

WM-68  
10/24/90

PART 506

**DEPARTMENT OF ENERGY  
ALBUQUERQUE OPERATIONS OFFICE  
CONTRACT NO. DE-AC04-83AL18796**

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**GREEN RIVER, UTAH**

**D R A F T**

**Completion Report**

**VOLUME 4B  
APPENDIX B**

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**Remedial Actions  
Contractor  
for the  
Uranium Mill Tailings  
Remedial Actions  
Project**

**MAY 1990**



**MK-FERGUSON COMPANY  
A MORRISON KNUDSEN COMPANY**

9011080155

UMTRA PROJECT - GREEN RIVER, UTAH

CALCULATIONS

FINAL DESIGN

CONTENTS

Calculation No

10-539-02-01	Flood Analysis - Brown's Wash: Hydrologic and Hydraulic Analysis of PMF
10-539-01-01	PMP for Erosion Protection: SOS Disposal Site
10-534-01-01	Hydrology: Flood Frequency Analysis (10 Year and 25 Year)
10-551-01-00	Flood Analysis - Brown's Wash: Hydrologic and Hydraulic Analysis of 100 Year Storm

Calculation Cover Sheet



Contract No. 5057

Discipline Earth Sci

Calc. No. 10-539-02-00<sup>01</sup>

No. of Sheets 23 \* 109 W

Project

LIMTRA - Green River

\*Sheet Nos. 21-23  
comprise 90 computer  
printed pages  
19 pages + 90 computer  
printed sheets

Feature

Flood Analysis - Brown Wash

Item

Hydrologic and Hydraulic analysis of PMF

Sources of Data

Sources of Formulae & References

- ① BOE, "Remedial Action Plan and Site Conceptual Design for Stabilization of the Inactive Uranium Mill Tailings at Green River, Utah", Draft, vol. II - Appendix D, Jan., 1987
- ② McCuen, R.H., "A Guide to Hydrologic Analysis using SCS Methods" Prentice-Hall, Inc., Englewood Cliffs, 1982.
- ③ Sheaffer, J.R., "Urban Storm Drainage Management", Marcel Dekker, Inc., 1982.
- ④ TAC, "Green River - Draft Rep, Site Conceptual Design - Civil Engineering calculations vol. 1" MKE Document No. 5057-GRN-C-04-0006N-00, 1987.

Preliminary Calc.

Final Calc.

Supersedes Calc. No. \_\_\_\_\_

Rev. No.	Revision	Calculation By	Date	Checked By	Date	Approved By	Date
1	Changed to Final Calc	W. J. ...	11-11-87	P. K. Cha	11/11/87	P. K. Cha	11/11/87
0		James K ...	4/21/87	H. ...	5/19/87	JRC	7/17/87

Project UMTRA - Green River  
Feature Hydrology  
Item Flood analysis of Brown Wash

Contract No. 5057  
Designed JKK  
Checked HM

Sheet 1  
File No. \_\_\_\_\_  
Date 4/10/87  
Date 5/11/87

Purpose: To determine the PMF peak flow in the Brown Wash at the vicinity of the tailings pile and its potential flooding.

Approach: TAC has performed studies to analyze the potential flooding of the pile due to either a 72-hr general or a 6-hr local PMF. MKE will check TAC's precipitation data and, if appropriate, will use them for an independent flood analysis to confirm TAC's results. The Corps of Engineers HEC1 and HEC2 computer codes will be used for the peak flow and water surface profile analyses, respectively.

Summary of Results: TAC has used 3 different methods of computing the lag time for the subbasins. Their results obtained by the most conservative method check closely with those derived by MKE, as summarized in the Table. Peak flow from PMF on Sh. 2.



Project UMTRA - Cereon River  
Feature Hydrology  
Item Flood analysis of Brown Wash

Contract No. 5054  
Designed Jrk  
Checked HM

Sheet 2  
File No. \_\_\_\_\_  
Date 4/10/87  
Date 5/1/87

Q (cfs) from PMF

		<u>General 72-hr.</u>	<u>local 6-hr.</u>
<u>TAC</u>	Approach ①	17,000	28,000
	②	12,000	23,000
	③	26,000	98,000
		or 35,000 (in RAP)	
<u>MKE</u>		36,000	90,000

The peak flow values obtained by TAC and MKE are rounded off to 100,000 cfs for use in the HEC2 water surface profile analysis. The results show that the existing tailings pile will be inundated with the maximum water level @ approx. 4092' at the vicinity of the existing pile (see water surface profile on sk. 18 and cross sections on sk. 13-16). The proposed pile at the new disposal location will be about 40 ft. above the maximum water level in the Brown Wash during a 6-hr. local PMF.

Project UMTRA - Coker River  
 Feature Hydrology  
 Item Flood Analysis of Brown Wash

Contract No. 5057  
 Designed FTK  
 Checked HM

File No. \_\_\_\_\_  
 Date 4/1/87  
 Date 5/11/87

Analysis

The entire watershed of Brown Wash upstream of the existing tailings pile comprises of a drainage area of about 83 sq. miles. It is divided into 9 subbasins as shown on Sheet 4. The Kirpich equation was used to derive the lag time for the individual sub-basins (sh. 5) which compared well with those obtained by the Tulsa USACE (sh. 7) method which considers the shape of the drainage basin as well as the hydraulic characteristics of the longest flow path. These lag time values are smaller than those derived by either the upland method (sh. 5) or the SCS curve number method and therefore, are used in HEC1 to compute the peak flow along the Brown Wash. The SCS curve number method, as adopted by TAC as one of their approaches to derive the lag times, is applicable only to drainage areas of less than 3 sq. miles whereas most of the subbasins designed for the computer simulation has area greater.

The precipitation data for the general and local PMF derived by TAC in their calculations (ref. (4)) were checked and found to be reasonable and thus were used in the HEC1 runs made by MKE to obtain the peak flow. A table of the hydraulic characteristics of the subbasin is summarized on sh. 5. HEC1 outputs are shown on sh. 20. and 21.



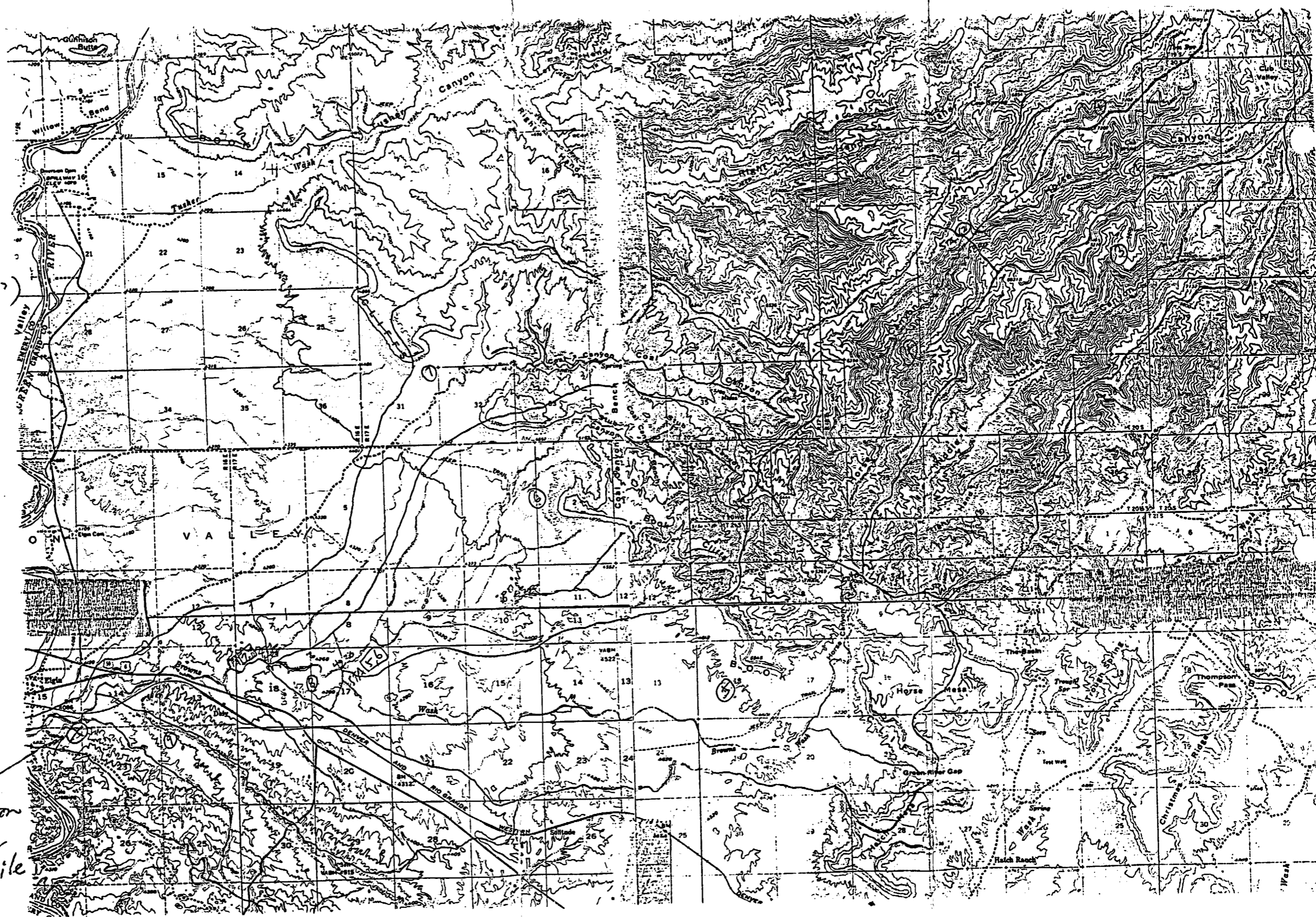
Sh. 4

Exhibit ①

Basin	Area (mi <sup>2</sup> )
1	2.6
2	5.5
3	12.1
4	6.4
5	20.7
6	11.5
7	12.2
8	1.5
9	11.6
<hr/>	
	$\Sigma = 95.1$

from ref. ④

Approx. location of existing tailings pile



0 1 2 miles

FKK 4/1/87  
HM 5/11/87

Project UMTRA - Green River  
 Feature Hydrology  
 Item Flood analysis of Brown Alesh

Contract No. 5057 Sheet 5  
 File No. \_\_\_\_\_  
 Designed JFK Date 4/1/87  
 Checked HM Date 5/11/87

Watershed

	L (mi)	Δh (ft)	S (%)	V (fps)	Kirpich Egn. (sh. 6)		Upland Method
					T <sub>c</sub> (hr.)	T <sub>L</sub> (hr.)	(see sh. 6) T <sub>c</sub> (hr.)
1	4.7 (24,816')	960	3.9	3.0	1.10	0.66	2.30
2	5.7 (30,096')	1,320	4.4	3.2	1.22	0.73	2.61
3	8.5 (44,880')	2,160	4.8	3.4	1.60	0.96	3.67
4	5.0 (26,400')	840	3.2	2.7	1.25	0.75	2.72
5	10.2 (53,856')	810	1.5	1.9	2.88	1.73	7.87
6	7.9 (41,712')	1,770	4.2	3.1	1.59	0.95	3.74
7	10.5 (55,440')	2,200	4.0	3.1	2.03	1.22	4.97
8	1.2 (6,336')	30	0.5	1.1	0.86	0.52	1.60
9	6.2 (32,736')	320	1.0	1.5	2.32	1.39	6.06

Project UNITRA - Coteau River  
Feature Hydrology  
Item Flood Analysis of Brown Wash

Contract No. 5057  
Designed JTK  
Checked HM

Sheet 6  
File No. \_\_\_\_\_  
Date 4/1/87  
Date 5/11/87

The time of Concentration  $T_c$  is calculated

- ① using the Kirpich Equation as follows:

$$T_c = (11.9 L^3 / \Delta h)^{0.385}$$

(hr)

where  $L$  = stream length in miles

$\Delta h$  = Difference in elevation in feet between upper and lower limits of the drainage basin

$$T_L (\text{time lag}) = 0.60 T_c$$

- ② using the upland method

$$T_c = \frac{l}{V \times 3600}$$

(hr)

where  $l$  = stream length in feet

$V$  = velocity in ft/sec as determined from chart on Sh. 8

Project UMTEA - GREEK RIVER  
 Feature Hydrology  
 Item Flood Analysis of Brown W24

Contract No. 5057  
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 File No. \_\_\_\_\_  
 Date 4/6/87  
 Date 5/12/87

The following Time Lag ( $t_p$ ) values are derived from Tulsa LISACE

$$t_p = 1.42 \left( \frac{L \cdot L_{ca}}{\sqrt{S}} \right)^{0.39}$$

where  $S$  = watershed slope (ft/mi)

$L$  = stream length (mi)

$L_{ca}$  = length along stream from study point to centroid of basin (mi)

from reference ③ Sh. 9 and 11

<u>Watershed</u>	$L_{ca}$ (mi)	$\frac{L \cdot L_{ca}}{\sqrt{S}} \left( \frac{\text{mi} \cdot \text{mi}}{\text{ft}/\text{mi}} \right)$	Time Lag $T_p$ (hr.) from Fig. on sh. 11
1	2.3	0.76	1.28
2	2.8	1.05	1.45
3	4.0	2.13	1.91
4	2.0	0.77	1.28
5	5.8	6.64	2.97
6	5.3	2.80	2.12
7	6.3	4.57	2.57
8	0.6	.14	0.66
9	3.2	2.76	2.11

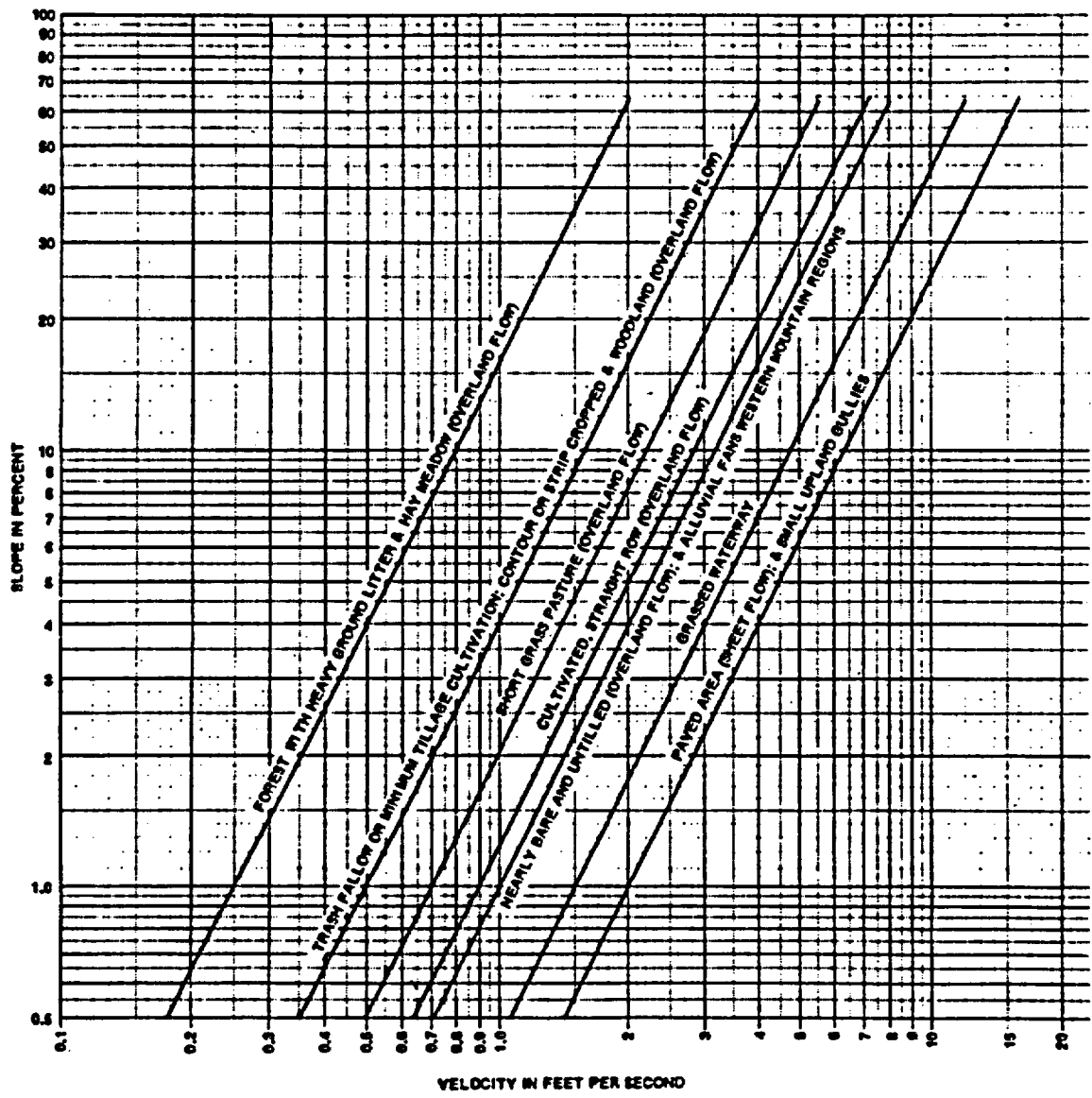


Figure 8. Velocities for upland method of estimating  $T_c$

Reference (2)

JTK 4/1/87

HM 5/12/87

sl. 9  
 Reference (3) JK 4/6/87  
 HM May 14/87

However, SCS notes that the numerator of 5.29 [484] is known to vary from 6.56 [600] to 3.28 [300], similar to variances noted by Snyder [9, 18]. Further, a relationship is derived to define the recommended unit rainfall duration for the unit hydrograph as:

$$t_u = 0.133t_c \quad \text{or} \quad \frac{t_c}{7.5} \quad (6.21)$$

where  $t_c$  = time of concentration as illustrated in Fig. 6.9 and the average relationship between the lag time  $t_p$  and the time of concentration is:

$$t_p = 0.6t_c \quad (6.22)$$

#### General Guidelines for Determining Parameters

The previous discussion presents basic relationships of synthetic unit hydrograph theory. Final determination of a synthetic unit hydrograph for a given watershed requires additional information. For example, values of  $C_t$  in Eq. (6.15) are needed to determine the lag time. The basic approach is to determine these types of coefficients or equations by analysis of rainfall runoff data from other similar watersheds. The HEC-1 computer program [28] provides an efficient means of analyzing such data.

Fortunately, many other hydrologists have already performed such analyses of local, regional, and national data and have arrived at coefficients and variations of and additions to the basic unit hydrograph equations. Any of these relationships, which are presented below, have potential application to the basin being studied and thus provide a savings in study effort. But the hydrologist must determine which equations are applicable based upon the similarity between the study basin and the watersheds for which the equations were derived.

The relationships available can generally be put into three categories:

1. Estimation of lag time  $t_p$
2. Estimation of a synthetic unit hydrograph discharge peak  $q_p$
3. Unit hydrograph shape factors

#### Estimation of Lag Time $t_p$

The various unit hydrograph methods are sensitive to lag time or other peak response time factors. The unit hydrograph peak discharge and shaping factors are usually a function of the lag time and other parameters. Most methods are usually derived with algorithms that are a direct or indirect function of the lag time. Thus, the determination of the lag time is critical to the reliability of the results.

#### Rural Areas

The Tulsa District Army Corps of Engineers [19] has derived a relationship for  $t_p$  based upon data for natural watersheds in the central and northeastern Oklahoma area, which is:

$$t_p = 0.1842 \left( \frac{LL_{ca}}{\sqrt{S}} \right)^{0.39} \quad \left[ t_p = 1.42 \left( \frac{LL_{ca}}{\sqrt{S}} \right)^{0.39} \right] \quad (6.23)$$



where  $S$  = watershed slope, m/m [ft/mi]  
 $L$  = stream length, km [mi]  
 $L_{ca}$  = length along stream to centroid of basin, km [mi]

Reference (3)

FK 4/6/87

HM 5/14/87

This equation, illustrated in Fig. 6.10, is recommended for natural watersheds. Note that the data and derivation were performed originally in British units; thus the graph is presented in these units only. It can be checked for unusual cases by estimating the time of concentration and multiplying by a factor of 0.60 as indicated earlier.

