Industry/TSTF Standard Technical Specifica   Maximum pressurizer water level limit bases   Priority/Classification 4) Change Bases   NUREGS Affected: 1430   ✓ 1431 1432   Description: This change makes clear the bases for the maximum pressurizer water level   Justification: The maximum pressurizer water level limit is based on ensuring that a stear maximum pressurizer water level is not credited in any safety analysis. This   Revision History	1434 1 limit. m bubble exists in the pressurizer.	
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Revision History		
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OG Revision 0 Revision Status: Active	Next Action:	
Revision Proposed by: WOG Mini-Group		
Revision Description: Original Issue	<u></u>	
<b>Owners Group Review Information</b> Date Originated by OG: 10-Oct-96		
Owners Group Comments (No Comments)		
Owners Group Resolution: Approved Date: 10-Oct-96		
TSTF Review Information		
TSTF Received Date: 15-Oct-96 Date Distributed for	Review 29-Oct-96	
OG Review Completed: 🗹 BWOG 🗹 WOG 🗹 CEOG 🗹 H	BWROG	
TSTF Comments:		
CEOG - Not applicable, accepts BWOG - Not applicable, accepts BWROG - Not applicable, accepts		
TSTF Resolution: Approved Date: 03-Dec-96		
NRC Review Information		
NRC Received Date: 27-Mar-97 NRC Reviewer: W	ESTON, M.	
NRC Comments:		
4/7/97 Rec'd pkg. 4/10/97 Forwarded to reviewer.		
Final Resolution: NRC Approves	Final Resolution Date: 03-Oc	ct-97
Incorporation Into the NUDECe		
Incorporation Into the NUREGs   File to BBS/LAN Date: TSTF Informed Date:	TSTF Approved Date:	

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(WOG-68, Rev. 0)

NUREG Rev Incorporated:

S/A 3.4.9 Bases	Pressurizer	
Action 3.4.9.A Bases	Pressurizer	
SR 3.4.9.1 Bases	Pressurizer	

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BASES	Pressurize B 3.4. TSTF-16
BACKGROUND (continued)	a loss of single phase natural circulation and decreased capability to remove core decay heat.
APPLICABLE SAFETY ANALYSES	In MODES 1, 2, and 3, the LCO requirement for a steam bubbl is reflected implicitly in the accident analyses. Safety analyses performed for lower MODES are not limiting. All analyses performed from a critical reactor condition assume the existence of a steam bubble and saturated conditions in the pressurizer. In making this assumption, the analyses neglect the small fraction of noncondensible gases normally present.
uhich ensures hat a steam ubble exists in e pressurizer,	Safety analyses presented in the FSAR (Ref. 1) do not take credit for pressurizer heater operation; however, an implicit initial condition assumption of the safety analyse is that the RCS is operating at normal pressure.
e pressurizer,	The maximum pressurizer water level limit satisfies Criterion 2 of the NRC Policy Statement. Although the heaters are not specifically used in accident analysis, the need to maintain subcooling in the long term during loss of offsite power, as indicated in NUREG-0737 (Ref. 2), is the reason for providing an LCO.

LCO

The LCO requirement for the pressurizer to be OPERABLE with a water volume  $\leq$  [1240] cubic feet, which is equivalent to [92]%, ensures that a steam bubble exists. Limiting the LCO maximum operating water level preserves the steam space for pressure control. The LCO has been established to ensure the capability to establish and maintain pressure control for steady state operation and to minimize the consequences of potential overpressure transients. Requiring the presence of a steam bubble is also consistent with analytical assumptions.

The LCO requires two groups of OPERABLE pressurizer heaters, each with a capacity  $\geq$  [125] kW, capable of being powered from either the offsite power source or the emergency power supply. The minimum heater capacity required is sufficient to maintain the RCS near normal operating pressure when accounting for heat losses through the pressurizer insulation. By maintaining the pressure near the operating

(continued)

