

MAR 1 1 2004

L-2004-043 10 CFR 50.55a(f)

U. S. Nuclear Regulatory Commission Attn: Document Control Desk Washington, D. C. 20555

Re: Turkey Point Units 3 and 4 Docket Nos. 50-250 and 50-251 Fourth-10 Year Interval Inservice Testing Program

The Turkey Point Units 3 and 4 Inservice Testing (IST) program has been revised to meet the requirements of the ASME OM Code for the Fourth 10-year testing interval.

This letter submits to Nuclear Regulatory Commission in Attachment 1 the Fourth 10-year testing interval IST program, Revision 0, beginning February 22, 2004 for Turkey Point Unit 3 and April 15, 2004 for Turkey Point Unit 4. The IST program includes the associated pump and valve relief requests, which have been previously submitted to NRC for approval under FPL letter L-2003-316, dated January 6, 2003. Attachment 2 provides a current set of drawings to assist in pump and valve identification.

If you have any questions please contact Walter Parker at (305) 246-6632.

Sincerely, my

Terry O.Jones Vice President Turkey Point Nuclear Plant

Attachments

cc: Regional Administrator, Region II, USNRC Senior Resident Inspector, USNRC, Turkey Point Plant

4047

ATTACHMENT 1 L-2004-043

Turkey Point Nuclear Plant Units 3 & 4

Inservice Testing Program Fourth Ten Year Interval

Revision 0 Commercial Service Dates:

> Unit 3 – 12/14/72 Unit 4 – 09/14/73

Florida Power and Light Company Turkey Point Nuclear Power Plant P.O. Box 3088 Florida City, Florida 33034

APPROVALS: 5-04 **Prepared By:** Date: Z T Coordinator Approved By: Date: 2 ngineering Operations Support Manager PT Approved By: Date PTN Engineering Manager

	IST I Florida Pow Turkey Point	Program Plan er and Light Comp Nuclear Power P	oany lant		
	REV	ISION LOG			
Effective Date	Revision Description	Prepared: IST Coordinator	Date	Approved: Engineering Operations Support Manager	Date
2/25/04	4 th Ten Year Interval, Revision 0 Submittal to NRC. In compliance with the 1998 Edition through 2000 Addenda except where relief is requested. For check valve condition monitoring, this submittal is in compliance with the 1995 Edition through 1996 Addenda, Appendix II and associated Federal Register modifications.	Fouldary	2125/0	Edno	2/25
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1.0 INTRODUCTION

1.1 Purpose

To provide requirements for the performance and administration of assessing the operational readiness of those pumps and valves whose specific functions are required to:

- Shutdown the reactor to the safe shutdown condition,
- Maintain the safe shutdown condition, or
- To mitigate the consequences of an accident.

1.2 Scope

The program plan was prepared to meet the requirements of the following subsections of the American Society of Mechanical Engineers (ASME) OM Code (1998 Edition through 2000 Addenda) except for Mandatory Appendix II *"Check Valve Condition Monitoring Program"*. The American Society of Mechanical Engineers (ASME) OM Code (1995 Edition through 1996 Addenda), will be used for Check Valve Condition Monitoring and will apply the modifications required in Federal Register Volume 64, No. 183 dated September 22, 1999 (see Technical Position TPv-02).

• Subsection ISTA, "General Requirements"

ISTA contains the requirements directly applicable to inservice testing including the Owner's Responsibility and Records Requirements.

• Subsection ISTB, "Inservice Testing of Pumps in Light-Water Reactor Nuclear Power Plants"

Establishes the requirements for inservice testing of pumps in light-water reactor nuclear power plants. The pumps covered are those provided with an emergency power source, that are required in shutting down a reactor to the safe shutdown condition, in maintaining the safe shutdown condition, or in mitigating the consequences of an accident. These pumps are either centrifugal or positive displacement type pumps.

 Subsection ISTC, "Inservice Testing of Valves in Light-Water Reactor Nuclear Power Plants"

Establishes the requirements for inservice testing of valves in light-water reactor nuclear power plants. The valves covered include those which provide overpressure protection and are required to perform a specific function, either actively by changing valve obturator position or passively by effectively maintaining required obturator position in shutting down a reactor to the safe shutdown condition, in maintaining the safe shutdown condition, or in mitigating the consequences of an accident.

 Mandatory Appendix I, "Inservice Testing of Pressure Relief Devices in Light-Water Reactor Nuclear Power Plants"

Provides the requirements for performance testing and monitoring of nuclear plant pressure relief devices. Methods, intervals, and record requirements for monitoring

and testing are established, as well as guidelines for the evaluation of results. Applies to safety valves, safety relief valves, pilot-operated pressure relief valves, power-actuated pressure relief valves, nonreclosing pressure relief devices and vacuum relief devices, including all accessories and appurtenances.

Mandatory Appendix II, "Check Valve Condition Monitoring Program"

Provides an alternative to the testing or examination requirements of ISTC-3510 through ISTC-5221. The purpose of this program is both to improve valve performance and to optimize testing, examination, and preventive maintenance activities in order to maintain the continued acceptable performance of a select group of check valves.

The Turkey Point Nuclear Power Plant fourth 120-month interval Pump and Valve Inservice Testing Plan will be in effect as follows:

	Begin	End
Unit 3	February 22, 2004	February 21, 2014
Unit 4	April 15, 2004	April 14, 2014

This plan will be updated as required in accordance with 10CFR50.55a(f).

This program plan provides a complete listing of those pumps and valves included in the program per the requirements of:

- ISTA "General Requirements,"
- ISTB "Inservice Testing of Pumps in Light-Water Reactor Nuclear Power Plants"
- ISTC "Inservice Testing of Valves in Light-Water Reactor Nuclear Power Plants"
- Mandatory Appendix I, "Inservice Testing of Pressure Relief Devices in Light-Water Reactor Nuclear Power Plants"
- Mandatory Appendix II, "Check Valve Condition Monitoring Program"

The key features of this Plan are: the Pump and Valve table listings, Relief Requests, Refueling Outage Justifications, Cold Shutdown Justifications, and Technical Positions. The Turkey Point Nuclear Power Plant Inservice Testing Basis Document includes the justification for inclusion of components in the scope of IST and also the justifications for exclusion from the program. Administrative procedures, surveillance testing procedures, and other records required to define and execute the Inservice Testing Program are all retained and available at Turkey Point Nuclear Power Plant.

2.0 INSERVICE TESTING PLAN FOR PUMPS

2.1 **Pump Inservice Testing Plan Description**

This program plan meets the requirements of ASME OM Code ISTB with the exception of specific relief requests contained in Attachment 3.

2.2 Pump Plan Table Description

The pumps included in the Turkey Point Nuclear Power Plant IST Plan are listed in Attachment 12. The information contained in these tables identifies those pumps to be tested to the requirements of the ASME OM Code, the testing parameters and frequencies, and associated relief requests. The headings for the pump tables are delineated below.

Pump Tag	Unique pump identification number.			
Category	Pump group as defined in ISTB-2000.			
	Group A Group B	Continuous or routinely operated pumps Standby pumps not operated routinely except for testing		
Safety Class	ASME Code classification of the pump.			
	1 2 3 SR NS	Class 1 Class 2 Class 3 Non-Code, Safety Related Non-Safety Related		
Pump Type	Pump type.			
	Centrifugal Vertical Positive Dis	placement		
Pump Driver	Pump driver	· type.		
	Motor Turbine Engine	Motor driven Steam turbine driven Engine Driven		
Nominal Speed	Pump speed	Pump speed for variable speed pumps only.		
<u>P&ID</u>	Piping and Instrumentation Drawing (Flow Diagram) on which the pump is represented.			
P&ID Coor.	The P&ID Coordinate location of the pump.			

IST Program Plan Florida Power and Light Company Turkey Point Nuclear Power Plant				
2.2 Pur	Pump Plan Table Description (Cont'd)			
Tes	t Type	Measured pump	o test parameters.	
		N DP Q V	Speed Differential Pressure Flow Rate Vibration	
		a - Denotes a Ca b - Denotes a Ca c - Denotes a Ca	ategory A Pump Test ategory B Pump Test omprehensive Pump Test	
Tes	Test Freq. Frequency for		performing the specified inservice test.	
		M3 CS Y2	Quarterly (92 Days) Cold Shutdown Biennially (2 Years)	
<u>Rel</u>	<u>ief Request</u>	A relief requerequirement is contains an in Attachment 3.	est number is listed when a specific code determined to be impracticable. Attachment 2 ndex of all the relief requests included ir	
<u>Tec</u>	: <u>h. Pos.</u>	A technical post the code are no needed. The te requirements an Positions for p contains an inde in Attachment 1	sition number is listed when the requirements of the easily interpreted and clarifying information is echnical position is used to document how Code rebeing implemented at the station. Technical umps are prefixed with "TPp". Attachment 10 ex of all the Station Technical Positions included 1.	
<u>Pun</u>	np Name	Descriptive nan	ne of the pump.	

3.0 INSERVICE TESTING PLAN FOR VALVES

3.1 Valve Inservice Testing Plan Description

This plan establishes the test intervals and parameters to be measured to meet the requirements of ISTA, ISTC, Appendix I, and Appendix II with the exception of the specific relief requests contained in Attachment 5.

Where the frequency requirements for valve testing have been determined to be impracticable, Cold Shutdown or Refuel Outage Justifications have been identified and written. These justifications are provided in Attachments 7 and 9 respectively.

3.2 Valve Plan Table Description

The valves included in the Turkey Point Nuclear Power Plant IST Plan are listed in Attachment 13. The information contained in these tables identify those valves that are required to be tested to the requirements of ISTC and Appendix I, the test parameters, frequency of testing, and the associated relief requests. The headings for the valve tables are delineated below.

Valve Tag	A unique	A unique identifier for the valve.		
<u>P&ID</u>	Piping an the valve	Piping and Instrumentation Drawing (Flow Diagram) on which the valve is represented.		
P&ID Coor.	The P&ID	O Coordinate location of the valve.		
Safety Class	The ASME Class abbreviation.			
	1 2 3 SR NS	Class 1 Class 2 Class 3 Non-Code, Safety Related Non-Safety Related		
<u>Cat.</u>	The ASM ISTC-130	1E OM Code category (or categories) as defined in 0.		
	A B C D A/C B/C	Seat Leakage Limited. Seat Leakage Not Required. Self-Actuating Valves. Single Use Valves. Both Categories A and C. Both Categories B and C.		
Size	The nomi	The nominal pipe size of the valve, in inches.		

_		IST	T Program Plan
		Florida Po	wer and Light Company
		<u>Turkey Poi</u>	int Nuclear Power Plant
2	Valve Plan Table D	escription (Co	ont'd)
	Valve Type	The valve	body style abbreviation.
		BAL	Ball Valve
		BTF	Butterfly Valve
		СК	Check Valve
		DAM	Damper
		DIA	Diaphragm Valve
		GA	Gate Valve
		GL	Globe Valve
		PLG	Plug Valve
		RPD	Rupture Disk
		RV	Relief Valve
		SCK	Stop Check Valve
		3W	3-Way Valve
		4W	4-Way Valve
	Act. Type	The valve	actuator type abbreviation.
		AO	Air Operator
		НО	Hydraulic Operator
		MAN	Manual
		MO	Motor Operator
		SA	Self-Actuating
		SO	Solenoid Operator
	Active/Passive	Active or 1	Passive function determination for the valve in
		accordance	e with ISTC-2000.
		А	Active
		Р	Passive
	Normal Position	The norma normal po power ope valve whe	al position abbreviation. The valve's position during over operation. If the system does not operate during eration, then the normal position is the position of the n the system is not operating.
		C	
			Locked Ulosed
		DE E	De-energized (3-way and 4-way solenoid valves)
			Chergized (3-way and 4-way solenoid valves)
		10	Upen Locked Open
		CVC	System Condition Dependent

		IST Florida Pov	Program Plan ver and Light Company
5.2	Valve Plan Table	Description (Co	nt'd)
	Safety Position The safety function position(s). For values the functions in the open and closed positions mor function position may be specified.		
		С	Closed
		DE	De-energized (3-way and 4-way solenoid valve
		Е	Energized (3-way and 4-way solenoid valves)
		DE/E	De-energized and Energized
		0	Open
		O/C	Open and Closed
	Test Type	The test ty	pe abbreviation.
		AT-01	Seat Leakage Rate Test (low pressure air),
			Appendix J
		AT-02	Seat Leakage Rate Test (high pressure water),
			Pressure Isolation Valve
		BTC	Exercise Test Closed
		BTO	Exercise Test Open
		CC	Exercise Test Closed – Check Valve ⁽¹⁾
		CO	Exercise Test Open – Check Valve ⁽¹⁾
		СР	Partial Exercise Test – Check Valve ⁽¹⁾
		DT	Rupture Disk Test
		FC	Fail Safe Test Closed
		FO	Fail Safe Test Open
		PIT	Position Indication Test
		RT	Relief Valve Test
		⁽¹⁾ Three lette tests to differ The letter foll disassembly a for radiograph	r designations may be used for check valve condition monitorin entiate between the various methods of exercising check valves lowing "CC", "CO", or "CP" should be "A" for acoustics, "D" and examination, "F" for flow indication, "M" for magnetics, "I hy, "U" for ultrasonics, or "X" for manual exercise.
	Test Freq.	The test frequency abbreviation.	
		App-J	Appendix J
		СМ	Condition Monitoring ⁽¹⁾
		CS	Cold Shutdown
		M3	Quarterly
		OP	Operating Activities ⁽²⁾
		RR	Refueling Outage
		YX	X Years (X = $1, 2,, 10$)
		⁽¹⁾ Frequency that valve g	v is as indicated in respective Condition Monitoring Plan roup.
		⁽²⁾ Satisfied i	in accordance with IST Program Technical Position, T

01, "Bi-directional Testing of Check Valves".

IST Program Plan
Florida Power and Light Company
Turkey Point Nuclear Power Plant

3.2 Valve Plan Table Description (Cont'd)

<u>Relief Request</u> A relief request number is listed when a specific code requirement is determined to be impracticable. Attachment 4 contains an index of all the relief requests included in Attachment 5.

<u>Deferred Just.</u> Deferred Test Justification. This section refers to Cold Shutdown Justifications and Refuel Outage Justifications.

> A Cold Shutdown Justification number is listed when the testing frequency coincides with Cold Shutdowns instead of being performed quarterly. Cold Shutdown Justification numbers for valves are prefixed with "CSJ". Attachment 6 contains an index of all the Cold Shutdown Justifications included in Attachment 7.

> A Refueling Justification number is listed when the testing frequency coincides with Refueling Justification instead of being performed quarterly or during Cold Shutdowns. Refueling Justification numbers for valves are prefixed with "RJ". Attachment 8 contains an index of all the Refueling Justifications included in Attachment 9.

<u>Tech. Pos.</u> A technical position number is listed when the requirements of the code are not easily interpreted and clarifying information is needed. The technical position is used to document how Code requirements are being implemented at the station. Technical Positions for valves are prefixed with "TPv". Attachment 10 contains an index of all the Station Technical Positions included in Attachment 11.

4.0 ATTACHMENTS:

Attachment 1 System and P&ID Listing

Attachment 2 Pump Relief Request Index

Attachment 3 Pump Relief Requests

Attachment 4 Valve Relief Request Index

Attachment 5 Valve Relief Requests

Attachment 6 Cold Shutdown Justification Index

Attachment 7 Cold Shutdown Justifications

Attachment 8 Refuel Outage Justification Index

Attachment 9 Refuel Outage Justifications

Attachment 10 Station Technical Position Index

Attachment 11 Station Technical Positions

Attachment 12 Inservice Testing Pump Table

Attachment 13 Inservice Testing Valve Table

ATTACHMENT 1

SYSTEM AND P&ID LISTING

System	System Name	P&ID
013	Instrument Air/Service Air	5610-M-3013-1
013	Instrument Air/Service Air	5613-M-3013-1,7
018	Condensate Storage	5613/4-M-3018-1
019	Intake Cooling Water	5613/4-M-3019-1
020	Primary Water Makeup	5613/4-M-3020-2
022	Emergency Diesel Generator	5613/4-M-3022-1,2,3,4,5,6
022	Emergency Diesel Generator	5614-3022-3,4
025	Control Building Ventilation	5610-M-3025-2
030	Component Cooling Water	5613/4-M-3030-1,2,3,4
030	Component Cooling Water	5613-M-3030-5
033	Spent Fuel Pit Cooling	5613/4-M-3033
036	Sampling	5613/4-M-3036-1
036	Sampling	5613/4-M-3037-1
041	Reactor Coolant System	5613/4-M-3041-2,3,4
046	Boric Acid	5610-M-3046-1
047	Chemical and Volume Control	5613/4-M-3047-1,2,3
050	Residual Heat Removal	5613/4-M-3050-1
053	Containment Purge	5613/4-M-3053-1
056	Emergency Containment Filtering	5610-M-3068-1
056	Emergency Containment Filtering	5613/4-M-3056-1
061	Liquid Waste Disposal System	5613/4-M-3061-1
062	Safety Injection	5613/4-M-3062-1,2
064	Safety Injection Accumulators	5613/4-M-3064-1
065	Nitrogen and Hydrogen	5610-M-3065-1
068	Containment Spray	5613/4-M-3068-1
072	Main Steam System	5613/4-M-3072-1
074	Blowdown	5613/4-M-3032-1,4
074a	Main Feedwater	5613/4-M-3074-3
075	Auxiliary Feedwater	5610-M-3075-1,2
075	Auxiliary Feedwater	5613/4-M-3075-1,2,3
094a	Post Accident Hydrogen Monitors	5613/4-M-3094-1
094Ь	Containment Condition Monitoring	5613/4-M-3094-1
094c	Post Accident Sampling	5613/4-M-3094-1
094d	Post Accident Hydrogen Control	5613/4-M-3094-1
101	Breathing Air	5613/4-M-3101-1

ATTACHMENT 2

PUMP RELIEF REQUEST INDEX

(Page 1 of 1)

Relief Request No.	Description	NRC Approval Date
PR-01	Boric Acid Transfer Pump Fixed Resistance	
PR-02	0.25 % Gauge Liquid	
PR-03	Containment Spray Pump Comprehensive Pump Test	
PR-04	RHR Discharge and Suction Pressure Gauge Range Requirements	
PR-05	No Comprehensive Test for Certain Group A Pumps	
PR-06	Categorization of Residual Heat Removal Pumps as Group B (Modes 1-4) and Group A (Modes 5-6)	

ATTACHMENT 3

PUMP RELIEF REQUESTS

IST Program Plan Florida Power and Light Company Turkey Point Nuclear Power Plant 10 CFR 50.55a Request Number PR-01

Proposed Alternative In Accordance with 10 CFR 50.55a(a)(3)(i)

Alternative Provides Acceptable Level of Quality and Safety

1. <u>ASME_Code_Component(s) Affected</u>

3P203A	3A Boric Acid Transfer Pump
3P203B	3B Boric Acid Transfer Pump
4P203A	4A Boric Acid Transfer Pump
4P203B	4B Boric Acid Transfer Pump

2. <u>Applicable Code Edition and Addenda</u>

ASME OM Code 1998 Edition through 2000 Addenda

3. <u>Applicable Code Requirement</u>

ISTB-5121(c) – Where it is not practical to vary system resistance, flow rate and pressure shall be determined and compared to their respective reference values.

4. <u>Reason for Request</u>

Pursuant to 10 CFR 50.55a, "Codes and Standards", paragraph (a)(3), relief is requested from the requirement of ASME OM Code ISTB-5121(c). The basis of the relief request is that the proposed alternative would provide an acceptable level of quality and safety.

The normal test loop for the subject pumps consists of fixed resistance flow paths to limit flow, however, flow measuring instruments are not installed. See Attachment 1, Boric Acid Transfer Pump Test Diagram. Since the system resistance is fixed and can be assumed to be constant, pump degradation can be detected by comparing successive measurements of pump differential pressure.

5. <u>Proposed Alternative and Basis for Use</u>

An alternate test circuit is available in which flow rate may be measured, however this flow path requires injection of highly concentrated boric acid solution into the reactor coolant system. During the quarterly group A test at normal power operations, this test is highly impractical since severe power level fluctuations would be created which would lead to a potential transient and subsequent trip of the reactor. Performing this test at cold shutdown intervals would also result in excessive boration of the reactor coolant system resulting in potential difficulties and delays in restarting the plant.

As an alternative to measuring differential pressure and flow during the group A quarterly test, only the differential pressure will be measured and compared to its reference value. Additionally, vibration measurements are also recorded and compared to their reference values. Manual isolation valves are closed and flow is recirculated back to the boric acid tank. See Attachment 1, Boric Acid Transfer Pump Test Diagram.

During the comprehensive inservice test when flow may be measured, full spectrum analysis will be performed above the required vibration analysis by the Code. When performing the comprehensive pump test, all required parameters will be measured and compared to their reference values.

Additionally, these pumps are included in the station preventive maintenance program which requires a pump inspection and oil analysis to be performed periodically.

Based on the preventive maintenance inspection results, full spectrum analysis, and continued quarterly and comprehensive testing, an accurate assessment of pump health and operational readiness is determined. This alternative provides an acceptable level of quality and safety.

6. **Duration of Proposed Alternative**

This proposed alternative will be utilized for the entire 4th 120 month interval.

7. Precedents

This relief request was previously approved for 3rd Ten Year Interval at Turkey Point as PR-1, and satisfies the requirements of Generic Letter 89-04, Position 9.

IST Program Plan Florida Power and Light Company Turkey Point Nuclear Power Plant 10 CFR 50.55a Request Number PR-01

(Continued)

Attachment 1

Boric Acid Transfer Pump Test Diagram



Proposed Alternative In Accordance with 10 CFR 50.55a(a)(3)(i)

Alternative Provides Acceptable Level of Quality and Safety

1. <u>ASME Code Component(s) Affected</u>

3P203A	3A Boric Acid Transfer Pump
3P203B	3B Boric Acid Transfer Pump
4P203A	4A Boric Acid Transfer Pump
4P203B	4B Boric Acid Transfer Pump
3P211A	3A Component Cooling Water Pump
3P211B	3B Component Cooling Water Pump
3P211C	3C Component Cooling Water Pump
4P211A	4A Component Cooling Water Pump
4P211B	4B Component Cooling Water Pump
4P211C	4C Component Cooling Water Pump
3P215A	3A Safety Injection Pump
3P215B	3B Safety Injection Pump
4P215A	4A Safety Injection Pump
4P215B	4B Safety Injection Pump

2. <u>Applicable Code Edition and Addenda</u>

ASME OM Code 1998 Edition through 2000 Addenda

3. Applicable Code Requirement

ISTB-3520(a) – *Gage Lines*. If the presence or absence of liquid in a gage line could produce a difference of more than 0.25% in the indicated value of the measured pressure, means shall be provided to ensure or determine the presence or absence of liquid as required for the static correction used.

4. <u>Reason for Request</u>

Pursuant to 10 CFR 50.55a, "Codes and Standards", paragraph (a)(3), relief is requested from the requirement of ASME OM Code ISTB-3520(a). The basis of the relief request is that the proposed alternative would provide an acceptable level of quality and safety.

For the group A and comprehensive pump tests, applying the 0.25% limit to low pressure measurements to these pumps results in complex venting procedures requiring valve manipulations, component disassembly, and breech of radioactive and chemically treated systems to perform the test. Turkey Point has implemented and mandated programs and policies to minimize the causes of these types of waste products.

Venting of the suction gages for the purposes of testing does not significantly effect the overall differential pressure measurement, while it significantly impacts the plant waste reduction program.

For the subject pumps, discharge pressure exceeds suction pressure by at least a factor of six, for which a 0.25% error introduced into the suction pressure measurement typically results in an error of 0.05% in the differential pressure calculation. This error is insignificant with respect to the potential 6% error allowance applied to both the suction and discharge pressure instruments.

5. <u>Proposed Alternative and Basis for Use</u>

As an alternative, the introduced error in conjunction with the specific range and accuracy of the gauges utilized will be verified to comply with the minimum Code required accuracy for calculation of the differential pressure. This calculation will verify that the square root of the sum of the errors of the specific gauges utilized, and will include a term to account for the error associated with the presence or absence of liquid, is less than the square root of the sum of the squares of 6 % of the associated suction and discharge lines.

This request applies to the Boric Acid Transfer and Component Cooling water pumps' group A test and all of the subject pumps' comprehensive tests. The Safety Injection pumps are considered group B. Flow rate is the only measured parameter during the group B test of the Safety Injection pumps.

This alternative provides an acceptable level of quality and safety.

6. **Duration of Proposed Alternative**

This proposed alternative will be utilized for the entire 4th 120 month interval.

7. <u>Precedents</u>

This relief request was previously approved for 3rd Ten Year Interval at Turkey Point as PR-4.

IST Program Plan Florida Power and Light Company Turkey Point Nuclear Power Plant 10 CFR 50.55a Request Number PR-03

Proposed Alternative In Accordance with 10 CFR 50.55a(a)(3)(i)

Alternative Provides Acceptable Level of Quality and Safety

1. ASME Code Component(s) Affected

3P214A	3A Containment Spray Pump
3P214B	3B Containment Spray Pump
4P214A	4A Containment Spray Pump
4P214B	4B Containment Spray Pump

2. Applicable Code Edition and Addenda

ASME OM Code 1998 Edition through 2000 Addenda

3. Applicable Code Requirement

ISTB-3300(e)(1) – Reference values shall be established within \pm 20% of pump design flow rate for the comprehensive test.

4. <u>Reason for Request</u>

Pursuant to 10 CFR 50.55a, "Codes and Standards", paragraph (a)(3), relief is requested from the requirement of ASME OM Code ISTB-3300(e)(1). The basis of the relief request is that the proposed alternative would provide an acceptable level of quality and safety.

The specified +/- 20% of pump design flow rate can not be achieved for the subject pumps during normal quarterly Group B testing or during Comprehensive testing. The design flow rate of the containment spray pump is 1450 gpm. This point is also the best efficiency point of the pump.

Attachment 1 is the pump characteristic curve which is representative of the Containment Spray pumps at Turkey Point.

5. Proposed Alternative and Basis for Use

The design of the containment spray system is such that the test loop for the pump consists of a 6" discharge line which separates into a 2" recirculation line back to the pump suction. The 6" discharge line terminates inside containment at the spray nozzles. Testing of the pump at the design flow rate, would require discharging flow through the spray nozzles and subsequently wetting containment. The discharge piping was not designed to be temporarily modified to allow pump design flow without flow being discharged to the containment via the spray nozzles.

During preoperational testing (1971 and 1972 for Unit #3 and Unit #4 respectively), the containment spray pumps were full flow tested. A test loop was constructed by installing a 6" section of piping in place of the discharge check valve (*-890A/B). This temporary section of piping was routed to the plant sump. See Attachment 2, Containment Spray System Preoperational Test Flow Diagram. With the discharge to containment isolated, the pumps were run for at least an hour in the recirculation mode (1" line) taking suction from the Refueling Water Storage Tank (RWST). After operating in recirculation, the pumps were then operated at substantial flow using the temporary test line. Three points on the manufacturers curve were then verified, with the acceptance criteria that the pump head and capacity be above the FSAR performance curve shown in Attachment 1. Each of the pumps delivered at least 1450 gpm when preoperationally tested. Attachments 3 and 4 contain the preoperational data plotted against the performance curve.

It should be noted that the originally installed 1" recirculation line was designed for a flow rate of 50 gpm to prevent pump damage when pumping to a closed loop. In 1982, a test recirculation line was installed for each containment spray pump to allow each pump to be tested at a minimum of 400 gpm for inservice testing purposes. During the design change process it was identified by the pump manufacturer (Gould) that a minimum recirculation flow of 300 gpm be provided for the short duration monthly test and 400 gpm be provided for the annual hour-long test. Turkey Point installed the necessary recirculation test flow path under design change PC/M 82-19, 20 on both Unit #3 and Unit #4. See Attachment 5, Current Containment Spray System Diagram.

As an alternative to testing at +/- 20 % of design flow, the test recirculation loop shown in Attachment 5 will be used. The reference flows are established at approximately 400 gpm, versus a design flow of 1450 gpm. The low flow rate is due to the 2" recirculation line. At this reference point of 400 gpm, the characteristic curve for the pump is not horizontal. Pump degradation as noted by measuring differential pressure can be detected for a given flow rate reference value.

The reference flow rate of 400 gpm corresponds to 27.6 % of pump design flow. At the reference conditions the flow values are currently at a point on the curve (Attachment 1) that is well sloped and repeatable. Any degradation in pump performance at the set flow rate be recognized or detected through a substantial change in measured pump differential pressure.

To establish the flow rate within \pm 20 % of design would require a flow rate of at least 1160 gpm. Establishing flows at 1160 gpm does not increase the ability to detect degradation or assess pump conditions since the slope of the pump curve is essentially constant from shutoff head to 1250 gpm. Therefore, testing at higher flows does not increase the ability to detect hydraulic degradation.

Past test data for the Unit #3 and #4 containment spray pumps is presented in Attachments 6 and 7 respectively. This test data was collected during the corresponding inservice test with the pump operating at a set flow rate of 400 gpm. Comparing this test data to the original pump performance and preoperational curves in Attachments 3 and 4 demonstrates the pumps are operating above the original performance curve and at or above the original preoperational curve. Additionally, vibration data collected during the inservice tests, has been below 0.325 in/sec in all cases. Based on this mechanical and hydraulic data, and the maintenance history, there is reasonable assurance that the pumps would perform their intended design function. Projecting the hydraulic pump performance at substantial flow rates would be expected to be above the performance curve at the design point, with adequate margin. Mechanical vibration projected at substantial flows would tend to be less than that at the reduced flow test point.

As expected, insignificant degradation has been experienced since these pumps are only operated for testing purposes.

To compensate for testing the containment spray pumps at reduced flow rates during the comprehensive test, as required by ISTB-3300(e)(1), additional activities will be performed as follows to assess operational readiness and determine pump health.

During all comprehensive inservice testing, full spectrum analysis is performed above the required vibration analysis by the Code. Additionally, these pumps are included in the station Preventive Maintenance Program which requires a pump inspection and oil analysis to be performed periodically. Based on the preventive maintenance inspection results, full spectrum analysis, oil analysis, and continued quarterly and comprehensive testing within 27.6% of design pump flow, an accurate assessment of pump health and operational readiness is determined.

Additionally, Turkey Point has previously modified the system to increase the test flow rate. However, reestablishing the full flow test loop for the purpose of periodic testing would require modifications to the plant and removal of check valve (*-890A/B). Post maintenance testing of system and verification of check valve (*-890A/B) would be a substantial burden. Substantial flow can only be achieved through the 6" discharge line which ultimately requires flow through the spray nozzles. A temporary modification to plug the nozzles and install a test return line capable of passing pump design flow would be highly labor intensive and would require a permanent modification to the containment spray piping system.

6. Duration of Proposed Alternative

This proposed alternative will be utilized for the entire 4th 120 month interval.

7. Precedents

- Similar relief request PR-6 was previously approved for North Anna Power Station on January 8, 2002. Docket Nos. 50-338 and 50-339 (TAC Nos. MB2221and MB2222).
- Similar relief request PR-1 was previously approved for Seabrook Station on May 30, 2003. Docket No. 50-443 (TAC No. MB6676).

Attachment 1

Containment Spray Pump Characteristic Curve



▲ - Pump Design Point (1450 gpm)

 \triangle - Pump Test Point (set parameter is flow at 400 gpm)

Attachment 2

Containment Spray System Preoperational Test Flow Diagram



10 CFR 50.55a Request Number PR-03 (Continued)

Attachment 3

Containment Spray Pump Preoperational Data - Unit #3





(Continued)

Attachment 4

Containment Spray Pump Preoperational Data - Unit #4





Attachment 5

Current Containment Spray System Diagram



^{---- 2&}quot; Test Recirculation Line

Attachment 6

Containment Spray Pump Operational Data - Unit #3

3A Containment Spray Pump DP Data @400 gpm



3B Containment Spray Pump DP Data @400 gpm



Attachment 7

Containment Spray Pump Operational Data - Unit #4

4A Containment Spray Pump DP Data @400 gpm





Proposed Alternative In Accordance with 10 CFR 50.55a(a)(3)(I)

Alternative Provides Acceptable Level of Quality and Safety

1. ASME Code Component(s) Affected

3P210A	3A Residual Heat Removal Pump
3P210B	3B Residual Heat Removal Pump
4P210A	4A Residual Heat Removal Pump
4P210B	4B Residual Heat Removal Pump

2. Applicable Code Edition and Addenda

ASME OM Code 1998 Edition through 2000 Addenda

3. <u>Applicable Code Requirement</u>

1STB-3510(b)(1) - The full-scale range of each analog instrument shall be not greater than three times the reference value.

4. <u>Reason for Request</u>

Pursuant to 10 CFR 50.55a, "Codes and Standards", paragraph (a)(3), relief is requested from the requirement of ASME OM Code ISTB-3510(b)(1). The basis of the relief request is that the proposed alternative would provide an acceptable level of quality and safety.

The installed suction and discharge pressure gauges of the residual heat removal pumps are sized to accommodate the pressure range of 4 to 600 psig expected under standby, cold shutdown, and emergency operation modes. The instrument range is 0 to 600 psig. As a result, the instrument range exceeds the requirement of ISTB-3510(b)(1) since during the quarterly and cold shutdown inservice tests, the suction/discharge pressures may be considerably less than the range requirements of ISTB-3510(b)(1).

5. <u>Proposed Alternative and Basis for Use</u>

As an alternative, the use of existing instrumentation, without meeting the 1/3 range requirements of the Code but which exceed the Code required accuracies will be applied to all inservice tests of the RHR pumps. This alternative will adequately provide for monitoring pump health conditions for the following reasons:

These specific gauges are calibrated to an accuracy of +/- 0.25 % and are of the "twice around" type such that they may accurately indicate pressure over all modes of Residual Heat Removal operations (Shutdown Cooling and Emergency Core Cooling). The gauge range on the first revolution is 0 to 300 psig and 300 to 600 psig on the second revolution. See Attachment 2, RHR Suction and Discharge Pressure Gauge.

Suction Pressure

Suction pressure measurements are recorded and used to derive the pump differential pressure through calculation. The accuracy of the suction pressure measurement normally has little or no effect on the results of this calculation since, generally, the pump discharge pressure exceeds the suction pressure by 6 to 7 times the reference value. When determining pump differential pressure (DP), typically the RHR pump DP is approximately 100 psi (discharge pressure approximately 120 psig while suction pressure is approximately 20 psig). The maximum effect of suction pressure inaccuracies is $0.25\% \times 600$ psig, or 1.5 psig. The Code required gauge range for this suction pressure reference value (20 psig) would be 0 to 60 psig. The Code accuracy requirement of 2% would cause a maximum inaccuracy of 2.0% x 60 psig, or 1.2 psig. See Attachment 1.

Discharge Pressure

Discharge pressure measurements are also recorded and used to derive the pump differential pressure through calculation. When determining pump differential pressure (DP), typically the RHR pump DP is approximately 100 psig (discharge pressure approximately 120 psig while suction pressure is approximately 20 psig). The maximum effect of the discharge pressure inaccuracies is $0.25\% \times 600$ psig, or 1.5 psig. The Code required gauge range for this discharge pressure reference value (120 psig) would be 0 to 360 psig. The Code accuracy requirement of 2% would cause a maximum inaccuracy of 2.0% x 360 psig, or 7.2 psig. See Attachment 1.

Combination

Based on the inaccuracies of the suction and discharge pressure gauges (+/-1.5 psig), the largest possible error in the differential pressure calculation is +/-3 psig. Use of gauges with Code required ranges, and applying the Code accuracy requirements, the largest possible inaccuracies would be 1.2 psig + 7.2 psig, or 8.4 psig. See Attachment 1.

Therefore, the use of permanently installed pressure instruments which exceed the Code required accuracies but do not meet the Code range requirements would reduce the overall instrument inaccuracies with respect to differential pressure for the quarterly test from 8.4 psig to 3.0 psig.

For the comprehensive pump test, the overall inaccuracy of the currently installed instruments is 3.0 psig versus 2.1 psig for an instrument which meets the range requirements. This difference is less than 1% (0.9 psig) of the overall reference differential pressure of 100 psi.

Additionally, during the RHR pump comprehensive testing, full vibration spectrum analysis is performed above the Code required vibration analysis. Further, these pumps are included in the station preventive maintenance program which requires each pump to be inspected on a periodic basis.

<u>10 CFR 50.55a Request Number PR-04</u> (Continued)

Based on the preventive maintenance inspection results, full spectrum analysis, and continued quarterly and comprehensive testing with the permanently installed pressure gauges, an accurate assessment of pump health and operational readiness is determined.

This alternative provides an acceptable level of quality and safety.

6. **Duration of Proposed Alternative**

This proposed alternative will be utilized for the entire 4th 120 month interval.

7. Precedents

A similar relief request was previously approved for 3rd Ten Year Interval at Turkey Point as PR-3.
IST Program Plan Florida Power and Light Company ______Turkey Point Nuclear Power Plant 10 CFR 50.55a Request Number PR-04 (Continued)

Attachment 1

Gauge Ranges and Accuracy Comparison

The following tables present a comparison between the permanently installed pressure gauges on the RHR pumps at Turkey Point along with the Code required ranges and accuracies for both a Group A or B test and a Comprehensive test.

Suction Pressure

	Gauge Range	Accuracy	Suction Pressure Inaccuracy
Turkey Point	0 – 600 psig	0.25 %	1.5 psig
Group A or B Test	0 – 60 psig	2.0 %	1.2 psig
Comprehensive Test	0 – 60 psig	0.5 %	0.3 psig

Discharge Pressure

	Gauge Range	Accuracy	Discharge Pressure Inaccuracy
Turkey Point	0 – 600 psig	0.25 %	1.5 psig
Group A or B Test	0 – 360 psig	2.0 %	7.2 psig
Comprehensive Test	0 – 360 psig	0.5 %	1.8 psig

Combination – Differential Pressure

Suction Gauge Range		Suction Pressure Accuracy	Discharge Gauge Range	Discharge Pressure Accuracy	Total Inaccuracy
Turkey Point	0 – 600 psig	0.25 % (1.5 psig)	0 – 600 psig	0.25 % (1.5 psig)	3.0 psig
Group A or B Test	0 – 60 psig	2.0 % (1.2 psig)	0 – 360 psig	2.0 % (7.2 psig)	8.4 psig
Comprehensive Test	0 – 60 psig	0.5 % (0.3 psig)	0 – 360 psig	0.5 % (1.8 psig)	2.1 psig

10 CFR 50.55a Request Number PR-04 (Continued)

Attachment 2

RHR Suction and Discharge Pressure Gauge



IST Program Plan Florida Power and Light Company Turkey Point Nuclear Power Plant 10 CFR 50.55a Request Number PR-05

Proposed Alternative In Accordance with 10 CFR 50.55a(a)(3)(i)

Alternative Provides Acceptable Level of Quality and Safety

1. <u>ASME Code Component(s) Affected</u>

3P201A	3A Charging Pump
3P201B	3B Charging Pump
3P201C	3C Charging Pump
3P211A	3A Component Cooling Water Pump
3P211B	3B Component Cooling Water Pump
3P211C	3C Component Cooling Water Pump
3P9A	3A Intake Cooling Water Pump
3P9B	3B Intake Cooling Water Pump
3P9C	3C Intake Cooling Water Pump
4P201A	4A Charging Pump
4P201B	4B Charging Pump
4P201C	4C Charging Pump
4P211A	4A Component Cooling Water Pump
4P211B	4B Component Cooling Water Pump
4P211C	4C Component Cooling Water Pump
4P9A	4A Intake Cooling Water Pump
4P9B	4B Intake Cooling Water Pump
4P9C	4C Intake Cooling Water Pump

2. <u>Applicable Code Edition and Addenda</u>

ASME OM Code 1998 Edition through 2000 Addenda

3. <u>Applicable Code Requirement</u>

ISTB-5123, 5223, 5323 – Comprehensive Test Procedure.

4. <u>Reason for Request</u>

Pursuant to 10 CFR 50.55a, "Codes and Standards", paragraph (a)(3), relief is requested from the requirement of ASME OM Code ISTB-5123, 5223, and 5323. The basis of the relief request is that the proposed alternative would provide an acceptable level of quality and safety.

The subject pumps are all categorized as group A pumps. These pumps are operated routinely during normal plant operations. Each pump is tested in accordance with its associated group A procedure. All of these pumps are operated at conditions within +/-20% of the design flow rate when tested each quarter (see attachments to this request). All of the required Code parameters are measured and compared to their respective reference values.

IST Program Plan Florida Power and Light Company <u>Turkey Point Nuclear Power Plant</u> <u>10 CFR 50.55a Request Number PR-05</u> (Continued)

At least once every two years, during the group A test, a full spectrum vibration analysis will be performed above the required vibration analysis by the Code. Additionally, these pumps are included in the station preventive maintenance program which requires a pump inspection and oil analysis to be performed periodically.

The intent of the Code required Comprehensive Test is to test the pump at substantial flow (biennially) such that pump degradation may be easily detected on the portion of the pump curve which is well sloped. Turkey Point tests each of these pumps at substantial flow (+/- 20% of design) each quarter.

Intake Cooling Water Pump

See Attachment 1, Intake Cooling Water Pump Curve

Inservice Testing Basis

The intake cooling water pump is required to operate to supply cooling water from the intake structure to the tube side of the component cooling water heat exchangers during design basis accident conditions to ensure heat removal capabilities of the component cooling water system [UFSAR 9.6.2]. The intake cooling water pumps supply cooling flow to the component cooling water and turbine plant cooling water system loads during normal plant operations, however, only one pump is required to satisfy design basis accident conditions. The C intake cooling water pump automatically starts on a loss of power or safety injection signal if either the A or B pump breaker is open. [UFSAR 9.6.2].

The intake cooling water pump is designed to deliver 16,000 gpm at 60 feet of developed head (approximately 26 psi) to the component cooling water heat exchangers during design basis accident conditions [DBD-019].

Inservice Testing

The Intake Cooling Water Pumps are vertical line shaft pumps. These pumps are tested each quarter in accordance with Turkey Point Operating Surveillance *-OSP-19.1. Each pump is tested at a flow rate of 15,400 gpm, which corresponds to the design accident flow rate of the system. During this test, the flow rate is set, while the differential pressure is measured. After the stabilization period, all required parameters of Table ISTB-3000-1 are measured and compared to the acceptance criteria of Table ISTB-5200-1. The design flow rate of the Intake Cooling Water Pump is 16,000 gpm. The test point of 15,400 gpm, corresponds to 96.25% of the design flow rate.

10 CFR 50.55a Request Number PR-05 (Continued)

Test Results

The following data tables indicate the hydraulic test data collected for the last inservice tests. Based on these results, pump operation has been acceptable. Applying the group A pump acceptance criteria to these pumps indicates acceptable performance. Additionally, if the comprehensive acceptance criteria would be applied, the data would also indicate acceptable performance.

3A ICW Pump Test Results

Date	Flow	DP	DP Reference	Group A Accept	Comprehensive Accept	
9/13/03	15400	27.5	27.1	25.7 - 29.8	25.7 - 27.9	

3B ICW Pump Test Results

Date	Flow	DP	DP Reference	Group A Accept	Comprehensive Accept	
9/13/03	15400	27.6	27.1	25.7 - 29.8	25.7 – 27.9	

3C ICW Pump Test Results

Date	Flow	DP	DP Reference	Group A Accept	Comprehensive Accept
9/13/03	15400	26.1	26.8	25.5 - 29.5	25.5 - 27.6

4A ICW Pump Test Results

Date	e Flow DP DP Reference		DP Reference	Group A Accept	Comprehensive Accept	
9/20/03	15400	26.2	27.2	25.8 - 29.9	25.8 - 28.0	

4B ICW Pump Test Results

Date	Flow	DP DP Reference		Group A Accept Comprehensive Acce		
9/20/03	15400	26.7	28.0	26.6 - 30.8	26.6 - 28.8	

4C ICW Pump Test Results

Date	Flow	DP	DP Reference	Group A Accept	Comprehensive Accept
9/20/03	15400	25.8	26.8	25.5 - 29.5	25.5 - 27.6

Charging Pumps

Inservice Testing Basis

The charging pump is required to pump water from the emergency boration makeup system or RWST to the reactor coolant system during emergency boration conditions [UFSAR 9.2.2/14.2.6]. The charging pump is designed to deliver 77 gpm @2385 psig of developed head to the reactor coolant system [UFSAR Table 9.2-3].

<u>10 CFR 50.55a Request Number PR-05</u> (Continued)

The charging pump takes suction from the volume control tank and discharges to the reactor coolant system through the tube side of the regenerative heat exchanger during normal operations [UFSAR 9.2]. This function is not required for safe shutdown or accident mitigation.

Inservice Testing

The Charging Pumps are positive displacement pumps. These pumps are tested each quarter in accordance with Turkey Point Operating Surveillance *-OSP-47.1. Each pump is tested at a flow rate of greater than 81 gpm, which corresponds to the design accident flow rate of the system. During this test, speed is set, while the resistance of the system can not be varied. Since the pump is a positive displacement type pump both the flow rate and the discharge pressure are measured. After the stabilization period, all required parameters of Table ISTB-3000-1 are measured and compared to the acceptance criteria of Table ISTB-5300-2. The design flow rate of the Charging Water Pump is 77 gpm. The test point of 81 gpm corresponds to 105 % of the design flow rate.

The Charging Pump is a positive displacement pump. No pump curve is provided.

Test Results

The following data tables indicate the hydraulic test data collected for the last inservice tests. Based on these results, pump operation has been acceptable. Applying the group A pump acceptance criteria to these pumps indicates acceptable performance. Additionally, if the comprehensive acceptance criteria would be applied, the data would also indicate acceptable performance.

3A Charging Pump Test Results

Date	Press	Press. Ref	Group A Accept Range	Comp Accept Range	Flow	Flow Ref	Group A Accept Range	Comp Accept Range
8/24/03	2350	2350	2186 - 2585	2186 - 2420	77.3	81.3	77.2 - 89.4	77.2 - 83.7

3B Charging Pump Test Results

Date	Press	Press. Ref	Group A Accept	Group A Comp Accept Accept		Flow Ref	Group A Accept	Comp Accept
			Range	Range			Range	Range
8/17/03	2350	2340	2176 - 2574	2176 - 2410	77.2	81.0	77.0 - 89.1	77.0 - 83.4

3C Charging Pump Test Results

Date	Press	Press. Ref	Group A Accept Range	Comp Accept Range	Flow	Flow Ref	Group A Accept Range	Comp Accept Range
8/24/03	2325	2350	2186 - 2585	2186 - 2420	77.8	81.4	77.3 - 89.5	77.3 - 83.8

<u>10 CFR 50.55a Request Number PR-05</u> (Continued)

4A Charging Pump Test Results

Date	Press	Press. Ref	Group A Accept Range	Comp Accept Range	Flow	Flow Ref	Group A Accept Range	Comp Accept Range
7/02/03	2350	2300	2139 - 2530	2139 - 2369	81.1	81.5	77.4 - 89.7	77.4 - 83.9

4B Charging Pump Test Results

Date	Press	Press. Ref	Group A Accept	Comp Accept	Flow	Flow Ref	Group A Accept	Comp Accept
			Range	Range			Range	Range
9/13/03	2390	2400	2232 - 2640	2232 - 2472	80.5	81.0	77.0 - 89.1	77.0 - 83.4

4C Charging Pump Test Results

Date	Press	Press. Ref	Group A Accept Range	Comp Accept Range	Flow	Flow Ref	Group A Accept Range	Comp Accept Range
9/13/03	2450	2390	<u>2223 - 2</u> 629	2223 - 2461	80.5	82.0	77.9 - 90.2	77.9 - 84.5

Component Cooling Water Pump

See Attachment 2, Component Cooling Water Pump Curve

Inservice Testing Basis

The component cooling water pump is required to operate to supply cooling water to the shell side of the component cooling water heat exchangers during design basis accident conditions to ensure heat removal capabilities of the component cooling water system [UFSAR 9.3.2]. One pump and three component cooling water heat exchangers are normally operated to provide cooling water for various components located in the auxiliary and containment buildings [UFSAR 9.3.1]. Following a loss-of-coolant accident, one component cooling water pump and two component cooling water heat exchangers accommodate the heat removal loads [UFSAR 9.3.3].

The component cooling water pump is designed to deliver 7,500 gpm at 185 feet of developed head to the component cooling water heat exchangers during design basis accident conditions [UFSAR Table 9.3-1].

The pump is operated during normal operations and shutdowns to supply cooling water for the component cooling water system loads [UFSAR 9.3.2]. These functions are not required for safe shutdown or accident mitigation.

10 CFR 50.55a Request Number PR-05

(Continued)

Inservice Testing

The Component Cooling Water Pumps are centrifugal pumps. These pumps are tested each quarter in accordance with Turkey Point Operating Surveillance *-OSP-30.1. Due to the configuration of the system the A pump is tested at a flow rate of 6,500 gpm and the B and C pumps are tested at 8500 gpm each quarter. During this test, the flow rate is set, while the differential pressure is measured. After the stabilization period, all required parameters of Table ISTB-3000-1 are measured and compared to the acceptance criteria of Table ISTB-5100-1. The design flow rate of the Component Cooling Water Pump is 7,500 gpm. Therefore the test point of 6,500 gpm, corresponds to 86.7% of the design flow rate for the A pumps while the test point of 8,000 gpm corresponds to 106.7% for the B and C pumps.

Test Results

The following data tables indicate the hydraulic test data collected for the last inservice tests. Based on these results, pump operation has been acceptable. Applying the group A pump acceptance criteria to these pumps indicates acceptable performance. Additionally, if the comprehensive acceptance criteria would be applied, the data would also indicate acceptable performance.

3A Component Cooling Water Pump Test Results

Date	Flow	DP	DP Reference	Group A Accept	Comprehensive Accept
7/6/03	6500	84.0	87.7	78.9 - 96.5	81.6 - 90.3

3B Component Cooling Water Pump Test Results

Date	Flow	DP	DP Reference	Group A Accept	Comprehensive Accept
7/6/03	8000	76.0	79.0	71.1 - 86.9	73.5 - 81.4

3C Component Cooling Water Pump Test Results

Date	Flow	DP	DP Reference	Group A Accept	Comprehensive Accept
8/3/03	8000	78.0	82.5	74.3 - 90.8	76.7 - 85.0

4A Component Cooling Water Pump Test Results

Date	Flow	DP	DP Reference	Group A Accept	Comprehensive Accept
6/29/03	6500	83.0	87.7	78.9 - 96.5	81.6-90.3

4B Component Cooling Water Pump Test Results

Date	Flow	DP	DP Reference	Group A Accept	Comprehensive Accept
6/27/03	8000	77.0	78.5	70.7 - 86.4	73.0 - 80.9

4C Component Cooling Water Pump Test Results

Date	Flow	DP	DP Reference	Group A Accept	Comprehensive Accept
6/29/03	8000	78.0	78.2	70.4 - 86.0	72.7 - 80.5

IST Program Plan Florida Power and Light Company <u>Turkey Point Nuclear Power Plant</u> <u>10 CFR 50.55a Request Number PR-05</u> (Continued)

5. <u>Proposed Alternative and Basis for Use</u>

As an alternative to performing Comprehensive Pump tests biennially, the subject pumps will be tested each quarter at +/- 20% of the design flow rate. The required inservice test parameters of Table ISTB-3000-1 based on pump type will be measured and compared to their reference values. The group A pump test acceptance criteria will be applied. Additionally, once every two years, full spectrum analysis will be performed above the Code required vibration measurements. Continued Preventive Maintenance, including periodic pump inspections and oil analysis, on each pump will assist in determining overall mechanical and hydraulic pump health.

Based on the preventive maintenance inspection results, full spectrum analysis, and continued quarterly group A testing at +/- 20% of design pump flow, an accurate assessment of pump health and operational readiness is determined on a quarterly frequency.

This alternative provides an acceptable level of quality and safety.

6. <u>Duration of Proposed Alternative</u>

This proposed alternative will be utilized for the entire 4th 120 month interval.