Also shown in Fig. 6.10 are relationships for California mountain and foothill regions [20, 26] as follows:

California mountains:

$$t_p = 0.1642 \left( \frac{LL_{ca}}{\sqrt{S}} \right)^{0.38} \quad \left[ t_p = 1.2 \left( \frac{LL_{ca}}{\sqrt{S}} \right)^{0.38} \right] \quad (6.24)$$

California foothills:

$$t_p = 0.0985 \left( \frac{LL_{ca}}{\sqrt{S}} \right)^{0.38} \quad \left[ t_p = 0.72 \left( \frac{LL_{ca}}{\sqrt{S}} \right)^{0.38} \right] \quad (6.25)$$

A report by Espey, et al. [21] for watersheds in Texas, New Mexico, and Oklahoma resulted in the following recommended equation:

$$T_R = 3.056 L_f^{0.12} S_f^{-0.52} \quad \left[ T_R = 2.65 L_f^{0.12} S_f^{-0.52} \right] \quad (6.26)$$

where  $T_R$  = time of rise in minutes which can be assumed to be equal to

$$T_R = T_p = \frac{t_u}{2} + t_p \quad (6.27)$$

and  $L_f$  = stream length, m [ft]  
 $S_f$  = slope, m/m [ft/ft]

This equation is based on data from small watersheds ranging as follows:  $L$ , 990 to 7700 m [3250 to 25,300 ft];  $S$ , 0.008 to 0.015 m/m [ft/ft]; and  $T_R$ , 30 to 150 min.

#### Urbanized Areas

Several approaches are presented here which should be used with judgment and in comparison to arrive at a recommended  $t_p$ .

The Tulsa District Army Corps has derived parallel relationships for 50 and 100 percent urbanized basins as follows:

For 50 percent urbanized:

$$t_p = 0.1193 \left( \frac{LL_{ca}}{\sqrt{S}} \right)^{0.39} \quad \left[ t_p = 0.92 \left( \frac{LL_{ca}}{\sqrt{S}} \right)^{0.39} \right] \quad (6.28)$$

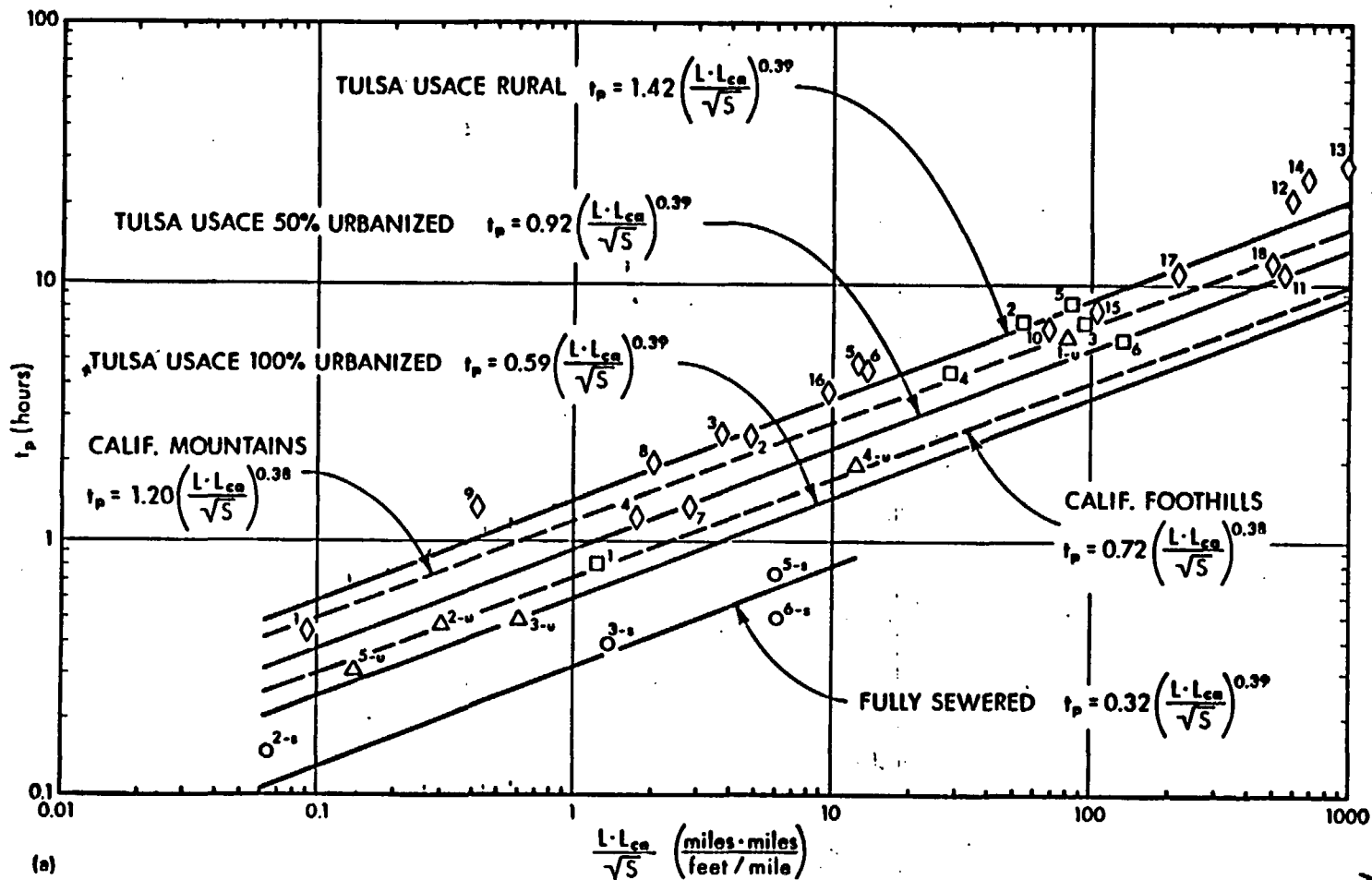


Figure 6.10 (a)  $t_p$  vs.  $LL_{ca} / \sqrt{S}$  for Synthetic Unit Hydrograph Procedure.

144

Runoff Hydrology: Example Techniques

Reference ③

Sh. 11

HM 5/17/77

File 4/6/67

Δ1-u Deep  
 Δ2-u Surf.  
 Δ3-u Deep  
 Δ4-u Deep  
 Δ5-u Crit.

DELINQUENT

Figur

6.4

Project UMTRA - Green River  
Feature Hydrology  
Item Flood analysis of Brown WashContract No. 5057Designed FTKChecked KMSheet 12

File No. \_\_\_\_\_

Date 4/15/87Date 5/11/87

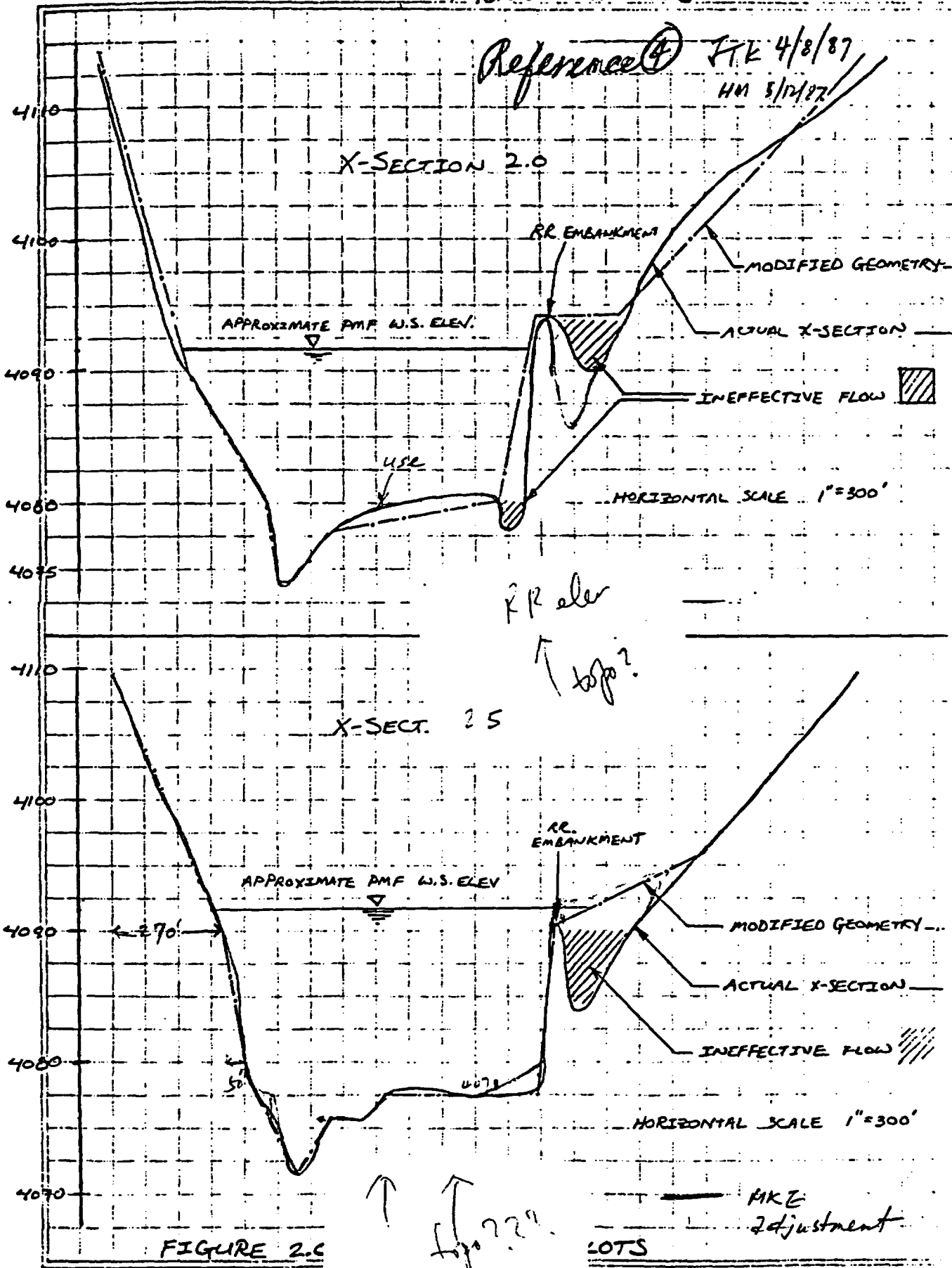
The 5 cross sections plotted in TAC's calculations (ref. (4)) were checked, adjusted and used in the HEC2 water surface profile analysis by MKE. The cross sections are shown on sh. 19 and results are included in the computer printout sh. 22-23. Inclusion of cross sections (1) and (7) from TAC calculation in the HEC2 analysis indicates insignificant difference in the result from the previous run using 5 cross-sections only, (see sh. 22-23) This suggests that modeling using (2) and (6) sections as the end stations is adequate enough. Computed water surface profiles are presented on sh. 17-18



DATE 2/7/87  
 BY RP CHKD. \_\_\_\_\_

SUBJECT CAN SURFACE-WATER FLOOD STUDIES  
HYDRAULIC ANALYSIS

SHEET NO. \_\_\_\_\_  
 JOB NO. \_\_\_\_\_



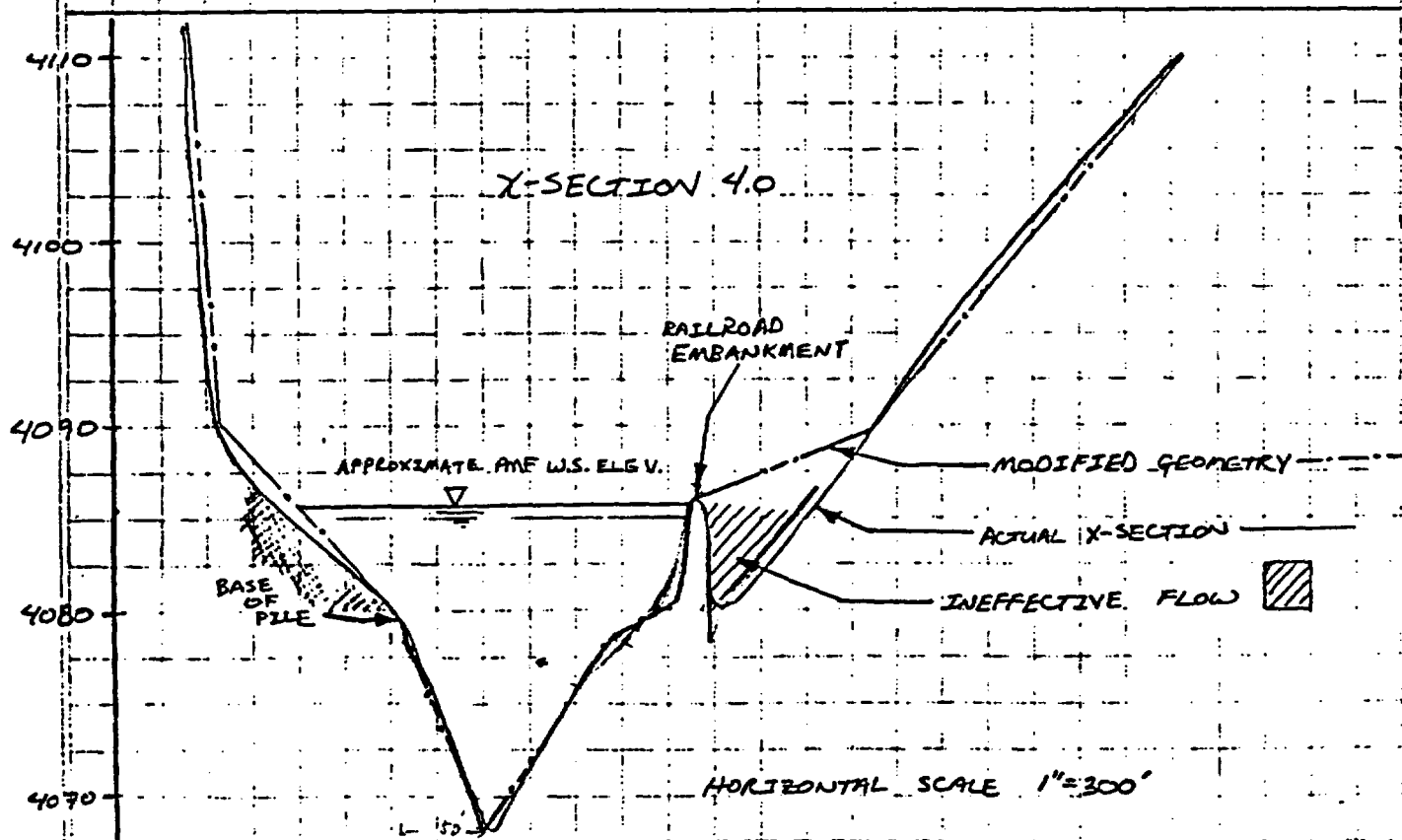
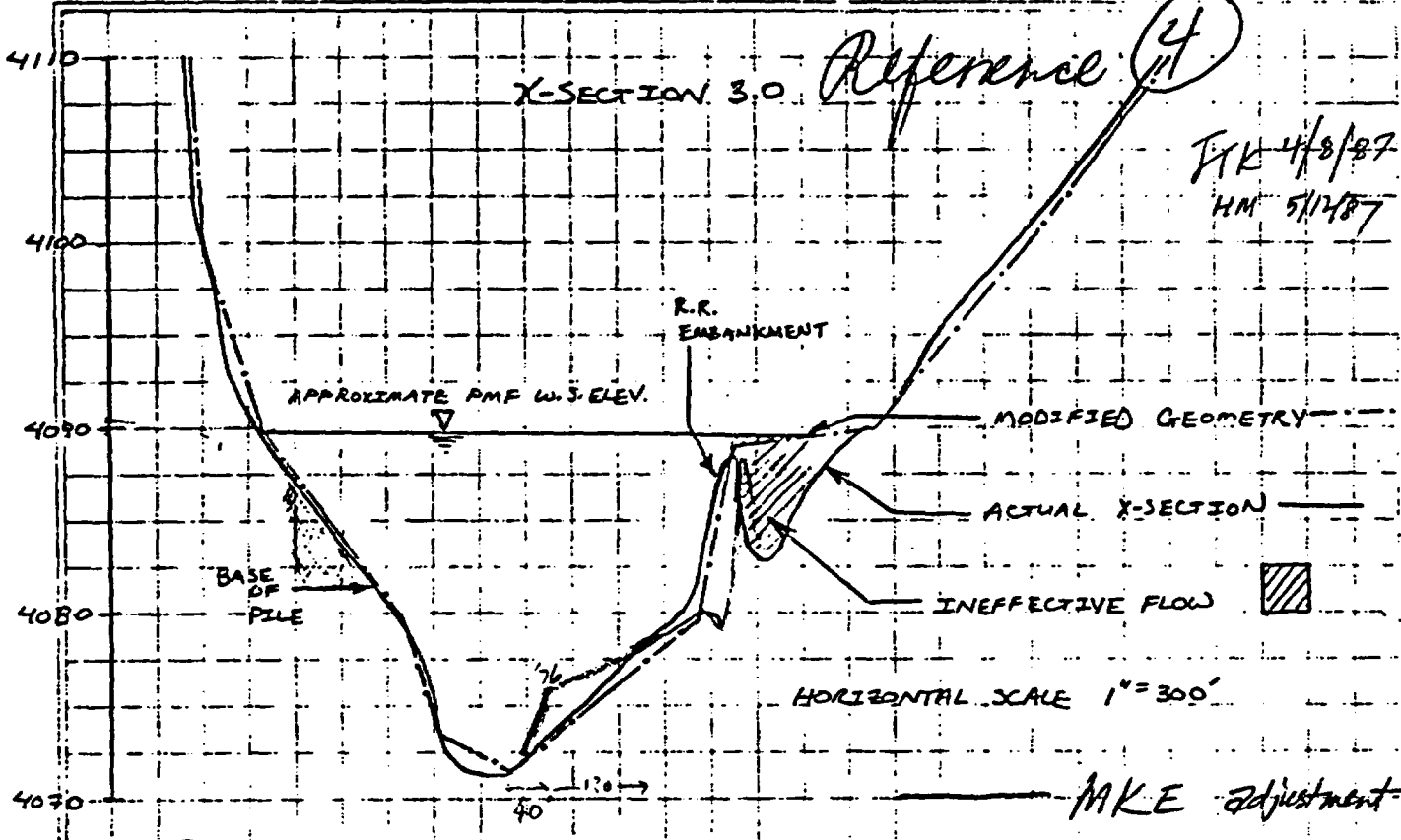


