

UNITED STATES NUCLEAR REGULATORY COMMISSION

WASHINGTON, D.C. 20555-0001

May 15, 2003

MEMORANDUM TO:

William M. Dean, Assistant for Operations Office of the Executive Director for Operations

FROM:

Robert C. Pierson, Director Division of Fuel Cycle Safety and Safeguards Office of Nuclear Material Safety and Safeguards

Subject: PRESENTATIONS TO RF GOSATOMNADZOR, MAY 26-30, 2003

In accordance with Management Directive 3.9 and subsequent OEDO guidance, information is provided below regarding a presentation to be made while on foreign travel. The information does not involve policy issues. The information is for your transmittal to Commissioner Assistants, for information.

Department of Energy meeting with RF Gosatomnadzor on plutonium disposition Meeting: Place: Moscow, Russia May 19-23, 2003 Dates: Margaret Chatterton, Christopher Tripp Author: "NRC Review of the Mixed Oxide Fuel Fabrication Facility" Title:

ADAMS Accession #:ML031320016

CC: Martin J. Virgilio, NMSS Margaret V. Federline, NMSS Theodore S. Sherr, NMSS

Christopher Tripp, NMSS/FCSS CONTACT: (301) 415-7733

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Place:	Moscow, Russia
Dates:	May 19-23, 2003
Author:	Margaret Chatterton, Christopher Tripp
Title:	"NRC Review of the Mixed Oxide Fuel Fabrication Facility"

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NRC Review of the Mixed Oxide Fuel Fabrication Facility

Meeting with RF Gosatomnadzor May 2003

Margaret Chatterton and Dr. Christopher S. Tripp U.S. Nuclear Regulatory Commission



Workshop Agenda

- Day 1: Introduction and Criticality Safety Concepts
- Day 2: NRC Regulatory Framework
- Day 3: NRC Review of NCS Issues in the MFFF CAR
- Day 4: NRC Review of Validation/Subcritical Margin
- Day 5: Status of NRC Review and Future Topics



Day 1 Agenda

- Introduction to NRC Regulations
- Nuclear Criticality Safety (NCS) Basic Concepts
- Aspects of Plutonium / Mixed Oxide (MOX)
- Dominant NCS Risks and Issues
- End-of-day Question-and-Answer Session



- Definition: Nuclear criticality safety (NCS) is the prevention or termination of inadvertent nuclear chain reactions for fissionable material operations in nonreactor environments
- k_{eff} = <u>(neutron production)</u> (total neutron absorption + neutron leakage)
- k_{eff} = 1 Critical
- k_{eff} < 1 <u>Sub</u>critical
- k_{eff} > 1 <u>Super</u>critical



Neutron Production = Neutron Multiplication : (1 Neutron In, More Neutrons Out)



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)

ABSORBED IN NON-FUEL



• Criticality Evaluations:

Uncertainties in

- » Experimental Data
- » Calculations

> Operational Scenarios

- » Normal Conditions
- » Credible Abnormal Conditions



- Process plant criticality accidents:
 - > Aqueous solutions
 - ≻ Pu
 - ≻ HEU
- Criticality yields: approaching 10¹⁸ fissions
- Consequences: acute radiation to workers
- Most recent criticality accident
 - > Japan (1999)
 - ➤ 2 worker fatalities



Decrease in Radiation Dose with Distance from Criticality Accident ~ 3 x 10¹⁷ fissions





Nuclear Criticality Safety Basic Concepts: Analysis Procedure

- Definition of process/operations
- Hazards and scenario development
- Controlled parameters
- Subcritical limits
- Controls
- Management measures



Nuclear Criticality Safety Basic Concepts: Hazards and Scenario Development

- What-If
- What-If Checklist
- Hazard and Operability Analysis (HazOp)
- Failure Modes and Effects Analysis (FMEA)
- Fault Tree Analysis
- Event Tree Analysis



Nuclear Criticality Safety Basic Concepts: Controlled Parameters

- Geometry
- Mass
- Density
- Isotopics
- Reflection
- Moderation

- Concentration
- Interaction
- Neutron absorbers
- Volume
- Heterogeneity
- Process variable



Nuclear Criticality Safety Basic Concepts: Examples of Controlled Parameters







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Nuclear Criticality Safety Basic Concepts: Control Types

- Passive Engineered
- Active Engineered
- Enhanced Administrative
- Simple Administrative



Nuclear Criticality Safety Basic Concepts: Management Measures

- Engineered Controls
 - Configuration Management
 - ➤ Maintenance
 - > Surveillance
 - ➤ Functional Testing...

- Administrative Controls
 - > Training and qualification
 - > Procedures
 - ➢ Postings
 - > Records Management
 - > Audits and Investigation...





Unique Aspects of Pu/MOX Processing

• Plutonium Chemistry:

Effect of Pu chemistry on process flow

Effect of Pu chemistry on system k_{eff}



Unique Aspects of Pu/MOX Processing

Effect of Plutonium Chemistry on Process Flow

> Up to six positive valence states

> Valence depends on acidity, temp, etc.

- > Pu can compound with up to 4 nitrate radicals
- Need to keep Pu out of solvent extraction raffinate stream
- Pu compounds include oxides, oxyfluorides and oxalate-nitrate mixtures



Unique Aspects of Pu/MOX Processing

- Effect of Plutonium Chemistry on System k_{eff}
 - > Neutron absorption by:
 - » Nitrogen
 - » Hydrogen
 - » Fluorine
 - » Oxygen
 - » Carbon
 - Nitrogen absorption can increase allowable limits by factors of three or four
 - > 3 nitrate radicals assumed instead of 4
 - More reactive oxyfluoride compound assumed for mixtures of oxalate and nitrate



Unique Aspects of Pu/MOX Processing: Plutonium/MOX Isotopics (Assay) Control

Isotopic mixture that has to be controlled:

Uranium Processing Plant	MOX Plant
²³⁵ U/U	²³⁹ Pu
	²⁴⁰ Pu
	²⁴¹ Pu
	²³⁵ U/U
	U/Pu

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Unique Aspects of Pu/MOX Processing: Fission Cross Sections





Unique Aspects of Pu/MOX Processing: Plutonium Physical Characteristics

Density Control

- PuO₂ lower density (more porous) than UO₂.
- After PuO₂ and UO₂ blended, difficult to predict final density.

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Dominant NCS Risks and Issues

- Historic risks
- Bounding assumptions
- Isotopic Blending of PuO₂ and UO₂
- Limited US industry experience
- Meeting performance criteria
- Criticality code validation



- 21 of the 22 total known world process nuclear criticality accidents occurred with HEU or Pu in solutions or slurries*
- Aqueous polishing (AP)
 - > Dissolution
 - ➢ Purification
 - Conversion

^{*} TP McLaughlin, et al, A Review of Criticality Accidents, 2000 Revision, LA-13638, May 2000



Overview of Aqueous Polishing Process





29 September 1999 Dissolution Mishap at the JCO





• MOX Process (MP)

Powder blending

- Lesser risks
 - Pellet production
 - ≻ Rod production
 - > Fuel assembly production



Overview of the MOX Process (MP)



Assemblies





Rodtay



	Low H/(U+Pu)	High H/(U+Pu)
Mass	6.4 kg MOX @ H/(U+Pu) ~ 100	60 kg MOX @ H/(U+Pu) ~ 0.1
Volume	17L MOX @ H/(U+Pu) ~ 40	1927L MOX @ H/(U+Pu) ~ 0.1

Moderation Spans broad spectrum, from:

- Damp, H/(U+Pu) ~ 0.1 (~0.33 wt% H₂O)
- Solutions, H/(U+Pu) 1500



MOX Mass (kg) versus H/U+Pu



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• Particularly sensitive operations include:

> Any operation that can lose geometry/volume control

- > Any operation that can lose moderation control
- Ancillary equipment/operations that could accumulate critical quantities



- Areas of highest NCS risk
 - > Aqueous Polishing
 - > Powder Handling
 - ➢ Blending
- Based upon "Unmitigated Risk"



Dominant NCS Risks and Issues

- Isotopics:
 - > Analysis based on bounding assumptions
 - Changes during MOX Process (blending)
- Density:
 - > Initially assumed full theoretical (11.46 g/cm³)
 - > Changes several times during process



Dominant NCS Risks and Issues: Effect of Isotopic Blending of PuO₂ and UO₂

- Relative isotopics important to NCS
- Credited downstream of Blending
- Homogeneity of mixed oxides very important


Dominant NCS Risks and Issues: Limited US Industry Experience

• Reprocessing:

- > Never had a MOX economy
- Progress stopped mid-1970's (Presidential and Congressional decision to stop support of AGNES plant in Barnwell, SC)
- > Closure in mid-1980's of Idaho Chemical Processing Plant

• Pu processing:

- Limited development work stopped mid-1970's
- > Some MOX fuel burned in US reactors



Dominant NCS Risks and Issues: Meeting Performance Criteria

- Integrated Safety Analysis (NUREG-1513 and NUREG-1718)
- Application of the Double Contingency Principle (10 CFR Parts 70.4 and 70.64(a)(9))



Dominant NCS Risks and Issues: Criticality Code Validation

- Paucity of available experimental data
- Loss of experimental facilities
- Need for:
 - Increased flexibility
 - > Increased fissile load
- Public attention to justifying margins of safety
- As operations move closer to upper subcritical limit (USL), scrutiny increases



Dominant NCS Risks and Issues: Criticality code validation

- Validation Requirements:
 - Determine calculational bias
 - > Determine uncertainties
 - > Establish area of applicability
 - > Establish margin of subcriticality
 - > Prepare a written report

(Reference: Section 4.3 of ANSI/ANS-8.1 - 1998.)