7. <u>Precedents</u>

None

<u>10 CFR 50.55a Request Number PR-05</u> (Continued)

Attachment 1

Intake Cooling Water Pump Curve



▲ - Pump Design Point (16000 gpm @ 60 feet of developed head)

 \triangle - Pump Test Point (set parameter is flow at 15400 gpm)

<u>10 CFR 50.55a Request Number PR-05</u> (Continued)

Attachment 2

Component Cooling Water Pump Curve



▲ - Pump Design Point (7500 gpm @ 185 feet of developed head)

 \triangle - Pump Test Point (set parameter is flow at 8000 gpm)

IST Program Plan Florida Power and Light Company <u>Turkey Point Nuclear Power Plant</u> 10 CFR 50.55a Request Number PR-06

Proposed Alternative In Accordance with 10 CFR 50.55a(a)(3)(i)

Alternative Provides Acceptable Level of Quality and Safety

1. ASME Code Component(s) Affected

Pump Number	Function
3P210A	Residual Heat Removal
3P210B	Residual Heat Removal
4P210A	Residual Heat Removal
4P210B	Residual Heat Removal

2. <u>Applicable Code Edition and Addenda</u>

ASME OM Code 1998 Edition through 2000 Addenda

3. <u>Applicable Code Requirement</u>

ISTB-1400(b), "identify each pump to be tested in accordance with the rules of this Subsection and categorize it as either a group A or group B pump and list the pumps in the plant records (see ISTB-9000). A pump that meets both group A and group B definitions shall be categorized as a group A pump."

4. <u>Reason for Request</u>

Pursuant to 10 CFR 50.55a, "Codes and Standards", paragraph (a)(3), relief is requested from the requirement of ASME OM Code ISTB-1400(b). The basis of the relief request is that the proposed alternative would provide an acceptable level of quality and safety.

The Residual Heat Removal pumps meet the categorization requirements of group A pumps in that they are operated routinely during plant shutdowns (Mode 5-6). However, these pumps also meet the requirements of group B, in that during normal operation (Modes 1-4) they are not operated except for testing.

During normal power operations, Modes 1-4, the residual heat removal pump is in a standby condition and is considered an essential part of the Emergency Core Cooling System (ECCS). The pump starts automatically upon receipt of a safety injection signal taking suction from the RWST during the injection phase of an accident. The pump is then aligned to take suction from the containment sump during the recirculation phase of an accident. The pump discharges to the reactor coolant system via the residual heat removal heat exchangers. The pump may also be aligned to pump to the suction of either the safety injection pumps or the containment spray pumps depending on plant emergency conditions. During normal plant shutdowns, the residual heat removal pump is used to cool down the reactor coolant system (shutdown cooling). This shutdown cooling function is not required for safe shutdown or accident mitigation.

IST Program Plan Florida Power and Light Company <u>Turkey Point Nuclear Power Plant</u> <u>10 CFR 50.55a Request Number PR-06</u> (Continued)

ASME ISTB-1400(b) states that if a pump meets both group A and group B definitions, it shall be categorized as a group A pump. The Residual Heat Removal pumps are tested during normal operation, Modes 1-4, using the minimum flow recirculation loop. This current test is essentially a group B test in that the pump is operated at low flow conditions (approximately 300 gpm) on minimum flow recirculation. The design flow rate of the Residual Heat Removal Pumps is 3750 gpm. This flow rate can only be achieved during shutdown periods (Modes 5-6) when injection into the reactor coolant system is possible. See Attachment 1, RHR System Diagram. Attachment 2, RHR Pump Characteristic Curve is also supplied,

The performance of a group A test at these low flow conditions does not reflect the intent of the Code for group A tests. Additionally, these pumps can not be tested as Group A or Comprehensive in these modes due to using the minimum flow recirculation line.

5. <u>Proposed Alternative and Basis for Use</u>

Turkey Point Nuclear Plant will test the Residual Heat Removal pumps as standby (group B) during Modes 1-4 and as routinely operated pumps (group A) when the plant is in Modes 5-6. When in cold shutdown or refueling, a comprehensive test may be substituted for the group A test should the comprehensive test schedule come due. ISTB-5000 permits substitution of a comprehensive test for a group A test.

This alternative is consistent with Generic Letter 89-04, Position 9, in which the NRC determined that, in cases where flow can only be established through a non-instrumented, minimum flow path during quarterly pump testing, and a path exists at cold shutdown or refueling outages to perform a test of the pump under full or substantial flow conditions, the increased interval is an acceptable alternative to the Code requirements.

Therefore testing the Residual Heat Removal pumps as group B during Modes 1-4 and as group A during Modes 5-6 provides reasonable assurance of the operational readiness of the pumps and provides an acceptable level of quality and safety.

6. <u>Duration of Proposed Alternative</u>

This proposed alternative will be utilized for the entire 4th 120 month interval.

7. <u>Precedents</u>

Similar relief request PR-12 was previously approved for Calvert Cliffs Nuclear Power Plant on May 16, 2002.

Docket Nos. 50-317 and 50-318 TAC Nos. MB3782 and MB3783

10 CFR 50.55a Request Number PR-06

(Continued)

Attachment 1

RHR System Diagram



To Other RHR Pump

IST Program Plan Florida Power and Light Company <u>Turkey Point Nuclear Power Plant</u> 10 CFR 50.55a Request Number PR-06

(Continued)

Attachment 2

RHR Pump Characteristic Curve



▲ - Full Flow Test Point (3750 gpm @ 240 feet of developed head)

 \triangle - Minimum Flow Test Point (Approximately 300 gpm)

ATTACHMENT 4

VALVE RELIEF REQUEST INDEX

(Page 1 of 1)

Relief Request No.	Description	NRC Approval Date
VR-01	Exercise Testing of Option B Check Valves with Only a Closed Safety Function	
VR-02	Position Indication Verification Performed in Accordance with Appendix J Seat Leakage Testing Frequency for Solenoid Operated Valves	
VR-03	Auxiliary Feedwater Pump Discharge Check Valve, 20-143, Exercise Frequency	

ATTACHMENT 5

VALVE RELIEF REQUESTS

Revision Date: 02/11/04

IST Program Plan Florida Power and Light Company Turkey Point Nuclear Power Plant 10 CFR 50.55a Request Number VR-01

Proposed Alternative In Accordance with 10 CFR 50.55a(a)(3)(i)

Alternative Provides Acceptable Level of Quality and Safety

1. <u>ASME Code Component(s) Affected</u>

Valve Number	Class	Category	Function
BA-3-201	2	AC	Containment Breathing Air Isolation Check Valve
3-40-340A	2	AC	Instrument Air to Containment Check Valve
3-40-336	2	AC	Instrument Air to Containment Check Valve
3-10-567	2	AC	Primary Water to Containment Check Valve
3-298A	1	AC	Reactor Coolant Pump Seal Injection Check Valve
3-298B	1	AC	Reactor Coolant Pump Seal Injection Check Valve
3-298C	1	AC	Reactor Coolant Pump Seal Injection Check Valve
3-945E	2	AC	Nitrogen Supply to Accumulators Check Valve
3-518	2	AC	Nitrogen Supply to Pressurizer Relief Tank
3-519	2	AC	Nitrogen Supply to Pressurizer Relief Tank
BA-4-201	2	AC	Containment Breathing Air Isolation Check Valve
4-40-340A	2	AC	Instrument Air to Containment Check Valve
4-40-336	2	AC	Instrument Air to Containment Check Valve
4-10-567	2	AC	Primary Water to Containment Check Valve
4-298A	1	AC	Reactor Coolant Pump Seal Injection Check Valve
4-298B	1	AC	Reactor Coolant Pump Seal Injection Check Valve
4-298C	1	AC	Reactor Coolant Pump Seal Injection Check Valve
4-945E	2	AC	Nitrogen Supply to Accumulators Check Valve
4-518	2	AC	Nitrogen Supply to Pressurizer Relief Tank
4-519	2	AC	Nitrogen Supply to Pressurizer Relief Tank

2. Applicable Code Edition and Addenda

ASME OM Code 1998 Edition through 2000 Addenda

3. <u>Applicable Code Requirement</u>

ISTC-3510 Exercising Test Frequency, states that "Active Category A, Category B, and Category C check valves shall be exercised nominally every 3 months, except as provided by ISTC-3520, ISTC-3540, ISTC-3550, ISTC 3560, ISTC-5221, and ISTC-5222.".

Specifically, relief is requested from performing both the open and closed exercise tests in accordance with ISTC-3510. These valves will be exercised open and closed commensurate Appendix J Option B test frequency requirements.

10 CFR 50.55a Request Number VR-01

(Continued)

4. <u>Reason for Request</u>

Pursuant to 10 CFR 50.55a, "Codes and Standards", paragraph (a)(3), relief is requested from the requirement of ASME OM Code ISTC-3510. The basis of the relief request is that the proposed alternative would provide an acceptable level of quality and safety.

The subject valves are all categorized as AC and are all considered containment isolation valves per the plant safety analysis. All of the subject valves have a safety function to close in order to isolate containment from their respective non-safety related systems during a Loss of Coolant Accident (LOCA) requiring containment isolation. The open function for each of these valves is considered a non-safety function since the systems are not required to shut the plant down to a safe shutdown condition, maintain safe shutdown or mitigate the consequences of an accident (See IST Basis Documents – Safety Function in Attachment 1). However, the current ASME OM Code requirements complied with by Turkey Point (1998 Edition through 2000 Addenda) for the 4th 120-Month Interval, requires testing of the non-safety "open" direction function of each of these check valves. The Code required frequency specified in ISTC-3520 is once every quarter with the exceptions listed above. Those exceptions which apply to check valves are ISTC-3520, ISTC-5221 and ISTC-5222.

Since these valves can be exercised adequately with flow in the open direction and seat leakage tested in the reverse direction, they are not candidates for a disassembly and examination program or condition monitoring program as delineated in ISTC-5221 and ISTC-5222 respectively.

Therefore the frequency requirements of ISTC-3520 would typically apply. That is, if exercising is not practicable during normal power operations the exercising shall be performed during cold shutdowns. If exercising is not practicable during normal power operations and cold shutdown, exercising shall be performed during refueling outages.

Each of the subject valves is required to be exercised both open and closed and seat leakage tested in accordance with the inservice testing requirements of Table ISTC-3500-1, INSERVICE TESTING REQUIREMENTS. For all of the subject valves, the seat leakage test constitutes the exercise closed test. This frequency is in accordance with the Appendix J frequency, since the only safety function of the valves in the closed direction is for containment isolation only. (See ISTC-3620 and Attachment 1, IST Basis Documents – Safety Function)

The open, non-safety direction test, can only be performed using flow when the containment isolation seat leakage test is performed, and only during refueling outages when containment entry is possible. Since the individual valve being tested must have its system properly drained, vented, and aligned correctly prior to performing the seat leakage test, an opportune window will exist to perform the open check valve test using flow. Additionally, test personnel, radiation exposure, and time/labor involved will be significantly reduced by performing the open exercise test along with the seat leakage/closure test (keeping in mind that this open test is the non-safety position test).

On October 4, 1996, Turkey Point received a Safety Evaluation with approval to implement Option B of the 10CFR50 Appendix J Program. (Technical Specification

IST Program Plan Florida Power and Light Company <u>Turkey Point Nuclear Power Plant</u> <u>10 CFR 50.55a Request Number VR-01</u> (Continued)

Amendments 192/186 for Unit #3 and #4 respectively). This program permits the extension of the Appendix J seat leakage testing to a frequency corresponding to the specific valve performance. Valves whose leakage test results indicate good performance may have their interval of testing increased based on these test results. The Turkey Point administrative program which implements Appendix J Option B requires individual containment isolation valves to pass four successful seat leakage tests before it can be included in the Option B program.

5. **Proposed Alternative and Basis for Use**

For the subject valves, Turkey Point Nuclear Plant will perform the check valve closure test in conjunction with the seat leakage test at a frequency in accordance with 10CFR50 Appendix J. The corresponding check valve open test (non-safety direction) will be performed at the same interval as the check valve closure test. This interval may be adjusted to a frequency of testing commensurate with Option B of 10CFR50 Appendix J Type C leakage testing based on valve seat leakage performance.

The only safety function of these valves is to provide a containment isolation barrier. Since they are not connected to any ECCS system and the open function is not required for safe shutdown or accident mitigation, a seat leakage test is their primary functional test. By verification of forward flow, along with a seat leakage test, an adequate assessment of valve health may be determined.

Performance of the both the open and closed tests during the same frequency has been endorsed by the ASME OM Code as stated in ISTC-3522(a), which states that "open and closed tests need only be performed at an interval when it is practicable to perform both tests". Additionally, performance of the check valve open test will include verification of fluid flow to open the check valve. This test will be performed during the same surveillance which seat leakage tests the valve (*-OSP-51.5) and will be scheduled and documented in the plant record system. Corrective actions will be taken in accordance with ISTC-5224 as stated.

Additionally, all of the subject check valves are included in the plant Check Valve Program which monitors check valve test performance, work history, industry experience and vendor correspondence to determine preventive maintenance (PM) activities. The Turkey Point Option B program further monitors the performance of the valve in that the allowable seat leakage limits for each individual valve are administratively set well below the Appendix J limit.

Therefore, the ability to detect degradation and ensure the operational readiness of the subject check valves to perform their intended function is not jeopardized by performing the open and closed check valve tests at the same frequency as specified by Option B. This frequency of testing provides reasonable assurance of the operational readiness of the subject check valves and provides an acceptable level of quality and safety.

IST Program Plan Florida Power and Light Company <u>Turkey Point Nuclear Power Plant</u> <u>10 CFR 50.55a Request Number VR-01</u> (Continued)

6. <u>Duration of Proposed Alternative</u>

This proposed alternative will be utilized for the entire 4th 120 month interval.

7. <u>Precedents</u>

None

<u>10 CFR 50.55a Request Number VR-01</u> (Continued)

Attachment 1 IST Basis Documents – Safety Function

Valve Group - BA-201, Containment Breathing Air Isolation Check Valve

This check valve must close to isolate containment from the breathing air system. This valve provides containment isolation for Penetration 30. Penetration 30 is considered a non essential penetration which is not required to be in service post accident [UFSAR Table 6.6-1].

This valve opens to provide a flow path from the breathing air receiver to containment during cold shutdown or refueling [5613/5614-M-3101-1]. This function is not required for safe shutdown or accident mitigation. The breathing air system is only required to function during cold shutdown or refueling [0-OP-101]. Additionally, upstream air operated valve CV-*-6165 outside containment is administratively maintained in the locked and pinned closed position during normal plant operation [0-OSP-205].

This penetration is isolated during all modes of operation when containment integrity is required and is not in service during any emergency or post accident conditions [0-OP-101]. Therefore, this valve only performs a containment isolation function and is not required to open or close for any other safety function. Since the valve is normally closed, with the upstream piping administratively locked and pinned closed by CV-*-6165, and a dead leg exists downstream, this valve is considered passive. No exercising is required.

Penetration 30



Valve Group - 340A, Instrument Air to Containment Check Valve

This check valve must close to isolate containment from the non safety instrument air system. This valve provides containment isolation for Penetration 29 [UFSAR Table 6.6-1]. The valve opens to provide a flow path of instrument air to the containment supply header when the instrument air system is operating. This function is not required safe shutdown or accident mitigation since the instrument air system is non safety related. Safety related equipment normally supplied by the instrument air system is designed to either fail to the required safe position or is provided with a safety related backup pneumatic supply. [UFSAR 9.17]



<u>10 CFR 50.55a Request Number VR-01</u> (Continued)

Attachment 1 (Continued) IST Basis Documents – Safety Function

Valve Group – 336, Instrument Air to Containment Check Valve

1

This check valve must close to isolate containment from the non safety instrument air system. This valve provides containment isolation for Penetration 29 [UFSAR Table 6.6-1].

The valve opens to provide a flow path of instrument air to the containment supply header when the instrument air system is operating. This function is not required safe shutdown or accident mitigation since the instrument air system is non safety related. Safety related equipment normally supplied by the instrument air system is designed to either fail to the required safe position or is provided with a safety related backup pneumatic supply. [UFSAR 9.17]



Valve Group - 567, Primary Water to Containment Check Valve

This check valve must close to isolate containment from the primary water system. This valve provides containment isolation for Penetration 47. Penetration 47 is considered a non essential penetration which is not required to be in service post accident [UFSAR Table 6.6-1].

This valve opens to provide a flow path from the primary water supply header to containment during cold shutdown or refueling. This function provides a supply source to facilitate maintenance and testing during outages [OP-020]. This function is not required for safe shutdown or accident mitigation. Additionally, downstream manual valve *-10-582 inside containment is administratively maintained in the locked closed position during normal power operations [OP-020/OSP-205]. The primary water system is not required for safe shutdown [UFSAR 9.6.2]. This penetration is isolated during all modes of operation when containment integrity is required and is not in service during any emergency or post accident conditions. Therefore this valve only performs a containment isolation function and not required to open or close for any other function. Since the valve is normally closed, since a dead leg exists downstream, this valve is considered passive. No exercising testing is required.



IST Program Plan Florida Power and Light Company <u>Turkey Point Nuclear Power Plant</u> <u>10 CFR 50.55a Request Number VR-01</u> (Continued)

Attachment 1 (Continued) IST Basis Documents – Safety Function

Valve Group – 298A/B/C, Reactor Coolant Pump Seal Injection Check Valve

This check valve must close to isolate containment from the chemical and volume control system during accident conditions when RCP seal injection flow is not required. The valve is considered a containment isolation valve for Penetration 24A/B/C [UFSAR Table 6.6-1].

This check valve opens to provide a flow path from the charging pump to the reactor coolant pump seals during normal plant operation [UFSAR 9.2.2]. This function is not required for safe shutdown or accident mitigation since the reactor coolant pumps are not required for safe shutdown or accident mitigation. [UFSAR 4.1.1] Additionally, the seal injection return valves (MOV-*-381 and MOV-8-6386) receive automatic closure signal to isolate the seal injection return flow path during a safety injection [UFSAR Table 6.6-1]

Penetration 24A. B and C



IST Program Plan Florida Power and Light Company <u>Turkey Point Nuclear Power Plant</u> <u>10 CFR 50.55a Request Number VR-01</u> (Continued)

Attachment 1 (Continued) IST Basis Documents – Safety Function

Valve Group - 945E, Nitrogen Supply to Accumulators Check Valve

This check valve must close to isolate containment from the non safety related nitrogen supply system during accident conditions. This valve is considered a containment isolation valve for Penetration 42 [UFSAR Table 6.6-1].

The valve opens to support safety injection accumulator refill to recharge and maintain the accumulators pressurized during normal power operations [*-OP-064]. This function is not required for safe shutdown or accident mitigation since the safety injection accumulators are considered a passive injection system and tank pressure is continuously monitored during normal plant operations [UFSAR 6.2].



Valve Group - 518/519, Nitrogen Supply to Pressurizer Relief Tank

This check valve must close to isolate containment from the non safety nitrogen supply system. This valve provides containment isolation for Penetration 6 [UFSAR Table 6.6-1].

The valve opens to provide a flow path from the nitrogen supply header to the pressurizer relief tank. This function is not required safe shutdown or accident mitigation since the nitrogen system is non safety related. The pressurizer relief tank is designed for full vacuum conditions to prevent tank collapse if the tank contents cool without nitrogen being supplied. [UFSAR 4.2]

Penetration 6



IST Program Plan Florida Power and Light Company Turkey Point Nuclear Power Plant 10 CFR 50.55a Request Number VR-02

Proposed Alternative In Accordance with 10 CFR 50.55a(a)(3)(i)

Alternative Provides Acceptable Level of Quality and Safety

1. <u>ASME Code Component(s) Affected</u>

Valve Number	Class	Category	Function
SV-3-6385	2	A	Pressurizer Relief Tank Vent Sample Isolation
SV-3-6427A	2	A	Reactor Coolant System Hot Leg Sample Isolation
SV-3-6427B	2	A	Reactor Coolant System Hot Leg Sample Isolation
SV-3-6428	2	Α	Reactor Coolant System Hot Leg Sample Isolation
SV-3-2911	2	A	Continuous Containment Air Monitor Isolation
SV-3-2912	2	A	Continuous Containment Air Monitor Isolation
SV-3-2913	2	A	Continuous Containment Air Monitor Isolation
SV-4-6385	2	A	Pressurizer Relief Tank Vent Sample Isolation
SV-4-6427A	2	Α	Reactor Coolant System Hot Leg Sample Isolation
SV-4-6427B	2	Α	Reactor Coolant System Hot Leg Sample Isolation
SV-4-6428	2	Α	Reactor Coolant System Hot Leg Sample Isolation
SV-4-2911	2	Α	Continuous Containment Air Monitor Isolation
SV-4-2912	2	A	Continuous Containment Air Monitor Isolation
SV-4-2913	2	А	Continuous Containment Air Monitor Isolation

2. <u>Applicable Code Edition and Addenda</u>

ASME OM Code 1998 Edition through 2000 Addenda

3. <u>Applicable Code Requirement</u>

ISTC-3700 Position Verification Testing, states "Valves with remote position indicators shall be observed locally at least once every 2 years to verify that valve operation is accurately indicated."

Specifically, relief is requested from performing the position indication verification on a 2 year frequency. Position indication verification will be performed at a frequency commensurate with the Option B test frequency for performing leakage rate testing.

4. <u>Reason for Request</u>

Pursuant to 10 CFR 50.55a, "Codes and Standards", paragraph (a)(3), relief is requested from the requirement of ASME OM Code ISTC-3700. The basis of the relief request is that the proposed alternative would provide an acceptable level of quality and safety.

The subject valves are all categorized as AC and are all considered containment isolation valves per the plant safety analysis. All of the subject valves have a safety function to close in order to isolate containment from their respective non-safety related systems during a Loss of Coolant Accident (LOCA) requiring containment isolation.

IST Program Plan Florida Power and Light Company <u>Turkey Point Nuclear Power Plant</u> <u>10 CFR 50.55a Request Number VR-02</u> (Continued)

Since these values are considered containment isolation values, they are each individually seat leakage testing in accordance with 10CFR50 Appendix J. The test arrangement for each value is listed in Attachment 1 - Local Leak Rate Test Diagrams. Note that only the test arrangements for Unit #3 are provided in the attachment. Unit #4 is typical.

Each of the subject values is a solenoid operated value designed such that the position of the value is not locally observable. The design of these values is such that the coil position is internal to the value body and not observable in either the energized or deenergized state. See Attachment 2 - Typical Solenoid Value Diagram, which is typical for the subject values.

In accordance with ISTC-3700, where local observation is not possible, other indications shall be used to verify valve position. The method used a Turkey Point is a pressure test using the local leakage rate testing equipment. This method involves pressurizing the containment penetration volume to approximately 40 psia, and verifying the penetration remains pressurized while the valve is indicating closed on the main control room board. The valve is then opened using the control switch in the main control room. A decrease in pressure is then verified along with valve position indicating open in the main control room. This method satisfies the requirement for position indication verification and ensures that the indicating system accurately reflects the valve position.

Since each of these valves is seat leakage tested using local leakage rate testing equipment during refueling outages, the current leakage rate tests have been modified to also perform the position indication verification test at the same time. Since the individual valve being tested must have its system properly drained, vented, and aligned correctly prior to performing the seat leakage test, an opportune window exists to perform the position indication verification. Additionally, test personnel, radiation exposure, and time/labor involved will be significantly reduced by performing the position indication verification test along with the seat leakage test.

On October 4, 1996, Turkey Point received a Safety Evaluation with approval to implement Option B of the 10CFR50 Appendix J Program. (Technical Specification Amendments 192/186 for Unit #3 and #4 respectively. This program permits the extension of the Appendix J seat leakage testing to a frequency corresponding to the specific valve performance. Valves whose leakage test results indicate good performance may have their interval of testing increased based on these test results. The Turkey Point administrative program which implements Appendix J Option B requires individual containment isolation valves to pass four successful seat leakage tests before it can be included in the Option B program.

5. <u>Proposed Alternative and Basis for Use</u>

For the subject valves, Turkey Point Nuclear Plant will perform the position indication verification in conjunction with the seat leakage test at a frequency in accordance with 10CFR50 Appendix J. This interval may be adjusted to a frequency of testing commensurate with Option B of 10CFR50 Appendix J Type C leakage testing based on valve seat leakage performance.

IST Program Plan Florida Power and Light Company Turkey Point Nuclear Power Plant 10 CFR 50.55a Request Number VR-02

(Continued)

Additionally, each of these subject valves is exercised on a quarterly frequency and their stroke times measured and compared to the ASME OM Code acceptance criteria. By continuing quarterly valve exercising and performance of the position indication verification and seat leakage test in accordance 10CFR50 Appendix J, an adequate assessment of valve health may be determined..

Therefore, the ability to detect degradation and ensure the operational readiness of the subject valves to perform their intended function is not jeopardized by performing the position indication verification test at the same frequency as specified by Option B. This frequency of testing provides reasonable assurance of the operational readiness of the subject valves and provides an acceptable level of quality and safety.

6. <u>Duration of Proposed Alternative</u>

This proposed alternative will be utilized for the entire 4th 120 month interval.

7. Precedents

None

10 CFR 50.55a Request Number VR-02 (Continued)

Attachment 1 Local Leak Rate Test Diagrams

Valve Group - SV-*-6385



Valve Group - SV-*-6427A/B and SV-*-6428



<u>10 CFR 50.55a Request Number VR-02</u> (Continued)

Attachment 1 Local Leak Rate Test Diagrams (Continued)

Valve Group - SV-*-2912



Valve Group - SV-*-2911/2912





<u>10 CFR 50.55a Request Number VR-02</u> (Continued)

Attachment 2 Typical Solenoid Valve Diagram



ITEM	DESCRIPTION	ITEM	DESCRIPTION
1	Cover Bolts	10	Seal
2	Locknut	11	Nameplate
3	Cover	12	Strap
4	O-Ring	14	Buckle
5	Bolt	15	Bolt
6	Lockwasher	16	Lockwasher
8	Switch Block Assy.	17	Spacer
9	Coil Shell Assy.		

10 CFR 50.55a Request Number VR-03

Relief Requested In Accordance with 10 CFR 50.55a(a)(3)(ii)

Hardship or Unusual Difficulty without Compensating Increase in Level of Quality or Safety

1. <u>ASME Code Component(s) Affected</u>

Valve Number	Class	Category	Function
20-143	3	С	Auxiliary Feedwater Pump Train A Discharge
			Check Valve

2. <u>Applicable Code Edition and Addenda</u>

ASME OM Code 1998 Edition through 2000 Addenda

3. <u>Applicable Code Requirement</u>

ISTC-3510 Exercising Test Frequency, states that "Active Category A, Category B, and Category C check valves shall be exercised nominally every 3 months, except as provided by ISTC-3520, ISTC-3540, ISTC-3550, ISTC 3560, ISTC-5221, and ISTC-5222.".

Specifically, relief is requested from performing the closed exercise test in accordance with ISTC-3510.

4. <u>Reason for Request</u>

Pursuant to 10 CFR 50.55a, "Codes and standards," paragraph (a)(3), relief is requested from the requirement of ASME OM Code, ISTC-3510. The basis of the relief request is that the Code requirement presents an undue hardship without a compensating increase in level of quality or safety.

The subject valve, 20-143 is categorized as C in the Inservice Testing Program with both an open and closed safety function. The following Inservice Testing Basis Document describes the valve functions in detail (See Attachment 1 - AFW System Diagram).

20-143 Basis

This check valve must open to provide a flow path from the auxiliary feedwater pump to the steam generators when the auxiliary feedwater pump is required to be operated. The auxiliary feedwater pump takes suction from the condensate storage tank. [UFSAR 9.11] This check valve must open to provide 466.8 gpm of auxiliary feedwater flow to the steam generators to maintain sufficient water level in the steam generators of both units. This flow rate is based on one AFW pump supplying a total of 233.4 gpm to three steam generators, the AFW system being shared between the units, and a loss of AC power simultaneously on both units. [UFSAR 14.1.12]

<u>10_CFR 50.55a Request Number VR-03</u> (Continued)

20-143 Basis (continued)

This check valve must close to prevent diversion of flow when the Auxiliary Feedwater Pump C is supply the Train 1 discharge header. This function is necessary in the event that the Auxiliary Pump A is out of service with Pump C is supplying Train 1 auxiliary feedwater. This alignment is considered an infrequent operation (*-OP-75) and is not the preferred alignment of the system. Additionally, downstream manual isolation valve *-142 may be closed after alignment of the C pump to the Train 1 discharge header. However, for a brief period time, prior to closure of the manual valve, this check valve must close.

During normal system alignment, this check valve closes when the auxiliary feedwater pump is not in operation to prevent reverse flow. Since Train 1 is normally isolated from Train 2 closure of this valve to prevent diversion of flow is not required. [UFSAR 9.11] Isolation of the Train 1 auxiliary feedwater during a steam generator tube rupture event is accomplished by closing the downstream flow control valve on the affected steam generator [UFSAR 14.2.4/DBD-075]. Therefore the closure of this valve is not required for safe shutdown or accident mitigation during normal system alignment.

Inservice Testing Requirements - Exercise Open and Closed on a Quarterly Frequency

Check valve 20-143 is exercised open on a quarterly frequency with flow during the performance of the quarterly inservice test of the "A" Auxiliary Feedwater Pump. *-OSP-75.6 verifies that during pump testing, design accident flow rate is achieved downstream of the check valve (> 466.8 gpm). Achieving this flow rate verifies the ability of check valve 20-143 to open to the position required to fulfill its intended function and satisfies the open exercise test requirements.

To test check valve 20-143 closed requires removing the Train 1, (Auxiliary Feedwater Pump A) from service and performing a reverse flow test to verify check valve closure. Since the Auxiliary Feedwater System at Turkey Point is a shared system, when the Train 1 pump (AFW Pump A) is removed from service, both Unit #3 and #4 Train 1 is supplied by the C AFW pump. In accordance with Turkey Point Operating Procedure, OP-75, the C AFW pump is manually aligned to the Train 1 supply piping by alignment of manual valves (See Attachment 1). Prior to declaring the pump operable in this configuration the corresponding Inservice Test is performed on the C AFW pump to ensure AFW Train Operability requirements are met in accordance with plant Technical Specification Table 3.7-3. During this test the AFW Pump A Train 1 supply manual isolation value *-142 may be left locked open to allow flow from the C AFW pump to close valve 10-142. Since this manual valve is the only isolation valve between the A AFW Pump Train 1 and AFW Pump C when it is aligned to Train 1, it is then closed to provide additional isolation should maintenance be required on the A AFW Pump. After testing is complete and the manual isolation valve (*-142) is closed, check valve 20-143 does not perform any safety function. Isolation of the out of service A AFW Pump is provided by the manual isolation valves.

<u>10 CFR 50.55a Request Number VR-03</u> (Continued)

Therefore, check valve 20-143 performs a closed safety function only during a limited time period when the AFW system Train 1 is being aligned from C AFW Pump.

Manual isolation valves, *-142 are included in the Inservice Testing Program and tested in accordance with ISTC.

5. **Proposed Alternative and Basis for Use**

Turkey Point Nuclear Plant will continue to perform the full open exercise test on check valve 20-143 during the quarterly during performance of the A AFW pump inservice test. The closure test of 20-143 will be performed only when the A AFW pump is taken out of service for maintenance. Since the C AFW pump will be operated to verify operability of Train 1 in accordance with Technical Specification Table 3.7-3 during this period, check valve 20-143 may be tested close.

To test this check valve closed requires removing the A AFW Pump from service and operating the C AFW Pump to verify closure. Although this test is not difficult, it does place undue hardship on the plant by placing the Auxiliary Feedwater System in an undesirable configuration without the designed redundancy. Since no function exists for check valve 20-143 during normal system alignment, the frequency of testing provides reasonable assurance of the operational readiness of the subject valve and provides an acceptable level of quality and safety. Strict adherence to the Code test frequency for testing the valve closed does not provide any increase in the level of quality or safety.

6. <u>Duration of Proposed Alternative</u>

This proposed alternative will be utilized for the entire 4th 120 month interval.

7. <u>Precedents</u>

None

<u>10 CFR 50.55a Request Number VR-03</u> (Continued)

Attachment 1

AFW System Diagram



Note: Manual valves AFPD-001/002/003 and *-20-142/242/342 are normally locked in the positions shown.

ATTACHMENT 6

COLD SHUTDOWN JUSTIFICATION INDEX

(Page 1 of 1)

Cold Shutdown Justification No.	Description
CSJ-01	AFW Turbine Steam Supply Valve (381/382/383) Closure Testing
CSJ-02	Containment Purge Supply/Exhaust Valve Exercising
CSJ-03	Safety Injection Hot Leg Injection Valve (MOV-*-866A/B) Exercising
CSJ-04	Safety Injection Pump Discharge Header Cross Tie Valve (MOV-878A/B) Exercising
CSJ-05	SI/CS Recirc to RWST Valve (MOV-*-856A/B) Exercising
CSJ-06	RWST Outlet Isolation Valve (MOV-*-864A/B) Exercising
CSJ-07	SI Cold Leg Injection Check Valve (*-875A/B/C) Exercise Close Test
CSJ-08	RHR Cold Leg Injection Check Valve (*-876A/B/C) Exercise Close Test
CSJ-09	Component Cooling to Excess Letdown Hx Check Valve (*-738) Exercise Close Test
CSJ-10	CCW to Containment Cooler Valve (MOV-*-1417/1418) Exercising
CSJ-11	CCW to RCP Valve (MOV-*-626/716A/B/730) Exercising
CSJ-12	Main Steam Non-Return Check Valve (*-10-4/5/6) Close Exercise Test
CSJ-13	Main Steam Atmospheric Dump Valve (CV-*-1606/7/8) Exercising
CSJ-14	RHR to Cold Leg Injection Valve (MOV-*-744A/B) Exercising
CSJ-15	SI Accumulator Isolation Valve (MOV-*-865A/B/C) Exercising
CSJ-16	CVCS Letdown Line Isolation Valve (CV-*-204) Exercising
CSJ-17	Feedwater Control Valve (FCV-*-478/488/498) Exercising
CSJ-18	Feedwater Control Valve Bypass Valve (FCV-*-479/489/499) Exercising
CSJ-19	CVCS Charging to Regen Hx Valve (HCV-*-121) Exercising
CSJ-20	RWST to Charging Suction Valve (LCV-*-115B) Exercising
CSJ-21	CVCS VCT to Charging Valve (LCV-*-115C) Exercising
CSJ-22	Emergency Boration to Charging Check Valve (*-357) Open Exercise Test
CSJ-23	Power Operated Relief Valve (PCV-*-455C/456) Exercising
CSJ-24	Reactor Vessel Head Vent Valve (SV-*-6318A/B/6611/6612) Exercising
CSJ-25	Reactor Coolant Pump Return Valve (MOV-*-381/6386) Exercising
CSJ-26	RHR Suction from RWST Isolation Valve (MOV-*-862A/B) Exercising
CSJ-27	Reactor Coolant System RHR Suction Valve (MOV-*-750/751) Exercising
CSJ-28	RHR Alternate Discharge Isolation Valve (MOV-*-863A/B) Exercising
CSJ-29	RHR Pump Discharge Check Valve (*-753A/B) Open/Close Exercise Test
CSJ-30	Main Steam Isolation Valve (POV-*-2604/2605/2606)Close Exercise Test
CSJ-31	RHR Alternate Low Head Safety Injection Valve (MOV-*-872) Exercising
IST Program Plan Florida Power and Light Company Turkey Point Nuclear Power Plant

ATTACHMENT 7

COLD SHUTDOWN JUSTIFICATIONS

	IST Pro Florida Power o Turkey Point N	ogram Plan and Light Company uclear Power Plant	
	Cold Shutdown	Iustification CSJ-01	
Component Tag	<u>System</u>	Safety Class	Category
3-10-381	075	3	С
3-10-382	075	3	С
3-10-383	075	3	С
4-10-381	075	3	С
4-10-382	075	3	С
4-10-383	075	3	С

These check valves open to provide a flow path from the steam generators to the auxiliary feedwater pump turbine when the auxiliary feedwater pump is required to be operating. They close to prevent backflow in the event of a steam line rupture upstream of the valve and to prevent reverse flow between the units.

Justification

It is impracticable to exercise these check valves closed during normal power operation since closure testing at normal power imposes a significant safety hazard to plant personnel.

To verify closure of these valves requires isolation of the associated steam supply line from the steam generator and depressurization of the line on the upstream side of the valve. During normal operations, steam in excess of 800 psig is required to be vented to allow the valve to close. This testing imposes a significant safety hazard on plant personnel. Additionally, to perform this testing during normal plant operations, the auxiliary feedwater system would be required to be placed in an undesirable lineup.

Alternative Test

These check valves will be exercised closed during cold shutdowns when auxiliary steam at much lower pressure (approximately 250 psig) may be used to close the valve.

	IST Pro Florida Power a Turkey Point Ni	gram Plan and Light Company uclear Power Plant	
	Cold Shutdown J	Justification CSJ-02	
Component Tag	<u>System</u>	Safety Class	Category
POV-3-2600	053	2	A
POV-3-2601	053	2	А
POV-3-2602	053	2	Α
POV-3-2603	053	2	Α
POV-4-2600	053	2	А
POV-4-2601	053	2	Α
POV-4-2602	053	2	Α
POV-4-2603	053	2	Α

These normally closed, air operated valves must close/remain closed to isolate containment from the Containment Purge Supply line. The valve closes automatically upon receipt of a Containment Ventilation System (CVS) Isolation signal. Additionally, this valve fails closed on loss of electrical power or pneumatic supply. This valve is opened to purge containment to support personnel entry – during unit shutdowns.

Justification

It is impracticable to exercise these butterfly valves closed during normal power operation since closure testing at normal power imposes possible operational considerations regarding valve operability.

To verify closure of these valves requires opening of the valve to perform exercise and fail safe testing. Opening of the valve during normal plant operations may cause significant operability concerns based on the valve design. Due to the history of these valves with respect to operational-related seat leakage, the plant staff has imposed restrictions on valve operation whereby unnecessary cycling of the valves is to be avoided and additional leaktests are performed based on cycling frequency. The plant staff has administratively controlled the operating cycles (fuses not normally installed) such that cycling of these valves at power is allowed only when absolutely necessary.

Alternative Test

These valves will be exercised closed and fail safe tested during cold shutdowns when containment integrity is not required.

	IST Pro Florida Power (Turkey Point N	ogram Plan and Light Company uclear Power Plant	
	Cold Shutdown	Justification CSJ-03	
Component Tag	System	Safety Class	Category
MOV-3-866A	062	1	A
MOV-3-866B	062	1	Α
MOV-4-866A	062	1	Α
MOV-4-866B	062	1	А

These motor operated valve must close or remain closed to isolate the hot leg injection line from the safety injection system during emergency conditions when hot leg injection is not required. This function ensures adequate core filling and cooling through the cold legs during a loss of coolant accident. The valve is maintained administratively locked closed with the breaker open to ensure valve closure since initial accident conditions require core cooling through the cold legs. This valve also receives a safety injection signal (SIS) to close to isolate containment from the safety injection system. The valve is required to open to provide a flow path from the safety injection pump to the reactor coolant system hot leg, during hot leg recirculation operation This function requires operator action to open the valve since it is normally closed with the breaker in the locked open position

Justification

It is impracticable to exercise these valves open or closed during normal power operation since opening of this valve during normal power operations places the plant in an undesirable configuration.

Exercising this valve open or closed requires aligning the system in a configuration where the Class 1 reactor coolant system is isolated from the lower pressure Class 2 safety injection system by only one valve (simple check). This configuration would place the plant in an undesirable alignment and cause undue risk.

Alternative Test

These valves will be exercised open and closed during cold shutdowns when reactor coolant system pressure is below 600 psig.

	IST Pro Florida Power o Turkey Point N	gram Plan and Light Company aclear Power Plant	
	Cold Shutdown	Justification CSJ-04	
Component Tag	<u>System</u>	Safety Class	Category
MOV-878A	062	2	В
MOV-878B	062	2	В

These motor operated valves must remain open to provide a flow path from the safety injection pump to the opposite unit during the injection phase of safety injection following a loss of coolant accident. The valves are maintained in the open position during normal power operations due to single failure analysis requiring at least two safety injection pumps for injection into the reactor coolant system. These valves may be closed prior to switch over to the recirculation phase of safety injection to isolate the non accident unit piping from the contaminated recirculated water on the accident unit.

Justification

It is impracticable to exercise these valves closed during normal power operation since closure of this valve during normal power operations places the plant in an undesirable and unanalyzed configuration.

Exercising these valves closed places the plant in a condition where the shared safety injection pumps are not available as required. Closure of the valves solely for testing would place the plant in an undesirable alignment and cause undue risk.

Alternative Test

These valves will be exercised closed during cold shutdowns when the safety injection system is not required to be operable for the opposite unit.

	IST Pro Florida Power (Turkey Point N	ogram Plan and Light Company uclear Power Plant			
Cold Shutdown Justification CSJ-05					
Component Tag	<u>System</u>	Safety Class	<u>Category</u>		
MOV-3-856A	062	2	В		
MOV-3-856B	062	2	В		
MOV-4-856A	062	2	· B		
MOV-4-856B	062	2	В		

These motor operated valves must remain open to provide a flow path from the safety injection and containment spray pumps to the RWST during the injection phase of an accident to prevent potential pump damage. Theses valves are maintained in the open position during normal power operations and do not receive any automatic actuation signals. Theses valves may be closed prior to switch over to the recirculation phase of safety injection to isolate the RWST from the containment spray and safety injection pumps. This function prevents contamination of the RWST.

Justification

It is impracticable to exercise these valves closed during normal power operation since closure of this valve during normal power operations places the plant in an undesirable and unanalyzed configuration.

Exercising these values closed places the plant in a condition where the associated safety injection pump may be damaged, if started, since the recirculation line would be isolated. Closure of the values solely for testing would place the plant in an undesirable alignment and cause undue risk.

Alternative Test

These valves will be exercised closed during cold shutdowns when the safety injection pumps and containment spray pumps are not required to be operable.

	IST Pro Florida Power Turkey Point N	ogram Plan and Light Company uclear Power Plant				
	Cold Shutdown Justification CSJ-06					
<u>Component Tag</u>	<u>Svstem</u>	Safety Class	<u>Category</u>			
MOV-3-864A	062	2	B			
MOV-3-864B	062	2	B			
MOV-4-864A	062	2	B			
MOV-4-864B	062	2	B			

These normally open motor operated valves must remain open to provide a flow path from the RWST to the suction of the safety injection, containment spray, and residual heat removal pumps during the injection phase of an accident. These valves are maintained administratively locked open with their breakers open to ensure the valve remains open during the injection phase. The valves must close prior to switch over to the recirculation phase of safety injection to isolate the RWST from the containment spray, safety injection and residual heat removal pumps. This function prevents contamination of the RWST.

Justification

It is impracticable to exercise these valves closed during normal power operation since closure of this valve during normal power operations places the plant in an undesirable and unanalyzed configuration.

Exercising these valves closed places the plant in a condition where the associated safety injection, residual heat removal, and containment spray pumps would all be inoperable due to an isolated suction path. Closure of the valves solely for testing would place the plant in an undesirable alignment and cause undue risk.

Alternative Test

These valves will be exercised closed during cold shutdowns when the safety injection pumps, containment spray pumps, and residual heat removal pumps are not required to be operable.

IST Program Plan Florida Power and Light Company <u>Turkey Point Nuclear Power Plant</u>

Cold Shutdown Justification CSJ-07

Component Tag	<u>System</u>	Safety Class	Category
3-875A	064	1	AC
3-875B	064	1	AC
3-875C	064	1	AC
4-875A	064	1	AC
4-875B	064	1	AC
4-875C	064	1	AC

Function

These check valves open to provide flow path from the safety injection pump to the reactor coolant system cold leg injection points during the injection phase of an accident, and to provide a flow path from the safety injection tank accumulator to the cold leg injection points when the reactor coolant system decreases below 660 psig, and must open to provide a flow path from the residual heat removal pump to the cold leg injection point during a large break LOCA when the RCS is rapidly depressurized, and during the alternate low head injection during the recirculation phase of an accident These check valves must close or remain closed to isolate the reactor coolant system from the lower pressure safety injection and residual heat removal systems during normal operations and emergency conditions when cold leg injection is not required. These valves are considered a pressure isolation valve, required to maintain the RCS pressure boundary. The valves must close to limit leakage to <1.0 gpm.

Justification

It is impracticable to exercise these valves closed during normal power operation since closure of this valve during normal power operations places the plant in an undesirable configuration along with an increase in personnel radiation exposure to perform testing.

Exercising this valve closed requires isolation and depressurization of the safety injection system accumulators to perform a leakage test to verify closure. Isolation of the accumulator during normal power operation places the plant in an undesirable condition. Personnel entry into containment would be required to perform the leakage test. This would result in an increase in personnel radiation exposure.

Alternative Test

These valves will be exercised closed during cold shutdowns when the safety injection system accumulators are not required and radiation levels permit entry into containment.

	IST Pro Florida Power o Turkey Point N	ogram Plan and Light Company uclear Power Plant	
	Cold Shutdown.	Justification CSJ-08	
Component Tag	<u>System</u>	Safety Class	Category
3-876A	064	1	AC
3-876B	064	1	AC
3-876C	064	1	AC
4-876A	064	1	AC
4-876B	064	1	AC
4-876C	064	1	AC

These check valves open to provide flow path from the residual heat removal system to the cold leg injection points during a large break LOCA when the RCS is rapidly depressurized. These valves must also open to provide normal low head injection during the injection phase of an accident. These check valves must close or remain closed to prevent reverse flow when the safety injection pump or accumulators are required to inject flow to the cold leg. The valves are also required to close when RHR is in service for alternate low head injection during the recirculation phase of an accident. The valves are required to close to isolate the reactor coolant system from the lower pressure residual heat removal system during emergency conditions when the residual heat removal system is not required. These valves are considered a pressure isolation valve, required to maintain the RCS pressure boundary. The valves must close to limit leakage to <1.0 gpm.

Justification

It is impracticable to exercise these valves closed during normal power operations since closure of these valves during normal power operations places the plant in an undesirable and unanalyzed configuration along with an increase in personnel radiation exposure to perform testing.

Exercising these valves closed during normal power operations requires isolation of the refueling water storage tank and depressurizing and draining of the residual heat removal system to perform leakage testing to verify closure. Isolation of the refueling water storage tank during normal operation would require defeating the normal safety injection interlocks and require declaring the low head residual heat removal system inoperable. Considering the amount of piping required to be drained, and the various LCO entered, this testing would place the plant in an unanalyzed and undesirable condition. This testing requires containment entry and significant test preparation, which may cause a delay in plant startup. Additionally, entry into containment for test preparation, performance and restoration imposes a significant increase in radiation exposure to plant personnel.

Alternative Test

These valves will be exercised closed during cold shutdowns when the residual heat removal system is not required and the RWST may be isolated.

	IST Pro Florida Power o Turkey Point No	gram Plan and Light Company aclear Power Plant	
	Cold Shutdown	Iustification CSJ-09	
Component Tag	<u>System</u>	Safety Class	Category
3-738	030	2	С
4-738	030	2	С

This check valve must close to isolate containment from the component cooling water system. This valve is exempt from Appendix J testing since it is connected to a closed system inside containment. The valve provides containment isolation for Penetration 12. In the open position this valve opens to provide component cooling water to the excess letdown heat exchanger during normal plant operating modes. This open function is not required for safe shutdown or accident mitigation.

Justification

It is impracticable to exercise this valve closed during normal power operations since significant plant piping would be required to be drained to perform a backflow test to verify closure. Additionally, performance of this test places the plant in an undesirable condition during plant operations.

To exercise this check valve closed requires performance of a backflow/leakage test. This test requires draining of the piping upstream and downstream of the check valve. Since the component cooling water is chemical treated with a corrosion inhibitor, a significant amount of time and labor is necessary to manage the disposal of this chemically treated water. Considering the amount of piping required to be drained, and the various LCO entered, this testing would place the plant in an undesirable condition during plant power operations.

Alternative Test

These valves will be exercised closed during cold shutdowns when component cooling water and excess letdown are not required.

	IST Pro Florida Power o Turkey Point N	ogram Plan and Light Company uclear Power Plant			
Cold Shutdown Justification CSJ-10					
Component Tag	<u>System</u>	Safety Class	<u>Category</u>		
MOV-3-1417	030	2	В		
MOV-3-1418	030	2	В		
MOV-4-1417	030	2	В		
MOV-4-1418	030	2	В		

These valves must close to provide containment isolation for the component cooling water supply/return line to the normal containment coolers and CRDM coolers. These valves close automatically on a Phase A containment isolation signal. The valve provides containment isolation for Penetrations 21 and 22. The valves are normally open to provide component cooling water to the normal containment coolers and CRDM coolers during normal plant operating modes and during plant fires. This open function is not required for safe shutdown or accident mitigation.

Justification

It is impracticable to exercise these valves closed during normal power operations since damage to plant equipment may occur.

Exercising these valves closed during normal power operations would isolate the normal cooling water supply to the normal containment coolers, control rod drive mechanism coolers, and the primary shield cooling coils. Isolation of the cooling water supply to this equipment may cause severe damage due to overheating of the equipment. Failure of this equipment due to overheating during normal power operations would result in potential equipment damage and subsequent plant shutdown.

Alternative Test

These valves will be exercised closed during cold shutdowns when the associated equipment being cooled is not required to be in operation.

IST Program Plan Florida Power and Light Company Turkey Point Nuclear Power Plant Cold Shutdown Justification CSJ-11				
Component Tag	System	Safety Class	Category	
MOV-3-626	030	2	B	
MOV-3-716A	030	3	В	
MOV-3-716B	030	2	В	
MOV-3-730	030	2	В	
MOV-4-626	030	2	В	
MOV-4-716A	030	3	B	
MOV-4-716B	030	2	B	
MOV-4-730	030	2	B	

These values close to provide containment isolation for the component cooling water supply/return line from the RCP bearing coolers. The values close automatically on a Phase B containment isolation signal. These values are normally open to provide cooling water to the reactor coolant pump seals and the main drive motors. The open function is not required for safe shutdown or accident mitigation.

Justification

It is impracticable to exercise these valves closed during normal power operations since damage to plant equipment may occur.

Exercising these valves closed during normal power operations would isolate the normal cooling water supply to reactor coolant pump seals and the main drive motors. Isolation of the cooling water supply to this equipment may result in degradation of the reactor coolant pump seals and motors, eventually resulting in potential damage to the reactor coolant pump and subsequent plant shutdown.

Alternative Test

These valves will be exercised closed during cold shutdowns when the associated reactor coolant pumps are not required to be in operation.

IST Program Plan Florida Power and Light Company Turkey Point Nuclear Power Plant

Cold Shutdown Justification CSJ-12

Component Tag	System	Safety Class	Category
3-10-004	072	SR	<u> </u>
3-10-005	072	SR	С
3-10-006	072	SR	С
4-10-004	072	SR	С
4-10-005	072	SR	С
4-10-006	072	SR	С

Function

These check valves must close to prevent reverse flow due to a rupture upstream of the check valve. This prevents a single line rupture from affecting other Steam Generators by preventing uncontrolled blow down of the intact Steam Generators. This valve is open during normal operations by system flow to provide steam to the turbine. This function is not required for safe shutdown or accident mitigation.

Justification

It is impracticable to exercise these valves closed during normal power operations since closure may result in a plant trip.

Exercising these valves closed during normal power operations to perform testing would require the steam generator to be isolated. Isolation of the steam generators during normal operation would cause a severe transient in the reactor coolant system and a subsequent trip of the reactor.

Alternative Test

These check valves will be exercised closed during cold shutdowns when the steam generator may be isolated.

IST Program Plan Florida Power and Light Company <u>Turkey Point Nuclear Power Plant</u>

Cold Shutdown Justification CSJ-13

Component Tag	<u>System</u>	Safety Class	Category
CV-3-1606	072	2	В
CV-3-1607	072	2	В
CV-3-1608	072	2	В
CV-4-1606	072	2	В
CV-4-1607	072	2	В
CV-4-1608	072	2	В

Function

This valve is an air operated relief valve with a controllable setpoint. This valve is opened (nonfaulted S/G) after a SGTR with a concurrent loss of offsite power to control reactor coolant system cooldown. The RCS cooldown allows RCS depressurization which will limit radioactive release to the faulted S/G. Theses valves are considered containment isolation valves for Penetrations 26A/B/C. They are considered secondary system barrier since the Steam Generators are a closed loop inside containment. During accidents requiring the use of the AFW Turbine, these valves must remain closed to prevent diverting steam from the AFW Turbine. The valves must close or remain closed to isolate the Steam Generator from atmosphere during a SGTR (faulted S/G) because this mitigates the release of radioactivity to atmosphere. These valves also fail to the closed position on loss of power. The valves are opened during normal operations, and their setpoints are modulated, to control RCS cooldown to RHR entry conditions.

Justification

It is impracticable to exercise these valves open or closed during normal power operations since exercising these valves may result in a plant transient and subsequent reactor trip.

Exercising these valves during normal power operations to perform testing would cause a power transient during normal plant operations due to the amount of steam released when the valve is opened. Exercising the valve may be performed with the block valve closed to limit the amount of steam released, however, this alignment places the plant in an undesirable condition. Normal operations with the block valve closed would limit the capability of the plant to limit a pressure transient and prevent lifting of a safety valve in the event of a pressure transient.