FIGURE 3.0 X-SECTION PLOTS

DATE 2/7/87  
BY RP CHKD. \_\_\_\_\_

SUBJECT GRN SURFACE WATER FLOOD STUDIES  
HYDRAULIC ANALYSIS

SHEET NO. 7  
JOB NO. \_\_\_\_\_

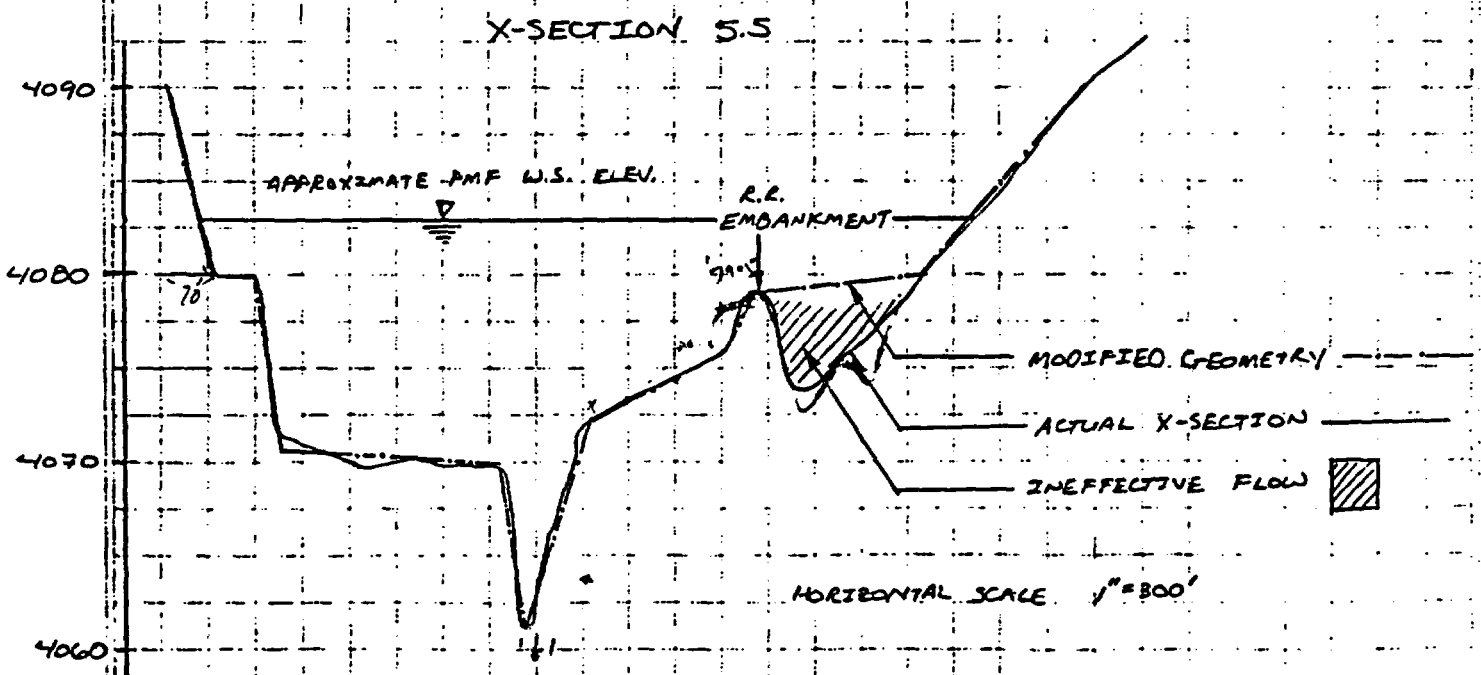
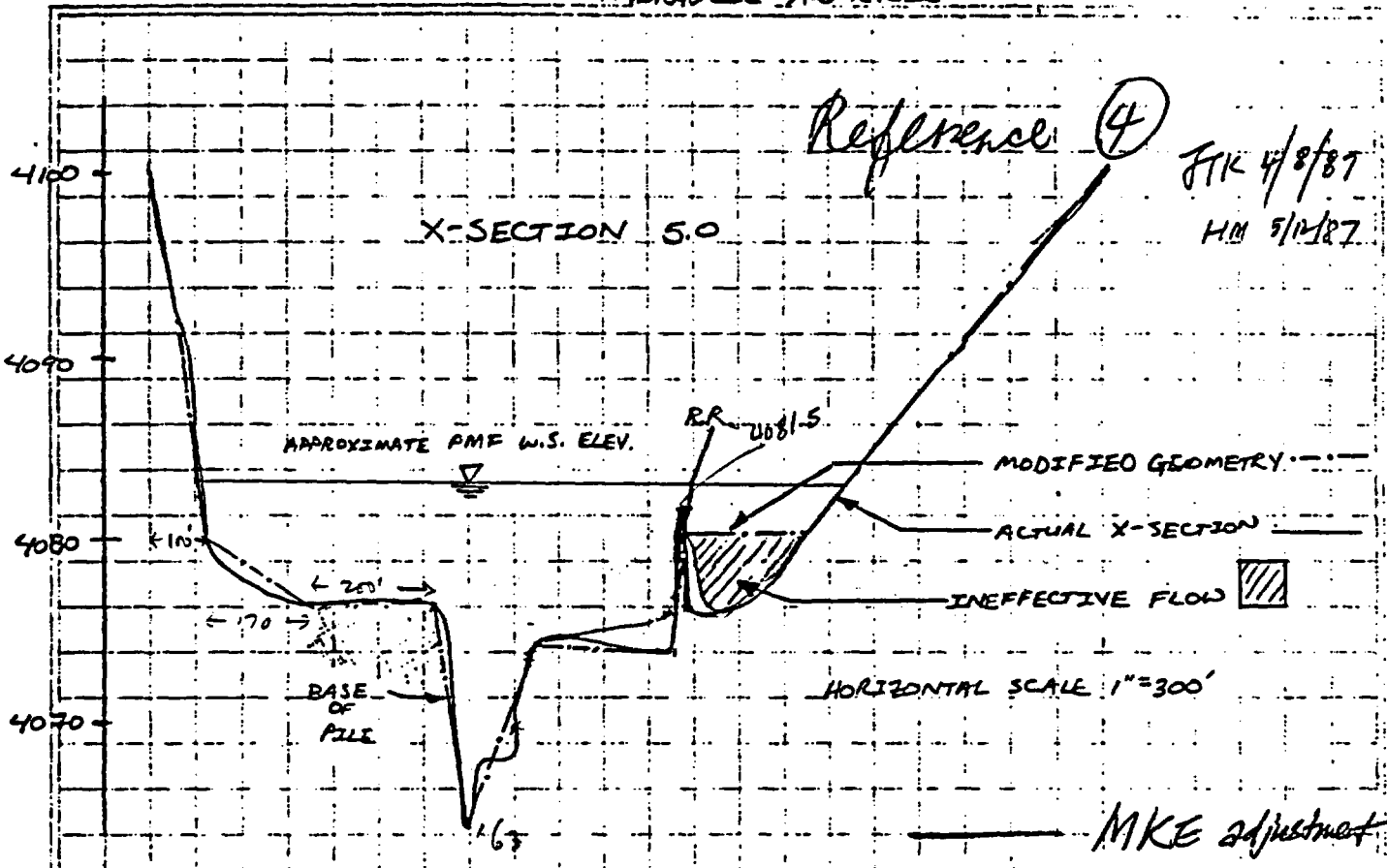


FIGURE 4.0 X-SECTION PLOTS

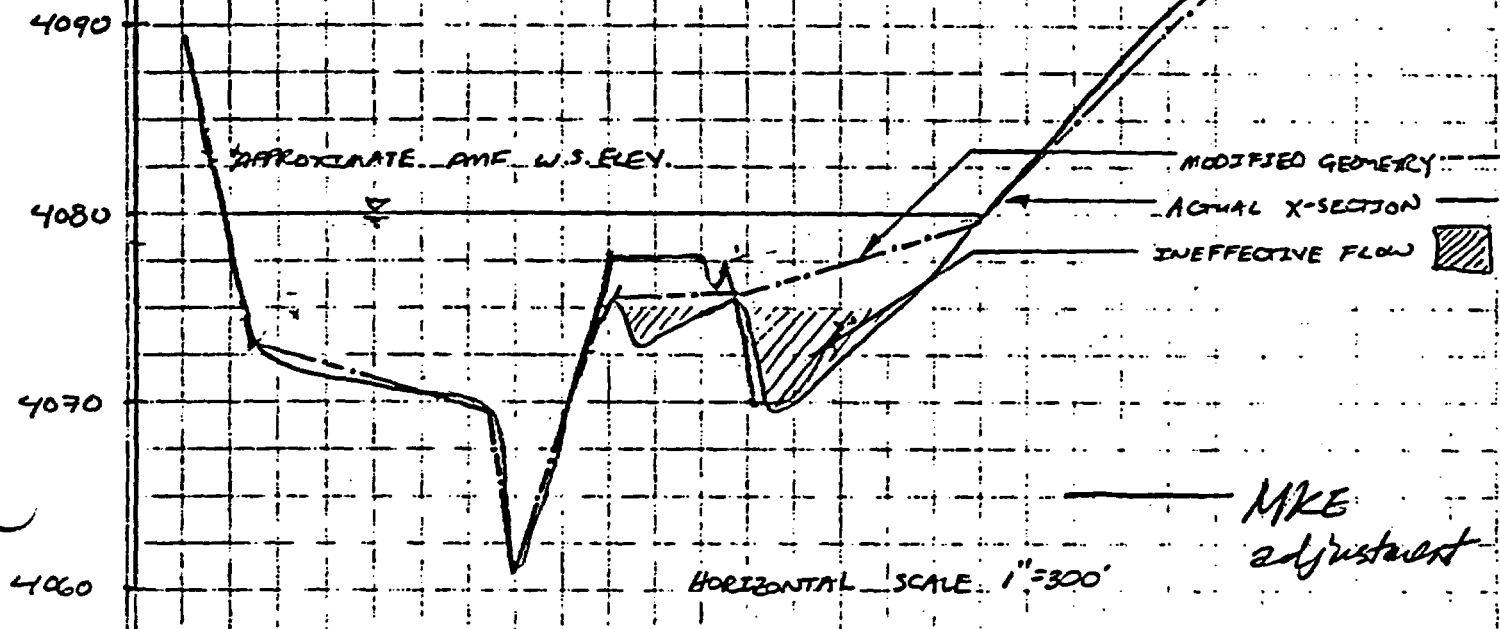
DATE 2/7/87  
BY RP CHKD. \_\_\_\_\_

SUBJECT GRW, SURFACE-WATER FLOOD STUDIES  
HYDRAULIC ANALYSIS

SHEET NO. \_\_\_\_\_  
JOB NO. \_\_\_\_\_

Reference (4) JTK 4/8/87  
HM 5/12/87

X-SECTION 6.0



X-SECTION 7.0

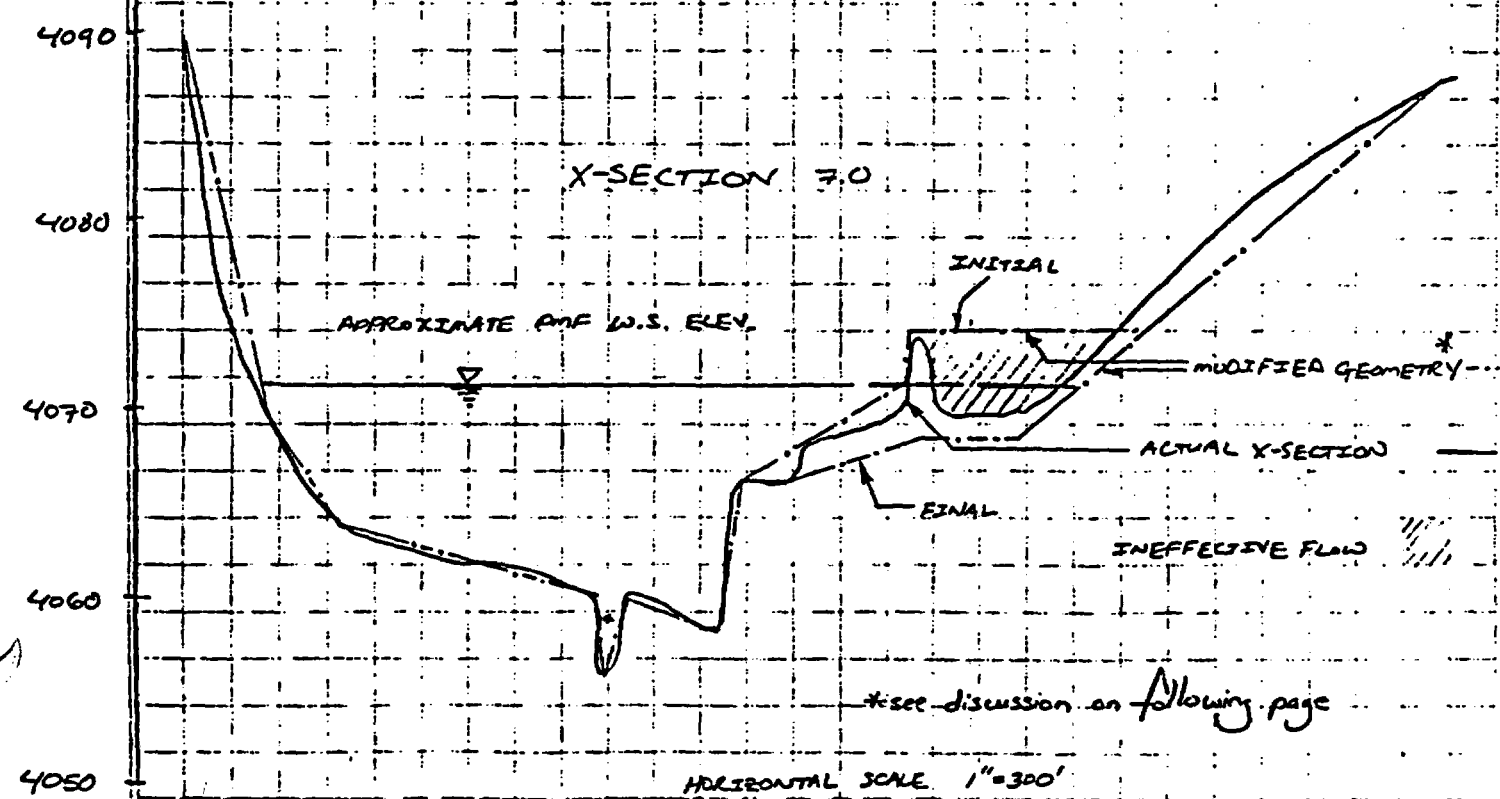
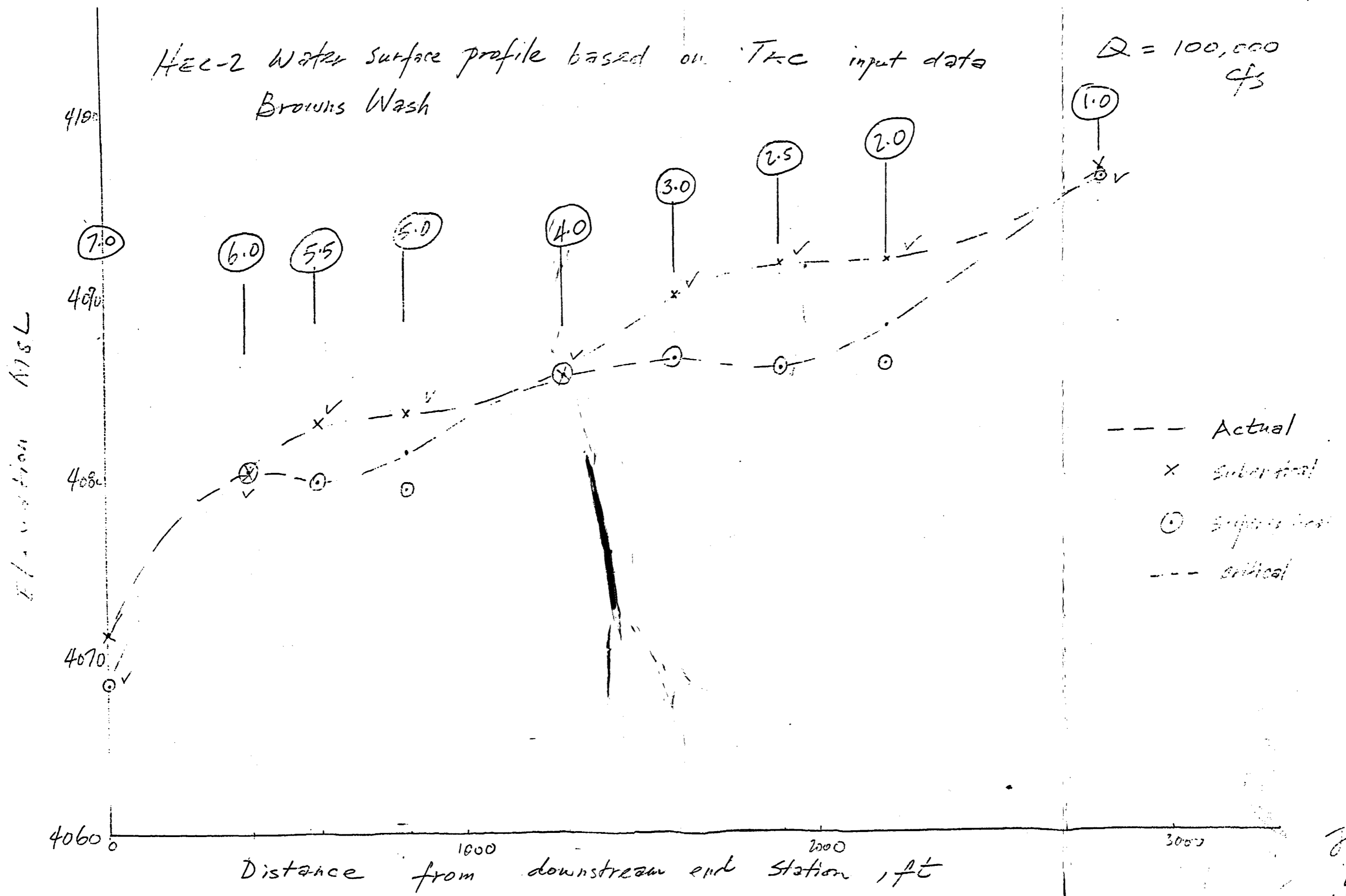