End-of-Day 1 Questions-and-Answers Session

COVER SHEET FOR CORRESPONDENCE

NRC FORM 8C (7-94) NRCMD 3.57

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NRC Review of the Mixed Oxide Fuel Fabrication Facility

Meeting with RF Gosatomnadzor May 2003

Margaret S. Chatterton U.S. Nuclear Regulatory Commission



Day 2 Agenda NRC Regulatory Framework for NCS

- 10 CFR 70, Domestic Licensing of Special Nuclear Material
- NUREG-1718, Standard Review Plan for MOX Fuel Fabrication Facility
- American National Standards Institute (ANSI) / American Nuclear Society (ANS) Series 8 Standards
- NRC Regulatory Guide 3.71, Nuclear Criticality Safety Standards for Fuels and Materials Facilities
- Regulatory Differences Between MFFF and Traditional U.S. Fuel Cycle Facilities Licensed by NRC
- End-of-day Question-and-Answer Session



NRC Regulations Pertaining to MFFF

- 70.22 Contents of Applications
- 70.23 Requirements for the Approval of Applications
- 70.24 Criticality Accident Requirements
- 70.61 Performance Requirements
- 70.62 Safety Program
- 70.64 Basic Design Criteria
- 70.65 Integrated Safety Assessment
- 70.72 Change Process



Nuclear Criticality Safety Regulations

• Criticality Accident Requirements: 70.24

• Performance Requirements: 70.61(b) and (d)

• Baseline Design Criteria: 70.64(a)(9)



70.24 Criticality Accident Requirements

- Apply if amount of SNM exceeds
 - ≻ 700 gm Uranium 235
 - ≻ 450 gm Plutonium
- Qualified monitoring system
 - > Gamma or neutron-sensitive radiation detectors
 - > Audible alarms
 - > Capable of detecting a criticality
 - > Coverage by two detectors
- Emergency Procedures



70.61 Performance Requirements

- 70.61(b) Criticality is Highly Unlikely
- 70.61(d) Under Normal and Credible Abnormal Conditions
 - > All nuclear processes are subcritical
 - > Including use of an approved margin of subcriticality
- Preventive controls and measures
 - Primary means of protection



70.64 New Facility and Process Requirements

• 70.64(a)(9) Double Contingency Principle

≻ Two

> Unlikely

> Independent

> Concurrent

- Changes in process conditions
- > Before criticality possible



Standard Review Plan (SRP) for the Review of an Application for a Mixed Oxide (MOX) Fuel Fabrication Facility: NUREG-1718

Guidance for review and evaluation

> Construction

> Operational applications

- » Possess special nuclear material (SNM)
- » Use special nuclear material (SNM)
- License amendments
- > License renewal applications



SRP for the Review of MFFF: NUREG-1718

- Ensures the quality and uniformity
- Improves communication and understanding of review and regulatory process
- Regulatory guidance for applicants and staff



Contents of the SRP for MOX Facilities

- Purpose of the review
- Responsibility for the review
- Areas of review
- Acceptance criteria
- Review procedures
- Evaluation findings
- References



SRP for the Review of MFFF: NUREG-1718

• Purpose of Review

> Organization for implementing NCS program

- NCS program to ensure safe operation of facility
- > Adequate controls & limits on parameters
- > Accident sequences
 - » Identified in the Criticality Safety Evaluations (CSEs)
 - » Documented in the (Integrated Safety Analysis) ISA



SRP for the Review of MFFF: NUREG-1718

- Responsibility for Review
- Reviewers
 - ➢ Nuclear process engineer
 - Chemical safety reviewer
 - > Project manager and fuel cycle inspector



SRP for the Review of MFFF: Areas of Review

- Organization and Administration
 - > Administrative organization of NCS program
 - » Authority
 - » Responsibilities
 - » Experience and education required

Management Measures

- Management functions SRP Sections 15.1-15.8
- Implementing requirements
 - » 10 CFR 70.64 (Baseline Design Criteria)
 - » 10 CFR 70.72 (Facility Change and Change Process)



SRP for the Review of MFFF: Areas of Review (continued)

- Technical Practices
 - NCS controls and limits
 - > Adequate safety margin for limits on controlled parameters
 - NCS methods validated
 - > Identification of NCS controls for each parameter
 - > Safety basis documentation
 - ➤ Section 5.3 (ISA Summary) related to NCS
 - Operability of Criticality Accident Alarm System (CAAS) and emergency response procedures



SRP for the Review of MFFF: NUREG-1718

- Acceptance Criteria
- Regulatory Requirements 10 CFR Part 70

>70.22, 70.24, 70.61, 70.62, 70.64, 70.65, 70.72, and Appendix A

Regulatory Guide 3.71

"Nuclear Criticality Safety Standards for Fuels and Materials Facilities"



American National Standards Institute/American Nuclear Society 8 Series Standards (ANSI/ANS-8.xx)

- Consensus Standards Specific to Criticality Safety
- Developed by Working Groups

> Industry Representatives

- » NRC Licensees
- » DOE Facilities

Regulatory Representatives

- » NRC
- » DOE



ANSI/ANS-8 Standards

• ANS Standards Subcommittee 8, "Operations with Fissionable Materials Outside Reactors"

National Standards

> Prevention and mitigation of criticality accidents

Standards approved by

> ANS Committee N-16 (Nuclear Criticality Safety)

> American National Standards Institute (ANSI)



ANSI/ANS-8 Standards

- NCS Standards contain
 - > Introduction
 - > Scope
 - > Definitions
 - ≻ Criteria
 - ≻ References
 - > Appendices
 - > Tables
- Standards reviewed every 5 years



ANSI/ANS-8 Standards

- Key words
 - > Shall = requirement
 - > Should = recommendation
 - > May = permission



- ANSI/ANS-8.1-1983 (Reaffirmed in 1988), "Nuclear Criticality Safety in Operations with Fissionable Materials Outside Reactors"
- ANSI/ANS-8.3-1997, "Criticality Accident Alarm System"
- ANSI/ANS-8.5-1996, "Use of Borosilicate-Glass Raschig Rings as a Neutron Absorber in Solutions of Fissile Material"
- ANSI/ANS-8.6-1983 (Reaffirmed in 1995), "Safety in Conducting Subcritical Neutron-Multiplication Measurements In Situ"





- ANSI/ANS-8.7-1998, "Guide for Nuclear Criticality Safety in the Storage of Fissile Materials"
- ANSI/ANS-8.9-1987 (Withdrawn 2001), "Nuclear Criticality Safety Criteria for Steel-Pipe Intersections Containing Aqueous Solutions of Fissile Materials"
- ANSI/ANS-8.10-1983 (Reaffirmed in 1999), "Criteria for Nuclear Criticality Safety Controls in Operations With Shielding and Confinement"
- ANSI/ANS-8.12-1987 (Reaffirmed in 2002), "Nuclear Criticality Control and Safety of Plutonium-Uranium Fuel Mixtures Outside Reactors"



- ANSI/ANS-8.15-1981 (Reaffirmed in 1995), "Nuclear Criticality Control of Special Actinide Elements"
- ANSI/ANS-8.17-1984 (Reaffirmed in 1997), "Criticality Safety Criteria for the Handling, Storage, and Transportation of LWR Fuel Outside Reactors"
- ANSI/ANS-8. 19-1996, "Administrative Practices for Nuclear Criticality Safety"
- ANSI/ANS-8.20-1999, "Nuclear Criticality Safety Training"



- ANSI/ANS-8.21-1995 (Reaffirmed in 2001), "Use of Fixed Neutron Absorbers in Nuclear Facilities Outside Reactors"
- ANSI/ANS-8.22-1997, "Nuclear Criticality Safety Based on Limiting and Controlling Moderators"
- ANSI/ANS-8.23-1997, "Nuclear Criticality Accident Emergency Planning and Response"



US NRC REGULATORY GUIDE 3.71: Nuclear Criticality Safety Standards for Fuels and Material Facilities

- Purpose
 - Provide guidance

> Describe procedures

- Endorsement of specific standards
- Consolidates and replaces previous guidance
- Procedures & methodology generally acceptable



- Not substitute for NCS analysis
- Commitment to standard
 - > All operations in accordance with requirements
 - Recommendations not followed; then justification



- Deviations/Modifications from Standards
 > ANSI/ANS-8.1 Section 4.3.6 validation details
 - » Adequacy of margins of subcriticality
 - Bias
 - Criticality parameters
 - » Demonstrate range of variables
 - » Demonstrate trends in bias for extensions



Deviations/Modifications from Standards

> ANSI/ANS-8.3

- » Section 4.2.1
 - Standard evaluation
 - Regulatory Guide requires
- » Section 4.5.1
 - Standard 1 detector
 - Regulatory Guide 2 detectors
- » Section 5.6
 - Standard documenting different minimum accident
 - Regulatory Guide specifies system requirements



- Deviations/Modifications from Standards
 > ANSI/ANS-8.10
 - » Section 4.2.1
 - Standard source strength and release estimates by analysis
 - Regulatory Guide specifies source strength and releases; less conservative requires justification

