	0.3580	0.0965	-0.2750	-0.0741	37.6170	4400.0000	48.9700	
39.0670	18.3730	0.2250	0.0632	-0.1360	-0.0382	34.7000	5690.0000	31.3600	
53.6110	20.1760	0.2210	0.0771	-0.1380	-0.0482	36.0800	2160.0000	25.8300	
36.5520	18.2480	0.2210	0.0592	-0.1530	-0.0410	38.0670	5430.0000	36.8100	

Mean 40.92 18.00 0.0713 -0.0474
 Std. dev 6.89 1.49 0.0159 0.1932 37.7
 CV 0.168 0.0828 0.223 0.4076
 R² 0.82 0.202 0.003 0.049

Daw

C:\CONSULT\SWR\CLIMATE\TEMPSTAT.PDW

Av. Miss.
2.1300
0.3300
2.5300
4.3200
0.0000
0.0200

DAW

DAW

1/8

\$?debug

128

```
PROGRAM WGENPAR.FOR Revised 6/97 GSM
c revised 11/97 - added prompt to screen for file names and number
c of years running - gsm
C *****
C *
C * DEE ALLEN WRIGHT *
C * COMPUTER PROGRAMMER *
C * FEBRUARY 25, 1983 *
C *
C *****
CHARACTER*80 FNAME,FPRN,fdata,fprn2
DIMENSION TMAX(105,365),TMIN(105,365),RAIN(105,365),RAD(105,365)
C DIMENSION AA(20)
character*80 TITLE
DIMENSION RC(365)
DIMENSION XDATA(30),YDATA(4,12)
DATA KR1,KW,kw1/2,6,7/
c change per cwr 11/5/97 gsm
c to prompt for file names
WRITE(*,5002)
5002 FORMAT(1X,'Enter the Input Weather file Name (e.g temple.wth)')
READ(*,11)fdata
11 FORMAT(a80)
WRITE(*,5003)
5003 FORMAT(1X,'Enter the Output file Name (e.g temp15.fil)the 15 repre
1sents the number of Years running')
READ(*,12)fprn
12 FORMAT(a80)
WRITE(*,5004)
5004 FORMAT(1X,'Enter the Output file Name which is the input for wgenp
lar2(e.g temp15.dat)')
READ(*,13)fprn2
13 FORMAT(a80)
fname = fdata
OPEN(KR1,FILE=FDATA,STATUS='OLD')
OPEN(KW,FILE=FPRN,STATUS='UNKNOWN')
OPEN(KW1,FILE=FPRN2,STATUS='UNKNOWN')
WRITE(*,*) ' Weather data set :',FDATA(1:58)
WRITE(*,*) ' Output :',FPRN(1:58)
WRITE(*,*) ' Output that is Input for wgenpc2 :',FPRN2(1:58)
c change per cwr 11/5/97 gsm
c to prompt for number of years
WRITE(*,5001)
5001 FORMAT(1X,'ENTER THE NUMBER OF YEARS (e.g 15)')
READ(*,10)nyrs
10 FORMAT(I10)

DO 1 I=1,30
XDATA(I)=0.0
1 CONTINUE
DO 2 I=1,4
DO 2 J=1,12
YDATA(I,J)=0.0
2 CONTINUE
C*****
C
```

input file
output file

initial

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```

C-----INPUT #1  TITLE OF DATA SET (20A4)
C
C*****
  READ(KR1,100)TITLE
c   READ(kr1,100)(AA(I),I=1,20)
100  FORMAT(A)
c   WRITE(kw,101) (AA(I),I=1,20)
  WRITE(kw,101) TITLE
101  FORMAT('1',///,'DATA IS -----',A,/)
  WRITE(kw1,1001) fName
1001  FORMAT(' Generation Parameters for ',a80)

```

```

C*****
C-----INPUT #2  NUMBER OF YEARS, LATITUDE, AND SOLAR RADIATION STATUS
C               (IF NO SOLAR RADIATION DATA, KSD = 1)
C*****
change per cwr 11/5/97 gsm
c to prompt to screen for Number of years
c   READ(kr1,102) NYRS,ALAT,KSD
c102  FORMAT(I10,F10.0,I10)
  READ(kr1,102) ALAT,KSD
102  FORMAT(10x,F10.0,I10)
  kgen=1
  write(kw1,1002)nyrs,kgen,alat
1002  format(2i5,f5.1)
  XYRS=NYRS
  XLAT=ALAT*6.2832/360.
  DO 6 I = 1,365
  XI = I
  SD = 0.4102*SIN(0.0172*(XI-80.25))
  CH = -TAN(XLAT)*TAN(SD)
  IF (CH .GT. 1.0) H = 0.
  IF (CH .GT. 1.0) GO TO 5
  IF(CH .LT. -1.0) H = 3.1416
  IF(CH .LT. -1.0) GO TO 5
c   H = ARCOS(CH)
  H = ACOS(CH)
5   DD=1.0+0.0335*SIN(0.0172 *(XI+88.2))
  RC(I)=889.2305*DD*((H*SIN(XLAT)*SIN(SD))+(COS(XLAT)*COS(SD)*SIN(H)
*)
  RC(I)=RC(I)*0.80
-6  CONTINUE
  v1m1 = 70.
  v2m1 = 40.
  v4m1 = 450.
  DO 7 I = 1,NYRS
  DO 7 J = 1,365

```

```

C*****
C----- INPUT #3  DAY, MO, YEAR, RADIATION, MAX TEMP, MIN TEMP, RAINFALL
C
C*****
8   READ(kr1,103) IMO,IDA,IYR,V1,V2,V3,V4
  IF(IMO .EQ. 2 .AND. IDA .EQ. 29) GO TO 8
  if(v1.eq.99.99) v1 = v1m1
  if(v2.eq.99.99) v2 = v2m1
  if(v3.eq.99.99) v3 = 0.0
  if(v4.eq.99.99) v4 = v4m1
  v1m1 = v1

```

```

v2m1 = v2
v4m1 = v4
TMAX(I,J) = V1
TMIN(I,J) = V2
RAIN(I,J) = V3
RAD(I,J) = V4
IF(RAD(I,J) .GT. RC(J)) RAD(I,J)=RC(J) -
CONTINUE

```

input
DATA
input

```

7
103 format(3i2,2f6.1,f6.2,6x,f6.2)
C 103 FORMAT(10X,4F10.2)
C103 FORMAT(2X,I4,2I3,F8.2,2F8.0,8X,F8.0)
WRITE(kw,104)
104 FORMAT('1',///,5X,'MAXIMUM TEMPERATURE',/)
CALL MSD(NYRS,TMAX,RAIN,1,XDATA,T)
WRITE(kw,105)
105 FORMAT('1',///5X,'MINIMUM TEMPERATURE',/)
CALL MSD(NYRS,TMIN,RAIN,2,XDATA,t2)
IF(KSD.EQ.1) GO TO 9
WRITE(kw,106)
106 FORMAT('1',///,5X,'SOLAR RADIATION ',/)
CALL MSD(NYRS,RAD,RAIN,3,XDATA,t3)
WRITE(kw,107)
9 CONTINUE
107 FORMAT('1',///,5X,'PRECIPITATION')
CALL PPRAIN(RAIN,NYRS,YDATA)
C--PHASE ANGLE SHIFTED BY 180 DEGREES
C--AND SIGNS CHANGED ON AMPLITUDES
XDATA(02)=XDATA(02)*(-1.0)
XDATA(04)=XDATA(04)*(-1.0)
XDATA(10)=XDATA(10)*(-1.0)
XDATA(12)=XDATA(12)*(-1.0)
XDATA(14)=XDATA(14)*(-1.0)
C WRITE(kw,101) (AA(I),I=1,20)
WRITE(kw,101) TITLE
WRITE(kw,707)
707 FORMAT(///,1X,'INPUT CARDS FOR THE WEATHER GENERATOR ARE AS FOLLOW
*S -----',////)
WRITE(kw,403)
403 FORMAT(///)
WRITE(kw,513) (YDATA(1,J),J=1,12)
WRITE(kw,514) (YDATA(2,J),J=1,12)
WRITE(kw,515) (YDATA(3,J),J=1,12)
WRITE(kw,516) (YDATA(4,J),J=1,12)
WRITE(kw1,613) (YDATA(1,J),J=1,12)
WRITE(kw1,613) (YDATA(2,J),J=1,12)
WRITE(kw1,613) (YDATA(3,J),J=1,12)
WRITE(kw1,613) (YDATA(4,J),J=1,12)
513 FORMAT('INPUT # 3 P(W/W) ',12F6.3)
514 FORMAT('INPUT # 4 P(W/D) ',12F6.3)
515 FORMAT('INPUT # 5 ALPHA ',12F6.3)
516 FORMAT('INPUT # 6 BETA ',12F6.3)
613 format(12f6.3)
WRITE(6,400)
400 FORMAT(////)
WRITE(kw,701)
WRITE(kw,501) XDATA(01)
WRITE(kw,502) XDATA(02)
WRITE(kw,503) XDATA(03)
WRITE(kw,504) XDATA(04)
write(kw,5504) t

```

input
DATA
input

4/9

```

701  FORMAT(5X,'INPUT # 7 ----',/)
501  FORMAT(15X,' 1   TXMD   ----  ',F10.3)
502  FORMAT(15X,' 2   ATX    ----  ',F10.3)
      }  FORMAT(15X,' 3   CVTX   ----  ',F10.3)
504  FORMAT(15X,' 4   ACVTX  ----  ',F10.3)
5504 FORMAT(15X,' 5   PHTX   ----  ',F10.3)
      write(kw1,614) (xdata(j),j=1,4),T
      format(5f8.3)
      WRITE(kw,702)
702  FORMAT(//,5X,'INPUT # 8 ----',/)
      WRITE(kw,505) XDATA(05)
505  FORMAT(15X,' 5   TXMW   ----  ',F10.3)
      write(kw1,614) xdata(5)
      WRITE(kw,703)
703  FORMAT(//,5X,'INPUT # 9 ----',/)
      WRITE(kw,506) XDATA(09)
      WRITE(kw,507) XDATA(10)
      WRITE(kw,508) XDATA(11)
      WRITE(kw,509) XDATA(12)
506  FORMAT(15X,' 6   TN     ----  ',F10.3)
507  FORMAT(15X,' 7   ATN    ----  ',F10.3)
508  FORMAT(15X,' 8   CVTN   ----  ',F10.3)
509  FORMAT(15X,' 9   ACVTN  ----  ',F10.3)
      write(kw1,614) (xdata(j),j=9,12)
      WRITE(kw,704)
704  FORMAT(//,5X,'INPUT # 10 ----',/)
      if(ksd.ne.1) go to 973
      xdata(13) = 450.
      xdata(14) = 190.
      xdata(17) = 290.
      write(kw1,615)xdata(13),xdata(14)
      write(kw1,617)xdata(17)
615  format(2f8.3,5x,'DEFAULT VALUES')
617  format(f8.3,13x,'DEFAULT VALUES')
      write(kw,616)
616  format('***DEFAULT VALUES DUE TO MISSING SOLAR RADIATION DATA***'
*)
973  continue
      WRITE(kw,510) XDATA(13)
      WRITE(kw,511) XDATA(14)
510  FORMAT(15X,'10   RMD    ----  ',F10.3)
511  FORMAT(15X,'11   AR     ----  ',F10.3)
      WRITE(kw,705)
705  FORMAT(//,5X,'INPUT # 11 ----',/)
      WRITE(kw,512) XDATA(17)
512  FORMAT(15X,'12   RMW    ----  ',F10.3)
      if(ksd.eq.1) go to 974
      write(kw1,614) xdata(13),xdata(14)
      write(kw1,614) xdata(17)
974  continue
      STOP
      END
      SUBROUTINE FOUR(XM,SD,CV,XDATA,t)
      DIMENSION XM(13),SD(13)
      DIMENSION CV(13)
      DIMENSION XDATA(30)
      DATA KW /6/
      DATA JCT /0/
      S = 0.
      S1 = 0.