FIGURE 5.0 X-SECTION PLOTS

HEC-2 Water surface profile based on TAC input data  
Browns Wash

Q = 100,000  
cfs



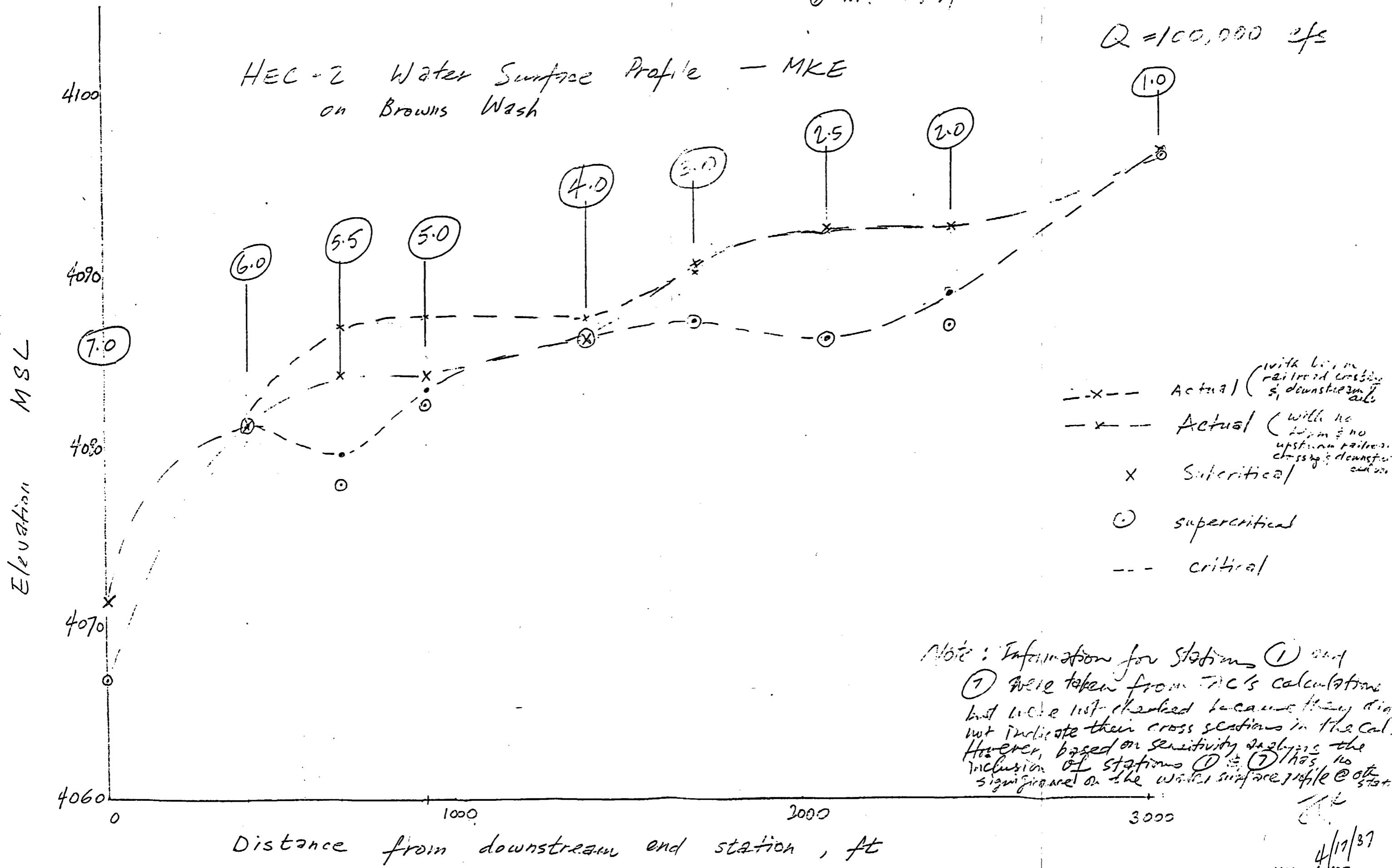
JHC  
4/17/87  
HM 5/14/87



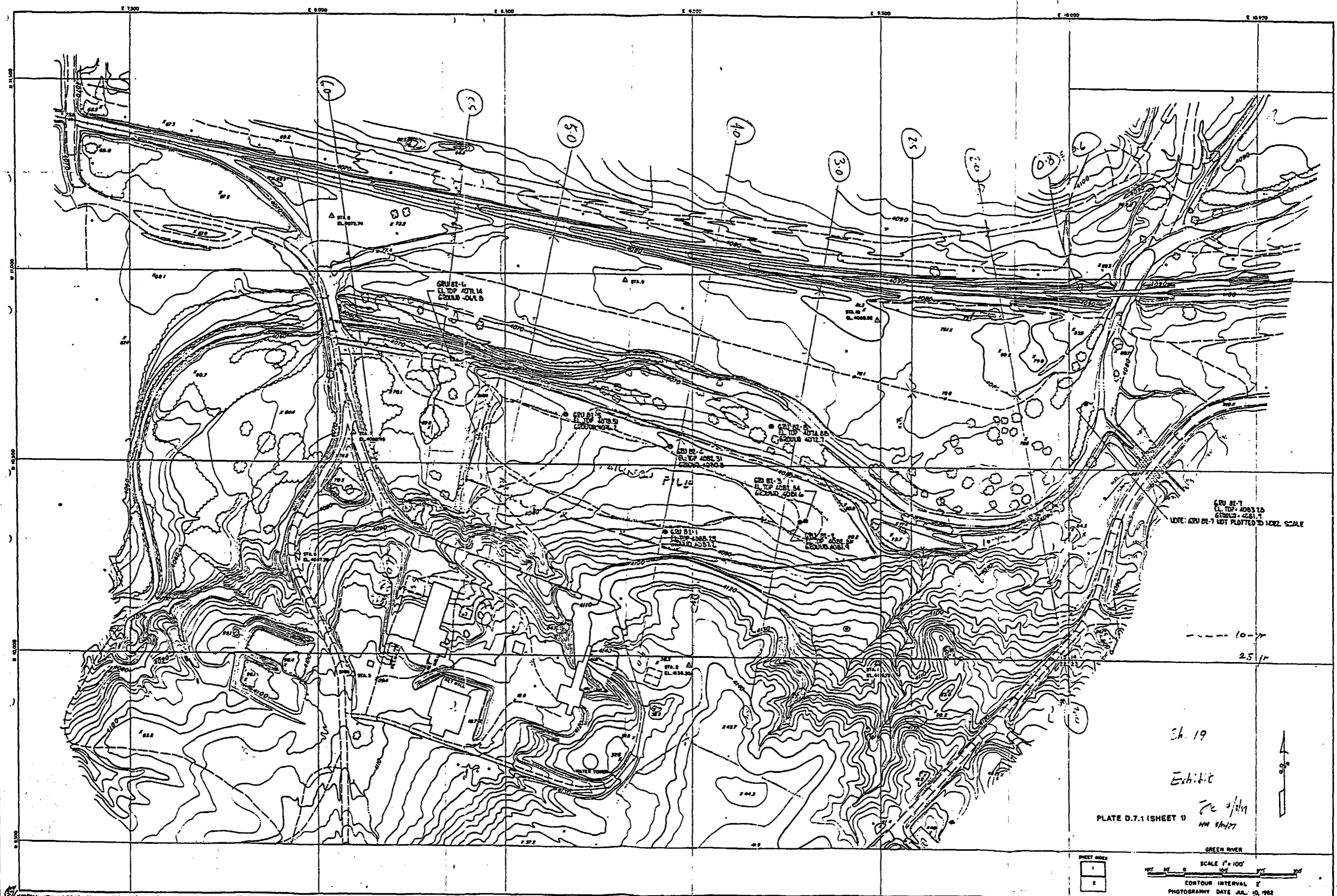
6-hr. PMF

Q = 100,000 cfs

HEC-2 Water Surface Profile - MKE  
on Browns Wash



4/17/37  
HM 5/17/37



GRU 81-7  
CL TOP 4063.16  
GRU 81-7  
NOTE: GRU 81-7 NOT PLOTTED TO THIS SCALE

10-17  
2.5-17

Sh. 19

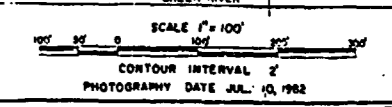
Exhibit

PLATE D.7.1 (SHEET 1)

7/24/62  
MM 5/1/77

GREEN RIVER

1	2
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UMTRA - Green River

Sh. 20-1

General PMF - 72 hr.

JTK

Computation of peak flow

4/3/87  
HM 5/11/87

\*\*\*\*  
FLOOD HYDROGRAPH PACKAGE HEC-1 (IBM XT 512K VERSION) - FEB 1, 1983  
U.S. ARMY CORPS OF ENGINEERS, THE HYDROLOGIC ENGINEERING CENTER, 689 SECOND STREET, DAVIS, CA. 95616  
\*\*\*\*

THIS HEC-1 VERSION CONTAINS ALL OPTIONS EXCEPT ECONOMICS, AND THE NUMBER OF PLANS ARE REDUCED TO 3

HEC-1 INPUT

PAGE 1

LINE	ID	1	2	3	4	5	6	7	8	9	10	
1	ID	UMTRA - GREEN RIVER - BROWN WASH										
2	ID	GENERAL PMF - 72 HR.										
3	IT	9	300									
4	IN	60										
5	ID	5										
6	KK	BAS1 SUB-BASIN 1										
7	KK	GENERAL PMF										
8	DA	2.6										
9	DB	19.4										
10	PI	0.01	0.02	0.02	0.02	0.02	0.01	0.03	0.03	0.03	0.03	
11	PI	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.11	0.12	
12	PI	0.12	0.12	0.12	0.11	0.11	0.12	0.12	0.12	0.12	0.11	
13	PI	0.25	0.25	0.25	0.25	0.25	0.25	0.60	0.60	0.69	0.69	
14	PI	0.60	0.60	0.16	0.17	0.17	0.17	0.17	0.16	0.11	0.12	
15	PI	0.12	0.12	0.12	0.11	0.06	0.07	0.07	0.07	0.07	0.06	
16	PI	0.05	0.05	0.05	0.05	0.05	0.05	0.03	0.03	0.04	0.04	
17	PI	0.03	0.03									
18	LU	0	0.2									
19	UD	0.66										
20	KK	BAS2										
21	KK	GEN. PMF										
22	DA	3.3										
23	LU	0	0.2									
24	UD	0.73										

Sh. 20.2

21.20.2

JTK 4/3/87  
HM 5/1/87

LU 0 0.2  
 UD 0.73

25 RK ST12 COMBINE FWS. 1,2 FLOWS  
 26 MC 2

27 RK 3,4 FLOW 1,2 FROM STR. 1,2 TO 3,4  
 28 RK 25400 .032 .04 TRAP 0 0.45

29 RK D854  
 30 RK GEN. PWF  
 31 DA 6.4  
 32 LU 0 0.2  
 33 UD 0.75

34 RK D853  
 35 RK GEN. PWF  
 36 DA 12.1  
 37 LU 0 0.2  
 38 UD .96

39 RK ST34 COMBINE FLOWS 3,4  
 40 MC 3

41 RK 3,6 FLOW 3,4 FROM STR. 3,4 TO 3,6  
 42 RK 53856 .015 .04 TRAP 0 0.03  
 MEC-1 INPUT

PAGE 2

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

43 RK D855  
 44 RK GEN. PWF  
 45 DA 20.7  
 46 LU 0 0.2  
 47 UD 1.73

48 RK D856  
 49 RK GEN. PWF  
 50 DA 11.8  
 51 LU 0 0.2  
 52 UD 0.95

53 RK ST56 COMBINE FLOWS 3,6  
 54 MC 3

55 RK 7,8 FLOW 3,6 FROM STR. 3,6 TO 7,8  
 56 RK 6336 0.005 .04 TRAP 0 0.025

57 RK D858  
 58 RK GEN. PWF  
 59 DA 0.5  
 60 LU 0 0.2  
 61 UD 0.52

62 RK D857  
 63 RK GEN. PWF  
 64 DA 12.2  
 65 LU 0 0.2  
 66 UD 1.22

67 RK ST78 COMBINE FLOWS 7,8  
 68 MC 3

69 RK 9 FLOWS 7,8 FROM STR. 7,8 TO 9  
 70 RK 32736 0.01 .04 TRAP 0 0.05

71 RK D859

KK BAS9  
 KM GENL PWF  
 BA 11.3  
 LU # 0.2  
 UD 1.39

76 KK ST9 COMBINE FLOWS  
 77 HC 2  
 78 ZZ

\*\*\*\*  
 FLOOD HYDROGRAPH PACKAGE HEC-1 (IBM XT SIZE VERSION) - FEB 1, 1985  
 U.S. ARMY CORPS OF ENGINEERS, THE HYDROLOGIC ENGINEERING CENTER, 609 SECOND STREET, DAVIS, CA. 95616  
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Sh. 20.3

FR 4/3/87  
 HM 5/1/87

UNTRA - GREEN RIVER - BROWN WASH  
 GENERAL PWF - 72 HR.

5 10 OUTPUT CONTROL VARIABLES  
 IPRINT 5 PRINT CONTROL  
 IPLOT 8 PLOT CONTROL  
 USCAL 0. HYDROGRAPH PLOT SCALE

17 HYDROGRAPH TIME DATA  
 NMIN 9 MINUTES IN COMPUTATION INTERVAL  
 IDATE 1 0 STARTING DATE  
 ITIME 0000 STARTING TIME  
 NO 300 NUMBER OF HYDROGRAPH ORDINATES  
 MODATE 2 0 ENDING DATE  
 MOTIME 2051 ENDING TIME

COMPUTATION INTERVAL .15 HOURS  
 TOTAL TIME BASE 44.85 HOURS

ENGLISH UNITS

RUNOFF SUMMARY  
 FLOW IN CUBIC FEET PER SECOND  
 TIME IN HOURS, AREA IN SQUARE MILES

OPERATION	STATION	PEAK FLOW	TIME OF PEAK	AVERAGE FLOW FOR MAXIMUM PERIOD			BASIN AREA	MAXIMUM STAGE	TIME OF MAX STAGE
				6-HOUR	24-HOUR	72-HOUR			
+	HYDROGRAPH AT								
+		BAS1	1137.	48.05	1064.	332.	177.	2.68	
+	HYDROGRAPH AT								
+		BAS2	2404.	48.05	2237.	701.	375.	5.50	
+	2 COMBINED AT								
+		ST12	3540.	48.05	3300.	1033.	553.	8.10	
+	ROUTED TO								
+		3,4	3539.	48.20	3201.	1027.	550.	8.10	
+	HYDROGRAPH AT								
+		BAS4	2797.	48.05	2599.	816.	437.	6.40	
+	HYDROGRAPH AT								
+		BAS3	5273.	48.35	4837.	1530.	823.	12.10	
+	3 COMBINED AT								
+		ST30	11607.	48.35	10703.	3301.	1009.	26.60	

+	ST34	11607.	48.33	18101.	3381.	1889.	26.60
+	ROU	5,6	11504.	41.70	18101.	3144.	26.60
+	HYDROGRAPH AT	8455	8863.	42.00	7782.	2536.	1357.
+	HYDROGRAPH AT	8456	5144.	48.35	4721.	1588.	883.
+	3 COMBINED AT	5736	25436.	41.85	22268.	7188.	3842.
+	ROUTED TO	7,8	25435.	42.00	22253.	7186.	3883.
+	HYDROGRAPH AT	8458	219.	39.98	287.	64.	34.
+	HYDROGRAPH AT	8457	5286.	48.88	4779.	1548.	824.
+	3 COMBINED AT	9778	38911.	41.85	27892.	8718.	4661.
+	ROUTED TO	9	38896.	42.38	26982.	8299.	4441.
+	HYDROGRAPH AT	8459	4873.	41.25	4366.	1415.	757.
+	2 COMBINED AT	579	35749.	42.15	31853.	9715.	5198.

Sh. 20.4

JTK

4/3/87

HM 5/11/87

\*\*\* NORMAL END OF REC-1 \*\*\*

UMTRA - Green River

Sh. 21.1

Local PMF - 6 hr.

Computation of peak flow

JTK 4/3/87  
HM 5/2/87

Sh. 21.2

JTK  
4/5/87

\*\*\*\*  
FLOOD HYDROGRAPH PACKAGE HEC-1 (IBM XT 512K VERSION) - FEB 1, 1985  
U.S. ARMY CORPS OF ENGINEERS, THE HYDROLOGIC ENGINEERING CENTER, 609 SECOND STREET, DAVIS, CA. 95616  
\*\*\*\*

THIS HEC-1 VERSION CONTAINS ALL OPTIONS EXCEPT ECONOMICS, AND THE NUMBER OF PLANS ARE REDUCED TO 3

1

HEC-1 INPUT

PAGE 1

LINE	ID	1	2	3	4	5	6	7	8	9	10
1	ID	UNTRA - GREEN RIVER - BROWN WASH									
2	ID	LOCAL PWF = 6.1%									
3	IT	9									
4	IN	15									
5	IO	5									
6	IK	BAS1 SUB-BASIN 1									
7	IK	LOCAL PWF									
8	BA	2.6									
9	PD	4.958									
10	PI	.0425	.0425	.0425	.0425	.065	.065	.065	.065	1.62	.84
11	PI	.46	.37	.202	.202	.202	.202	.065	.065	.065	.065
12	PI	.0225	.0225	.0225	.0225						
13	LU	0 0.2									
14	LD	.66									
15	IK	BAS2									
16	IK	LOCAL PWF									
17	BA	3.5									
18	PD	4.958									
19	PI	.0425	.0425	.0425	.0425	.065	.065	.065	.065	1.62	.84





70	KK	7.8	FLOW 5,6 FROM STA. 5,6 TO 7,8								
71	KK	6336	0.005	.04	TRAP	0	0.025				
72	KK	0458									
73	KK	LOCAL PPF									
74	BA	0.5									
75	PB	5.99									
76	PI	.0425	.0425	.0425	.0425	.065	.065	.065	2.27	1.05	
77	PI	.49	.41	.2275	.2275	.2275	.2275	.065	.065	.065	
78	PI	.0225	.0225	.0225	.0225						
79	LU	0	0.2								
80	UB	0.52									
81	KK	0457									
82	KK	LOCAL PPF									
83	BA	12.2									
84	PB	5.34									
85	PI	.0425	.0425	.0425	.0425	.065	.065	.065	.065	1.74	.96
86	PI	.48	.48	.225	.225	.225	.225	.065	.065	.065	.065
87	PI	.0225	.0225	.0225	.0225						
88	LU	0	0.2								
89	UB	1.22									

Sh. 21.4

JKK

4/3/07

HM 5/11/07

HEC-1 INPUT

PAGE 3

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

90	KK	ST78	COMBINE FLOWS 7,8								
91	HC	3									
92	KK	9	FLOWS 7,8 FROM STA. 7,8 TO 9								
93	KK	32736	0.01	.04	TRAP	0	0.05				
94	KK	0459									
95	KK	LOCAL PPF									
96	BA	11.3									
97	PB	4.11									
98	PI	.0425	.0425	.0425	.0425	.065	.065	.065	.065	1.01	.68
99	PI	.43	.34	.1975	.1975	.1975	.1975	.065	.065	.065	.065
100	PI	.0225	.0225	.0225	.0225						
101	LU	0	0.2								
102	UB	1.39									
103	KK	ST9	COMBINE FLOWS								
104	HC	2									
105	ZZ										

\*\*\*\*  
 FLOOD HYDROGRAPH PACKAGE HEC-1 (IBM XT 512K VERSION) - FEB 1, 1985  
 U.S. ARMY CORPS OF ENGINEERS, THE HYDROLOGIC ENGINEERING CENTER, 609 SECOND STREET, DAVIS, CA. 95616  
 \*\*\*\*

UTTRA - GREEN RIVER - BROWN WASH  
 LOCAL PPF - 6 HR.