WOG STS

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Rev 1, 04/07/95

BASES	Pressurizer B 3.4.9 TSTF-162
LCO (continued)	conditions, a wide margin to subcooling can be obtained in the loops. The exact design value of [125 kW is derived from the use of seven heaters rated at 17.9 kW each]. The amount needed to maintain pressure is dependent on the heat losses.
APPLICABILITY	The need for pressure control is most pertinent when core heat can cause the greatest effect on RCS temperature, resulting in the greatest effect on pressurizer level and RCS pressure control. Thus, applicability has been designated for MODES 1 and 2. The applicability is also provided for MODE 3. The purpose is to prevent solid water RCS operation during heatup and cooldown to avoid rapid pressure rises caused by normal operational perturbation, such as reactor coolant pump startup.
	In MODES 1, 2, and 3, there is need to maintain the availability of pressurizer heaters, capable of being powered from an emergency power supply. In the event of a loss of offsite power, the initial conditions of these MODES give the greatest demand for maintaining the RCS in a hot pressurized condition with loop subcooling for an extended period. For MODE 4, 5, or 6, it is not necessary to control pressure (by heaters) to ensure loop subcooling for heat transfer when the Residual Heat Removal (RHR) System is in service, and therefore, the LCO is not applicable.
ACTIONS	A.1 and A.2
	Pressurizer water level control malfunctions or other plant evolutions may result in a pressurizer water level above the nominal upper limit, even with the plant at steady state

bring the plant to a MODE in Which the LCO does not apply. Pressurizer water level control malfunctions or other plant evolutions may result in a pressurizer water level above the nominal upper limit, even with the plant at steady state conditions. Normally the plant will trip in this event since the upper limit of this LCO is the same as the Pressurizer Water Level - High Trip.

If the pressurizer water level is not within the limit, action must be taken to restore the plant to operation within the bounds of the safety analyses. To achieve this status, the unit must be brought to MODE 3, with the reactor trip breakers open, within 6 hours and to MODE 4 within 12 hours. This takes the unit out of the applicable MODES.

(continued)

Rev 1, 04/07/95

Pressurizer B 3.4.9 TSTF-162

### BASES

ACTIONS

<u>A.1 and A.2</u> (continued)

and pestores the unit to operation within the bounds of the safety analyses.

The allowed Completion Times are reasonable, based on operating experience, to reach the required plant conditions from full power conditions in an orderly manner and without challenging plant systems.

## <u>B.1</u>

If one required group of pressurizer heaters is inoperable, restoration is required within 72 hours. The Completion Time of 72 hours is reasonable considering the anticipation that a demand caused by loss of offsite power would be unlikely in this period. Pressure control may be maintained during this time using normal station powered heaters.

## C.1 and C.2

If one group of pressurizer heaters are inoperable and cannot be restored in the allowed Completion Time of Required Action B.1, the plant must be brought to a MODE in which the LCO does not apply. To achieve this status, the plant must be brought to MODE 3 within 6 hours and to MODE 4 within 12 hours. The allowed Completion Times are reasonable, based on operating experience, to reach the required plant conditions from full power conditions in an orderly manner and without challenging plant systems.

#### SURVEILLANCE REQUIREMENTS

# <u>SR\_3.4.9.1</u>

This SR requires that during steady state operation, pressurizer level is maintained below the nominal upper limit to provide a minimum space for a steam bubble. The Surveillance is performed by observing the indicated level. The Frequency of 12 hours corresponds to verifying the parameter each shift. The 12 hour interval has been shown by operating practice to be sufficient to regularly assess level for any deviation and verify that operation is within

(continued)

Pressurizer B 3.4.9 TSTF-162

SURVEILLANCE REQUIREMENTS

BASES

<u>SR 3.4.9.1</u> (continued) (exists in the pressurieer.

safety analyses assumptions. Alarms are also available for early detection of abnormal level indications.

# SR 3.4.9.2

The SR is satisfied when the power supplies are demonstrated to be capable of producing the minimum power and the associated pressurizer heaters are verified to be at their design rating. This may be done by testing the power supply output and by performing an electrical check on heater element continuity and resistance. The Frequency of 92 days is considered adequate to detect heater degradation and has been shown by operating experience to be acceptable.

SR 3.4.9.3

This SR is not applicable if the heaters are permanently powered by Class 1E power supplies.

This Surveillance demonstrates that the heaters can be manually transferred from the normal to the emergency power supply and energized. The Frequency of 18 months is based on a typical fuel cycle and is consistent with similar verifications of emergency power supplies.

REFERENCES

1. FSAR, Section [].

2. NUREG-0737, November 1980.