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131

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S2 = 0.
WRITE(kw,200)
200  FORMAT(//,3X,' PERIOD MEAN STD DEV CV')
DO 10 I = 1,13
WRITE(kw,201)I,XM(I),SD(I),CV(I)
201  FORMAT(I10,3F10.2)
S = S + XM(I)
S1 = S1 + SD(I)
S2 = S2 + CV(I)
10  CONTINUE
XBAR=S/13.
XBAR1=S1/13.
XBAR2=S2/13.
SUMA = 0.
SUMB = 0.
SUMA1 = 0.
SUMB1 = 0.
SUMA2=0.
SUMB2 = 0.
DO 15 K = 1,13
XK = K
SUMA=SUMA+(XM(K)-XBAR)*COS(6.2832*XK/13.)
SUMA1=SUMA1+(SD(K)-XBAR1)*COS(6.2832*XK/13.)
SUMA2=SUMA2+(CV(K)-XBAR2)*COS(6.2832*XK/13.)
SUMB=SUMB+(XM(K)-XBAR)*SIN(6.2832*XK/13.)
SUMB1=SUMB1+(SD(K)-XBAR1)*SIN(6.2832*XK/13.)
SUMB2=SUMB2+(CV(K)-XBAR2)*SIN(6.2832*XK/13.)
-15 CONTINUE
A = SUMA*(2./13.)
A1= SUMA1*(2./13.)
A2 = SUMA2*(2./13.)
B = SUMB*(2./13.)
B1 = SUMB1*(2./13.)
B2 = SUMB2*(2./13.)
T = ATAN(-B/A)
T1= ATAN(-B1/A1)
T2=ATAN(-B2/A2)
C = A/COS(T)
C1 = A1/COS(T1)
C2 = A2/COS(T2)
WRITE(kw,100)
100  FORMAT(/,'FOURIER COEFFICIENTS--MEAN')
WRITE(kw,101) XBAR,C,T
101  FORMAT('MEAN =',F10.4,5X,'AMPLITUDE =',F10.4,5X,'PHASE =',
*F10.4)
t=(3.1416+t)*58.091
JCT=JCT+1
XDATA(JCT)=XBAR
JCT=JCT+1
XDATA(JCT)=C
WRITE(kw,102)
102  FORMAT(/,'FOURIER COEFFICIENTS--STD. DEV.')
WRITE(kw,101)XBAR1,C1,T1
WRITE(kw,103)
}  FORMAT(/,'FOURIER COEFFICIENTS--CV')
WRITE(kw,101) XBAR2,C2,T2
JCT=JCT+1
XDATA(JCT)=XBAR2
JCT=JCT+1
XDATA(JCT)=C2

```

13 - 58 day periods

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5/8

132

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```

RETURN
END
SUBROUTINE MSD(NYRS,W,RAIN,ID,XDATA,t)
DIMENSION W(105,365),RAIN(105,365),XM(13),XM1(13),SD(13),SD1(13)
DIMENSION CX(13),CX1(13)
DIMENSION XDATA(30)
DATA KW /6/
DO 20 I = 1,13
NF=I*28
NI=NF-27
XN = 0.
XN1 = 0.
SUM = 0.
SUM1 = 0.
SS = 0.
SS1 = 0.
DO 15 JD=NI,NF
DO 15 JY = 1,NYRS
IF(ID .EQ. 2) GO TO 11
IF(RAIN(JY,JD))11,11,12
11 CONTINUE
XN = XN + 1.
SUM = SUM+W(JY,JD)
SS = SS + (W(JY,JD)*W(JY,JD))
GO TO 15
12 CONTINUE
XN1 = XN1 + 1.
SUM1 = SUM1 + W(JY,JD)
SS1=SS1+(W(JY,JD)*W(JY,JD))
CONTINUE
IF(XN .LE. 2.) XM(I) = 0.
IF(XN .LE. 2.) SD(I) = 0.
IF(XN .LE. 2.) CX(I) = 0.
IF(XN .LE. 2.) GO TO 400
XM(I) = SUM / XN
SD(I) = SQRT((SS-SUM*SUM/XN)/(XN-1.))
IF(XM(I) .LT. 0.001) XM(I) = 0.001
CX(I) = SD(I) / XM(I)
400 CONTINUE
IF(ID .EQ. 2) GO TO 20
IF(XN1 .LE. 2.) XM1(I)=0.
IF(XN1 .LE. 2.) SD1(I) = 0.
IF(XN1 .LE. 2.) CX1(I) = 0.
IF(XN1 .LE. 2.) GO TO 500
XM1(I) = SUM1 / XN1
SD1(I)=SQRT((SS1-SUM1*SUM1/XN1)/(XN1-1.))
IF(XM1(I) .LT. 0.001) XM1(I) = 0.001
CX1(I)=SD1(I)/XM1(I)
500 CONTINUE
20 CONTINUE
IF(ID .EQ. 2) GO TO 25
WRITE(kw,100)
100 FORMAT(10X,'DRY DAYS')
CALL FOUR(XM,SD,CX,XDATA,t)
WRITE(kw,101)
101 FORMAT(/,10X,'WET DAYS')
CALL FOUR(XM1,SD1,CX1,XDATA,t)
GO TO 30
25 WRITE(kw,102)
102 FORMAT(10X,'WET AND DRY DAYS')

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```

30 CALL FOUR(XM,SD,CX,XDATA,t)
CONTINUE
RETURN
END
SUBROUTINE PPRAIN(XRAIN,NYR,YDATA)
DIMENSION XRAIN(105,365)
DIMENSION NWD(12),NDD(12),NDW(12),NWW(12)
DIMENSION SUM(12),SUM2(12),SUM3(12)
DIMENSION SL(12),PWW(12),PWD(12),RBAR(12)
DIMENSION ALPHA(12),BETA(12)
DIMENSION NW(12),IC(12),SUML(12)
C DIMENSION RLBAR(12),AL2(12),BE2(12),DATE(12)
DIMENSION RLBAR(12),DATE(12)
DIMENSION PPPW(12),ND(12)
DIMENSION YDATA(4,12)
CHARACTER *36 A(2)
DATA DATE /'JAN.','FEB.','MAR.','APR.','MAY ','JUNE',
* 'JULY','AUG.','SEP.','OCT.','NOV.','DEC.'/
DATA A(1) /'
DATA A(2) /'NOT ENOUGH DATA TO DEFINE PARAMETERS'/
DATA KW /6/
DO 10 I =1,12
ND(I) = 0
PPPW(I) = 0.
NWD(I) = 0
NWW(I) = 0
NDD(I) = 0
NDW(I) =0
NW(I) = 0
SL(I) = 0.
SUML(I) = 0.
SUM(I) = 0.
SUM2(I) = 0.
PWW(I) = 0.
PWD(I) = 0.
ALPHA(I) = 0.
BETA(I) = 0.
10 SUM3(I) = 0.
XYR=NYR
RIM1 = 0.
DO 20 J = 1,NYR
DO 30 K = 1,365
IF(K .GE. 001 .AND. K .LE. 031) MO = 1
IF(K .GE. 032 .AND. K .LE. 059) MO = 2
IF(K .GE. 060 .AND. K .LE. 090) MO = 3
IF(K .GE. 091 .AND. K .LE. 120) MO = 4
IF(K .GE. 121 .AND. K .LE. 151) MO = 5
IF(K .GE. 152 .AND. K .LE. 181) MO = 6
IF(K .GE. 182 .AND. K .LE. 212) MO = 7
IF(K .GE. 213 .AND. K .LE. 243) MO = 8
IF(K .GE. 244 .AND. K .LE. 273) MO = 9
IF(K .GE. 274 .AND. K .LE. 304) MO = 10
IF(K .GE. 305 .AND. K .LE. 334) MO = 11
IF(K .GE. 335 .AND. K .LE. 365) MO = 12
RAIN=XRAIN(J,K)
IF(RAIN .GT. 0.00) NW(MO)=NW(MO)+1
ND(MO)=ND(MO)+1
IF(RAIN) 5,5,3
3 IF(RIM1)2,2,4
2 NWD(MO)=NWD(MO)+1

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135