5 10

OUTPUT CONTROL VARIABLES

IPRINT 5 PRINT CONTROL  
 IPLOT 0 PLOT CONTROL  
 USCAL 0. HYDROGRAPH PLOT SCALE

11

HYDROGRAPH TIME DATA

MIN 9 MINUTES IN COMPUTATION INTERVAL  
 IDATE 1 0 STARTING DATE  
 ITIME 0000 STARTING TIME  
 NO 300 NUMBER OF HYDROGRAPH ORDINATES  
 NDATE 0 FINISH DATE

NAME NO 0000 SIMPLI.  
 NO 300 NUMBER OF HYDROGRAPH ORDINATES  
 MODATE 2 0 ENDING DATE  
 MODTIME 2051 ENDING TIME

COMPUTATION INTERVAL .15 HOURS  
 TOTAL TIME BASE 44.65 HOURS

ENGLISH UNITS

RUNOFF SUMMARY  
 FLOW IN CUBIC FEET PER SECOND  
 TIME IN HOURS, AREA IN SQUARE MILES

OPERATION	STATION	PEAK FLOW	TIME OF PEAK	AVERAGE FLOW FOR MAXIMUM PERIOD			BASIN AREA	MAXIMUM STAGE	TIME OF MAX STAGE
				6-HOUR	24-HOUR	72-HOUR			
HYDROGRAPH AT									
+	BAS1	4220.	3.00	1088.	272.	146.	2.60		
HYDROGRAPH AT									
+	BAS2	8487.	3.00	2301.	576.	300.	5.50		
2 COMBINED AT									
+	5T12	12636.	3.00	3350.	840.	454.	8.10		
ROUTED TO									
+	3,4	12383.	3.15	3304.	840.	454.	8.10		
HYDROGRAPH AT									
+	BAS4	9630.	3.15	2678.	670.	355.	6.40		
HYDROGRAPH AT									
+	BAS3	17106.	3.30	5327.	1304.	741.	12.10		
3 COMBINED AT									
+	5T34	38432.	3.15	11303.	2902.	1533.	26.00		
ROUTED TO									
+	5,6	34831.	4.05	11423.	2912.	1530.	26.00		
HYDROGRAPH AT									
+	BAS5	23187.	4.20	10720.	2741.	1467.	28.70		
HYDROGRAPH AT									
+	BAS6	23930.	3.30	7210.	1807.	967.	11.00		
3 COMBINED AT									
+	5T36	71154.	4.05	29163.	7453.	3992.	59.10		
ROUTED TO									
+	7,8	70792.	4.20	29273.	7497.	4012.	59.10		
HYDROGRAPH AT									
+	BAS8	1216.	2.05	263.	66.	35.	.50		
HYDROGRAPH AT									
+	BAS7	14057.	3.60	3577.	1402.	750.	12.20		
3 COMBINED AT									
+	5T78	84443.	4.05	35040.	8965.	4790.	71.00		
ROUTED TO									
+	9	81819.	4.35	34632.	8972.	4882.	71.00		
HYDROGRAPH AT									
+	BAS9	8670.	3.90	3637.	923.	495.	11.30		

Sh. 21.5

JTK

4/3/07

HM 5/1/07

HYDROGRAPH AT

2455 8870 3.90 3857. 923. 493. 11.30

2 COMBINED AT

579 89741. 4.35 38163. 9897. 5297. 83.10

\*\*\* NORMAL END OF REC-1 \*\*\*

St. 21.6

JFK

4/3/87

MM 5/11/87

\*\*\*\*\*  
 \* WATER SURFACE PROFILES \*  
 \* VERSION OF NOVEMBER 1976 \*  
 \* UPDATED MAY 1984 \*  
 \*  
 \* RUN DATE 9-APR-87 TIME 09:24:14 \*  
 \*\*\*\*\*

\*\*\*\*\*  
 \* U. S. ARMY CORPS OF ENGINEERS \*  
 \* THE HYDROLOGIC ENGINEERING CENTER \*  
 \* 609 SECOND STREET, SUITE D \*  
 \* DAVIS, CALIFORNIA 95616 \*  
 \* (916) 440-2105 (FTS) 448-2105 \*  
 \*\*\*\*\*