> ANSI/ANS-8.17

- » Standard allows burnup credit
- » Regulatory Guide burnup credit only by measurement



Regulatory Acceptance Criteria

- Organization and Administration
 - > Commits to ANSI/ANS 8.1 and 8.19
 - NCS independent of operations
 - Commits to NCS postings
 - Commits to Policy, "All personnel shall report defective NCS conditions to the NCS function, directly or through a designated supervisor, and take no further action not specified by approved written procedures until NCS has analyzed the situation."
 - > Commits to policy of instilling a safety ethic



Regulatory Acceptance Criteria (Continued)

Management Measures

≻ Training

- » ANSI/ANS 8.19 and 8.20
- » Process variables if credited for NCS
- » Postings

> Procedures

- » ANSI/ANS 8.19
- » Postings and procedures controls


Management Measures

> Audits and Assessments

- » ANSI/ANS 8.19
- » Annual reviews
- » Committee to conduct and document NCS walkthroughs
 - Weaknesses
 - Corrective actions



Technical Practices

> Analytical Methodology

- » ANSI/ANS 8.1
- » Intent of Regulatory Guide 3.71 on validation report
 - Adequacy of subcritical margin
 - Determination of area of applicability (AOA)
 - Use of codes within AOA
 - Justification for extensions



- Validation Report
 - > Documented, reviewed, and approved
 - > Contents
 - » Description of theory
 - » Description of AOA range of values
 - » Description of computer codes, assumptions, techniques
 - » Description of verification of math operations
 - » Description of benchmarks
 - » Description of bias, uncertainty in bias, uncertainty in methods
 - » Description of software and hardware



Validation Report

> In configuration management program

- Commits to perform NCS evaluations
- Commits to assuming credible optimum conditions
- Commits to variability and uncertainty in setting safety limits



- Additional technical practices
 - CSEs main source of adequate criticality controls
 - >CSEs provide safety basis
 - Controls from CSEs are Items Relied on for Safety (IROFS) (ISA Summary)
 - Single NCS control maintains 2 or more parameters considered only 1 component for DCP
 - Commits to "No single credible event or failure could result in a criticality accident."
 - Commits to preferred use of passive engineered controls



- Additional technical practices (continued)
 - Controls and control parameters into management measures
 - Commits to describing control parameters for each NCS process
 - > Parameters controlled by measurement
 - » Reliable methods
 - » Reliable instruments



- Methods of NCS control
 - Passive geometry preferred
 - Commitment to passive geometry whenever possible
 - > Justification if not passive geometry
 - Controls to establish limits = IROFS
 - > Interactions fully evaluated



- Mass control
 - > Mass limits for given weight percents
 - » Weight of material
 - » Physical measurements
 - > Theoretical densities used
 - > Measurements = instruments subject to Quality Assurance (QA)
 - Overbatching possible; single batch limited to largest overbatch safely subcritical
 - > No overbatching; single batch limited to safely subcritical



- Geometry control
 - > All dimensions verified
 - > All credible transfers to unfavorable geometry
 - » Evaluated
 - » Controls (IROFS)

Large single units - conservative margin of safety
Mechanisms for change evaluated



- Density control
 - Process variable controls = IROFS
 - Process characteristics controlled
 - Measurements = instruments in QA



- Isotopics control
 - Uranium enrichment, Plutonium concentration, ratio of Pu to U
 - Different isotopic mixtures
 - » Label and segregate
 - » Labels & postings distinctive and clear
 - » Based on dual independent sampling and analysis
 - > Measurements = instruments in QA



- Reflection control
 - > Wall thickness and reflecting material bounding
 - > Minimal equivalent 1 inch tight filling water jacket
 - » account personnel
 - » transient incidental reflection
 - » justified for less
 - Testable personnel barrier if loss of reflection control = criticality
 - > Full water reflection = 12 inches water



- Moderation control
 - ➤ Commits to ANSI/ANS 8.22
 - Process variable controls identified as IROFS
 - Measurements = instruments in QA
 - Design sufficient to preclude moderation
 - > Sampling dual independent
 - Firefighting procedures restrict moderators
 - > Limits on firefighting agents in CSE and ISA
 - Favorable geometry drains



- Concentration control
 - Process controls identified as IROFS
 - Controls to preclude higher concentration
 - ➤ Tanks closed and locked
 - > Sampling dual independent
 - If concentration only control for unfavorable geometry
 - » Robustness of controls when transferring
 - » Precautions to avoid precipitating agents
 - Surveillance ensures controls effectiveness
 - Measurements = instruments in QA



Interaction control

Engineered design with minimal spacing

- » Structural integrity
- » Periodic inspections

> Spacing by procedures

- » Postings
- » Visual indicators painted lines
- » Justification required

Follow ANSI/ANS 8.7



- Neutron absorber control
 - Commits to ANSI/ANS 8.5 for Borosilicate-glass Raschig rings
 - > Commits to ANSI/ANS 8.21 for fixed absorbers
- Heterogeneity control
 - > Process variable controls IROFS in CSE and ISA
 - > Computer models validated with benchmark experiments
 - Assumptions on physical scale based on observed physical characteristics



• Volume control

> Geometric devices restrict SNM volume

- > Engineering devices limit SNM accumulation
- Measurements = instruments in QA
- > Volume limited to % of critical volume
 - » Spherical geometry
 - » Optimal concentration
 - » Full water reflection



- Subcriticality of operations
 - Commits to ANSI/ANS 8.1,8.5,8.7,8.9,8.10, 8.12, 8.15, 8.21 and 8.22
 - Justification for minimal subcritical margin
 - » Normal conditions
 - » Credible abnormal conditions
 - > Rigorous definition of abnormal conditions
 - Less conservative margin commensurate with & offset by unlikelihood
 - Commits to K-subcritical = 1.0 bias margin



Subcriticality of operations (continued)

Commits to control parameter operating limits

- » Adequate margin
- » Studies of sensitivity
- > Subcritical limit calculations with AOA of method
- Documentation in CSE
- > Benchmark experiments similar to applications
 - » Physical characteristics
 - » Neutronic characteristics



Baseline design criteria

Commits to double contingency principle

- > "Unlikely" consistent with ANSI/ANS 8.1
- > 2 parameter control preferred
- > Means for detecting and correcting failures
- > "Highly unlikely"
 - » Time interval to detect
 - » Time interval to correct failure



SRP for the Review of MFFF

- Review Procedures
 - ≻ Two step review process
 - » Construction Approval
 - » License to Possess and Use SNM



SRP for the Review of MFFF

- Acceptance review
 - Primary reviewer determines if application addresses areas of review
- Safety evaluation
 - > Against acceptance criteria
 - > Identify and resolve all issues
 - » Requests for Additional Information (RAIs)
 - » Responses to RAIs

> Document findings in Safety Evaluation Report



Regulatory Differences Between MFFF and Other Fuel Cycle Facilities Licensed by NRC

- New facility licensed under new Part 70
- Plutonium facility
 - ≻ 70.22(f)
 - ≻70.23 (a)(8) and (b)
 - » Construction approval



NRC Regulatory Framework

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End-of-day Questions-and-Answers Session

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NRC Review of the Mixed Oxide Fuel Fabrication Facility

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Dr. Christopher S. Tripp U.S. Nuclear Regulatory Commission



Day 3 Agenda

NRC Review of NCS Issues in the MFFF CAR

End-of-day Question-and-Answer Session



Overview of Current Fuel Cycle



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Process Familiarization

- Construction application for MOX had several unique aspects:
 - > Little regulatory experience with MOX
 - First new application under 10 CFR Part 70
 - Unique aspects related to Pu-processing facility (70.23(b)).
 - > Unique aspects related to new facility (70.64).



Process Familiarization

- Training on MOX process at Los Alamos National Lab (LANL)
 - > Pu metallurgy
 - > Pu Chemistry
 - ➢ Fire Protection
 - Processing Methods
 - Confinement/Ventilation
 - > Radiological, Chemical, and Nuclear Safety
- Site visits by technical reviewers, managers, and Project Manager
- Briefing by COGEMA on plans for U.S. facility



"Americanization" of MOX Fuel Cycle

- U.S. MOX Fuel Fabrication Facility (MFFF) a combination of following two processes:
 - LaHague: Aqueous Polishing of Spent Nuclear Fuel, Immobilization
 - MELOX: Fabrication of purified PuO2 powder into MOX assemblies
- Use of weapons-grade vs. reactor-grade Pu:
 - > Advantages: Fewer impurities, no need for hot cells & immobilization
 - > Disadvantage: Less favorable isotopic mix for nuclear safety



Comparison of Weapons-Grade and Spent Fuel





Design Bases for the MFFF

- Fuel Facility Licensing (Part 70)
 - > 50.4 definition of "Design Bases" not applied to most FF
 - > Baseline Design Criteria (BDC) apply to new FF
 - Part 70 Performance-Based
 - > Unique processes/designs
 - > Unique license conditions
 - > No Technical Specifications
 - ➢ No standard failure database



Design Basis of the MFFF

- "Reasonable assurance": Not possible to guarantee acceptability without detailed process-specific information
- Burden on applicant to provide acceptable design at the OL stage. Must be in conformance with approved design bases
- Design basis = basis for the design. That information needed to provide reasonable assurance of an acceptable design