```

GO TO 6
4  NWW(MO)=NWW(MO)+1
6  CONTINUE
   SUML(MO)=SUML(MO)+ALOG(RAIN)
   SUM(MO)=SUM(MO)+RAIN
   SUM2(MO)=SUM2(MO) + RAIN * RAIN
   SUM3(MO)=SUM3(MO)+RAIN*RAIN*RAIN
   SL(MO) = SL(MO)+ALOG(RAIN)
GO TO 9
5  IF(RIM1) 7,7,8
7  NDD(MO)=NDD(MO)+1
   GO TO 9
8  NDW(MO)=NDW(MO)+1
9  RIM1 = RAIN
30 CONTINUE
20 CONTINUE
   DO 120 I = 1,12
   XXND=ND(I)
   YYNW=NW(I)
   PPPW(I) = YYNW/XXND
   III=1
   IF(NW(I) .LT. 3) III=2
   IC(I) = III
   IF(NW(I) .LT. 3) GO TO 120
   XNWW=NWW(I)
   XNWD=NWD(I)
   XXNW=NWW(I)+NDW(I)
   XND=NDD(I)+NWD(I)
   XNW=NW(I)
   PWW(I)=XNWW/XXNW
   PWD(I)=XNWD/XND
   RBAR(I)=SUM(I)/XNW
   RLBAR(I)=SUML(I)/XNW
   Y=ALOG(RBAR(I))-RLBAR(I)
   ANUM=8.898919+9.05995*Y+0.9775373*Y*Y
   ADOM=Y*(17.79728+11.968477*Y+Y*Y)
   ALPHA2=ANUM/ADOM
   IF(ALPHA2 .GE. 1.0) ALPHA2=0.998
   BETA2=RBAR(I)/ALPHA2
   ALPHA(I)=ALPHA2
   BETA(I)=BETA2
120 CONTINUE
   WRITE(kw,201)
201  FORMAT(///,8X,'--MARKOV CHAIN--'                -GAMMA DIST-',/,
*1X,' MONTH  P(W/W)    P(W/D)                      ALPHA  BETA',/)
   DO 130 I = 1,12
   WRITE(kw,202)DATE(I),PWW(I),PWD(I),ALPHA(I),BETA(I),A(IC(I))
202  FORMAT(1X,A4,F8.3,F10.3,11X,F11.3,F7.3,5X,A36)
130  CONTINUE
   DO 400 J=1,12
   YDATA(1,J)=PWW(J)
   YDATA(2,J)=PWD(J)
   YDATA(3,J)=ALPHA(J)
   YDATA(4,J)=BETA(J)
)  CONTINUE
   RETURN
   END

```

-----_927174474=--

Temple, Texas Weather Data for year 1982-1996

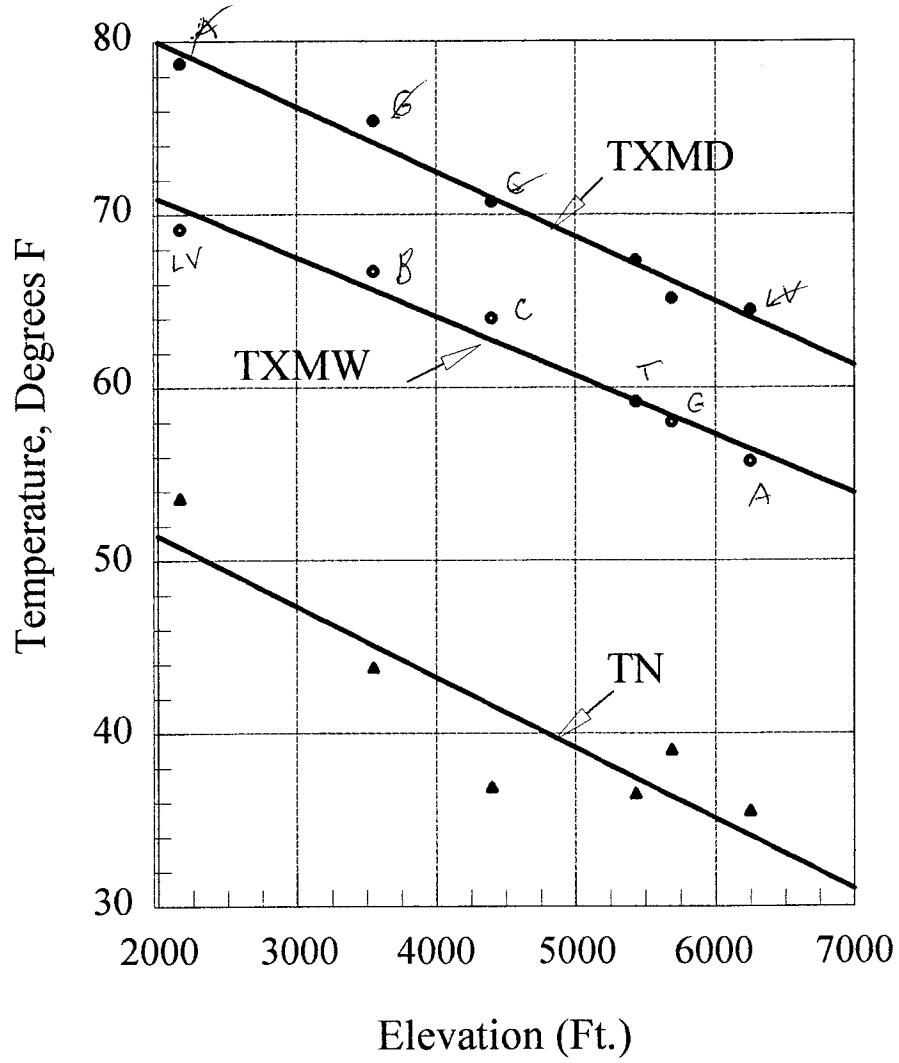
*2000
Total
Data starts on*

Jan 1

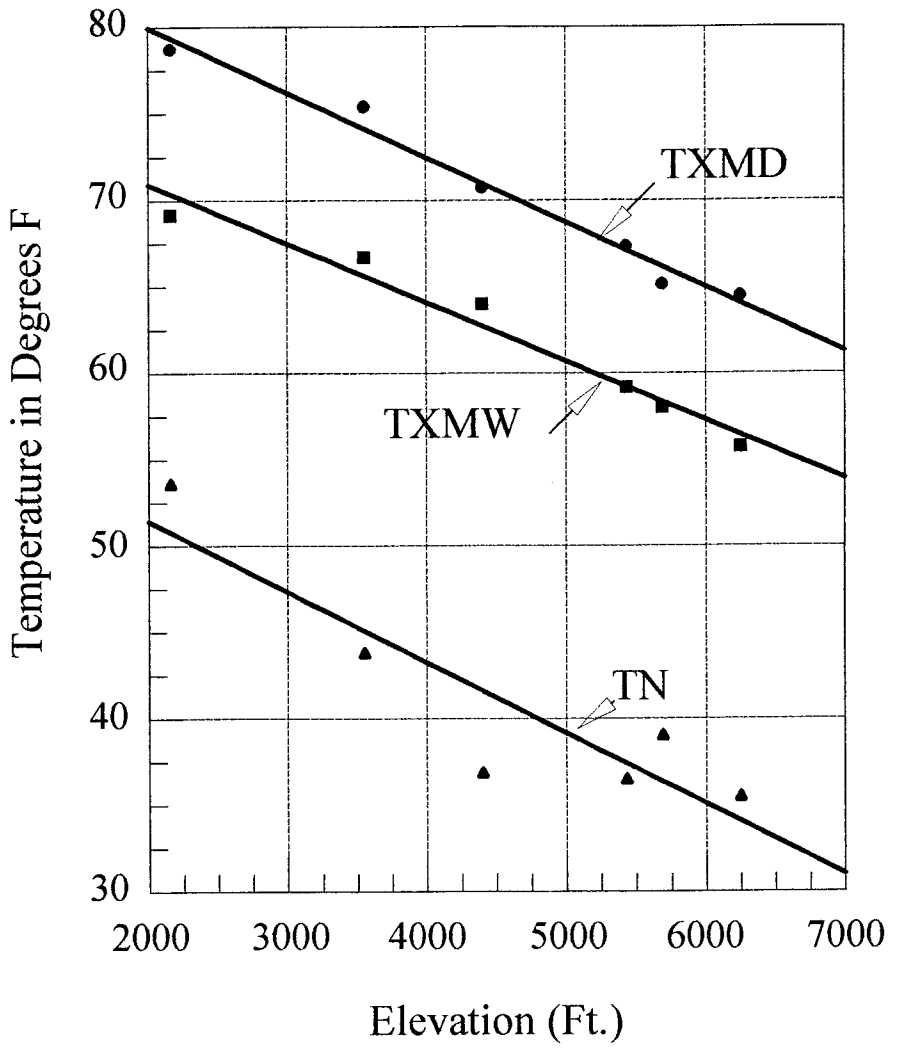
	15	31.05		
1 182	60.1	34.0	.00	296.36
282	75.0	54.0	.00	139.10
1 382	73.9	53.1	.00	273.42
1 482	62.1	37.9	.01	332.45
1 582	69.1	33.1	.00	316.44
1 682	75.9	50.0	.00	290.38
1 782	50.0	28.9	.00	171.12
1 882	46.9	24.1	.00	319.54
1 982	60.1	28.9	.00	321.45
11082	45.0	10.0	.00	321.45
11182	28.0	7.0	.00	293.49
11282	43.0	24.1	.33	135.27
11382	25.0	15.1	.09	104.20
11482	46.0	16.0	.00	352.52
11582	66.9	30.0	.00	339.38
11682	41.0	17.1	.00	295.40
11782	37.9	12.0	.00	322.41
11882	73.0	35.1	.00	329.58
11982	72.0	41.0	.00	275.33
12082	73.9	63.0	.01	161.32
12182	70.0	61.0	.00	53.06
12282	75.9	51.1	.00	158.22
12382	52.0	30.9	.00	358.50
12482	66.0	30.9	.00	346.55
12582	64.0	44.1	.00	319.54
12682	61.0	30.9	.00	368.54
12782	68.0	37.0	.00	230.40
12882	69.1	43.0	.00	334.36
12982	72.0	62.1	.00	115.20
13082	66.9	42.1	.00	101.10
13182	53.1	35.1	.33	389.57
2 182	55.9	30.0	.00	281.30
2 282	61.0	45.0	.11	248.32
2 382	37.9	28.0	.00	159.17
2 482	37.0	27.0	.00	136.23
2 582	34.0	21.0	.05	48.99
2 682	33.1	15.1	.00	302.33
2 782	43.0	25.0	.00	278.43
2 882	46.9	37.0	.06	85.08
2 982	45.0	23.0	.00	390.53
21082	44.1	23.0	.00	272.46
21182	57.0	28.9	.00	361.61
21282	69.1	33.1	.00	359.46
21382	39.9	27.0	.00	253.34
21482	59.0	30.0	.00	264.33
21582	73.0	51.1	.00	238.28
21682	80.1	48.9	.00	436.65
21782	84.9	46.9	.00	431.63
21882	68.0	42.1	.00	347.51
21982	66.9	45.0	.00	271.27
22082	61.0	54.0	.17	215.34
22182	79.0	48.9	.00	466.77

*VI
VI
VI
VI
VI*

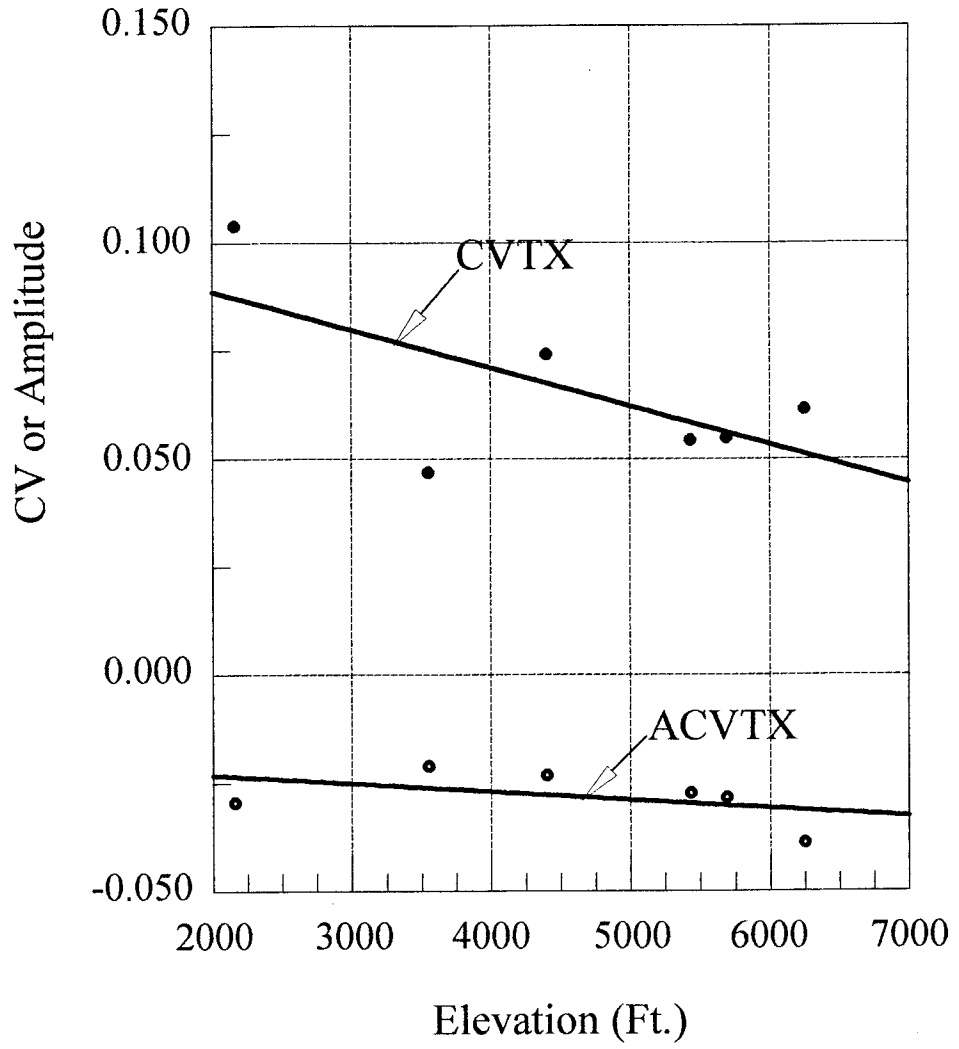
DAW



Tempstat.pdw



DAW



DAW

SUMMARY OF MIXEX2000 RUNS C16-C21

Four harmonics for Markov Chain Parameters. Alpha optimized, Two harmonics for Beta, Three harmonics for the mean daily precipitation given a wet day. DAW 1-21-2000 FILE: CLIMATE\Summary1.wpd

: STATION NUMBER 260046 ADAVEN Run C21

Mean of alpha before optimization = 0.279512

FINAL LOG-LIKELIHOOD VALUE=-F= 436.09814

PARAMETER	MEAN	AMP	PAN	AMP	PAN
ALFA	0.15440				
BETA	1.708 0.67243E-01	0.563 0.22164E-01	-1.7430	0.0196 0.77122E-03	5.3109
MEAN	7.994 0.28716	1.723 0.67838E-01	-2.6423	0.899 0.35359E-01	0.22040 0.14954E-01

conversions from inches to mm