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X   X   XXXXXXX   XXXXX           XXXXX
X   X   X         X   X         X   X
X   X   X         X   X         X   X
XXXXXXXX XXXX     X   X         XXXXX
X   X   X         X   X         X
X   X   X         X   X         X
X   X   XXXXXXX   XXXXX           XXXXXXX
  
```

Sh. 22 A.1

UMTRA - Green  
 River

Using TAC's data 12/4

Subcritical flow  
 using 7 cross sections

For 4/1/87 use 4/1/87

Sh. 22A-2

FRK 4/9/87  
HM 5/14/87

\*\*\*\*\*  
 HEC2 RELEASE DATED NOV 76 UPDATED MAY 1984  
 ERROR CORR - 01, 02, 03, 04, 05, 06  
 MODIFICATION - 50, 51, 52, 53, 54, 55, 56  
 \*\*\*\*\*

T1 UMTRA - GREEN RIVER - LOCAL PMF  
 T2 WATER SURFACE PROFILE ON BROWN WASH  
 T3

J1	ICHECK	ING	NINV	IDIR	STRT	METRIC	HVINS	Q	WSEL	FG
	0.	0.	0.	0.	0.009000	0.00	0.0	100000.	4074.000	0.000
J2	NPROF	IPLT	PRFVS	XSECV	XSECH	FN	ALLDC	IBW	CHNIM	ITRACE
	-1.000	0.000	0.000	0.000	0.000	0.000	-1.000	0.000	0.000	0.000
J3	VARIABLE CODES FOR SUMMARY PRINTOUT									
	38.000	43.000	1.000	2.000	13.000	14.000	15.000	35.000	60.000	59.000
	55.000	26.000	56.000	0.000	38.000	58.000	25.000	1.000	42.000	8.000
	51.000	10.000	4.000	53.000	54.000	33.000	5.000	0.000	0.000	0.000
NC	0.045	0.050	0.035	0.100	0.300	0.000	0.000	0.000	0.000	0.000
X1	7.000	12.000	242.000	970.000	0.000	0.000	0.000	0.000	0.000	0.000
GR	4090.000	0.000	4070.000	140.000	4064.000	242.000	4060.000	665.000	4056.000	680.000
GR	4060.000	710.000	4068.000	860.000	4066.000	915.000	<del>4066.000</del>	970.000	4068.000	1180.000
GR	4068.000	1350.000	4088.000	2040.000	0.000	0.000	0.000	0.000	0.000	0.000
X1	6.000	8.000	110.000	890.000	385.000	410.000	400.000	0.000	0.000	0.000
GR	4090.000	0.000	<del>4074.000</del>	110.000	4070.000	490.000	4062.000	525.000	4076.000 <sup>076</sup>	685.000
GR	<del>4076.000</del> <sup>110</sup>	890.000	4080.000	1265.000	4100.000	1885.000	0.000	0.000	0.000	0.000
X1	5.500	11.000	180.000	890.000	100.000	270.000	190.000	0.000	0.000	0.000
GR	4090.000	0.000	4080.000	80.000	4080.000	140.000	4071.000	180.000	4070.000	530.000
GR	4062.000	570.000	4073.000	680.000	<del>4076.000</del>	890.000	<del>4079.000</del>	940.000	4080.000	1200.000
GR	4090.000	1460.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
NC	0.000	0.000	0.000	0.200	0.500	0.000	0.000	0.000	0.000	0.000
X1	5.000	10.000	270.000	876.000	230.000	290.000	250.000	0.000	0.000	0.000
GR	4100.000	0.000	4080.000	95.000	<del>4076.000</del>	270.000	4076.000	470.000	4064.000	530.000
GR	4074.000	635.000	<del>4064.000</del> <sup>4076</sup>	876.000	4080.000 <sup>4080</sup>	890.000	4080.000 <sup>4102</sup>	1090.000	4110.000	1885.000

X1	4.000	9.000	385.000	840.000	470.000	440 420.000 1/60	440.000 460	0.000	0.000	1.000
GR	4130.000	0.000	4090.000	100.000	4080.000	385.000	4068.000	530.000	4078.000	800.000 750
GR	4080.000	840.000	4086.000	870.000	4090.000	1165.000	4120.000	1930.000	0.000	0.000
X1	3.000	11.000	400.000	880.000	315.000	320 305.000 3/8	320.000 318	0.000	0.000	1.000
GR	4130.000	0.000	4100.000	80.000	4090.000	170.000	4080.000	400.000	4074.000	455.000
GR	4072.000	570.000	4080.000	880.000	4088.000	925.000	4090.000	1150.000	4110.000	1640.000
GR	4120.000	1820.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
NC	0.000	0.000	0.000	0.100	0.300	0.000	0.000	0.000	0.000	0.000
X1	2.500	11.000	300.000	960.000	365.000	240.000 280	300.000 380	0.000	0.000	0.000
GR	4110.000	0.000	4090.000	250.000	4080.000	300.000	4073.000	420.000	4076.000	500.000
GR	4076.000	560.000	4078.000	620.000	4078.000 460	960.000	4091.000	1000.000	4096.000	1330.000
GR	4110.000	1700.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
X1	2.000	10.000	380.000	920.000	335.000 370	250.000 380 370	300.000 350	0.000	0.000	0.000
GR	4114.000	0.000	4090.000	200.000	4080.000	380.000	4074.000	400.000	4074.000	430.000
GR	4078.000	510.000	4080.000	920.000	4094.000	990.000	4094.000	1170.000	4120.000	1890.000
X1	1.000	7.000	150.000	765.000	730.000	510.000	610.000	0.000	0.000	0.000
GR	4104.000	0.000	4090.000	150.000	4084.000	390.000	4080.000	470.000	4102.000	765.000
GR	4110.000	1145.000	4120.000	1385.000	0.000	0.000	0.000	0.000	0.000	0.000
EJ	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000

Sh. 22A.3

JTK 4/9/87  
HM 5/14/87

9-APR-87 09:24:14

PAGE 3

Sh. 22. A. 4

JTK 4/9/87  
HM 5/12/87

SECNO	DEPTH	CWSEL	CRISW	WSELK	EQ	HV	HL	QLOSS	BANK ELEV
Q	GLOB	GCH	GROB	ALOB	ACH	AROB	VOL	TWA	LEFT/RIGHT
TIME	VLOB	VCH	VROB	XNL	XNCH	XNR	WTN	ELMIN	SSTA
SLOPE	XLOBL	XLCH	XLOBR	ITRIAL	IDC	ICONT	CORAR	TOPWID	ENDST

\*PROF 1

CRITICAL DEPTH TO BE CALCULATED AT ALL CROSS SECTIONS

CCHV= 0.100 CEHV= 0.300

\*SECNO 7.000

3720 CRITICAL DEPTH ASSUMED

7.00	15.15	4071.15	4071.15	4074.00	4074.11	2.96	0.00	0.00	4064.00
100000.	3022.	87956.	9022.	428.	6044.	1577.	0.	0.	4066.00
0.00	7.07	14.55	5.72	0.045	0.035	0.050	0.000	4056.00	131.97
0.007001	0.	0.	0.	0	10	4	0.00	1326.60	1458.57

\*SECNO 6.000

7185 MINIMUM SPECIFIC ENERGY

3720 CRITICAL DEPTH ASSUMED

6.00	18.22	4080.22	4080.22	0.00	4083.66	3.43	2.98	0.14	4074.00
100000.	829.	95414.	3758.	133.	6283.	834.	70.	12.	4076.00
0.01	6.23	15.19	4.51	0.045	0.035	0.050	0.000	4062.00	67.23
0.007943	385.	400.	410.	0	11	0	0.00	1204.65	1271.87

\*SECNO 5.500

3301 HV CHANGED MORE THAN HVINS

5.50	20.81	4082.81	4079.53	0.00	4084.61	1.80	0.79	0.16	4071.00
100000.	2424.	93317.	4258.	492.	8409.	1228.	110.	18.	4076.00
0.01	4.92	11.10	3.47	0.045	0.035	0.050	0.000	4062.00	57.54
0.002537	100.	190.	270.	3	8	0	0.00	1215.48	1273.01

CCHV= 0.200 CEHV= 0.500

\*SECNO 5.000

5.00	19.29	4083.29	4081.19	0.00	4085.57	2.28	0.72	0.24	4076.00
100000.	5373.	90789.	3838.	952.	7201.	960.	165.	24.	4064.00
0.02	5.64	12.61	4.00	0.045	0.035	0.050	0.000	4064.00	79.36
0.003265	230.	250.	290.	3	12	0	0.00	1097.89	1177.25

\*SECNO 4.000



9-APR-87 09:24:14

SECNO	DEPTH	CHSEL	CRISW	WSELK	EQ	HV	HL	GLOSS	BANK	ELEV
G	GLOB	GCH	GROB	ALOB	ACH	AROB	VOL	TWA	LEFT/RIGHT	
TIME	VLOB	VCH	VROB	XML	XNCH	XNR	WTN	ELMIN	BSTA	
SLOPE	XLOBL	XLCH	XLOBR	ITRIAL	IDC	ICONT	CORAR	TOPWID	ENDST	

Sh. 22A.5

JTK 4/9/87  
HM 5/14/87

3301 HV CHANGED MORE THAN HVINS

7185 MINIMUM SPECIFIC ENERGY  
3720 CRITICAL DEPTH ASSUMED

4.00	17.44	4085.44	4085.44	0.00	4090.60	5.15	2.06	1.44	4080.00
100000.	2306.	97334.	360.	422.	5277.	74.	241.	33.	4080.00
0.03	5.46	18.45	4.85	0.045	0.035	0.050	0.000	4068.00	229.86
0.007205	470.	440.	420.	0	11	0	0.00	637.35	867.22

\*SECNO 3.000

3301 HV CHANGED MORE THAN HVINS

3.00	17.89	4089.89	4086.49	0.00	4092.47	2.58	1.35	0.52	4080.00
100000.	5689.	92666.	1646.	1125.	6957.	466.	293.	39.	4080.00
0.03	5.06	13.32	3.53	0.045	0.035	0.050	0.000	4072.00	172.54
0.002788	315.	320.	305.	4	15	0	0.00	965.01	1137.56

CCHV= 0.100 CEHV= 0.300  
\*SECNO 2.500

3301 HV CHANGED MORE THAN HVINS

2.50	18.65	4091.65	4085.88	0.00	4093.19	1.54	0.62	0.10	4080.00
100000.	1542.	97239.	1219.	350.	9650.	300.	359.	45.	4078.00
0.04	4.41	10.08	4.06	0.045	0.035	0.050	0.000	4073.00	229.36
0.001576	365.	300.	240.	2	19	0	0.00	813.61	1042.97

\*SECNO 2.000

3301 HV CHANGED MORE THAN HVINS

2.00	17.78	4091.78	4088.18	0.00	4094.00	2.21	0.60	0.20	4080.00
100000.	7433.	90862.	1706.	1235.	7335.	347.	425.	51.	4080.00
0.05	6.02	12.39	4.91	0.045	0.035	0.050	0.000	4074.00	185.11
0.002633	335.	300.	250.	2	15	0	0.00	793.82	978.93

Sh. 22A.6

9-APR-87 09:24:14

SECNO	DEPTH	CWSEL	CRISW	WSELK	EQ	HV	HL	CLOSS	BANK	ELEV
Q	QLOB	QCH	QROB	ALOB	ACH	AROB	VOL	TWA	LEFT/RIGHT	
TIME	VLOB	VCH	VROB	XNL	XNCH	XNR	WTN	ELMIN	SSTA	
SLOPE	XLOBL	XLCH	XLOBR	ITRIAL	IDC	ICONT	CORAR	TOPWID	ENDST	

\*SECNO 1.000

3301 HV CHANGED MORE THAN HVINS

7185 MINIMUM SPECIFIC ENERGY

3720 CRITICAL DEPTH ASSUMED

1.00	16.93	4096.93	4096.93	0.00	4101.81	4.88	2.63	0.80	4090.00	
100000.	1755.	98245.	0.	258.	5501.	0.	530.	61.	4102.00	
0.06	6.82	17.86	0.00	0.045	0.035	0.000	0.000	4080.00	75.72	
0.008167	730.	610.	510.	0	11	0	0.00	621.34	697.06	

JTK  
4/9/87  
HM 9/14/87

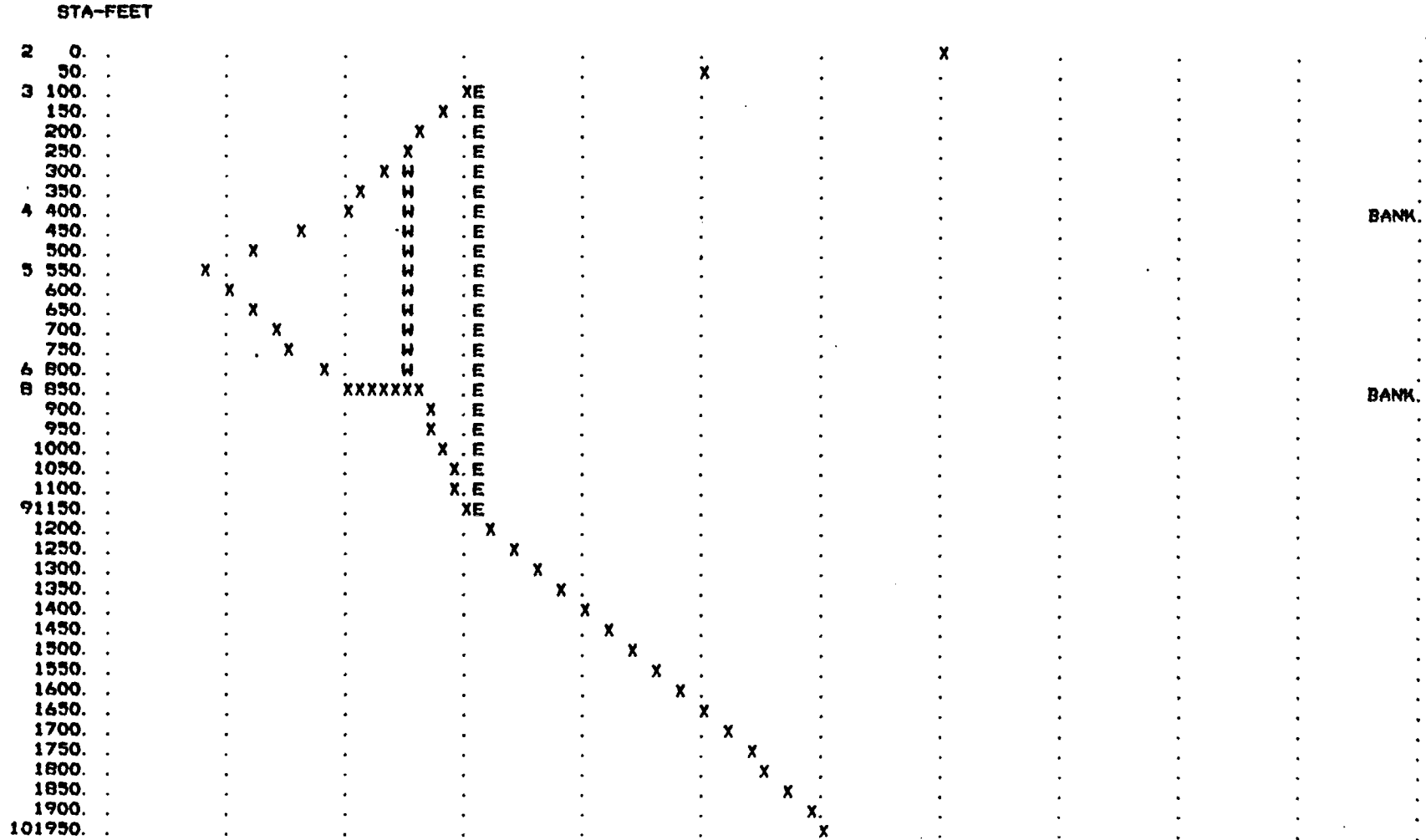
CROSS SECTION 4.00  
 STREAM  
 DISCHARGE= 100000.

PLOTTED POINTS (BY PRIORITY)-B=BOTTOM BRIDGE, T=TOP BRIDGE, X=GROUND, W=WATER SUR, E=ENERGY GRADIENT, C=CRITICAL WSEL

ELEV 4060. 4070. 4080. 4090. 4100. 4110. 4120. 4130. 4140. 4150. 4160.

*Sh. 22A.7*

*JFK 4/9/87  
 HM 5/14/87*



NRD= 0 ELLC= 9999999.00 ELTRD= 9999999.00

EL(I), STA(I)	4130.00	0.00	4090.00	100.00	4080.00	385.00	4068.00	530.00	4078.00	800.00
	4080.00	840.00	4086.00	870.00	4090.00	1165.00	4120.00	1930.00		







\*\*\*\*\*  
 HEC2 RELEASE DATED NOV 76 UPDATED MAY 1984  
 ERROR CORR - 01, 02, 03, 04, 05, 06  
 MODIFICATION - 30, 31, 32, 33, 54, 55, 56  
 \*\*\*\*\*

*Sh. 22x.11*

*JK 4/9/87*  
*HM 5/14/87*

NOTE- ASTERISK (\*) AT LEFT OF CROSS-SECTION NUMBER INDICATES MESSAGE IN SUMMARY OF ERRORS LIST

SUMMARY PRINTOUT

	SECNO	Q	CWSEL	CRWS	GLOB	GCH	GRDB	GLOBP	GCHP	GRDBP	VLOB	VCH	VROB
*	7.000	100000.00	4071.15	4071.15	3022.18	87956.16	9021.66	3.02	87.96	9.02	7.07	14.55	5.72
*	6.000	100000.00	4080.22	4080.22	828.76	95413.52	3757.72	0.83	93.41	3.76	6.23	15.19	4.51
	5.500	100000.00	4082.81	4079.53	2424.47	93317.07	4258.46	2.42	93.32	4.26	4.92	11.10	3.47
	5.000	100000.00	4083.29	4081.19	5373.17	90789.27	3837.36	5.37	90.79	3.84	5.64	12.61	4.00
*	4.000	100000.00	4085.44	4085.44	2306.18	97334.28	359.55	2.31	97.33	0.36	5.46	18.45	4.85
	3.000	100000.00	4089.89	4086.49	5688.55	92665.67	1645.78	5.69	92.67	1.65	5.06	13.32	3.53
	2.500	100000.00	4091.65	4085.88	1541.68	97238.88	1219.45	1.54	97.24	1.22	4.41	10.08	4.06
	2.000	100000.00	4091.78	4088.18	7432.88	90861.55	1705.56	7.43	90.86	1.71	6.02	12.39	4.91
*	1.000	100000.00	4096.93	4096.93	1755.21	98244.80	0.00	1.76	98.24	0.00	6.82	17.86	0.00

9-APR-87 09:24:14

PAGE 7 Sh. 22A.12

JTK 4/9/87  
HIM 5/14/87

SUMMARY PRINTOUT

	SECNO	KRATIO	AREA	CHSEL	ELMIN	DEPTH	DIFWSX	HV	TOPWID	BBTA	ENDST	K*CHSL	10K*8
*	7.000	0.00	8048.28	4071.15	4056.00	15.15	0.00	2.96	1326.60	131.97	1458.57	0.00	70.01
*	6.000	0.94	7249.86	4080.22	4062.00	18.22	9.07	3.43	1204.65	67.23	1271.87	15.00	79.43
	5.500	1.77	10129.13	4082.81	4062.00	20.81	2.59	1.80	1215.48	57.54	1273.01	0.00	25.37
	5.000	0.88	9113.40	4083.29	4064.00	19.29	0.48	2.28	1097.89	79.36	1177.25	8.00	32.65
*	4.000	0.67	5773.03	4085.44	4068.00	17.44	2.15	5.15	637.35	229.86	867.22	9.09	72.05
	3.000	1.61	8547.39	4089.89	4072.00	17.89	4.45	2.58	965.01	172.54	1137.56	12.50	27.88
	2.500	1.33	10299.36	4091.65	4073.00	18.65	1.76	1.54	813.61	229.36	1042.97	3.33	15.76
	2.000	0.77	8916.78	4091.78	4074.00	17.78	0.13	2.21	793.82	185.11	978.93	3.33	26.33
*	1.000	0.57	5758.50	4096.93	4080.00	16.93	5.15	4.88	621.34	75.72	697.06	9.84	81.67



SUMMARY OF ERRORS AND SPECIAL NOTES

CAUTION	SECNO=	7.000	PROFILE= 1	CRITICAL DEPTH ASSUMED
CAUTION	SECNO=	6.000	PROFILE= 1	CRITICAL DEPTH ASSUMED
CAUTION	SECNO=	6.000	PROFILE= 1	MINIMUM SPECIFIC ENERGY
CAUTION	SECNO=	4.000	PROFILE= 1	CRITICAL DEPTH ASSUMED
CAUTION	SECNO=	4.000	PROFILE= 1	MINIMUM SPECIFIC ENERGY
CAUTION	SECNO=	1.000	PROFILE= 1	CRITICAL DEPTH ASSUMED
CAUTION	SECNO=	1.000	PROFILE= 1	MINIMUM SPECIFIC ENERGY

Sh. 22A.13

JTK 4/9/87

HM 5/12/87

9-APR-87 09:24:25

PAGE 1

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HEC2 RELEASE DATED NOV 76 UPDATED MAY 1984  
ERROR CORR - 01,02,03,04,05,06  
MODIFICATION - 50,51,52,53,54,55,56  
\*\*\*\*\*



\* WATER SURFACE PROFILES \*  
\* VE OF NOVEMBER 1976 \*  
\* UPL J MAY 1984 \*  
\* RUN DATE 16-APR-87 TIME 15:51:20 \*  
\*\*\*\*\*

\* U.S. ARMY CORPS OF ENGINEERS \*  
\* THE HYDROLOGIC ENGINEERING CENTER \*  
\* 609 SECOND STREET, SUITE 100 \*  
\* DAVIS, CALIFORNIA 95616 \*  
\* (916) 440-2105 (FTS) 448-2105 \*  
\*\*\*\*\*

SH. 22B-2

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X      X  XXXXXXXX  XXXXX      XXXXX
X      X  X          X          X
X      X  X          X          X
XXXXXXX XXXX      X          XXXXX
X      X  X          X          X
X      X  X          X          X
X      X  XXXXXXXX  XXXXX      XXXXXXXX

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JR 4/16/87  
HM 5/14/87

\*\*\*\*\*  
 HEC2 RELEASE DATED NOV 76 UPDATED MAY 1984  
 ERROR CORR - 01, 02, 03, 04, 05, 06  
 MODIFICATION - 50, 51, 52, 53, 54, 55, 56  
 \*\*\*\*\*

Sh. 22 B. 3

T1 UMTRA - GREEN RIVER - LOCAL PMF  
 T2 WATER SURFACE PROFILE ON BROWN WASH  
 T3 DISCHARGE = 100000 CFS

FRK 4/16/87  
 HM 5/14/87

J1	ICHECK	ING	NINV	IDIR	STRT	METRIC	HWINS	Q	WSEL	FG
	0.	0.	0.	0.	0.009000	0.00	0.0	100000.	4074.000	0.000
J2	NPROF	IPLDT	PRFVS	XSECV	XSECH	FN	ALLDC	IBW	CHNIM	ITRACE
	-1.000	0.000	0.000	0.000	0.000	0.000	-1.000	0.000	0.000	0.000
J3	VARIABLE CODES FOR SUMMARY PRINTOUT									
	38.000	43.000	1.000	2.000	13.000	14.000	15.000	35.000	60.000	59.000
	55.000	26.000	56.000	0.000	38.000	58.000	25.000	1.000	42.000	8.000
	51.000	10.000	4.000	53.000	54.000	33.000	5.000	0.000	0.000	0.000

NC	0.045	0.050	0.035	0.100	0.300	0.000	0.000	0.000	0.000	0.000
X1	7.000	12.000	242.000	970.000	0.000	0.000	0.000	0.000	0.000	0.000
QR	4090.000	0.000	4070.000	140.000	4064.000	242.000	4060.000	665.000	4036.000	680.000
QR	4060.000	710.000	4068.000	860.000	4066.000	915.000	4066.000	970.000	4068.000	1180.000
QR	4068.000	1350.000	4088.000	2040.000	0.000	0.000	0.000	0.000	0.000	0.000
X1	4.000	8.000	110.000	890.000	385.000	410.000	400.000	0.000	0.000	0.000
QR	4090.000	0.000	4074.000	110.000	4070.000	490.000	4062.000	525.000	4078.000	685.000