Alternative Test

These valves will be exercised open and closed during cold shutdowns when overpressure protection the reactor coolant system is not required.

	IST Pro Florida Power o Turkey Point N	ogram Plan and Light Company uclear Power Plant	
	Cold Shutdown	Justification CSJ-14	
Component Tag	<u>System</u>	Safety Class	Category
MOV-3-744A	064	2	В
MOV-3-744B	064	2	В
MOV-4-744A	064	2	В
MOV-4-744B	064	2	В

These valves must open automatically upon receipt of a safety injection signal to provide a flow path from the RHR pump to the reactor coolant system cold legs during the injection phase of an accident. These valves are also required to be opened/closed by remote manual operations during the recirculation phase of an accident to support hot/cold leg recirculation depending on reactor coolant system pressure. The valves are also opened during normal shutdown cooling operations to facilitate normal decay heat removal. These valves are required to close by remote manual operation to isolate the RHR system when the system is aligned for hot leg injection and alternate low head injection. However, this function is redundant to downstream check valves which are required to close to isolate the reactor coolant system pressure boundary.

Justification

It is impracticable to exercise these valves open or closed during normal power operation since opening of this valve during normal power operations places the plant in an undesirable configuration.

Exercising these valves open or closed requires aligning the system in a configuration where the Class 1 reactor coolant system is isolated from the lower pressure Class 2 residual heat removal system by two check valves. This configuration would place the plant in an undesirable alignment and cause undue risk.

Alternative Test

These valves will be exercised open and closed during cold shutdowns when reactor coolant system pressure is below residual heat removal system design pressure (600 psig).

	IST Pro Florida Power o Turkey Point N	ogram Plan and Light Company uclear Power Plant		
Cold Shutdown Justification CSJ-15				
Component Tag	<u>System</u>	Safety Class	Category	
MOV-3-865A	064	2	В	
MOV-3-865B	064	2	В	
MOV-3-865C	064	2	В	
MOV-4-865A	064	2	· B	
MOV-4-865B	064	2	В	
MOV-4-865C	064	2	В	

These valves must remain open to provide a flow path from the safety injection accumulator to the reactor coolant system during injection when the reactor coolant system pressure falls below the accumulator pressure. During normal operation, this valve is maintained in the open position with it's power removed to prevent inadvertent operation. Since these valves are not required to change positions to perform this function, the open position is considered passive. These valves must close by remote manual operation to isolate the safety injection accumulator from the reactor coolant system after injection is complete to assist in maintaining the safe shutdown condition.

Justification

It is impracticable to exercise these valves open or closed during normal power operation since closing this valve during normal power operations places the plant in an undesirable configuration.

Exercising these valves closed during normal plant operations requires the safety injection accumulator to be isolated. Isolating the a safety injection accumulator during normal power operations places the plant in an undesirable plant configuration and an unanalyzed condition.

Alternative Test

These valves will be exercised closed during cold shutdowns when the safety injection accumulators are not required.

	IST Pro Florida Power d Turkey Point Ni	gram Plan Ind Light Company Iclear Power Plant	
Cold Shutdown Justification CSJ-16			
Component Tag	<u>System</u>	Safety Class	<u>Category</u>
CV-3-204	047	2	Α
CV-4-204	047	2	Α

This air operated valve must close automatically to isolate containment from the chemical volume control system letdown line. This valve provides containment isolation for Penetration 14. The valve closes automatically upon receipt of a Phase A containment isolation signal and fails closed on loss of electrical power or pneumatic supply. The valve is open during normal power operations to provide a letdown flow path from the reactor coolant system and regenerative heat exchanger to the non regenerative heat exchanger via the letdown orifices.

Justification

It is impracticable to exercise this valve closed during normal power operation since closing this valve during normal power operations may result in a plant trip.

Exercising this valve closed during normal plant operations would causes pressurizer level fluctuations and potential chemical volume and control system transients which would result in a potential trip of the plant.

Alternative Test

These valves will be exercised closed and fail safe tested during cold shutdowns when reactor coolant system normal letdown is not required.

IST Program Plan Florida Power and Light Company Turkey Point Nuclear Power Plant

Cold Shutdown Justification CSJ-17

Component_Tag	System	Safety Class	Category
FCV-3-478	074	2	B
FCV-3-488	074	2	В
FCV-3-498	074	2	В
FCV-4-478	074	2	В
FCV-4-488	074	2	В
FCV-4-498	074	2	В

Function

These normally open valves must close automatically on a Feedwater Isolation Signal (FWIS) during accident conditions requiring feedwater isolation. The valves are required to close within 9.0 seconds upon receipt of a Safety Injection signal and they fail closed on loss of pneumatic supply or electrical power. The valves are used to throttle flow in response to a signal from the Steam Generator Water Level Control System. These valves are opened to allow flow into the associated steam generator during normal power operations.

Justification

It is impracticable to exercise these valves closed during normal power operation since closing this valve during normal power operations would result in a plant trip.

Exercising these valves closed during normal plant operations would causes a severe steam generator level transient and subsequent reactor trip.

Alternative Test

These valves will be exercised closed and fail safe tested during cold shutdowns when feedwater flow control is not required.

	IST Pro Florida Power o Turkey Point N	ogram Plan and Light Company uclear Power Plant		
Cold Shutdown Justification CSJ-18				
Component Tag	<u>System</u>	Safety Class	Category	
FCV-3-479	074	2	В	
FCV-3-489	074	2	В	
FCV-3-499	074	2	В	
FCV-4-479	074	2	В	
FCV-4-489	074	2	В	
FCV-4-499	074	2	В	

These valves must close automatically on a Feedwater Isolation Signal (FWIS) during accident conditions requiring feedwater isolation. These valves are required to close within 13.0 seconds upon receipt of a safety injection signal and fails closed on loss of electrical power or pneumatic supply. The valves are opened to bypass the main feedwater regulating valve to allow flow into the associated S/G during low power operations.

Justification

It is impracticable to exercise these valves closed during normal power operation since exercising this valve during normal power operations would result in a plant trip.

To exercise these values closed requires opening the value to perform the close and fail safe tests. Opening of these values during normal plant operations may cause a severe steam generator level transient and subsequent reactor trip. Additionally, this testing requires the installation of electrical jumpers to defeat various safeguards logic which could also lead to an inadvertent plant transient or trip.

Alternative Test

These valves will be exercised closed and fail safe tested during cold shutdowns when feedwater flow control is not required.

	IST Pro Florida Power a Turkey Point Na	gram Plan and Light Company uclear Power_Plant	
	Cold Shutdown Justification CSJ-19		
Component Tag	System	Safety Class	<u>Category</u>
HCV-3-121 HCV-4-121	047	2	B

This air operated valve opens to provide a flow path from the charging pump to the reactor coolant system via the regenerative heat exchanger during emergency boration. The valve is required to open to provide a flow path to the RCS during a rod cluster control assembly accident requiring emergency boration. During normal power operation, this valve is open to provide the normal return flow path from the charging pump to the reactor coolant system via the regenerative heat exchanger to support processing of the water let down from the reactor coolant system. The valve does not receive any automatic actuation signals and fails open on loss of electrical power or pneumatic supply. The valve is closed when the charging system is removed from service (charging pumps not operating).

Justification

It is impracticable to exercise this valve open during normal power operation since exercising this valve during normal power operations would result in a potential plant trip.

To exercise this valve open requires closing the valve to perform the open stroke time and fail safe open tests. Closing of this valve during normal plant operations would disrupt the normal charging return flow and result in reactor coolant pump seal flow loss and pressurizer level oscillations which may result in a reactor trip.

Alternative Test

These valves will be exercised open and fail safe tested during cold shutdowns when charging is not required and the charging pumps are not in operation.

	Cold Shutdown Justification CSJ-20		
Component Tag	<u>System</u>	Safety Class	Category
LCV-3-115B	047	2	B
LCV-4-115B	047	2	В

This normally closed air operated valve must open during emergency boration to provide a backup borated water suction source from the RWST to the charging pumps. This valve is opened by remote manual operation in the event that the boric pumps fail to start. This valve opens automatically upon receipt of a low level in the volume control tank to provide a flow path from the RWST to the charging pump suction for automatic makeup of borated water to the reactor coolant system. Upon initiation of a low volume control tank level the normal suction for the charging pumps is isolated by LCV-*-115C, which closes. To ensure a suction path is available to the charging pumps, the valve is interlocked such that LCV-*-115C will not begin to close until LCV-*-115B is full open. The valve may also be opened by remote manual operation. This valve must remain closed to isolate the charging pump suction piping from the RWST during normal power operations and during emergency boration when the boric acid pumps are providing emergency boration. This function is considered passive since the valve is not required to change position to perform this function. The valve fails closed on loss of electrical power or pneumatic supply.

Justification

It is impracticable to exercise this valve open during normal power operation since exercising this valve during normal power operations would cause a power transient and potential plant trip.

To exercise this valve open requires injection of refueling water storage tank borated water into the reactor coolant system. During normal power operations, this test would cause a severe power transient which may lead to a plant trip.

Alternative Test

These valves will be exercised open and fail safe tested during cold shutdowns when the chemical volume and control system is not required to be in operation.

	IST Pro Florida Power o Turkey Point Ni	gram Plan and Light Company aclear Power Plant_	
	Cold Shutdown Justification CSJ-21		
Component Tag	<u>System</u>	Safety Class	Category
LCV-3-115C	047	2	В
LCV-4-115C	047	2	В

This valve closes automatically upon receipt of a low level in the volume control tank to isolate the volume control tank. Valve LCV-*-115B opens to provide a flow path from the RWST to the charging pump suction for automatic makeup of borated water to the reactor coolant system. To ensure a suction path is available to the charging pumps, the valve is interlocked such that LCV-*-115C will not begin to close until LCV-*-115B is full open. The valve is required to be closed by remote manual operation during emergency boration in the event of a failure of the boric acid pumps, when the RWST is aligned to the charging pump suction. The valve opens/remains open during normal operations to provide a flow path from the VCT to the charging pump suction.

Justification

It is impracticable to exercise this valve closed during normal power operation since exercising this valve during normal power operations would cause a power transient and potential plant trip.

To exercise this valve closed requires aligning the charging pumps take suction from the refueling water storage tank during normal operation. This would cause injection of refueling water storage tank borated water into the reactor coolant system. During normal power operations, this test would cause a severe power transient which may lead to a plant trip.

Alternative Test

This valve will be exercised closed during cold shutdowns when the chemical volume and control system is not required to be in operation.

	IST Pro Florida Power (Turkey Point Ni	gram Plan and Light Company yclear Power Plant	
	Cold Shutdown J	Iustification CSJ-22	
<u>Component Tag</u> 3-357 4-357	<u>Svstem</u> 047 047	<u>Safety Class</u> 2 2	<u>Category</u> C C

This check valve opens to provide a flow path from the RWST to the charging pump suction when a low level in the volume control tank automatically opens LCV-*-115B for automatic makeup of borated water to the reactor coolant system. Upon initiation of a low volume control tank level the normal suction for the charging pumps is isolated by LCV-*-115C, which closes. This valve closes to isolate the charging pump suction piping from the RWST during normal power operations and during emergency boration when the boric acid pumps are providing emergency boration. However, normally closed downstream valves LCV-*115B and *-358 are relied upon for isolating the emergency boration flow path when it is not required.

Justification

It is impracticable to exercise this valve open during normal power operation since exercising this valve during normal power operations would cause a power transient and potential plant trip.

To exercise this valve open requires aligning the charging pumps take suction from the refueling water storage tank during normal operation. This would cause injection of refueling water storage tank borated water into the reactor coolant system. During normal power operations, this test would cause a severe power transient which may lead to a plant trip.

Alternative Test

This valve will be exercised open during cold shutdowns when the chemical volume and control system is not required to be in operation.

	IST Pro Florida Power o Turkey Point N	ogram Plan and Light Company uclear Power Plant		
Cold Shutdown Justification CSJ-23				
Component Tag	<u>System</u>	Safety Class	Category	
PCV-3-455C	041	1	В	
PCV-3-456	041	1	В	
PCV-4-455C	041	1	В	
PCV-4-456	041	I	В	

This normally closed air operated valve must close to maintain the RCS pressure boundary in order to contain the coolant under operating temperature and pressure conditions. This valve must open during reactor heat up and cooldown when the Overpressure Mitigation System is in operation. During OMS operation, the reactor temperature and pressure are below normal operating bands. The lower temperature of the RCS requires lower relief setpoints to avoid brittle fracture. During these conditions the PORV setpoints are varied by the OMS according to system conditions. The subject valve must open to allow a relief path since the Safety Valve setpoints are too high to provide protection during these conditions. This valve will also automatically open at 2335 psig during normal operations (normal operating temperature and pressure) to mitigate pressure transients during a SGTR or an Appendix R fire. This function is considered important to safety but does not support safe shutdown or accident mitigation since the Pressurizer Safety Valves (RV-*-551A/B/C) are relied upon for overpressure protection of the reactor coolant system.

Justification

It is impracticable to exercise this valve open and closed during normal power operation since exercising this valve during normal power operations may cause equipment damage or a plant trip.

Exercising this valve during normal power operations would cause a rapid depressurization of the reactor coolant system causing a pressure transient and subsequent trip of the plant. Additionally, exercising this valve each quarter at power would eventually damage the valve seat.

Alternative Test

This valve will be exercised open and closed and fail safe tested during cold shutdowns when the reactor coolant system pressure is depressurized.

IST Program Plan Florida Power and Light Company Turkey Point Nuclear Power Plant					
Cold Shutdown Justification CSJ-24					
<u>Component Tag</u>	<u>System</u>	Safety Class	<u>Category</u>		
SV-3-6318A	041	2	В		
SV-3-6318B	041	2	В		
SV-3-6611	041	2	В		
SV-3-6612	041	2	В		
SV-4-6318A	041	2	В		
SV-4-6318B	041	2	В		
SV-4-6611	041	2	В		
SV-4-6612	041	2	В		

Valves SV-*-6318A/B must open during post-accident conditions to vent the vessel head so that the non-condensible gas bubble does not disrupt cooling to the core by inhibiting natural circulation. The reactor vessel head vent system provides a means of venting the vessel head to either the containment sump or the pressurizer relief tank. These valves must remain closed during normal operations to establish the RCS pressure boundary. These valves are administratively maintained closed when RCS temperature exceeds 200F by locking their control switches and removing the fuses to the valves' power supply. These valves isolate the reactor vessel head from downstream piping which leads to the containment sump, containment atmosphere, pressurizer relief tank or a sample connection. Since these valves are not required to change position to perform the closed safety function they are considered passive in the closed direction.

Valves SV-*-6611/6612 must open during post-accident conditions to vent the vessel head so that the non-condensible gas bubble does not disrupt cooling to the core by inhibiting natural circulation. The reactor vessel head vent system provides a means of venting the vessel head to either the containment sump or the pressurizer relief tank. These valves isolate the reactor vessel head vent from piping which leads to either the containment sump or containment atmosphere. This closed function is considered passive since the valves are administratively maintained closed when RCS temperature exceeds 200F by locking its control switch and removing the fuses to the valve's power supply. These valve fail closed on loss of electrical power.

Justification

It is impracticable to exercise these valves during normal power operation since exercising these valves during normal power operations may result in a loss of coolant in excess of allowable limits. Exercising these valves during normal power operations may lead to a loss of coolant in excess of allowable limits and potential plant shutdown. These valves are administratively maintained closed to isolate the Class 1 reactor coolant system pressure boundary. Failure of these valves during testing at normal power conditions would require a containment entry and potential shutdown of the plant.

Alternative Test

The SV-*-6318A/B will be exercised open during cold shutdowns when the reactor coolant system pressure is depressurized. Valves SV-*-6611/6612 will be exercised open and fail safe tested open during cold shutdowns when the reactor coolant system pressure is depressurized.

	IST Pro Florida Power o Turkey Point N	ogram Plan and Light Company uclear Power Plant		
Cold Shutdown Justification CSJ-25				
Component Tag	System	Safety Class	<u>Category</u>	
MOV-3-381	047	2	Α	
MOV-3-6386	047	2	Α	
MOV-4-381	047	2	А	
MOV-4-6386	047	2	Α	

These motor operated valve must close automatically to isolate containment from the chemical volume and control system seal water injection return line. These valves provide containment isolation for Penetration 25. The valves close automatically upon receipt of a Phase A containment isolation signal. These valves may also be closed by remote manual operation.

The valves are open during normal power operations to provide a return flow path from the reactor coolant pump seal injection system (and excess letdown if in operation) to the volume control tank. This function is not required for safe shutdown or accident mitigation since the reactor coolant pumps (and letdown) are not required for safe shutdown or accident mitigation.

Justification

It is impracticable to exercise these valves during normal power operation since exercising these valves during normal power operations may result in damage to the reactor coolant pump seals.

Exercising these valves closed during normal power operations would interrupt flow from the reactor coolant pump seals. Loss of reactor coolant pump seal flow with the reactor coolant pump in operation would damage the seals due to overheating.

Alternative Test

These valves will be exercised closed during cold shutdowns when the reactor coolant pumps are not in operation.

	IST Pro Florida Power o Turkev Point N	ogram Plan and Light Company 'uclear Power Plant			
Cold Shutdown Justification CSJ-26					
<u>Component Tag</u>	<u>System</u>	Safety Class	Category		
MOV-3-862A	050	2	В		
MOV-3-862B	050	2	В		
MOV-4-862A	050	2	В		
MOV-4-862B	050	2	В		

These normally locked open motor operated valves must remain open to provide a flow path from the RWST to the suction of the residual heat removal pumps during the injection phase of an accident. These valves are maintained administratively locked open with the breaker open to ensure the valves remain open during the injection phase. The valves are maintained in the open position during normal power operations and does not receive any automatic actuation signals. After the valves are closed during the recirculation phase, they are not required to be reopened to support any accident analysis events. Therefore, the open function is considered passive.

These valves must close prior to switch over to the recirculation phase of safety injection to isolate the RWST from the residual heat removal pumps. This function prevents contamination of the RWST. The valves are closed by remote manual operation in accordance with procedure. These valves are also closed when RHR is initiated for normal plant cooldown (shutdown cooling). The valves are interlocked such that when they ares open, the shutdown cooling isolation valves (MOV-*-750/751) are closed.

Justification

It is impracticable to exercise these valves closed during normal power operation since closure of either valve during normal power operations places the plant in an undesirable and unanalyzed configuration.

Exercising these valves closed places the plant in a condition where the shared residual heat removal pumps are not available as required. Closure of the valves solely for testing would place the plant in an undesirable alignment and cause undue risk.

Alternative Test

These valves will be exercised closed during cold shutdowns when the residual heat removal pumps are not required to be in operation.

IST Program Plan Florida Power and Light Company <u>Turkey Point Nuclear Power Plant</u> Cold Shutdown Justification CSJ-27				
MOV-3-750	050	1	A	
MOV-3-751	050	1	Α	
MOV-4-750	050	1	Α	
MOV-4-751	050	1	А	

These normally closed motor operated valves must open to provide a flow path from the reactor coolant system hot leg to the suction of the residual heat removal pumps during alternate hot leg recirculation operations. This function is initiated by the operator following switchover from the RWST to containment sump and requires opening the valve by remote manual operation. These valves are also opened when RHR is initiated for normal plant cooldown (shutdown cooling). The valves are maintained in the closed position during normal power operations and do not receive any automatic actuation signals. The valves are interlocked such that they can not be opened until the RWST suction isolation valves (MOV-*-862A/B) are closed. Additionally, the valves are interlocked with reactor pressure such that they will automatically close and can not be opened with reactor pressure greater than 525 psig.

These valves must close to isolate the reactor coolant system from the lower pressure residual heat removal system during emergency conditions when hot leg recirculation is not required to be in service. These valves are considered a pressure isolation valve, required to maintain the RCS pressure boundary. The valves must close to limit leakage to <1.0 gpm.

Justification

It is impracticable to exercise these valves open or closed during normal power operation since exercising this valve during normal power operations places the plant in an undesirable and unanalyzed configuration.

Exercising these valves open/closed during normal operations would require defeating the reactor pressure interlock and RWST suction valve interlocks to cycle the valves open and closed. This testing would place the plant in an undesirable alignment and cause undue risk.

Alternative Test

These valves will be exercised open and closed during cold shutdowns when the residual heat removal system is not required to be in operation and reactor pressure is less than 525 psig.

	IST Pro Florida Power o Turkey Point N	ogram Plan and Light Company uclear Power Plant		
Cold Shutdown Justification CSJ-28				
Component Tag	<u>System</u>	Safety Class	Category	
MOV-3-863A	050	2	В	
MOV-3-863B	050	2	В	
MOV-4-863A	050	2	В	
MOV-4-863B	050	2	В	

These normally locked closed motor operated valves must open by remote manual operation to provide a flow path from the discharge of the RHR heat exchanger to the suction of the safety injection pumps during recirculation. This function is initiated by the operator following switchover from the RWST to containment sump and requires opening the valve by remote manual operation after the RWST suction valves (MOV-*-862A/B and MOV-*-864A/B) are closed. These valves are also opened to provide a flow path to the containment spray pumps and/or alternate low head injection path in the event that the safety injection pump can not be started.

The valves are required to remain closed to prevent divergence of injection flow to the RHR pump suction during the injection phase of an accident. These valves do not receive any automatic actuation signals and are administratively maintained closed with the breaker locked in the off position. Since these valves are not required to be closed to support any accident conditions after being open during recirculation, the closed position is considered passive.

Justification

It is impracticable to exercise these valves open during normal power operation since exercising these valves during normal power operations places the plant in an undesirable and unanalyzed configuration.

Exercising these valves open during normal operations would require alignment of the plant in a undesirable configuration in which the residual heat removal system could not perform its function.

Alternative Test

These valves will be exercised open during cold shutdowns when the residual heat removal system is not required to be in operation.

	IST Pro Florida Power Turkey Point N	ogram Plan and Light Company uclear Power Plant		
Cold Shutdown Justification CSJ-29				
Component Tag	System	Safety Class	Category	
3-753A	050	2	С	
3-753B	050	2	С	
4-753A	050	2	С	
4-753B	050	2	. C	

These check valves must open to provide a flow path from the residual heat removal pump to the reactor coolant system during ECCS injection and recirculation modes of operation.

These valves must close to prevent backflow through an idle pump during ECCS injection and recirculation modes of operation. Closure of these valves ensures adequate flow to the reactor coolant system in the event of a failure of the respective residual heat removal pump to start.

Justification

It is impracticable to fail safe test these valves during normal power operation since exercising these valve during normal power operations would require injection into the reactor coolant system.

To perform the necessary check valve open and closed testing requires operating the residual heat removal pump at full flow conditions. This testing can only be performed by injection into the reactor coolant system. During normal power operations, this test would require injection of borated refueling water storage tank water into the reactor. During normal power operations, this test would cause a severe power transient which may lead to a plant trip.

Alternative Test

These check valves will be exercised open and closed during cold shutdowns when the residual heat removal system is not required to be in operation and full flow testing may be performed.

IST Program Plan Florida Power and Light Company <u>Turkey Point Nuclear Power Plant</u>

Cold Shutdown Justification CSJ-30

Component Tag	<u>System</u>	Safety Class	Category
POV-3-2604	072	2	B
POV-3-2605	072	2	В
POV-3-2606	072	2	В
POV-4-2604	072	2	В
POV-4-2605	072	2	В
POV-4-2606	072	2	В

Function

These valves must close to isolate containment from the Steam Generators (closed loop inside containment) from the Main Steam Header. These valves are a secondary system barrier since the Steam Generators are a closed loop inside containment. These valves are required to close in the event of a Main Steam Line Break or Steam Generator Tube Rupture. The valves will close in response to a Main Steam Isolation Signal. These valves open during normal operation. These valves held open by an air actuator. The open function does not support safe shutdown or accident mitigation.

Justification

It is impracticable to exercise these valves closed during normal power operation since exercising this valve during normal power operations would cause a plant trip.

Closing these valves for testing during normal power operations would interrupt steam flow from the steam generator to the main steam/turbine systems. Exercising these valves closed would isolate the steam generator which would result in a severe power transient in the steam and reactor coolant systems which would lead to a subsequent trip of the plant.

Alternative Test

These valves will be exercised closed during cold shutdowns when the main steam system is not required to be in operation.

	IST Pro Florida Power o Turkey Point Na	gram Plan and Light Company aclear Power Plant	
	Cold Shutdown	Justification CSJ-31	
<u>Component Tag</u>	<u>System</u>	Safety Class	Category
MOV-3-872	050	2	В
MOV-4-872	050	2	В

These normally closed motor operated valves must open by remote manual operation to provide a flow path from the discharge of the RHR heat exchanger to the alternate low head safety injection points in the event that the safety injection pump can not be started. This function is initiated by the operator following switchover from the RWST to containment sump and requires opening the valves by remote manual operation after the RWST suction valves (MOV-*-862A/B and MOV-*-864A/B) are closed.

The valves are considered containment isolation valves for penetration 11, however, they are exempt from Appendix J Type C testing since they are connected to a penetration which is considered essential and may be in service post accident. These valves do not receive any automatic actuation signals and are operated by remote manual operation.. Since the valves are not required to be closed to support any accident conditions after being open to support alternate low head injection, the closed position is considered passive.

Justification

It is impracticable to exercise these valves open during normal power operation since exercising this valve during normal power operations places the plant in an undesirable and unanalyzed configuration.

Exercising this valve open during normal operations would require alignment of the plant in a undesirable configuration in which the residual heat removal system could not perform its function.

Alternative Test

These valves will be exercised open during cold shutdowns when the residual heat removal system is not required to be in operation.

IST Program Plan Florida Power and Light Company Turkey Point Nuclear Power Plant

ATTACHMENT 8

REFUELING OUTAGE JUSTIFICATION INDEX

(Page 1 of 1)

Refueling Outage Justification No.	Description
RJ-01	Service Air to Containment Check Valve (3-40-205) Closure Testing
RJ-02	Instrument Air to Containment Check Valve (*-40-336) Closure Testing
RJ-03	Instrument Air to Containment Check Valve (*-40-340A) Closure Testing
RJ-04	Boric Acid Pump Discharge Check Valve (3-397A/B,4-397C/D) Open Testing
RJ-05	N2 to PRT Check Valve (*-518/519) Closure Testing
RJ-06	SI Hot-Leg Injection Check Valve (*-874A/B) Open/Close Testing
RJ-07	SI Pump Discharge Check Valve (*-879A/B/C/D) Open Testing
RJ-08	SI Cold Leg Branch Injection Check Valve (*-873A/B/C) Open/Close Testing
RJ-09	SI Cold Leg Injection Check Valves (*-875A/B/C) Open Testing
RJ-10	SI Accumulator Discharge Check Valves (*-875D/E/F)
RJ-11	Containment Atmosphere Sample Return Check Valve (*-11-003) Closure Testing
RJ-12	Alternate Low Head Injection Check Valve (*-876D/E) Closure Testing
RJ-13	CCW Supply to RCP Thermal Barrier Check Valve (8-721A/B/C) Closure Testing
RJ-14	Charging Header Containment Isolation Check Valve (*-312C) Closure Testing
RJ-15	Emergency Boration Check Valve (*-351) Open Testing
RJ-16	RCP Seal Water Containment Isolation Check Valve (*-298A/B/C) Closure Testing
RJ-17	Containment Spray Suction Relief Discharge Check Valve (*-2052) Open/Close Testing
RJ-18	Safety Injection N2 Supply Check Valve (*-945E) Closure Testing
RJ-19	Low Head Injection Check Valve (*-876A/B/C) Open Testing

IST Program Plan Florida Power and Light Company Turkey Point Nuclear Power Plant

ATTACHMENT 9

REFUELING OUTAGE JUSTIFICATIONS

IST Program Plan Florida Power and Light Company Turkey Point Nuclear Power Plant			
	Refueling Outage	e Justification RJ-01	
Component Tag 3-40-205	Svstem 013	<u>Safety Class</u> 2	<u>Category</u> AC

This check valve must close to isolate containment from the non safety related service air system. This valve provides containment isolation for penetration 34. This valve opens to provide service air to containment in order to facilitate testing and maintenance. This function is not required for safe shutdown or accident mitigation since the penetration is normally isolated by upstream locked closed manual valve 3-40-204.

Justification

It is impracticable to exercise this check valve open or closed during normal power operations or cold shutdowns since closure testing imposes an increase in personnel radiation exposure.

To verify closure of this valve requires a backflow/leakage test. This testing requires entry into containment for test alignment and performance. During normal power operations and during cold shutdown periods this testing would result in an increase in personnel radiation exposure.

Alternative Test

This check valve will be exercised open and closed during each refueling outage.

Refueling Outage Justification RJ-02				
Component Tag	<u>System</u>	Safety Class	Category	
3-40-336	013	2	AC	
4-40-336	013	2	AC	

This check valve must close to isolate containment from the non safety instrument air system. This valve provides containment isolation for penetration 29.

The valve opens to provide a flow path of instrument air to the containment supply header when the instrument air system is operating. This function is not required safe shutdown or accident mitigation since the instrument air system is non safety related.

Justification

It is impracticable to exercise this check valve open or closed during normal power operations or cold shutdowns since closure testing imposes an increase in personnel radiation exposure and requires significant system off normal alignments to perform testing which may delay a unit startup.

To exercise this valve open/closed requires a forward flow test coupled with a backflow or leakage test. This testing requires entry into containment for test alignment and performance. During normal power operations and during cold shutdown periods this testing would result in an increase in personnel radiation exposure. Additionally, the instrument air supply to containment would be required to be isolated. Isolation of the instrument air system during normal operations or during cold shutdown periods would essentially require all components served by the system to be out of service causing the unit to be shutdown.

Alternative Test

This check valve will be exercised open and closed during each refueling outage.
	IST Pro Florida Power o Turkev Point Ni	gram Plan and Light Company uclear Power Plant		
Refueling Outage Justification RJ-03				
<u>Component Tag</u>	<u>System</u>	Safety Class	Category	
3-40-340A	013	2	AC	
4-40-340A	013	2	AC	

This check valve must close to isolate containment from the non safety instrument air system. This valve provides containment isolation for penetration 29.

The valve opens to provide a flow path of instrument air to the containment supply header when the instrument air system is operating. This function is not required safe shutdown or accident mitigation since the instrument air system is non safety related.

Justification

It is impracticable to exercise this check valve open or closed during normal power operations or cold shutdowns since exercise testing imposes an increase in personnel radiation exposure and requires significant system off normal alignments to perform testing which may delay a unit startup.

To exercise this valve open/closed requires a forward flow test coupled with a backflow or leakage test. This testing requires entry into containment for test alignment and performance. During normal power operations and during cold shutdown periods this testing would result in an increase in personnel radiation exposure. Additionally, the instrument air supply to containment would be required to be isolated. Isolation of the instrument air system during normal operations or during cold shutdown periods would essentially require all components served by the system to be out of service causing the unit to be shutdown.

Alternative Test

	IST Pro Florida Power o Turkey Point N	ogram Plan and Light Company uclear Power Plant		
Refueling Outage Justification RJ-04				
Component Tag	<u>System</u>	Safety Class	<u>Category</u>	
3-397A	046	2	С	
3-397B	046	2	С	
4-397C	046	2	С	
4-397D	046	2	С	

These check valves are required to open to provide a flow path from the boric acid transfer pump to the charging pumps suction header in the event that emergency boration is required. The valves also open during normal power operation to support normal boric acid batching/transfer. This function is not required for safe shutdown or accident mitigation. These valves must close to prevent backflow when the associated pump is idle and the other pump is required for emergency boration.

Justification

It is impracticable to exercise these check valves open during normal power operations or cold shutdowns since testing during power operations may cause a plant trip. Testing during cold shutdowns would delay a unit startup.

To exercise open these check valves requires operating the boric acid transfer pump at conditions which provide full design accident flow through the check valve. During normal power operations this testing would lead to the injection of high concentrations of boric acid into the reactor coolant system which may cause a plant trip. During cold shutdown periods this testing would cause a potential delay in unit startup due to the high boric acid concentrations in the reactor coolant system.

Alternative Test

	IST Pro Florida Power o Turkey Point N	ogram Plan and Light Company uclear Power Plant		
Refueling Outage Justification RJ-05				
Component Tag	<u>System</u>	Safety Class	Category	
3-518	065	2	AC	
3-519	065	2	AC	
4-518	065	2	AC	
4-519	065	2	AC	

This check valve must close to isolate containment from the non safety nitrogen supply system. This valve provides containment isolation for Penetration 6. The valve opens to provide a flow path from the nitrogen supply header to the pressurizer relief tank. This function is not required safe shutdown or accident mitigation since the nitrogen system is non safety related. The pressurizer relief tank is designed for full vacuum conditions to prevent tank collapse if the tank contents cool without nitrogen being supplied.

Justification

It is impracticable to exercise these check valves open or closed during normal power operations or cold shutdowns since closure testing imposes an increase in personnel radiation exposure and requires significant system off normal alignments to perform testing which may delay a unit startup.

To exercise this valve open/closed requires a forward flow test coupled with a backflow or leakage test. This testing requires entry into containment for test alignment and performance. During normal power operations and during cold shutdown periods this testing would result in an increase in personnel radiation exposure. Additionally, the nitrogen supply to the pressurizer relief tank would be interrupted, which may cause a pressure transient in the tank.

Alternative Test

	IST Pro Florida Power o Turkey Point N	ogram Plan and Light Company uclear Power Plant		
Refueling Outage Justification RJ-06				
Component Tag	<u>System</u>	Safety Class	<u>Category</u>	
3-874A	062	1	AC	
3-874B	062	1	AC	
4-874A	062	I	AC	
4-874B	062	1	AC	

These check valves must open to provide flow path from the safety injection pump to the reactor coolant system hot leg during the hot leg recirculation phase of operation following a loss of coolant accident. The hot leg recirculation phase is initiated by manual operation since the upstream motor operated valve MOV-*-866A/B is maintained closed with power source removed during normal operation. These check valves must close or remain closed to isolate the reactor coolant system from the lower pressure safety injection system during emergency conditions when hot leg recirculation is not required to be in service. These valves are considered a pressure isolation valve, required to maintain the RCS pressure boundary.

Justification

It is impracticable to exercise these check valves open during normal power operations or cold shutdowns since open testing requires injection of borated water into the reactor coolant system. It is impracticable to exercise these check valves closed during normal power operations or cold shutdowns since closure testing imposes an increase in personnel radiation exposure and requires significant system off normal alignments to perform testing which may delay a unit startup.

To verify check valve full open position requires operation of the safety injection pump and injection in to the reactor coolant system. This test can not be performed during normal power operations since the safety injection pump discharge pressure is lower than the normal reactor coolant system pressure. This test can not be performed during cold shutdowns since injection into the reactor coolant system requires placing the plant in a configuration outside of design. Additionally, injection of borated refueling water storage tank water may cause a delay in plant startup due to the high concentration of boric acid in the reactor coolant system.

Verification of valve closure requires the performance of a leakage test. This testing requires entry into containment for test alignment and performance. During normal power operations and during cold shutdown periods this testing would result in an increase in personnel radiation exposure. Additionally, due the amount of piping required to be isolated, drained, and vented to perform a leakage test, a delay in plant startup from the cold shutdown condition would be incurred.

Alternative Test

	IST Pro Florida Power o Turkey Point N	ogram Plan and Light Company uclear Power Plant		
Refueling Outage Justification RJ-07				
<u>Component Tag</u> 3-879A	System	Safety Class	<u>Category</u>	
3-879B	062	2	c	
4-879C 4-879D	062 062	2 2	C C	

These check valves must open to provide a flow path from the safety injection pump to the reactor coolant system during ECCS injection and recirculation modes of operation. These valves must close to prevent backflow through an idle pump during ECCS injection and recirculation modes of operation. Closure of this valve ensures adequate flow to the reactor coolant system in the event of a failure of the respective safety injection pump to start.

Justification

It is impracticable to exercise these check valves open during normal power operations or cold shutdowns since open testing requires injection of borated water into the reactor coolant system.

To verify check valve full open position requires operation of the safety injection pump at design accident conditions, and injection in to the reactor coolant system. This test can not be performed during normal power operations since the safety injection pump discharge pressure is lower than the normal reactor coolant system pressure. This test can not be performed during cold shutdowns since injection into the reactor coolant system requires placing the plant in a configuration outside of design. Additionally, injection of borated refueling water storage tank water may cause a delay in plant startup due to the high concentration of boric acid in the reactor coolant system.

Alternative Test

These check valves will be exercised open during each refueling.

IST Program Plan Florida Power and Light Company Turkey Point Nuclear Power Plant

Refueling Outage Justification RJ-08

Component Tag	System	Safety Class	Category
3-873A	064		AC
3-873B	064	1	AC
3-873C	064	1	AC
4-873A	064	1	AC
4-873B	064	1	AC
4-873C	064	1	AC

Function

This check valve must open to provide flow path from the safety injection pump to the reactor coolant system cold leg injection points during the injection phase of an accident. This check valve must close or remain closed to isolate the reactor coolant system from the lower pressure safety injection system during emergency conditions when cold leg injection is not required. This valve is considered a pressure isolation valve, required to maintain the RCS pressure boundary. The valve must close to limit leakage to <1.0 gpm.

Justification

It is impracticable to exercise these check valves open during normal power operations or cold shutdowns since open testing requires injection of borated water into the reactor coolant system. It is impracticable to exercise these check valves closed during normal power operations or cold shutdowns since closure testing imposes an increase in personnel radiation exposure and requires significant system off normal alignments to perform testing which may delay a unit startup.

To verify check valve full open position requires operation of the safety injection pump and injection in to the reactor coolant system. This test can not be performed during normal power operations since the safety injection pump discharge pressure is lower than the normal reactor coolant system pressure. This test can not be performed during cold shutdowns since injection into the reactor coolant system requires placing the plant in a configuration outside of design. Additionally, injection of borated refueling water storage tank water may cause a delay in plant startup due to the high concentration of boric acid in the reactor coolant system.

Verification of valve closure requires the performance of a leakage test. This testing requires entry into containment for test alignment and performance. During normal power operations and during cold shutdown periods this testing would result in an increase in personnel radiation exposure. Additionally, due the amount of piping required to be isolated, drained, and vented to perform a leakage test, a delay in plant startup from the cold shutdown condition would be incurred.

Alternative Test

	IST Pro Florida Power o Turkey Point N	gram Plan and Light Company uclear Power Plant		
Refueling Outage Justification RJ-09				
Component Tag	<u>System</u>	Safety Class	Category	
3-875A	064	1	AC	
3-875B	064	1	AC	
3-875C	064	1	AC	
4-875A	064	1	AC	
4-875B	064	1	AC	
4-875C	064	1	AC	

This check valve must open to provide flow path from the safety injection pump to the reactor coolant system cold leg injection points during the injection phase of an accident. The valve must also open to provide a flow path from the safety injection tank accumulator to the cold leg injection points when the reactor coolant system decreases below 660 psig. Additionally, this check valve must open to provide a flow path from the residual heat removal pump to the cold leg injection point during a large break LOCA when the RCS is rapidly depressurized and during the alternate low head injection during the recirculation phase of an accident. This check valve must close or remain closed to isolate the reactor coolant system from the lower pressure safety injection and residual heat removal systems during normal operations and emergency conditions when cold leg injection is not required. This valve is considered a pressure isolation valve, required to maintain the RCS pressure boundary. The valve must close to limit leakage to <1.0 gpm.

Justification

It is impracticable to exercise these check valves open during normal power operations or cold shutdowns since open testing requires injection of borated water into the reactor coolant system which would cause a delay in plant startup.

To verify check valve full open position requires injection of the safety injection accumulator to verify full design accident flow through the subject valve. This test can not be performed during normal power operations since the safety injection accumulator pressure is lower than the normal reactor coolant system pressure. This test can not be performed during cold shutdowns since injection into the reactor coolant system from the safety injection accumulators requires significant plant preparation to perform the test. Additionally, injection of borated safety injection accumulator water during cold shutdowns would cause a delay in plant startup due to the high concentration of boric acid in the reactor coolant system. Additionally, the performance of this test during cold shutdowns would result in an increase in personnel radiation exposure.

Alternative Test

IST Program Plan Florida Power and Light Company <u>Turkey Point Nuclear Power Plant</u>

Refueling Outage Justification RJ-10

Component Tag	System	Safety Class	Category
3-875D	064	1	C
3-875E	064	1	С
3-875F	064	1	С
4-875D	064	1	С
4-875E	064	1	С
4-875F	064	1	С

Function

This check valve must open to provide a flow path from the safety injection tank accumulator to the reactor coolant system cold leg during accident conditions whenever the reactor coolant system pressure decreases below 660 psig. This valve must close to prevent reverse flow during the injection phase of an accident when the safety injection pump is providing flow to the reactor coolant system cold leg injection path. The valve must also close when the residual heat removal pump is providing flow to the cold leg injection path or during recirculation when the alternate low head injection path is used.

Justification

It is impracticable to exercise these check valves open or closed during normal power operations or cold shutdowns since open testing requires injection of borated water into the reactor coolant system which would cause a delay in plant startup. It is impracticable to exercise these check valves closed during normal power operations or cold shutdowns since closure testing imposes an increase in personnel radiation exposure and requires significant system off normal alignments to perform testing which may delay a unit startup.

To verify check valve full open position requires injection of the safety injection accumulator to verify full design accident flow through the subject valve. This test can not be performed during normal power operations since the safety injection accumulator pressure is lower than the normal reactor coolant system pressure. This test can not be performed during cold shutdowns since injection into the reactor coolant system from the safety injection accumulators requires significant plant preparation to perform the test. Additionally, injection of borated safety injection accumulator water during cold shutdowns would cause a delay in plant startup due to the high concentration of boric acid in the reactor coolant system.

Verification of valve closure requires the performance of a leakage test. This testing requires entry into containment for test alignment and performance. During normal power operations and during cold shutdown periods this testing would result in an increase in personnel radiation exposure. Additionally, due the amount of piping required to be isolated, drained, and vented to perform a leakage test, a delay in plant startup from the cold shutdown condition would be incurred.

Alternative Test

	IST Pro Florida Power a Turkey Point Ni	gram Plan and Light Company uclear Power Plant	
Refueling Outage Justification RJ-11			
Component Tag	<u>System</u>	Safety Class	Category
3-11-003	094	2	AC
4-11-003	094	2	AC

This check valve must close to isolate containment Penetration 32 from the exhaust of the Containment Air Monitor. The valve will close due to reverse flow if the associated containment isolation valves do not close or the line ruptures. This check valve must open to establish a flow path from the exhaust of the Containment Air Monitor and Hydrogen Monitors back to containment. This function is required to allow operators to monitor post accident conditions and take necessary actions to mitigate the consequences of an accident. The Containment Air Monitor takes a suction from the Containment Cooler Exhaust Header.

Justification

It is impracticable to exercise this check valve open or closed during normal power operations or cold shutdowns since closure testing imposes an increase in personnel radiation exposure.

To exercise this valve open/closed requires a forward flow test coupled with a backflow or leakage test. This testing requires entry into containment for test alignment and performance. During normal power operations and during cold shutdown periods this testing would result in an increase in personnel radiation exposure.

Alternative Test

	IST Pro Florida Power Turkey Point N	ogram Plan and Light Company uclear Power Plant		
Refueling Outage Justification RJ-12				
Component Tag	<u>System</u>	Safety Class	<u>Category</u>	
3-876D	064	- 1	AC	
3-876E	064	1	AC	
4-876D	064	1.	AC	
4-876E	064	1	AC	

This check valve must open to provide flow path from the residual heat removal system to the cold leg injection points. The valve opens to provide alternate low head injection during the recirculation phase of an accident. This check valve must close or remain closed to prevent reverse flow when the safety injection pump or accumulators are required to inject flow to the cold leg. The valve is also required to close when RHR is in service for low head injection during the recirculation phase of an accident. The valve is required to close to isolate the reactor coolant system from the lower pressure residual heat removal system during emergency conditions when the residual heat removal system is not required. This valve is considered a pressure isolation valve, required to maintain the RCS pressure boundary. The valve must close to limit leakage to <1.0 gpm.

Justification

It is impracticable to exercise this check valve open or closed during normal power operations or cold shutdowns since closure testing imposes an increase in personnel radiation exposure and may delay plant startup.

To exercise this valve open/closed requires a forward flow test coupled with a backflow or leakage test. This testing requires entry into containment for test alignment and performance. During normal power operations and during cold shutdown periods this testing would result in an increase in personnel radiation exposure along with a high potential for delaying plant startup due to the significant amount of piping required to be filled and vented.

Alternative Test

IST Program Plan Florida Power and Light Company <u>Turkey Point Nuclear Power Plant</u> <u>Refueling Outage Justification RJ-13</u>				
Component Tag	<u>System</u>	Safety Class	<u>Category</u>	
3-721A	030	3	C	
3-721B	030	3	С	
3-721C	030	3	С	
4-721A	030	3	С	
4-721B	030	3	С	
4-721C	030	3	С	

These check valves must close to prevent uncontrolled RCS blowdown into the low pressure CCW system in the event of a RCP thermal barrier cooling coil rupture. The piping downstream of these check valves is designed for full RCS pressure, whereas the piping upstream is designed to CCW system pressure requirements. These valves open to allow cooling water flow to the reactor coolant pumps and motors during normal plant operating modes. This function prevents RCP pump damage and degradation of the pump seals that could result because a blockage of RCP cooling water. This function is not required for safe shutdown or accident mitigation.

Justification

It is impracticable to exercise these check valves closed during normal power operations or cold shutdowns since closure testing imposes an increase in personnel radiation exposure and may delay plant startup.

To verify closure of this valve requires a backflow/leakage test. This testing requires entry into containment for test alignment and performance. During normal power operations and during cold shutdown periods this testing would result in an increase in personnel radiation exposure along with a high potential for delaying plant startup due to the significant amount of piping required to be filled and vented.

Alternative Test

	IST Pro Florida Power o <u>Turkey Point N</u>	gram Plan and Light Company uclear Power Plant	
	Refueling Outage	Justification RJ-14	
Component Tag	<u>System</u>	Safety Class	Category
3-312C	047	1	AC
4-312C	047	1	AC

This check valve must open to provide a flow path from the charging pump to the reactor coolant system during emergency boration. The valve must open to provide a flow rate of 45 gpm during a rod cluster control assembly accident requiring emergency boration. During normal power operation, this valve opens to provide the normal return flow path from the charging pump to the reactor coolant system to support processing of the water let down from the reactor coolant system. This valve must close to isolate containment from the chemical and volume control system during accident conditions when the charging line is not required. The valve is considered a containment isolation valve for Penetration 15.

Justification

It is impracticable to exercise this check valve closed during normal power operations since interruption of charging flow may result in a plant trip. During cold shutdowns it is impracticable to exercise this check valve closed since closure testing imposes an increase in personnel radiation exposure and may delay plant startup.

To verify closure of this valve requires a backflow/leakage test. This testing requires entry into containment for test alignment and performance. During normal power operations and during cold shutdown periods this testing would result in an increase in personnel radiation exposure along with a high potential for delaying plant startup due to the significant amount of piping required to be filled and vented.

Alternative Test

	IST Pro Florida Power o Turkey Point Ni	ogram Plan and Light Company uclear Power Plant	
Refueling Outage Justification RJ-15			
Component Tag	<u>System</u>	Safety Class	<u>Category</u>
3-351	047	2	С
4-351	047	2	С

This check valve must open to provide a flow path from the boric acid pumps to the suction of the charging pumps during emergency conditions requiring emergency boration. The valve closes to prevent backflow and isolate the emergency boration flow path during normal operations and during emergency conditions when the RWST is supplying the charging pump suction for emergency boration However, normally closed upstream motor operated valve MOV-*-350 is relied upon for isolating the emergency boration flow path when it is not required. Therefore, this check valve does not perform a safety function in the closed position.

Justification

It is impracticable to exercise this check valve open during normal power operations since injection of highly concentrated boric acid into the reactor coolant system may lead to a plant trip. During cold shutdowns it is impracticable to exercise this check valve open since injection of highly concentrated boric acid into the reactor coolant system may lead to a delay in plant startup.

To exercise open position this check valve requires operation of the boric acid transfer pump at design accident flow conditions (60 gpm) to verify the check valve full open position. Performing this test during normal power operations would result in highly concentrated boric acid being injected into the reactor coolant system resulting in a power transient and possible trip of the plant. Performance of this test during cold shutdowns would result in a potential delay of plant startup due to the high boric acid concentration in the reactor coolant system.

Alternative Test

	IST Pro Florida Power (Turkey Point N	ogram Plan and Light Company Juclear Power Plant	<u></u>
Refueling Outage Justification RJ-16			
Component Tag	<u>System</u>	Safety Class	<u>Category</u>
3-298A	047	1	AC
3-298B	047	1	AC
3-298C	047	1	AC
4-298A	047	1	AC
4-298B	047	1	AC
4-298C	047	1	AC

These check valves must close to isolate containment from the chemical and volume control system during accident conditions when RCP seal injection flow is not required. The valves are considered containment isolation valves for Penetrations 24A/B/C. These check valves open to provide a flow path from the charging pump to the reactor coolant pump seals during normal plant operation. This function is not required for safe shutdown or accident mitigation since the reactor coolant pumps are not required for safe shutdown or accident mitigation. Additionally, the seal injection return valves (MOV-*-381 and MOV-8-6386) receive automatic closure signal to isolate the seal injection return flow path during a safety injection.

Justification

It is impracticable to exercise these check valves closed during normal power operations since interrupting seal injection flow would damage the reactor coolant pump seals. During cold shutdowns it is impracticable to exercise these check valves closed since closure testing imposes an increase in personnel radiation exposure and may delay plant startup.

To verify closure of this valve requires a backflow/leakage test. This testing requires entry into containment for test alignment and performance. During normal power operations and during cold shutdown periods this testing would result in an increase in personnel radiation exposure along with a high potential for delaying plant startup due to the significant amount of piping required to be filled and vented.

Additionally, interrupting reactor coolant pump seal injection flow when the reactor coolant pumps are in operation would damage the pump seal and ultimately the pump.

Alternative Test

	IST Pro Florida Power a Turkey Point Na	gram Plan and Light Company uclear Power Plant	
Refueling Outage Justification RJ-17			
Component Tag	<u>System</u>	Safety Class	<u>Category</u>
3-2052	050	2	<u> </u>
4-2052	050	2	С

<u>Function</u>

This check valve must open to provide a flow path from the containment spray suction relief line to the containment recirculation sump. The containment spray suction relief valve (RV-*-871) opens to prevent overpressurization of the containment spray pump suction piping. Overpressurization could occur due to thermal expansion should the piping become isolated with fission products in the water. This valve must close to isolate containment from the containment spray system. This valve is considered a containment isolation valve for penetration 54A.

Justification

It is impracticable to exercise this check valve open or closed during normal power operations or cold shutdowns since testing requires leakage testing (to verify closure) and forward flow testing (to verify open) which would result in airborne contamination in the containment sump resulting in significant clean up efforts. which would delay unit startup. Additionally, this testing would impose an increase in personnel radiation exposure.

To verify check valve full open position requires injection of either water or air into the containment sump at 25 gpm to verify full design accident flow. This testing would cause the containment to be breached and requires the containment spray system to be aligned in an unanalyzed condition. The addition of air or water to the containment sump to perform this test would create a significant cleanup effort due to the potential for airborne contamination, thus personnel radiation exposure would be increased.

Verification of valve closure requires the performance of a leakage test. This testing requires entry into containment for test alignment and performance. During normal power operations and during cold shutdown periods this testing would result in an increase in personnel radiation exposure. Additionally, due the amount of piping required to be isolated, drained, and vented to perform a leakage test, a delay in plant startup from the cold shutdown condition would be incurred.

Alternative Test

	IST Pro Florida Power a <u>Turkey Point N</u> t	gram Plan and Light Company aclear Power Plant	
Refueling Outage Justification RJ-18			
Component Tag	<u>System</u>	Safety Class	Category
3-945E	064	2	AC
4-945E	064	2	AC

This check valve must close to isolate containment from the non safety related nitrogen supply system during accident conditions. This valve is considered a containment isolation valve for Penetration 42. The valve opens to support safety injection accumulator refill to recharge and maintain the accumulators pressurized during normal power operations. This function is not required for safe shutdown or accident mitigation since the safety injection accumulators are considered a passive injection system and tank pressure is continuously monitored during normal plant operations.

Justification

It is impracticable to exercise this check valve closed during normal power operations or during cold shutdowns since closure testing imposes an increase in personnel radiation exposure and may delay plant startup due the significant amount of piping required to isolated.

To verify closure of this valve requires a backflow/leakage test. This testing requires entry into containment for test alignment and performance. During normal power operations and during cold shutdown periods this testing would result in an increase in personnel radiation exposure along with a high potential for delaying plant startup due to the significant amount of piping required to be realigned, drained, and vented.