~ 2.54

: STATION NUMBER 260718 BEATTY8N Run C19

Mean of alpha before optimization = 0.350364

FINAL LOG-LIKELIHOOD VALUE=-F= 620.78119

PARAMETER	MEAN	AMP	PAN	AMP	PAN
ALFA	0.32741				
BETA	1.019 mm 0.40053E-01	+ 0.0594 mm -0.23393E-02	1.146 -2.0150	0.457 0.18011E-01	3.0356
MEAN	4.47 mm 0.17597	0.500 0.19679E-01	3.1388	0.692 0.27261E-01	1.8101 0.12525E-01

= -3.144

: STATION NUMBER 261358 CALIENTE Run C20

Mean of alpha before optimization = 0.213767

FINAL LOG-LIKELIHOOD VALUE=-F= 1641.54407

PARAMETER	MEAN	AMP	PAN	AMP	PAN
ALFA	0.14383				
BETA	0.254 0.10050E-01	0.110 0.43232E-02	-1.3439	0.095 0.37392E-02	-0.37800
MEAN	4.44 0.17488	0.8725 0.34353E-01	-2.1941	0.364 0.14331E-01	-0.11906 0.52707E-03

~ 5.905

~ 6.1641

~ 1.02

Daw

ADAVEN MARKOV CHAIN AMPS & PHASE ANGLES (ADAVEN4.MCP)

2.3819	0.36420	0.37052	0.33419	0.22590	.0
0.0000	-1.6064	-77698	2.5482	-47310	.0
0.55822	0.17989	0.16553	0.23534	0.29469	.0
0.0000	-1.2667	-50407	2.3300	-61901	.0

BEATTY8N MARKOV CHAIN AMPLITUDES AND PHASE ANGLES 4 HARMONICS

2.7511	0.48574	0.29087	0.17459	0.39786
0.0000	-1.2549	-1.2489	2.1432	-.76458
0.67330	0.25265	0.19815	0.13475	0.93316E-01
0.0000	-1.6849	-84431	-18030	2.5517

Caliente Markov Chain Amplitudes and Phase angles (CALIEN4.OUT)

2.3243	0.22288	0.38381	0.30365	0.36045
0.0000	-1.4470	-76353	2.4941	-.34840
0.36226	0.16423E-01	0.12902	0.55821E-01	0.75858E-01
0.0000	-1.3244	-2.4432	2.2575	2.3834

GOLDFIELD MC AMPLITUDES AND PHASE ANGLES (GOL4.MCP)

2.7418	0.36363	0.26168	0.28914	0.36333
0.0000	-1.8682	-.99035	2.3544	-.77460
0.73884	0.41390E-01	0.28228	0.25068	0.18313
0.0000	2.9089	-.10338	-.82215	-.70106

TONOPAH MC AMPLITUDES AND PHASE ANGLES (TON4.MCP) FROM TONOPA4.OUT

2.5885	0.21903	0.23607	0.23945	0.37065
0.0000	-1.7080	-.94035	2.4147	-.72411
0.57021	0.31977E-01	0.15006	0.22222	0.20179E-01
0.0000	-1.0422	-.77094	-.48563	0.11229

LAS VEGAS MC AMPLITUDES AND PHASE ANGLES (VEG4.MCP) FROM VEGAS4.OUT

2.9128	0.33880	0.50975	0.35487	0.33495
0.0000	-.65039	-.99029	2.7165	-.48979
0.90554	0.29772	0.25580	0.57257E-01	0.24337
0.0000	-.68118	-.81057	2.7144	2.3980

DAW

: STATION NUMBER 263285 GOLDFIELD Run C16 (Rerun)

Mean of alpha before optimization = 0.356002

FINAL LOG-LIKELIHOOD VALUE=-F= 613.81427

PARAMETER	MEAN	AMP	PAN	AMP	PAN
ALFA	0.33287				
BETA	0.52928E-01	0.96944E-02	5.1045	0.22432E-01	0.36756
MEAN	0.20904	0.49021E-01	-2.0018	0.44465E-01	0.57591

: STATION NUMBER 268170 TONOPAH Run C17

Mean of alpha before optimization = 0.323169

FINAL LOG-LIKELIHOOD VALUE=-F= 1712.73584

PARAMETER	MEAN	AMP	PAN	AMP	PAN
ALFA	0.25966				
BETA	0.14217E-01	0.54713E-04	-5.2390	0.11297E-02	-0.21891
MEAN	0.14018	0.32714E-01	-1.3301	0.16682E-01	0.43866

264436 LAS VEGAS WSO AIRPORT Run C18

veg C18.02

Mean of alpha before optimization = 0.328283

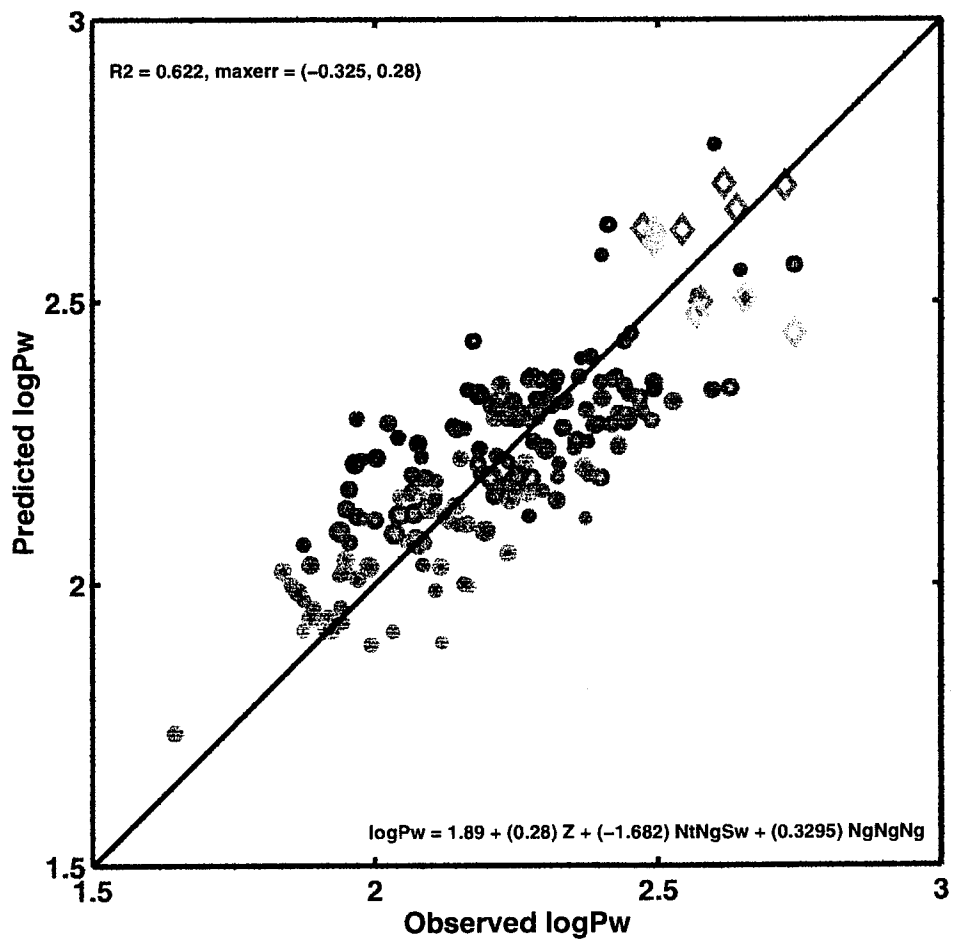
FINAL LOG-LIKELIHOOD VALUE=-F= 1117.51428

PARAMETER	MEAN	AMP	PAN	AMP	PAN
ALFA	0.29425				
BETA	0.11864E-01	0.64399E-02	0.48476	-0.46219E-04	2.1934
MEAN	0.15097	0.27687E-01	-1.7864	0.21515E-01	2.0457

Summarized in PLOT sheet MCMEPAR2.POW

81.24

Daw



*Plot from Stothoff
HAFit_Pw_3_C.pdf*

MIXEX

CALL CALCUL p 9
CALL SORT14
CALL SORT1R4

CALL ESTADI p 13

CALL MIXEXP p 14

CALL ASIMPLX
FPLIK p 17

CALL FOUTER

CALL SERIES

CALL COEFF

CALL FOURI p 9

CALL LIKMEX p 19 - Most likely for errors

CALL MLIK p 21 looks O.K.

CALL ASIMPLX

TOTALIK p 22

RETURN

MS WORD 144

MS WORD

MIXEX.DEF.DOC

22-141 50 SHEETS
22-142 100 SHEETS
22-144 200 SHEETS



p 20

CALFA

145

> 0 N=2

= 0 N=3

done

- X(1) = β
- X(2) = 0
- X(3) = 1st am α
- X(4) = 1st ϕ α