QR	4078.000	890.000	4080.000	1265.000	4100.000	1885.000	0.000	0.000	0.000	0.000
X1	5.500	11.000	180.000	890.000	150.000	280.000	270.000	0.000	0.000	0.000
QR	4090.000	0.000	4080.000	80.000	4080.000	140.000	4071.000	180.000	4070.000	530.000
QR	4062.000	570.000	4073.000	680.000	4076.000	890.000	4079.000	940.000	4080.000	1200.000
QR	4090.000	1460.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
NC	0.000	0.000	0.000	0.200	0.500	0.000	0.000	0.000	0.000	0.000
X1	5.000	10.000	270.000	876.000	230.000	290.000	250.000	0.000	0.000	0.000
QR	4100.000	0.000	4080.000	95.000	4076.000	270.000	4076.000	470.000	4064.000	530.000
QR	4074.000	635.000	4076.000	876.000	4082.000	890.000	4082.000	1090.000	4110.000	1885.000

Sh. 22 B. 4



SECNO	DEPTH	CWSEL	CRWS	WSELK	E0	HV	HL	OLOSS	BANK ELEV
G	GLOB	GCH	GROB	ALOB	ACH	AROB	VOL	TWA	LEFT/RIGHT
TIME	VLOB	VCH	VROB	XNL	XNCH	XNR	WTN	ELMIN	BSTA
SLOPE	XLOBL	XLCH	XLOBR	ITRIAL	IDC	ICONT	CORAR	TOPWID	ENDST

Sh. 22B.5

\*PROF 1

CRITICAL DEPTH TO BE CALCULATED AT ALL CROSS SECTIONS

CCHV= 0.100 CEHV= 0.300

\*SECNO 7.000

3720 CRITICAL DEPTH ASSUMED

7.00	15.15	4071.15	4071.15	4074.00	4074.11	2.96	0.00	0.00	4064.00
100000.	3022.	87956.	9022.	428.	6044.	1577.	0.	0.	4066.00
0.00	7.07	14.55	5.72	0.045	0.035	0.050	0.000	4056.00	131.97
0.007001	0.	0.	0.	0	10	4	0.00	1326.60	1458.57

\*SECNO 6.000

7185 MINIMUM SPECIFIC ENERGY

3720 CRITICAL DEPTH ASSUMED

6.00	19.23	4081.23	4081.23	0.00	4084.42	3.19	2.81	0.07	4074.00
100000.	1168.	95213.	3617.	180.	6503.	861.	72.	12.	4078.00
0.01	6.49	14.64	4.20	0.045	0.035	0.050	0.000	4062.00	60.27
0.007056	385.	400.	410.	0	13	0	0.00	1242.99	1303.26

\*SECNO 5.500

3301 HV CHANGED MORE THAN HVINS

5.50	22.05	4084.05	4079.53	0.00	4085.43	1.38	0.83	0.18	4071.00
100000.	2930.	91205.	5865.	650.	9290.	1723.	130.	19.	4076.00
0.02	4.50	9.82	3.40	0.045	0.035	0.050	0.000	4062.00	47.61
0.001739	150.	270.	280.	3	11	0	0.00	1257.66	1305.27

CCHV= 0.200 CEHV= 0.500

\*SECNO 5.000

3301 HV CHANGED MORE THAN HVINS

5.00	19.92	4083.92	4083.07	0.00	4086.99	3.07	0.71	0.84	4076.00
100000.	8396.	89778.	1826.	1073.	6136.	505.	187.	26.	4076.00
0.02	7.83	14.63	3.61	0.045	0.035	0.050	0.000	4064.00	76.38
0.005440	230.	250.	290.	3	15	0	0.00	1068.16	1144.54

Jrk 4/16/87  
HM 5/12/87

Sh. 22B.6

JTK 4/16/87  
HM 5/14/87

SECNO	DEPTH	CWSEL	CRWS	WSELK	EQ	HV	HL	DLOSS	BANK ELEV
G	GLOB	GCH	GROB	ALOB	ACH	AROB	VOL	TWA	LEFT/RIGHT
TIME	VLOB	VCH	VROB	XNL	XNCH	XNR	WTN	ELMIN	SSTA
SLOPE	XLOBL	XLCH	XLOBR	ITRIAL	IDC	ICONT	CORAR	TOPWID	ENDST

\*SECNO 4.000

3301 HV CHANGED MORE THAN HVINS

7185 MINIMUM SPECIFIC ENERGY  
3720 CRITICAL DEPTH ASSUMED

4.00	18.09	4086.09	4086.09	0.00	4091.12	5.03	2.85	0.98	4080.00
100000.	3088.	96426.	486.	528.	5271.	93.	259.	36.	4080.00
0.03	5.84	18.29	5.23	0.045	0.035	0.050	0.000	4068.00	211.44
0.007098	470.	460.	440.	0	11	0	0.00	665.19	876.63

\*SECNO 3.000

3301 HV CHANGED MORE THAN HVINS

3.00	18.42	4090.42	4087.25	0.00	4092.99	2.57	1.38	0.49	4080.00
100000.	6845.	90925.	2230.	1247.	6791.	610.	312.	42.	4080.00
0.04	5.49	13.39	3.66	0.045	0.035	0.050	0.000	4072.00	166.24
0.002911	315.	318.	320.	4	11	0	0.00	994.00	1160.24

CCHV= 0.100 CEHV= 0.300  
\*SECNO 2.500

3301 HV CHANGED MORE THAN HVINS

2.50	19.41	4092.41	4086.14	0.00	4093.84	1.43	0.74	0.11	4080.00
100000.	1768.	97086.	1146.	407.	9991.	342.	396.	50.	4080.00
0.05	4.35	9.72	3.35	0.045	0.035	0.050	0.000	4073.00	219.87
0.001399	365.	380.	380.	2	19	0	0.00	873.24	1093.10

\*SECNO 2.000

3301 HV CHANGED MORE THAN HVINS

2.00	18.54	4092.54	4088.80	0.00	4094.71	2.17	0.65	0.22	4080.00
100000.	8786.	88643.	2570.	1385.	7174.	506.	475.	56.	4080.00
0.05	6.34	12.36	5.08	0.045	0.035	0.050	0.000	4074.00	178.78
0.002565	350.	350.	300.	2	15	0	0.00	801.88	980.66



16-APR 15:51:21

PAGE

SECNO	DEPTH	CWSEL	CRISW	WSELK	EQ	HV	HL	OLOSS	BANK ELEV
Q	GLOB	GCH	GRWB	ALOB	ACH	AROB	VOL	TWA	LEFT/RIGHT
TIME	VLOB	VCH	VROB	XNL	XNCH	XNR	WTN	ELMIN	SSTA
SLOPE	XLOBL	XLCH	XLOBR	ITRIAL	IDC	ICONT	CORAR	TOPWID	ENDST

\*SECNO 1.000

3301 HV CHANGED MORE THAN HVINS

7185 MINIMUM SPECIFIC ENERGY

3720 CRITICAL DEPTH ASSUMED

1.00	16.94	4096.94	4096.94	0.00	4101.81	4.87	2.59	0.81	4090.00
100000.	1758.	98242.	0.	258.	5505.	0.	580.	67.	4102.00
0.06	6.81	17.85	0.00	0.045	0.035	0.000	0.000	4080.00	75.64
0.008149	730.	610.	310.	0	11	0	0.00	621.52	697.16

Sh. 22 B. 7

JK 4/16/87

HM 5/17/87

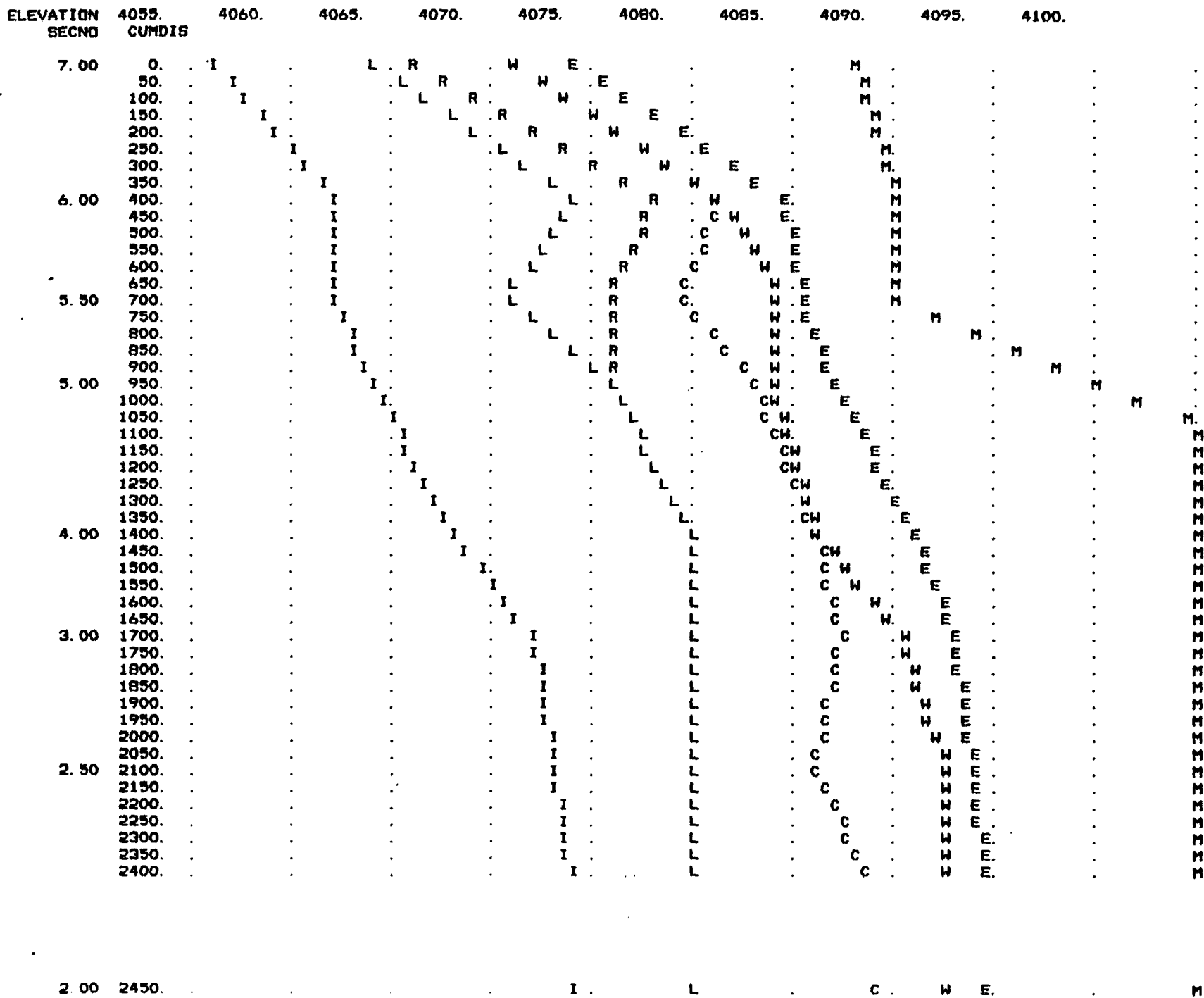
Sh. 22 B. 9





PLOTTED POINTS (BY PRIORITY)-E-ENERGY, W-WATER SURFACE, I-INVERT, C-CRITICAL W. S., L-LEFT BANK, R-RIGHT BANK, M-LOWER END STA

FKL  
4/16/87  
MM 9/2/17





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 HEC2 RELEASE DATED NOV 76 UPDATED MAY 1984  
 ERROR CORR - 01, 02, 03, 04, 05, 06  
 MODIFICATION - 50, 51, 52, 53, 54, 55, 56  
 \*\*\*\*\*

Sh. 22B.12

JTK 4/16/87  
HM 5/12/87

NOTE- ASTERISK (\*) AT LEFT OF CROSS-SECTION NUMBER INDICATES MESSAGE IN SUMMARY OF ERRORS LIST

DISCHARGE = 100000 CFS

SUMMARY PRINTOUT

	SECNO	Q	CWSEL	CRIWS	QLOB	GCH	GROB	GLOBP	GCHP	GROBP	VLOB	VCH	VROB
*	7.000	100000.00	4071.15	4071.15	3022.18	87956.16	9021.66	3.02	87.96	9.02	7.07	14.55	5.72
*	6.000	100000.00	4081.23	4081.23	1167.62	95215.20	3617.18	1.17	95.22	3.62	6.49	14.64	4.20
	5.500	100000.00	4084.05	4079.53	2929.98	91205.13	5864.88	2.93	91.21	5.86	4.50	9.82	3.40
	5.000	100000.00	4083.92	4083.07	8396.17	89777.63	1826.18	8.40	89.78	1.83	7.83	14.63	3.61
*	4.000	100000.00	4086.09	4086.09	3087.51	96426.41	486.08	3.09	96.43	0.49	5.84	18.29	5.23
	3.000	100000.00	4090.42	4087.25	6844.99	90925.29	2229.72	6.84	90.93	2.23	5.49	13.39	3.66
	2.500	100000.00	4092.41	4086.14	1768.09	97085.75	1146.17	1.77	97.09	1.15	4.35	9.72	3.35
	2.000	100000.00	4092.54	4088.80	8786.27	88643.24	2570.50	8.79	88.64	2.57	6.34	12.36	5.08
*	1.000	100000.00	4096.94	4096.94	1758.18	98241.83	0.00	1.76	98.24	0.00	6.81	17.85	0.00

16-APR-87 15:51:21

PAGE 7

DISCHARGE = 100000 CFS

SUMMARY PRINTOUT

	SECND	KRATIO	AREA	CWSEL	ELMIN	DEPTH	DIFWSX	HV	TOPWID	SSTA	ENDST	K*CHSL	10K*8
*	7.000	0.00	8048.28	4071.15	4056.00	15.15	0.00	2.96	1326.60	131.97	1458.57	0.00	70.01
*	6.000	1.00	7543.91	4081.23	4062.00	19.23	10.09	3.19	1242.99	60.27	1303.26	15.00	70.56
	5.500	2.01	11663.37	4084.05	4062.00	22.05	2.82	1.38	1257.66	47.61	1305.27	0.00	17.39
	5.000	0.57	7714.19	4083.92	4064.00	19.92	-0.13	3.07	1068.16	76.38	1144.54	8.00	54.40
*	4.000	0.88	5892.35	4086.09	4068.00	18.09	2.17	5.03	665.19	211.44	876.63	8.70	70.98
	3.000	1.56	8647.54	4090.42	4072.00	18.42	4.33	2.57	994.00	166.24	1160.24	12.58	29.11
	2.500	1.44	10739.97	4092.41	4073.00	19.41	1.99	1.43	873.24	219.87	1093.10	2.63	13.99
	2.000	0.74	9065.85	4092.54	4074.00	18.54	0.13	2.17	801.88	178.78	980.66	2.86	25.65
*	1.000	0.56	5763.05	4096.94	4080.00	16.94	4.40	4.87	621.52	75.64	697.16	9.84	81.49

Sh. 22B.13

JK

4/16/87

HM 5/14/87

16-APR-87 15:51:21

Sh. 22B.14  
PAGE 8

FTK 4/16/87  
HM 5/14/87

SUMMARY OF ERRORS AND SPECIAL NOTES

CAUTION	SECNO=	7.000	PROFILE= 1	CRITICAL DEPTH ASSUMED
CAUTION	SECNO=	6.000	PROFILE= 1	CRITICAL DEPTH ASSUMED
CAUTION	SECNO=	6.000	PROFILE= 1	MINIMUM SPECIFIC ENERGY
CAUTION	SECNO=	4.000	PROFILE= 1	CRITICAL DEPTH ASSUMED
CAUTION	SECNO=	4.000	PROFILE= 1	MINIMUM SPECIFIC ENERGY
CAUTION	SECNO=	1.000	PROFILE= 1	CRITICAL DEPTH ASSUMED
CAUTION	SECNO=	1.000	PROFILE= 1	MINIMUM SPECIFIC ENERGY



16-APR-87 15:51:32

PAGE 1

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HEC2 RELEASE DATED NOV 76 UPDATED MAY 1984  
ERROR CORR - 01,02,03,04,05,06  
MODIFICATION - 50,51,52,53,54,55,56  
\*\*\*\*\*

Sh. 22B.15

JTK 4/16/87  
HM 9/14/87



\*\*\*\*\*  
 \* WATER SURFACE PROFILES \*  
 \* VERSION OF NOVEMBER 1976 \*  
 \* UPDATED MAY 1984 \*  
 \* \*  
 \* RUN DATE 21-APR-87 TIME 11:26:38 \*  
 \*\*\*\*\*

\*\*\*\*\*  
 \* U. S. ARMY CORPS OF ENGINEERS \*  
 \* THE HYDROLOGIC ENGINEERING CENTER \*  
 \* 609 SECOND STREET, SUITE D \*  
 \* DAVIS, CALIFORNIA 95616 \*  
 \* (916) 440-2105 (FTS) 448-2105 \*  
 \*\*\*\*\*

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X      X  XXXXXXXX  XXXXX      XXXXX
X      X  X          X          X
X      X  X          X          X
XXXXXXXX XXXX      X          XXXXX
X      X  X          X          X
X      X  X          X          X
X      X  XXXXXXXX  XXXXX      XXXXXXXX
  
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Sh. 22c.1

LIMTRA - Green River

Subcritical flow

using 5 cross sections

JK 4/21/87  
 HM 5/11/87

Sh. 22 C. 2

\*\*\*\*\*  
 HEC2 RELEASE DATED NOV 76 UPDATED MAY 1984  
 ERROR CORR - 01, 02, 03, 04, 05, 06  
 MODIFICATION - 50, 51, 52, 53, 54, 55, 56  
 \*\*\*\*\*

JK 4/21/87  
 HM 9/19/81

T1 UMTRA - GREEN RIVER - LOCAL PMF  
 T2 WATER SURFACE PROFILE ON BROWN WASH  
 T3 DISCHARGE = 100000 CFS

J1	ICHECK	ING	NINV	IDIR	STRT	METRIC	HVINS	G	WBEL	FG
	0.	0.	0.	0.	0.009000	0.00	0.0	100000.	4074.000	0.000

J2	NPROF	IPLT	PRFVS	XSECV	XSECH	FN	ALLDC	IBW	CHNIM	ITRACE
	-1.000	0.000	0.000	0.000	0.000	0.000	-1.000	0.000	0.000	0.000

J3 VARIABLE CODES FOR SUMMARY PRINTOUT

38.000	43.000	1.000	2.000	13.000	14.000	15.000	35.000	60.000	59.000
55.000	26.000	56.000	0.000	38.000	58.000	25.000	1.000	42.000	8.000
51.000	10.000	4.000	53.000	54.000	33.000	5.000	0.000	0.000	0.000

NC	0.045	0.050	0.035	0.100	0.300	0.000	0.000	0.000	0.000	0.000
X1	6.000	8.000	110.000	890.000	385.000	410.000	400.000	0.000	0.000	0.000
GR	4090.000	0.000	4074.000	110.000	4070.000	490.000	4062.000	525.000	4078.000	685.000
GR	4078.000	890.000	4080.000	1265.000	4100.000	1885.000	0.000	0.000	0.000	0.000
X1	5.500	11.000	180.000	890.000	150.000	280.000	270.000	0.000	0.000	0.000
GR	4090.000	0.000	4080.000	80.000	4080.000	140.000	4071.000	180.000	4070.000	530.000
GR	4062.000	570.000	4073.000	680.000	4076.000	890.000	4079.000	940.000	4080.000	1200.000
GR	4090.000	1460.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
NC	0.000	0.000	0.000	0.200	0.500	0.000	0.000	0.000	0.000	0.000
X1	5.000	10.000	270.000	876.000	230.000	290.000	250.000	0.000	0.000	0.000
GR	4100.000	0.000	4080.000	95.000	4076.000	270.000	4076.000	470.000	4064.000	530.000
GR	4074.000	635.000	4076.000	876.000	4082.000	890.000	4082.000	1090.000	4110.000	1885.000
X1	4.000	9.000	385.000	840.000	470.000	440.000	460.000	0.000	0.000	1.000
GR	4130.000	0.000	4090.000	100.000	4080.000	385.000	4068.000	530.000	4078.000	750.000
GR	4080.000	840.000	4086.000	870.000	4090.000	1165.000	4120.000	1930.000	0.000	0.000

X1	3.000	12.000	400.000	880.000	315.000	320.000	318.000	0.000	0.000	1.000
QR	4130.000	0.000	4100.000	80.000	4090.000	170.000	4080.000	400.000	4074.000	455.000
QR	4072.000	570.000	4076.000	620.000	4080.000	880.000	4088.000	925.000	4090.000	1150.000
QR	4110.000	1640.000	4120.000	1820.000	0.000	0.000	0.000	0.000	0.000	0.000
NC	0.000	0.000	0.000	0.100	0.300	0.000	0.000	0.000	0.000	0.000
X1	2.500	12.000	300.000	960.000	365.000	380.000	380.000	0.000	0.000	0.000
QR	4110.000	0.000	4090.000	250.000	4080.000	300.000	4073.000	420.000	4076.000	500.000
QR	4076.000	560.000	4078.000	620.000	4078.000	800.000	4080.000	960.000	4091.000	1000.000
QR	4096.000	1330.000	4110.000	1700.000	0.000	0.000	0.000	0.000	0.000	0.000
X1	2.000	11.000	380.000	900.000	350.000	300.000	350.000	0.000	0.000	0.000
QR	4114.000	0.000	4090.000	200.000	4080.000	380.000	4074.000	400.000	4074.000	430.000
QR	4078.000	510.000	4080.000	600.000	4080.000	900.000	4094.000	990.000	4094.000	1170.000
QR	4120.000	1890.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
EJ	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000

SH. 22C. 3

FRK 4/21/87  
HM 5/19/87

Sh. 22 C. 4

21-APR-87 11:26:38

JTK 4/21/87  
HN 5/14/87

SECNO	DEPTH	CWSEL	CRWS	WSELK	EG	HV	HL	OLOSS	BANK	ELEV
G	GLOB	GCH	GROB	ALOB	ACH	AROB	VOL	TWA	LEFT	RIGHT
TIME	VLOB	VCH	VROB	XML	XNCH	XNR	WTN	ELMIN	SSTA	
SLOPE	XLOBL	XLCH	XLOBR	ITRIAL	IDC	ICONT	CORAR	TOPWID	ENDST	

\*PROF 1

CRITICAL DEPTH TO BE CALCULATED AT ALL CROSS SECTIONS

CCHV= 0.100 CEHV= 0.300

\*SECNO 6.000

3720 CRITICAL DEPTH ASSUMED

6.00	18.96	4080.96	4080.96	4074.00	4084.43	3.47	0.00	0.00	4074.00	
100000.	1120.	95806.	3074.	166.	6286.	748.	0.	0.	4078.00	
0.00	6.73	15.24	4.11	0.045	0.035	0.050	0.000	4062.00	62.17	
0.007998	385.	400.	410.	0	17	6	0.00	1232.48	1294.65	

\*SECNO 5.300

3301 HV CHANGED MORE THAN HVINS

5.50	22.13	4084.13	4079.53	0.00	4085.49	1.36	0.85	0.21	4071.00	
100000.	2962.	91072.	5966.	661.	9347.	1757.	58.	8.	4076.00	
0.01	4.48	9.74	3.40	0.045	0.035	0.050	0.000	4062.00	46.97	
0.001698	150.	270.	280.	3	11	0	0.00	1260.39	1307.36	

CCHV= 0.200 CEHV= 0.500

\*SECNO 5.000

3301 HV CHANGED MORE THAN HVINS

5.00	20.00	4084.00	4083.07	0.00	4087.01	3.00	0.69	0.82	4076.00	
100000.	8467.	89616.	1917.	1089.	6187.	528.	115.	15.	4076.00	
0.01	7.78	14.48	3.63	0.045	0.035	0.050	0.000	4064.00	75.98	
0.005274	230.	250.	290.	3	15	0	0.00	1070.94	1146.92	

\*SECNO 4.000

3301 HV CHANGED MORE THAN HVINS

7185 MINIMUM SPECIFIC ENERGY

3720 CRITICAL DEPTH ASSUMED

4.00	18.09	4086.09	4086.09	0.00	4091.12	5.03	2.80	1.01	4080.00	
100000.	3091.	96422.	487.	529.	5273.	93.	187.	24.	4080.00	
0.02	5.84	18.29	5.23	0.045	0.035	0.050	0.000	4068.00	211.32	
0.007088	470.	460.	440.	0	11	0	0.00	665.61	876.93	

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Sh. 22 C. 5

FRK 4/21/87  
HM 5/19/87

SECNO	DEPTH	CWSEL	CRISW	WSELK	EQ	HV	HL	OLOSS	BANK	ELEV
Q	GLOB	GCH	GROB	ALOB	ACH	AROB	VOL	TWA	LEFT/RIGHT	
TIME	VLOB	VCH	VRQB	XLN	XNCH	XNR	WTN	ELMIN	SSTA	