Additionally, interrupting nitrogen supply would cause all of the safety injection accumulator tanks to be inoperable which would place the plant in an unanalyzed condition.

Alternative Test

	IST Pro Florida Power o <u>Turkey Point N</u>	ogram Plan and Light Company uclear Power Plant	
Refueling Outage Justification RJ-19			
Component Tag	<u>System</u>	Safety Class	Category
3-876A	064	1	AC
3-876B	064	1	AC
3-876C	064	1	AC
4-876A	064	1	AC
4-876B	064	1	AC
4-876C	064	1	AC

These check valves open to provide flow path from the residual heat removal system to the cold leg injection points during a large break LOCA when the RCS is rapidly depressurized. The valve must also open to provide normal low head injection during the injection phase of an accident. These check valves must close or remain closed to prevent reverse flow when the safety injection pump or accumulators are required to inject flow to the cold leg. The valve is also required to close when RHR is in service for alternate low head injection during the recirculation phase of an accident. The valve is required to close to isolate the reactor coolant system from the lower pressure residual heat removal system during emergency conditions when the residual heat removal system is not required. This valve is considered a pressure isolation valve, required to maintain the RCS pressure boundary. The valve must close to limit leakage to <1.0 gpm.

Justification

It is impracticable to exercise these valves open during normal power operations or during cold shutdowns since injection into the reactor is required to perform open exercise testing. The residual heat removal system is not designed to inject at elevated pressures and testing imposes an increase in personnel radiation exposure and may cause a delay in plant startup.

Exercising these valves open requires the residual heat removal pump to deliver flow to the reactor vessel, thereby, exercising open the subject check valves. This testing cannot be performed during normal power operations since the reactor vessel is at approximately 2000 psig. The design discharge pressure of the residual heat removal pump is approximately 600 psig. Additionally, injection into the vessel would cause severe thermal transients resulting in a trip of the reactor. Since these valves do not have individual flow instruments, non-intrusive techniques are required to verify the full open exercise. This testing requires containment entry and significant test preparation, which may cause a delay in plant startup. Additionally, entry into containment for test preparation, performance and restoration even during cold shutdowns imposes a significant increase in radiation exposure to plant personnel.

Alternative Test

These valves will be exercised open during each refueling outage.

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ATTACHMENT 10

STATION TECHNICAL POSITION INDEX

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Technical Position No.	Description
TPv-01	Bi-directional Testing of Check Valves
TPv-02	Check Valve Condition Monitoring
TPv-03	Passive Valves Without Test Requirements
TPv-04	Fail Safe Testing of Valves
TPv-05	Classification of Skid Mounted Components
TPv-06	D/E of AFW Pump Lube Oil Cooling Water Return Check Valves
TPv-07	Primary Water Check Valve Considered Passive
TPv-08	Check Valve Closure Verification in Conjunction with Appendix J Seat Leakage Testing
TPv-09	Testing of Power Operated Valves with both Active and Passive Safety Functions
TPv-10	Breathing Air Check Valve Considered Passive
TPv-11	Manual Valve Exercise Frequency
TPv-12	Method for Establishing Acceptance Criteria for Power Operated Valves
TPp-01	Containment Spray Pump Category B Pump Testing
TPp-A	Categorization of IST Pumps (Group A or B)

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ATTACHMENT 11

STATION TECHNICAL POSITIONS

IST Program Plan Florida Power and Light Company <u>Turkey Point Nuclear Power Plant</u> <u>Technical Position TPv-01</u> (Page 1 of 3)

Bi-directional Testing of Check Valves

Purpose

The purpose of this Technical Position is to establish the station position for the verification of the non-safety direction exercise testing of check valves by normal plant operations.

Applicability

This Technical Position is applicable to testing of the non-safety function (direction) of check valves which are included in the Inservice Testing Program. This position applies to those check valves required to be tested in accordance with Subsection ISTC (ASME OM Code 1998 Edition through 2000 Addenda) and Appendix II - Condition Monitoring (ASME OM Code 1995 Edition through 1996 Addenda). This Technical Position does not apply to testing of the safety function (direction) of check valves included in the Inservice Testing Program.

Background

The ASME OM Code 1998 through 2000 Addenda section ISTC-3550, "Valves in Regular Use", states:

"Valves that operate in the course of plant operation at a frequency that would satisfy the exercising requirements of this Subsection need not be additionally exercised, provided that the observations otherwise required for testing are made and analyzed during such operation and recorded in the plant record at intervals no greater than specified in ISTC-3510."

Section ISTC-3510 requires that check valves shall be exercised nominally every 3 months with exceptions (for extended periods) referenced.

Section ISTC-5221(a)(2) states:

"Check valves that have a safety function in only the open direction shall be exercised by initiating flow and observing that the obturator has traveled to either the full open position or to the position required to perform its intended function(s) (see ISTC-1100), and verify closure."

Section ISTC-5221(a)(3) states:

"Check valves that have a safety function in only the close direction shall be exercised by initiating flow and observing that the obturator has traveled [to] at least the partially open position,² and verify that on cessation or reversal of flow, the obturator has traveled to the seat."

"²The partially open position should correspond to the normal or expected system flow."

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Normal or expected system flow may vary with plant configuration and alignment, however, the open "safety function" of a check valve typically requires a specified design accident flow rate. Since Turkey Point Operations staff is trained in recognizing normal plant conditions, Operator judgment is acceptable in determining the check valve non-safety direction by obtaining normal or expected flow rates for the plant operating condition.

In summary, check valve non-safety function direction is satisfactorily demonstrated by verifying closure or passing normal or expected flow as applicable.

Position

Turkey Point will verify the non-safety position of check valves included in the Inservice Testing Program using the plant surveillance program. In lieu of a dedicated surveillance to perform the non-safety direction testing, the following alternate verifications may be performed as follows:

- 1. An appropriate means shall be determined which establishes the method for determining the open/closed non-safety function of the check valve during normal operations. The position determination may be by direct indicator, or by other positive means such as changes in system pressure, flow rate, level, temperature, seat leakage, etc. This determination shall be documented in the respective Condition Monitoring Plan for the specific check valve group. For check valves included in the Inservice Testing Program and not included in the Condition Monitoring Plan, this determination shall be documented for the specific check valve group.
- 2. Observation and analysis of plant processes that a check valve is satisfying its' non-safety direction function may used. As an example, a check valve that has a safety function only in the closed direction and normally provides a flow path to maintain plant operations. If the check valve is not open to pass flow, an alarm or indication would identify a problem to the operator. The operator would respond to take appropriate actions. A Condition Report would then be generated for the abnormal plant condition which would identify the check valve failure.
- 3. Observation and analysis of plant logs and other records satisfied by Operator or Engineering reviews may be an acceptable method for verifying a check valves non-safety direction during normal plant operations.

The open/closed non-safety function shall be recorded at a frequency required by ISTC-3510, nominally every 3 months, with exceptions as provided, in plant records such as Turkey Point Operating Logs, Electronic Rounds, chart recorders, automated data loggers, etc. The safety function direction testing requires a Quality Record in the form of a surveillance test. Records as indicated above in 1 through 3 are satisfactory for the non-safety direction testing. A condition report shall be generated for any issues regarding check valve operability.

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Justification

This Technical Position requires that the method of determining the non-safety position be established and documented in either the Condition Monitoring Plan or the IST Bases Document. The plant systems and operator actions provide for the observations and analysis that the valve is satisfying its' non-safety function. Additionally, the recording of parameters which demonstrate valve position is satisfied at a frequency in accordance with ISTC-3510. These actions collectively demonstrate the non-safety position of Inservice Testing Program check valves in regular use as required by ISTC-3550.

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Check Valve Condition Monitoring

<u>Purpose</u>

The purpose of this Technical Position is to document Turkey Point's position on establishing and implementing a Check Valve Condition Monitoring Program in accordance with mandatory Appendix II of the ASME OM Code 1995 Edition through 1996 Addenda and the associated modifications delineated in the Federal Register Volume 64, No. 183. The Condition Monitoring Program specified in Appendix II provides certain flexibility in establishing test types, examinations, and preventive maintenance activities along with their associated intervals, when justified based on check valve performance and operating condition.

Applicability

This Technical Position is applicable to certain valves or groups of valves as permitted by ISTC-5222, Condition Monitoring Program.

Background

10CFR50.55a was revised 9/22/99 to endorse the ASME OMa-1995 Edition with 1996 Addenda with modifications. This edition of the ASME OM Code provides provisions to implement a check valve condition monitoring program for selected valves or groups of valves in accordance with mandatory Appendix II. Turkey Point's Inservice Testing Program for the 4th Ten Year Interval has been developed in accordance with the ASME OM Code 1998 Edition through 2000 Addenda. This edition of the Code provides an alternative in section ISTC-5222, Condition Monitoring Program, to the testing requirements of ISTC-3510, ISTC-3520, ISTC-3540 and ISTC-5221. This section specifies that the program shall be implemented in accordance with Appendix II, Check Valve Condition Monitoring Program and the modifications stated in the Federal Register.

Position

Turkey Point will implement a Check Valve Condition Monitoring program for selected valves or groups of valves in accordance with ISTC-5222 and Appendix II. The following guidelines will be adhered to for administering this program. Additionally, if the Appendix II program is discontinued for a valve or group of valves, then the requirements of ISTC-3510, ISTC-3520, ISTC-3550, and ISTC-3521 shall be implemented.

1. <u>Purpose</u>

The purpose of the Check Valve Condition Monitoring Program is to improve check valve performance and to optimize testing, examination, and preventive maintenance activities in order to maintain the continued acceptable performance of a select valve or group of valves.

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2. <u>Scope</u>

The Turkey Point Valve Check Valve Condition Monitoring Program will be applied to individual check valves or groups of check valves which are either candidates for improved performance or candidates which will be monitored for improved valve performance.

- a. Candidates for improved valve performance are those check valves which may exhibit one or more of the following attributes:
 - i. The valve(s) exhibits an unusually high failure rate during inservice testing or operations;
 - ii. The valve(s) can not be exercised under normal operating conditions or during shutdown;
 - iii. The valve(s) exhibits unusual, abnormal, or unexpected behavior during exercising or operations.
- b. Candidates for monitoring for improved valve performance using optimization techniques, examination, and preventive maintenance activities are those check valves with documented acceptable performance that:
 - i. Have had their performance improved under this program;
 - ii. Cannot be exercised or are not readily exercised during normal operating condition or during shutdown;
 - iii. Can only be disassembled and examined; or
 - iv. It is decided that all of the associated activities of the valve or group will be optimized.
- 3. <u>Groupings</u>

For valves which are grouped together the following valve attributes shall be considered:

- a. Valves shall be of the same manufacturer, design, size, service media, materials of construction, and orientation.
- b. Maintenance and modification history shall be reviewed.
- c. Test history and results shall be reviewed.
- d. System design shall be considered to determine potential flow instabilities, degree of disassembly, and the need for tolerance and dimensional measurements

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4. <u>Analysis</u>

An analysis of the test and maintenance history shall be performed to establish the basis for specifying inservice testing, examination, and preventive maintenance activities. This analysis shall include the following:

- a. Identify any common failure mode or corrective maintenance patterns.
- b. Analyze these common patterns to determine their significance and to identify potential failure mechanisms:
 - i. Determine if certain preventive maintenance activities would mitigate the failure or maintenance patterns;
 - ii. Determine if certain condition monitoring activities are possible and effective in monitoring for these failure mechanisms;
 - iii. Determine if periodic disassembly and examination would be an effective method in monitoring for these failure mechanisms.
 - iv. Determine if the valve grouping is required to be changed.
- 5. <u>Condition Monitoring Activities</u>
 - a. Performance Improvement Activities
 - i. If sufficient information is not available or the results of the analysis performed in 4 above are not conclusive, an interim period not to exceed 2 refueling outages shall be established to determine the cause of the failure or maintenance patterns. The following activities shall be performed at sufficient intervals over the interim period.
 - 1. Identify interim tests (e.g. nonintrusive) to assess the performance of the valve of group of valves.
 - 2. Identify interim examinations to evaluate potential degradation mechanisms.
 - 3. Identify other types of analysis to be performed which will assess check valve condition.
 - 4. Identify which of these activities will be performed on each valve.
 - 5. Identify the interval of each activity.
 - ii. Complete or revise the condition monitoring test plans to document the check valve program performance improvement activities and their associated frequencies.
 - iii. Perform these activities at their assigned intervals unit:
 - 1. Sufficient information is obtained to permit an adequate analysis.
 - 2. Until the end of the interim period (2 refueling outages or 3 years, whichever is longer).

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- iv. After performance, a review shall be performed for each activity to determine if changes to the program are required. If changes are required, the program shall be revised before the next performance of the activity.
- b. Optimization of Condition Monitoring Activities
 - i. If sufficient information is available to assess the performance adequacy of the check valve or group, then the following activities shall be performed:
 - 1. Identify appropriate preventive maintenance activities including the intervals that are required to maintain the continued acceptable performance of the check valve or group of check valves.
 - 2. Identify the applicable examination activities including the interval that will be used to periodically assess the condition of each check valve or group of check valves.
 - 3. Identify the applicable test activities including intervals that will be used to periodically verify the acceptable performance of each check valve or group of check valves.
 - 4. Identify which of these activities, including the interval, will be performed on each valve in the group.
 - ii. Revise the condition monitoring plans to document the optimized condition monitoring program activities and associated intervals for each activity.
 - iii. Continue performance of these activities at their associated intervals.
 - iv. Review the results of the performance of each activity to determine if changes to the optimized condition monitoring program are required.

6. <u>Test Requirements and Frequency</u>

The following requirements apply when implementing the above plans for a single valve or group of valves

- a. Valve opening and closing functions must be demonstrated when flow testing or examination methods (nonintrusive, or disassembly and inspection) are used.
- b. The initial interval for tests and associated examinations may not exceed two fuel cycles or 3 years, whichever is longer.
- c. Extension of the initial interval may not exceed one fuel cycle per extension with the maximum interval not to exceed 10 years.

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d. Trending and evaluation of existing data must be used to reduce or extend the time interval between tests.

7. <u>Documentation</u>

The condition monitoring program shall be documented per the Check Valve Condition Monitoring Administrative Procedure. The plan for each check valve or group of check valves shall be documented in the Condition Monitoring Tab and shall contain as a minimum the following information:

- a. The list of valves in each group including the group basis.
- b. Date the valve or group of valves was evaluated for inclusion or exclusion from the condition monitoring program.
- c. Safety function of valve or valve group.
- d. Analysis/justification which forms the basis for the program.
- e. Identification of the failure or maintenance patterns for each valve
- f. Condition monitoring activities including intervals for each valve or valve group.
- g. Expert Panel review results and comments

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Technical Position TPv-03 (Page 1 of 1)

Passive Valves Without Test Requirements

Purpose

The purpose of this Technical Position is to establish the station position for valves which perform a passive safety function, however, no testing in accordance with ISTC is required.

Applicability

This Technical Position is applicable to valves which perform a passive function in accordance with ISTC-2000 and do not have inservice testing requirements per Table ISTC-3500-1. This position is typical of Category B, passive valves which do not have position indication.

"An example is a manual valve which must remain in its normal position during an accident, to perform its intended function."

Typically, manual valves which perform a safety function, are locked in their safety position and administratively controlled by TPN procedures. These valves would be considered passive. If they do not have remote position indicating systems and categorized as B, they would not be subjected to any test requirements in accordance with Table ISTC-3500-1.

<u>Position</u>

The TPNP Inservice Testing Program, Valve Tables - Attachment 13, will not list valves which meet the following criteria.

- The valve is categorized B (seat leakage in the closed position is inconsequential for fulfillment of the valves' required function(s)) in accordance with ISTC-1300.
- The valve is considered passive (valve maintains obturator position and is not required to change obturator position to accomplish the required function(s)) in accordance with ISTC-2000.
- The valve does not have a remote position indicating system which detects and indicates valve position.

Justification

Valves which meet this position will not be listed in the TPNP Inservice Testing Program, Valve Tables - Attachment 13, however, the basis for categorization and consideration of active/passive functions shall be documented in the IST Program Basis Document.

IST Program Plan Florida Power and Light Company <u>Turkey Point Nuclear Power Plant</u> <u>Technical Position TPv-04</u> (Page 1 of 1)

Fail Safe Testing of Valves

Purpose

The purpose of this Technical Position is to establish the station position for fail safe testing of valves in conjunction with stroke time exercising or position indication testing.

Applicability

This Technical Position is applicable to valves with fail safe actuators required to be tested in accordance with ISTC-3560.

Background

The ASME OM Code 1998 through 2000 Addenda section ISTC-3560 requires;

"Valves with fail-safe actuators shall be tested by observing the operation of the actuator upon loss of valve actuating power in accordance with the exercising frequency of ISTC-3510."

Section ISTC-3510 states;

"Active Category , Category B, and Category C check valves shall exercised nominally every 3 months..."

Position

In cases where normal valve operator action moves the valve to the open or closed position by deenergizing the operator electrically, by venting air, or both, the exercise test will satisfy the fail safe test requirements and an additional test specific for fail safe testing will not be performed.

Turkey Point Nuclear Plant will also use remote position indication as applicable to verify proper fail safe operation, provided that the indication system for the valve is periodically verified in accordance with ISTC-3700.

Justification

Turkey Point Nuclear Plant Inservice Testing Program valves that fail open or closed upon loss of actuator power use the fail safe mechanism to stroke the valve to its safety position. For example, an air operated valve that fails closed may use air to open the valve against spring force. When the actuator control switch is placed in the closed position, air is vented from the diaphragm and the spring moves the obturator to the closed position.

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(Page 1 of 2)

Classification of Skid Mounted Components

Purpose

The purpose of this technical position is to clarify requirements for classification of various skid mounted components, and to clarify the testing requirements of these components.

Background

The ASME Code allows classification of some components as skid mounted when their satisfactory operation is demonstrated by the satisfactory performance of the associated major components. Testing of the major component is sufficient to satisfy Inservice Testing requirements for skid mounted components. In section 3.4 of NUREG 1482, the NRC supports the designation of components as skid mounted:

"The staff has determined that the testing of the major component is an acceptable means for verifying the operational readiness of the skid-mounted and component subassemblies if the licensee documents this approach in the IST Program. This is acceptable for both Code class components and non-Code class components tested and tracked by the IST Program."

In the 1996a addenda to the ASME OM Code (endorsed by 10CFR50.55(a) in October 2000), the term skid-mounted was clarified by the addition of ISTA paragraph 1.7:

ISTA 1.7 Definitions

Skid mounted components and component sub assemblies – components integral to or that support operation of major components, even though these components may not be located directly on the skid. In general, these components are supplied by the manufacturer of the major component. Examples include: diesel skid-mounted fuel oil pumps and valves, steam admission and trip throttle valves for high-pressure coolant injection or auxiliary feedwater turbine-driven pumps, and solenoid-operated valve provided to control the air-operated valve.

This definition was further clarified in the 1998 Edition of the ASME Code:

ISTA-2000 DEFINITIONS

Skid mounted pumps and valves – pumps and valves integral to or that support operation of major components, even though these components may not be located directly on the skid. In general, these pumps and valves are supplied by the manufacturer of the major component. Examples include:

- (a) diesel fuel oil pumps and valves;
- (b) steam admission and trip throttle valves for high-pressure coolant injection pumps;
- (c) steam admission and trip throttle valves for auxiliary feedwater turbine driven pumps;
- (d) solenoid-operated valves provided to control an air-operated valve.

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Additionally the Subsections pertaining to pumps (ISTB) and valves (ISTC) includes exclusions/exemptions for skid mounted components;

ISTB-1200(c) Exclusions

Skid-mounted pumps that are tested as part of the major component and are justified by the Owner to be adequately tested.

ISTC-1200 Exemptions

Skid-mounted valves are excluded from this Subsection provided they are tested as part of the major component and are justified by the Owner to be adequately tested.

Position

The 1998 ASME OM Code definition of skid mounted should be used for classification of components in the Turkey Point Inservice Testing Program. In addition, for a component to be considered skid mounted:

- The major component associated with the skid mounted component must be surveillance tested at a frequency sufficient to meet ASME Code test frequency for the skid mounted component.
- Satisfactory operation of the skid mounted component must be demonstrated by satisfactory operation of the major component.
- The IST Bases Document should describe the bases for classifying a component as skid mounted, and the IST Program Plan should reference this technical position for the component.

Justification

Classification of components as skid mounted eliminates the need for testing of sub components that are redundant with testing of major components provided testing of the major components demonstrates satisfactory operation of the "skid mounted" components.

IST Program Plan Florida Power and Light Company Turkey Point Nuclear Power Plant

<u>Technical Position TPv-06</u> (Page 1 of 2)

Disassembly and Examination of AFW Pump Lube Oil Cooling Water Return Check Valves

<u>Purpose</u>

The purpose of this Technical Position is to establish the station position for the sample disassembly and examination program for groups of check valves which are impractical to test using flow, system pressure, level, temperature, seat leakage or nonintrusive techniques in accordance with ISTC-5221(a) and ISTC-5221(b).

Applicability

This Technical Position is applicable to Auxiliary Feedwater Pump Lube Oil Cooling Water Return Check Valves

AFWU-3-017 AFWU-4-016

This check must open to provide a return flow path of cooling water from the auxiliary feedwater pump lube oil cooler to the condensate storage tank when the auxiliary feedwater pump is required to be operated. Lube oil cooling water is required to ensure proper AFW pump operation. The valve must open to provide 60 gpm (20 gpm per pump) of return flow when three auxiliary feedwater pumps are operating. This check valve is required to close to prevent backflow from the condensate storage tank to the lube oil cooling water return header when the auxiliary feedwater pumps are not in operation. This function is necessary to conserve condensate storage tank inventory.

Background

The ASME OM Code 1998 through 2000 Addenda section ISTC-3510 requires check valves to be exercised nominally every 3 months, except as provided in ISTC-5221 and ISTC-5222. ISTC-5221(c) states that,

"If the test methods in ISTC-5221(a) and ISTC-5221(b) are impractical for certain check valves, or if sufficient flow cannot be achieved or verified, a sample disassembly examination program shall be used to verify valve obturator movement."

Position

For the subject valves, TPNP will verify check valve obturator movement using a disassembly and examination program in accordance with the following:

• Check valves are grouped in accordance with ISTC-5221(c) such that the valve in the group are of similar design, application and service condition. In accordance with ISTC-5221(c)(1) the grouping of check valves shall consider as a minimum, valve manufacturer, design, service, size, material of construction, and orientation.

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- In accordance with ISTC-5221(c)(2) during the disassembly process, the full stroke motion of the obturator shall be verified. Immediately prior to reassembly, the full stroke motion of the obturator shall be reverified. Check valves that have their obturator disturbed before full stroke motion is verified shall be examined to determine if a condition exists that could prevent full opening or reclosure of the obturator.
- At least one valve from the group shall be disassembled and examined at each refueling outage with all valves in the group being disassembled and examined at least once every 8 years in accordance with ISTC-5221(c)(3).
- Per the requirements of ISTC-5221(c)(4), before return to service, valves that were disassembled for examination or that have received maintenance that could affect their performance, shall be exercised full or partial stroke, if practicable, with flow. Those valves shall also be tested for other requirements if applicable (closure verification or seat leakage testing) before returning them to service.
- The corrective actions of ISTC-5224 shall be applied. Check valves in a sample disassembly and examination program that are not capable of full stroke movement, or have failed or have unacceptably degraded valve internals, shall have the cause of failure analyzed and the condition corrected. Other check valves in the sample group that may also be affected by this failure mechanism shall be examined or tested during the same refueling outage to determine the condition of internal components and their ability to function.¹

¹An evaluation should be made to determine if there are valves outside the sampling group that could be affected by the failure mechanism. Valves that are determined to be directly affected by the failure mechanism should be examined or tested.

Justification

To full stroke exercise these check valves requires operation of the design accident flow conditions. This test is impracticable to perform during any operating or non operating condition due to the extensive amount of cleanup required.

These valves will be included in a sample disassembly and examination program in accordance with ISTC-5221(c).

IST Program Plan Florida Power and Light Company <u>Turkey Point Nuclear Power Plant</u> <u>Technical Position TPv-07</u> (Page 1 of 2)

Primary Water Check Valve Considered Passive

Purpose

The purpose of this Technical Position is to establish the station position for classification and categorization of the Primary Water to Containment Check Valve as Passive category A.

Applicability

This Technical Position is applicable to Primary Water to Containment Check Valve:

3-10-567 4-10-567

This check valve must close to isolate containment from the primary water system. This valve provides containment isolation for Penetration 47. Penetration 47 is considered a non essential penetration which is not required to be in service post accident. This valve opens to provide a flow path from the primary water supply header to containment during cold shutdown or refueling. This function provides a supply source to facilitate maintenance and testing during outages. This function is not required for safe shutdown or accident mitigation. Additionally, downstream manual valve *-10-582 inside containment is administratively maintained in the locked closed position during normal power operations. The primary water system is not required for safe shutdown or accident mitigation.

Background

The ASME OM Code 1998 through 2000 Addenda section ISTC-2000 provides a definition of passive valves.

"*passive valves*: valves that maintain obturator position and are not required to change obturator position to accomplish the required function(s)"

The Code also provides valve category definitions as follows:

"Category A – valves for which seat leakage is limited to a specific maximum amount in the closed position for fulfillment of their required function"

"Category C – valves that are self-actuating in response to some system characteristic, such as pressure (relief valves) or flow direction (check valves) for fulfillment of the required functions"

Position

Turkey Point Nuclear Plant classifies this valve as passive since it is not required to change position to perform its intended function. The valve has been categorized as Category A since it is not self actuated due to the downstream line being isolated.

IST Program Plan Florida Power and Light Company <u>Turkey Point Nuclear Power Plant</u> <u>Technical Position TPv-07</u> (Page 2 of 2)

Justification

This penetration is isolated during all modes of operation when containment integrity is required and is not in service during any emergency or post accident conditions. Therefore this valve only performs a containment isolation function and not required to open or close for any other function. Since the valve is normally closed, and since a dead leg exists downstream, this valve is considered passive. No exercising testing is required since the valve is considered a category A valve based on ISTC-1300, Valve Categories.

The valve is seat leakage tested in accordance with Appendix J requirements.

IST Program Plan Florida Power and Light Company <u>Turkey Point Nuclear Power Plant</u>

Technical Position TPv-08 (Page 1 of 1)

Check Valve Closure Verification in Conjunction with Appendix J Seat Leakage Testing

<u>Purpose</u>

The purpose of this Technical Position is to establish the station position for the verification of check valve closure in conjunction with Appendix J leakage testing.

Applicability

This Technical Position is applicable check valves included in the IST Program which are categorized as AC and are Containment Isolation Valves:

Background

These check valves are categorized as AC in accordance with ASME OM Code ISTC-1300, Valve Categories:

"Category A – valves for which seat leakage is limited to a specific maximum amount in the closed position for fulfillment of their required function"

"Category C – values that are self-actuating in response to some system characteristic, such as pressure (relief values) or flow direction (check values) for fulfillment of the required functions"

Based on the valve category, the following test requirements of Table ISTC-3500-1 apply:

Category A test	Leakage Test in accordance with Appendix J Program
Category C test	Check Valve Exercise Test Open and Closed

Position

These valves require a seat leakage test in accordance with 10CFR50 Appendix J and a closure verification in accordance with ISTC-3522. Turkey Point Nuclear Plant will perform the Category C testing in accordance with the frequency requirements of ISTC-3510 where practicable. If testing is not practicable during quarterly operations or during shutdowns, the check valve will be tested during refueling outages.

The verification of check valve closure will be performed as the seat leakage test required by Appendix J.

Justification

All valves for this position will be documented in the IST Program Plan as category AC. A deferred testing justification shall also be documented describing the impracticability of performing a closure test during normal operations or during cold shutdowns.
<u>Technical Position TPv-09</u> (Page 1 of 2)

Testing of Power Operated Valves with Both Active and Passive Safety Functions

Purpose

The purpose of this Technical Position is to establish the testing requirements for power operated valves which have both an active and passive safety function.

Applicability

This Technical Position is applicable to power operated valves which have an active safety function in one direction while performing a passive safety function in the other direction. The following valves apply to this situation at TPNP:

Valve Tag No.	Active Safety	Passive Safety
_	Direction	Direction
LCV-*-115B	Open	Closed
MOV-*-350	Open	Closed
MOV-*-535	Closed	Open
MOV-*-536	Closed	Open
MOV-*-749A/B	Open	Closed
MOV-*-856A/B	Closed	Open
MOV-*-860A/B	Open	Closed
MOV-*-861A/B	Open	Closed
MOV-*-862A/B	Closed	Open
MOV-*-863A/B	Open	Closed
MOV-*-864A/B	Closed	Open
MOV-*-865A/B/C	Closed	Open
MOV-*-872	Open	Closed
MOV-878A/B	Closed	Open
SV-*-6318A/B	Closed	Open
SV-*-6611	Open	Closed
SV-*-6612	Open	Closed

Background

The IST Program requires valves to be exercised to the position(s) required to fulfill their safety function(s). In addition, valves with remote position indication shall have their position indication verified. The Code does not restrict position indication to active valves.

Position

Several valves included in the plant are designed to perform passive safety functions during accident conditions, and then based on plant accident response, are designed to change positions to perform another (active) function. Once in their final position, there exist no conditions in which they would be required to be placed in their original passive position.

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These valves are typically emergency core cooling system valves, which require changing position during different phases of the accident. After the original passive safety function (e.g. provide flow path) is performed, the valves are repositioned to perform the active safety function (e.g. provide containment isolation or to allow injection from another water source). The valves are not required to return to their original position.

Power operated valves with passive functions in one direction and active in the other, will be exercised and stroke timed to only their active position. If these valves have position indication, the position indication verification will include verification of both positions.

Justification

Code Interpretation 01-02 (response to inquiry OMI 99-07) addressed this issue.

Question: If a valve has safety functions in both the open and closed positions and is maintained in one of these positions, but is only required to move from the initial position to the other and is not required to return to the initial position, is stroke timing in both directions required?

Reply: No

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(Page 1 of 2)

Breathing Air Check Valve Considered Passive

Purpose

The purpose of this Technical Position is to establish the station position for classification and categorization of the Containment Breathing Air Check Valve as Passive category A.

Applicability

This Technical Position is applicable to Containment Breathing Air Check Valve:

BA-3-201 BA-4-201

This check valve must close to isolate containment from the breathing air system. This valve provides containment isolation for Penetration 30. Penetration 30 is considered a non essential penetration which is not required to be in service post accident. This valve opens to provide a flow path from the breathing air receiver to containment during cold shutdown or refueling. This function is not required for safe shutdown or accident mitigation. The breathing air system is only required to function during cold shutdown or refueling. Additionally, upstream air operated valve CV-*-6165 outside containment is administratively maintained in the locked and pinned closed position during normal plant operation.

Background

The ASME OM Code 1998 through 2000 Addenda section ISTC-2000 provides a definition of passive valves.

"*passive valves*: valves that maintain obturator position and are not required to change obturator position to accomplish the required function(s)"

The Code also provides valve category definitions as follows:

"Category A – valves for which seat leakage is limited to a specific maximum amount in the closed position for fulfillment of their required function"

"Category C – valves that are self-actuating in response to some system characteristic, such as pressure (relief valves) or flow direction (check valves) for fulfillment of the required functions"

Position

TNPP classifies this value as passive since it is not required to change position to perform its intended function. The value has been categorized as Category A since it is not self actuated due to the downstream line being isolated.

IST Program Plan Florida Power and Light Company <u>Turkey Point Nuclear Power Plant</u> <u>Technical Position TPv-10</u> (Page 2 of 2)

Justification

This penetration is isolated during all modes of operation when containment integrity is required and is not in service during any emergency or post accident conditions [0-OP-101]. Therefore, this valve only performs a containment isolation function and is not required to open or close for any other safety function. Since the valve is normally closed, with the upstream piping administratively locked and pinned closed by CV-*-6165, and a dead leg exists downstream, this valve is considered passive. No exercising testing is required since the valve is considered a category A valve based on ISTC-1300, Valve Categories.

The valve is seat leakage tested in accordance with Appendix J requirements.

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(Page 1 of 2)

Manual Valve Exercise Frequency

Purpose

The purpose of this Technical Position is to establish the station position for the frequency of exercising those manual valves which are required to be exercised.

Applicability

This Technical Position is applicable to the manual valves included in the Inservice Testing Program.

Background

The ASME OM Code 1998 through 2000 Addenda section ISTC-3540 states;

"Manual valves shall be full-stroke exercised at least once every 5 years, except where adverse conditions¹ may require the valve to be tested more frequently to ensure operational readiness."

¹Harsh service environment, lubricant hardening, corrosive or sediment laden process fluid, or degraded valve components are some examples of adverse conditions.

In the Federal Register for the Proposed Rule Change dated September 26, 2002, the NRC stated the following with regards to manual valve exercise frequency;

"Section 50.55a(b)(3)(vi) in the proposed rule would require an exercise interval of 2 years for manual valves within the scope of the ASME OM Code rather than the exercise interval of 5 years specified in the 1999 and the 2000 Addenda of the ASME Code. The 1998 Edition of the ASME OM Code specified an interval of 3 months for manual valves within the scope of the Code. The 1999 Addenda to the ASME OM Code revised ISTC-3540 to extend the exercise frequency for manual valves to 5 years."

The NRC goes further to state that;

"Section 50.55a(b)(3)(vi) is revised to clarify that the interval for exercising manual valves may not exceed 2 years when using the 1999 Addenda and 2000 Addenda of ISTC-3540"

IST Program Plan Florida Power and Light Company <u>Turkey Point Nuclear Power Plant</u> <u>Technical Position TPv-11</u> (Page 1 of 2)

Position

Turkey Point Nuclear Plant will perform exercising of manual valves within the scope of the IST Program at a frequency not to exceed 2 years.

Justification

The NRC Rule Change will be adopted for the frequency of exercising manual valves at least once every 2 years. This interval is more frequent than required by the Edition of the Code used by TPNP, therefore no other justification is required.

IST Program Plan Florida Power and Light Company <u>Turkey Point Nuclear Power Plant</u> <u>Technical Position TPv-12</u> (Page 1 of 2)

Method for Establish Acceptance Criteria for Power Operated Valves

Purpose

The purpose of this Technical Position is to establish the station position for establishing the stroke time acceptance criteria for power operated valves, including the Limiting Stroke time.

Applicability

Power Operated Valves Requiring Stroke Time Testing

Background

The IST Program requires that a valves' stroke time reference value be established in accordance with ASME OM Code 1998 through 2000 Addenda section ISTC-3300. In accordance with the definition in ISTC-2000, reference values are defined as follows:

"one or more values of test parameters measure when the equipment is know to be operating acceptably."

Acceptable ranges are then determined based on these reference values in accordance with ISTC-5114 for Power Operated Relief Valves, ISTC-5122 for Motor Operated Valves, ISTC-5132 for Pneumatically Operated Valves, ISTC-5142 for Hydraulically Operated Valves, and ISTC-5152 for Solenoid Operated Valves.

In accordance with the Valve Stroke Testing requirements for the various operator types, the limiting value(s) of full-stroke time of each valve shall be specified by the Owner. Subsection ISTC does not provide specific guidance on determining the limiting value(s). In accordance with NRC Generic Letter 89-04, "Guidance on Developing Acceptable Inservice Testing Programs"

"the limiting value should be a reasonable deviation from this reference stroke time based on the valve size, valve type, and actuator type. The deviation should not be so restrictive that it results in a valve being declared inoperable due to reasonable stroke time variations. However, the deviation used to establish the limit should be such that corrective action would be taken for a valve that may not perform its intended function. When the calculated limiting value for a full-stroke is greater than a Technical Specification (TS) or safety analysis limit, the TS or safety analysis limit should be used as the limiting value of full-stroke time.

Position

Turkey Point Nuclear Plant will use Table TPv-12-1 to establish Acceptable Ranges in accordance with ISTC-5114 for Power Operated Relief Valves, ISTC-5122 for Motor Operated Valves, ISTC-5132 for Pneumatically Operated Valves, ISTC-5142 for Hydraulically Operated Valves, and ISTC-5152 for Solenoid Operated Valves. Table TPv-12-1 will also be used as general guidance to establish the Limiting Value(s) for power-operated valves. Establishment of Acceptable Ranges and Limiting Value(s) will be as follows:

-	IST Program Plan	
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	Turkey Point Nuclear Power Plant	
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	(Page 2 of 2)	

- T_{Ref} is the reference value in seconds of a valve when it is know to be operating acceptably
- Reference values may be rounded off to the nearest tenth of a second. Acceptable Ranges may be rounded off to the nearest tenth of a second. Calculated IST Limiting Values may be rounded off to the nearest whole number. Standard rounding techniques are used when rounding (e.g., 10.45 rounds to 10.5, and 10.44 round to 10.4).
- The most conservative limiting value between the IST calculated limit (as determined from Table TPv-12-1), UFSAR limit, or Technical Specification limit should be used as the Maximum/Limiting stroke time. Any deviations from this criteria will be evaluated.
- When a valve or its control system has been replace, repaired, or has undergone maintenance¹ that could affect the valve's performance, a new reference value shall be determined or the previous value reconfirmed by an inservice test run before it is returned to service or immediately if not removed from service.

Valve Operator	Reference Stroke Time (Seconds)	Acceptable Range	Limiting Stroke Time
Motor	$T_{Ref} > 10.0$	$0.85T_{Ref} - 1.15T_{Ref}$	1.25T _{Ref}
Motor	$T_{Ref} \le 10.0$	$0.75T_{Ref} - 1.25T_{Ref}$	1.50T _{Ref}
Pneumatic ²	$T_{Ref} > 10.0$	$0.75T_{Ref} - 1.25T_{Ref}$	1.75T _{Ref}
Pneumatic ²	$T_{Ref} \le 10.0$	$0.50T_{Ref} - 1.50T_{Ref}$	2.00T _{Ref}
All (Optional)	$T_{Ref} < 2.0$	\leq 2.0 seconds	> 2.0 seconds

Table	TPv-12-1
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¹Adjustment of stem packing, limit switches, or control system valves, and removal of the bonnet, stem assembly, actuator, obturator, or control system components are examples of maintenance that could affect valve performance.

²Pneumatic operators are air, hydraulic or solenoid operator types.

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Containment Spray Pump Category B Pump Testing

Purpose

The purpose of this Technical Position is to establish the station position for performing the quarterly Containment Spray Pump test at conditions less than 20 % of Design Flow Rate.

Applicability

This Technical Position is applicable to the following pumps

Pump Number	Class	Group	Function
3P214A	2	B	Containment Spray
3P214B	2	B	Containment Spray
4P214A	2	B	Containment Spray
4P214B	2	B	Containment Spray

Background

The IST Program requires that each pump required to tested to the rules of Subsection ISTB, be categorized as either a Group A or Group B pump. ISTB-2000, SUPPLEMENTAL DEFINITIONS defines these groupings as follows:

group A pumps: pumps that are operated continuously or routinely during normal operation, cold shutdown, or refueling operations.

group B pumps: pumps in standby systems that are not operated routinely except for testing.

The Containment Spray pumps are categorized as Group B pumps since they are in a standby system and not operated routinely except for testing.

In accordance with ISTB-3300(e)(2);

Reference values shall be established within $\pm 20\%$ of pump design flow for the group A and group B tests, if practicable. If not practicable, the reference point flow rate shall be established at the highest practical flow.

Position

It is not practicable to test the Containment Spray pumps within $\pm 20\%$ of pump design flow during normal power operations. Turkey Point Nuclear Power Plant will perform the category B pump test at a reference flow point as high as practical.

IST Program Plan Florida Power and Light Company <u>Turkey Point Nuclear Power Plant</u> <u>Technical Position TPp-01</u> (Page 2 of 2)

Justification

To test the containment spray pumps at $\pm 20\%$ of design pump flow conditions (1450 gpm) requires operating the pump in a range of 1160 – 1740 gpm. Since a downstream recirculation flow path capable of this flow range does not exist, injection of borated water from the Refueling Water Storage Tank into the containment is the only possible flow path to perform this test to satisfy these conditions.

This test is impracticable to perform during any mode of operation due to the extensive system alteration and amount of cleanup required.

<u>Technical Position TPp-A</u> (Page 1 of 2)

Position

Turkey Point Nuclear Power Plant has categorized the pumps required to be included in the Inservice Testing Program as either Group A or B in accordance with the requirements of ISTB-1300/2000.

Group A pumps are pumps that are operated continuously or routinely during normal operation, cold shutdown, or refueling operations. The following pumps are categorized as Group A at Turkey Point Nuclear Power Plant:

Pump Number	Class	Group	Function
3P201A	2	A	Charging
3P201B	2	A	Charging
3P201C	2	A	Charging
3P203A	2	Α	Boric Acid Transfer
3P203B	2	A	Boric Acid Transfer
3P210A	2	Α	Residual Heat Removal
3P210B	2	A	Residual Heat Removal
3P211A	3	A	Component Cooling Water
3P211B	3	Α	Component Cooling Water
3P211C	3	Α	Component Cooling Water
3P9A	3	A	Intake Cooling Water
3P9B	3	A	Intake Cooling Water
3P9C	3	Α	Intake Cooling Water
4P201A	2	A	Charging
4P201B	2	A	Charging
4P201C	2	Α	Charging
4P203A	2	A	Boric Acid Transfer
4P203B	2	Α	Boric Acid Transfer
4P210A	2	A	Residual Heat Removal
4P210B	2	Α	Residual Heat Removal
4P211A	3	Α	Component Cooling Water
4P211B	3	Α	Component Cooling Water
4P211C	3	A	Component Cooling Water
4P9A	3	Α	Intake Cooling Water
4P9B	3	A	Intake Cooling Water
4P9C	3	Α	Intake Cooling Water

Technical Position TPp-A (Page 2 of 2)

Group B pumps are those pumps in standby systems that are not operated routinely except for testing. The following pumps are categorized as Group B at Turkey Point Nuclear Power Plant:

Pump Number	Class	Group	Function
P2A	3	В	Auxiliary Feedwater
P2B	3	В	Auxiliary Feedwater
P2C	3	В	Auxiliary Feedwater
3P214A	2	В	Containment Spray
3P214B	2	В	Containment Spray
3P214C	2	В	Containment Spray
3P215A	2	В	Safety Injection
3P215B	2	В	Safety Injection
3P215C	2	В	Safety Injection
4P214A	2	B	Containment Spray
4P214B	2	В	Containment Spray
4P214C	2	В	Containment Spray
4P215A	2	В	Safety Injection
4P215B	2	В	Safety Injection
4P215C	2	В	Safety Injection

Group A Pump Tests – Group A tests are performed quarterly for each pump categorized as A. The following inservice test parameters are measured for each Group A pump test:

- Speed (if pump is variable speed)
- Differential Pressure
- Discharge Pressure, (for positive displacement pumps)
- Flow Rate
- Vibration

Group B Pump Tests - Group B tests are performed quarterly for each pump categorized as B. The following inservice test parameters are measured for each Group B pump test.

- Speed (if pump is variable speed)
- Differential Pressure⁽¹⁾
- Flow Rate⁽¹⁾

⁽¹⁾ For positive displacement pumps, flow rate shall be measured or determined, for all other pumps, differential pressure or flow rate shall be measured or determined.

Comprehensive Pump Tests – Comprehensive pump tests are performed biennially for all pumps in the Inservice Testing Program. The following inservice test parameters are measured for each Comprehensive pump test:

- Speed (if pump is variable speed)
- Differential Pressure
- Discharge Pressure, (for positive displacement pumps)
- Flow Rate

• Vibration

The following instrument accuracy requirements apply to each test type:

Parameter	Group A	Group B	Comprehensive
Pressure	+/- 2.0%	+/- 2.0%	+/- 0.5%
Flow Rate	+/- 2.0%	+/- 2.0%	+/- 2.0%
Speed	+/- 2.0%	+/- 2.0%	+/- 2.0%
Vibration	+/- 5.0%	+/- 5.0%	+/- 5.0%
Differential Pressure	+/- 2.0%	+/- 2.0%	+/- 0.5%

ATTACHMENT 12

INSERVICE TESTING PUMP TABLE

Revision Date: 02/11/04

Turkey Point Nuclear Plant
IST Program Plan
Pump Table

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Pump Tag	Safety Class	Pump Type	Pump Driver	Nominal Speed	P&ID	P&ID Coor.	Category	Test Type	Test Freq.	Relief Request	Tech. Pos.
P2A	3	Centrifugat	Turbine	5900	5610-M-3075-2	B3	Group B	DPc	Y2		
								Nb	M3		
								Nc	Y2		
								Qb	M3		
								Qc	Y2		
	Pump	Name: AFW Pi	IMD A					Vc	Y2		
. <u></u>						•					
P2B	3	Centrifugal	Turbine	5900	5610-M-3075-2	D3	Group B	DPc	Y2		
				•				Nb	M3		
								Nc	Y2		
								Qb	M3		
								Qc	Y2		
								Vc	Y2		
	Pump	Name: AFW Pu	ımp B								
P2C	3	Centrifugal	Turbine	5900	5610-M-3075-2	F3	Group B	DPc	Y2		
								Nb	M3		
								Nc	Y2		
								Qb	M3		
								Qc	Y2		
								Vc	Y2		
	Pump	Name: AFW Po	ump C								
3P201A	2 F	Positive Displacement	nt Motor	1745	5613-M-3047-2	G5	Group A	Na	M3	PR-05	
								PDa	M3	PR-05	
			÷					Qa	M3	PR-05	
								Va	M3	PR-05	
	Pump	Name: 3A Cha	rging Pum	0							
3P201B	2 F	ositive Displacemer	nt Motor	1745	5613-M-3047-2	F5	Group A	Na	мз	PR-05	
								PDa	МЗ	PR-05	
								Qa	M3	PR-05	
								Va	M3	PR-05	
	Pump	Name: 3B Cha	raina Pum	0							

Turkey Point Nuclear Plant
IST Program Plan
Pump Table

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									Pump Table		
Pump Tag	Safety Class	Pump Type	Pump Driver	Nominal Speed	P&ID	P&ID Coor.	Category	Test Type	Test Freq.	Relief Request	Tech. Pos.
3P201C	2	Positive Displacement	Motor	1745	5613-M-3047-2	D5	Group A	Na	М3	PR-05	
								PDa	M3	PR-05	
								Qa	мз	PR-05	
								Va	М3	PR-05	
	Purr	np Name: 3C Charg	ing Pum	p							
3P203A	2	Centrifugal	Motor	1800	5610-M-3046-1	D6	Group A	DPa	M3	PR-01,02	
								DPc	Y2	PR-02	
								Qc	Y2		
								Va	М3	PR-01	
								Vc	Y2		
	Pun	np Name: Boric Acl	id Transf	er Pump 3	A						
3P203B	2	Centrifugal	Motor	1800	5610-M-3046-1	E5	Group A	DPa	М3	PR-01,02	
								DPc	Y2	PR-02	
								Qc	Y2		
								Va	МЗ	PR-01	
								Vc	Y2		
	Pur	np Name: Boric Aci	id Transf	er Pump 3	IB						
3P210A	2	Centrifugal	Motor	N/A	5613-M-3050-1	C3	Group A	DPa	CS	PR-04	
								DPb	мз	PR-04,06	
								DPc	Y2	PR-04	
								Qa	CS		
				•				Qc	Y2		
								Va	CS		
								Vc	Y2		
	Pun	np Name: 3A Resid	ual Heat	Removal	Pump						
3P210B	2	Centrifugal	Motor	N/A	5613-M-3050-1	E3	Group A	DPa	CS	PR-04	
				·				DPb	мз	PR-04,06	
								DPc	Y2	PR-04	·
								Qa	CS		
								Qc	Y2		
								Va	CS		
								Vc	Y2		
	Рип	np Name: 3B Resid	ual Heat	Removal	Pump						

Turkey Point Nuclear Plant
IST Program Plan
Pump Table

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Pump Tag	Safety Class	Pump Type	Pump Driver	Nominal Speed	P&ID	P&ID Coor.	Category	Test Type	Test Freq.	Relief Request	Tech. Pos.
3P211A	3	Centrifugal	Motor	1800	5613-M-3030-1	F5	Group A	DPa	M3	PR-02,05	
								Qa	M3	PR-05	
								Va	M3	PR-05	
	Pump	Name: Compo	nent Cooli	ng Water I	Pump 3A						
3P211B	3	Centrifugal	Motor	1800	5613-M-3030-1	F3	Group A	DPa	МЗ	PR-02,05	
								Qa	M3	PR-05	
						•		Va	M3	PR-05	
	Pump	Name: Compo	nent Cooli	ng Water I	Pump 3B						
3P211C	3	Centrifugat	Motor	1800	5613-M-3030-1	F2	Group A	DPa	M3	PR-02,05	
								Qa	M3	PR-05	
								Va	M3	PR-05	
	Pump	Name: Compo	nent Cooli	ng Water	Pump 3C						
3P214A	2	Centrifugal	Motor	1800	5613-M-3068-1	D3	Group B	DPa	M3	PR-03	
								Qa	M3	PR-03	TPp-01
								Va	M3	PR-03	
	Pump	Name: Contain	iment Spra	y Pump 3	A						
3P214B	2	Centrifugal	Motor	1800	5613-M-3068-1	G3	Group B	DPa	M3	PR-03	
								Qa	M3	PR-03	TPp-01
								Va	M3	PR-03	
	Pump	Name: Contair	ment Spra	y Pump 3	B			_		_	
3P215A	2	Centrifugal	Motor	1800	5613-M-3062-1	E3	Group B	DPc	Y2	PR-02	
								Qb	M3		
								Qc	Y2		
								Vc	Y2		
	Pump	Name: Safety I	njection P	ump 3A				•			
3P215B	2	Centrifugal	Motor	1800	5613-M-3062-1	G3	Group B	DPc	Y2	PR-02	
								Qb	M3		
								Qc	Y2		
								Vc	Y2		
	Pump	Name: Safety I	njection P	ump 3B							

Turkey Point Nuclear Plant
IST Program Plan
Pump Table

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Pump Tag	Safety Class	Pump Type	Pump Driver	Nominal Speed	P&ID	P&ID Coor.	Category	Test Type	Test Freq.	Relief Request	Teci Pos
3P9A	3	Vertical	Motor		5613-M-3019-1	F2	Group A	DPa	М3	PR-05	
								Qa	МЗ	PR-05	
	Pump	Name: Intake C	ooling Wa	ater Pump	3 A			Va	МЗ	PR-05	
3P9B	3	Vertical	Motor		 5613-M-3019-1	D2	Group A	DPa	МЗ	PR-05	
								Qa	МЗ	PR-05	
								Va	· M3	PR-05	
	Pump	Name: Intake C	ooling Wa	ater Pump	3B						
3P9C	3	Vertical	Motor		5613-M-3019-1	B2	Group A	DPa	М3	PR-05	
								Qa	M3	PR-05	
								Va	M3	PR-05	
	Pump	Name: Intake C	ooling Wa	ater Pump	3C						
4P201A	2 F	Positive Displacement	Motor	1745	5614-M-3047-2	G5	Group A	Na	МЗ	PR-05	
								PDa	M3	PR-05	
								Qa	M3	PR-05	
	Pump	Name: 4A Char	ging Pum	q				Va	M3	PR-05	-
4P201B	2 F	Positive Displacement	Motor	1745	5614-M-3047-2	F5	Group A	Na	M3	PR-05	
								PDa	М3	PR-05	
								Qa	М3	PR-05	
								Va	М3	PR-05	
 .	Pump	Name: 4B Char	ging Pum	ip							
4P201C	2 F	Positive Displacement	Motor	1745	5614-M-3047-2	D5	Group A	Na	М3	PR-05	
								PDa	M3	PR-05	
								Qa	M3	PR-05	
	Pump	Name: 4C Char	ging Pum	IP				Va	M3	PR-05	
	2	Centrifucal	Motor	1800		E5	Group A	Dna	M3	PR-01.02	
	-	o o no no gon			5010 in 00101	20	Citabu	DPc	Y2	PR-02	
								2, 0	·-		
								uc	12		
								UC Va	12 M3	PR-01	