Design Bases of the MFFF

- Proposed and justified design bases based on regulations
- Agreed upon in public meeting with DCS held January 2001
- 10 design bases for nuclear safety
- Mix of programmatic and technical design criteria (mostly qualitative)



Design Bases Functions and Values

- Adherence to the DCP
- Required for new facilities
- Long a cornerstone of the U.S. approach to nuclear safety
- Similar to single-failure criterion:
 - > Two or more failures needed for criticality accident
 - "Unlikely" (discussed in detail later)
 - > Independent (statistically, $P_{AB} = P_A P_{AIB} = P_B P_{AIB}$)
 - Concurrent (not simultaneous occurrence; simultaneous failed state)


- Maximum k-effective, methodology for determining Upper Subcritical Limits
- Methodology for determining bias and uncertainty (validation)
- Choice of administrative margin
- USLs for normal and credible abnormal conditions



- Subcritical under normal and credible abnormal conditions
- Tied to specification of USLs
- Tied to DCP: "credible abnormal" = 1 contingency/control failure in accordance with DCP
- Requires worst-case upsets considered, shown subcritical

,	Controlled Parameters	Uncontrolled Parameters
Normal	At safety limits	Worst-case
Abnormal	One parameter as worst-case at a time Rest at safety limits	Worst-case
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 Dominant controlled parameters for each major process step





- Dominant controlled parameters for each major process step
- Parameter Information contained in Tables 6-1 (AP) and 6-2 (MP)
- Reviewed to confirm that an appropriate design strategy used
- Bounding/input assumptions reviewed in CAR
- Subcritical limits derived during design reviewed in LA



- Preferred* design approach/control hierarchy
- Passive engineered (PEC)
- Active engineered (AEC)
- Enhanced administrative (EA)
- Simple administrative (SA)

^{*} Expected in a majority of cases — deviations should be the exception, not the rule.



• Controlled parameter

> Geometry/volume (with or without neutron absorber)

- ≻ Mass
- ➤ Moderation

> Other controlled parameters...

- Double contingency implementation
 - Multi-parameter control (two or more changes in system parameters)
 - Single-parameter control (two or more changes in one system parameter)



- Criticality accident alarm system (CAAS)
- Management measures/safety grades
- Organization and administration of NCS Program:
- Roles and responsibilities during design phase
- Education/experience for NCS positions
- Key elements/functions of program



- Technical practices, related to:
- Deriving subcritical limits
- Factors to be considered for different control modes
- Compliance with ANSI/ANS-8 Series standards
- Documentation of criticality evaluations



- Approach to balancing fire and nuclear safety risks:
- Fire impact on nuclear safety
- Nuclear safety impacts on fire
- ISA will consider cross-discipline safety risks; overall risk to workers must be minimized.
- Moderating fire suppression agents will not be used in moderation-control areas



Chronology of NRC Review

- Determination of design bases in each safety discipline – Jan 2000
- Review of CAR against acceptance criteria in the SRP – Feb 2001
- Formulation of questions (screened for relevance to design basis)
- Issuance of request for additional information (RAI) – June 2001
- Receipt of RAI responses August 2001



Chronology of NRC Review (continued)

- Formulation of additional questions based on responses
- Communication of additional questions by telephone calls and meetings
- Receipt and review of subsequent responses in "clarification letters" – Nov. 2001 – March 2002
- Writing/issuing the draft safety evaluation report (SER), including categorizing remaining questions into a discrete list of open issues - Apr 2002



Chronology of NRC Review (continued)

- Telephone calls and meetings to resolve open issues
- Review of validation report
- Review of revised CAR Oct 2002
- Telephone calls and meetings to resolve open issues
- Revised validation reports submitted Jan 2003
- Writing and issuing revised draft SER Apr 2003



- CAR submitted February 2001
- Followed SRP format (August 2000)
- Organization and Administration
 - Location of Nuclear Safety organization in corporate structure
 - > Roles and responsibilities
 - > Education and experience levels for NCS positions



- Main issues with Organization/administration:
 - > Roles and responsibilities originally only defined for the operations phase
 - Little justification given for experience levels of NCS positions
 - > No mention of specific MOX/Pu experience (NCS-1)



- Management Measures for the MFFF (Chapter 14)
 - Configuration Management
 - ➤ Maintenance
 - > Training
 - > Procedures
 - > Audits/Assessments
 - > Incident Investigation
 - > Records Management



- Configuration Control
 - > Control of safety basis documents
 - > Control of process equipment
 - > Control of safety controls
 - Includes <u>change control</u> ensures changes are not made that invalidate safety basis; compliance of "asbuilt" process with safety basis



Importance of Maintaining Configuration Control

Ex: 1999 Tokai-mura criticality accident



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Regulatory Role of Validation Reports

- SRP Section 6.4.3.3.1: "As part of providing reasonable assurance that an adequate margin of subcriticality has been provided...the applicant has, at the facility, a documented, reviewed, and approved validation report...The validation report should contain the following..."
 - Description of the theory of the methodology
 - > Description of the area(s) of applicability (AOA)
 - Description of benchmark experiments
 - Bias and uncertainty in: bias, methodology, data, and margin of subcriticality



Regulatory Role of Validation Reports (continued)

- Validation report submitted separately from CAR. Schedule:
 - > Part I: June 2001
 - Revised Part I and Initial Part II: Dec 2001
 - Revised Parts I and II, Initial Part III: Jan 2003
- Plant is divided into 5 different AOAs
 - > AOA(1): Pu nitrate solutions
 - > AOA(2): MOX fuel pellets, rods, and assemblies
 - > AOA(3): PuO2 powder
 - > AOA(4): MOX powder
 - > AOA(5): Pu solution compounds (oxalates, fluorides, etc.)



- AOA addressed by the report
- Description of the calculational method:
 - > Computer code and version (code, cross section libraries)
 - Cross-section libraries to be used
 - > Hardware platform
- Description of the code validation methodology
- Description of anticipated MOX design applications covered by the report



- Description of benchmark experiments
- Analysis of the validation results:
 - Calculated k-eff and standard deviations
 - Results of the statistical methodology
 - Result of trends to determine larges bias/uncertainty across the AOA
 - Determination of the USL
- Justification of the chosen "administrative margin"





- Identify and Characterize Design Applications
 - Described chemical form, reflection, moderation, isotopic range, density, geometric shape, neutron energy by process area
 - > Described for anticipated normal and abnormal conditions
- Select and Group Benchmark Experiments
 - Generally from the International Handbook of Criticality Safety Benchmark Experiments (ICSBEP) Handbook
 - Choose systems with similar physical and neutronic characteristics



- Code Validation Methodology
 - > NUREG/CR-6361 contains two statistical methods
 - Statistical analysis—ORNL code USLSTATS
 - > Both methods require normally distributed data
 - If <25 benchmarks, statistical techniques cannot be used



- Method 1: "Confidence Band with Administrative Margin"
 - Linear least-squares approach to calculate bias
 - Constant width confidence band at 95% confidence level
 - Arbitrary administrative margin ?k_m



 $W = \max(w(x)|x_A \leq x \leq x_B)$

$USL_1 = 1 + \beta(x) - \Delta k_M - W$

1





- Method 2: "Single-Sided Uniform Width Closed Interval Approach/Lower Tolerance Band"
 - Combined lower tolerance band with subcritical margin
 - Determines tolerance band

 $USL_2 = 1 + \beta(x) - C_{\alpha/p}S_p$



 S_k^2 = variance of regression fit (without variance) σ_i^2 = variance of individual data point (within variance) P = proportion of all future critical calculations (99.5%) $\dot{\alpha}$ = confidence (95%) $G_{\alpha P}$ = statistical multiplier



.

:



- Upper Safety Limit USL-2 normally significantly lower than USL-1 without additional margin ?k_m
- USLSTATS allows user to select administrative margin (Method 1)
- Necessary but not sufficient test for acceptability of ?k_m:

USL-1 (with margin) < USL-2



 Non-normally distributed data: Non-Parametric Margin (NPM)

> Confidence β that a fraction q of critical systems above limit:

 $\beta=1-q^{N}$ (N data points)

 \succ Lowest k-effective in data set used, with margin based on β

- If k-eff of experiment is not exactly 1, calculated value of k-eff is normalized to k=1
- Positive corrections to the bias not allowed



- Bias:
 - Determined as function of most important parameters of the system
 - > Includes:
 - Neutron energy (Energy of Average Lethargy Causing Fission, EALF)
 - » Moderation (H/X or v^m/v^f)
 - » ²⁴⁰Pu content
 - » Pu/(U+Pu) content



- Justification of administrative margin used:
 - > ?k_m=0.05 assumed for all cases
 - Fuel cycle and nuclear industry practice (comparison of licensing basis across NRC licensees and DOE facilities)
 - Comparison of statistical methods. USL-1 (with 0.05) < USL-2</p>



<u>Choice of the minimum subcritical margin</u> ?k_m

> Wide variation in industry, little guidance

Compared MOX plant to HEU facilities

- » HEU & Pu plants show high sensitivity of k-eff to changes in underlying data, system parameters
- » Unknown or unquantified uncertainties can have large impact on bias
- » MOX-portion of plant (i.e. <6.3wt% Pu) was more similar to LEU plants</p>