- X(5) = ~~2nd am α~~ OK
- X(6) = ~~2nd ϕ α~~ OK
- X(7) = 3rd am α
- X(8) = 3rd ϕ α
- X(9) = 1st am α
- X(10) = 1st ϕ β

if MAY H=3
Daw 4/2/04

- X(1) = 2
- X(2) = β
- X(3) = 0
- X(4) = 1st am α
- X(5) = 1st ϕ α
- etc

etc

22-141 50 SHEETS
22-142 100 SHEETS
22-144 200 SHEETS



Should revise MIXEX so that it reads in
the Fourier Coef. for P_{00} and P_{10}

0 146

Also write out a file that can be used to
create a graph.

DAY P00 P10 PWET α β θ μ ϵ P_T ϵ N_T ϵ P₀ ϵ N₀

22-141 50 SHEETS
22-142 100 SHEETS
22-144 200 SHEETS



LIKMEX

ALFA (I), I=1, 365 mixed exponential parameter
for day I.

BETA (I) "

TETA (I) "

CALFA - Input value for α , if CALFA > 0, then
 α is a constant and is not optimized. This option
is used when α is a regional constant.
if CALFA = 0
IN COMMON SEIS

KALFA - Code. if KALFA = 0
if KALFA = 1

FOURIER SERIES

$$f(t) = \frac{a_0}{T} + \sum_1^{\infty} \left(a_n \cos \frac{n\pi t}{T} + b_n \sin \frac{n\pi t}{T} \right)$$

or

$$f(t) = \sum_{-\infty}^{\infty} c_n e^{in\pi t/T}$$

MAXA, MAXB, MAXT - Maximum number of harmonics
for α , β and θ respectively

MAXH - Maximum number of harmonics considered
= MAX(MAXA, MAXB, MAXT)

$x(1)$
 $x(2)$ - Parameters to be optimized

$x(N)$

if CALFA > 0 N=2 and $x(1) = \text{BEMEAN}$, $x(2) = \bar{\mu}$

if CALFA = 0 N=3 and $x(1) = \text{ALMEAN}$, $x(2) = \text{BEMEAN}$, $x(3) = \bar{\mu}$

SUBROUTINES

DW

✓ ASIMPLX (SXFUNC, NPAR, ITMAX, PAREPS, FNEPS, STEP
KIST, IP, A)

✓ AMP_FAZE (PAR, AM, PH) - May not be used

22-141 50 SHEETS
22-142 100 SHEETS
22-144 200 SHEETS



✓ CALCUL

✓ COEFF (F, NSTUDY, AMP, PAN, YMEAN, MAXH)

✓ ESTADI

✓ FOURI (IPR)

✓ FCUTER (NSTUDY) -

✓ FPLIK (N, X, F)

✓ LIKMEX

✓ MLIK

✓ MIXEXP

✓ SERIES

✓ TOTALIK (N, X, F)

✓ SORTI4 (R, N, IDR)

✓ SORT1R4 (R, N, IDR)

CALFA 1

p 15 in SUB MIXEXP

149

ORMOM1(I)=

DA = CALFA

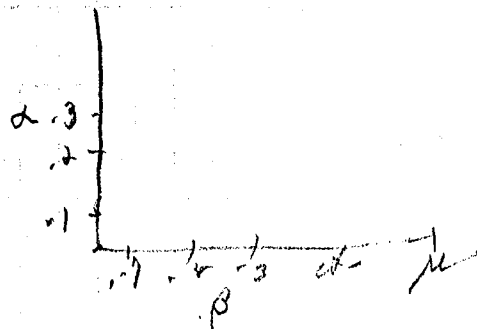
$$f(x) = \alpha \frac{e^{-x/\beta}}{\beta} + (1-\alpha) \frac{e^{-x/\theta}}{\theta}$$

$$\mu = \alpha \beta + (1-\alpha) \theta$$

$$\beta = 0.1 \mu$$

$$\mu = \alpha [0.1 \mu] + (1-\alpha) \theta$$

$$\theta = \frac{\mu - \alpha(0.1\mu)}{1-\alpha}$$



Sub FPLIK looks O.K. but not sure of the function of KALFA

It appears that if KALFA = 1 then CALFA (input) = 0
And CALFA is used to calculate the average of α for all periods

		CALPHA	
	KALFA	0	> 0 MAXA = 0
	0		
	1	MAXA = 0	MAXA = 0

should not be used
DAW 4/2/04

22-141 50 SHEETS
22-142 100 SHEETS
22-144 200 SHEETS



Problem with SORTIIY (NTEMP, NCOUNT, -1)

0: 150

NTEMP(L) L=1 → NCOUNT # of years

Trying to get CDF of # of wet days per period as specified by NUMSAV

NTEMP(

L

1 N1

2 N2

:

N

NCOUNT Ncount

1	0	2
2	10	
3	11	
4	9	
5	2	
6	1	
7	4	
8	8	
9	7	
10	6	

SORTIIY(R, N, IDR)

of yrs set = 10

MC	MPD	LL	L	LR	RN	I	J
1234567	5	0	1	N(10)	N-1(10)	1	N-1(10)
0.5							10

FR = R(5) (1)

22-141 50 SHEETS
22-142 100 SHEETS
22-144 200 SHEETS



PAN(I, J) Phase angle in radians

C 151

AMP(I, J) Amplitude

I	$P_{11}^?$	$P_{12}^?$	J				
1			3	4	5	6	
			1st Amp α	1st Amp β	1st Amp θ	1st amp μ	
2			2nd " α	2nd " β	2nd θ	2nd amp μ	
3			3rd α	3rd β	3rd θ	3rd amp μ	
4							
5							
6							

MAXIT

A(I) parameters to be optimized in ASIMPLX - returns from ASIMPLX

KIST - ^{DAW 4/2/04} ~~PARAMETER~~ returned from ASIMPLX

IF CALFA > 0 then,

$$\begin{aligned}
 X(3) &= AMP(1,3) & X(4) &= PAN(1,3) \\
 X(5) &= AMP(2,3) & X(6) &= PAN(2,3) \\
 X(7) &= AMP(3,3) & X(8) &= PAN(3,3)
 \end{aligned}$$



$P(I, N1) \quad I=1, N$

DAW

* Initial parameters and function value:

* Index	Function value	Function parameters			
* 21	-1616.9	0.42231E-01	0.23119	0.0000	0.0000