									Pump	Table	
Pump Tag	Safety Class	Pump Type	Pump Driver	Nominal Speed	P&ID	P&ID Coor.	Category	Test Type	Test Freq.	Relief Request	Tech. Pos.
4P203B	2	Centrifugal	Motor	1800	5610-M-3046-1	F4	Group A	Dpa	M3	PR-01,02	
								DPc	Y2	PR-02	
								Qc	Y2		
								Va	M3	PR-01	
								Vc	Y2		
	Pump	Name: Boric A	cid Transf	er Pump 4	В						
4P210A	2	Centrifugal	Motor	N/A	5614-M-3050-1	C3	Group A	DPa	cs	PR-04	
								DPb	M3	PR-04,06	
	•							DPc	Y2	PR-04	
								Qa	cs		
								Qc	Y2		
								Va	cs		
								Vc	Y2		
	Pump	Name: 4A Resi	dual Heat	Removal	Pump						
4P210B	2	Centrifugal	Motor	N/A	5614-M-3050-1	E3	Group A	DPa	CS	PR-04	
								DPb	M3	PR-04,06	
								DPc	Y2	PR-04	
								Qa	CS		
								Qc	Y2		
								Va	CS		
								Vc	Y2		
	Pump	Name: 4B Res	idual Heat	Removal	Pump						
4P211A	3	Centrifugal	Motor	1800	5614-M-3030-1	F5	Group A	DPa	М3	PR-02,05	
						•		Qa	M3	PR-05	
								Va	М3	PR-05	
	Pump	Name: Compo	nent Cooli	ng Water i	Pump 4A						
4P211B	3	Centrifugal	Motor	1800	5614-M-3030-1	F3	Group A	DPa	M3	PR-02,05	
								Qa	МЗ	PR-05	
								Va	М3	PR-05	
	Pump	Name: Compo	nent Cooli	ng Water	Pump 4B						
4P211C	3	Centrifugal	Motor	1800	5614-M-3030-1	F2	Group A	DPa	МЗ	PR-02,05	
								Qa	M3	PR-05	
								Va	M3	PR-05	
	Pump	Name: Compo	nent Cooli	ng Water	Pump 4C						

									Pump	Table	
Pump Tag	Safety Class	Pump Type	Pump Driver	Nominal Speed	P&ID	P&ID Coor.	Category	Test Type	Test Freq.	Relief Request	Tech. Pos.
4P214A	2	Centrifugal	Motor	1800	5614-M-3068-1	C3	Group B	DPa	М3	PR-03	
								Qa	M3	PR-03	TPp-01
	Pump	Name: Contair	nment Spra	ay Pump 4	A			Va	МЗ	PR-03	
4P214B	2	Centrifugal	Motor	1800	5614-M-3068-1	F3	Group B	DPa	 M3	 PR-03	
							•	Qa	M3	PR-03	TPp-01
								Va	M3	PR-03	
_	Pump	Name: Contair	nment Spra	ay Pump 4	В						
4P215A	2	Centrifugal	Motor	1800	5614-M-3062-1	E3	Group B	DPc	Y2	PR-02	
								Qb	M3		
								Qc	Y2		
	Pump	Name: Safety I	Injection P	ump 4A				Vc	Y2		
4P215B	2	Centrifimal	 Motor	1800	5614-M-3062-1	63	Group B	DPc	¥2	PR-02	
	•	ocnanogua	motor	1000	00141110002-1	00	Cloup D	Ob	M3	111-02	
								Qc	Y2		
								Vc	¥2		
	Pump	Name: Safety i	Injection P	ump 4B							
4P9A	3	Vertical	Motor		5614-M-3019-1	F2	Group A	DPa	М3	PR-05	
								Qa	M3	PR-05	
								Va	М3	PR-05	
	Pump	Name: Intake (Cooling Wa	ater Pump	4A						
4P9B	3	Vertical	Motor		5614-M-3019-1	D2	Group A	DPa	M3	PR-05	_
								Qa	М3	PR-05	
	Pump	Name: Intake (Cooling W	ater Pump	4B			Va	M3	PR-05	
4000					EC14 14 2040 4						<u></u>
ットコレ	3	VENUCAI	IVIOLOT		0014-11-0019-1	DZ	Group A	Ura Os	MD MR	FR_03	
								W (G	1110	11,000	

Pump Name: Intake Cooling Water Pump 4C

Va

МЗ

PR-05

Turkey Point Nuclear Plant IST Program Plan

ATTACHMENT 13

INSERVICE TESTING VALVE TABLE

Safety P&ID Safety Valve Act. Active / Normal Test Test Relief Deferred Tech. Coor. Class Cat. Size Type Type Passive Position Position Type Freq. Request Just. Pos. P&ID Valve Tag 3-40-204 5610-M-3013-1 2 2.0 MAN Ρ LC С D6 Α GA AT-01 App-J Valve Name: Serv Air to Cntmt Isol 3-40-205 5610-M-3013-1 C7 2 A/C 2.0 СК SA A SYS С AT-01 App-J CC RR RJ-01 CO RR RJ-01 TPv-01 Valve Name: Service Air to Containment Check Valve 3-40-336 5613-M-3013-7 **B**3 2 A/C 2.0 СК SA A SYS С AT-01 App-J CC RR **VR-01 RJ-02** CO RR **VR-01** RJ-02 TPv-01 Valve Name: Instrument Air to Containment Check Valve С 3-40-340A 5613-M-3013-7 **B**3 2 A SYS A/C 2.0 SCK SA AT-01 App-J CC RR **VR-01 RJ-03** CO RR VR-01 RJ-03 TPv-01 Valve Name: Instrument Air to Containment Check Valve 5610-M-3013-1 D7 2 2.0 GL MAN Ρ LC С HV-3-17 А AT-01 App-J Valve Name: Hydrogen Recombiner Isolation Valve 4-40-204 5610-M-3013-1 F6 2 Α 2.0 GA MAN Ρ LC С AT-01 App-J Serv Air to Cntmt Isol Valve Name: 4-40-205 5610-M-3013-1 F7 2 A 2.0 GA MAN Ρ LC С AT-01 App-J Service Air to Containment Manual Iso Valve Valve Name: 4-40-336 5613-M-3013-7 D3 2 A/C 2.0 CK SA A SYS С AT-01 App-J CC RR VR-01 RJ-02 CO RR VR-01 RJ-02 TPv-01 Valve Name: Instrument Air to Containment Check Valve 4-40-340A 5613-M-3013-7 D3 СК SA A SYS С 2 A/C 2.0 AT-01 App-J CC RR VR-01 RJ-03 CO RR **VR-01** RJ-03 TPv-01 Valve Name: Instrument Air to Containment Check Valve

Instrument Air/Service Air (013)

Condensate Storage (018)

Valve Tag	P&ID	P&ID Coor.	Safety Class	Cat.	Size	Vaive Type	Act. Type	Active / Passive	Normal Position	Safety Position	Test Type	Test Freq.	Relief Request	Deferred Just.	Tech. Pos.
3-20-401	5613-M-3018-1	D3	3	с	8.0	СК	SA	A	SYS	0	CCD	СМ			TPv-01,02
											COF	СМ			TPv-02
	Valve Name:	Cond	ensate	Stora	ge Tan	ik Outlei	t Check	Valve							
4-20-401	5614-M-3018-1	E6	3	С	8.0	СК	SA	A	SYS	0	CCD	СМ			TPv-01,02
											COF	СМ			TPv-02
	Valve Name:	Cond	ensate	Stora	ge Tar	k Outle	t Check	Valve							

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P&ID Safety Valve Act. Active / Normal Safety Test Test Relief Deferred Tech. Cat. Size Coor. Class Type Type Passive Position Position Type Freq. Request Just. Pos. P&ID Valve Tag 24.0 SYS O/C 3-50-311 5613-M-3019-1 F3 3 С СК SA A CC М3 CO М3 Valve Name: ICS Pump 3A Disch Check Valve 3-50-315 5613-M-3019-1 B4 3 В 8.0 GA MAN Α С С BTC Y2 TPv-11 Valve Name: **ICW/TPCW Basket Strainer Isolation Valve** 3-50-321 5613-M-3019-1 D3 24.0 A SYS O/C CC M3 3 С СК SA CO M3 Valve Name: ICW Pump 3B Disch Check Valve 3-50-331 5613-M-3019-1 B3 СК SA Α. SYS O/C CC M3 3 С 24.0 CO M3 Valve Name: ICW Pump 3C Disch Check Valve С 3-50-335 5613-M-3019-1 GA MAN Α С F4 3 в 8.0 BTC Y2 TPv-11 Valve Name: **ICW/TPCW Basket Strainer Isolation Valve** POV-3-4882 5613-M-3019-1 30.0 0 С M3 **B**4 BTF AO A BTC 3 В FC M3 TPv-04 PIT Y2 Valve Name: ICW/TPCW Isolation Valve to Hx 3A POV-3-4883 5613-M-3019-1 F4 30.0 AO Α 0 С BTC M3 3 В BTF FC M3 TPv-04 PIT Y2 Valve Name: ICW/TPCW Isolation Valve to Hx 3B 4-50-311 5614-M-3019-1 24.0 A SYS O/C M3 F3 3 С CK SA CC M3 CO Valve Name: ICW Pump 4A Disch Check Valve 4-50-315 5614-M-3019-1 F4 8.0 GA MAN A С С BTC 3 В Y2 TPv-11 Valve Name: ICW/TPCW Basket Strainer Isolation Valve 4-50-321 5614-M-3019-1 D3 3 С 24.0 СК SA A SYS O/C CC M3 CO M3 ICW Pump 4B Disch Check Valve Valve Name:

Intake Cooling Water (019)

Intake Cooling Water (019)

Valve Tag	P&ID	P&ID Coor.	Safety Class	Cat.	Size	Valve Type	Act. Type	Active / Passive	Normal Position	Safety Position	Test Type	Test Freq.	Relief Request	Deferred Just.	Tech. Pos.
4-50-331	5614-M-3019-1	B3	3	С	24.0	СК	SA	A	SYS	O/C	СС	M3		<u></u> .	-
	Valve Name:	ICW F	ump 4	C Dis	ch Che	ck Valv	e				CO	М3			
4-50-335	5614-M-3019-1	C4	3	B	8.0	GA	MAN	A	с	С	BTC	Y2			TPv-11
	Valve Name:		PCW E	laske	Strain	ier Isola	tion Va	lve							
POV-4-4882	5614-M-3019-1	F4	3	В	30.0	BTF	AO	A	0	С	BTC	M3			
											FC	M3			TPv-04
•											PIT	Y2			
	Valve Name:	ICW/T	PCW I	solatio	on Valv	/e to Hx	4A								
POV-4-4883	5614-M-3019-1	B4	3	B	30.0	BTF	AO	A	0	С	BTC	M3			
											FC	мз			TPv-04
											PIT	Y2			
	Valve Name:	ICW/Т	PCW Is	solatio	on Valv	/e to Hx	4B								

P&ID Safety Valve Act. Active / Normal Safety Test Test Relief Deferred Tech. Coor. Class Cat. Size Type Type Passive Position Position Type Freq. Request Just. Pos. P&ID Valve Tag Ρ С 3-10-567 5613-M-3020-2 C5 2 A/C СК SA С VR-01 2.0 AT-01 App-J TPv-07 Valve Name: **Primary Water to Containment Line Check Valve** 3-10-582 5613-M-3020-2 2 2.0 MAN Ρ LC С AT-01 App-J D6 A GA Primary Water to Containment Line Isolation Valve Valve Name: RV-3-302 5613-M-3020-2 D6 2 A/C 0.75 RV SA A С O/C AT-01 App-J RT Y10 Valve Name: **Primary Water to Containment Line Relief Valve** 4-10-567 5614-M-3020-2 D5 2 A/C 2.0 СК SA Ρ С С VR-01 TPv-07 AT-01 App-J Valve Name: **Primary Water to Containment Line Check Valve** 5614-M-3020-2 **C**6 MAN Ρ LC Ç 4-10-582 2 A 2.0 GA AT-01 App-J Valve Name: **Primary Water to Containment Line Isolation Valve** RV-4-302 5614-M-3020-2 D6 2 A/C RV SA A С O/C AT-01 App-J 0.75 RT Y10 Valve Name: Primary Water to Containment Line Relief Valve

Primary Water Makeup (020)

P&ID Safety Valve Act. Active / Normal Safety Test Test Relief Deferred Tech. Coor. Class Cat. Freq. Size Type Type Passive Position Position Туре Request Just. Pos. P&ID Valve Tag 5613-M-3022-1 С 3-70-274A C2 SR С 1.5 CK SA SYS CC M3 A CO OP TPv-01 Valve Name: 3A EDG Air Receiver Tanks C & D Inlet Check Valves 3-70-274B 5613-M-3022-2 C2 SR С 1.5 СК SA A SYS С CC M3 co OP TPv-01 Valve Name: 3B EDG Air Receiver Tanks C & D Inlet Check Valves 3-70-276A D2 SYS С CC 5613-M-3022-1 SR С 1.5 СК SA A M3 CO OP **TPv-01** Valve Name: 3A EDG Air Receiver Tanks A & B Inlet Check Valves 3-70-276B 5613-M-3022-2 D2 SR С 1.5 CK SA A SYS С CC M3 CO OP TPv-01 Valve Name: **3B EDG Air Receiver Tanks A & B Inlet Check Valves** RV-3-210A 5613-M-3022-1 **B4** SR С RV SA A С O/C RT Y10 Valve Name: **3A EDG Air Receiver Tank A Relief Valve** RV-3-210B 5613-M-3022-2 **B**4 SR С RV SA A С O/C RT Y10 Valve Name: **3B EDG Air Receiver Tank A Relief Valve** RV-3-211A 5613-M-3022-1 **B4** SR С RV SA С O/C A RT Y10 Valve Name: **3A EDG Air Receiver Tank B Relief Valve** RV-3-211B 5613-M-3022-2 **B**4 SR С RV SA A C O/C RT Y10 Valve Name: **3B EDG Air Receiver Tank B Relief Valve** С RV-3-212A 5613-M-3022-1 **B**3 SR С RV SA A O/C RT Y10 Valve Name: **3A EDG Air Receiver Tank C Relief Valve** RV-3-212B 5613-M-3022-2 **B**3 SR С RV SA A С O/C RT Y10 Valve Name: **3B EDG Air Receiver Tank C Relief Valve** RV-3-213A 5613-M-3022-1 B3 С RV SA С O/C SR A RT Y10 Valve Name: 3A EDG Air Receiver Tank D Relief Valve 5613-M-3022-2 С O/C RV-3-213B **B**3 SR С RV SA A RT Y10 Valve Name: **3B EDG Air Receiver Tank D Relief Valve**

Emergency Diesel Generator (022)

Emergency Diesel Generator (022)

Valve Tag	P&ID	P&ID Coor.	Safety Class	Cat.	Size	Valve Type	Act. Type	Active / Passive	Normal Position	Safety Position	Test Type	Test Freq.	Relief Request	Deferred Just.	Tech. Pos.
RV-3-214A	5613-M-3022-5 Valve Name:	B6 3A ED	SR 9 G M air	C n Lube	e Oil P	RV ump Dis	SA sch Reli	A ef Valve	С	0/C	RT	Y10			
RV-3-214B	5613-M-3022-6 Valve Name:	86 38 ED	SR IG Maiı	C n Lube	e Oil P	RV ump Dis	SA sch Reli	A ef Valve	C	O/C	RT	Y10			
4-70-530A	5614-M-3022-1	D2	SR	С	1.5	СК	SA	A	SYS	c	CC	М3			
	Valve Name:	4A ED)G Air F	Receiv	/er Tar	nks A &	B Inlet (Check Va	lves		со	OP			TPv-01
4-70-530B	5614-M-3022-2	D2	SR	С	1.5	СК	SA	A	SYS	С	сс	М3			-
	Valve Name:	4B ED)G Air I	Receiv	/er Tar	nks A &	B Inlet (Check Va	lves		со	OP			TPv-01
4-70-531A	5614-M-3022-1	D3	SR	С	1.5	СК	SA	A	SYS	С	сс	M3			
	Valve Name:	4A ED)G Air I	Receiv	ver Tar	nks C &	D Inlet (Check Va	lves		со	OP			TPv-01
4-70-531B	5614-M-3022-2	D3	SR	C	1.5	СК	SA	A	SYS	С	CC	МЗ		<u> </u>	
	Valve Name:	4B ED)G Air I	Receiv	ver Tar	nks C &	D Inlet (Check Va	lves		CO	OP			TPv-01
RV-4-1451A	5614-M-3022-5 Valve Name:	E4 4A ED	SR I G Co o	C ling W	1.0 Vater E	RV Expansio	SA on Tank	A Relief Va	C alve	O/C	RT	Y10			
RV-4-1451B	5614-M-3022-5	E4	SR	С	1.0	RV	SA	A	С	O/C	RT	Y10			
	Valve Name:	4A ED	G Coo	ling V	Vater E	Expansion	on Tank	Relief Va	alve						
RV-4-1452A	5614-M-3022-5 Valve Name:	B5 4A ED	SR OG Main	C n Lube	e Oil P	RV ump Dis	SA sch Reli	A ef Valve	С	O/C	RT	Y10			
RV-4-1452B	5614-M-3022-6 Valve Name:	B6 4B ED	SR)G Maiı	C n Lube	e Oil P	RV ump Dis	SA sch Reli	A ef Valve	С	0/C	RT	¥10			<u> </u>
RV-4-1456A	5614-M-3022-1 Valve Name:	B2 4A ED	SR D G Air I	C Receiv	ver Tar	RV nk A Rel	SA lief Valv	A	С	O/C	RT	Y10			
RV-4-1456B	5614-M-3022-2	B2	SR	с		RV	SA	A	С	O/C	RT	Y10			

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Emergency Diesel Generator (022)

Valve Tag	P&ID	P&ID Coor.	Safety Class	Cat.	Size	Valve Type	Act. Type	Active I Passive	Normal Position	Safety Position	Test Type	Test Freq.	Relief Request	Deferred Just.	Tech. Pos.
RV-4-1457A	5614-M-3022-1	B3	SR	С		RV	SA	A	с	O/C	RT	Y10			
	Valve Name:	4A EC)G Air F	Receiv	er Tan	k B Rel	ief Valv	e							
RV-4-1457B	5614-M-3022-2	B3	SR	С		RV	SA	A	С	O/C	RT	Y10		·	*- <u></u> *-
	Valve Name:	4B E0	DG Air F	Receiv	er Tan	k B Rel	ief Valv	e							
RV-4-1458A	5614-M-3022-1	B4	SR	С		RV	SA	A	с	O/C	RT	Y10			÷
	Valve Name:	4A EC)G Air F	Receiv	rer Tan	k C Rel	ief Valv	e [.]							
RV-4-1458B	5614-M-3022-2	B4	SR	С		RV	SA	A	С	O/C	RT	Y10			
	Valve Name:	4B EI	DG Air F	Receiv	er Tar	k C Rel	ief Valv	e							
RV-4-1459A	5614-M-3022-1	B4	SR	С		RV	SA	A	С	O/C	RT	Y10		· · · · · · · · · · · · · · · · · · ·	-
	Valve Name:	4A EC)G Air F	Receiv	er Tan	k D Rel	ief Valv	e							
RV-4-1459B	5614-M-3022-2	B4	SR	С		RV	SA	A	С	O/C	RT	Y10			
	Valve Name:	4B EC)G Air F	Receiv	er Tar	k D Rel	ief Valv	е							

	Vaive Tag	P&ID	P&ID Coor.	Safety Class	Cat.	Size	Valve Type	Act. Type	Active / Passive	Normal Position	Safety Position	Test Type	Test Freq.	Relief Request	Deferred Just.	Tech. Pos.
	3-702A	5613-M-3030-1	E4	3	С	16.0	СК	SA	A	SYS	O/C	CC	М3			
		Valve Name:	ccw	Pump	3A Dis	scharg	e Check	Valve				CO	M3 ⁻			
	3-702B	5613-M-3030-1	E3	3	с	-16.0	СК	SA	A	SYS	O/C	сс	M3	-		
<i>;</i>		Valve Name:	ccw	Pump	3B Dis	scharg	e Check	Valve				CO	М3			
	3-702C	5613-M-3030-1	E2	3	C	16.0	СК	SA	A	SYS	O/C	СС	M3			
		Valve Name:	ccw	Pump	3C Dis	scharg	e Check	Valve				CO	М3			
	3-721A	5613-M-3030-5	E6	3	С		СК	SA	A	SYS	с	сс	RR		RJ-13	
		Valve Name:	ccw	Supply	r to Th	ermal	Barrier	Cooler	Valve			CO	М3			TPv-01
	3-721B	5613-M-3030-5	B6	3	С	1.5	СК	SA	A	SYS	с	сс	RR		RJ-13	
		Valve Name:	ccw	Supply	to Th	ermal	Barrier	Cooler	Valve			CO	М3			TPv-01
	3-721C	5613-M-3030-5	Ç6	3	С	1.5	СК	SA	A	SYS	с	сс	RR		RJ-13	
		Valve Name:	ccw	Supply	r to Th	ermal	Barrier	Cooler	Valve			CO	M3			TPv-01
	3-738	5613-M-3030-5	D3	2	С	3.0	СК	SA	A	SYS	С	сс	CS		CSJ-09	
		Valve Name:	ccw	Check	Valve	to Exc	cess Let	down H	leat Exch	anger		CO	М3			TPv-01
)	CV-3-2903	5613-M-3030-4 Valve Name:	D3 3B Er	2 nergen	B Icy Co	10.0 ntainm	BTF nent Cod	AO oler Inle	P	0	0	PIT	Y2	<u> </u>		
	CV-3-2904	5613-M-3030-4	C3	2	В	10.0	BTF	AO	Ρ	0	0	PIT	Y2			
		Valve Name:	3C Er	nergen	cy Co	ntainn	nent Coo	oler inle	et							
	CV-3-2905	5613-M-3030-4	B3	2	В	10.0	BTF	AO	P	0	0	PIT	Y2			
		Valve Name:	3A En	nergen	cy Co	ntainm	nent Coo	oler inle	t							
	CV-3-2906	5613-M-3030-4	G3	2	В	10.0	BTF	AO	A	C	0	BTO	М3			
,												FO PIT	M3 Y2			TPv-04
-		Valve Name:	3B En	nergen	cy Co	ntainn	nent Cod	oler Out	let			• • •	16			

Component Cooling Water (030)

Revision Date: 2/11/2004

	Valve Tag	P&ID	P&ID Coor.	Safety Class	Cat.	Size	Valve Type	Act. Type	Active / Passive	Normal Position	Safety Position	Test Type	Test Freq.	Relief Request	Deferred Just.	Tech. Pos.
	CV-3-2907	5613-M-3030-4	F3	2	В	10.0	BTF	AO	A	С	0	BTO	М3			
												FO	М3			TPv-04
		Valve Name:	3C Er	nergen	cy Co	ntainm	ent Coo	oler Out	let			PIT	Y2			
	CV-3-2908	5613-M-3030-4	E3	2	B	10.0	BTF	AO	A	C	0	BTO	M3			
/												FO	МЗ			TPv-04
												PIT	Y2			
		Valve Name:	3A Er	nergen	cy Co	ntainm	ent Coo	ler Out	let							
	CV-3-739	5613-M-3030-5	C2	2	В	3.0	GL	AO	A	0	С	BTC	M3			
												FC	МЗ			TPv-04
												PIT	Y2			
		Valve Name:	Exces	ss Letd	own H	leat Ex	change	r Outlei	t							
	MOV-3-1417	5613-M-3030-5	B2	2	B	10.0	GA	МО	A	0	С	BTC	CS		CSJ-10	
												PIT	Y2			
		Valve Name:	ccw	to Norr	nal Co	ontainr	nent Co	oler								
	MOV-3-1418	5613-M-3030-5	F2	2	В	10.0	GA	мо	A	0	С	BTC	CS		CSJ-10	
												PIT	Y2			
		Valve Name:	ccw	to Norr	nal Co	ontainr	nent Co	oler								
	MOV-3-626	5613-M-3030-5	H3	2	в	3.0	GA	МО	A	0	С	BTC	CS		CSJ-11	
												PIT	Y2			
		Valve Name:	RCP	Seal Co	oling	Water	Outlet									
	MOV-3-716A		E2	3	в	6.0	GA	MO	A	0	С	BTC	CS		CSJ-11	
,												PIT	Y2			
		Valve Name:	RCP	CCW In	let							·				
	MOV-3-716B	5613-M-3030-5	E2	2	В	6.0	GA	МО	A	0	C ·	BTC	CS		CSJ-11	
												PIT	Y2			
		Valve Name:	RCP	CCW In	let											
	MOV-3-730	5613-M-3030-5	G3	2	В	6.0	GA	МО	A	0	С	BTC	CS		CSJ-11	
												Pit	Y2			
		Valve Name:	RCP	Bearing	I CCW	/ Outle	t									

Component Cooling Water (030)

	Valve Tag	P&ID	P&ID Coor.	Safety Class	Cat.	Size	Valve Type	Act. Type	Active I Passive	Normal Position	Safety Position	Test Type	Test Freq.	Relief Request	Deferred Just.	Tech. Pos.
	MOV-3-749A	5613-M-3030-2	F7	3	В	16.0	GA	мо	A	С	0	BTO	M3			TPv-09
		Valve Name:	3A RH	IR Hea	t Excl	nanger	Сотро	nent Co	oling Ou	tlet		pit	Y2			
	MOV-3-749B	5613-M-3030-2	F7	3	В	16.0	GA	МО	A	С	0	BTO PIT	M3 Y2			TPv-09
/		Valve Name:	3B RH	IR Hea	t Excl	nanger	Compo	nent Co	ooling Ou	tlet						
	RV-3-1423	5613-M-3030-4 Valve Name:	D5 ECC I	3 Relief \	C /alve	0.75	RV	SA	A	С	0/C	RT	Y10			
	RV-3-1424	5613-M-3030-4 Valve Name:	C5 ECC I	3 Relief \	C /alve	0.75	RV	SA	A	С	O/C	RT	Y10			
	RV-3-1425	5613-M-3030-4 Valve Name:	B5 ECC I	3 Relief V	C /alve	0.75	RV	SA	A	С	0/C	RT	Y10			
/	RV-3-1426	5613-M-3030-5 Valve Name:	E4 NCC	3 Therma	C al Reli	0.75 ef Valv	RV re	SA	A	с	0/C	RT	Y10	<u>-</u>		
	RV-3-1427	5613-M-3030-5 Valve Name:	E4 NCC	3 Therma	C al Reli	0.75 ef Valv	RV re	SA	A	С	0/C	RT	Y10			
	RV-3-1428	5613-M-3030-5 Vaive Name:	C4 NCC	3 Therma	C al Reli	0.75 ef Valv	RV /e	SA	A	C	0/C	RT	Y10		······	
	RV-3-1429	5613-M-3030-5 Valve Name:	A4 NCC	3 Therma	C al Reli	0.75 ef Valv	RV	SA	A	С	O/C	RT	Y10			
	RV-3-1430	5613-M-3030-5 Valve Name:	D4 Rod D	3 Drive C	C ooler	0.75 Therm	RV al Relief	SA I Valve	A	с	0/C	RT	Y10			
	RV-3-1431	5613-M-3030-5 Valve Name:	B4 Rod D	3 Drive C	C ooler	0.75 Therm	RV al Relief	SA Valve	A	C	O/C	RT	Y10	- -		<u> </u>
	RV-3-707	5613-M-3030-1 Valve Name:	C7 Surge	3. e Tank	C Relief	3.0 Valve	RV	SA	A	С	O/C	RT	Y10			
,	RV-3-715	5613-M-3030-5 Valve Name:	C3 Exces	3 ss Letd	C own H	3.0 leat Ex	RV	SA er Relief	A Valve	С	0/C	RT	Y10			

Component Cooling Water (030)

Component Cooling Water (030)

Valve Tag	P&ID	P&ID Coor.	Safety Class	Cat.	Size	Valve Type	Act. Type	Active / Passive	Normal Position	Safety Position	Test Type	Test Freq.	Relief Request	Deferred Just.	Tech. Pos.	
RV-3-722A	5613-M-3030-5 Valve Name:	E7 RCP T	3 herma	C I Barr	0.75 ier Co	RV oler The	SA ermal Re	A elief Valve	C	0/C	RT	Y10				
RV-3-722B	5613-M-3030-5 Valve Name:	B7 RCP T	3 herma	C I Barr	0.75 ier Co	RV oler The	SA rmal Re	A elief Valve	C	O/C	RT	Y10				
RV-3-722C	5613-M-3030-5	C7	3	С	0.75	RV	SA	A	С	O/C	RT	Y10		_		
	Valve Name:	RCP T	herma	l Barr	ier Co	oler The	ermal Re	elief Valvo	e 							
RV-3-729	5613-M-3030-5 Valve Name:	F7 RCP C	3 Dil Coo	C Iers R	3.0 Relief V	RV /alve	SA	A	С	O/C	RT	Y10				
RV-3-747A	5613-M-3030-2 Valve Name:	E7 RHR H	3 Ix The	C rmal F	1.0 Relief V	RV /alve	SA	A	С	O/C	RT	Y10				
RV-3-747B	5613-M-3030-2 Valve Name:	E8 RHR H	3 Ix The	C rmal F	1.0 Relief \	RV /aive	SA	A	С	O/C	RT	Y10				
4-702A	5614-M-3030-1	E4	3	С	16.0	СК	SA	A	SYS	0/C	СС	мз				
	Valve Name:	ccwi	Pump	4A Dis	scharg	e Checł	Valve				со	М3				
4-702B	5614-M-3030-1	E3	3	C	16.0	СК	SA	A	SYS	O/C	сс	M3				
	Valve Name:	ccwi	Pump	4B Dis	scharg	e Checl	Valve				CO	М3				
4-702C	5614-M-3030-1	E2	3	С	16.0	СК	SA	A	SYS	O/C	сс	M3	<u> </u>	<u> </u>		
	Valve Name:	CCW Pump 4C Discharge Check Valve														
4-721A	5614-M-3030-4	E6	3	С	1.5	СК	SA	A	SYS	С	сс	RR		RJ-13		
	Valve Name:	ccws	Supply	to Th	iermal	Barrier	Cooler	Valve			CO	М3			TPv-01	
4-721B	5614-M-3030-4	B6	3	C	1.5	СК	SA	A	SYS	с	сс	RR		RJ-13		
	Valve Name:	ccws	Supply	to Th	ermai	Barrier	Cooler	Valve			CO	M3			TPv-01	
4-721C	5614-M-3030-4	D6	3	С	1.5	СК	SA	A	SYS	С	CC	RR		RJ-13		
	Valve Name:	ccws	Supply	to Th	ermai	Barrier	Cooler	Valve			CO	M3			IPv-01	

Revision Date: 2/11/2004

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P&ID Safety Valve Act. Active I Normal Safety Test Test Relief Deferred Tech. Position Position Coor. Class Cat. Freq. Size Request Just. Type Type Passive Type Pos. Valve Tag P&ID 4-738 5614-M-3030-4 D3 2 С 3.0 СК SA A SYS С CC CS CSJ-09 CO M3 TPv-01 Valve Name: CCW Check Valve to Excess Letdown Heat Exchanger 0 CV-4-2903 5614-M-3030-3 D3 2 В 10.0 BTF AO Ρ 0 ΡΠ Y2 Valve Name: **4B Emergency Containment Cooler Inlet** CV-4-2904 5614-M-3030-3 C3 2 В 10.0 BTF AO Ρ 0 0 PIT Y2 Valve Name: **4A Emergency Containment Cooler Inlet** CV-4-2905 5614-M-3030-3 B3 2 В 10.0 BTF AO Ρ 0 0 PIT Y2 Valve Name: 4C Emergency Containment Cooler Inlet CV-4-2906 5614-M-3030-3 G3 A С 0 BTO 2 В 10.0 BTF AO M3 М3 FO TPv-04 PIT Y2 Valve Name: **4B Emergency Containment Cooler Outlet** CV-4-2907 5614-M-3030-3 F3 2 В 10.0 BTF AO Α С 0 BTO M3 FO M3 TPv-04 PIT Y2 Valve Name: **4A Emergency Containment Cooler Outlet** С CV-4-2908 5614-M-3030-3 E3 2 В 10.0 BTF AO A 0 BTO M3 FO М3 TPv-04 PIT Y2 Valve Name: **4C Emergency Containment Cooler Outlet** С CV-4-739 5614-M-3030-4 C2 0 2 В 3.0 GL AO A BTC MЗ FC M3 TPv-04 PIT Y2 Valve Name: **Excess Letdown Heat Exchanger Outlet** MOV-4-1417 5614-M-3030-4 **B**2 2 В 10.0 GA A 0 С CS **CSJ-10** MO BTC Y2 PIT Valve Name: **CCW to Normal Containment Cooler** MOV-4-1418 5614-M-3030-4 F2 0 С CS CSJ-10 2 В 10.0 GA MO A BTC PIT Y2 Valve Name: **CCW to Normal Containment Cooler**

Component Cooling Water (030)

Revision Date: 2/11/2004

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	Valve Tag	P&ID	P&ID Coor.	Safety Class	Cat.	Size	Valve Type	Act. Type	Active / Passive	Normal Position	Safety Position	Test Type	Test Freq.	Relief Request	Deferred Just.	Tech. Pos.	
	MOV-4-626	5614-M-3030-4	H3	2	В	3.0	GA	МО	A	0	С	BTC PIT	CS Y2		CSJ-11		
		Valve Name:	RCP Seal Cooling Water Outlet														
	MOV-4-716A	5614-M-3030-4	E2	3	B	6.0	GA	мо	A	0	С	BTC	CS V2		CSJ-11		
)		Valve Name:	RCP (CCW In	let							F 11	12				
	MOV-4-716B	5614-M-3030-4	E2	2	В	6.0	GA	МО	A	0	С	BTC	CS V2		CSJ-11	_	
		Valve Name:															
	MOV-4-730	5614-M-3030-4	G3	2	В	6.0	GA	МО	A	0	С	BTC	CS Y2		CSJ-11		
		Valve Name:	RCP Bearing CCW Outlet														
J	MOV-4-749A	5614-M-3030-2	F6	3	В	16.0	GA	МО	A	С	0	BTO PIT	M3 Y2			TPv-09	
		Valve Name:	3A RHR Heat Exchanger Component Cooling Outlet														
	MOV-4-749B	5614-M-3030-2	F7	3	В	16.0	GA	МО	A	С	0	BTO	M3			TPv-09	
		Valve Name:	3B RH	IR Hea	t Excl	nanger	Compo	nent Co	ooling Ou	tlet		FII	12				
	RV-4-1423	5614-M-3030-3 Valve Name:	D5 ECC I	3 Relief V	C /alve	0.75	RV	SA	A	с	0/C	RT	Y10				
)	RV-4-1424	5614-M-3030-3 Valve Name:	C5 ECC I	3 Relief V	C /alve	0.75	RV	SA	A	c	0/C	RT	Y10				
	RV-4-1425	5614-M-3030-3 Valve Name:	B5 ECC I	3 Relief V	C /alve	0.75	RV	SA	A	С	0/C	RT	¥10				
	RV-4-1426	5614-M-3030-4 Valve Name:	E4 NCC	3 Therma	C al Reli	0.75 ef Valv	RV	SA	A	c	0/C	RT	Y10				
	RV-4-1427	5614-M-3030-4 Valve Name:	D4 NCC	3 Therma	C I Reli	0.75 ef Valv	RV	SA	A	c	O/C	RT	Y10				
)	RV-4-1428	5614-M-3030-4 Valve Name:	B4 NCC	3 Therma	C al Reli	0.75 ef Valv	RV	SA	A	c	O/C	RT	Y10				

Component Cooling Water (030)

Revision Date: 2/11/2004

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Component Cooling Water (030)

Valve Tag	P&ID	P&ID Coor.	Safety Class	Cat.	Size	Valve Type	Act. Type	Active / Passive	Normal Position	Safety Position	Test Type	Test Freq.	Relief Request	Deferred Just.	Tech. Pos.						
Valve Tag RV-4-1429 RV-4-1430 RV-4-1431 RV-4-707 RV-4-707 RV-4-715 RV-4-722A RV-4-722B RV-4-722B	5614-M-3030-4	A4	3	C	0.75	RV	SA	A	С	O/C	RT	Y10									
	valve Name.	NCC		a Read		e															
RV-4-1430	5614-M-3030-4	D4	3	С	0.75	RV	SA	A	С	O/C	RT	Y10									
	Valve Name:	Rod D	rive Co	ooler '	Therma	al Relief	Valve														
Valve Tag RV-4-1429 RV-4-1430 RV-4-1431 RV-4-707 RV-4-707 RV-4-715 RV-4-722A RV-4-722B RV-4-722P RV-4-729 RV-4-747A	5614-M-3030-4	C4	3	С	0.75	RV	SA	A	С	O/C	RT	Y10									
	Valve Name:	Rod D)rive Co																		
RV-4-707	5614-M-3030-1	C7	3	С	3.0	RV	SA	A	С	0/C	RT	Y10									
	Valve Name:	Surge	Tank I	Relief	Valve								Relief Deferred Tech. 110 110 110 110 110 110 110 110 110 110 110 110 110 110 110 110 110 110 110 110 110 110 110 110 110 110 110 110 110 110								
RV-4-715	5614-M-3030-4	C3	3	с	3.0	RV	SA	A	С	O/C	RT	Y10									
	Valve Name:	Exces	s Letd	own H	leat Ex	change	r Relief	Valve													
RV-4-722A	5614-M-3030-4	E7	3	Ċ	Ó.75	RV	SA	A	с	O/C	RT	Y10			_						
	Valve Name:	RCP	ſherma	l Barr	ier Co	oler The	ermai Ro	elief Valv	Ð												
RV-4-722B	5614-M-3030-4	B7	3	с	0.75	RV	SA	A	С	0/C	RT	Y10									
	Valve Name:	RCP 1	Therma	l Barr	ier Co	oler The	rmal R	elief Valv	Ð												
RV-4-722C	5614-M-3030-4	C7	3	С	0.75	RV	SA	A	С	O/C	RT	Y10									
	Valve Name:	RCP	Therma	l Barr	ier Co	oler The	rmal R	elief Valv	Ð												
RV-4-729	5614-M-3030-4	F7	3	с	3.0	RV	SA	A	c	0/C	RT	Y10									
	Valve Name:	RCP (Dil Coo	iers R	elief V	alve															
RV-4-747A	5614-M-3030-2	E 6	3	С	1.0	RV	SA	A	С	0/C	RT	Y10									
	Valve Name:	4 B7 3 C 0.75 RV SA A C O/C RT Y10 RCP Thermal Barrier Cooler Thermal Relief Valve A C O/C RT Y10 4 C7 3 C 0.75 RV SA A C O/C RT Y10 4 C7 3 C 0.75 RV SA A C O/C RT Y10 RCP Thermal Barrier Cooler Thermal Relief Valve Relief Valve C O/C RT Y10 4 F7 3 C 3.0 RV SA A C O/C RT Y10 RCP Oil Coolers Relief Valve 2 E6 3 C 1.0 RV SA A C O/C RT Y10 RHR Hx Thermal Relief Valve Relief Valve SA A C O/C RT Y10																			
RV-4-747B	5614-M-3030-2	E8	3	С	1.0	RV	SA	A	с	O/C	RT	Y10									
	Valve Name:	RHR I	Hx The	rmal F	Relief V	/alve															
\bigcirc							Samp	ling ((036)					Turkey IST Pro Valve 1	Point Nucl ogram Plan Fable	ear Plant					
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	Valve Tag	P&ID	P&ID Coor.	Safety Class	Cat.	Size	Valve Type	Act. Type	Active / Passive	Normal Position	Safety Position	Test Type	Test Freq.	Relief Request	Deferred Just.	Tech. Pos.					
	CV-3-951	5613-M-3036-1	A2	2	A	0.375	GL	OA	A	c	С	AT-01	App-J								
												BTC	М3								
												FC	M3			TPv-04					
		Valve Name:	Press	surizer	Stean	n Space	e Sampl	e Isolat	ion Valve	•		РП	¥2								
\bigcirc	CV-3-953	5613-M-3036-1	B2	2	A	0.375	GL	AO	A	С	С	AT-01	App-J		·						
												BTC	M3								
												FC	M3			TPv-04					
												PIT	Y2								
		Valve Name:	Press	urizer	Liquio	I Space	e Sampl	e Isolat	ion Valve						-						
	CV-3-955C	5613-M-3036-1	D2	2	A	0.375	GL	AO	A	C	С	AT-01	App-J								
												BTC	M3								
												FC	M3			TPv-04					
		Valve Name:	3A Ad	cumula	ator S	ample	Valve					РП	¥2								
\bigcirc																					
	CV-3-955D	5613-M-3036-1	E2	2	A	0.375	GL	AO	A	С	С	AT-01	App-J								
												FC	M3		•	TDUM					
												PIT	Y2			11 4-0-4					
		Valve Name:	3B A0	cumul	ator S	ample	Valve														
	 CV-3-955E	5613-M-3036-1		2	A	0.375	GL	AO	A	с	с	AT-01	App-J								
												BTC	M3								
												FC	M3			TPv-04					
												PIT	Y2								
\bigcirc		Valve Name:	3C Ad	cumul	ator S	ample	Valve														
	CV-3-956A	5613-M-3036-1	A3	2	A	0.375	GL	AO	A	c	С	AT-01	Арр-Ј								
												BTC	M3								
												FC	M3			TPv-04					
			_	-			•					PIT	Y2								
		Valve Name:	Press	urizer	Stean	n Space	e Sampl	e Isolat	ion Valve	•											

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\bigcirc							Samp	ling (l)36)					Turkey IST Pro Valve T	Point Nucl ogram Plan Table	ear Plant
	Valve Tag	P&ID	P&ID Coor.	Safety Class	Cat.	Size	Valve Type	Act. Type	Active / Passive	Normal Position	Safety Position	Test Type	Test Freq.	Relief Request	Deferred Just.	Tech. Pos.
	CV-3-956B	5613-M-3036-1	B3	2	A	0.375	GL	AO	A	С	С	AT-01	App-J			
												BTC	M3			
												FC	M3			TPv-04
		Valve Name:	Press	urizer l	Liquic	l Space	e Sampi	e Isolat	ion Valve	1		PIT	Y2			
\cup		5613-M-3036-1	F3	2		0.375	GI	AO	A	C	<u>с</u>	AT-01				
	•••••			-		0.010	01			•	•	BTC	M3			
												FC	M3			TPv-04
												PIT	Y2			
		Valve Name:	Accu	mulator	r Sam	ple Iso	lation V	alve								
	RV-3-300	5613-M-3036-1	B3	2	A/C	0.375	RV	SA	A	c	O/C	AT-01	App-J			
												RT	Y10			
		Valve Name:	Press	urizer l	Liquic	I Space	e Sampi	e Line I	Relief Val	ve						
• ,	RV-3-301	5613-M-3036-1	D3	2	A/C	0.75	RV	SA	A	С	O/C	AT-01	App-J			
\bigcirc				• •								RT	Y10			
		valve Name:	Accu	mulato	r Sam		e Relief	Valve								_
	SV-3-6427A	5613-M-3036-1	C2	2	A	0.375	GL	SO	A	C	С	AT-01	App-J			
												BTC	M3			
												FC	M3			TPv-04
												PIT	App-J	VR-02		
		Valve Name:	RCS	Loop A	Hot L	.eg Sar	nple Isc	lation \	/alve							
	SV-3-6427B	5613-M-3036-1	C2	2	. A	0.375	GL	SO	A	C	С	AT-01	App-J			
												BTC	M3			
\bigcirc												FC	M3			TPv-04
						-						PIT	App-J	VR-02		
	·	Valve Name:	RCS	Loop B	Hot L	.eg Sar	npie Isc	lation \	/alve							
	SV-3-6428	5613-M-3036-1	C3	2	A	0.375	GL	SO	Α	С	C	AT-01	Арр-Ј			
												BTC	М3			
												FC	M3			TPv-04
												PIT	App-J	VR-02		
		Valve Name:	RCS	Hot Leg	y Sam	pie iso	lation V	aive								

						Samp	ling (()36)					Turkey IST Pro Valve T	Point Nucl ogram Plan Table	ear Plant
Vaive Tag	P&ID	P&ID Coor.	Safety Class	Cat.	Size	Valve Type	Act. Type	Active / Passive	Normal Position	Safety Position	Test Type	Test Freq.	Relief Request	Deferred Just.	Tech. Pos.
CV-4-951	5614-M-3036-1	A2	2	A	0.375	GL	OA	A	C	С	AT-01 BTC FC	App-J M3 M3			TPv-04
	Valve Name:	Press	urizer (Steam	n Space	e Sampl	e Isolat	ion Valve			PIT	Y2			
CV-4-953	5614-M-3036-1	B2	2	A	0.375	GL	AO	A	C	С	AT-01 BTC FC PIT	App-J M3 M3 Y2			TPv-04
	Valve Name:	Press	urizer l	Liquic	l Space	e Sampl	e Isolat	ion Valve							
CV-4-955C	5614-M-3037-1	D2	2	A	0.375	GL	OA	A	С	С	AT-01 BTC FC PIT	App-J M3 M3 Y2			TPv-04
	Valve Name:	4A Ac	cumula	ator S	ample	Valve									
CV-4-955D	5614-M-3036-1 Valve Name:	E2	2	A ator S	0.375	GL	AO	A	C	С	AT-01 BTC FC PIT	App-J M3 M3 Y2			TPv-04
CV-4-955E	5614-M-3036-1	E2	2	A	0.375	GL	AO	A	c	с	AT-01 BTC FC	App-J M3 M3	<u> </u>		TPv-04
	Valve Name:	4C Ac	cumula	ator S	ample	Valve					PIT	Y2			
CV-4-956A	5614-M-3036-1	A3	2	A	0.375	GL	AO	A	C	С	AT-01 BTC FC PIT	App-J M3 M3 Y2			TPv-04

\bigcirc					-		Samp	oling ((036)					Turkey IST Pro Valve 7	Point Nucl ogram Plan Table	ear Plant
	Valve Tag	P&ID	P&ID Coor.	Safety Class	Cat.	Size	Valve Type	Act. Type	Active / Passive	Normal Position	Safety Position	Test Type	Test Freq.	Relief Request	Deferred Just.	Tech. Pos.
	CV-4-956B	5614-M-3036-1	B3	2	A	0.375	GL	OA	A	С	. C	AT-01	App-J			
												BTC	M3			
												FC	M3			TPv-04
			_									PIT	Y2			
		Valve Name:	Press	urizer	Liquid	Space	e Sampl	e Isolat	ion Valve	! 	<u>.</u> _	_				
\bigcirc	CV-4-956D	5614-M-3036-1	E3	2	A	0.375	GL	AO	A	c	c	AT-01	App-J			
									•			BTC	M3			
												FC	M3			TPv-04
	•											PIT	Y2			
		Valve Name:	Accu	mulato	r Sam	ple Iso	lation V	alve								
		5614 14 2026 1			NC	0.375			·		0/0	AT 01	App. 1			
	KV-4-300	30 14-M-3030- I	DJ	2	NG	0.375	ΠV	94	×	C	U/C		NPP-0			
		Valve Name:	Press	urizer l	Liquio	l Space	e Sampl	e Line F	Relief Val	ve		NI	110			
	RV-4-301	5614-M-3036-1	D3	2	A/C	0.75	RV	SA	A	С	O/C	AT-01	App-J			
\bigcirc												RT	Y10			
		Valve Name:	Accu	mulato	r Sam	ple Lin	e Relief	Valve								
	SV-4-6427A	5614-M-3036-1	C2	2	A	0.375	GL	so	A	С	С	AT-01	App-J			
												BTC	М3			
												FC	M3			TPv-04
												PIT	App-J	VR-02		
		Valve Name:	RCS	Loop A	Hot L	.eg Sar	nple Isc	lation V	/alve							
	SV-4-6427B	5614-M-3036-1	C2	2	A	0.375	GL	so	A	с	С	AT-01	App-J			
												BTC	M3			
$\langle \rangle$												FC	M3			TPv-04
\smile												PIT	App-J	VR-02		
		Valve Name:	RCS	Loop B	Hot L	.eg Sar	npie isc	lation \	/alve							
	SV-4-6428	5614-M-3036-1	C3	2	A	0.375	GL	SO	A	С	с	AT-01	App-J			
												BTC	M3			
												FC	мз			TPv-04
												PIT	App-J	VR-02		
		Valve Name:	RCS	Hot Leg	g Sam	ple Iso	lation V	alve								

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					R	eacto	r Cool	lant Sy	ystem (041)				Turkey IST Pro Valve T	Point Nucl ogram Plan Table	ear Plant
Va	live Tag	P&ID	P&ID Coor.	Safety Class	Cat.	Size	Valve Type	Act. Type	Active / Passive	Normal Position	Safety Position	Test Type	Test Freq.	Relief Request	Deferred Just.	Tech. Pos.
CV	/-3-516	5613-M-3041-2	G2	2	A	0.375	GL	AO	A	С	С	AT-01	App-J			
												BTC	M3			
												FC	M3			TPv-04
		Valve Name:	Cont	lso Viv	PRT t	o GA						Pii	.12			
C/	/-3-519A	5613-M-3041-3	A8	2	A	3.00	DIA	AO	A	c	С	AT-01	App-J	<u> </u>		
												BTC	M3			
												FC	M3			TPv-04
		Valve Name:	PWS	upply t	o Con	tainme	ent					PIT	Y2	-		
C١	V-3-519B	5613-M-3041-3	A2	2	A	3.00	DIA	AO	A	С	С	AT-01	App-J			
												BIC	MD			
												PIT	Y2			1114-04
		Valve Name:	PRT I	Makeup	Valve	•										
c١		5613-M-3041-3	B7	2	A	0.75	DIA	AO	A	c	С	AT-01	App-J			
												BTC	М3			
							•					FC	M3			TPv-04
		Valve Name:	3A RO	CP Stan	ld Pip	e Fill						PIT	¥2			
C\	/-3-522B	5613-M-3041-3	B7	2	A	0.75	DIA	AO	A	С	с	AT-01	App-J			
												BTC	M3			
												FC	M3			TPv-04
												PIT	Y2			
-		Valve Name:	3B R(CP Stan	id Pip	e Fill										
C١	V-3-522C	5613-M-3041-3	C7	2	A	0.75	DIA	AO	A	С	С	AT-01	App-J			
												BIC	MD			
												PIT	ΝΟ Y2			179-04
		Valve Name:	3C R(CP Star	nd Pip	e Fill							12			
M	OV-3-535	5613-M-3041-2	B6	1	В	3.00	GA	MO	A	0	O/C	BTC	M3			TPv-09
												PIT	Y2			
		Valve Name:	Press	urizer l	PORV	Stop \	/aive									

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P&ID Safety Valve Act. Active / Normal Safety Test Test Relief Deferred Tech. Coor. Class Cat. Size Passive Position Position Freq. Type Type Туре Request Just. Pos. P&ID Valve Tag 5613-M-3041-2 3.00 MO A 0 O/C M3 MOV-3-536 **C**6 В GA BTC TPv-09 1 PIT Y2 Valve Name: Pressurizer PORV Stop Valve PCV-3-455C 5613-M-3041-2 C7 1 В 3.00 GL AO A С O/C BTC CS CSJ-23 CSJ-23 BTO CS FC CS CSJ-23 TPv-04 Y2 PIT Valve Name: **Pressurizer PORV** С O/C PCV-3-456 5613-M-3041-2 B7 В 3.00 GL AO Α BTC CS CSJ-23 1 CSJ-23 BTO CS FC CS CSJ-23 TPv-04 PIT Y2 Valve Name: Pressurizer PORV RV-3-551A 5613-M-3041-2 B5 1 С 4.00 RV SA A С O/C RT Y5 Valve Name: **Pressurizer Safety Valve A** С RV-3-551B 5613-M-3041-2 B4 1 С 4.00 RV SA A O/C RT Y5 Valve Name: **Pressurizer Safety Valve B** С RV-3-551C 5613-M-3041-2 A O/C **B**3 1 С 4.00 RV SA RT Y5 Pressurizer Safety Valve C Valve Name: RV-3-6587 5613-M-3041-4 SA A С O/C Y10 C4 SR С 0.50 RV RT Valve Name: N2 Supply Relief С RV-3-6588 5613-M-3041-4 F4 SR С 0.50 RV SA A O/C RT Y10 Valve Name: N2 Supply Relief 1.00 GA С O/C CS CSJ-24 SV-3-6318A 5613-M-3041-2 D7 2 В SO A BTO TPv-09 PIT Y2 Valve Name: **Reactor Vessel Head Vent** SV-3-6318B 5613-M-3041-2 E7 2 В 1.00 GA SO A С O/C BTO CS CSJ-24 TPv-09 PIT Y2 Valve Name: **Reactor Vessel Head Vent**

Reactor Coolant System (041)