Licensee/Certificate Holder	Normal Conditions	Credible Abnormal Conditions
High Enriched Uranium Facilities		
BWXT Lynchburg, VA	K ≤ 0.94 (≤ 10wt% U-235); ≤ 0.92 (> 10wt% U-235)	K ≤ 0.97 (≤10wt% U-235); ≤ 0.95 (>10wt% U-235)
NFS Erwin, TN	K + 2σ - bias ≤ 0.90	K + 2σ - bias ≤ 0.95
Gaseous Diffusion Plant Facilities		
USEC Paducah, OH	K ≤ 0.9534 (includes bias, uncertainty, ∆k _m)	Same as normal
USEC Portsmouth, OH	$K \le 0.9605$ (includes blas, uncertainty, Δk_m)	Same as normal
Low Enriched Uranium Facilities		
Framatome ANP Lynchbrug, VA	K + 2σ - bias ≤ 0.87	K + 2σ - blas ≤ 0.95
Framatome ANP Richland, WA	$K = K_{calc} - 2\sigma - blas - 0.05$	K = K _{cale} - 2σ - bias - 0.03
Global Nuclear Fuels Wilmington, NC	K + 3σ - bias ≤ 0.97	Same as normal
Westinghouse Columbia, SC	K + 2σ + blas + uncertainty ≤ 0.95	$K + 2\sigma + blas + uncertainty \le 0.98$
Westinghouse Hematite, MO	K ≤ 0.95 (includes blas and uncertainty)	Same as normal



- ?k_m = 0.05 acceptable for finished MOX (AOA(2)):
 - > Low ²³⁹Pu content (lower sensitivity)
 - > MOX fuel neutronically well-characterized for use in reactors
 - > Material inherently low-risk due to fixed configuration
 - Chosen benchmarks unusually close in terms of configuration to anticipated applications (fuel rod lattices)
 - > Most of these benchmarks are well-moderated
- ?k_m = 0.05 accepted for abnormal case
- Lower normal case limit deemed appropriate, margin depends on sensitivity of system changes in k-eff



- Why arguments for choosing subcritical margin not accepted by NRC:
 - Historical practice HEU facilities, most similar to most of MOX (lower limit in normal case)
 - Comparison of USL-1 and USL-2 Method-2 contains additional statistical uncertainties not included in Method-1, but...
 - » USL-1 (with $?k_m$) < USL-2 necessary, but not sufficient, to show $?k_m$ acceptable
 - » Possibly other systematic (non-statistical) uncertainties that cannot be determined by comparing two statistical techniques


- Insufficient benchmark data to apply statistical techniques
- <25 benchmarks in some cases applicability of Methods 1 and 2 was questionable
 - In original validation, only 14 benchmarks for AOA(4) (MOX powders)
 - >AOA(1) had 182 and AOA(3) had 46, but these two did not pass the chi-squared test for normality





05/08/2003



- Several changes made to the validation:
 - Significantly more benchmarks (66 instead of 14 for AOA(4))
 - > Use of NPM in computing results for AOA(1),(3), and (4)
 - Use of Sensitivity/Uncertainty (S/U) codes from ORNL to identify additional benchmarks in AOA(3) and (4)



- Area of applicability compared to range covered by benchmarks
 - AOA consisted of identifying range of parameters over which code was valid:
 - » Fissile form (chemical composition, physical form, densities, etc.)
 - Materials of composition (including strong absorbers, reflectors, moderators)
 - » Neutron energy range
 - » Neutron moderation (strongly correlated to neutron energy)
 - » Isotopic nature (²⁴⁰Pu, Pu/(U+Pu))



- Should also include code options:
 - Number of neutron generations, neutrons per generation required for convergence
 - > Variance reduction techniques
 - Cross-section treatments (albedos, biasing/variance reduction, etc.)
- Definition of AOA in Part III not clear (range of neutron energy and moderation, material forms)



- <u>AOA exceeded range of parameters covered by</u> <u>benchmarks</u> (significantly in some cases):
 - AOA(2): benchmarks up to 0.91eV EALF; design applications up to 1eV
 - AOA(3): benchmarks down to 1eV; design applications down to 0.05eV
 - AOA(4): benchmarks up to 210 H/Pu; design applications up to 1900 H/Pu



- AOA(4): benchmarks up to 210 H/Pu; design applications up to 291 H/Pu
- AOA(5): benchmarks down to 0.135eV; design applications down to 0.1eV*
- AOA(5): benchmarks up to 858 H/Pu (and none in range of 49.6 to 78); design applications up to 83000 H/Pu*

^{*} Based on worst-case comparison of several tables; some internal disagreement



- Shortcomings with respect to materials included in benchmarks:
 - >AOA(1), (3), and (5): No cases with Cadmium or Borated Concrete
 - >AOA(2): No cases with Borated Shield (composition unknown) or Concrete
 - >AOA(4): No cases with Water or Concrete (benchmarks had plexiglass)



Table showing comparison of design applications and benchmarks for different AOAs (**bold** = areas of disagreement)

	AOA	Description	Exp.	H/Pu_or vm/vf	EALF (eV)	240Pu wt%	PuO2 wt%	Absorbers/Reflectors
Design	1	Pu nitrate solutions		100-200	.1425	4	100	Cd/water, Borated Concrete
Bench.			191	85-1157	.0555	.54-4.67	100	Cd/water, Concrete
Design	2	MOX pellets, rods, assemblies		1.9-10	.1-1	<u>4</u>	2-6.3	Water, <u>Concrete, Borated shield</u>
Bench.			36	1.1-10.75	.0891	8-22	1.5-6.6	Water
Design	3	PuO2 powder		.3- <u>1900</u>	<u>.05</u> -65keV	4	100	Water, Cd, Borated Concrete
Bench.			90	0-210	1-1MeV	2.2-20.2	100	Water, Plexiglass
Design	4	MOX powder		1.6- <u>291</u>	.8-317	4	6.3-22	Water, Concrete
Bench.			66	0-210	.6-1740	2.2-11.6	1.5-100	Plexiglass
Design	5	Pu compound solutions		5.973- <u>83k</u>	<u>,1</u> •67	4	100	Pu(C2O4)2, PuO2F2 Water, <u>Cd, Borated Concrete</u>
Bench.			119	.04-858	.135-4900	2.2-18.35	100	PuO2, PuN Water, Plexiglass



 Different approaches to lack of benchmark data in each Part of Validation Report.

Part I:

- Lack of Pu-Nitrate benchmarks with strong absorbers, but...
- U-Nitrate benchmarks with strong absorbers
- Tried to show:
 - UN systems applicable to PuN systems, because absorbers had similar neutron absorption spectra
 - Boron and cadmium had little effect on the bias





Energy-ev

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- Not sufficient because:
 - Comparison of boron absorption spectra only shows part of story, doesn't consider other neutron reactions
 - > Method of substituting of Pu for U not well-described
 - Study done at very thermal energies, where the source spectrum dependencies largely forgotten
 - Insufficient benchmarks to demonstrate lack of bias dependency of strong absorbers (boron, cadmium)





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Part III: Basic approach:

- (1) Show that reference fissile materials (PuO_2 , PuO_2F_2) bound the various aqueous solutions of Pu compounds
- (2) Show that the chosen benchmarks (PuO₂-polystyrene and Pu Nitrate) are applicable to validate bounding materials in AOA(5)
- Benchmarks divided into two groups, to cover high and low H/Pu range
 - Group 1 = PuO₂-polystyrene blocks covering 0.685-49000eV (0.04-49.6 H/Pu) range (used in AOA(3))
 - Group 2 = PuN solutions covering 0.135-0.551eV (78-858 H/Pu) range (used in AOA(1))



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- Step (1): Determine bounding fissile materials over range of H/Pu
- Step (2): compare EALF vs. H/Pu for:
 - Different chemical compounds
 - > Differing geometrical shapes
 - > Differing reflector materials



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- Differing, seemingly arbitrary, standards for determining applicability of benchmarks to design cases
- <u>Part II</u>: A more sophisticated treatment is ORNL's S/U methodology
 - Purpose: To determine applicability of benchmark experiments to specified design application
 - Determines correlation (between benchmarks and applications) with respect to:
 - » Computed sensitivities
 - » Known uncertainties in underlying cross section data





x = reaction (fission, absorption, etc.) i = energy group



S = sensitivity profileE = integral parameter

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 $S_{\rm max} = {\rm Sensitivity Vector (reactions \times energy groups)}$ $S_{\rm max} = {\rm Cross section uncertainty data (diagonal)}$ $S_{\rm kk} = {\rm Uncertainty matrix}$







• Use of S/U codes in AOA(3) and (4):

> Approach

- » Choose pool of benchmark data, based on traditional techniques (physical similarity, neutronic parameters)
- » Choose design applications to compare with
- » Employ S/U techniques to "screen" out benchmarks that are applicable
- » Analyze bias/uncertainties
- > Originally 14 benchmarks for AOA(4).
- > 298 candidates considered.



- Summary of 298 candidate benchmarks:
 - >61 Pu benchmarks (fast Pu-metal, PuO₂-polystyrene blocks)
 - > 237 mixed Pu/U systems (U/Pu solutions, fuel pin lattices, UO₂-PuO₂ blocks)
- 18 LEU experiments also considered



- Design applications: Generic models developed with similar characteristics to anticipated design applications
- These models used in the S/U analysis to screen benchmarks:
 - ➢ AOA 4-1: H/Pu = 1.58; EALF = 127eV

➢ AOA 4-2: H/Pu = 1.58; EALF = 3751eV

> AOA 4-3: H/Pu = 1.58; EALF = 27.8eV

> AOA 4-4: H/Pu = 0.3; EALF = 2355eV

- AOA 4-4 is for a critical mass of dry powder, which exceeds the mass of anything expected at the MFFF
- Additional cases for 4-4 run (163, 40, 8 kg Pu)



- Benchmarks applicable to each sub-AOA determined:
 - > AOA 4-1: 59 benchmarks
 - > AOA 4-2: 53 benchmarks
 - > AOA 4-3: 44 benchmarks
 - > AOA 4-4-Critical: No benchmarks meeting c_k 0.8 criterion, so relaxed to c_k 0.7.