		0.0000	0.0000	0.0000	0.0000
		0.21613E-01	-3.0452	0.10292E-01	-1.2723
		0.10846E-01	-3.2023	0.37666E-01	-2.3754
		0.16949E-01	0.19985	0.10403E-02	2.4562

* *** Iteration limit exceeded ***

* Minimal location found:

* Index	Function value	Function parameters			
* 1000	-1628.0	0.30856E-01	0.62211	-0.30348E-01	0.46808
		0.29741E-01	-0.59271	-0.49147E-01	0.71457
		0.12548E-01	-3.2669	0.82554E-02	-1.9751
		0.10120E-01	-2.0485	0.31935E-01	-2.2096
		0.83871E-02	0.13030	0.33215E-03	2.7271

* Number of function evaluations = 1000

OPTIMIZED PARAMETERS

β	$x(1)$	$x(2)$	$x(3)$
→ 0.03086	0.62211	-0.03035	
ϕ_{13}	$x(4)$	$x(5)$	$x(6)$
→ 0.46808	0.02974	-0.59271	
α_{33}	$x(7)$	$x(8)$	$x(9)$
→ -0.04915	0.71457	0.01255	
	$x(10)$		
	-3.26694	0.00826	-1.97514
ϕ_{14}			
→ 0.01012	-2.04848	0.03193	
α_{34}			
→ -2.20961	0.00839	0.13030	
	0.00033	2.72712	

looks like it is optimizing everything!

F= -1628.01147KIST= 3

FINAL LOG-LIKELIHOOD VALUE=-F= 1628.01147

1

PARAMETER	MEAN	AMP	PAN	AMP	PAN
ALFA	0.29800				
BETA	0.30856E-01	0.12548E-01	-3.2669	0.82554E-02	-1.9751
MEAN	0.44592	0.31935E-01	-2.2096	0.83871E-02	0.13030

0.

	TPDD365	TPWD365	ALPZ	BETZ	JAE	XMU	ACP	TDW	ACPRE
345	0.8571	0.5456	0.0100	4.5144	2.8664	2.8909	42.65	0.03	46.012
346	0.8567	0.5449	0.0100	4.3358	2.7693	2.7929	42.86	0.03	46.593
347	0.8562	0.5445	0.0100	4.1486	2.6670	2.6898	43.07	0.03	47.154
348	0.8559	0.5443	0.0100	3.9533	2.5597	2.5817	43.27	0.03	47.694
349	0.8557	0.5443	0.0100	3.7501	2.4477	2.4687	43.48	0.03	48.211
350	0.8556	0.5446	0.0100	3.5395	2.3311	2.3512	43.69	0.03	48.703
351	0.8555	0.5452	0.0100	3.3219	2.2102	2.2293	43.90	0.03	49.170
352	0.8555	0.5459	0.0100	3.0977	2.0852	2.1033	44.11	0.03	49.611
353	0.8557	0.5470	0.0100	2.8674	1.9563	1.9734	44.32	0.03	50.023
354	0.8559	0.5482	0.0100	2.6315	1.8238	1.8399	44.53	0.03	50.406
355	0.8562	0.5497	0.0100	2.3903	1.6880	1.7030	44.74	0.03	50.760
356	0.8566	0.5515	0.0100	2.1445	1.5492	1.5631	44.94	0.03	51.083
357	0.8570	0.5534	0.0100	1.8944	1.4075	1.4204	45.15	0.03	51.376
358	0.8576	0.5556	0.0100	1.6407	1.2634	1.2752	45.35	0.03	51.637
359	0.8582	0.5580	0.0100	1.3839	1.1171	1.1278	45.56	0.03	51.866
360	0.8589	0.5606	0.0100	1.1244	0.9689	0.9785	45.76	0.03	52.063
361	0.8596	0.5633	0.0100	0.8628	0.8192	0.8276	45.96	0.03	52.229
362	0.8604	0.5663	0.0100	0.5997	0.6681	0.6754	46.16	0.03	52.363
363	0.8613	0.5694	0.0213	0.3356	0.5182	0.5224	46.35	0.03	52.466
364	0.8622	0.5726	0.1676	0.0711	0.4189	0.3687	46.55	0.03	52.537
365	0.8632	0.5760	0.3141	0.0100	0.2967	0.2146	46.74	0.03	52.579

↑ WRY ↑ WRY ↑ WRY ↓ WRY

Adatest.03

theory 2nd step
 May be
 Daw 4/2/04
 changed
 mostly zero
 TANT365

1-10-99 run 4 cols 1, 2, 3, 4, 5, 6, 7, 8, 10, unchanged
 9 - changed 10? also

TAW

OPTIMIZED PARAMETERS
 .07126 .17990
 F = -101.42070
 ST = 2
 LOG-L = 101.42070000
 ALFA = .31400000
 BETA = .07126127
 TETA = .17989500

*Something to write for the
 correlation input of α & β for
 the individual periods*

Daw 154

THEORETICAL MEAN PRECIPITATION FOR WET DAYS FOR EACH PERIOD

.1414 .1355 .1565 .1527 .1304 .1694 .1573 .1283 .1461
 .1893 .2124 .2336 .2197 .2579 .1583 .2525 .1336 .1636

THEORETICAL PRECIPITATION STD DEV FOR WET DAYS FOR EACH PERIOD

.1827 .1761 .2091 .1876 .1667 .1991 .2085 .1489 .1873
 .2412 .2786 .3110 .2197 .3466 .1998 .2992 .1648 .1795

LOG-LIKELIHOOD VALUES FOR MIXED EXPONENTIAL. 14-DAY PERIODS

79.31602 103.31190 69.71939 57.22364 106.54180 58.85901
 79.67467 95.78465 92.14661 40.23861 39.10471 37.06954
 60.16747 21.37925 72.28218 69.85530 62.45535 91.72600

TOTAL OF THE LOG-LIKLIHOOD VALUES= 1660.52100