	Valve Tag	P&ID	P&ID Coor.	Safety Class	Cat.	Size	Valve Type	Act. Type	Active / Passive	Normal Position	Safety Position	Test Type	Test Freq.	Relief Request	Deferred Just.	Tech. Pos.
	SV-3-6385	5613-M-3041-2	G2	2	A	0.375	GA	so	A	с	с	AT-01	Арр-Ј			
												BTC	М3			
												FC	M3			TPv-04
		Valve Name:	PRT t	o Gas /	Analy:	zer						PIT	App-J	VR-02		
	<u> </u>														00104	
\smile	50-3-0011	5013-M-3041-2	F/	2	В	1.00	GA	50	A	L.	0	FO	CS CS		CSL24	1PV-09 TPv_04
												PIT	Y2		000-24	11 1-1-1
		Valve Name:	RCS	Vent to	Atmo	sphere)									
	SV-3-6612	5613-M-3041-2	F6	2	В	1.00	DAM	so	A	С	0	BTO	CS	<u> </u>	CSJ-24	TPv-09
												FO	CS		CSJ-24	TPv-04
												PIT	Y2			
		Valve Name:	Vent	to PRT			_									
	CV-4-516	5614-M-3041-2	G2	2	A	0.375	GL	AO	A	С	С	AT-01	App-J			
\bigcirc												BTC	М3			
												FC	M3			TPv-04
		Valve Name:	Cont	lso Viv	PRT	to Gar						PIT	Y2			
	CV-4-519A				A	3.00	DIA			 C		AT-01	Appal			
			710	-	~	0.00	0	7.0		Ŭ	Ŭ	BTC	M3			
												FC				TPv-04
												PIT	Y2			
		Valve Name:	PWS	upply t	o Cor	tainme	ent									
	CV-4-519B	5614-M-3041-3	A2	2	A	3.00	DIA	AO	A	C	С	AT-01	App-J			
÷												BTC	М3			
												FC	M3			TPv-04
												PIT	Y2			
		Valve Name:	PRT	Makeup	Valv	e 						•				
	CV-4-522A	5614-M-3041-3	87	2	A	0.75	DIA	AO	A	С	C	AT-01	Арр-Ј			
												BTC	M3			
												FC	M3			TPv-04
\		Valve Name	44 20	CP Star	nd Pin	e Fill					·	PIT	Y2			
\smile		Turto Humor			- a i i ip	• • • •										

Reactor Coolant System (041)

				R	eacto	r Coo	lant Sy	ystem (041)				Turkey IST Pro Valve T	Point Nuc ogram Plar Fable	lear Plant I
Valve Tag	P&ID	P&ID Coor.	Safety Class	Cat.	Size	Vaive Type	Act. Type	Active / Passive	Normal Position	Safety Position	Test Type	Test Freq.	Relief Request	Deferred Just.	Tech. Pos.
CV-4-522B	5614-M-3041-3	87	2	A	0.75	DIA	AO	A	с	С	AT-01	App-J			
											BTC	M3			
											FC	M3			TPv-04
	Valve Name:	4B R0	CP Star	nd Pip	e Fill						PIT	Y2			
CV-4-522C		C7	2	A	0.75	DIA	 AO		с	с	AT-01	App-J			
			-						-		BTC	M3			
											FC	M3			TPv-04
						•					PIT	Y2			
	Valve Name:	4C R(CP Star	nd Pip	e Fill										
MOV-4-535	5614-M-3041-2	B6	1	В	3.00	GA	мо	A	0	O/C	BTC	M3			TPv-09
											PIT	Y2			
	Valve Name:	Press	urizer	PORV	Stop \	/aive									
MOV-4-536	5613-M-3041-2	C6	. 1	B	3.00	GA	мо	A	0	O/C	BTC	М3			TPv-09
	Vaive Name:	Press	urizer	PORV	Stop \	/alve					PIT	Y2			
PCV-4-455C	5614-M-3041-2	C7	1	В	3.00	GL	AO	Α	С	0/C	BTC	CS		CSJ-23	
											BTO	CS		CSJ-23	
											FC	CS		CSJ-23	TPv-04
											PIT	Y2			
	Valve Name:	Press	urizer i	PORV	,										
PCV-4-456	5614-M-3041-2	B7	1	ъВ	3.00	GL	AO	Α	С	O/C	BTC	CS		CSJ-23	
											BTO	CS		CSJ-23	
						•					FC	CS		CSJ-23	TPv-04
	Valve Name:	Press	urizer	PORV	,						PIT	Y2			
	5614.M 3041.2				4.00	DV					DT				
NV-4-331N	Valve Name	Droce	ı urizor '	U Səfatı	v Valvo	A	54	~	U	00	NI	15			
		F1033				^									-
RV-4-551B	5614-M-3041-2	B4	1.	С	4.00	RV	SA	A	С	O/C	RT	Y5			
	Valve Name:	Press	surizer	Safety	/ Valve	В						_			
RV-4-551C	5614-M-3041-2	B3	1	C	4.00	RV	SA	A	С	O/C	RT	Y5			

P&ID Safety Valve Act. Active / Normal Safety Test Test Relief Deferred Tech. Coor. Class Cat. Size Type Type Passive Position Position Type Freq. Request Just. Pos. P&ID Valve Tag С RV-4-6587 5614-M-3041-4 C4 SR С 0.50 RV SA A O/C RT Y10 Valve Name: N2 Supply Relief С RV-4-6588 5614-M-3041-4 F4 SR С 0.50 RV SA A O/C RT Y10 Valve Name: N2 Supply Relief SV-4-6318A 5614-M-3041-2 D7 2 B 1.00 GA SO A С O/C BTO CS CSJ-24 TPv-09 PIT Y2 Valve Name: **Reactor Vessel Head Vent** С 0/C CSJ-24 SV-4-6318B GA SO A BTO CS TPv-09 5614-M-3041-2 E7 2 В 1.00 PIT Y2 Valve Name: **Reactor Vessel Head Vent** SV-4-6385 5614-M-3041-2 2 0.375 GA SO A С С AT-01 App-J G2 Α BTC M3 FC TPv-04 M3 PIT App-J VR-02 Valve Name: PRT to Gas Analyzer С A 0 CSJ-24 SV-4-6611 5613-M-3041-2 2 1.00 GA SO BTO CS TPv-09 F7 в FO CS CSJ-24 TPv-04 PIT Y2 Valve Name: **RCS Vent to Atmosphere** С SV-4-6612 5613-M-3041-2 2 DAM SO A 0 BTO CS CSJ-24 TPv-09 F6 В 1.00 FO CS CSJ-24 TPv-04 PIT Y2

Reactor Coolant System (041)

Valve Name:

Vent to PRT

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Boric Acid (046)

Valve Tag	P&ID	P&ID Coor.	Safety Class	Cat.	Size	Valve Type	Act. Type	Active / Passive	Normal Position	Safety Position	Test Type	Test Freq.	Relief Request	Deferred Just.	Tech. Pos.
3-397A	5610-M-3046-1	D7	2	С	2.0	СК	SA	A	SYS	O/C	сс	RR	_	RJ-04	
	Valve Name:	Boric	Acid P	ump [Discha	rge Che	ck Valv	e			CO	RR		RJ-04	
3-397B	5610-M-3046-1	E6	2	С	2.0	СК	SA	A	SYS	O/C	сс	RR		RJ-04	
	Valve Name:	Boric	Acid P	ump [Discha	rge Che	ck Valv	' e			CO	RR		RJ-04	
HCV-105	5610-M-3046-1	C5	2	В	2.0	GL	AO	A	С	С	BTC	M3			
											FC	M3			TPv-04
	Valve Name:	Boric	Acid S	torage	e Tank	Recircu	ulation (Control V	alv		_			_	
HCV-110	5610-M-3046-1	C7	2	В	2.0	GL	AO	A	С	С	BTC	M3			
											FC	M3			TPv-04
	Valve Name:	Boric	Acid S	torage	e Tank	Recircu	ulation (Control V	alv						
4-397C	5610-M-3046-1	E5	2	С	2.0	СК	SA	A	SYS	O/C	сс	RR		RJ-04	
											со	RR		RJ-04	
	Valve Name:	Boric	Acid P	ump [Discha	rge Che	ck Valv	e							
4-397D	5610-M-3046-1	F4	2	С	2.0	СК	SA	A	SYS	O/C	СС	RR		RJ-04	
											со	RR		RJ-04	
	Valve Name:	Boric	Acid P	ump [Discha	rge Che	ck Valv	e							
HCV-104	5610-M-3046-1	C4	2	в	2.0	GL	AO	A	с	С	BTC	M3		· · · ·	
											FC	М3			TPv-04
	Valve Name:	Boric	Acid S	torage	e Tank	Recircu	ulation (Control V	alv						

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Valve Tag	P&ID	P&ID Coor.	Safety Class	Cat.	Size	Vaive Type	Act. Type	Active I Passive	Normal Position	Safety Position	Test Type	Test Freq.	Relief Request	Deferred Just.	Tech. Pos.
3-298A	5613-M-3047-3	F4	1	A/C	2.0	СК	SA	A	SYS	с	AT-01	App-J			
											cc	RR	VR-01	RJ-16	TPv-08
	Valve Name:	3A RO	CP Seal	Injec	tion Cl	heck Va	lve				CO	RR	VR-01	RJ-16	TPv-01
3-298B				A/C	20	СК	SA	 A	SYS	c	AT-01				· · · ·
•			•		2.0	••••	•••		••••	•	CC	RR	VR-01	RJ-16	TPv-08
											со	RR	VR-01	RJ-16	TPv-01
	Valve Name:	3B R(CP Seal	l Injec	tion Cl	heck Va	lve								
3-298C	5613-M-3047-3	D4	1	A/C	2.0	СК	SA	A	SYS	с	AT-01	App-J			
											CC	RR	VR-01	RJ-16	TPv-08
	Value Nomer	20 D/		1-1-0-0	tion Cl	haak Va					со	RR	VR-01	RJ-16	TPv-01
,	valve Name:	30 R		пјес											
3-312A	5613-M-3047-2	C8	1	С	3.0	СК	SA	Å	SYS	0	CCF	СМ			TPv-01,02
	Valve Name:	Charg	jing Lir	ne Che	eck Va	lve					COF	СМ			TPv-02
3-312B	5613-M-3047-2	A8	1	С	3.0	СК	SA	A	SYS	0	CCF	СМ			TPv-01,02
											COF	СМ			TPv-02
	Valve Name:	Loop	C Char	ging l	Line C	heck Va	lve								
3-312C	5613-M-3047-2	E7	1	A/C	3.0	СК	SA	A	SYS	O/C	AT-01	App-J			
											СС	RR		RJ-14	TPv-08
											со	М3			
	Valve Name:	Charg	jing Lir	ne Che	eck Va	lve				-					
3-351		F1	2	С	2.0	СК	SA	A	SYS	0	CCR	СМ			TPv-01,02
	Valve Name:	Emer	gency l	Borati	on Che	eck Valv	'e				COF	СМ		RJ-15	TPv-02
3-357	5613-M-3047-2	F3	2	С	4.0	СК	SA	A	SYS	0	CCR	СМ			TPv-01,02
											COF	СМ		CSJ-22	TPv-02
	Valve Name:	Emer	gency I	Makeu	ip to C	harging	Pumps	Check V	alve						
CV-3-200A	5613-M-3047-1	A2	1	A	2.0	GL	AO	A	0	С	AT-01	App-J			
											BTC	M3			
											FC	M3			TPv-04
											PIT	Y2			
	Valve Name:	Letdo	wn Ori	tice S	top Va	Ive									

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				Cher	nical	and V	olume	e Contro	ol (047)				IST Pro Valve T	ogram Plan Table	I
Valve Tag	P&ID	P&ID Coor.	Safety Class	Cat.	Size	Valve Type	Act. Type	Active / Passive	Normal Position	Safety Position	Test Type	Test Freq.	Relief Request	Deferred Just.	Tech. Pos.
CV-3-200B	5613-M-3047-1	B2	1	A	2.0	GL	OA	A	0	с	AT-01	App-J			
											BTC	M3			
											FC	M3			TPv-04
											PIT	Y2			
	Valve Name:	Letdo	wn Ori	fice S	top Va	lve									
V-3-200C	5613-M-3047-1	C2	1	A	2.0	GL	AO	A	0	С	AT-01	App-J			
											BTC	М3			
											FC	М3			TPv-04
						•					PIT	Y2			
	Valve Name:	Letdo	wn Ori	fice S	top Va	lve									
:V-3-204	5613-M-3047-1	C4	2	A	2.0	GL	AO	A	0	С	AT-01	App-J			
											BTC	CS		CSJ-16	
											FC	CS		CSJ-16	TPv-04
											PIT	Y2			
	Valve Name:	Letdo	wn Lin	e Isola	ation V	alve									
V-3-310A	5613-M-3047-2	C7	1	в	2.0	GL	AO	A	0	0	BTO	М3			
											FO	M3			TPv-04
											PIT	Y2			
	Valve Name:	Loop	A Char	ging l	solatio	on Valve	•								
CV-3-310B	5613-M-3047-2	A7	1	В	2.0	GL	AO	A	С	0	BTO	M3			
											FO	M3			TPv-04
											PIT	Y2			
	Valve Name:	Charg	jing Lir	ne Sto	p Valv	e Loop	С								
CV-3-311	5613-M-3047-2	B7	1	B	2.0	GA	AO	 Р	c	С	PIT	Y2			
	Valve Name:	Auxili	ary Sp	ray Iso	olation	Valve					•				
CV-3-387	5613-M-3047-3	B8	1	B	0.75	GL	AO	A	с	C	BTC	M3			
											FC	M3			TPv-04
											PIT	Y2			
	Valve Name:	Exces	ss Letd	own I	solatio	n Valve									
FCV-3-113B	5613-M-3047-2	D3	2	В	2.0	PLG	AO	A	с	с	BTC	МЗ		<u> </u>	- <u></u>
											FC	M3			TPv-04
											PIT	Y2			
	Valve Name:	Blend	ier Flov	v to C	haroin	a Pump									

Turkey Point Nuclear Plant

Valve Tag	P&ID	P&ID Coor.	Safety Class	Cat.	Size	Valve Type	Act. Type	Active I Passive	Normal Position	Safety Position	Test Type	Test Freq.	Relief Request	Deferred Just.	Tech. Pos.
FCV-3-114B	5614-M-3047-2	B2	SR	В	2.0	PLG	AO	A	С	С	BTC FC	M3 M3	_		TPv-04
	Valve Name:	Blend	ler Flov	v to V	ст						PIT	Y2			
HCV-3-121	5613-M-3047-2	F7	2	В	3.0	GL	AO	A	0	0	BTO	CS		CSJ-19	
	Valve Name:	Charç	ging Flo	ow to i	Regen	erative I	leat Ex	changer			FU	65		623-19	124-04
LCV-3-115B	5613-M-3047-2	F4	2	B	4.0	BTF	AO	A	С	O/C	BTO FC	CS CS		CSJ-20 CSJ-20	TPv-09 TPv-04
	Valve Name:	Emer	gency I	Makeu	ıp to C	harging	Pumps	i			PIT	Y2			
LCV-3-115C	5613-M-3047-2	C4	2	В	4.0	GL	МО	A	0	С	BTC	CS V2		CSJ-21	
	Valve Name:	VCT (Outlet Is	solatio	on Valv	ve						12			
MOV-3-350	5613-M-3047-2	F1	2	B	2.0	GA	МО	A	С	O/C	BTO	M3 V2			TPv-09
	Valve Name:	Emer	gency I	Borati	on Val	ve						12			
MOV-3-381	5613-M-3047-3	HЗ	2	A	3.0	GA	МО	A	0	С	AT-01 BTC	App-J CS		CSJ-25	
	Valve Name:	RCP	Seal Wa	ater R	eturn a	and Exc	ess Lete	down Isol	I		PIT	Y2			
MOV-3-6386	5613-M-3047-3	H5	2	A	3.0	GA	MO	A	0	С	AT-01 BTC	App-J CS		CSJ-25	
	Valve Name:	RCP	Seal Re	turn l	sol -						PII	12			
RV-3-203	5613-M-3047-1	A3	2	A/C	2.0	RV	SA	A	С	O/C	AT-01 RT	App-J Y10			
	Valve Name:	Letdd	lown Li	ne Re	lief Va	lve									
RV-3-283A	5613-M-3047-2 Valve Name:	G5 Charg	2 ging Pu	C mp 3/	0.75 A Discl	RV harge Ro	SA elief Val	A	С	orc	RT	Y10			
RV-3-283B	5613-M-3047-2 Valve Name:	E5 Charg	2 ging Pu	C mp 3E	0.75 B Discl	RV harge Ro	SA elief Va	A	C	O/C	RT	Y10			

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Chemical and Volume Control (047)

Valve Tag	P&ID	P&ID Coor.	Safety Class	Cat.	Size	Valve Type	Act. Type	Active / Passive	Normal Position	Safety Position	Test Type	Test Freq.	Relief Request	Deferred Just.	Tech. Pos.
RV-3-283C	5613-M-3047-2	C5	2	С	0.75	RV	SA	A	С	O/C	RT	Y10			
	Valve Name:	Charg	ing Pu	mp 30	Disc	harge R	elief Va	ive							
RV-3-303	5613-M-3047-3	G4	2	A/C	0.75	RV	SA	A	С	O/C	AT-01	App-J			
	Valve Name:	RCP S	Seal Re	eturn F	Relief \	/alve					RT	Y10			
RV-3-304	5613-M-3047-3	D8	1	С	0.75	RV	SA	A `	c	0/C	RT	Y5			
	Valve Name:	Exces	s Letd	own H	leat E	change	r Relief	Valve							
4-298A	5614-M-3047-3	F4	1	A/C	2.0	СК	SA	A	SYS	с	AT-01	App-J			
											CC	RR	VR-01	RJ-16	TPv-08
	Value Name:		D Sool	Inion	tion C	hook Va					co	RR	VR-01	RJ-16	TPv-01
·	valve Name.	4A KU		- injec	<u> </u>										
4-298B	5614-M-3047-3	B4	1	A/C	2.0	СК	SA	A	SYS	С	AT-01	App-J			
											00 00	RR	VR-01	RJ-16	TPv-08
	Valve Name:	4B RC	P Sea	l Injec	tion C	heck Va	ive				00	nn	11-01	10-10	179-01
4-298C	5614-M-3047-3	D4	1	A/C	2.0	СК	SA	A	SYS	с	AT-01	App-J			
											CC	RR	VR-01	RJ-16	TPv-08
	Valve Name:	4C RC	CP Sea	l injec	tion C	heck Va	lve				со	RR	VR-01	RJ-16	TPv-01
4-312A	5614-M-3047-2	C8	1	С	3.0	СК	SA	A	SYS	0	CCF	СМ			TPv-01,02
											COF	СМ			TPv-02
	Valve Name:	Charg	jing Lir	ne Che	eck Va										
4-312B	5614-M-3047-2	A7	1	С	3.0	СК	SA	A	SYS	0	CCF	СМ			TPv-01,02
	Valve Name:	Loop	C Chai	rging l	Line C	heck Va	ive				COF	СМ			TPv-02
4-3120	5614-M-3047-2	F7		A/C	30	СК	SA	A	SYS	0/C	AT-01	Ann-1		<u> </u>	
			•		0.0	••••	••••		010	0.0	CC	RR		RJ-14	TPv-08
											со	M3			
	Valve Name:	Charg	ing Li	ne Che	eck Va	lve									
4-351	5614-M-3047-2	F1	2	C	2.0	СК	SA	A	SYS	0	CCR	СМ			TPv-01,02
	Valve Name	Fmer	aency	Borati	on Ch	eck Valu	/e				COF	СМ		RJ-15	TPv-02
		Emer	Beuch	oorati		UN VAI									

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	·			Chei	mical	and V	olume	e Contro	ol (047)				Turkey IST Pro Valve T	Point Nuc ogram Plai Table	lear Plant n
Valve Tag	P&ID	P&ID Coor.	Safety Class	Cat.	Size	Valve Type	Act. Type	Active / Passive	Normal Position	Safety Position	Test Type	Test Freq.	Relief Request	Deferred Just.	Tech. Pos.
4-357	5614-M-3047-2	F3	2	C	4.0	СК	SA	A	SYS	0	CCR	СМ			TPv-01,02
	Valve Name:	Emer	gency l	Makeı	ıp to C	harging	Pumps	Check V	alve		COF	СМ		CSJ-22	TPv-02
CV-4-200A	5614-M-3047-1	A2	1	A	. 2.0	GL	AO	A	0	C	AT-01	App-J	<u></u>		
											BTC	М3			
											FC	М3			TPv-04
	Valve Name:	Letdo	wn Ori	fice S	ton Va	lve					PIT	Y2 -			
													·	-	
CV-4-200B	5614-M-3047-1	B2	1	A	2.0	GL	AO	A	0 ·	С	AI-01	App-J			
											FC	MG			TRUM
											PIT	¥2			111104
	Valve Name:	Letdo	wn Ori	fice S	top Va	lve					•••				
CV-4-200C	5614-M-3047-1	C2	1	A	2.0	GL		A	0	С	AT-01	App-J	·		
							•				BTC	M3			
											FC	M3			TPv-04
	Value Name:	Lotdo		fico S	ton Va	hvo.					PIT	Y2			
	valve Maille.	Leido		nce 3											
CV-4-204	5614-M-3047-1	C4	2	A	2.0	GL	AO	Α	0	С	AT-01	App-J			
											BTC	CS		CSJ-16	
											FC	CS		CSJ-16	TPv-04
											PIT	Y2			
	Valve Name:	Letdo	wn Lin	e Isol	ation \	/alve		_							
CV-4-310A	5614-M-3047-2	C7	1	В	2.0	GL	OA	A	0	0	BTO	M3			
											FO	М3			TPv-04
											PIT	Y2			
<u></u>	Valve Name:	Loop	A Char	ging l	solatio	on Valve									
CV-4-310B	5614-M-3047-2	A7	1	В	2.0	GL	AO	A	C	0	BTO	МЗ			
											FO	M3			TPv-04
	Valve Name:	Charç	ging Lir	ne Sto	p Valv	e Loop (C				PIT	Y2			
 CV-4-311		B7		В	2.0	GA			<u>с</u>		PIT	Y2	<u> </u>		
	Valve Name:	Auxili	iarv Sni	rav Ise	olation	Valve		•	~	v					
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Valve Tag	P&ID	P&ID Coor.	Safety Class	Cat.	Size	Valve Type	Act. Type	Active I Passive	Normal Position	Safety Position	Test Type	Test Freq.	Relief Request	Deferred Just.	Tech. Pos.
CV-4-387	5614-M-3047-3	B8	1	В	0.75	GL	OA	A	C	С	BTC	МЗ			
											FC	M3			TPv-04
	Valve Name:	Exces	s Letd	own l	solatio	n Valve					PII	¥2			
FCV-4-113B	5614-M-3047-2	D3	2	В	2.0	PLG	AO	A	с	С	BTC	M3			
											FC	МЗ			TPv-04
		•									PIT	Y2			
	Valve Name:	Blend	ler Flov	v to C	hargin	g Pump									
FCV-4-114B	5613-M-3047-2	B2	SR	В	2.0	PLG	AO	A	С	С	BTC	МЗ			
											FC	M3			TPv-04
	Valve Name:	Blend	ler Flov	v to V	ст						PIT	¥2			
HCV-4-121	5614-M-3047-2		2	B	3.0	GL	AO	A	. 0	0	BTO	CS	<u> </u>	CSJ-19	<u> </u>
									-		FO	CS		CSJ-19	TPv-04
	Valve Name:	Charg	jing Flo	ow to l	Regen	erative ł	leat Ex	changer							
LCV-4-115B	5614-M-3047-2	F4	2	В	4.0	BTF	AO	A	С	0/C	BTO	CS		CSJ-20	TPv-09
											FC	CS		CSJ-20	TPv-04
	Valve Name:	Emerg	gency I	Makeu	ip to C	harging	Pumps	5			PIT	¥2			
LCV-4-115C	5614-M-3047-2	C4	2	В	4.0	GL	MO	A	0	с	BTC	CS		CSJ-21	
	Valve Name:	VCT C	Dutiet I:	solatio	on Valv	/e					PIT	Y2			
MOV-4-350	5614-M-3047-2	F1	2	В	2.0	GA	MO	A	с	0/C	вто			<u></u>	TPv-09
											РЛ	¥2			
	Valve Name:	Emer	gency E	Borati	on Val	ve									
MOV-4-381	5614-M-3047-3	НЗ	2	A	3.0	GA	MO	A	0	С	AT-01	App-J		_	
											BTC	CS		CSJ-25	
											PIT	Y2			
	Valve Name:	RCPS	Seal Wa	ater R	eturn a	Ind Exce	ess Let	down Iso	l 						
MOV-4-6386	5614-M-3047-3	H5	2	A	3.0	GA	MO	A	0	С	AT-01	App-J			
											BTC	CS		CSJ-25	
	Valve Name:	RCPS	Seal Re	turn l	sol						PIT	Y2			

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Chemical and Volume Control (047)

Valve Tag	P&ID	P&ID Coor.	Safety Class	Cat.	Size	Valve Type	Act. Type	Active / Passive	Normal Position	Safety Position	Test Type	Test Freq.	Relief Request	Deferred Just.	Tech. Pos.
RV-4-203	5614-M-3047-1	A3	2	A/C	2.0	RV	SA	A	С	0/C	AT-01 RT	App-J			
	Valve Name:	Letdd	iown Li	ne Re	lief Va	ive						110			
RV-4-283A	5614-M-3047-2	G5	2	С	0.75	RV	SA	A	с	O/C	RT	Y10	·		
	Valve Name:	Charg	jing Pu	mp 4/	A Discl	harge R	elief Va	lve							
RV-4-283B	5614-M-3047-2	E5	2	С	0.75	RV	SA	A	с	0/C	RT	Y10			
	Valve Name:	Charg	jing Pu	mp 4E	3 Discl	harge R	elief Va	lve							
RV-4-283C	5614-M-3047-2	C5	2	С	0.75	RV	SA	A	с	0/C	RT	Y10			
	Valve Name:	Charg	jing Pu	mp 40	C Discl	harge R	elief Va	lve							
RV-4-303	5613-M-3047-3	G4	2	A/C	0.75	RV	SA	A	С	O/C	AT-01	App-J			
											RT	Y10			
	Valve Name:	RCP	Seal Re	turn F	Relief V	/alve									
RV-4-304	5614-M-3047-3	D8	1	С	0.75	RV	SA	A	с	0/C	RT	Y5			
	Valve Name:	Exces	s Letd	own H	leat Ex	change	r Relief	Valve							

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P&ID Safety Valve Act. Active I Normat Safety Test Test Relief Deferred Tech. Coor. Class Cat. Size Type Type Passive Position Position Type Freq. Request Just. Pos. Valve Tag P&ID 2 SA SYS CC RJ-17 3-2052 5613-M-3050-1 A7 С 1.0 СК A O/C RR **RJ-17** co RR Valve Name: **Containment Spray Suction Relief Line Check Valve** 3-741A 5613-M-3050-1 D7 2 В 2.0 GA MAN A LC O/C BTC Y2 TPv-11 BTO Y2 TPv-11 Valve Name: **RHR Recirc Line Isolation Valve** 3-752A LO C2 2 MAN A O/C BTC Y2 TPv-11 5613-M-3050-1 В 14.0 GA BTO Y2 TPv-11 Valve Name: **RHR Pump 3A Manual Suction Stop Valve** 3-752B 5613-M-3050-1 E2 2 в 14.0 GA MAN A LO O/C BTC Y2 TPv-11 BTO Y2 TPv-11 RHR Pump 3B Manual Suction Stop Valve Valve Name: CS 3-753A 5613-M-3050-1 C4 2 С 10.0 СК A SYS O/C CSJ-29 SA CC CO CS CSJ-29 **RHR Pump 3A Discharge Check Valve** Valve Name: 3-753B SYS O/C CSJ-29 5613-M-3050-1 E4 2 С 10.0 СК SA A CC CS co CS CSJ-29 Valve Name: **RHR Pump 3B Discharge Check Valve** HCV-3-758 5613-M-3050-1 C6 2 в 12.0 BTF AO Ρ 0 0 PIT Y2 **RHR Hx Outlet Flow Valve** Valve Name: MOV-3-750 5613-M-3050-1 MO A С O/C Y2 F8 1 A 14.0 GA AT-02 BTC CS CSJ-27 **BTO** CS CSJ-27 PIT Y2 Valve Name: Loop 3C RHR Pump Suction Stop Valve AT-02 MOV-3-751 5613-M-3050-1 F7 1 A 14.0 GA MO Α С O/C Y2 BTC CS CSJ-27 BTO CS CSJ-27 PIT Y2

Residual Heat Removal (050)

Valve Name: Loop 3C RHR Pump Suction Stop Valve

	Valve Tag	P&ID	P&ID Coor.	Safety Class	Cat.	Size	Valve Type	Act. Type	Active <i>I</i> Passive	Normal Position	Safety Position	Test Type	Test Freq.	Relief Request	Deferred Just.	Tech. Pos.
	MOV-3-860A	5613-M-3050-1	A6	2	B	14.0	GA	мо	A	С	O/C	BTO	М3			TPv-09
		Valve Name:	Conta	inment	t Sout	h Reci	rculatio	n Sump	lsol Valv	/e		PIT	Y2			
	MOV-3-860B	5613-M-3050-1	B6	2	В	-14.0	GA	мо	A	С	0/C	BTO	М3			TPv-09
1		Valve Name:	Conta	inment	t Norti	h Reci	rculatio	n Sump	Isol Valv	e		PIT	Y2			
	MOV-3-861A	5613-M-3050-1	A5	2	B	14.0	GA	МО	A	c	0/C	BTO	M3 Y2			TPv-09
		Valve Name:	Conta	inment	t Sout	h Reci	rculatio	n Sump	sol Valv	/e						
	MOV-3-861B	5613-M-3050-1	B5	2	В	14.0	GA	мо	A	С	O/C	BTO PIT	M3 Y2			TPv-09
		Valve Name:	Conta	inment	t Nort	h Reci	rculatio	n Sump	Isol Valv	e						
,	MOV-3-862A	5613-M-3050-1	E1	2	B	14.0	GA	МО	A	LO	0/C	BTC	CS Y2		CSJ-26	TPv-09
		Valve Name:	RHR	Suction	n from	RWST	ī									
	MOV-3-862B	5613-M-3050-1	E1	2	В	14.0	GA	мо	A	LO	0/C	BTC	CS Y2		CSJ-26	TPv-09
		Valve Name:	RHR	Suction	1 from	RWST	r									
	MOV-3-863A	5613-M-3050-1	F5	2	в	8.0	GA	МО	A	LC	O/C	BTO	CS		CSJ-28	TPv-09
		Valve Name:	RHR	Alterna	te Dis	ch Isol	l					PII	12			
,	MOV-3-863B	5613-M-3050-1	F5	2	В	8.0	GA	МО	A	LC	O/C	BTO	CS V2		CSJ-28	TPv-09
		Valve Name:	RHR	Alterna	te Dis	ch Isol	I			•		FII	12			
	MOV-3-872	5613-M-3050-1	G6	2	В	8.0	GA	МО	A	С	0/C	BTO	CS		CSJ-31	TPv-09
		Valve Name:	Alterr	ate Lo	w Hea	d SI						PII	12			
	4-2052	5614-M-3050-1	A7	2	с	1.0	СК	SA	A	SYS	O/C	сс	RR		RJ-17	
,		Valve Name:	Conta	inment	t Spra	y Suct	ion Reli	ef Line	Check Va	lve		CO	RR		RJ-17	

Residual Heat Removal (050)

Valve Tag	P&ID	P&ID Coor.	Safety Class	Cat.	Size	Valve Type	Act. Type	Active / Passive	Normal Position	Safety Position	Test Type	Test Freq.	Relief Request	Deferred Just.	Tech. Pos.
4-741A	5614-M-3050-1	D7	2	В	2.0	GA	MAN	A	LC	O/C	BTC	Y2			TPv-11
	Valve Name:	RHRI	Recirc I	Line Is	solatio	n Valve					BTO	Y2			TPv-11
4-752A	5614-M-3050-1	C2	2	В	14.0	GA	MAN	A	LO	O/C	BTC	Y2			TPv-11
											BTO	Y2			TPv-11
	Valve Name:	RHR	Pump 4	A Mai	nual Si	uction S	itop Val	ve							
4 - 752B	5614-M-3050-1	E2	2	В	14.0	GA	MAN	A	LO	O/C	BTC	Y2			TPv-11
	Valve Name:	RHR	Pump 4	B Mai	nual Si	uction S	itop Val	ve			BTO	Y2			TPv-11
4-753A	5614-M-3050-1	C4	2	С	10.0	СК	SA	A	SYS	O/C	сс	CS		CSJ-29	
											CO	CS		CSJ-29	
	Valve Name:	RHR	Pump 4	A Dis	charge	e Check	Valve								
4-753B	5614-M-3050-1	E4	2	С	10.0	СК	SA	A	SYS	O/C	сс	CS		CSJ-29	
	Valve Name:	RHR	Pump 4	B Dis	charge	e Check	Valve				со	CS		CSJ-29	
HCV-4-758	5614-M-3050-1	C6	2	В	12.0	BTF	AO	P	0	0	PIT	Y2		<u></u>	
	Valve Name:	RHR	Hx Out!	et Flo	w Valv	re									
MOV-4-750	5614-M-3050-1	F8	1	A	14.0	GA	MO	A	с	O/C	AT-02	Y2			
											BTC	CS		CSJ-27	
											BTO	CS		CSJ-27	
	Valve Name:	Loop	4A RHI	R Pum	np Suc	tion Sto	p Valve				PIT	Y2			
MOV-4-751		 F7	1		14.0	GA	MO	Α			AT-02	Y2			
			-						-		BTC	CS		CSJ-27	
											BTO	CS		CSJ-27	
											PIT	Y2			
	Valve Name:	Loop	4A RHI	R Pun	np Suc	tion Sto	p Valve								
MOV-4-860A	5614-M-3050-1	A6	2	B	14.0	GA	МО	A	С	0/C	BTO	М3			TPv-09
			•				. 6		_		PIT	Y2			

Residual Heat Removal (050)

Valve Tag	P&ID	P&ID Coor.	Safety Class	Cat.	Size	Valve Type	Act. Type	Active / Passive	Normal Position	Safety Position	Test Type	Test Freq.	Relief Request	Deferred Just.	Tech. Pos.
MOV-4-860B	5614-M-3050-1	B6	2	B	14.0	GA	МО	A	С	O/C	BTO	M3			TPv-09
	Valve Name:	Conta	inment	Sout	h Reci	rculatio	n Sump	Isol Valv	/e		PIT	Y2			
MOV-4-861A	5614-M-3050-1	A5	2	В	.14.0	GA	MO	A	С	O/C	BTO	М3			TPv-09
	Valve Name:	Conta	linment	Nort	h Recii	culation	n Sump	Isol Valv	e		Pit	Y2			
MOV-4-861B	5614-M-3050-1	B5	2	В	14.0	GA	МО	A	С	O/C	BTO	М3		-	TPv-09
	Valve Name:	Conta	inment	Sout	h Reci	rculatio	n Sump	lsol Valv	/e		PIT	¥2			
MOV-4-862A	5614-M-3050-1	E1	2	В	14.0	GA	MO	A	LO	O/C	BTC	CS		CSJ-26	TPv-09
	Valve Name:	RHR	Suction	from	RWST						Pit	Y2			
MOV-4-862B	5614-M-3050-1	D1	2	В	14.0	GA	мо	A	LO	O/C	BTC	CS		CSJ-26	TPv-09
	Valve Name:	RHR	Suction	from	RWST						PIT	Y2			
MOV-4-863A	5614-M-3050-1	F5	2	В	8.0	GA	MO	A	LC	0/C	BTO	CS		CSJ-28	TPv-09
	Valve Name:	RHR	Alternat	te Dis	ch Isol						PIT	Y2			
MOV-4-863B	5614-M-3050-1	F5	2	В	8.0	GA	мо	A	LC	O/C	BTO	CS		CSJ-28	TPv-09
	Valve Name:	RHR	Aitema	te Dis	ch Isol						PIT	Y2			
MOV-4-872	5614-M-3050-1	G6	2	В	8.0	GA	МО	A	с	O/C	BTO	CS		CSJ-31	TPv-09
	Valve Name:	Alterr	nate Lov	w Hea	d SI						PIT	Y2			

Residual Heat Removal (050)

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Valve Tag	P&ID	P&ID Coor.	Safety Class	Cat.	Size	Valve Type	Act. Type	Active / Passive	Normal Position	Safety Position	Test Type	Test Freq.	Relief Request	Deferred Just.	Tech. Pos.
3-2025	5613-M-3053-1 Valve Name:	A6 Isolat	2 ion Val	A ve for	0.75 Penet	GL ration 6	MAN 5B	Р	LC	С	AT-01	App-J			
3-2026	5613-M-3053-1 Valve Name:	B6 Isolat	2 ion Val	A ve for	0.75 Penet	GL ration 6	MAN 5C	P	LC	с	AT-01	App-J			
CV-3-2819	5613-M-3053-1	E7	2	A	2.00	GL	OA	A	0	С	AT-01 BTC FC PIT	App-J M3 M3 Y2			TPv-04
	Valve Name:	Conta	inmen	t Instr	ument	Air Ble	ed Cont	rol Valve							
CV-3-2826	5613-M-3053-1	E6	2	A	2.00	GL	AO	A	0	С	AT-01 BTC FC PIT	App-J M3 M3 Y2		·	TPv-04
_	Valve Name:	Conta	inmen	t Instr	ument	Air Ble	ed Cont	rol Valve							
POV-3-2600	5613-M-3053-1	C6	2	A	48.0	BTF	OA	A	С	С	AT-01 BTC FC PIT	App-J CS CS Y2		CSJ-02 CSJ-02	TPv-04
	Valve Name:	Conta	linmen	t Purg	le Sup	ply Isola	ition								
POV-3-2601	5613-M-3053-1 Valve Name:	C7 Conta	2 ainment	A t Purg	48.0 je Supj	BTF ply Isola	AO	A	С	С	AT-01 BTC FC PIT	App-J CS CS Y2		CSJ-02 CSJ-02	TPv-04
	5612 M 2052 1	 DC			54.0	DTE					AT 01				
PUV-3-2602	2013-M-3023-1 Valve Name:	Do Cont≉	Z	A t Purc	54.U 	ØIF aust Iso	AU	A	U	U	BTC FC PIT	App-J CS CS Y2		CSJ-02 CSJ-02	TPv-04

Containment Purge (053)

	Valve Tag	P&ID	P&ID Coor.	Safety Class	Cat.	Size	Valve Type	Act. Type	Active I Passive	Normal Position	Safety Position	Test Type	Test Freq.	Relief Request	Deferred Just.	Tech. Pos.
	POV-3-2603	5613-M-3053-1	D7	2	A	54.0	BTF	AO	A	С	С	AT-01	App-J			
												BTC	CS		CSJ-02	
												FC	CS		CSJ-02	TPv-04
												PIT	Y2			
		Valve Name:	Conta	inment	Purg	e Exha	ust Isol	lation								
\bigcirc	4-2025	5614-M-3053-1	A3	2	A	0.75	GL	MAN	Р	LC	С	AT-01	App-J			
		Valve Name:	Isolat	ion Val	ve for	Penet	ration 6	5C								
	4-2026	5614-M-3053-1	B3	2	A	0.75	GL	MAN	P	LC	С	AT-01	App-J			
		Valve Name:	Isolat	ion Val	ve for	Penet	ration 6	5B								
	CV-4-2819	5614-M-3053-1	E2	2	A	2.00	GL	AO	A	0	С	AT-01	App-J			
												BTC	M3			
												FC	МЗ			TPv-04
												PIT	Y2			
		Valve Name:	Conta	inment	Instr	ument	Air Blee	ed Cont	rol Valve							
\bigcirc	CV-4-2826	5614-M-3053-1	E3	2	A	2.00	GL	AO	A	0	С	AT-01	App-J			
												BTC	М3			
												FC	M3			TPv-04
												PIT	Y2			
		Valve Name:	Conta	inment	Instr	ument	Air Blee	ed Cont	rol Valve		_					
	POV-4-2600	5614-M-3053-1	B3	2	A	48.0	BTF	AO	A	С	С	AT-01	App-J			
												BTC	CS		CSJ-02	
			•		•				•			FC	CS		CSJ-02	TPv-04
			_	_	_	_						PIT	Y2			
\bigcirc		Valve Name:	Conta	inment	Purg	e Supp	ly Isola	tion								
	POV-4-2601	5614-M-3053-1	B2	2	A	48.0	BTF	AO	A	С	С	AT-01	App-J			
												BTC	CS		CSJ-02	
												FC	CS		CSJ-02	TPv-04
												PIT	Y2			
		Valve Name:	Conta	inment	Purg	e Supp	oly isola	tion								

Containment Purge (053)

\bigcirc						Con	tainme	ent Pu	rge (05	3)				Turkey IST Pro Valve 1	Point Nucl ogram Plan Fable	ear Plant
	Valve Tag	P&ID	P&ID Coor.	Safety Class	Cat.	Size	Valve Type	Act. Type	Active I Passive	Normal Position	Safety Position	Test Type	Test Freq.	Relief Request	Deferred Just.	Tech. Pos.
	POV-4-2602	5614-M-3053-1	D-3	2	A	54.0	BTF	AO	A	с	С	AT-01	App-J			
												BTC	CS		CSJ-02	
												FC	CS		CSJ-02	TPv-04
												PIT	Y2			
		Valve Name:	Conta	linmen	t Purg	e Exha	aust Iso	lation								·
\bigcirc	POV-4-2603	5614-M-3053-1	D-2	2	A	54.0	BTF	AO	A	c	с	AT-01	App-J			
												BTC	CS		CSJ-02	
												FC	CS		CSJ-02	TPv-04
												PIT	Y2			

Valve Name: Containment Purge Exhaust Isolation

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\bigcirc				I	Liqui	id Wa	iste Di	sposa	I Syste	m (061))			Turkey IST Pro Valve T	Point Nucl ogram Plan Fable	lear Plant
	Valve Tag	P&ID	P&ID Coor.	Safety Class	Cat.	Size	Valve Type	Act. Type	Active I Passive	Normal Position	Safety Position	Test Type	Test Freq.	Relief Request	Deferred Just.	Tech. Pos.
	CV-3-2821	5613-M-3061-1	H6	2	A	3.0	GL	AO	A	0	С	AT-01	App-J			
												BTC	M3			_
												FC	M3			TPv-04
		Valve Name:	Cntm	t Sump	Pum	p Discl	h Line C	ntmnt l	so Valve			PII	12			
\smile	CV-3-2822	5613-M-3061-1	H5	2	A	3.0	GL	AO	A	0	С	AT-01	App-J			
												BTC	M3			
												FC	МЗ			TPv-04
												PIT	Y2			
		Valve Name:	Cntm	t Sump	Pum	p Discl	h Line C	ntmnt l	so Valve						_	
	CV-3-4658A	5613-M-3061-1	B 6	2	A	1.0	DIA	AO	A	0	С	AT-01	App-J			
												BTC	M3			
												FC	M3			TPv-04
		Valve Name:	RCDI	to VH	Line (Cntmt	lso Viv					ΡΙΤ	¥2			
\smile	CV-3-4658B	5613-M-3061-1	B6	2	A	1.0	DIA	AO	A	0	с	AT-01	App-J			
												BTC	M3			
												FC	M3			TPv-04
												PIT	Y2			
		Valve Name:	RCDI	to VH	Line (Cntmt	lso Viv									
	CV-3-4659A	5613-M-3061-1	D6	2	A	0.75	DIA	AO	A	С	С	AT-01	App-J			
												BTC	M3			
												FC	M3			TPv-04
. ,						_						PIT	¥2			
\bigcirc		Valve Name:	RCDI	to Gas	s Anai	yzer C	ntmnt Is									
	CV-3-4659B	5613-M-3061-1	D6	2	A	0.75	DIA	AO	A	С	С	AT-01	App-J			
												BTC	M3			
												FC	M3			TPv-04
		Valve Name [.]	RCDI	to Gas	: Anal	vzer C	ntmnt le	o Viv				PIT	Y2			

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\bigcirc				1	Liqui	id Wa	ste Di	sposa	I Syste	m (061)	i			Turkey IST Pro Valve T	Point Nucl ogram Plan Fable	ear Plant
	Valve Tag	P&ID	P&ID Coor.	Safety Class	Cat.	Size	Valve Type	Act. Type	Active / Passive	Normal Position	Safety Position	Test Type	Test Freq.	Relief Request	Deferred Just.	Tech. Pos.
	CV-3-4668A	5613-M-3061-1	G5	2	A	3.0	DIA	AO	A	0	C	AT-01	App-J		-	
												BTC	М3			
												FC	M3			TPv-04
		Valve Name:	RCDT	Pump	Disch	ı Cntm	t Isolati	on Valv	e			PIT	Y2			
\bigcirc	CV-3-4668B	5613-M-3061-1	G6	2	A	3.0	DIA	AO	A	0	С	AT-01	App-J	<u> </u>	·	<u> </u>
												BTC	M3			
												FC	M3			TPv-04
												PIT	Y2			
		Valve Name:	RCDT	Pump	Disch	Cntm	t Isolati	on Valv	e							
	CV-4-2821	5614-M-3061-1	- H6	2	A	3.0	GL	AO	A	0	С	AT-01	App-J			
												BTC	M3			
												FC	M3			TPv-04
		Valve Name:	Cntm	t Sump	Pum	o Discl	h Line C	ntmnt l	so Valve			PIT	Y2			
\bigcirc	<u>.</u>	·····														
	CV-4-2822	5614-M-3061-1	H5	2	A	3.0	GL	AO	A	0	С	AT-01	App-J			
												BTC	M3			
												FC	M3			TPv-04
		Valve Name:	Cntm	t Sump	Pum	o Discl	h Line C	intmnt l	so Valve			PII	12			
				. <u> </u>												
	CV-4-4658A	5614-M-3061-1	B6	2	A	1.0	DIA	AO	A	0	С	AT-01	App-J			
												BTC	M3		-	TD . 04
												PU	M3 V2			164-04
\bigcirc		Valve Name:	RCDT	to VH	Line C	Cntmt I	so Viv					FII	12			
	CV-4-4658B		B6	2		1.0	DIA	AO	A	0	с	AT-01	App-J	-		
				-						-	•	BTC	M3			
												FC	M3			TPv-04
												PIT	¥2			
		Valve Name:	RCDT	to VH	Line C	Cntmt I	iso Viv									

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Tu	key Point Nuclear Plant
IST	Program Plan
Va	lve Table

Valve Tag	P&ID	P&ID Coor.	Safety Class	Cat.	Size	Valve Type	Act. Type	Active / Passive	Normal Position	Safety Position	Test Type	Test Freq.	Relief Request	Deferred Just.	Tech. Pos.
CV-4-4659A	5614-M-3061-1	D6	2	A	0.75	DIA	AO	A	С	С	AT-01	App-J			
											BTC	M3			
											FC	M3			TPv-04
											PIT	Y2			
	Valve Name:	RCDT	to Gas	s Anal	yzer C	ntmnt Is	o VIv					_		_	
CV-4-4659B	5614-M-3061-1	D6	2	A	0.75	DIA	AO	A	С	С	AT-01	App-J			
											BTC	M3			
											FC	МЗ			TPv-04
											PIT	Y2			
	Valve Name:	RCDT	to Gas	s Anal	yzer C	ntmnt Is	o VIv						,		
 CV-4-4668A	5614-M-3061-1	G5	2	A	3.0	DIA	AO	A	0	С	AT-01	App-J			
											BTC	M3			
											FC	M3			TPv-04
											PIT	Y2			
	Valve Name:	RCDT	Pump	Disch	n Cntm	t Isolati	on Valv	e							
CV-4-4668B	5614-M-3061-1	G6	2	A	3.0	DIA	AO	A	0	С	AT-01	App-J			
											BTC	M3			
											FC	M3			TPv-04

Liquid Waste Disposal System (061)

Valve Name: RCDT Pump Disch Cntmt Isolation Valve

		Safety Injection (062)											IST Pro Valve 1	ogram Pla Fable	'n
Valve Tag	P&ID	P&ID Coor.	Safety Class	Cat.	Size	Valve Type	Act. Type	Active / Passive	Normal Position	Safety Position	Test Type	Test Freq.	Relief Request	Deferred Just.	Tech. Pos.
3-874A	5613-M-3062-1	C7	1	A/C	2.0	СК	SA	A	SYS	O/C	AT-02	Y2			
											CC	RR		RJ-06	TPv-08
	Valve Name:	SI Ho	t Leg Ir	njectio	on Loo	p A Che	ck Valv	e			со	RR		RJ-06	
3-874B	5613-M-3062-1	F7		A/C	2.0	СК	SA	A	SYS	0/C	AT-02	Y2	. <u> </u>		<u> </u>
											сс	RR		RJ-06	TPv-08
											со	RR		RJ-06	
	Valve Name:	SI Ho	t Leg Ir	njectio	on Loo	p B Che	ck Valv	e							
3-874C	5613-M-3062-1	F2	2	С	2.0	СК	SA	A	SYS	0	CCR	СМ			TPv-01,02
											COF	СМ			TPv-02
	Valve Name:	SI Pu	mp Min	imum	Flow/	Test Re	turn Ch	eck Valve)		_				
3-879A	5613-M-3062-1	G5	2	C	3.0	СК	SA	A	SYS	O/C	CC	МЗ			
	Valve Name:	Safet	y Inject	ion Pi	ump 31	B Disch	arge Ch	eck Valve	9		со	RR		RJ-07	
3-879B	5613-M-3062-1	E4	2	С	3.0	СК	SA	A	SYS	O/C	СС	M3		_	_
	Valve Name:	Safet	y Inject	ion Pi	ump 3/	A Disch	arge Ch	eck Valve	•		со	RR		RJ-07	
3-893A	5613-M-3062-1	F4	2	С	0.75	СК	SA	Α	SYS	0	CCR	СМ			TPv-01,02
											COF	СМ			TPv-02
	Valve Name:	Safet	y Inject	ion P	ump 3l	B Minim	um Flo	w Check '	Valve						
3-893B	5613-M-3062-1	E4	2	С	0.75	СК	SA	A	SYS	0	CCR	СМ			TPv-01,02
	Valve Name:	Safet	y Inject	ion P	ump 3/	A Minim	um Flov	w Check \	Valve		COF	СМ			TPv-02
MOV-3-843A	5613-M-3062-2	B 6	2	В	4.0	GA	MO	Α	С	O/C	BTC	M3			
											BTO	M3			
	Valve Name:	SI Co	id Leg	Inject	ion Va	lve					PIT	¥2			
MOV-3-843B	5613-M-3062-2	C6	2	В	4.0	GA	MO	A		O/C	BTC	мз			
			-	-				••	-	2. •	BTO	M3			
											PIT	Y2			
	Valve Name:	SI Co	ld Leg	Inject	ion Va	lve									