• Concerns with reducing correlation criterion:

- > Adding experiments can reduce USL, because amount of NPM is a function of number of experiments
- Less applicability is indicated by reduced c_k criterion, but no additional margin applied
- ➤ "Decomposition Problem"

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- NRC Concerns with application of S/U:
 - Set of "design applications" not representative of the whole AOA
 - Small changes in parameters can make significant differences in set of applicable benchmarks
 - May not be appropriate to lump all benchmarks into a single group for bias calculation
 - Set of benchmarks applicable in differing portions of AOA may be mutually exclusive



H/Pu vs. EALF - Benchmarks Applicable to AOA(4) Using S/U Methodology



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Apparent anomalies in calculated results

> Statistical techniques require well-behaved data

> Benchmarks drawn from small data sets may not display this





Issues from Validation Reports

Scope of review limited to:

- » Quality of benchmark data (number and benchmarks, range of important parameters, normality of data)
- » Description and application of methodology
- » Comparison of the benchmarks with the required AOA
- » Reasonableness of results

Did <u>not</u> independently confirm either modeling of benchmarks or statistical calculations



- Major open issues:
 - Range of parameters defining AOA significantly exceeds range covered by benchmarks
 - > Questions about application of S/U to AOA(3) and (4)
 - Validity of methods for demonstrating applicability in Parts I & III
 - > Apparent anomalies (data clusters, double humps) in k-effective data



- NRC will obtain S/U code to do independent confirmation of:
 - Validity of neutron absorption spectrum comparison as sufficiency test for applicability, Part I
 - Correct application of S/U in choosing benchmarks, Part II
 - Validity of neutron energy (EALF) comparison as sufficient test for applicability, Part III



Changes Made to Validation Reports

- Addition of Non-Parametric Techniques (NUREG/CR-6698) to description of methodology
- Use of S/U methodology to define additional benchmarks in Part II, for both AOA(3) and (4)
- Addition of significant amounts of benchmark data to all AOAs
- Addition of Part III, covering miscellaneous Pucompound solutions



Changes Made to Validation Reports

• Current Status:

> Communicated major issues to DCS in March 2003

- Many revolve around range of AOA compared to available benchmarks, methods to validate code where data sparse
- DCS stated its actual anticipated calculations often done at optimal conditions – may not need entire range



Changes Made to Validation Reports

- In some cases, boundaries of AOA were somewhat ambiguous from the VR
- DCS agreed to review needed range in parameter space and give more precise definition of AOA
- NRC action Obtain and apply S/U code to resolve open issues in all parts of VR. Obtain code May 2003



Subcritical Margin Issue

- Validation reviewed to enable finding regarding subcritical margin
- Includes allowances for bias and uncertainties and minimum subcritical (administrative) margin for unknown uncertainties
- Margin varies from facility to facility
 - > BWTX: 0.92 normal, 0.95 abnormal
 - > NFS: 0.90 normal, 0.95 abnormal
- 0.92 and 0.95 appropriate limits for MFFF provided satisfied with validation effort
- DCS continued to state 0.95 was acceptable for both normal and abnormal conditions



Subcritical Margin Issue

- Previously stated 0.95 (exclusive of bias and uncertainty) for abnormal conditions is design basis value, 0.95 also accepted for normal case for AOA-2
- Justification for 0.05 margin not found sufficient; little guidance as to what appropriate amount of margin should be
 - NUREG-1718 (Section 6.4.3.3.4) has limited guidance:
 - Minimum subcritical margin must be justified, but 0.05 generally accepted when bias/uncertainty negligible


- Different limits for normal vs. abnormal can be justified based on:
 - Lower margin for abnormal conditions acceptable because achieving abnormal conditions unlikely
 - Increased risk must be commensurate with risk of achieving abnormal state
 - > Abnormal case assumes "worst-case" conditions—greater actual margin



Approach taken in March meeting

> 0.95 acceptable for abnormal limit for all AOAs

- > 0.95 acceptable for normal case for AOA(2)
- Additional normal case margin needed for remaining AOAs – consistent with approach for HEU facilities



- Rather than specify a specific numerical limit for normal case, allow to be determined on a case-by-case basis
- Because it is determined based on design, cannot be done prior to design
- Recognized that k-eff is not a good measure of safety. Fraction critical (in mass or other parameters) is often a better indicator of available safety margin.



K(x) for Normal and Abnormal Condition





- Allow margin to be specified as a fraction critical or in terms of k-eff
- Allows greater flexibility/consideration of risk
- Example: SRP Section 6.4.3.3.2.2 on geometry control
 - > 90% minimum critical diameter
 - > 85% minimum critical slab thickness
 - > 75% minimum critical spherical volume
 - Safe batch 45% minimum critical mass to allow for double batching



End-of-Day 4 Questions-and-Answers Session

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NRC Review of the Mixed Oxide Fuel Fabrication Facility

Meeting with RF Gosatomnadzor May 2003

Margaret S. Chatterton and Dr. Christopher S. Tripp U.S. Nuclear Regulatory Commission



Day 5 Agenda

- Survey of Draft Safety Evaluation Report
- Status of NCS Open Issues
- Lessons Learned from MOX review
- Anticipated topics for further investigation
- Closeout question-and-answer session



Survey of Draft Safety Evaluation Report (DSER)

- CAR follows SRP
- DSER follows CAR
- First draft April 30, 2002
- Revised to address comments, revised CAR
- Second draft April 30, 2003
- Final draft anticipated September 2003



Survey of DSER: Purpose of SER

• Document staff findings, for:

> Concurrence chain (NRC management)

- > The applicant
- ≻ The public

> Other stakeholders (Congress, hearing parties,...)

- Document scope of review
- Survey of DSER



Survey of DSER: Purpose of SER (continued)

- Document conditions of acceptance
- Consolidate basis for approval/denial
- Preserve institutional knowledge for future licensing
- Provide justification for regulatory decisions to the public



- Conduct of Review
 - > Review objectives
 - > Applicable regulations
 - > Documents reviewed (Scope)
- Organization and Administration
 - Acceptability of NCS design staff qualifications and experience
 - Acceptability of placement of NCS within design team



- Management measures
 - > Detailed review outside DSER scope
 - Control classification reviewed as part of MPQAP
- Technical practices review
 - > Commitment to baseline design criteria (70.64(a)(9))
 - Commitment to follow 70.24, RG-3.71, and ANSI/ANS-8.3 for criticality alarms



- Criticality control design criteria
 - > Requirement for control modes acceptable (based on SRP)
 - > Additional clarifications summarized
 - » How geometric tolerances combined
 - Justification of bounding isotopics (based on NRC confirmatory calculations) and density (commitment to measure)
 - » Modeling neutron reflection
 - » Prohibition on hydrogenous fire suppression agents in moderator controlled areas
 - » Only fixed neutron absorbers used



- Review of Process Description
 - > Text description in CAR Chapter 11
 - Criticality Control Units (CAR Tables 6-1, -2)
 - » Overall approach acceptable
 - » Acceptability bounding isotopics, powder density
 - » Exclusion of Pu from auxiliary (non-fissile bearing) systems
 - » Adherence to preferred design approach
 - » Dual vs. single parameter control



• For each AOA:

> Summary of experimental data, code

- > Application of method to AOA:
 - » Selection of benchmarks (traditional method, spectral comparison, S/U)
 - » Trending parameters chosen for k-eff fit
 - » Normality of Data
 - » Calculation of Upper Subcritical Limit

> Staff continues to review; open issue (NCS-4)



Subcritical Margins

> Discusses DCS's justification for $\Delta k_m = 0.05$

> Acceptability of 0.05 for abnormal conditions

> Acceptability of 0.05 for AOA(2) normal conditions

Need for additional normal condition margin for remaining AOAs

> Design basis includes:

- » Abnormal case limit for each AOA
- » Methodology for normal condition limit for each AOA



- Lack of Principal Systems, Structures, and Components (PSSCs) for NCS
- Commitment to Double Contingency Principle
 - > Only DCP portion of baseline design criteria met
 - Acceptable definition of "unlikely" (SRP)
 - Acceptable methodology for demonstrating "highly unlikely" (SRP)
 - » Two robust, independent controls
 - » Method of determining likelihood
 - » Failure detection or additional margin



Commitments to ANSI/ANS-8 standards

> For each standard:

- » Whether part of design basis
- » Reiterate commitment to which section
- » Acceptability of exceptions/clarification
- » Justification if not part of design basis
- Evaluation findings & Open Items
- References
- Justification for closed open items from first draft (Appendix)



Status of NCS Open Issues

- Design basis USL for each process type
- Determination of normal condition subcritical margin
- Clarification of commitment to dual vs. single parameter control



Lessons Learned

- Important to set ground rules up front
- Frequent communication necessary
- Correspondence is inefficient: necessary for documentation
- Telephone conversations streamline processincreases potential for misunderstanding on both sides