A(1) = A0 = (2 X MEAN)		PHI	C	
A(1)=	.62800	B(1)= .00000	.00000	.00000
A(2)=	.00000	B(2)= .00000	-2.83313	.00000
A(3)=	.00000	B(3)= .00000	1.79663	.00000
A(4)=	.00000	B(4)= .00000	2.08045	.00000
A(5)=	.00000	B(5)= .00000	2.28080	.00000
A(6)=	.00000	B(6)= .00000	2.27565	.00000
A(7)=	.00000	B(7)= .00000	2.24721	.00000
A(8)=	.00000	B(8)= .00000	2.31241	.00000
A(9)=	.00000	B(9)= .00000	2.51480	.00000
A(10)=	.00000	B(10)= .00000	2.55010	.00000
A(11)=	.00000	B(11)= .00000	2.90136	.00000
A(12)=	.00000	B(12)= .00000	3.02167	.00000
A(

A(1) = A0 = (2 X MEAN)		PHI	C	
A(1)=	.08796	B(1)= -.02204	.00000	.00000
A(2)=	-.00420	B(2)= .00498	-2.95334	.02244
A(3)=	-.00941	B(3)= -.00970	-1.08417	.01064
A(4)=	-.00267	B(4)= .00461	-2.87332	.01006
A(5)=	-.00961	B(5)= .00709	-1.12384	.01066
A(6)=	.01799	B(6)= -.01872	1.19548	.01933
A(7)=	.00204	B(7)= .00572	3.03318	.01883
A(8)=	.00245	B(8)= -.02072	.40477	.00623
A(9)=	.00855	B(9)= -.00964	2.75001	.02242
A(10)=	-.02998	B(10)= .01805	-1.88193	.03149
A(11)=	.00354	B(11)= -.00736	.19380	.01839
A(12)=	.00718	B(12)= .00000	2.36863	.01028
A(

A(1) = A0 = (2 X MEAN)

			PHI	C
A(1)=	.46154	B(1)=	-.02183	.00000
A(2)=	-.04451	B(2)=	.02095	-2.02675
A(3)=	.01250	B(3)=	.00147	.53795
A(4)=	-.00070	B(4)=	-.01000	-.44500
A(5)=	.00012	B(5)=	.00266	3.12966
A(6)=	-.00582	B(6)=	.00953	-1.14253
A(7)=	-.00362	B(7)=	.00142	-.36307
A(8)=	-.00207	B(8)=	-.00914	-.97075
A(9)=	-.00665	B(9)=	-.00629	-2.51275
A(10)=	.01004	B(10)=	.00407	2.13056
A(11)=	-.01457	B(11)=	.02384	-1.29852
A(12)=	.01819	B(12)=	.00000	.65159

A(1) = A0 = (2 X MEAN)

			PHI	C
A(1)=	.34976	B(1)=	-.02405	.00000
A(2)=	-.02899	B(2)=	.01545	-2.26348
A(3)=	.00697	B(3)=	-.00098	.42363
A(4)=	.00036	B(4)=	-.00803	2.79189
A(5)=	-.00519	B(5)=	.00817	-2.56756
A(6)=	-.00012	B(6)=	.00295	-.01517
A(7)=	-.00125	B(7)=	.00315	-.40177
A(8)=	-.00245	B(8)=	-.01096	-.66043
A(9)=	.00039	B(9)=	-.00840	3.10623
A(10)=	.00022	B(10)=	.00620	3.11554
A(11)=	-.00881	B(11)=	.01206	-.95764
A(12)=	.01641	B(12)=	.00000	.93700

MEAN OF THE M.E.D. PARAMETERS

ALFA= .314000
 BETA= .043980
 TETA= .230770
 MEAN= .174878

AMPLITUDE FOR ALFA	.00000	.00000
PHASE ANGLE FOR ALFA	-2.94502	1.57285
AMPLITUDE FOR BETA	.02244	.01064
PHASE ANGLE FOR BETA	-3.06523	-1.30795
AMPLITUDE FOR TETA	.04957	.02440
PHASE ANGLE FOR TETA	-2.13864	.31417
AMPLITUDE FOR MEAN	.03767	.01695
PHASE ANGLE FOR MEAN	-2.37537	.19985

LIKELIHOOD WITH MAXH (LS) HARMONICS 1617.99800

OPTIMIZACION CON TODOS LOS PARAMETROS

ALFA VALUE IS CONSTANT AND IS EQUAL TO .3140

INITIAL PARAMETERS

.04398 .23479

* Simplex nonlinear optimization algorithm *

Daw

=====
Linear Regression Report

Data File Name: C:\consult\swri\CLIMATE\MCMEPAR2.PDW

=====

IndVar: PMM - *near zero precip*
DepVar: BMM *P*

Equation: $y=a*x+b$

Parameter a:	0.0042298210	<i>±.0033</i>
Parameter b:	0.047096418	<i>±.457</i>
Uncertainty da:	0.0033075704	
Uncertainty db:	0.65737697	
Sum Sqrs:	1.34860652	
StdDev:	0.51934700	
R-Sq r2:	0.29020208	
Correlation:	0.53870407	

=====

----Created by David A. Woolhiser with PSI-Plot
----Fri Jan 21 11:47:53 2000

=====

DW

Linear Regression Report

Data File Name: C:\consult\swri\CLIMATE\MCMEPAR2.PDW

IndVar: PMM \bar{P}_n
DepVar: Alpha α

Equation: $y=a*x+b$

Parameter a:	-0.00086764000	$\pm .000313$
Parameter b:	0.41291108	$\pm .00126$
Uncertainty da:	0.00031325946	
Uncertainty db:	0.062260067	
Sum Sqrs:	0.012096938	
StdDev:	0.049187271	
R-Sq r2:	0.65727988	
Correlation:	-0.81072799	

-----Created by David A. Woolhiser with PSI-Plot
 -----Fri Jan 21 11:35:50 2000

=====
 Linear Regression Report

 Data File Name: C:\consult\swri\CLIMATE\MCMEPAR2.PDW