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Turkey Point Nuclear Plant

P&ID	P&ID Coor.	Safety Class	Cat.	Size	Valve Type	Act. Type	Active / Passive	Normat Position	Safety Position	Test Type	Test Freq.	Relief Request	Deferred Just.	Tech. Pos.
5613-M-3062-1	B1	2	В	2.0	GL	мо	A	0	O/C	BTC	CS		CSJ-05	TPv-09
Valve Name:	HSSI	Pump l	Recirc	ulatio	n to RW	ST				PIT	¥2			
5613-M-3062-1	B1	2	В	2.0	GL	мо	A	0	O/C	BTC	CS		CSJ-05	TPv-09
Valve Name:	HSSI	Pump l	Recirc	ulatio	n to RW	ST				PIT	Y2			
5613-M-3062-1	C4	2	В	16.0	GA	мо	A	0	O/C	BTC	CS	<u></u>	CSJ-06	TPv-09
Valve Name:	RWST	[Outle	t Isola	tion V	alve					PIT	Y2			
5613-M-3062-1	C4	2	В	16.0	GA	МО	A	0	O/C	BTC	CS		CSJ-06	TPv-09
Valve Name:	RWST	[Outlet	t Isola	tion V	alve					pit	Y2			
														<u> </u>
5613-M-3062-1	D7	1	A	2.0	GA	MO	A	C	O/C	BTC	CS		CSJ-03	
										PIT	US Y2		051-05	
Valve Name:	Loop	A Hot I	.eg Sa	afety Ir	jection	Isolatio	n Valve							
5613-M-3062-1	F7	1	A	2.0	GA	мо	A	с	O/C	BTC	CS		CSJ-03	
										BTO	CS		CSJ-03	
Valve Name:	Loop	B Hot I	_eg Sa	afety Ir	ijection	Isolatio	on Valve			PIT	Y2			
5613-M-3062-1	E6	2	В	3.0	GA	МО	A	С	O/C	BTC	МЗ			
							•			BTO	M3			
Valve Name:		A & B I	Hot Le	g Safe	ty Injec	tion Val	ve			PIT	Y2			
	 								010				00104	TD: 00
5613-M-3062-1	US	2	в	4.0	GA	MÜ	A	0	010	PIT	US Y2		651-04	194-09
Valve Name:	SI Pu	mp Dis	charg	e Heac	ler Unit	Cross 1	lie Vlave							
5613-M-3062-1	D5	2	В	4.0	GA	MO	A	0	O/C	BTC	CS		CSJ-04	TPv-09
Valve Name:	SI Pur	mp Dis	charg	e Head	ler Unit	Cross 1	lie Vlave			PIT	Y2			
		•	5											
5613_M_3062_1	FR			0.25	- RV	 \$A	Δ		0/0	 דק	Y10			
	P&ID 5613-M-3062-1 Valve Name: 5613-M-3062-1 Valve Name:	P&ID Coor. 5613-M-3062-1 B1 Valve Name: HSSI 5613-M-3062-1 B1 Valve Name: HSSI 5613-M-3062-1 B1 Valve Name: HSSI 5613-M-3062-1 C4 Valve Name: RWST 5613-M-3062-1 C4 Valve Name: RWST 5613-M-3062-1 D7 Valve Name: Loop 5613-M-3062-1 F7 Valve Name: Loop 5613-M-3062-1 E6 Valve Name: Loop 5613-M-3062-1 D5 Valve Name: Loop 5613-M-3062-1 D5 Valve Name: SI Put 5613-M-3062-1 D5 Valve Name: SI Put 5613-M-3062-1 D5 Valve Name: SI Put	P&ID Coor. Class 5613-M-3062-1 B1 2 Valve Name: HSSI Pump I 5613-M-3062-1 B1 2 Valve Name: HSSI Pump I 5613-M-3062-1 C4 2 Valve Name: RWST Outlet 5613-M-3062-1 C4 2 Valve Name: RWST Outlet 5613-M-3062-1 D7 1 Valve Name: Loop A Hot I 5613-M-3062-1 F7 1 Valve Name: Loop B Hot I 5613-M-3062-1 F7 1 Valve Name: Loop A Hot I 1 5613-M-3062-1 E6 2 Valve Name: Loop A & B I 1 5613-M-3062-1 D5 2 Valve Name: SI Pump Dis 1 5613-M-3062-1 D5 2 Valve Name: SI Pump Dis 5613-M-3062-1 D5 2 Valve Name: SI Pump Dis 5613-M-3062-1 D5 2	P&ID Coor. Class Cat. 5613-M-3062-1 B1 2 B Valve Name: HSSI Pump Recirc 5613-M-3062-1 B1 2 B Valve Name: HSSI Pump Recirc 5613-M-3062-1 C4 2 B Valve Name: RWST Outlet Isola 5613-M-3062-1 C4 2 B Valve Name: RWST Outlet Isola B 5613-M-3062-1 D7 1 A Valve Name: Loop A Hot Leg Sa Sa 5613-M-3062-1 F7 1 A Valve Name: Loop B Hot Leg Sa Sa 5613-M-3062-1 F7 1 A Valve Name: Loop A Hot Leg Sa Sa 5613-M-3062-1 E6 2 B Valve Name: Loop A & B Hot Leg Sa Sa 5613-M-3062-1 D5 2 B Valve Name: SI Pump Discharg Sa 5613-M-3062-1 D5 2 B Valve Name: SI Pump Discharg 5613-M-3062-1 <td>P&ID Coor. Class Cat. Size 5613-M-3062-1 B1 2 B 2.0 Valve Name: HSSI Pump Recirculation 5613-M-3062-1 B1 2 B 2.0 Valve Name: HSSI Pump Recirculation 20 20 Valve Name: HSSI Pump Recirculation 20 20 5613-M-3062-1 C4 2 B 16.0 Valve Name: RWST Outlet Isolation Value 30 30 5613-M-3062-1 C4 2 B 16.0 Valve Name: RWST Outlet Isolation Value 30 5613-M-3062-1 D7 1 A 2.0 Valve Name: Loop A Hot Leg Safety In 5613-M-3062-1 F7 1 A 2.0 Valve Name: Loop A & B Hot Leg Safety In 5613-M-3062-1 E6 2 B 3.0 Valve Name: Loop A & B Hot Leg Safety In 5613-M-3062-1 D5 2 B 4.0 Valve Name: SI Pump Discha</td> <td>PBID Coor. Class Cat. Size Type 5613-M-3062-1 B1 2 B 2.0 GL Valve Name: HSSI Pump Recirculation to RW 5613-M-3062-1 B1 2 B 2.0 GL Valve Name: HSSI Pump Recirculation to RW 5613-M-3062-1 C4 2 B 16.0 GA Valve Name: RWST Outlet Isolation Valve 5613-M-3062-1 C4 2 B 16.0 GA Valve Name: RWST Outlet Isolation Valve 5613-M-3062-1 D7 1 A 2.0 GA Valve Name: Loop A Hot Leg Safety Injection 5613-M-3062-1 F7 1 A 2.0 GA Valve Name: Loop A & B Hot Leg Safety Injection 5613-M-3062-1 E6 2 B 3.0 GA Valve Name: Loop A & B Hot Leg Safety Injection 5613-M-3062-1 D5 2 B 4.0 GA Valve Name: SI Pump Discharge Header Unit 5613-M-3062-1 D5</td> <td>P&IDCoor.ClassCat.SizeTypeType5613-M-3062-1B12B2.0GLMOValve Name:HSSI Pump Recirculation to RWST5613-M-3062-1B12B2.0GLMOValve Name:HSSI Pump Recirculation to RWST5613-M-3062-1C42B16.0GAMOValve Name:RWST Outlet Isolation Valve5613-M-3062-1C42B16.0GAMOValve Name:RWST Outlet Isolation Valve5613-M-3062-1D71A2.0GAMOValve Name:Loop A Hot Leg Safety Injection Isolation5613-M-3062-1F71A2.0GAMOValve Name:Loop B Hot Leg Safety Injection Isolation5613-M-3062-1E62B3.0GAMOValve Name:Loop A & B Hot Leg Safety Injection Isolation5613-M-3062-1D52B4.0GAMOValve Name:Loop A & B Hot Leg Safety Injection Valve5613-M-3062-1D52B4.0GAMOValve Name:SI Pump Discharge Header Unit Cross T5613-M-3062-1D52B4.0GAMOValve Name:SI Pump Discharge Header Unit Cross T5613-M-3062-1D52B4.0GAMO</td> <td>PBID Coor. Class Cat. Size Type Type Passive 5613-M-3062-1 B1 2 B 2.0 GL MO A Valve Name: HSSI Pump Recirculation to RWST 5613-M-3062-1 B1 2 B 2.0 GL MO A Valve Name: HSSI Pump Recirculation to RWST 5613-M-3062-1 C4 2 B 16.0 GA MO A Valve Name: RWST Outlet Isolation Valve 5613-M-3062-1 C4 2 B 16.0 GA MO A Valve Name: RWST Outlet Isolation Valve 5613-M-3062-1 D7 1 A 2.0 GA MO A Valve Name: Loop A Hot Leg Safety Injection Isolation Valve 5613-M-3062-1 F7 1 A 2.0 GA MO A Valve Name: Loop A & B Hot Leg Safety Injection Isolation Valve 5613-M-3062-1 E6 2 B 3.0 GA MO A Valve Nam</td> <td>PAID Coor, Class Cat. Size Type Type Passive Position 5613-M-3062-1 B1 2 B 2.0 GL MO A O Valve Name: HSSI Pump Recirculation to RWST 5613-M-3062-1 B1 2 B 2.0 GL MO A O Valve Name: HSSI Pump Recirculation to RWST 5613-M-3062-1 C4 2 B 16.0 GA MO A O Valve Name: RWST Outlet Isolation Valve 5613-M-3062-1 C4 2 B 16.0 GA MO A O Valve Name: RWST Outlet Isolation Valve 5613-M-3062-1 D7 1 A 2.0 GA MO A C Valve Name: Loop A Hot Leg Safety Injection Isolation Valve 5613-M-3062-1 F7 1 A 2.0 GA MO A C Valve Name: Loop A & B Hot Leg Safety Injection Isolation Valve 5613-M-3062-1 E6 2</td> <td>PBD Coor. Class Cat. Size Type Type Passive Position Position 5613-M-3062-1 B1 2 B 2.0 GL MO A O O/C Valve Name: HSSI Pump Recirculation to RWST 5613-M-3062-1 B1 2 B 2.0 GL MO A O O/C Valve Name: HSSI Pump Recirculation to RWST 5613-M-3062-1 C4 2 B 16.0 GA MO A O O/C Valve Name: RWST Outlet Isolation Valve 5613-M-3062-1 C4 2 B 16.0 GA MO A O O/C Valve Name: RWST Outlet Isolation Valve 5613-M-3062-1 D7 1 A 2.0 GA MO A C O/C Valve Name: Loop A Hot Leg Safety Injection Isolation Valve 5613-M-3062-1 F7 1 A 2.0 GA MO A C O/C Valv</td> <td>PBID Coor. Class Cat. Size Type Type Passive Position Position Type 5613.M-3062-1 B1 2 B 2.0 GL MO A O O/C ETC PIT Valve Name: HSSI Pump Rectrcutation to RWST 5613.M-3062-1 B1 2 B 2.0 GL MO A O O/C ETC PIT Valve Name: HSSI Pump Rectrcutation to RWST 5613.M-3062-1 C4 2 B 16.0 GA MO A O O/C ETC PIT Valve Name: RWST Outlet Isolation Valve 5613.M-3062-1 C4 2 B 16.0 GA MO A O O/C ETC PIT Valve Name: RWST Outlet Isolation Valve 5613.M-3062-1 D7 1 A 2.0 GA MO A C O/C ETC BTO PIT Valve Name: Loop A Hot Leg Safety Injection Isolation Valve 5613.M-3062-1 F7 1 A</td> <td>PAID Coor, Class Cat. Size Type Type Passive Position Position Type Freq. 5613.M-3062-1 B1 2 B 2.0 GL MO A O O/C BTC CS 5613.M-3062-1 B1 2 B 2.0 GL MO A O O/C BTC CS 5613.M-3062-1 B1 2 B 2.0 GL MO A O O/C BTC CS 5613.M-3062-1 C4 2 B 16.0 GA MO A O O/C BTC CS Yalve Name: RWST Outlet Isolation Valve S MO A O O/C BTC CS 5613.M-3062-1 D7 1 A 2.0 GA MO A C O/C BTC CS 5613.M-3062-1 D7 1 A 2.0 GA MO <</td> <td>PBID Coor. Class Cat. Size Type Type Passive Position Position Type Free, Request 5613.M3062-1 B1 2 B 2.0 GL MO A O O/C BTC CS Yalve Name: HSSI Pump Recirculation to RWST E S GL MO A O O/C BTC CS Yalve Name: HSSI Pump Recirculation to RWST E S GL MO A O O/C BTC CS Yalve Name: HSSI Pump Recirculation to RWST E S GA MO A O O/C BTC CS Yalve Name: RWST Outlet Isolation Valve E S GA MO A O O/C BTC CS Yalve Name: Loop A Hot Leg Safety Injection Isolation Valve E S S S S S S S S S S S S S</td> <td>PBID Coor. Class Cat. Size Type Type Passive Position Position Type Freq. Request Just. 5613.M.3062-1 B1 2 B 2.0 GL MO A O O/C BTC CS CSJ-05 Valve Name: HSSI Pump Recirculation to RWST HSSI Pump Recirculation to RWST FTT Y2 CSJ-05 5613.M.3062-1 C4 2 B 16.0 GA MO A O O/C BTC CS CSJ-05 5613.M.3062-1 C4 2 B 16.0 GA MO A O O/C BTC CS CSJ-06 PIT Y2 Valve Name: RWST Outlet Isolation Valve FT Y2 CSJ-06 5613.M.3062-1 C4 2 B 16.0 GA MO A O O/C BTC CS CSJ-06 PIT Y2 Valve Name: RWST Outlet Isolation Va</td>	P&ID Coor. Class Cat. Size 5613-M-3062-1 B1 2 B 2.0 Valve Name: HSSI Pump Recirculation 5613-M-3062-1 B1 2 B 2.0 Valve Name: HSSI Pump Recirculation 20 20 Valve Name: HSSI Pump Recirculation 20 20 5613-M-3062-1 C4 2 B 16.0 Valve Name: RWST Outlet Isolation Value 30 30 5613-M-3062-1 C4 2 B 16.0 Valve Name: RWST Outlet Isolation Value 30 5613-M-3062-1 D7 1 A 2.0 Valve Name: Loop A Hot Leg Safety In 5613-M-3062-1 F7 1 A 2.0 Valve Name: Loop A & B Hot Leg Safety In 5613-M-3062-1 E6 2 B 3.0 Valve Name: Loop A & B Hot Leg Safety In 5613-M-3062-1 D5 2 B 4.0 Valve Name: SI Pump Discha	PBID Coor. Class Cat. Size Type 5613-M-3062-1 B1 2 B 2.0 GL Valve Name: HSSI Pump Recirculation to RW 5613-M-3062-1 B1 2 B 2.0 GL Valve Name: HSSI Pump Recirculation to RW 5613-M-3062-1 C4 2 B 16.0 GA Valve Name: RWST Outlet Isolation Valve 5613-M-3062-1 C4 2 B 16.0 GA Valve Name: RWST Outlet Isolation Valve 5613-M-3062-1 D7 1 A 2.0 GA Valve Name: Loop A Hot Leg Safety Injection 5613-M-3062-1 F7 1 A 2.0 GA Valve Name: Loop A & B Hot Leg Safety Injection 5613-M-3062-1 E6 2 B 3.0 GA Valve Name: Loop A & B Hot Leg Safety Injection 5613-M-3062-1 D5 2 B 4.0 GA Valve Name: SI Pump Discharge Header Unit 5613-M-3062-1 D5	P&IDCoor.ClassCat.SizeTypeType5613-M-3062-1B12B2.0GLMOValve Name:HSSI Pump Recirculation to RWST5613-M-3062-1B12B2.0GLMOValve Name:HSSI Pump Recirculation to RWST5613-M-3062-1C42B16.0GAMOValve Name:RWST Outlet Isolation Valve5613-M-3062-1C42B16.0GAMOValve Name:RWST Outlet Isolation Valve5613-M-3062-1D71A2.0GAMOValve Name:Loop A Hot Leg Safety Injection Isolation5613-M-3062-1F71A2.0GAMOValve Name:Loop B Hot Leg Safety Injection Isolation5613-M-3062-1E62B3.0GAMOValve Name:Loop A & B Hot Leg Safety Injection Isolation5613-M-3062-1D52B4.0GAMOValve Name:Loop A & B Hot Leg Safety Injection Valve5613-M-3062-1D52B4.0GAMOValve Name:SI Pump Discharge Header Unit Cross T5613-M-3062-1D52B4.0GAMOValve Name:SI Pump Discharge Header Unit Cross T5613-M-3062-1D52B4.0GAMO	PBID Coor. Class Cat. Size Type Type Passive 5613-M-3062-1 B1 2 B 2.0 GL MO A Valve Name: HSSI Pump Recirculation to RWST 5613-M-3062-1 B1 2 B 2.0 GL MO A Valve Name: HSSI Pump Recirculation to RWST 5613-M-3062-1 C4 2 B 16.0 GA MO A Valve Name: RWST Outlet Isolation Valve 5613-M-3062-1 C4 2 B 16.0 GA MO A Valve Name: RWST Outlet Isolation Valve 5613-M-3062-1 D7 1 A 2.0 GA MO A Valve Name: Loop A Hot Leg Safety Injection Isolation Valve 5613-M-3062-1 F7 1 A 2.0 GA MO A Valve Name: Loop A & B Hot Leg Safety Injection Isolation Valve 5613-M-3062-1 E6 2 B 3.0 GA MO A Valve Nam	PAID Coor, Class Cat. Size Type Type Passive Position 5613-M-3062-1 B1 2 B 2.0 GL MO A O Valve Name: HSSI Pump Recirculation to RWST 5613-M-3062-1 B1 2 B 2.0 GL MO A O Valve Name: HSSI Pump Recirculation to RWST 5613-M-3062-1 C4 2 B 16.0 GA MO A O Valve Name: RWST Outlet Isolation Valve 5613-M-3062-1 C4 2 B 16.0 GA MO A O Valve Name: RWST Outlet Isolation Valve 5613-M-3062-1 D7 1 A 2.0 GA MO A C Valve Name: Loop A Hot Leg Safety Injection Isolation Valve 5613-M-3062-1 F7 1 A 2.0 GA MO A C Valve Name: Loop A & B Hot Leg Safety Injection Isolation Valve 5613-M-3062-1 E6 2	PBD Coor. Class Cat. Size Type Type Passive Position Position 5613-M-3062-1 B1 2 B 2.0 GL MO A O O/C Valve Name: HSSI Pump Recirculation to RWST 5613-M-3062-1 B1 2 B 2.0 GL MO A O O/C Valve Name: HSSI Pump Recirculation to RWST 5613-M-3062-1 C4 2 B 16.0 GA MO A O O/C Valve Name: RWST Outlet Isolation Valve 5613-M-3062-1 C4 2 B 16.0 GA MO A O O/C Valve Name: RWST Outlet Isolation Valve 5613-M-3062-1 D7 1 A 2.0 GA MO A C O/C Valve Name: Loop A Hot Leg Safety Injection Isolation Valve 5613-M-3062-1 F7 1 A 2.0 GA MO A C O/C Valv	PBID Coor. Class Cat. Size Type Type Passive Position Position Type 5613.M-3062-1 B1 2 B 2.0 GL MO A O O/C ETC PIT Valve Name: HSSI Pump Rectrcutation to RWST 5613.M-3062-1 B1 2 B 2.0 GL MO A O O/C ETC PIT Valve Name: HSSI Pump Rectrcutation to RWST 5613.M-3062-1 C4 2 B 16.0 GA MO A O O/C ETC PIT Valve Name: RWST Outlet Isolation Valve 5613.M-3062-1 C4 2 B 16.0 GA MO A O O/C ETC PIT Valve Name: RWST Outlet Isolation Valve 5613.M-3062-1 D7 1 A 2.0 GA MO A C O/C ETC BTO PIT Valve Name: Loop A Hot Leg Safety Injection Isolation Valve 5613.M-3062-1 F7 1 A	PAID Coor, Class Cat. Size Type Type Passive Position Position Type Freq. 5613.M-3062-1 B1 2 B 2.0 GL MO A O O/C BTC CS 5613.M-3062-1 B1 2 B 2.0 GL MO A O O/C BTC CS 5613.M-3062-1 B1 2 B 2.0 GL MO A O O/C BTC CS 5613.M-3062-1 C4 2 B 16.0 GA MO A O O/C BTC CS Yalve Name: RWST Outlet Isolation Valve S MO A O O/C BTC CS 5613.M-3062-1 D7 1 A 2.0 GA MO A C O/C BTC CS 5613.M-3062-1 D7 1 A 2.0 GA MO <	PBID Coor. Class Cat. Size Type Type Passive Position Position Type Free, Request 5613.M3062-1 B1 2 B 2.0 GL MO A O O/C BTC CS Yalve Name: HSSI Pump Recirculation to RWST E S GL MO A O O/C BTC CS Yalve Name: HSSI Pump Recirculation to RWST E S GL MO A O O/C BTC CS Yalve Name: HSSI Pump Recirculation to RWST E S GA MO A O O/C BTC CS Yalve Name: RWST Outlet Isolation Valve E S GA MO A O O/C BTC CS Yalve Name: Loop A Hot Leg Safety Injection Isolation Valve E S S S S S S S S S S S S S	PBID Coor. Class Cat. Size Type Type Passive Position Position Type Freq. Request Just. 5613.M.3062-1 B1 2 B 2.0 GL MO A O O/C BTC CS CSJ-05 Valve Name: HSSI Pump Recirculation to RWST HSSI Pump Recirculation to RWST FTT Y2 CSJ-05 5613.M.3062-1 C4 2 B 16.0 GA MO A O O/C BTC CS CSJ-05 5613.M.3062-1 C4 2 B 16.0 GA MO A O O/C BTC CS CSJ-06 PIT Y2 Valve Name: RWST Outlet Isolation Valve FT Y2 CSJ-06 5613.M.3062-1 C4 2 B 16.0 GA MO A O O/C BTC CS CSJ-06 PIT Y2 Valve Name: RWST Outlet Isolation Va

Safety Injection (062)

P&ID Safety Valve Active I Normal Safety Test Test Relief Deferred Tech. Act. Coor. Class Cat. Size Type Type Passive Position Position Type Freq. Request Just. Pos. Valve Tag P&ID С O/C RV-3-857 5613-M-3062-2 C5 2 С 0.75 RV SA A RT Y10 Valve Name: Safety Injection Cold Leg Header Relief Valve 4-874A 5614-M-3062-1 C7 A/C 2.0 СК SA A SYS O/C AT-02 Y2 1 CC RR RJ-06 TPv-08 CO RR RJ-06 Valve Name: SI Hot Leg Injection Loop A Check Valve 4-874B SA A SYS O/C AT-02 5614-M-3062-1 F7 1 A/C 2.0 СК Y2 СС RR RJ-06 TPv-08 CO RR RJ-06 Valve Name: SI Hot Leg Injection Loop B Check Valve 0 4-874C 5614-M-3062-1 F2 2 С 2.0 СК SA A SYS CCR СМ TPv-01,02 TPv-02 COF СМ Valve Name: SI Pump Minimum Flow/Test Return Check Valve 4-879C 5614-M-3062-1 E4 2 ¢ 3.0 СК SA A SYS O/C CC M3 CO RR RJ-07 Safety Injection Pump 4A Discharge Check Valve Valve Name: 4-879D 5614-M-3062-1 G5 2 С SA A SYS O/C СС 3.0 СК M3 CO RR RJ-07 Valve Name: Safety Injection Pump 4B Discharge Check Valve 4-893C 5614-M-3062-1 SYS 0 TPv-01,02 E4 2 С 0.75 СК SA A CCR CM COF TPv-02 СМ Valve Name: Safety Injection Pump 4A Minimum Flow Check Valve 4-893D TPv-01,02 5614-M-3062-1 F4 2 С 0.75 СК SA A SYS 0 CCR CM COF CM TPv-02 Safety Injection Pump 4B Minimum Flow Check Valve Valve Name: MOV-4-843A 5614-M-3062-2 **C**6 2 В 4.0 GA MO A С O/C BTC M3 BTO M3 PIT Y2 Valve Name: SI Cold Leg Injection Valve

Safety Injection (062)

Valve Tag	P&ID	P&ID Coor.	Safety Class	Cat.	Size	Valve Type	Act. Type	Active / Passive	Normal Position	Safety Position	Test Type	Test Freq.	Relief Request	Deferred Just.	Tech. Pos.
MOV-4-843B	5614-M-3062-2	D6	2	В	4.0	GA	мо	A	С	O/C	BTC	МЗ			
											BTO	M3			
	Valve Name:	SI Co	ld Leg I	injecti	ion Val	ve					PIT	Y2			
MOV-4-856A	5614-M-3062-1	B1	2	В	2.0	GL	мо	A		0/C	BTC	cs		CSJ-05	TPv-09
											PIT	Y2			
	Valve Name:	HSSI	Pump I	Recirc	ulatio	n to RW	ST								
MOV-4-856B	5614-M-3062-1	B1	2	В	2.0	GL	мо	A	0	O/C	BTC	cs		CSJ-05	TPv-09
											PIT	Y2			
	Valve Name:	HSSI	Pump I	Recirc	ulatio	n to RW	ST							_	
MOV-4-864A	5614-M-3062-1	C4	2	В	16.0	GA	мо	A	0	O/C	BTC	CS		CSJ-06	TPv-09
											PIT	Y2			
	Valve Name:	RWS	l Outlei	t Isola	tion V	alve									
MOV-4-864B	5614-M-3062-1	C4	2	В	16.0	GA	мо	A	0	O/C	BTC	CS		CSJ-06	TPv-09
											PIT	Y2			
	Valve Name:	RWSI	[Outle	t Isola	tion V	alve									
MOV-4-866A	5614-M-3062-1	D7	1	A	2.0	GA	мо	A	С	O/C	BTC	CS		CSJ-03	
											BTO	CS		CSJ-03	
											PIT	Y2			
	Valve Name:	Loop	A Hot I	_eg Sa	afety Ir	njection	Isolatic	n Valve							
MOV-4-866B	5614-M-3062-1	F7	1	A	2.0	GA	МО	A	С	O/C	BTC	CS		CSJ-03	
									•		BTO	CS		CSJ-03	
				-							PIT	Y2			
	Valve Name:	Loop	B Hot I	_eg Sa	afety Ir	ijection	Isolatic	on Valve			•	_			
MOV-4-869	5614-M-3062-1	E6	2	В	3.0	GA	мо	A	С	0/C	BTC	М3			
											BTO	M3			
											PIT	Y2			
	Valve Name:	Loop	A & B I	Hot Le	eg Safe	ety Injec	tion Va	ive		_					
RV-4-6511	5614-M-3062-1	F7	2	С	0.25	RV	SA	A	с	O/C	RT	Y10			
	Valve Name:	Safety	y Inject	ion He	ot Leg	Relief V	alve								
RV-4-857	5614-M-3062-2	C4	2	С	0.75	RV	SA	A		O/C	RT	Y10			

Safety Injection (062)

				Safe	ty Inj	ection	Accu	mulator	rs (064)				IST Pro Valve 1	ogram Pla Fable	n
Valve Tag	P&ID	P&ID Coor.	Safety Class	Cat.	Size	Valve Type	Act. Type	Active / Passive	Normal Position	Safety Position	Test Type	Test Freq.	Relief Request	Deferred Just.	Tech. Pos.
3-873A	5613-M-3064-1	B2	1	A/C	2.0	СК	SA	A	SYS	O/C	AT-02	Y2			
											cc	RR		RJ-08	TPv-08
	Valve Name:	Loop	A Cold	l Leg E	Branch	Line C	heck Va	llve			CO	RR		RJ-08	
3-873B		B2	1	A/C	2.0	СК	SA	A	SYS	0/C	AT-02	Y2			
											сс	RR		RJ-08	TPv-08
											со	RR		RJ-08	
	Valve Name:	Loop	B Cold	l Leg E	Branch	Line C	heck Va	lve							
3-873C	5613-M-3064-1	B2	1	A/C	2.0	СК	SA	A	SYS	O/C	AT-02	Y2			
											CC	RR		RJ-08	TPv-08
											со	RR		RJ-08	
	Valve Name:	Loop	C Cold	I Leg E	Branch	Line C	heck Va								
3-875A	5613-M-3064-1	D8	1	A/C	10.0	СК	SA	A	SYS	O/C	AT-02	Y2			
											CCF	СМ		CSJ-07	TPv-08,02
							·				COA	СМ		RJ-09	TPv-02
	Valve Name:	Loop	A Cold	l Leg !	njectic	on Chec	k Valve				COF	СМ		RJ-09	TPv-02
3-875B	5613-M-3064-1	E8	 1	A/C	10.0	СК	SA	A	SYS	0/C	AT-02	Y2	<u> </u>		
											CCF	СМ		CSJ-07	TPv-08
											COA	СМ		RJ-09	TPv-02
											COF	СМ		RJ-09	TPv-02
	Valve Name:	Loop	B Cold	l Leg l	njectio	on Chec	k Valve							·	
3-875C	5613-M-3064-1	E8	1	A/C	10.0	СК	SA	A	SYS	0/C	AT-02	Y2			
											CCF	СМ		CSJ-07	TPv-08
											COA	СМ		RJ-09	TPv-02
											COF	СМ		RJ-09	TPv-02
	Valve Name:	Loop	C Cold	l Leg l	njectio	on Chec	k Valve		_		_				_
3-875D	5613-M-3064-1	C7	1	С	10.0	СК	SA	A	SYS	O/C	CCF	СМ		RJ-10	TPv-08,02
											COA	СМ			TPv-08,02
											COF	СМ		RJ-10	TPv-08,02
	Valve Name:	SI Ac	cumula	ator 3A	Chec	k Valve									

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	Valve Tag	P&ID	P&ID Coor.	Safety Class	Cat.	Size	Valve Type	Act. Type	Active / Passive	Normal Position	Safety Position	Test Type	Test Freq.	Relief Request	Deferred Just.	Tech. Pos.
	3-875E	5613-M-3064-1	G5	1	С	10.0	СК	SA	A	SYS	 O/C	CCF	СМ		RJ-10	TPv-08,02
												COA	СМ			TPv-08,02
												COF	СМ		RJ-10	TPv-08,02
		Valve Name:	SI Acc	cumula	itor 3E	Chec	k Valve									
	3-875F	5613-M-3064-1	G3	1	С	10.0	СК	SA	A	SYS	0/C	CCF	СМ		RJ-10	TPv-08,02
)												COA	СМ			TPv-08,02
												COF	СМ		RJ-10	TPv-08,02
		Valve Name:	SI Ac	cumula	itor 30	Chec	k Valve									
	3-876A	5613-M-3064-1	H7	1	A/C	8.0	СК	SA	A	SYS	0/C	AT-02	Y2			
												СС	CS		CSJ-08	TPv-08
												со	RR		RJ-19	
		Valve Name:	RHR	Cold Le	eg Inje	ction (Check V	alve								
	3-876B	5613-M-3064-1	G5	1	A/C	8.0	СК	SA	A	SYS	O/C	AT-02	Y2			
												СС	CS		CSJ-08	TPv-08
												со	RR		RJ-19	
		Valve Name:	RHR	Cold Le	eg Inje	ction (Check V	alve								
	3-876C	5613-M-3064-1	G3	1	A/C	8.0	СК	SA	A	SYS	O/C	AT-02	Y2	-		
												CC	CS		CSJ-08	TPv-08
												CO	RR		RJ-19	
		Valve Name:	RHR	Cold Le	eg Inje	ction (Check V	alve								
	3-876D	5613-M-3064-1	G5	1	A/C	8.0	СК	SA	A	SYS	O/C	AT-02	Y2			
												CC	RR		RJ-12	TPv-08
												со	RR		RJ-12	
		Valve Name:	Alterr	ate Lo	w Hea	d Injec	ction Lin	e Chec	k Valve							
	3-876E	5613-M-3064-1	G3	1	A/C	8.0	СК	SA [†]	A	SYS	O/C	AT-02	Y2			
												CC	RR		RJ-12	TPv-08
												со	RR		RJ-12	
		Valve Name:	Altern	ate Lo	w Hea	d Injec	ction Lin	e Chec	k Valve							
	3-945E	5613-M-3064-1	B2	2	A/C	1.0	SCK	SA	A	SYS	С	AT-01	App-J			
												СС	RR	VR-01	RJ-18	TPv-08
												со	RR	VR-01	RJ-18	TPv-01
ノ		Valve Name:	N2 Su	ipply to	o Accu	mulate	ors Che	ck Valv	e							

Safety Injection Accumulators (064)

				Safe	ty Inj	ection	Accu	mulator	rs (064)				וST Pro Vaive ל	ogram Plan Table	1
Valve Tag	P&ID	P&ID Coor.	Safety Class	Cat.	Size	Vaive Type	Act. Type	Active / Passive	Normal Position	Safety Position	Test Type	Test Freq.	Relief Request	Deferred Just.	Tech. Pos.
CV-3-851A	5613-M-3064-1	C7	2	В	1.0	GL	AO	A	С	с	BTC	МЗ			
											FC	M3			TPv-04
	Valve Name:	3A Ac	cumula	ator M	lakeup	Valve					PIT	Y2			
CV-3-851B	 5613-M-3064-1	C5	2	В	1.0	GL	AO	A	С	С	BTC	<u>_</u> МЗ			
											FC	МЗ			TPv-04
							·				PIT	Y2			
_	Valve Name:	3B Ad	cumula	ator N	lakeup	Valve									
CV-3-851C	5613-M-3064-1	C3	2	В	1.0	GL	AO	A	С	С	BTC	МЗ			
											FC	МЗ			TPv-04
											PIT	Y2			
	Valve Name:	3C Ac	cumul	ator N	lakeup	Valve									
MOV-3-744A	5613-M-3064-1	Н3	2	В	10.0	GA	MO	A	С	 0/C	BTC	CS		CSJ-14	
											BTO	CS		CSJ-14	
·											PIT	Y2			
	Valve Name:	RHR	Discha	rge to	Cold I	eg Isol	ation Va	alve							
MOV-3-744B	5613-M-3064-1	G3	2	В	10.0	GA	MO	A	С	0/C	BTC	 CS		CSJ-14	
											BTO	CS		CSJ-14	
											PIT	Y2			
	Valve Name:	RHR	Discha	rge to	Cold I	_eg Isol	ation Va	alve							
MOV-3-865A	5613-M-3064-1	F6	2	В	10.0	GA	мо	A	0	0/C	BTC	CS		CSJ-15	TPv-09
											ΡΙΤ	Y2			
	Valve Name:	SI 3A	Accum	nulato	r Discł	narge Is	olation	Valve							
MOV-3-865B	5613-M-3064-1	F4	2	В	10.0	GA	мо	A	0	0/C	BTC	CS		CSJ-15	 TPv-09
											PIT	Y2			
	Valve Name:	SI 3B	Accum	nulato	r Discł	narge Is	olation	Valve							
MOV-3-865C	5613-M-3064-1	F2	2	B	10.0	GA	мо		0	0/C	BTC	CS	<u>.</u>	CSJ-15	TPv-09
											РП	Y2			
	Valve Name:	SI 3C	Accum	nulato	r Disct	narge Is	olation	Valve							
RV-3-706	5613-M-3064-1	G2	2	С	2.0	RV	SA	A	с	0/C	RT	Y10			<u>.</u>
	Valve Name:	RHR	to SI Co	old Le	g Relie	ef Valve									•

Turkey Point Nuclear Plant

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Safety Injection Accumulators (064)

Valve Tag	P&ID	P&ID Coor.	Safety Class	Cat.	Size	Valve Type	Act. Type	Active I Passive	Normal Position	Safety Position	Test Type	Test Freq.	Relief Request	Deferred Just.	Tecl Pos
RV-3-858A	5613-M-3064-1 Valve Name:	D6 SI 3A	2 Accum	C Iulatoi	2.0 Relie	RV f Valve	SA	A	С	O/C	RT	Y10			-
RV-3-858B	5613-M-3064-1	D4	2	С	2.0	RV	SA	A	С	O/C	RT	Y10			
	Valve Name:	SI 3B	Accum	ulato	r Relie	f Valve									
RV-3-858C	5613-M-3064-1	D2	2	С	2.0	RV	SA	A	С	O/C	RT	Y10			
	Valve Name:	SI 3C	Accum	ulato	r Relie	f Valve									
4-873A ·	5614-M-3064-1	B2	1	A/C	2.0	СК	SA	A	SYS	O/C	AT-02	Y2			
											СС	RR		RJ-08	TP
											со	RR		RJ-08	
	Valve Name:	Loop	A Cold	Leg E	Branch	Line Cl	neck Va	lve							
4-873B	5614-M-3064-1	B2	1	A/C	2.0	СК	SA	A	SYS	O/C	AT-02	Y2			
											CC	RR		RJ-08	TP۱
											со	RR		RJ-08	
	Valve Name:	Loop	B Cold	Leg E	Branch	Line Cl	heck Va	lve							
4-873C	5614-M-3064-1	B2	1	A/C	2.0	СК	SA	A	SYS	O/C	AT-02	Y2			
											CC	RR		RJ-08	TP
											со	RR		RJ-08	
	Valve Name:	Loop	C Cold	Leg E	Branch	Line Cl	heck Va	lve							<u></u>
4-875A	5614-M-3064-1	D8	1	A/C	10.0	СК	SA	Α	SYS	O/C	AT-02	Y2			
											CCF	СМ		CSJ-07	TP۱
											COA	СМ		RJ-09	TP
					•	<u> </u>					COF	СМ		RJ-09	TP
<u> </u>	Valve Name:	Loop	A Cold	Leg li	njectic	n Checi	k Valve								
4-875B	5614-M-3064-1	E8	1	A/C	10.0	СК	SA	A	SYS	O/C	AT-02	Y2			
											CCF	CS		CSJ-07	TP
											COA	СМ		RJ-09	TP۱
	Mal	• • •			• .•	<u>.</u>					COF	СМ		RJ-09	TP
	valve Name:	L00p	B Cold	Legi	njectio	on Checi	k Valve				- <u>.</u>				
4-875C	5614-M-3064-1	E8	1	A/C	10.0	СК	SA	A	SYS	O/C	AT-02	Y2			
											CCF	CS		CSJ-07	TP۱
											COA	СМ		RJ-09	TP
	Value Norres	1.00	0.0-1-1	1.0-1	nia chi -		L \/a				COF	СМ		RJ-09	TP
	Valve Name:		C Cold	Leg l	njectic ———	on Chec	k Valve								

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	Valve Tag	P&ID	P&ID Coor.	Safety Class	Cat.	Size	Valve Type	Act. Type	Active / Passive	Normal Position	Safety Position	Test Type	Test Freq.	Relief Request	Deferred Just.	Tech. Pos.
	4-875D	5614-M-3064-1	G7	1	С	10.0	СК	SA	A	SYS	O/C	CCF	СМ		RJ-10	TPv-08,02
												COA	СМ			TPv-08,02
												COF	СМ		RJ-10	TPv-08,02
		Valve Name:	SI Aco	cumula	tor 4A	Chec	k Valve									
	4-875E	5614-M-3064-1	G5	1	С	10.0	СК	SA	A	SYS	O/C	CCF	СМ		RJ-10	TPv-08,02
												COA	СМ			TPv-08,02
												COF	СМ		RJ-10	TPv-08,02
		Valve Name:	SI Ac	cumula	tor 4E	Chec	k Valve									
	4-875F	5614-M-3064-1	G3	1	с	10.0	СК	SA	A	SYS	O/C	CCF	СМ		RJ-10	TPv-08,02
												COA	СМ			TPv-08,02
												COF	СМ		RJ-10	TPv-08,02
		Valve Name:	SI Ace	cumula	tor 40	Chec	k Valve									
	4-876A	5614-M-3064-1	H7	1	A/C	8.0	СК	SA	A	SYS	O/C	AT-02	Y2			·
												СС	CS		CSJ-08	TPv-08
												со	RR		RJ-19	
		Valve Name:	RHR	Cold Le	eg Inje	ction (Check V	alve								
	4-876B	5614-M-3064-1	G5	1	A/C	8.0	ск	SA	A	SYS	O/C	AT-02	Y2			
												СС	CS		CSJ-08	TPv-08
												со	RR		RJ-19	
		Valve Name:	RHR	Cold Le	eg Inje	ction (Check V	alve								
	4-876C	5614-M-3064-1	G3	1	A/C	8.0	СК	SA	A	SYS	O/C	AT-02	Y2			
												cc	CS		CSJ-08	TPv-08
												со	RR		RJ-19	
/		Valve Name:	RHR	Cold Le	eg Inje	ction (Check V	alve								
	4-876D	5614-M-3064-1	G5	1	A/C	8.0	СК	SA	A	SYS	O/C	AT-02	Y2			
												СС	RR		RJ-12	TPv-08
												со	RR		RJ-12	
		Valve Name:	Altern	ate Lo	w Hea	d Injed	ction Lin	e Chec	k Valve							
	4-876E	5614-M-3064-1	G5	1	A/C	8.0	СК	SA	A	SYS	O/C	AT-02	Y2			
												СС	RR		RJ-12	TPv-08
												со	RR		RJ-12	
)		Valve Name:	Alterr	ate Lo	w Hea	d Injed	ction Lin	e Chec	k Valve							

Safety Injection Accumulators (064)
Valve Tag	P&ID	P&ID Coor.	Safety Class	Cat.	Size	Valve Type	Act. Type	Active / Passive	Normal Position	Safety Position	Test Type	Test Freq.	Relief Request	Deferred Just.	Tech. Pos.
4-945E	5614-M-3064-1	C2	2	A/C	1.0	СК	SA	A	SYS	с	AT-01	App-J			
											CC	RR	VR-01	RJ-18	TPv-08
	Valve Name:	N2 Su	ylgaly to	Accu	imulate	ors Che	ck Valv	e			CO	RR	VR-01	RJ-18	TPv-01
<u></u>								<u> </u>						<u> </u>	
CV-4-851A	5614-M-3064-1	C5	2	В	1.0	GL	AO	A	C	C	BIC	M3			70.04
											PIT	V0 V2			124-04
	Valve Name:	48 Ac	cumula	ator M	lakeup	Valve					E II	12			
CV-4-851B	5614-M-3064-1	C7	2	B	1.0	GL	AO	A	с	с	BTC	МЗ		<u>-</u>	
											FC	МЗ			TPv-04
											ΡΠ	Y2			
	Valve Name:	4A Ac	cumula	ator M	lakeup	Valve									
CV-4-851C	5614-M-3064-1	СЗ	2	B	1.0	GL	AO	A	C	С	BTC	M3			
			•								FC	M3			TPv-04
											PIT	Y2			
	Valve Name:	4C Ac	cumula	ator M	lakeup	Valve									
MOV-4-744A	5614-M-3064-1	НЗ	2	В	10.0	GA	мо	A	С	0/C	BTC	CS		CSJ-14	
											BTO	CS		CSJ-14	
	Valve Name:	RHR I	Discha	rge to	Cold L	.eg isola	ation Va	alve			PIT	Y2			
					40.0									00144	
MU4-4-144D	30 14-IVI-3004-1	63	2	D	10.0	GA	MU	Ä	U	0/0	BTO	03 09		CSJ-14	
				·							PIT	Y2		000-14	
	Valve Name:	RHRI	Discha	ge to	Cold L	.eg Isola	ation Va	alve							
MOV-4-865A	5614-M-3064-1	F6	2	В	10.0	GA	мо	Α	0	O/C	BTC	CS	·	CSJ-15	TPv-09
											ΡΙΤ	Y2			
	Valve Name:	SI 4A	Accum	ulato	r Disch	arge Is	olation	Valve							
MOV-4-865B	5614-M-3064-1	F4	2	B	10.0	GA	МО	A	0	O/C	BTC	CS		CSJ-15	TPv-09
											PIT	Y2			
	Valve Name:	SI 4B	Accum	ulato	r Discł	arge Is	olation	Valve							
MOV-4-865C	5614-M-3064-1	F2	2	В	10.0	GA	МО	A	0	0/C	BTC	CS		CSJ-15	TPv-09
											ΡΙΤ	Y2			
	Valve Name:	SI 4C	Accum	ulato	r Discł	arge Is	olation	Valve							

Safety Injection Accumulators (064)

Safety Injection Accumulators (064)

Valve Tag	P&ID	P&ID Coor.	Safety Class	Cat.	Síze	Vaive Type	Act. Type	Active / Passive	Normal Position	Safety Position	Test Type	Test Freq.	Relief Request	Deferred Just.	Tech. Pos.
RV-4-706	5614-M-3064-1 Valve Name:	G2 RHR 1	2 10 SI Co	C Did Le	2.0 g Relie	RV ef Valve	SA	A	С	O/C	RT	Y10			
RV-4-858A	5614-M-3064-1 Valve Name:	D6 SI 4A	2 Accum	C Iulatoi	2.0 Relie	RV f Valve	SA	A	С	O/C	RT	Y10			
RV-4-858B	5614-M-3064-1 Valve Name:	D4 SI 4B	2 Accum	C nulato	2.0 Relie	RV f Valve	SA	A	c	O/C	RT	Y10			
RV-4-858C	5614-M-3064-1 Valve Name:	D2 S1 4C	2 Accum	C nulator	2.0 r Relie	RV f Valve	SA	A	C	O/C	RT	Y10			

Valve Tag	P&ID	P&ID Coor.	Safety Class	Cat.	Size	Valve Type	Act. Type	Active / Passive	Normal Position	Safety Position	Test Type	Test Freq.	Relief Request	Deferred Just.	Tech. Pos.
3-3449	5610-M-3065-1	C6	2	A	0.375	GL	MAN	P	LC	с	AT-01	App-J			
	Valve Name:	N2 to	RCDT	PCV-	-1014 \$	Sensing	Line Is	olation V	alve						
3-4639	5610-M-3065-1	C6	2	A	0.75	DIA	MAN	P	LC	С	AT-01	App-J	·		
	Valve Name:	N2 Su	upply to	RCD	T Isola	tion Val	ve								
3-4656	5610-M-3065-1	C7	2	A	1.0	DIA	MAN	Р	LC	С	AT-01	App-J			
	Valve Name:	N2 SL	upply to	RCD	T Isola	tion Val	ve								
3-518	5610-M-3065-1	D7	2	A/C	0.75	СК	SA	A	SYS	С	AT-01	App-J			
											СС	RR	VR-01	RJ-05	
											со	RR	VR-01	RJ-05	TPv-01
	Valve Name:	N2 Si	upply to	Pres	surizer	Relief	Tank Cl	neck Valv	e						
3-519	5610-M-3065-1	D6	2	A/C	0.75	SCK	SA	A	SYS	C	AT-01	App-J			
											СС	RR	VR-01	RJ-05	
											со	RR	VR-01	RJ-05	TPv-01
	Valve Name:	N2 SL	upply to	PRT	Stop C	heck V	alve								
CV-3-855	5610-M-3065-1	E6	2	A	1.0	GA	AO	A	с	с	AT-01	App-J			
											BTC	M3			
											FC	M3			TPv-04
											PIT	Y2			
	Valve Name:	N2 SL	ipply to	SIA	cumul	ators Is	olation	Valve							
4-3449	5610-M-3065-1	A6	2	A	0.375	GL	MAN	P	LC	С	AT-01	App-J			
	Valve Name:	N2 to	RCDT	PCV-	-1014 \$	Sensing	Line Is	olation V	alve						
4-4639	5610-M-3065-1	B6	2	A	0.75	DIA	MAN	. P	LC	с	AT-01	App-J			
	Valve Name:	N2 Si	upply to	RCD	T isola	tion Val	ve				ŗ				
4-4656	5610-M-3065-1	B7	2	A	1.0	DIA	MAN	P	LC	C ·	AT-01	App-J			
	Valve Name:	N2 SL	upply to	RCD	T Isola	tion Val	ve								
4-518	5610-M-3065-1	A7	2	A/C	0.75	СК	SA	Α	SYS	с	AT-01	App-J			
											СС	RR	VR-01	RJ-05	
											со	RR	VR-01	RJ-05	TPv-01
	Valve Name:	N2 Si	ipply to	Pres	surizer	Relief	Tank Cl	neck Valv	e						

Nitrogen and Hydrogen (065)

				N	litrog	en anc	i Hydr	ogen (C)65)				Turkey IST Pro Valve 1	Point Nucl ogram Plan Fable	ear Plan
Valve Tag	P&ID	P&ID Coor.	Safety Class	Cat.	Size	Valve Type	Act. Type	Active / Passive	Normal Position	Safety Position	Test Type	Test Freq.	Relief Request	Deferred Just.	Tech. Pos.
4-519	5610-M-3065-1	A6	2	A/C	0.75	СК	SA	A	SYS	c	AT-01	App-J			
											СС	RR	VR-01	RJ-05	
											СО	RR	VR-01	RJ-05	TPv-01
	Valve Name:	N2 Si	pply to	PRT	Stop C	heck Va	alve								
CV-4-855	5610-M-3065-1	E3	2	A	1.0	GA	AO	A	С	С	AT-01	App-J			
											BTC	МЗ			
											FC	M3			TPv-04
											PIT	Y2			

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Valve Name: N2 Supply to SI Accumulators Isolation Valve

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	Valve Tag	P&ID	P&ID Coor.	Safety Class	Cat.	Size	Vaive Type	Act. Type	Active / Passive	Normal Position	Safety Position	Test Type	Test Freq.	Relief Request	Deferred Just.	Tech. Pos.
	3-883M	5613-M-3068-1	C5	2	A	1.0	GL	MAN	Р	LC	С	AT-01	App-J			
		Valve Name:	Conta	inmen	t Spra	y Pum	p 3A Te	st Line	Isol							
	3-883N	5613-M-3068-1	E5	2	A	1.0	GL	MAN	P	LC	С	AT-01	App-J		<u> </u>	
		Valve Name:	Conta	linmen	t Spra	y Pum	р 3В Те	st Line	Isol							
)	3-890A	5613-M-3068-1	D6	2	A/C	6.0	СК	SA	A	с	O/C	AT-01	App-J			
												CCD	СМ			TPv-02
												COD	СМ			TPv-02
		Valve Name:	Conta	inmen	t Spra	y Pum	p Diach	arge Ch	eck Valv	e						
	3-890B	5613-M-3068-1	G6	2	A/C	6.0	СК	SA	A	С	O/C	AT-01	App-J			
												CCD	СМ			TPv-02
												COD	СМ			TPv-02
		Valve Name:	Conta	linmen	t Spra	y Pum	p Diach	arge Cł	neck Valv	e			_			
	MOV-3-880A	5613-M-3068-1	D5	2	A	6.0	GA	мо	A	c	O/C	AT-01	App-J			
												BTC	М3			
												BTO	M3			
												PIT	Y2			
		Valve Name:	Conta	linmen	t Spra	y Pum	p Disch	arge Iso	plation Va	lve						
	MOV-3-880B	5613-M-3068-1	G5	2	A	6.0	GA	МО	A	C	O/C	AT-01	App-J			
												BTC	М3			
												BTO	M3			
												PIT	Y2			
		Valve Name:	Conta	linmen	t Spra	y Pum	p Disch	arge Iso	olation Va	lve						
	RV-3-871	5613-M-3068-1	C2	2	C	0.75	RV	SA	A	С	O/C	RT	Y10			
		Valve Name:	Conta	inmen	t Spra	y Pum	p Suctio	on Relie	f Valve							
	4-883M	 5614-M-3068-1	C5	2	A	1.0	GL	MAN		LC	C	AT-01	App-J			
		Valve Name:	Conta	inmen	t Spra	y Pum	p Test L	ine Iso	lation Val	ve						
	4-883N	5614-M-3068-1	D5	2	A	1.0	GL	MAN	P	LC	с	AT-01	App-J			
		Valve Name:	Conta	inmen	t Spra	y Pum	p Test L	ine Isol	lation Val	ve						
	4-890A	5614-M-3068-1	C6	2	A/C	6.0	СК	SA	A	c	O/C	AT-01	App-J		<u> </u>	
,												CCD	СМ			TPv-02
												COD	СМ			TPv-02
		Valve Name:	Conta	inmen	t Spra	y Pum	p Diach	arge Ch	neck Valv	e						

Containment Spray (068)

ľ						Con	tainme	ent Sp	ray (06	B)				Turkey IST Pro Valve 1	Point Nucl ogram Plan Table	lear Plant
	Valve Tag	P&ID	P&ID Coor.	Safety Class	Cat.	Size	Valve Type	Act. Type	Active / Passive	Normal Position	Safety Position	Test Type	Test Freq.	Relief Request	Deferred Just.	Tech. Pos.
	4-890B	5614-M-3068-1	F6	2	A/C	6.0	СК	SA	A	С	O/C	AT-01	App-J			
												CCD	СМ			TPv-02
												COD	СМ			TPv-02
		Valve Name:	Conta	ainmen	t Spra	y Pum	p Diach	arge Ch	neck Valv	e						
	MOV-4-880A	5614-M-3068-1	C5	2	A	6.0	GA	MO	A	С	O/C	AT-01	App-J			
												BTC	МЗ			
												BTO	M3			
												PIT	Y2			
		Valve Name:	Conta	ainmen	t Spra	y Pum	p Disch	arge Ise	olation Va	lve						
	MOV-4-880B	5614-M-3068-1	F5	2	A	6.0	GA	мо	A	С	O/C	AT-01	App-J			
												BTC	М3			
												BTO	М3			
												PIT	Y2			
		Valve Name:	Conta	ainmen	t Spra	y Pum	p Disch	arge iso	olation Va	alve						
	RV-4-871	5014-M-3068-1	G2	2	С	0.75	RV	SA	A	с	O/C	RT	Y10		-	
		Valve Name:	Conta	ainmen	t Spra	y Pum	p Suctio	on Relie	f Valve							