Lessons Learned

- Written communication and face-to-face meetings effective
- Important to be involved early in the design process
- Ambiguous responses should be questioned
- Drawbacks to accepting "IOUs" for future commitments (e.g., CAR changes)



Lessons Learned

- Things not always as they seem (e.g., dualparameter control)
- Precise language important

> Inspectable and enforceable

Commitments unambiguous



- Demonstration of bounding nature of incoming plutonium isotopics
- Demonstration of bounding powder densities
- Review of normal condition margin
- Applying validation to actual design calculations



- ISA review
 - Likelihood determination for accident sequences
 - > Frequencies for IROFS
 - ➤ Management measures to IROFS
- Exemptions from criticality accident alarm coverage



- Emergency response procedures for criticality events
- Application of design principles to actual design
- Integration of fire protection and criticality safety concerns



- Administrative practices for NCS
 - > NCS program
 - > NCS training
 - > Procedures
 - ➢ Audits
 - > Investigations



Closeout Questions-and-Answers Session

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- Nuclear Safety Training (for fissile material operators)
 - Curriculum Contents
 - > Administration

Audits

- NCS Function Audits
- > Plant Operations Audits
- Corrective Actions

Procedures

- ➤ Review and approval
- > Postings



NCS Review of the CAR: Technical Practices for Nuclear Safety

- Design principles include:
 - > Preferred control hierarchy
 - Documentation in NCSEs Flowdown of IROFS to ISA
 - Compliance with DCP demonstrated, defense-indepth



- Criticality Accident Alarm System (CAAS) Specifications:
 - > CAAS required in all plant areas as specified in 70.24(a).
 - > Specific areas to be exempted identified
 - Exemptions allowed if "will not endanger life or property" and "in the public interest" (10 CFR 70.17)
 - Considered on case-by-case basis (sufficiently low risk/benefit) (NCS-9)
 - Commitment to follow ANSI/ANS-8.3-1997 (as qualified in RG-3.71)



- Additional commitments beyond ANSI/ANS-8.3-1997
 - > Operations will be placed into safe shutdown when inoperable
 - > Coverage areas will be determined using shielding codes
 - Effects of both fixed and transient shielding considered
- Additional Technical Specifications
 - Each area covered by two gamma or neutron detectors



- Control Categories
- Control Modes:
 - > Geometry
 - » Fixed equipment dimensions
 - » "Safe" or "favorable" geometry
 - » Safe diameter columns, slab & annular tanks (AP)
 - » Most reliable means of control



- Mass
 - Limits based on worst-case geometry and material form
 - > Subcritical with largest overbatch resulting from a single failure

Density

- Conservative assumptions based on process history, handbook data, or standards
- PuO2 power bounding density of 7 g/cm³; MOX 3.5 5.5 g/cm³
- Measured initially, and periodically where form of material changes (NCS-3)


- Isotopics
 - Design basis bounding assumptions (96 wt% ²³⁹Pu, 4wt% ²⁴⁰Pu, <1wt% ²⁴¹Pu)
 - > Controlled by computer during blending (PuO₂ and UO₂)
 - ➢ Master blend 22wt% Pu
 - ➢ Final blend 6.3wt% Pu

Reflection

> Administratively controlled (one of least reliable means)

> Analysis uses:

- I-inch water for transient reflectors (personnel, temporary materials, water) + any fixed reflection modeled explicitly
- » 12-inches water reflection uncontrolled



- Moderation
 - > Used in combination with mass control
 - > Amounts of moderator added to process are strictly limited
 - Gloveboxes + inert atmosphere primary moderation barrier
 - Hydrogenous firefighting agents excluded (moderator-control zones)

Concentration

- Limited to systems with low expected quantities of fissile material
- Typically only control mode when used => single-parameter limits are established



- Interaction
 - Fixed placement of fissile material equipment, and/or spacing controls
 - Preferred means are passive features such as "birdcages" and array spacers
- Absorber
 - > Fixed, removable, or soluble neutron absorbers
 - > Only fixed absorbers anticipated
 - > One of the most reliable means of control



- Volume
 - Limits the container volume to less than a spherical critical mass
 - > Considered one of the most reliable means of control
- Heterogeneity
 - > Used for pellets, rods, and assemblies
 - > Homogeneity relied on during/after blending



Process variable control

> Supports the previous 11 parameters

- Doesn't directly affect k-eff
- Affects values of the previous parameters, due to changes in temperature, pressure, etc.
- Important process variable and could be considered the 12th control mode



- Specific information related to control modes is provided in CAR Tables 6-1 and 6-2
- Facility divided into Criticality Control Units (CCUs)
- Physicochemical form specified
- Controlled parameters defined
- Allowed ranges in parameter values determined
- Specific controls identified



Controlled Parameters for Aqueous Polishing

Table 6-1. Preliminary Definition of Reference Fissile Medium and Control Methods for Principal AP Process Units (Continued)

	Control Method											_		
Criticniity Control Unit	Physicochemical Characteristica (PC)	(IA) stars (IA).	. Geometry (G)	Density (D)	Isotopics (1)	Reflection (R)		Concentration (C)	Interaction (IN)	Neutron absorber (A)	Valume (V)	Heterogeneity (H)	Process Fariable	Comments
UO2 Dissolution														
Buffer Tank	YES Fu(NO ₂) ₂ + II ₂ O [3,6]			NO9L		DND -		YES [7]	1BD [2]	TA NOTIN L'ANNA NATION	NO NO NO NO NO NO NO NO NO NO NO NO NO N	SNO1	NO 3	
KOB Dissolution Unit														
Electrolyzer	NO 11 1,10014 41110	NO NA NA NA	YES ,	NO [1,9] d≤7	NO[1] 205002			NOV A	TBD [2]	YES Cd. costing	NO NA NA	NO.	20-1-2- 2-1-2-2-	
Reception tank	1110		YES slab	NO [1,9] d≤7	NO 111 1739 U Z	INO5		S NOST	TBD [2]	YES Cd coating	ANO	VINO.	NO	
PuO ₂ filter	NO 10074 HiO		YES Cylin -der	NO [1,9] _J≤7			UNO7		TBD [2]		NO.	NO	T NO	Double control to guarantee absence of PuO ₂ in downstream equipment.
Dilution and sampling tank	YES Pu(NO ₁) ₂ + H ₂ O[3.8]	TNOL	YES Slab	PENO:		NO	1 NO S		TBD [2]	YES Cd . coating	NO	NO/A	PC	
Buller Tank	YES Pu(NO3)3 + II2O [3,6]	NO 4 1X	YES Annul -ar		NO([1] 19232	NO NI		22NO15	(LBD [2]	YES Cole- manite concrete	+NOU Date: State	NO.	1-NO	Culemanite concrete ' is a type of borated concrete.

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Controlled Parameters for MOX Process

Table 6-2. Preliminary Definition of Reference Fissile Medium and Control Methods for MP Process Units (Continued)

	Control Method													
Criticality Control Unit	Physicochemical Characteristics (PC)	Mass (N)	Geometry (G)	Density (D)	Isotopics (I) '.	Reflection (R)	Moderation (MN)	Concentration (C)	Interaction (IN)	Neutron absorber (A)	Yolume (Y)	Heterogeneity (H)	Process variable	Comments
Powder Aren													······································	
Primary blend ball milling Scrap milling	NO Minsiler Ulend NO Dis chrited Serap Pow- der	YES YES		YES [1,6] d≤5.5 .* YES [1,6] d≤5.5	YIES ²⁴⁰ Pu $\geq 4\%[1];$ $M_{r}/(M_{U}+M_{r})$ $\leq 22\% [5]$ · YES ²⁴⁰ Pu $\geq 4\%[1];$ $M_{r}/(M_{U}+M_{r})$ $\leq 22\% [5].$		YES YES				NUT CONTRACTOR NOT CONTRACTOR	YES	M M,H	-U metal balls are present in the ball- mill and are accounted for as reflector in the criticality calculations Homogeneity of discarded scrap powder is required by downstream unit.
Final dosing	NO. Master Ulend	YES	NO	YES [1,6] d≤5.5	YES $^{240}Pu \ge 4\%[1];$ $M_{r,J}(M_{U}+M_{r,s})$ $\le 22\% [5]$ $M_{r,J}(M_{U}+M_{r,s})$ $\le 6.3\%$ in jar		YES			NO: NO: NO: NO: NO: NO: NO: NO: NO: NO:			M,I	The relative quantity of master blend and UO_2 is controlled; used in downstream units.