 =====

 IndVar:
 DepVar:

 PMM
 MUMM

 P_A (mm)
 μ
Equation: $y=a*x+b$

Parameter a:	0.014050940	± 0.00302
Parameter b:	2.21517346	± 0.9978
Uncertainty da:	0.0050204943	
Uncertainty db:	0.99781922	
Sum Sqrs:	3.10713429	
StdDev:	0.78830632	
R-Sq r2:	0.66195700	
Correlation:	0.81360740	

 ----Created by David A. Woolhiser with PSI-Plot
 ----Fri Jan 21 11:48:52 2000

=====
Linear Regression Report

Data File Name: C:\consult\swri\CLIMATE\MCMEPAR2.PDW
=====

IndVar: PMM
DepVar: LOGITA

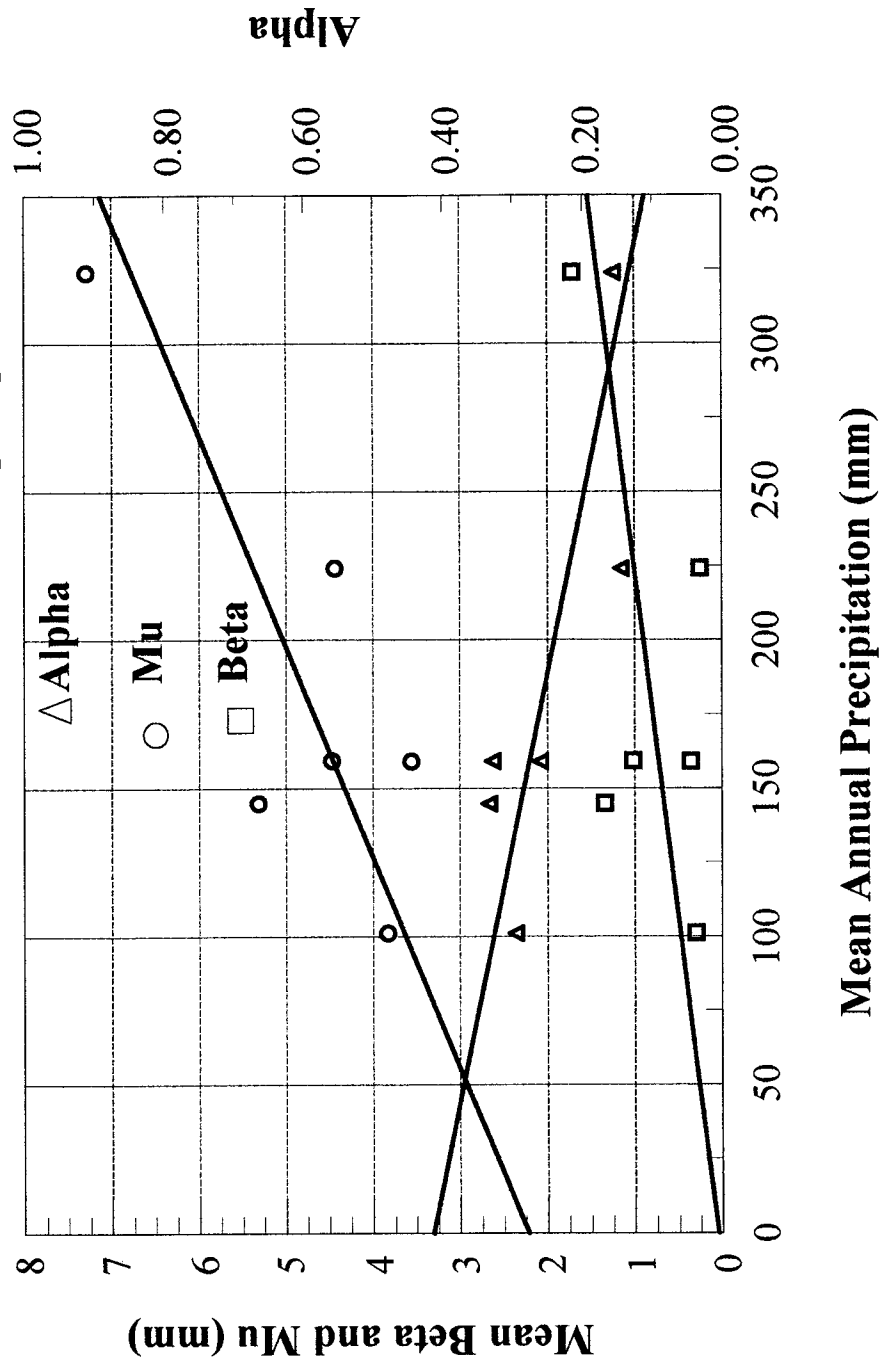
\bar{P}_1
 $\ln\left(\frac{S}{1-P_1}\right)$

Equation: $y=a*x+b$

Parameter a: -0.0050773200 ± .00177
Parameter b: -0.19578828 ± .352
Uncertainty da: 0.0017724579
Uncertainty db: 0.35227458
Sum Sqrs: 0.38727450
StdDev: 0.27830721
R-Sq r2: 0.67228507
Correlation: -0.81992992

=====
----Created by David A. Woolhiser with PSI-Plot
----Fri Jan 21 12:06:36 2000
=====

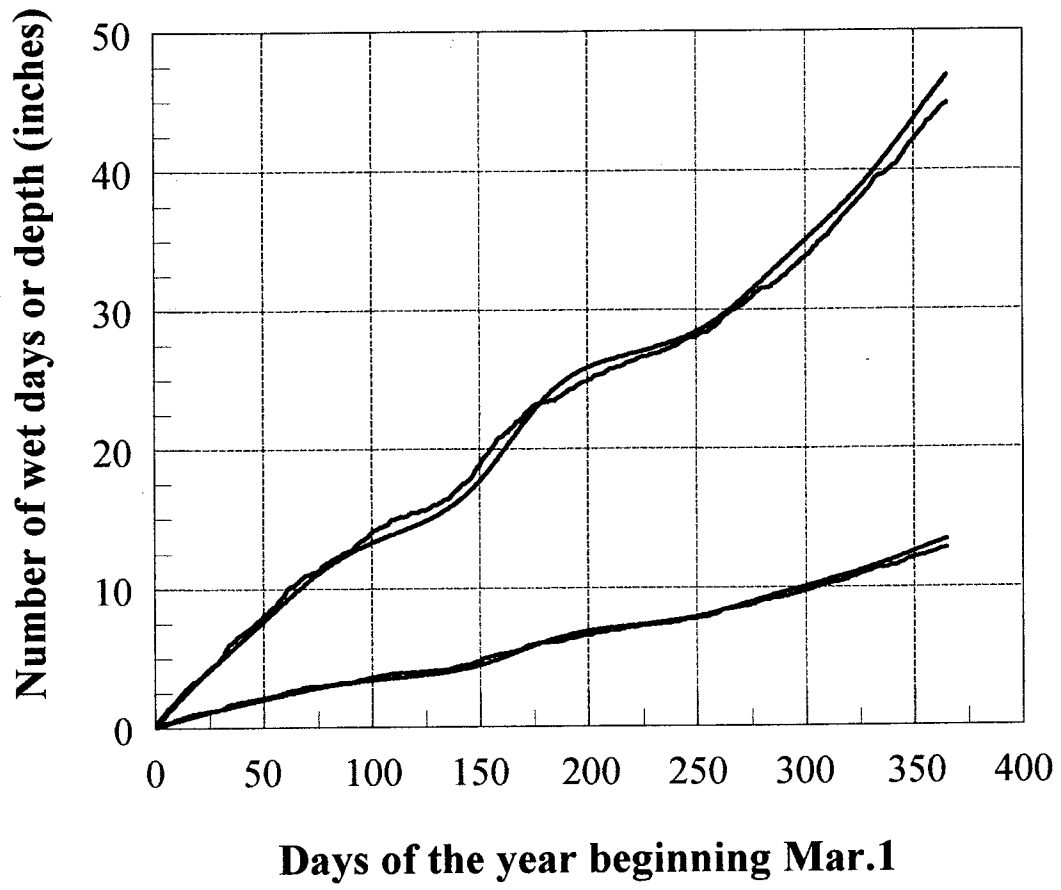
Relation between mean annual parameters
 of the ME distribution and mean annual precipitation



DAW

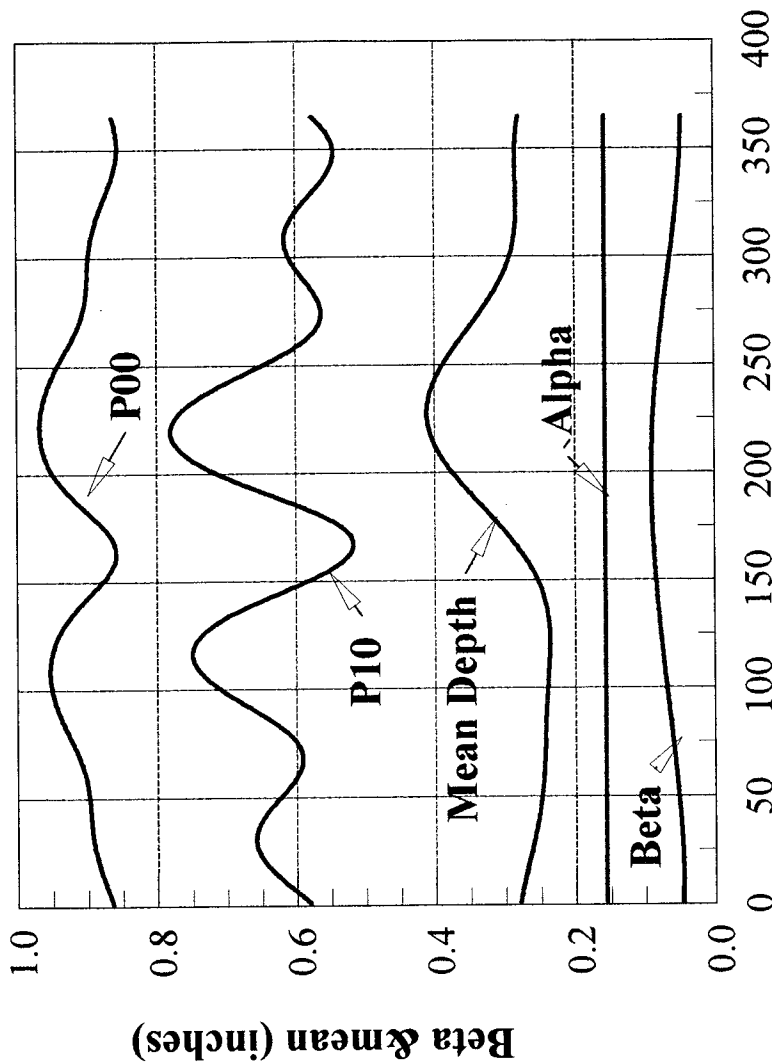
DWS

Adac21.o3



PAW 1-19-2000
ADCHIPAR.

Adac21.03



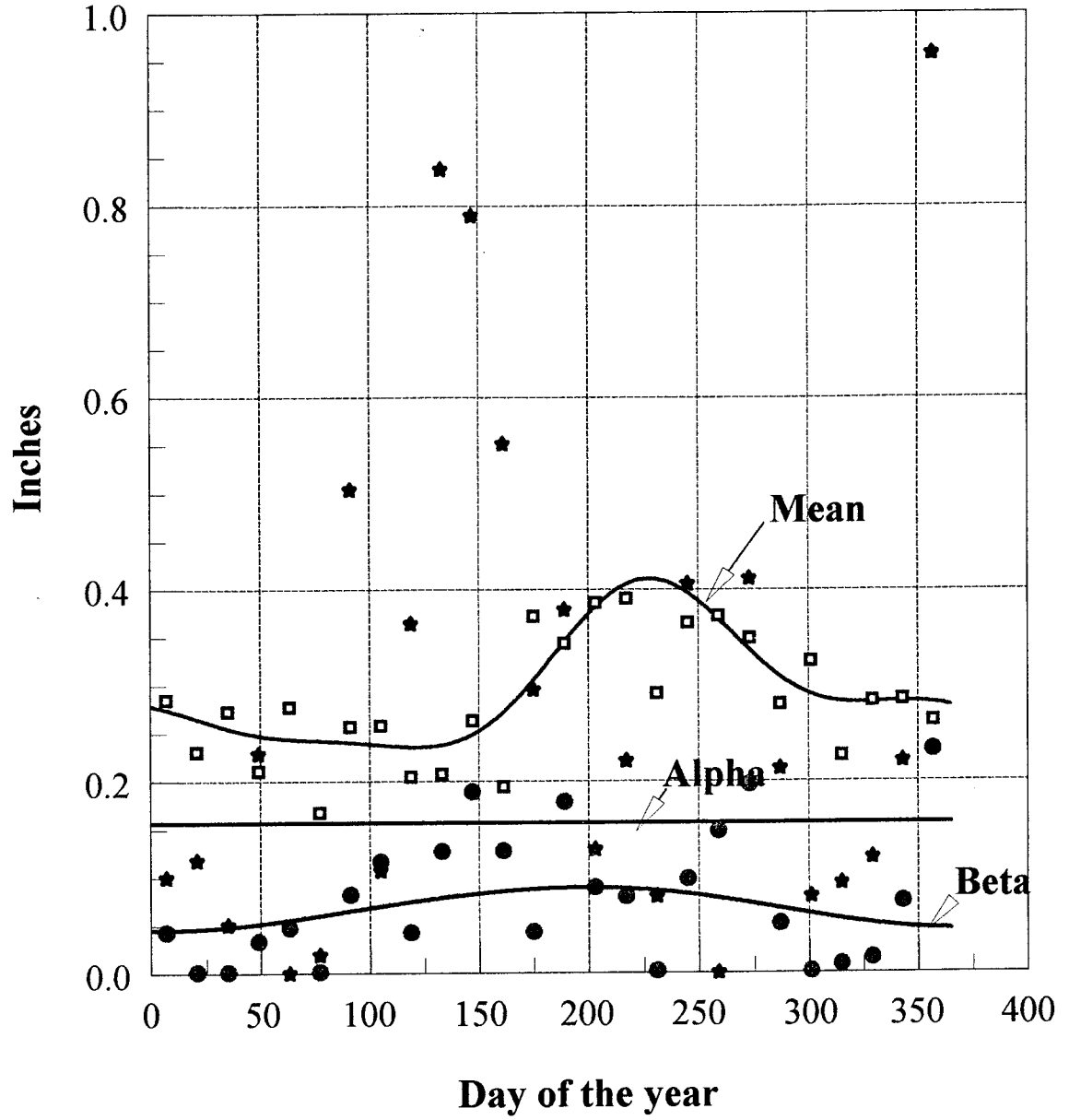
Day of Year Beginning Mar. 1

Adaven, NV
 Markov Chain 4
 Number of Harmonics 0
 Alpha 2
 Beta 3
 Mean

[Handwritten signature]

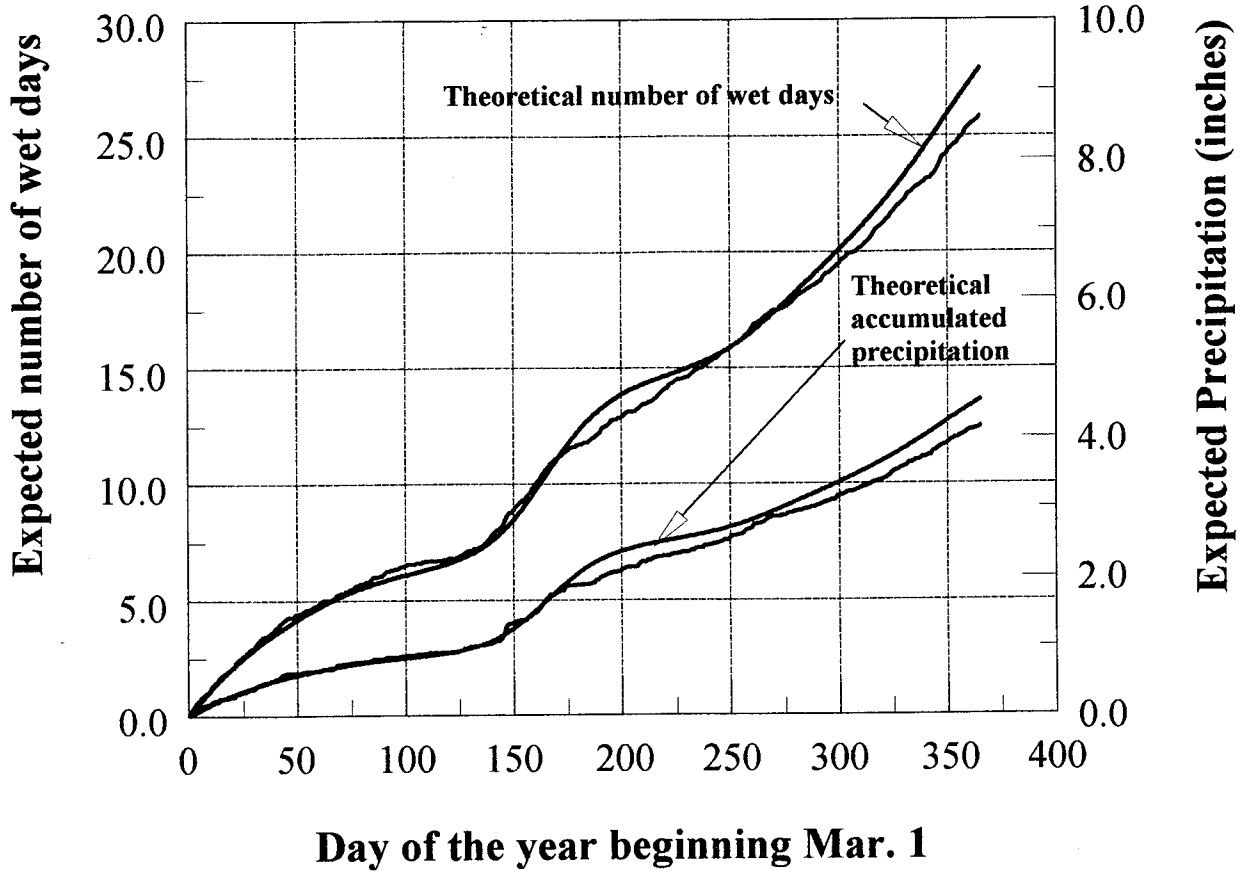
ADAC21PDW

Daw



DAW

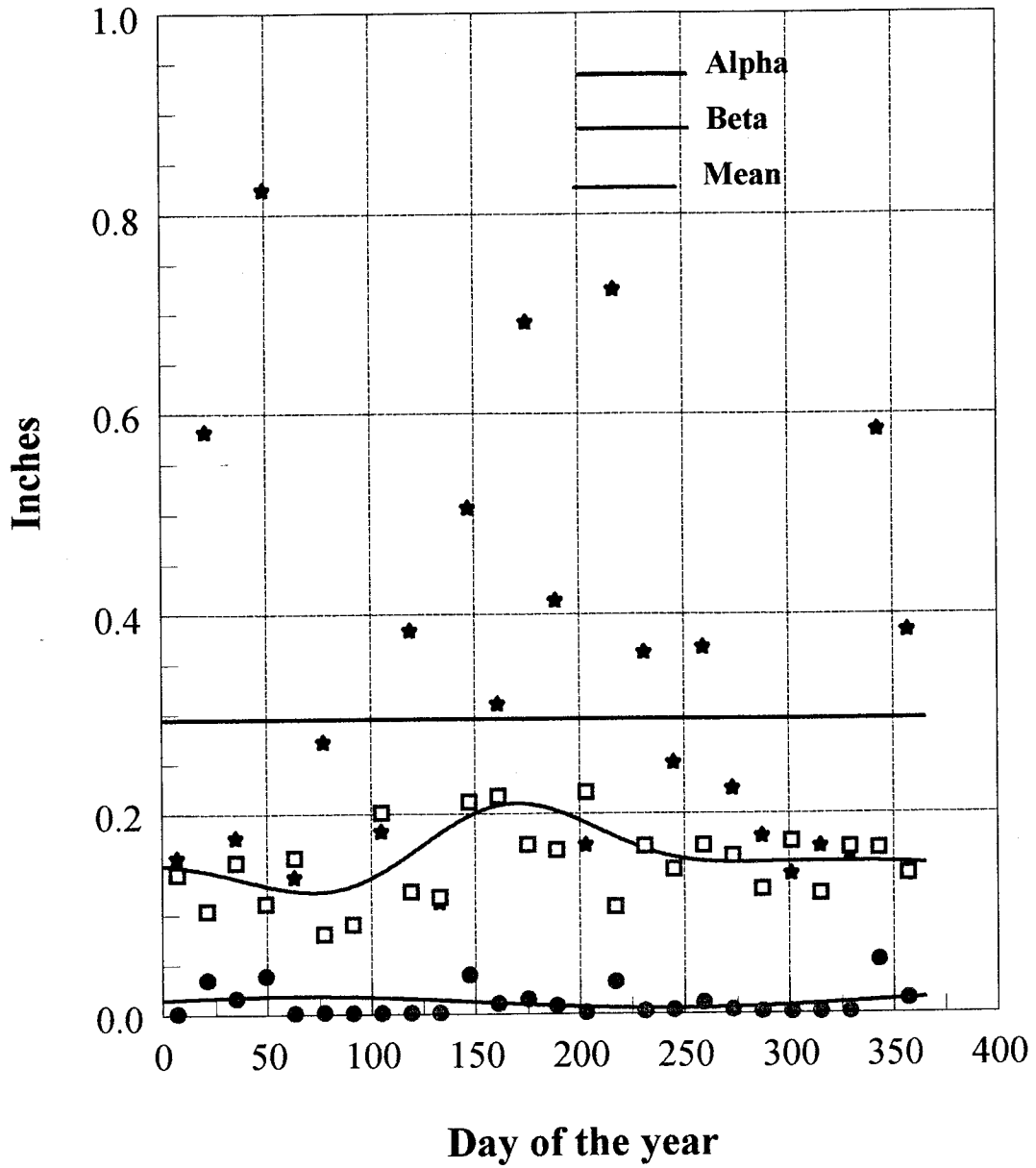
Theoretical and Empirical Accumulated Wet days and Precipitation - Las Vegas



File: VEGC18.pgw
VEGC18.pdw
DAW 1-25-00

Mixed Exponential Parameters Las Vegas, NV

DAW



File: VEGC18PAR.pgw
VEGC18.pdw
DAW 1-25-00

=====
Linear Regression ReportData File Name: C:\consult\swri\CLIMATE\Mepar2.pdw
=====

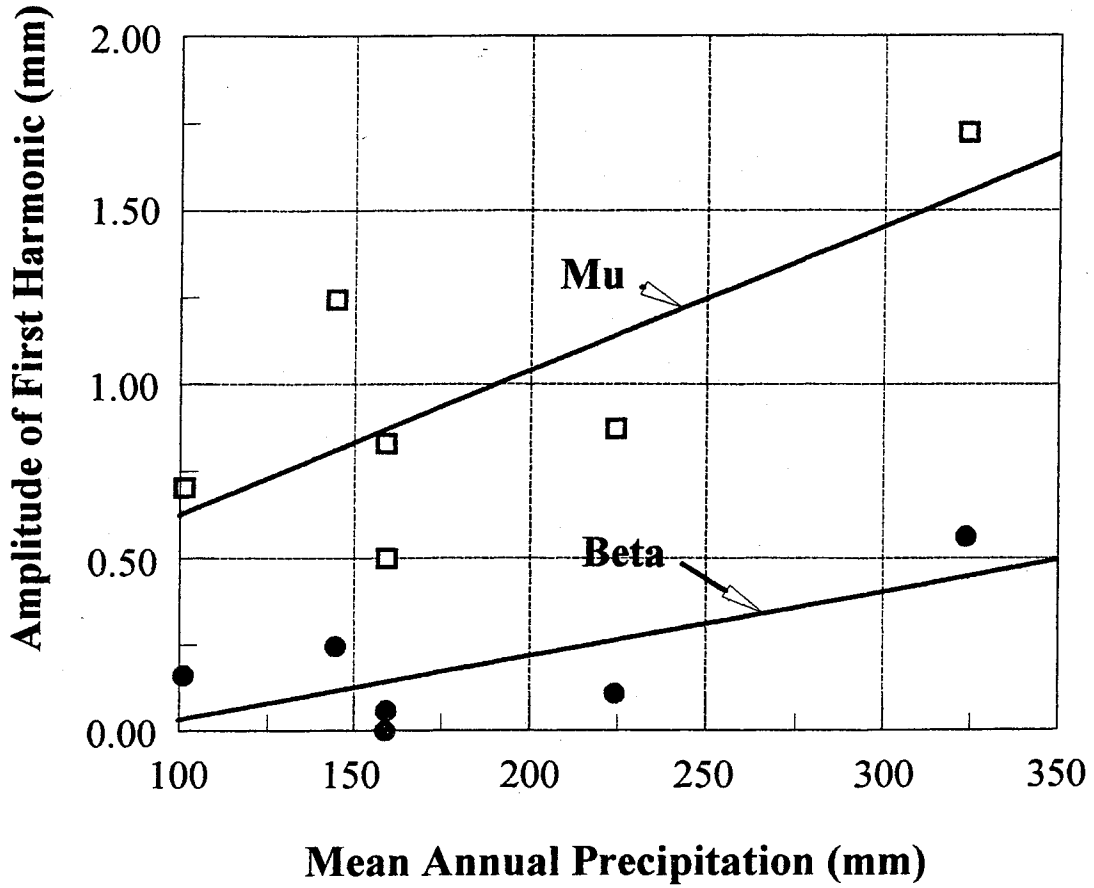
IndVar:	PMM
DepVar:	BC1

Equation: $y=a*x+b$

Parameter a:	0.0018447932
Parameter b:	-0.15146680
Uncertainty da:	0.00088734104
Uncertainty db:	0.17635832
Sum Sqrs:	0.097061768
StdDev:	0.13932822
R-Sq r2:	0.51936326
Correlation:	0.72066862

=====
----Created by David A. Woolhiser with PSI-Plot
----Thu Jan 27 11:02:20 2000
=====

DAW



File: Mepar2.pdw
MEC1B&MU.pgw

DAW 1-27-00

Daw

=====
Linear Regression Report

Data File Name: C:\consult\swri\CLIMATE\Mepar2.pdw
=====

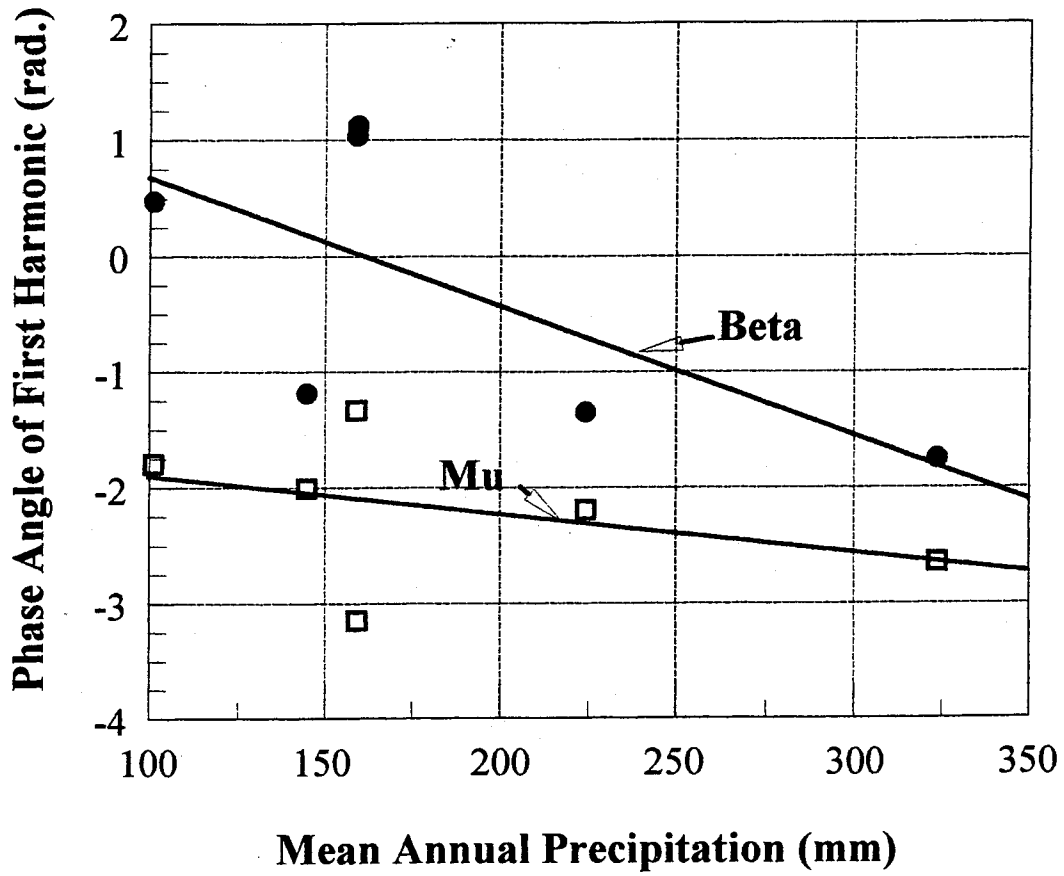
IndVar: PMM
DepVar: MUPHI1 *Ch1*

Equation: $y=a*x+b$

Parameter a: -0.0033165247
Parameter b: -1.56830706
Uncertainty da: 0.0037279367
Uncertainty db: 0.74092443
Sum Sqrs: 1.71318445
StdDev: 0.58535194
R-Sq r2: 0.16518152
Correlation: -0.40642530

=====
----Created by David A. Woolhiser with PSI-Plot
----Thu Jan 27 11:07:18 2000
=====

DAW

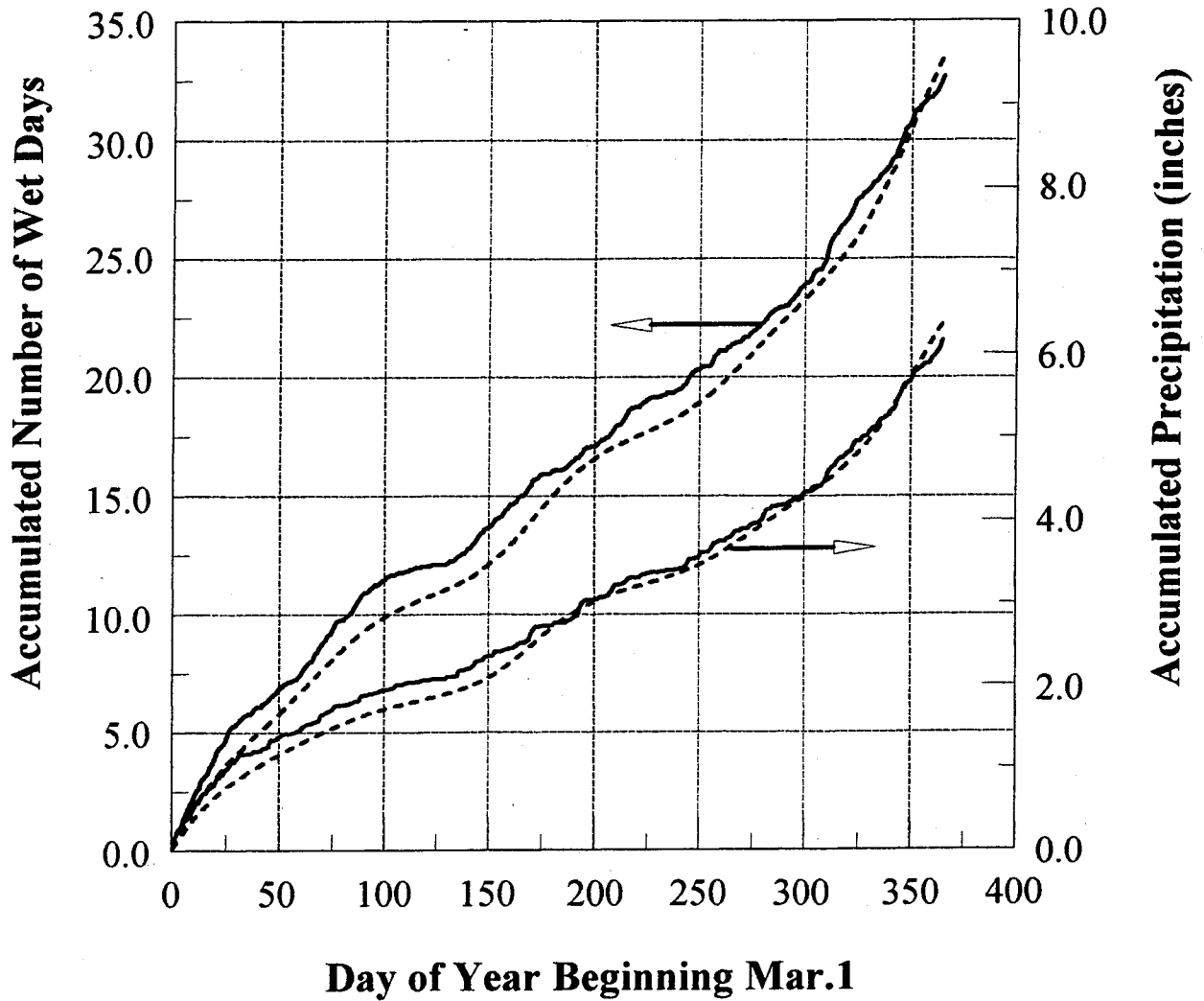


Mepar2.pdw

DAW 1-27-00

MEPHI1B*MU.PGW

Theoretical and Empirical Accumulated Precipitation and Wet Days
Beatty8n Nevada



File: BEAC19ACCUM.PGW
BEAC19.O3
DAW 1-28-00

BEATTY 8N

24 NDD NDW NWD NWW ND NW; # OF PERIODS= 26

24	NDD	NDW	NWD	NWW	ND	NW	# OF PERIODS= 26
228	37	36	34	265	70	.8604	.514
241	33	37	22	274	59	.879	.627
298	16	16	6	314	22		
295	15	17	9	310	26		
277	24	22	13	301	35		
279	23	23	11	302	34		
290	16	17	13	306	30		
312	11	11	2	323	13	.965	0.846
326	3	5	2	329	7	.9909	0.714
312	10	8	6	322	14		
282	22	23	9	304	32		
289	21	19	7	310	26		
299	13	16	8	312	24		
299	16	14	7	315	21		
300	16	15	5	316	20		
294	15	17	10	309	27		
317	10	9	0	327	9		
293	16	18	9	309	27		
298	16	15	7	314	22		
296	19	18	3	315	21		
294	15	16	8	309	24		
283	22	21	10	305	31		
250	30	28	28	280	56	.892	0.5
272	24	26	14	296	40		
253	31	28	22	284	50		
282	28	29	15	310	44		

Draw
1/28/00

only 7 wet days ?

! only 9 wet days ?