P&ID Safety Valve Act. Active I Normal Safety Test Test Relief Deferred Tech. Coor. Class Size Request Cat. Position Position Freq. Passive Туре Just. Pos. Type Type Valve Tag P&ID CSJ-12 3-10-004 5613-M-3072-1 G7 26.0 СК SA A SYS С CC CS SR С CO M3 TPv-01 Main Steam Header A Check Valve Valve Name: SYS С CSJ-12 3-10-005 5613-M-3072-1 D7 SR С 26.0 СК SA А CC CS MЗ CO TPv-01 Valve Name: Main Steam Header B Check Valve 3-10-006 SYS С CSJ-12 5613-M-3072-1 **B**7 SR С 26.0 СК SA A CC CS CO M3 TPv-01 Valve Name: Main Steam Header C Check Valve CV-3-1606 5613-M-3072-1 F4 2 6.00 GL AO A С O/C CS CSJ-13 В BTC BTO CS CSJ-13 FC CS CSJ-13 TPv-04 Valve Name: Atmosheric Steam Dump A CV-3-1607 5613-M-3072-1 D4 2 6.00 GL AO A С O/C BTC cs CSJ-13 в CS CSJ-13 BTO FC CS **CSJ-13** TPv-04 Valve Name: Atmosheric Steam Dump B CV-3-1608 С O/C 5613-M-3072-1 **B**4 2 GL AO A BTC CS **CSJ-13** в 6.00 CS **CSJ-13** BTO CS CSJ-13 FC TPv-04 Valve Name: Atmosheric Steam Dump C MOV-3-1400 5613-M-3072-1 F6 2 В 2.00 GL MO A С С BTC M3 PIT M3 Valve Name: **MSIV A Bypass Isolation Valve** С С MOV-3-1401 5613-M-3072-1 D6 2 В 2.00 GL MO A BTC M3 PIT M3 Valve Name: **MSIV B Bypass Isolation Valve** MOV-3-1402 5613-M-3072-1 **B**6 2 2.00 GL MO Α С С BTC M3 В PIT M3 Valve Name: **MSIV C Bypass Isolation Valve**

Main Steam System (072)

Main Steam System (072)

	Valve Tag	P&ID	P&ID Coor.	Safety Class	Cat.	Size	Valve Type	Act. Type	Active / Passive	Normal Position	Safety Position	Test Type	Test Freq.	Relief Request	Deferred Just.	Tech. Pos.
	POV-3-2604	5613-M-3072-1	G6	2	В	26.0	СК	AO	A	0	С	BTC	CS Y2		CSJ-30	
		Valve Name:	Main	Steam	Heade	er A Iso	olation \	/alve								
	POV-3-2605	5613-M-3072-1	D6	2	B	26.0	СК	OA	A	0	С	BTC	CS Y2		CSJ-30	_
/		Valve Name:	Main	Steam	Heade	er B Iso	olation \	/alve								
	POV-3-2606	5613-M-3072-1	B6	2	B	26.0	СК	AO	A	0	c	BTC	CS Y2		CSJ-30	
		Valve Name:	Main	Steam	Heade	er C Iso	olation \	/alve								
	RV-3-1400	5613-M-3072-1 Valve Name:	G5 Main 3	2 Steam	B Heade	6.00 er A - \$	RV Safety V	SA aive	A	C	O/C	RT	Y5			
ł	RV-3-1401	5613-M-3072-1 Valve Name:	G5 Main :	2 Steam	B Heade	6.00 er A - \$	RV Safety V	SA alve	A	С	O/C	RT	¥5			
	RV-3-1402	5613-M-3072-1 Valve Name:	H5 Main S	2 Steam	B Heade	6.00 er A - 3	RV Safety V	SA Zalve	A	С	O/C	RT	¥5			
	RV-3-1403	5613-M-3072-1 Valve Name:	F5 Main S	2 Steam	B Heade	6.00 er A - \$	RV Safety V	SA 'alve	A	С	O/C	RT	Y5			
	RV-3-1405	5613-M-3072-1 Valve Name:	E5 Main S	2 Steam	B Heade	6.00 er B - 3	RV Safety V	SA 'alve	A	С	O/C	RT	¥5			
,	RV-3-1406	5613-M-3072-1 Valve Name:	D5 Main S	2 Steam	B Heade	6.00 er B - 1	RV Safety V	SA 'alve	A	C	O/C	RT	Y5		<u></u>	
	RV-3-1407	5613-M-3072-1 Valve Name:	E5 Main :	2 Steam	B Heade	6.00 er B - 3	RV Safety V	SA 'alve	A	С	O/C	RT	¥5	·		
	RV-3-1408	5613-M-3072-1 Valve Name:	D5 Main S	2 Steam	B Heade	6.00 er B - \$	RV Safety V	SA alve	A	С	O/C	RT	Y5	-		
	RV-3-1410	5613-M-3072-1 Valve Name:	B5 Main :	2 Steam	B Heade	6.00 er C - 3	RV Safety V	SA Valve	A	С	O/C	RT	¥5			
/	RV-3-1411	5613-M-3072-1 Valve Name:	B5 Main :	2 Steam	B Heade	6.00 er C - 3	RV Safety V	SA Zalve	A	С	O/C	RT	¥5			

Main Steam System (072)

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Valve Tag	P&ID	P&ID Coor.	Safety Class	Cat.	Size	Valve Type	Act. Type	Active / Passive	Normal Position	Safety Position	Test Type	Test Freq.	Relief Request	Deferred Just.	Tech. Pos.
RV-3-1412	5613-M-3072-1	C5	2	В	6.00	RV	SA	A	С	O/C	RT	Y5			
	Valve Name:	Main	Steam	Heade	rC-S	Safety V	alve								
RV-3-1413	5613-M-3072-1	A5	2	В	6.00	RV	SA	A	С	0/C	RT	Y5			
	Valve Name:	Main	Steam	Heade	rC-S	Safety V	alve								
4-10-004	5614-M-3072-1	G6	SR	С	26.0	СК	SA	A	SYS	с	сс	CS	<u> </u>	CSJ-12	
	Valve Name:	Main	Steam	Heade	er A Ch	eck Val	ve	·			CO	М3			TPv-01
4-10-005	5614-M-3072-1	D6	SR	С	26.0	СК	SA	A	SYS	c	сс	CS		CSJ-12	
	Valve Name:	Main	Steam	Heade	r B Ch	ieck Val	ve				со	М3	·		TPv-01
4-10-006	5614-M-3072-1	B6	SR	С	26.0	СК	SA	A	SYS	с	СС	CS		CSJ-12	
	Valve Name:	Main	Steam	Heade	er C Ch	ieck Val	ve				CO	М3			TPv-01
CV-4-1606	5614-M-3072-1	F4	2	В	6.00	GL	AO	A	С	O/C	BTC	CS		CSJ-13	
											BTO	CS		CSJ-13	
	Valve Name:	Atmo	sheric \$	Steam	Dump	A					FC	CS		CSJ-13	TPv-04
CV-4-1607		D4	2	В	6.00	GL	AO	A	с	O/C	BTC	cs		CSJ-13	
											BTO	CS		CSJ-13	
	Valve Name:	Atmo	sheric \$	Steam	Dump	B					FC	CS		CSJ-13	_TPv-04
CV-4-1608	5614-M-3072-1	B4	2	В	6.00	GL	AO	A	с	O/C	BTC	CS		CSJ-13	
											BTO	CS		CSJ-13	
	Valve Name:	Atmo	sheric \$	Steam	Dump	C					FC	CS		CSJ-13	TPv-04
MOV-4-1400	 5614-M-3072-1	F 6	2	В	2.00	GL	мо		c	с	BTC	МЗ			
											PIT	M3			
	Valve Name:	MSIV	А Вура	iss Isc	olation	Valve									
MOV-4-1401	5614-M-3072-1	D6	2	В	2.00	GL	мо	A	С	с	BTC	M3			
	Valve Name:	MSIV	В Вура	iss Isa	olation	Valve					PIT	М3			

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Main Steam System (072)

Valve Tag	P&ID	P&ID Coor.	Safety Class	Cat.	Size	Valve Type	Act. Type	Active / Passive	Normal Position	Safety Position	Test Type	Test Freq.	Relief Request	Deferred Just.	Tech. Pos.
MOV-4-1402	5614-M-3072-1	A6	2	B	2.00	GL	мо	A	C	С	BTC	M3 M3			
	Valve Name:	MSIV	С Вура	iss Iso	olation	Valve					r ii				
POV-4-2604	5614-M-3072-1	G6	2	В	26.0	СК	AO	A	0	C	BTC	CS		CSJ-30	
	Valve Name:	Main	Steam I	Heade	er A Iso	plation \	/alve				PIT	Y2			
POV-4-2605	5614-M-3072-1	D6	2	В	26.0	СК	AO	A	0	С	BTC	CS		CSJ-30	
	Valve Name:	Main	Steam	Heade	er B Iso	plation \	/alve		:		PIT	Y2			
POV-4-2606	5614-M-3072-1	B6	2	В	26.0	СК	AO	A	0	С	BTC	CS		CSJ-30	
	Valve Name:	Main	Steam	Heade	er C Iso	olation \	/alve				PIT	Y2			
RV-4-1400	5614-M-3072-1	G5	2	В	6.00	RV	SA	A	с	O/C	RT	Y5	<u></u>		
	Valve Name:	Main	Steam i	Heade	er A - S	Safety V	'alve								
RV-4-1401	5614-M-3072-1	G5	2	В	6.00	RV	SA	A	С	O/C	RT	¥5			
	Valve Name:	Main	Steam	Heade	er A - 1	Safety V	alve								
RV-4-1402	5614-M-3072-1	H5	2	В	6.00	RV	SA	A	С	O/C	RT	Y5			
	Valve Name:	Main	Steam	Heade	er A - S	Safety V	alve								
RV-4-1403	5614-M-3072-1	F5	2	В	6.00	RV	SA	A	С	0/C	RT	¥5		·	
	Valve Name:	Main	Steam	Heade	er A - S	Safety V	'aive								
RV-4-1405	5614-M-3072-1	E5	2	В	6.00	RV	SA	A	· C	0/C	RT	Y5			
	Valve Name:	Main	Steam	Heade	er B - S	Safety V	alve								
RV-4-1406	5614-M-3072-1	D5	2	B	6.0 ⁰	RV	SA	A	С	O/C	RT	Y5			
	Valve Name:	Main	Steam	Heade	er B - S	Safety V	alve								
RV-4-1407	5614-M-3072-1	E5	2	В	6.00	RV	SA	A	С	O/C	RT	Y5			
	Valve Name:	Main	Steam	Heade	er B - 3	Safety V	alve								
RV-4-1408	5614-M-3072-1	D5	2	В	6.00	RV	SA	A	с	0/C	RT	Y5			
	Valve Name:	Main	Steam	Heade	er B - S	Safety V	/alve								

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Main Steam System (072)

Valve Tag	P&ID	P&ID Coor.	Safety Class	Cat.	Size	Valve Type	Act. Type	Active / Passive	Normal Position	Safety Position	Test Type	Test Freq.	Relief Request	Deferred Just.	Tech. Pos.
RV-4-1410	5614-M-3072-1 Valve Name:	B5 Main	2 Steam	B Heade	6.00 er C - 3	RV Safety V	SA alve	A	С	O/C	RT	¥5			
RV-4-1411	5614-M-3072-1 Valve Name:	B5 Main	2 Steam	B Heade	6.00 er C - 3	RV Safety V	SA alve	A	c	0/C	RT	¥5			
RV-4-1412	5614-M-3072-1 Valve Name:	C5 Main	2 Steam	B Heade	6.00 er C - 3	RV Safety V	SA alve	A	C	O/C	RT	¥5			
RV-4-1413	5614-M-3072-1 Valve Name:	A5 Main	2 Steam	B Heade	6.00 er C - 3	RV Safety V	SA aive	A	C	O/C	RT	¥5			

Blowdown (074)

Valve Tag	P&ID	P&ID Coor.	Safety Class	Cat.	Size	Valve Type	Act. Type	Active / Passive	Normal Position	Safety Position	Test Type	Test Freq.	Relief Request	Deferred Just.	Tech. Pos.
CV-3-6275A	5613-M-3074-4	G2	2	В	6.0	GL	OA	A	0	С	BTC	МЗ			
	Valve Name:	3A St	eam Ge	enerati	or Blo	wdown	Stop Va	lve			PIT	Y2			
CV-3-6275B	5613-M-3074-4	E2	2	В	6.0	GL	AO	A	0	С	BTC	M3			
											PIT	Y2			
	Valve Name:	3B St	eam Ge	enerat	or Blo	wdown	Stop Va	lve							
CV-3-6275C	5613-M-3074-4	C2	2	В	6.0	GL	AO	A	0	С	BTC	MЗ			
•											PIT	Y2			
	Valve Name:	3C St	eam Ge	enerat	or Blo	wdown	Stop Va	lve							
MOV-3-1425	5613-M-3032-1	D2	2	В	1.0	GA	МО	A	0	С	BTC	M3			
											PIT	Y2			
	Valve Name:	3C St	eam Ge	enerat	or Liqu	uid Sam	ple Val	/e							
MOV-3-1426	5613-M-3032-1	C2	2	B	1.0	GA	мо	A	0	с	BTC	M3			
											PIT	Y2			
	Valve Name:	3B St	eam Ge	enerat	or Liqı	uid Sam	ple Valv	/e							
MOV-3-1427	5613-M-3032-1	A2	2	в	1.0	GA	МО	A	0	C	BTC	M3			
											PIT	Y2			
	Valve Name:	3A St	eam Ge	enerat	or Liqu	uid Sam	ple Valv	/e							
CV-4-6275A	5614-M-3074-4	G2	2	В	6.0	GL	AO	A	0	c	BTC	M3			
											PIT	Y2			
	Valve Name:	4A St	eam Ge	enerat	or Blov	wdown	Stop Va	lve							
CV-4-6275B	5614-M-3074-4	E2	2	В	6.0	GL	AO	A	0	с	BTC	M3			
											PIŢ	Y2			
	Valve Name:	4B St	eam Ge	enerat	or Blo	wdown	Stop Va	live							
CV-4-6275C	5614-M-3074-4	C2	2	В	6.0	GL	AO	A	0	c	BTC	M3	···-		
											PIT	Y2			
	Valve Name:	4C St	eam Ge	enerat	or Blo	wdown	Stop Va	lve	·						
MOV-4-1425	5614-M-3032-1	D2	2	в	1.0	GA	МО	A	0	С	BTC	M3			
											PIT	Y2			
	Valve Name:	4C St	eam Ge	enerat	or Liqu	uid Sam	pie Val	/e							

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Blowdown (074)

Valve Tag	P&ID	P&ID Coor.	Safety Class	Cat.	Size	Valve Type	Act. Type	Active / Passive	Normal Position	Safety Position	Test Type	Test Freq.	Relief Request	Deferred Just.	Tech. Pos.
MOV-4-1426	5614-M-3032-1	C3	2	в	1.0	GA	мо	A	0	С	BTC	M3			
											PIT	Y2			
	Valve Name:	4B St	eam Ge	enerat	or Liqu	uid Sam	ple Val	/e							
MOV-4-1427	5614-M-3032-1	A2	2	В	1.0	GA	MO	A	0	С	BTC	M3			
											PIT	Y2			
	Valve Name:	44 St	aam Ge	norat	ortia	uid Sam	nla Vali								

Valve Tag	P&ID	P&ID Coor.	Safety Class	Cat.	Size	Valve Type	Act. Type	Active I Passive	Normal Position	Safety Position	Test Type	Test Freq.	Relief Request	Deferred Just.	Tech. Pos.
3-20-137	5613-M-3074-3	G6	2	С	0.50	СК	SA	A	SYS	c	СС	M3			
	Valve Name:	A S/G	FW ch	em In	jectior	n Check	Valve				co	М3			TPv-01
3-20-237	5613-M-3074-3	E6	2	С	0.50	СК	SA	A	SYS	c	CC	М3		_	
	Valve Name:	B S/G	FW ch	iem In	jectior	n Check	Valve				со	МЗ			TPv-01
3-20-337	5613-M-3074-3	B6	2	С	0.50	СК	SA	A	SYS	С	CC	М3			
	Valve Name:	C S/G	FW ch	em In	jectior	n Check	Valve	·			CO	М3			TPv-01
FCV-3-478	5613-M-3074-3	G4	2	В	12.0	GL	AO	A	0	с	BTC	cs		CSJ-17	
											FC	CS		CSJ-17	
	Valve Name:	A S/G	FW Co	ontrol	Valve						PIT	Y2			
FCV-3-479	 5613-M-3074-3	нз	2	В	4.0	GA	AO	A	с	С	BTC	CS		 CSJ-18	
											FC	CS		CSJ-18	TPv-04
	Valve Name:	A S/G	FW FC	:V By	oass V	alve					рIT	Y2			
FCV-3-488	5613-M-3074-3	D4	2	В	12.0	GL	AO	A	0	с	BTC	CS		 CSJ-17	
											FC	CS		CSJ-17	
	Valve Name:	B S/G	FW Co	ontrol	Valve						Pit	Y2			
FCV-3-489	5613-M-3074-3	E3	2	В	4.0	GA	AO	A	c	с	BTC	cs		CSJ-18	
											FC	CS		CSJ-18	TPv-04
	Valve Name:	B S/G	FW FC	V By	pass V	alve					PIT	Y2			
												_			
FCV-3-498	5613-M-3074-3	B4	2	B	12.0	GL	AO	A	0	С	BTC	CS		CSJ-17	
											FC	CS		CSJ-17	
	Valve Name:	C S/G	FW Co	ontrol	Valve						Pli	¥2			
FCV-3-499	5613-M-3074-3	СЗ	2	В	4.0	GA	AO	A	c	С	BTC	CS		CSJ-18	
											FC	CS		CSJ-18	TPv-04
	Valve Name:	C S/G	FW FC	CV By	pass V	alve					PIT	Y2			

Main Feedwater (074a)

Valve Tag	P&ID	P&ID Coor.	Safety Class	Cat.	Size	Valve Type	Act. Type	Active / Passive	Normal Position	Safety Position	Test Type	Test Freq.	Relief Request	Deferred Just.	Tech. Pos.
4-20-137	5614-M-3074-3	G6	2	С	0.50	СК	SA	A	SYS	С	CC	M3			
	Valve Name:	A S/G	FW ch	em Inj	jectior	n Check	Valve				со	M3			TPv-01
4-20-237	5614-M-3074-3	D6	2	С	0.50	СК	SA	A	SYS	С	СС	M3			
	Valve Name:	B S/G	FW ch	iem In	jectior	n Check	Valve				CO	М3			TPv-01
4-20-337	5614-M-3074-3	B6	2	С	0.50	СК	SA	A	SYS	с	СС	M3			
	Valve Name:	C S/G	FW ch	iem In	jectior	n Check	Valve				CO	М3			TPv-01
FCV-4-478	5614-M-3074-3	G4	2	В	12.0	GL	AO	A	0	С	BTC	cs		CSJ-17	
											FC	CS		CSJ-17	
	Valve Name:	A S/G	FW Co	ontrol	Valve						PIT	Y2			
FCV-4-479		НЗ		B	4.0	GA		Α	C	<u>с</u>	BTC	CS		CSI-18	<u> </u>
			-	-		0.1			· ·	•	FC	CS		CSJ-18	TPv-04
											PIT	Y2			
	Valve Name:	A S/G	FWFC	С Вур	bass V	alve				_					
FCV-4-488	5614-M-3074-3	D4	2	В	12.0	GL	AO	A	0	С	BTC	cs		CSJ-17	
											FC	CS		CSJ-17	
	Valve Name:	B S/G	FW Co	ontrol	Valve						Pit	Y2			
		<u> </u>												00148	
FUV-4-489	5014-M-3074-3	EJ	2	В	4.0	GA	AO	A	. C	C	FC	CS		CSL18	TDUM
											РП	Y2		000-10	111-04
	Valve Name:	B S/G	FWFC	CV By	oass V	alve									
FCV-4-498	5614-M-3074-3	B4	2	В	12.0	GL	AO	Α	0		BTC	cs		CSJ-17	
											FC	CS		CSJ-17	
											PIT	¥2			
1	Valve Name:	C S/G	FW Co	ontrol	Valve										
FCV-4-499	5614-M-3074-3	C3	2	В	4.0	GA	AO	A	С	С	BTC	CS		CSJ-18	
											FC	CS		CSJ-18	TPv-04
	Valve Name:	C S/G	FWFC	CV Byr	oass V	alve					PIT	Y2			

Main Feedwater (074a)

Safety P&ID Safety Active / Normal Relief Deferred Tech. Valve Act. Test Test Coor. Class Cat. Size Type Туре Passive Position Position Type Freq. Request Just. Pos. Valve Tag P&ID 20-143 5610-M-3075-2 **B**7 3 С 6.0 СК SA A SYS O/C CC M3 VR-03 TPv-01 CO M3 Valve Name: AFW Pump A Discharge Check Valve 20-243 5610-M-3075-2 D7 3 С 6.0 СК SA A SYS O/C CC M3 CO M3 Valve Name: AFW Pump B Discharge Check Valve O/C 20-343 5610-M-3075-2 F7 3 С 6.0 СК SA A SYS CC М3 М3 CO Valve Name: AFW Pump C Discharge Check Valve AFSS-003B 5610-M-3075-1 СК A SYS 0 TPv-01,02 D4 3 С 4.0 SA CCR СМ COF СМ TPv-02 Valve Name: AFW Pump B Turbine Steam Supply Check Valve AFSS-003C 5610-M-3075-1 F4 3 С 4.0 СК SA A SYS 0 CCR СМ TPv-01,02 COF CM TPv-02 Valve Name: AFW Pump C Turbine Steam Supply Check Valve С 3 С 1.0 RV O/C RV-6401A 5610-M-3075-2 A4 SA А RT Y10 Valve Name: AFW Pump A LO Cooler Cooling Water Relief Valve RV-6401B С 5610-M-3075-2 C4 3 С 1.0 RV SA Α O/C RT Y10 Valve Name: AFW Pump B LO Cooler Cooling Water Relief Valve RV-6401C 5610-M-3075-2 F4 3 С 1.0 RV SA Α С O/C RT Y10 Valve Name: AFW Pump C LO Cooler Cooling Water Relief Valve 3-10-083 SYS 0 5613-M-3075-1 **C7** 3 С 4.0 СК SA А CCD CM TPv-01.02 СМ TPv-02 COF AFW A Train 1 Steam Supply Check Valve Valve Name: 3-10-087 5613-M-3075-1 F7 3 С 4.0 СК SA Α С 0 CCD СМ TPv-01,02 COD СМ TPv-02 Valve Name: AFW Train 1 Steam Supply Check Valve 3-10-375 5613-M-3075-1 G3 2 С 3.0 CK SA A SYS 0 CCD СМ TPv-01,02 COF TPv-02 CM Valve Name: **AFW Train 2 Steam Supply Check Valve**

P&ID Safety Valve Act. Active / Normal Safety Test Test Relief Deferred Tech. Cat. Just. Coor. Class Size Type Type Passive Position Position Type Freq. Request Pos. P&ID Valve Tag 0 5613-M-3075-1 2 С 3.0 CK A SYS CCD CM TPv-01,02 3-10-376 E3 SA COF TPv-02 СМ Valve Name: AFW Train 2 Steam Supply Check Valve СМ TPv-01,02 3-10-377 5613-M-3075-1 C3 2 С 3.0 СК SA Α SYS 0 CCD COF CM TPv-02 Valve Name: AFW Train 1 Steam Supply Check Valve 3-10-381 5613-M-3075-1 G4 Α SYS O/C CCF CSJ-01 3 С 4.0 СК SA CM TPv-02 COF СМ TPv-02 Valve Name: **AFW Steam Supply Check Valve** CSJ-01 3-10-382 5613-M-3075-1 E4 3 С 4.0 CK SA Α SYS O/C CCF СМ TPv-02 COF CM TPv-02 Valve Name: **AFW Steam Supply Check Valve** 3-10-383 5613-M-3075-1 C4 С A SYS O/C CCF СМ CSJ-01 TPv-02 3 4.0 CK SA COF СМ TPv-02 Valve Name: **AFW Steam Supply Check Valve** SYS 0 3-20-140 5613-M-3075-2 F7 2 С СК SA A CCR СМ TPv-01,02 4.0 COF СМ TPv-02 Valve Name: Auxiliary Feedwater Pump S/G Supply Check Valve 3-20-142 5613-M-3075-2 C2 3 В 6.0 GA MAN A LO O/C BTC Y2 TPv-11 Y2 BTO TPv-11 Valve Name: AFW Pmp A Train 1 Disch Isol 3-20-240 5613-M-3075-2 D7 2 С 4.0 СК SA Α SYS 0 CCR CM TPv-01,02 TPv-02 COF СМ Valve Name: Auxiliary Feedwater Pump S/G Supply Check Valve 3-20-340 B7 SYS 0 CCR TPv-01,02 5613-M-3075-2 2 С 4.0 СК SA A СМ COF СМ TPv-02 Valve Name: Auxiliary Feedwater Pump S/G Supply Check Valve SYS O/C 3-20-456 5610-M-3075-2 A6 3 С 2.0 CK SA A CC M3 CO M3 Valve Name: **AFW Pump Recirculation to CST Check Valve**

	Valve Tag	P&ID	P&ID Coor.	Safety Class	Cat.	Size	Valve Type	Act. Type	Active / Passive	Normal Position	Safety Position	Test Type	Test Freq.	Relief Request	Deferred Just.	Tech. Pos.
	AFPD-3-010	5613-M-3075-2	H3	3	C	4.0	СК	SA	A	SYS	0	CCR	СМ			TPv-01,02
												COF	СМ			TPv-02
		Valve Name:	Auxili	ary Fee	edwat	er Pun	np S/G S	Supply C	Check Va	lve						
	AFPD-3-012	5613-M-3075-2	E3	3	С	4.0	СК	SA	A	SYS	0	CCR	СМ			TPv-01,02
,												COF	СМ			TPv-02
		Valve Name:	Auxili	iary Fee	edwat	er Pun	np S/G S	Supply C	Check Va	lve						
	AFPD-3-014	5613-M-3075-2	C3	3	С	4.0	СК	SA	A	SYS	0	CCR	СМ			TPv-01,02
	•											COF	СМ			TPv-02
		Valve Name:	Auxili	ary Fee	edwat	er Pun	np S/G S	Supply C	Check Va	lve						
	AFSS-3-005	5613-M-3075-1	B6	3	С	4.0	СК	SA	A	SYS	0	CC	M3			TPv-01
												со	M3			
		Valve Name:	AFW	Pump 1	Turbin	e Stea	ım Supp	oly Chec	k Valve							
	AFWU-3-017	5610-M-3075-2	A6	3	С	2.0	СК	SA	Α	SYS	O/C	CCD	СМ			TPv-06,02
/												COD	СМ			TPv-06,02
		Valve Name:	AFW	Pump l	LO Co	oling \	Water R	eturn Ci	heck Valv	re						
	CV-3-2816	5613-M-3075-2	F7	2	В	4.0	GL	AO	A	С	O/C	BTC	МЗ			
												BTO	MЗ			
												PIT	Y2			
		Valve Name:	Train	1 S/G /	A Feed	d Flow	Control	Valve								
	CV-3-2817	5613-M-3075-2	D7	2	В	4.0	GL	AO	A	С	O/C	BTC	МЗ		-	
												BTO	M3			
												PIT	Y2			
/		Valve Name:	Train	1 S/G I	B Feed	d Flow	Contro	l Valve								
	CV-3-2818	5613-M-3075-2	B7	2	В	4.0	GL	AO	A	с	O/C	BTC	МЗ			
												BTO	M3	•		
												PIT	Y2			
		Valve Name:	Train	1 S/G (C Feed	d Flow	Contro	l Valve								
	CV-3-2831	5613-M-3075-2	G7	2	В	4.0	GL	AO	A	c	O/C	BTC	M3			
												BTO	M3			
												PIT	Y2			
/		Valve Name:	Train	2 AFW	Flow	to 3A	S/G									

Valve Tag	P&ID	P&ID Coor.	Safety Class	Cat.	Size	Vaive Type	Act. Type	Active / Passive	Normai Position	Safety Position	Test Type	Test Freq.	Relief Request	Deferred Just.	Tech. Pos.
CV-3-2832	5613-M-3075-2	E7	2	В	4.0	GL	AO	A	С	O/C	BTC	МЗ			
											BTO	M3			
	Valve Name:	Train	2 4 514/	Flow	to 2B	8/6					PIT	¥2			
			2 APW	FIOW	10 30										
CV-3-2833	5613-M-3075-2	C7	2	В	4.0	GL	OA	Α	С	O/C	BTC	М3			
											BTO	M3			
				_	_	_					PIT	Y2			
	Valve Name:	Train	2 AFW	Flow	to 3C	S/G 				_			_	_	
MOV-3-1403	5613-M-3075-1	G3	2	В	4.0	GL	MO	Α	С	O/C	BTC	МЗ			
											BTO	M3			
											PIT	Y2			
	Valve Name:	S/G A	Stm S	upply	to Aux	k Fd Pur	nps								
MOV-3-1404	5613-M-3075-1	E3	2	В	4.0	GL	МО	A	C	O/C	BTC	M3			
											BTO	МЗ			
							•				PIT	Y2			
	Valve Name:	S/G B	Stm S	upply	to Aux	c Fd Pur	nps								
MOV-3-1405	5613-M-3075-1	СЗ	2	В	4.0	GL	мо	A	С	0/C	BTC	M3		···=	
											BTO	M3			
											PIT	Y2			
	Valve Name:	S/G C	Stm S	upply	to Au	k Fd Pur	nps								
	5613-M-3075-3	A7	SR	D		RPD	SA	A	C	0	RT	¥5	_		
	Valve Name:	N2 St	ipply H	eader	Ruptu	re Disk									
	5613-M-3075-3		SR	D	<u> </u>	RPD	SA	A	C	0	RT	Y5			
	Valve Name:	N2 SL	ipply H	- eader	Ruptu	re Disk	••••		•	•					
<u> </u>		<u> </u>													
4-10-083	5614-M-3075-1	A7	3	С	4.0	СК	SA	Α	SYS	0	CCD	СМ			TPv-01,02
					_						COF	СМ			TPv-02
	Valve Name:	AFW.	A Train	1 Ste	am Su	ipply Ch	eck Val	lve							
4-10-087	5614-M-3075-1	D7	3	С.	4.0	СК	SA	A	С	0	CCD	CM			TPv-01,02
											COD	СМ			TPv-02
	Valve Name:	AFW	Train 1	Stear	n Supp	oly Chec	k Valve)							

P&ID Safety Relief Valve Act. Active I Normal Safety Test Test Deferred Tech. Size Type Freq. Coor. Class Cat. Passive Position Position Request Just. Pos. Type Type Valve Tag P&ID SYS TPv-01,02 4-10-375 5614-M-3075-1 F4 2 С 3.0 СК SA A 0 CCD СМ COF CM TPv-02 Valve Name: AFW Train 2 Steam Supply Check Valve SYS 0 4-10-376 5614-M-3075-1 D3 2 С A CCD CM TPv-01,02 3.0 CK SA TPv-02 COF CM Valve Name: AFW Train 2 Steam Supply Check Valve 4-10-377 5614-M-3075-1 С СК SA A SYS 0 CCD СМ TPv-01,02 **B**3 2 3.0 CM COF TPv-02 Valve Name: AFW Train 2 Steam Supply Check Valve 4-10-381 5614-M-3075-1 F4 3 C 4.0 СК SA Α SYS O/C CCF СМ CSJ-01 TPv-02 COF CM TPv-02 Valve Name: **AFW Steam Supply Check Valve** 4-10-382 SYS O/C CSJ-01 5614-M-3075-1 D4 3 С 4.0 CK SA A CCF СМ TPv-02 COF TPv-02 CM Valve Name: **AFW Steam Supply Check Valve** 4-10-383 SA A SYS O/C CSJ-01 5614-M-3075-1 **B4** 3 С 4.0 СК CCF CM TPv-02 COF СМ TPv-02 Valve Name: **AFW Steam Supply Check Valve** 4-20-140 5614-M-3075-2 2 СК A SYS 0 TPv-01,02 F7 С 4.0 SA CCR СМ COF CM TPv-02 Valve Name: Auxiliary Feedwater Pump S/G Supply Check Valve 4-20-142 LO O/C 5614-M-3075-2 B2 3 В MAN A BTC Y2 TPv-11 6.0 GA BTO Y2 TPv-11 Valve Name: AFW Pmp A Train 1 Disch Isol 4-20-240 5614-M-3075-2 D7 2 С 4.0 СК SA A SYS 0 CCR CM TPv-01,02 COF CM TPv-02 Valve Name: Auxiliary Feedwater Pump S/G Supply Check Valve 4-20-340 5614-M-3075-2 B7 2 С 4.0 СК SA SYS 0 CCR СМ TPv-01,02 A COF СМ TPv-02 Valve Name: Auxiliary Feedwater Pump S/G Supply Check Valve

	Valve Tag	P&ID	P&ID Coor.	Safety Class	Cat.	Size	Valve Type	Act. Type	Active / Passive	Normal Position	Safety Position	Test Type	Test Freq.	Relief Request	Deferred Just.	Tech. Pos.
	4-20-458	5610-M-3075-2	G6	3	С	2.0	СК	SA	A	SYS	O/C	СС	МЗ			
		Valve Name:	AFWI	Pump F	Recirc	ulatior	n to CST	Check	Valve			CO	M3 ⁻			
•	AFPD-4-009	5614-M-3075-2	H3	3	С	· 4.0	СК	SA	Å	SYS	0	CCR	СМ			TPv-01,02
												COF	СМ			TPv-02
		Valve Name:	Auxili	ary Fee	edwate	er Purr	np S/G S	Supply C	Check Val	ve						
	AFPD-4-011	5614-M-3075-2	E3	3	С	4.0	СК	SA	A	SYS	0	CCR	СМ			TPv-01,02
												COF	СМ			TPv-02
		Valve Name:	Auxili	ary Fee	edwate	er Purr	np S/G S	Supply C	Check Val	lve						
	AFPD-4-013	5614-M-3075-2	C3	3	С	4.0	СК	SA	A	SYS	0	CCR	СМ			TPv-01,02
												COF	СМ			TPv-02
		Valve Name:	Auxili	ary Fee	edwate	er Purr	np S/G S	Supply C	Check Val	ve						
	AFSS-4-005	5613-M-3075-1	F5	3	С	4.0	СК	SA	A	SYS	0	сс	M3			Tpv-01
	•											со	M3			
		Valve Name:	AFW	Pump 1	Furbin	e Stea	m Supp _	ly Chec	k Valve				-			
	AFWU-4-016	5610-M-3075-2	G 6	3	С	2.0	СК	SA	A	SYS	0/C	CCD	СМ			TPv-06,02
												COD	СМ			TPv-06,02
		Valve Name:	AFWI	Pump L	_O Co	oling V	Vater Re	eturn Cl	heck Valv	'e						
	CV-4-2816	5614-M-3075-2	F7	2	В	4.0	GL	AO	A	С	O/C	BTC	МЗ			
												BTO	M3			
							•					PIT	Y2			
		Valve Name:	Train	1 S/G /	A Feed	I Flow	Control	Valve								
	CV-4-2817	5614-M-3075-2	D7	2	В	4.0	GL	AO	A	с	O/C	BTC	M3			
												BTO	M3			
												PIT	Y2			
		Valve Name:	Train	1 S/G E	3 Feed	I Flow	Control	Valve								
•	CV-4-2818	5614-M-3075-2	B7	2	B	4.0	GL	AO	A	С	O/C	BTC	МЗ			
												BTO	M3			
												PIT	Y2			
		Valve Name:	Train	1 S/G (C Feed	Flow	Control	Valve								

	Valve Tag	P&ID	P&ID Coor.	Safety Class	Cat.	Size	Valve Type	Act. Type	Active / Passive	Normal Position	Safety Position	Test Type	Test Freq.	Relief Request	Deferred Just.	Tech. Pos.
	CV-4-2831	5614-M-3075-2	G7	2	В	4.0	GL	AO	A	С	O/C	BTC	M3			
												BTO	M3			
												Pit	Y2			
		Valve Name:	Train	2 AFW	Flow	to 4A S	S/G								_	
,	CV-4-2832	5614-M-3075-2	E7	2	В	4.0	GL	AO	A	C	0/C	BTC	МЗ			
/												BTO	M3			
												PIT	Y2			
		Valve Name:	Train	2 AFW	Flow	to 4B :	S/G									
	CV-4-2833	5614-M-3075-2	C7	2	B	4.0	GL	AO	A	С	O/C	BTC	МЗ			
												BTO	M3			
												PIT	Y2			
		Valve Name:	Train	2 AFW	Flow	to 4C	S/G									
	MOV-4-1403	5614-M-3075-1	F3	2	B	4.0	GL	мо	A	с	0/C	BTC	M3		_	
,												BTO	M3			
/												PIT	Y2			
		Valve Name:	S/G A	Stm S	upply	to Au	c Fd Pun	nps								
	MOV-4-1404	5614-M-3075-1	D3	2	В	4.0	GL	МО	A	С	O/C	BTC	M3			
												BTO	M3			
												PIT	Y2			
		Valve Name:	S/G B	Stm S	upply	to Au	k Fd Pur	nps								
	MOV-4-1405		B3	2	В	4.0	GL	MO	A	c	0/C	BTC	МЗ			
			·									BTO	M3			
												PIT	Y2			
/		Valve Name:	S/G C	Stm S	upply	to Au	c Fd Pur	nps								
	RVD-4-001	5614-M-3075-3	A7	SR	D		RPD	SA	A	С	0	RT	Y5			
		Valve Name:	N2 SI	ipply H	eader	Ruptu	re Disk									
	RVD-4-002	5614-M-3075-3	F7	SR	D		RPD	SA	A	с	0	RT	Y5		· · ·	
		Valve Name:	N2 Sı	ipply H	eader	Ruptu	re Disk									

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Valve Tag	P&ID	P&ID Coor.	Safety Class	Cat.	Size	Valve Type	Act. Type	Active I Passive	Normal Position	Safety Position	Test Type	Test Freq.	Relief Request	Deferred Just.	Tech. Pos.
PAHM-3-001A	5613-M-3094-1	B3	2	A	0.75	GL	MAN	A	LC	O/C	AT-01	App-J			
											BTC	Y2 '			TPv-11
											BTO	Y2			TPv-11
	Valve Name:	Hydro	ogen Mo	onitor	Outle	Isolatio	on							_	· _
PAHM-3-001B	5613-M-3094-1	B2	2	A	0.75	GL	MAN	A	LC	0/C	AT-01	App-J			
											BTC	Y2			TPv-11
											BTO	Y2			TPv-11
	Valve Name:	Hydro	ogen Mo	onitor	Outle	l Isolatio	n								
PAHM-3-002A	5613-M-3094-1	D4	2	A	0.75	GL	MAN	A	LC	O/C	AT-01	App-J			
											BTC	Y2			TPv-11
											BTO	Y2			TPv-11
	Valve Name:	Hydro	ogen Mo	onitor	r Inlet I	solation	I								
PAHM-3-002B	5613-M-3094-1	C3	2	A	0.75	GL	MAN	A	LC	0/C	AT-01	App-J			
											BTC	Y2			TPv-11
											BTO	Y2			TPv-11
	Valve Name:	Hydro	ogen Mo	onitor	Outlet	Isolatio	on	_	_						
PAHM-4-001A	5613-M-3094-1	B2	2	A	0.75	GL	MAN	A	LC	O/C	AT-01	App-J			
											BTC	Y2			TPv-11
											BTO	Y2			TPv-11
	Valve Name:	Hydro	gen Mo	onitor	Outlet	t Isolatio	on								
PAHM-4-001B	5613-M-3094-1	B3	2	A	0.75	GL	MAN	A	LC	O/C	AT-01	App-J			
											BTC	Y2			TPv-11
											BTO	Y2			TPv-11
	Valve Name:	Hydro	gen Mo	onitor	r Outlei	lsolatio	n								
PAHM-4-002A	5614-M-3094-1	D5	2	A	0.75	GL	MAN	A	LC	O/C	AT-01	App-J			
											BTC	Y2			TPv-11
											BTO	Y2			TPv-11
	Valve Name:	Hydro	ogen Mo	onito	r inlet i	solation	l								
PAHM-4-002B	5614-M-3094-1	C3	2	A	0.75	GL	MAN	A	LC	0/C	AT-01	App-J			
											BTC	Y2			TPv-11
											BTO	Y2			TPv-11
	Valve Name:	Hydro	gen Mo	onitor	Outlet	t Isolatio	on								

Post Accident Hydrogen Monitors (094a)

				Po	ost Ad	cciden	it Sam	pling (0	94c)				Turkey IST Pro Valve 1	Point Nucl ogram Plan Fable	ear Plant
Valve Tag	P&ID	P&ID Coor.	Safety Class	Cat.	Size	Valve Type	Act. Type	Active / Passive	Normal Position	Safety Position	Test Type	Test Freq.	Relief Request	Deferred Just.	Tech. Pos.
3-11-003	5613-M-3094-1	B2	2	A/C	1.00	СК	SA	A	SYS	0/C	AT-01	App-J			
											CC	RR		RJ-11	TPv-08
	Valve Name:	Cont.	Air Mo	nitor	Exhaus	st Chec	k Valve				co	RR		RJ-11	
HV-3-001	5613-M-3094-1		2		2 00		MAN	A	10	0/0	AT-01				
			•		2.00	2			20	0.0	BTC	Y2			TPv-11
											BTO	Y2			TPv-11
	Valve Name:	PACV	/ Peneti	ration	16 - U	pstream	n Isolati	on							
HV-3-002	5613-M-3094-1	H4	2	A	2.00	DIA	MAN	A	LC	O/C	AT-01	App-J			
											BTC	Y2			TPv-11
											BTO	¥2			TPv-11
	Valve Name:	PACV	/ Peneti	ration	16 - D	ownstre	eam Iso	lation		_	_				
HV-3-003	5613-M-3094-1	G2	2	A	2.00	DIA	MAN	A	LC	O/C	AT-01	App-J			
											BTC	Y2			TPv-11
	Valve Name:	PACV	/ Peneti	ration	53 - U	pstream	ı Isolati	on			BTO	Y2	•		TPv-11
10/2004								· · ·	10		AT 04				
HV-J-004	5013-M-3094-1	64	2	A	2.00	DIA	MAN	A		0/0		App-J			TD. 44
											BTO	12 V2			TDv.11
	Valve Name:	PACV	/ Peneti	ration	53 - D	ownstre	eam Iso	lation			510	12			
SV-3-2911	5613-M-3094-1	A3	2	A	1.00	GL	SO	A	0	O/C	AT-01	App-J			
		•									BTC	М3			
											BTO	МЗ			
											FC	M3			TPv-04
											PIT	App-J	VR-02		
	Valve Name:	Soler	ioid Val	ve fo	r Cont.	Air Moi	nitor Ini	et						_	
SV-3-2912	5613-M-3094-1	B3	2	A	1.00	GL	SO	A	0	O/C	AT-01	App-J			
											BTC	М3			
											BTO	M3			
											FC	M3			TPv-04
											PIT	App-J	VR-02		
	Valve Name:	Soler	ioid Val	ve fo	r Cont.	Air Mo	nitor Ou	tlet							

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				Po	ost Ac	cciden	t Sam	pling (0	94c)				IST Pro Valve 1	ogram Plan Fable	l
Valve Tag	P&ID	P&ID Coor.	Safety Class	Cat.	Size	Valve Type	Act. Type	Active I Passive	Normal Position	Safety Position	Test Type	Test Freq.	Relief Request	Deferred Just.	Tech. Pos.
SV-3-2913	5613-M-3094-1	A3	2	A	1.00	GL	SO	A	0	0/C	AT-01	App-J			
											BTC	М3			
											BTO	МЗ			
											FC	M3			TPv-04
											PIT	App-J	VR-02		
	Valve Name:	Solen	old Val	ve for	Cont.	Air Mor	nitor Inio	et							
4-11-003	5614-M-3094-1	B2	2	A/C	1.00	СК	· SA	A	SYS	O/C	AT-01	App-J			
											cc	RR		RJ-11	TPv-08
											со	RR		RJ-11	
	Valve Name:	Cont.	Air Mo	nitor l	Exhaus	st Chec	k Valve								
HV-4-001	5614-M-3094-1	H2	2	A	2.00	DIA	MAN	A	LC	O/C	AT-01	App-J			
											BTC	Y2			TPv-11
											BTO	Y2			TPv-11
	Valve Name:	PACV	Peneti	ration	16 - Uj	pstream	i Isolati	on							
HV-4-002	5614-M-3094-1	H4	2	A	2.00	DIA	MAN	A	LC	O/C	AT-01	App-J			
											BTC	Y2			TPv-11
	Valve Name:	PACV	Peneti	ration	16 - D	ownstre	am Isol	lation			BTO	Y2			TPv-11
HV-4-003	5614-M-3094-1	G2	2	A	2.00	DIA	MAN	A	LC	0/0	A1-01	App-J			TD- 44
											BIC	¥2			1PV-11
	Valve Name:	PACV	Peneti	ration	51 - U	pstream	n Isolati	on			вю	12			199-11
	5614.M.3094.1	 G4		Δ	2 00		ΜΔΝ				AT_01	App. 1	·		
	001111000011	0.	-		2.00	0		~	. 20	0,0	BTC	Y2			TPv-11
											BTO	Y2			TPy-11
	Valve Name:	PACV	Peneti	ration	51 - D	ownstre	am Isol	lation							
SV-4-2911		A3	2	A	1.00	GL	SO	A	0	0/C	AT-01	App-J		· · · · ·	
											BTĊ	M3			
											BTO	M3			
											FC	мз			TPv-04
											PIT	App-J	VR-02		
	Valve Name:	Solen	oid Val	ve for	Cont.	Air Mor	hitor Inl	et							

Turkey Point Nuclear Plant

Valve Tag	P&ID	P&ID Coor.	Safety Class	Cat.	Size	Valve Type	Act. Type	Active / Passive	Normal Position	Safety Position	Test Type	Test Freq.	Relief Request	Deferred Just.	Tech. Pos.
SV-4-2912	5614-M-3094-1	B 3	2	A	1.00	GL	SO	A	0	- O/C	AT-01	App-J			
											BTC	M3			
											BTO	M3			
											FC	M3			TPv-04
											PIT	App-J	VR-02		
	Valve Name:	Solen	oid Val	ve for	Cont.	Air Mor	itor Ou	tlet							·
SV-4-2913	5614-M-3094-1	A3	2	A	1.00	GL	SO	A	0	O/C	AT-01	App-J	<u></u>		. <u> </u>
											BTC	М3			
											BTO	M3			
											FC	M3			TPv-04
											PIT	App-J	VR-02		
	Valve Name:	Solen	oid Val	ve for	Cont.	Air Mor	nitor Inle	et							

Post Accident Sampling (094c)

Post Accident Hydrogen Control (094d)

Valve Tag	P&ID	P&ID Coor.	Safety Class	Cat.	Size	Vaive Type	Act. Type	Active / Passive	Normal Position	Safety Position	Test Type	Test Freq.	Relief Request	Deferred Just.	Tech. Pos.
4678	5613-M-3094-1	F7	NS	В	2.00	DIA	MAN	A	LC	0	вто	Y2			TPv-11
	Valve Name:	PACV	Filter	Train	to Was	ste Gas I	Release	Hdr. Isol	l						
HV-3-18	5613-M-3094-1	G5	NS	В	2.00	GA	MAN	A	LC	0	BTO	Y2			TPv-11
	Valve Name:	Hydro	ogen Re	ecomt	oiner Ir	niet Isol.									
HV•7	5613-M-3094-1	F5	NS	B	3.00	DIA	MAN	A	С	0	BTO	Y2			TPv-11
	Valve Name:	PACV	Filter	Inlet I	sol.										
HV-77	5613-M-3094-1	F7	NS	В	3.00	DIA	MAN	A	С	0	BTO	¥2		· · · · · · · · · · · · · · · · · · ·	TPv-11
	Valve Name:	PACV	Filter	Outlet	isol.										
HV-8	5613-M-3094-1	F7	NS	В	2.00	DIA	MAN	A	LC	0	BTO	Y2		<u> </u>	TPv-11
	Valve Name:	PACV	Filter	to Wa	ste Ga	s Comp	•								
HV-4-18	5614-M-3094-1	G5	NS	В	2.00	GA	MAN	A	LC	0	вто	Y2			TPv-11
	Valve Name:	Hydro	ogen Re	ecomt	oiner Ir	niet Isol.									

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Breathing Air (101)

Valve Tag	P&ID	P&ID Coor.	Safety Class	Cat.	Size	Valve Type	Act. Type	Active / Passive	Normal Position	Safety Position	Test Type	Test Freq.	Relief Request	Deferred Just.	Tech. Pos.
BA-3-201	5613-M-3101-1 Valve Name:	D3 Conta	2 ainment	A/C t Brea	2.5 thing /	CK Air Isola	SA tion Ch	P eck Valve	C	C	AT-01	Арр-Ј	VR-01		TPv-10
CV-3-6165	5613-M-3101-1	D2	2	A	2.5	GA	AO	Р	LC	С	AT-01 PIT	App-J Y2			
	Valve Name:	Conta	inmen	t Brea	thing /	Air Isola	tion Va	lve							
BA-4-201	5614-M-3101-1 Valve Name:	D3 Conta	2 ainment	A/C t Brea	2.5 thing /	CK Air Isola	SA tion Ch	P eck Valve	С	c	AT-01	App-J	VR-01		TPv-10
CV-4-6165	5614-M-3101-1	D2	2	A	2.5	GA	AO	P	LC	С	AT-01 PIT	App-J Y2			
	Valve Name:	Conta	inmen	t Brea	thing /	Air Isola	tion Va	lve							

ATTACHMENT 2 L-2004-043





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his pay is which inter 54.1			POD
9	TURKEY POINT NUCLEAR UNIT 3	STONE & WEBSTER ENGINEERING CORP.	
FPL	COMPONENT COOLING WATER	ORANNIC HAMBER 5613-M-3030	573 030
	SYSTEM	SET 4	REV 22



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	<u>NOTES:</u> 1. FOR CONET: 5510-М-3 2. THE REFER 10 THE TO 3. SV-4-154 АНО <u>FAL</u> A КЕТЕРЕНИЕ 0	PRAL NOTES & LECEND SEE DWG NO. -3000 SH. 2. ERENCE LEVEL FOR BOTTOM OF TANK (B.O.T.) IS TOP OF THE TANK FOUNDATION. 540 IS <u>FAL CLOSE</u> ON LOSS OF POWER <u>LAS IS</u> ON LOSS OF AR. DRAWINGS:				
	5614-W-300 5614-W-307 5614-W-307 5614-W-307 5614-W-307 5614-W-307 5614-W-307 5610-W-307 5610-W-307	3 SH 1 SH 3 SH 1 & 2 SH 1 & 2 SH 1 SH 1 SH 1 SH 1 SH 1 SH 1 SH 2 SH 2 SH 2 SH 2 SH 2	TURBINE PLANT OC WATER SYSTEM INSTRUMENT AR S CONDENSATE SYSTE FEEDWATER SYSTE STEAN GENERATOR CONDENSATE RECC CONTROL BULDING CONTROL BULDING CONTROL BULDING CONTROL BULDING CONTROL BULDING CONTROL BULDING FEEDWATER SYSTE STORAGE & DEAER AUJGUARY FEEDWA AUJGUARY FEEDWA	XOLING YSTEM EM M WET LAYUP S WET LAYUP SYSTEM AYUP SYSTEM XAOE SYSTEM YCABLE SPRE/ M - DEMMERAL XATON TER SYSTEM - TER PUMPS	YSTEM . G VOING JZED	
				PO	D	
	TURKEY POINT NUCLEAR UNIT 4	STONE & WEBSTER ENGINEERING				
	P 410	DRAWING N	575			
EPL	CONDENSATE STORAGE SYSTEM	5614-	018			
•••		SHEET 1	23			





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9	11-24-98	ISSUED AS-BUILT PER CRN-14-9439 (PC/N 98-036).	RH	RV	Ē.	μ	3	12-14-92	ISSUED AS-BUILT FOR PC/M 89-542.	TAN	MIN	N.S
8_	7-8-97	ISSUED AS-BUILT PER PC/N 96-029 AND INCORPORATED CRN-N-8922	RH	BSC	2	JN	12	02-06-03	ISSUED AS-BUILT PER CRN-W-10634 (PC/M 02-065).	RH	RV	0
7	2-25-94	ISSUED AS-BUILT FOR DOR-TPM-93-548		NITALS	ON FIL	E	11	05-09-01	ISSUED AS-BUILT PER CRN-W-10292 (PC/M 00-016).	RH	RV	N
6	12-16-93	ISSUED AS-BUILT FOR PC/N 93-054.	RH	RV	0.18	80	10	03-29-00	ISSUED AS-BUILT PER CRN-M-9993 (PC/N 99-061).	JPG	RCR	-
5_	09-20-93	ISSUED AS-BUILT FOR DOR-TPM-93-309.	SM	MO	UK	MEN	0	5-14-91	THIS DWG CREATED PER THE P & ID RECONSTITUTION PROJECT SCOPE	BAN	NO	四
4	04-01-93	ISSUED AS-BUILT FOR PC/N 92-067 AND PC/N 93-046.	28	BA	UK	3ND	=		AND ISSUED INTO THE FPL DWG SYSTEM PER DCR-TPM-91-137.	-		-
3	DATE	REVISION	EV.		400	400	80	0475		~		