- Review of CAR Tables 6-1 and 6-2:
 - > Adherence to design principles (preference for passive geometry, etc.)
 - > Reasonableness of design parameters and bounding values
 - Consistency with process description, industry practice
- Geometry (with absorber) control utilized in AP process.
- Impracticable in much of MP process: mass/moderation used.
- Bounding parameter values: isotopics, powder density, moderation
- Type of absorber, geometric shape specified



- Inconsistencies with Chapter 11 process description
- Criticality evaluation
 - > Single and multi-parameter limits (ANSI/ANS-8.1-1983)
 - ➤ Handbooks
 - Validated computational methods

Validation method (NCS-4)

- Compare measured results for critical benchmarks against calculated results using the code
- Choose benchmark experiments that are physically and neutronically similar to the systems that will need to be calculated by the code



- Important characteristics of benchmark experiments:
 - > System geometry
 - Fissile material content
 - > Moderator-to-fuel ratio
 - > Absorber/reflector materials
 - Average neutron energy

• SCALE-5 code under development by ORNL

- Sensitivity analysis: sensitivity of k-eff to changes in underlying cross sections
- Uncertainty analysis: combines sensitivity information & crosssection covariance data => correlation coefficient for benchmark comparison



- k-eff calculated for each benchmark experiment in area of applicability (AOA)
 - Trended using a linear regression fit, as a function of the most important parameters
 - > Pu/MOX isotopics (²⁴⁰Pu, Pu/(U+Pu) content)
 - > Energy of average lethargy causing fission (EALF)
 - ➤ H/X or vm/vf ratio
- Benchmarks mostly from the International Handbook of Evaluated Criticality Safety Benchmark Experiments





- 15 ANSI/ANS-8 standards endorsed by RG-3.71:
 - > Single and multiple-parameter subcritical limits
 - > Programmatic commitments:
- Compliance with standard = commitment to all "shall" statements
- NUREG-1718 (SRP):
 - Compliance with "shall" and "should" statements acceptable (subject to limitations)
 - Can propose alternate means of meeting intent of ("should" statements).
 - More specific commitments included in CAR as appropriate. (NCS-10)



- ANSI/ANS-8.1 (Design Basis)
- ANSI/ANS-8.3 (Design Basis)
- ANSI/ANS-8.7 (Non-Design Basis)
- ANSI/ANS-8.9 (Non-Design Basis)



- ANSI/ANS-8.10 (Non-Design Basis)
- ANSI/ANS-8.12 (Non-Design Basis)
- ANSI/ANS-8.15 (Non-Design Basis)
- ANSI/ANS-8.17 (Design Basis)



- ANSI/ANS-8.19 (Design Basis)
- ANSI/ANS-8.20 (Design Basis)
- ANSI/ANS-8.21 (Design Basis)
- ANSI/ANS-8.22 (Design Basis)
- ANSI/ANS-8.23 (Non-Design Basis)



- 40 Questions out of 239 on NCS
- <u>RAI-40</u>: Meaning of "unlikely" for meeting DCP
- <u>RAI-41</u>: Sufficiency of DCP in meeting §70.61
 - DCP used to ensure "subcritical under normal and credible abnormal conditions"
 - Deterministic means (DCP/single-failure criterion) to satisfy 70.61(b) and (c)



RAI Major Issues: Chronology in CAR (NCS-5)

- Aug 2000: SRP Issued with Appendix A (NCS example using index method.) Section 5.4.3.2(B)(viii) also had acceptance criteria for qualitative methods.
- Jan 2001: "Highly Unlikely" methodology as part of NCS design bases.
- Feb 2001: Original CAR took position that DCP + management measures + standards = Highly Unlikely.



RAI Major Issues: Chronology in CAR (NCS-5) (continued)

- July 2001: RAIs 40 & 41 issued
- Aug 2001: RAI response restated CAR position on "Highly Unlikely." Asked for clarification whether 70.61(d) implies meeting 70.61(b) or are two separate requirements.
- Dec 2001: NRC letter said index method acceptable, summarized existing guidance.
- Mar 2002: DCS letter defined "unlikely" for DCP as qualitatively comparable to 1/100 yrs.



RAI Major Issues: Chronology in CAR (NCS-5) (continued)

- Oct 2002: Revised CAR presented more details on deterministic approach, still in terms of broad programmatic requirements, not specific control characteristics
- Jan 2003: Meeting to address.
- Feb 2003: DCS submitted revised words to Chapter 5
- Mar 2003: NRC proposed revised wording to reference NUREG-1718, make wording more explicit.

> DCS revised, and ultimately agreement reached.

> DCS moved this to Chapter 6.



NCS-5 Resolution

- Final Resolution
 - General approach: DCP + QA + industry codes/standards + management measures
 - Description of accident sequences and IROFS in NCSEs/ISA Summary
 - "Unlikely" determination for each DCP control based on all "availability and reliability" qualities in NUREG-1718
 - > In addition to DCP, must have
 - » (a) Failure detection on specified frequency
 - » (b) Safety margin such that multiple failures required for criticality, or
 - » (c) Other means, demonstrated comparable to (a),(b)



NCS-1 Resolution

 <u>RAI-68</u>: Description of the qualifications and duties of the NCS staff during the design phase (NCS-1)

NCS Function not described for design phase of MFFF

- DCS clarified that qualifications same as for design phase NRC: No acceptable guidance; compared proposed qualifications to those at other fuel facilities (especially HEU facilities)
- > Need for Pu/MOX processing experience

Resolution:

- (a) DCS provided information on experience of staff (COGEMA, SGN); did not commit to MOX/Pu experience requirements
- > (b) DCS committed to provide training on MOX/Pu processing



- <u>RAI-72</u>: Commitment to follow the preferred hierarchy of controls "where practicable"
- <u>RAI-74</u>: Dispositioning of CAAS exemptions. Original CAR stated two cases in which criticality coverage will not be required:
 - When limited to less than half of a minimum critical mass with no potential for double batching
 - > When used for storage of closed shipping containers
 - Exemptions historically based on low inherent risk, reviewed on case-by-case basis by NRC. (NCS-9)
- <u>RAI 77</u>: Neutron absorbers for criticality safety (fixed absorbers only)



- <u>RAI-79</u>: Basis for certain technical assumptions/practices:
 - Isotopic abundance in the CAR bounds the worst case feed material
 - ➤ How reflection (nominal vs. full) used to NCSEs
- <u>RAI-80</u>: No statement two-parameter control preferred to single-parameter control
 - CAR appeared to imply that dual, independent control is distinct from geometry control (not needed for safe geometry)
 - NRC agreed that if no identifiable accident sequences leading to criticality, intent of DCP met
 - DCS committed to evaluate potential failure paths leading to unsafe geometry

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- <u>RAI-81</u>: Clarification how DCP implemented when only one control identified in Tables 6-1 and 6-2; revision of Tables 6-1 and 6-2 to clarify control strategy
- <u>RAI-82</u>: Whether physicochemical form receive the same kind of programmatic treatment as other control modes
- <u>RAI-88</u>: Information on methods to be used when there is scarcity of benchmark data

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- <u>RAI-90</u>: Commitment to ANSI/ANS-8 Series standards
 - > Commitment to Requirements vs. Recommendations (NCS-10)
 - > Any exceptions or qualifications (NCS-6,7,8)
 - Additional details specified in SRP
- <u>RAI-91/94</u>: Justification for the use of the administrative margin (NCS-4) Validation Reports
- <u>RAI-98</u>: Clarification that the tables be revised to reflect wherever a parameter was controlled, regardless of whether it was controlled downstream



- <u>RAI-99</u>: Requested a cross-reference between the information in Tables 6-1 and 6-2 with the Process Description in Chapter 11
- <u>RAI-100</u>: Requested CCUs with controlled parameters to be defined for certain process steps not included in the tables
- <u>RAI-103/104</u>: Concerned Tables 6-3 and 6-4 ("permissible" spherical volume, slab thickness, cylinder diameter, spherical mass) for fissile materials in the AP and MP processes



Changes to the CAR

- NCS Function during design phase (Section 6.1.1)
- Identified that specific areas needing CAAS exemptions would be submitted for NRC approval
- Change to technical criteria
 - > 6.3.3.2.4 analysis of bounding nature of isotopics
 - ≻ 6.3.3.2.5 modeling of water reflection



Changes to the CAR

- Theoretical density for incoming PuO₂ assumed until confirmed.
- Preferred control hierarchy commitment
- Tables 6-3 and 6-4 not to be used as subcritical limits
- Added section discussing each ANSI/ANS-8.1 standard



Changes to the CAR

- Removed reference to specific subcritical margin (0.05) deferred to Validation Reports
- Added summary of design bases
- Significant changes to Tables 6-1 and 6-2



NCS Open Items

- NCS-1: MOX/Pu experience
- NCS-2: Design bases for auxiliary systems
- NCS-3: Bounding densities
- NCS-4: Validation/Subcritical Margin
- NCS-5: "Highly unlikely" for criticality



NCS Open Items

- NCS-6,8: Extension of codes AOA beyond experimental benchmark data (ANSI/ANS-8.1, 8.17)
- NCS-7: Commitment to ANSI/ANS-8.15 (special actinides)
- NCS-9: Dispositioning of CAAS exemptions
- NCS-10: Clarification of ANSI standard commitments



End-of-Day 3 Questions-and-Answers Session

NRC FORM 8C (7-94) NRCMD 3.57

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NRC Review of the Mixed Oxide Fuel Fabrication Facility

Meeting with RF Gosatomnadzor May 2003

Dr. Christopher S. Tripp U.S. Nuclear Regulatory Commission


Day 4 Agenda

• NRC Review of Validation

NRC Review of Subcritical Margin

End-of-day Question-and-Answer Session



Regulatory Role of Validation Reports

- Design basis #2 maximum k-eff for normal and credible abnormal conditions
- <u>Only</u> design basis that fits cleanly into the 10 CFR 50.2 definition.
 - >70.61(d): "the risk of nuclear criticality accidents must be limited by assuring that under normal and credible abnormal conditions, all nuclear processes are <u>subcritical</u>, including use of an approved margin of subcriticality for safety"
 - > ANSI/ANS-8.1: Requirements for code validation