SLOPE	XLOBL	XLCH	XLOBR	ITRIAL	IDC	ICONT	CORAR	TOPWID	ENDBT	

\*SECNO 3.000

3301 HV CHANGED MORE THAN HVINS

3.00	18.42	4090.42	4087.25	0.00	4092.99	2.57	1.38	0.49	4080.00	
100000.	6842.	90930.	2228.	1246.	6789.	609.	240.	30.	4080.00	
0.03	5.49	13.39	3.66	0.045	0.035	0.050	0.000	4072.00	166.26	
0.002913	315.	318.	320.	4	11	0	0.00	993.92	1160.18	

CCHV= 0.100 CEHV= 0.300  
\*SECNO 2.500

3301 HV CHANGED MORE THAN HVINS

2.50	19.41	4092.41	4086.14	0.00	4093.84	1.43	0.74	0.11	4080.00	
100000.	1768.	97086.	1146.	407.	9991.	342.	324.	38.	4080.00	
0.04	4.35	9.72	3.35	0.045	0.035	0.050	0.000	4073.00	219.88	
0.001400	365.	380.	380.	2	19	0	0.00	873.18	1093.05	

\*SECNO 2.000

3301 HV CHANGED MORE THAN HVINS

2.00	18.54	4092.54	4088.79	0.00	4094.71	2.17	0.65	0.22	4080.00	
100000.	8786.	88644.	2570.	1385.	7174.	506.	403.	44.	4080.00	
0.05	6.34	12.36	5.08	0.045	0.035	0.050	0.000	4074.00	178.78	
0.002566	350.	350.	300.	2	15	0	0.00	801.87	980.65	

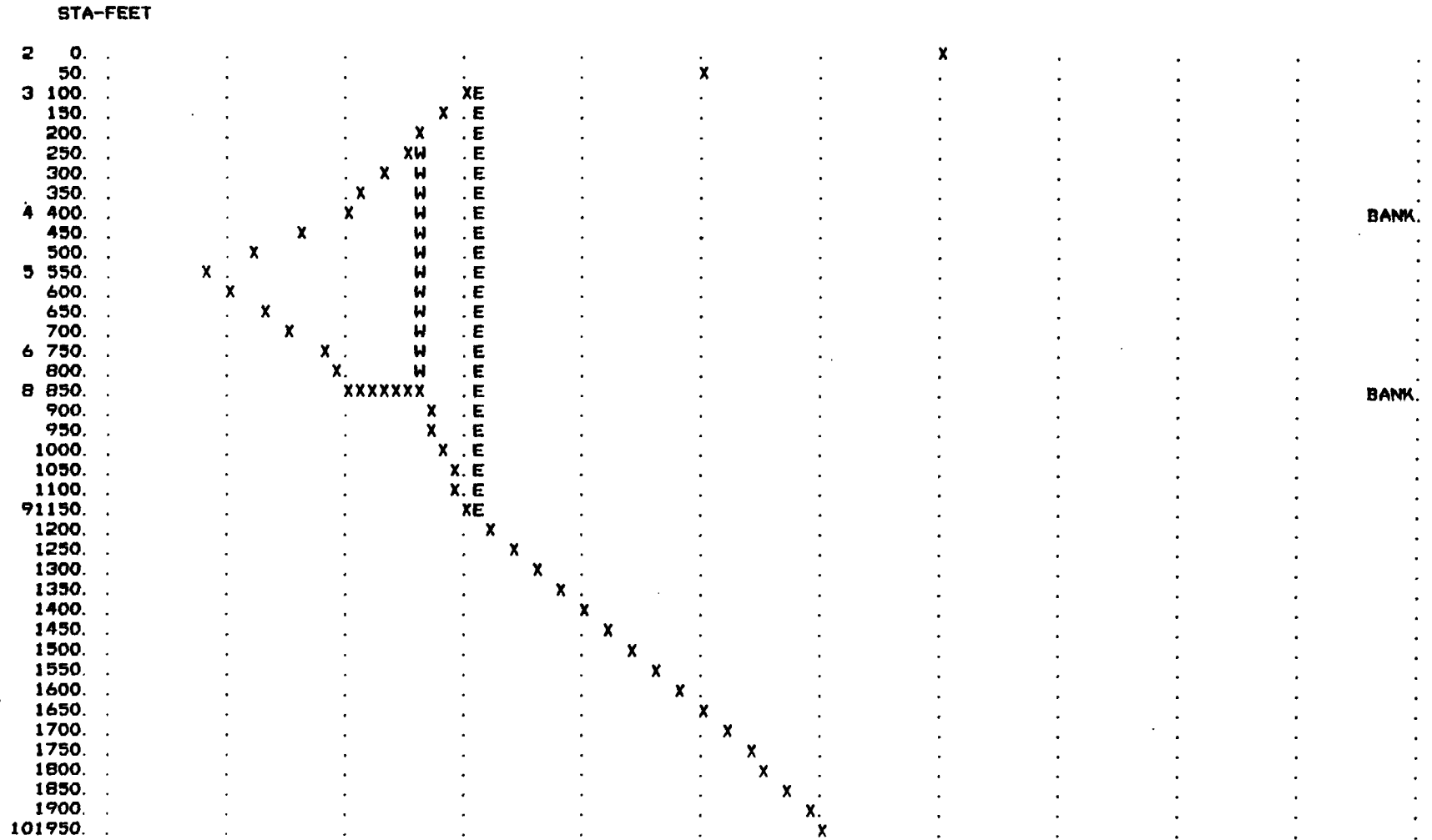
sh. 22C.6

CROSS SECTION 4.00  
 STREAM DISCHARGE = 100000 CFS  
 DISCHARGE = 100000.

JTK 4/21/87  
 HM 5/14/87

PLOTTED POINTS (BY PRIORITY)-B=BOTTOM BRIDGE, T=TOP BRIDGE, X=GROUND, W=WATER SUR, E=ENERGY GRADIENT, C=CRITICAL WSEL

ELEV 4060. 4070. 4080. 4090. 4100. 4110. 4120. 4130. 4140. 4150. 4160.



NRD= 0 ELLC= 9999999.00 ELTRD= 9999999.00

EL(I), STA(I)	4130.00	0.00	4090.00	100.00	4080.00	385.00	4068.00	530.00	4078.00	750.00
	4080.00	840.00	4086.00	870.00	4090.00	1165.00	4120.00	1930.00		



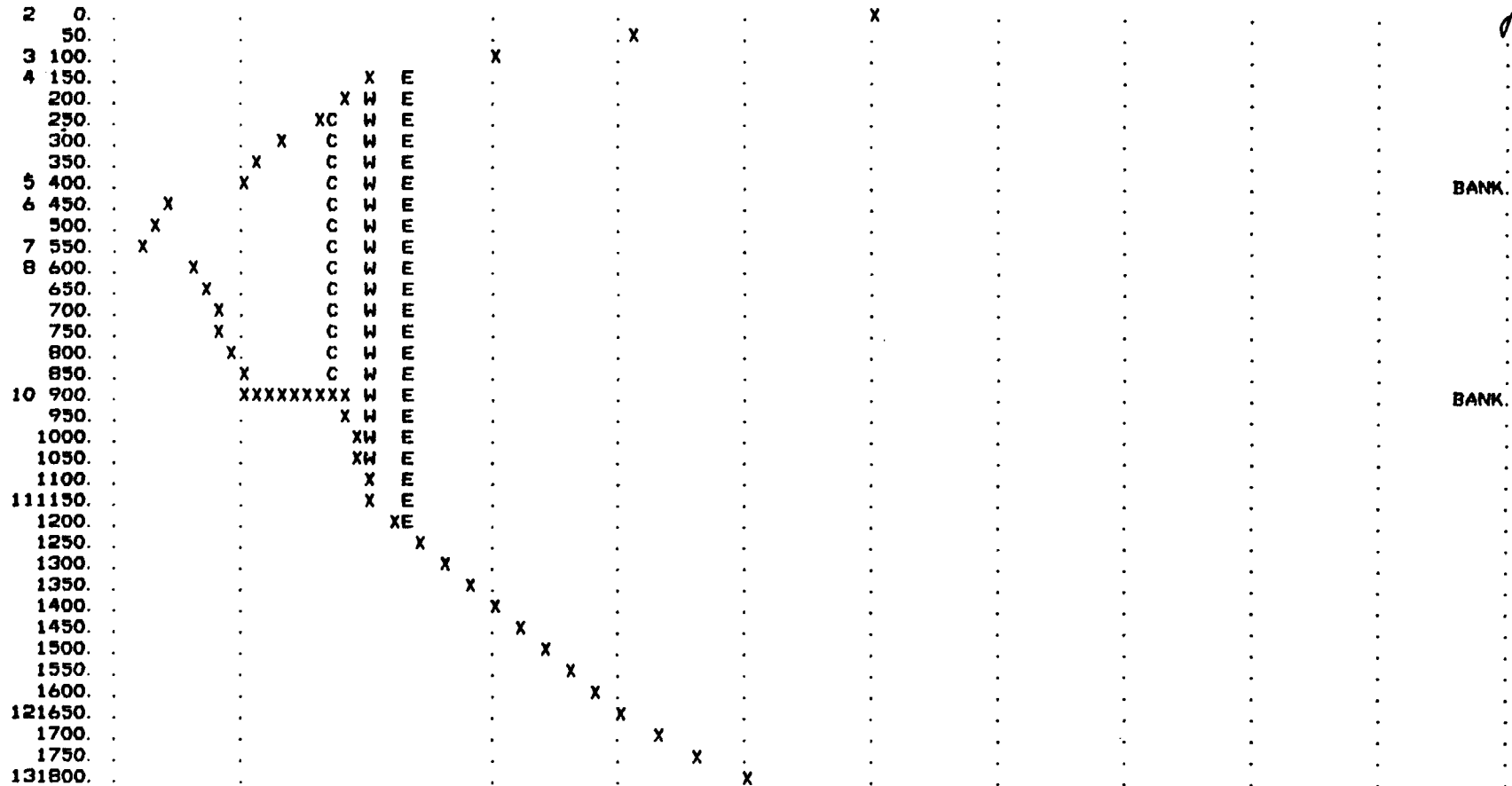
CROSS SECTION 3.00  
 STREAM DISCHARGE = 100000 CFS  
 DISCHARGE= 100000.

PLOTTED POINTS (BY PRIORITY)-B=BOTTOM BRIDGE, T=TOP BRIDGE, X=GROUND, W=WATER SUR, E=ENERGY GRADIENT, C=CRITICAL WSEL

ELEV 4070. 4080. 4090. 4100. 4110. 4120. 4130. 4140. 4150. 4160. 4170.

Sh. 22C.7

STA-FEET



JTK 4/21/87  
 HM 5/19/17

NRD= 0 ELLC= 9999999.00 ELTRD= 9999999.00

EL(I), STA(I)

4130.00	0.00	4100.00	80.00	4090.00	170.00	4080.00	400.00	4074.00	455.00
4072.00	570.00	4076.00	620.00	4080.00	880.00	4088.00	925.00	4090.00	1150.00
4110.00	1640.00	4120.00	1820.00						

PROFILE FOR STREAM DISCHARGE = 100000 CFS

Sh. 22C-B

PK 4/21/87

PLOTTED POINTS (BY PRIORITY)-E-ENERGY, W-WATER SURFACE, I-INVERT, C-CRITICAL W. S., L-LEFT BANK, R-RIGHT BANK, M-LOWER END STA

HM 8/14/87

ELEVATION SECND	4060. CUMDIS	4070.	4080.	4090.	4100.	4110.	4120.	4130.	4140.	4150.
6.00	0.	I		L R	W E	M				
	50.	I		L R	CW E	M				
	100.	I		L R	CW E	M				
	150.	I		L R	CW E	M				
	200.	I		L R	CW E	M				
	250.	I		L R	CW E	M				
5.50	300.	I		L R	CW E	M				
	350.	I		L R	CW E	M				
	400.	I		L R	CW E	M				
	450.	I		L R	CW E	M				
	500.	I		L R	CW E	M				
5.00	550.	I		L R	CW E	M				
	600.	I		L R	CW E	M				
	650.	I		L R	CW E	M				
	700.	I		L R	CW E	M				
	750.	I		L R	CW E	M				
	800.	I		L R	CW E	M				
	850.	I		L R	CW E	M				
	900.	I		L R	CW E	M				
	950.	I		L R	CW E	M				
4.00	1000.	I		L R	CW E	M				
	1050.	I		L R	CW E	M				
	1100.	I		L R	CW E	M				
	1150.	I		L R	CW E	M				
	1200.	I		L R	CW E	M				
	1250.	I		L R	CW E	M				
3.00	1300.	I		L R	CW E	M				
	1350.	I		L R	CW E	M				
	1400.	I		L R	CW E	M				
	1450.	I		L R	CW E	M				
	1500.	I		L R	CW E	M				
	1550.	I		L R	CW E	M				
	1600.	I		L R	CW E	M				
	1650.	I		L R	CW E	M				
2.50	1700.	I		L R	CW E	M				
	1750.	I		L R	CW E	M				
	1800.	I		L R	CW E	M				
	1850.	I		L R	CW E	M				
	1900.	I		L R	CW E	M				
	1950.	I		L R	CW E	M				
	2000.	I		L R	CW E	M				
2.00	2050.	I		L R	CW E	M				

\*\*\*\*\*  
 HEC2 RELEASE DATED NOV 76 UPDATED MAY 1984  
 ERROR CORR - 01,02,03,04,05,06  
 MODIFICATION - 50,51,52,53,54,55,56  
 \*\*\*\*\*

*Sh. 22c.9*

NOTE- ASTERISK (\*) AT LEFT OF CROSS-SECTION NUMBER INDICATES MESSAGE IN SUMMARY OF ERRORS LIST

*FTK 4/21/87*  
*HM 5/14/87*

DISCHARGE = 100000 CFS

SUMMARY PRINTOUT

	SECNO	Q	CWSEL	CRWS	GLOB	GCH	GROB	GLOBP	GCHP	GROBP	VLOB	VCH	VROB
*	6.000	100000.00	4080.96	4080.96	1119.98	95806.41	3073.61	1.12	95.81	3.07	6.73	15.24	4.11
	5.500	100000.00	4084.13	4079.53	2961.67	91072.47	5965.85	2.96	91.07	5.97	4.48	9.74	3.40
	5.000	100000.00	4084.00	4083.07	8467.16	89615.53	1917.31	8.47	89.62	1.92	7.78	14.48	3.63
*	4.000	100000.00	4086.09	4086.09	3090.94	96422.21	486.87	3.09	96.42	0.49	5.84	18.29	5.23
	3.000	100000.00	4090.42	4087.25	6842.18	90930.22	2227.60	6.84	90.93	2.23	5.49	13.39	3.66
	2.500	100000.00	4092.41	4086.14	1767.90	97086.11	1145.98	1.77	97.09	1.15	4.35	9.72	3.35
	2.000	100000.00	4092.54	4088.79	8785.67	88644.07	2570.26	8.79	88.64	2.57	6.34	12.36	5.08

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DISCHARGE = 100000 CFS  
SUMMARY PRINTOUT

JK 4/21/87  
HM 4/19/87

SECNO	KRATIO	AREA	CHSEL	ELMIN	DEPTH	DIFWSX	HV	TOPWID	SSTA	ENDST	K*CHSL	10K*8	
*	6.000	0.00	7200.34	4080.96	4062.00	18.96	0.00	3.47	1232.48	62.17	1294.65	0.00	79.98
	5.500	2.17	11764.48	4084.13	4062.00	22.13	3.17	1.36	1260.39	46.97	1307.36	0.00	16.98
	5.000	0.57	7803.74	4084.00	4064.00	20.00	-0.13	3.00	1070.94	75.98	1146.92	8.00	52.74
*	4.000	0.86	5895.09	4086.09	4068.00	18.09	2.09	5.03	665.61	211.32	876.93	8.70	70.88
	3.000	1.56	8645.11	4090.42	4072.00	18.42	4.32	2.57	993.92	166.26	1160.18	12.58	29.13
	2.500	1.44	10739.32	4092.41	4073.00	19.41	1.99	1.43	873.18	219.88	1093.05	2.63	14.00
	2.000	0.74	9065.25	4092.54	4074.00	18.54	0.13	2.17	801.87	178.78	980.65	2.86	25.66

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PAGE 7

SUMMARY OF ERRORS AND SPECIAL NOTES

CAUTION SECNO= 6.000 PROFILE= 1 CRITICAL DEPTH ASSUMED  
CAUTION SECNO= 4.000 PROFILE= 1 CRITICAL DEPTH ASSUMED  
CAUTION SECNO= 4.000 PROFILE= 1 MINIMUM SPECIFIC ENERGY

*Sh. 22C.11*

*JTK 4/21/87*  
*HM 5/11/87*

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PAGE 1

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HEC2 RELEASE DATED NOV 76 UPDATED MAY 1984  
ERROR CORR - 01,02,03,04,05,06  
MODIFICATION - 50,51,52,53,54,55,56  
\*\*\*\*\*

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*****
* WATER SURFACE PROFILES *
* VERSION OF NOVEMBER 1976 *
* UPDATED MAY 1984 *
* *
* RUN DATE 9-APR-87 TIME 14:24:18 *
*****

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*****
* U. S. ARMY CORPS OF ENGINEERS *
* THE HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET, SUITE D *
* DAVIS, CALIFORNIA 95616 *
* (916) 440-2105 (FTS) 448-2105 *
*****

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X X XXXXXXX XXXXX XXXXX
X X X X X
X X X X X
XXXXXXXX XXXX X XXXXX
X X X X X
X X X X X
X X XXXXXXX XXXXX

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Sh. 23A.1

LIMTRA - Green River

using TAC's data ref (4)

Supercritical flow

using 7 cross sections

JRK 4/9/87

HM 5/19/87

9-APR-87 14:24:18

\*\*\*\*\*  
 HEC2 RELEASE DATED NOV 76 UPDATED MAY 1984  
 ERROR CORR - 01, 02, 03, 04, 05, 06  
 MODIFICATION - 50, 51, 52, 53, 54, 55, 56  
 \*\*\*\*\*

*JTK*  
*4/9/87*  
*HM 5/14/87*

T1 UMTRA - GREEN RIVER - LOCAL PMF  
 T2 WATER SURFACE PROFILE ON BROWN WASH  
 T3 DISCHARGE = 100000 CFS

J1	ICHECK	ING	NINV	IDIR	STRT	METRIC	HVINS	Q	WSEL	F0
	0.	0.	0.	1.	0.009000	0.00	0.0	100000.	4074.000	0.000
J2	NPROF	IPL0T	PRFVS	XSECV	XSECH	FN	ALLDC	IBW	CHNIM	ITRACE
	-1.000	0.000	0.000	0.000	0.000	0.000	-1.000	0.000	0.000	0.000
J3	VARIABLE CODES FOR SUMMARY PRINTOUT									
	38.000	43.000	1.000	2.000	13.000	14.000	15.000	35.000	60.000	59.000
	55.000	26.000	56.000	0.000	38.000	58.000	25.000	1.000	42.000	8.000
	51.000	10.000	4.000	53.000	54.000	33.000	5.000	0.000	0.000	0.000
NC	0.045	0.050	0.035	0.100	0.300	0.000	0.000	0.000	0.000	0.000
X1	1.000	7.000	150.000	765.000	730.000	510.000	610.000	0.000	0.000	0.000
QR	4104.000	0.000	4090.000	150.000	4084.000	390.000	4080.000	470.000	4102.000	765.000
QR	4110.000	1145.000	4120.000	1385.000	0.000	0.000	0.000	0.000	0.000	0.000
X1	2.000	10.000	380.000	920.000 <sup>900</sup>	335.000 <sup>350</sup>	250.000 <sup>300</sup>	300.000	0.000	0.000	0.000
QR	4114.000	0.000	4090.000	200.000	4080.000	380.000	4074.000	400.000	4074.000	430.000
QR	4078.000	510.000	4080.000	920.000 <sup>900</sup>	4094.000	990.000	4094.000	1170.000	4120.000	1890.000
X1	2.500	11.000	300.000	960.000 <sup>400, 700</sup>	365.000	240.000 <sup>300</sup>	380.000 <sup>380</sup>	0.000	0.000	0.000
QR	4110.000	0.000	4090.000	250.000	4080.000	300.000	4073.000	420.000	4076.000	500.000
QR	4076.000	560.000	4078.000	620.000	4078.000 <sup>4000</sup>	960.000	4091.000	1000.000	4096.000	1330.000
QR	4110.000	1700.000	0.000	0.000 <sup>4070, 800</sup>	0.000	0.000	0.000	0.000	0.000	0.000
NC	0.000	0.000	0.000	0.100 <sup>0.2</sup>	0.300 <sup>0.5</sup>	0.000	0.000	0.000	0.000	0.000
X1	3.000	11.000 <sup>2</sup>	400.000	880.000	315.000	300.000 <sup>300</sup>	320.000	0.000	0.000	1.000
QR	4130.000	0.000	4100.000	80.000	4090.000	170.000	4080.000	400.000	4074.000	455.000
QR	4072.000	570.000	4080.000	880.000	4088.000	925.000	4090.000	1150.000	4110.000	1640.000
QR	4120.000	1820.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000

*4.76* *820*





*Sh.23A.4*

*JFK 4/9/87*  
*HM 5/19/87*

SECNO	DEPTH	CWSEL	CRIBS	WSELK	EQ	HV	HL	DLOSS	BANK ELEV
G	GLOB	GCH	GROB	ALOB	ACH	AROB	VOL	TWA	LEFT/RIGHT
TIME	VLOB	VCH	VROB	XNL	XNCH	XNR	WTN	ELMIN	SSTA
SLOPE	XLOBL	XLCH	XLOBR	ITRIAL	IDC	ICONT	CORAR	TOPWID	ENDST

\*PROF 1

CRITICAL DEPTH TO BE CALCULATED AT ALL CROSS SECTIONS

CCHV= 0.100 CEHV= 0.300

\*SECNO 1.000

3840	SECTION NOT HIGH ENOUGH	4347.487	4154.000	4080.000	4154.000	4083.000			14
3840	SECTION NOT HIGH ENOUGH	4347.487	4204.000	4080.000	4204.000	4083.000			14
3840	SECTION NOT HIGH ENOUGH	4347.487	4254.000	4080.000	4254.000	4083.000			14
3840	SECTION NOT HIGH ENOUGH	4347.487	4304.000	4080.000	4304.000	4083.000			14
1.00	16.62	4096.62	4096.93	4074.00	4101.83	5.21	0.00	0.00	4090.00
100000.	1630.	98370.	0.	235.	5332.	0.	0.	0.	4102.00
0.00	6.94	18.45	0.00	0.045	0.035	0.000	0.000	4080.00	79.03
0.008992	0.	0.	0.	0	35	11	0.00	613.87	692.91

\*SECNO 2.000

3301 HV CHANGED MORE THAN HVINS

2.00	12.00	4086.00	4088.26	0.00	4093.86	7.87	7.71	0.27	4080.00
100000.	3042.	96207.	751.	323.	4206.	90.	72.	9.	4080.00
0.01	7.41	22.87	8.37	0.045	0.035	0.050	0.000	4074.00	272.14
0.018846	730.	610.	510.	7	16	0	0.00	677.82	949.96

\*SECNO 2.500

3301 HV CHANGED MORE THAN HVINS

3685 20 TRIALS ATTEMPTED WSEL, CWSEL  
3693 PROBABLE MINIMUM SPECIFIC ENERGY  
3720 CRITICAL DEPTH ASSUMED

2.50	12.89	4085.89	4085.89	0.00	4090.28	4.39	3.69	2.71	4080.00
100000.	540.	98821.	639.	87.	5846.	96.	109.	14.	4078.00
0.01	6.23	16.91	6.67	0.045	0.035	0.050	0.000	4073.00	270.56
0.008656	335.	300.	250.	20	8	0	0.00	713.70	984.27

CCHV= 0.100 CEHV= 0.300

\*SECNO 3.000

3685 20 TRIALS ATTEMPTED WSEL, CWSEL  
3693 PROBABLE MINIMUM SPECIFIC ENERGY

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PAGE 4

Sh. 23A. 5

JTK 4/9/87  
HM 5/14/87

SECNO	DEPTH	CWSEL	CRISW	WSELK	EQ	HV	HL	OLOSS	BANK ELEV
Q	GLOB	GCH	GROB	ALOB	ACH	AROB	VOL	TWA	LEFT/RIGHT
TIME	VLOB	VCH	VROB	XML	XNCH	XNR	WTN	ELMIN	SSTA
SLOPE	XLOBL	XLCH	XLOBR	ITRIAL	IDC	ICONT	CORAR	TOPWID	ENDST
3720	CRITICAL DEPTH ASSUMED								
3.00	14.53	4086.53	4086.53	0.00	4091.41	4.87	2.38	1.99	4080.00
100000.	3037.	96301.	662.	491.	5347.	120.	150.	19.	4080.00
0.02	6.18	18.01	5.51	0.045	0.035	0.050	0.000	4072.00	249.70
0.007242	365.	300.	240.	20	8	0	0.00	667.06	916.76

\*SECNO 4.000

3685 20 TRIALS ATTEMPTED WSEL, CWSEL  
3693 PROBABLE MINIMUM SPECIFIC ENERGY

3720	CRITICAL DEPTH ASSUMED								
4.00	17.43	4085.43	4085.43	0.00	4090.60	5.17	2.32	1.96	4080.00
100000.	2293.	97350.	357.	420.	5269.	74.	193.	24.	4080.00
0.02	5.46	18.48	4.86	0.045	0.035	0.050	0.000	4068.00	230.36
0.007243	315.	320.	305.	20	11	0	0.00	636.77	867.13

\*SECNO 5.000

3301 HV CHANGED MORE THAN HVINS

5.00	15.07	4079.07	4081.16	0.00	4085.84	6.76	4.60	0.16	4076.00
100000.	1155.	97747.	1099.	206.	4640.	99.	247.	31.	4064.00
0.03	5.62	21.07	11.06	0.045	0.035	0.050	0.000	4064.00	135.88
0.016381	470.	440.	420.	7	8	0	0.00	753.31	889.18

CCHV= 0.200 CEHV= 0.500

\*SECNO 5.500

3301 HV CHANGED MORE THAN HVINS

3685 20 TRIALS ATTEMPTED WSEL, CWSEL  
3693 PROBABLE MINIMUM SPECIFIC ENERGY

3720	CRITICAL DEPTH ASSUMED								
5.50	17.53	4079.53	4079.53	0.00	4083.53	4.00	2.83	1.43	4071.00
100000.	1258.	98261.	481.	162.	6082.	138.	280.	36.	4076.00
0.03	7.77	16.16	3.48	0.045	0.035	0.050	0.000	4062.00	142.08
0.008281	230.	250.	290.	20	11	0	0.00	936.04	1078.13

\*SECNO 6.000

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Sh. 23A. 6  
PAGE 5

SECNO	DEPTH	CWSEL	CRHS	WSELK	EQ	HV	HL	DLOSS	BANK ELEV
G	GLOB	GCH	GROB	ALOB	ACH	AROB	VOL	TWA	LEFT/RIGHT
TIME	VLOB	VCH	VROB	XNL	XNCH	XNR	WTN	ELMIN	BSTA
SLOPE	XLOBL	XLCH	XLOBR	ITRIAL	IDC	ICONT	CORAR	TOPWID	ENDST

FRK 4/9/87  
HM 5/19/87

3301 HV CHANGED MORE THAN HVINS

3685 20 TRIALS ATTEMPTED WSEL. CWSEL  
3693 PROBABLE MINIMUM SPECIFIC ENERGY  
3720 CRITICAL DEPTH ASSUMED

6.00	18.22	4080.22	4080.22	0.00	4083.66	3.43	1.55	2.74	4074.00
100000.	829.	95414.	3758.	133.	6283.	834.	310.	41.	4076.00
0.04	6.23	15.19	4.51	0.045	0.035	0.050	0.000	4062.00	67.23
0.007943	100.	190.	270.	20	B	0	0.00	1204.65	1271.87

\*SECNO 7.000

3301 HV CHANGED MORE THAN HVINS

7.00	12.38	4068.38	4071.24	0.00	4076.94	8.56	5.69	1.03	4064.00
100000.	1633.	96259.	2108.	163.	4030.	357.	365.	52.	4066.00
0.04	10.01	23.89	5.90	0.045	0.035	0.050	0.000	4056.00	167.53
0.032377	385.	400.	410.	B	10	0	0.00	1195.60	1363.13

CROSS SECTION 3.00  
 STREAM DISCHARGE = 100000 CFS  
 DISCHARGE= 100000.

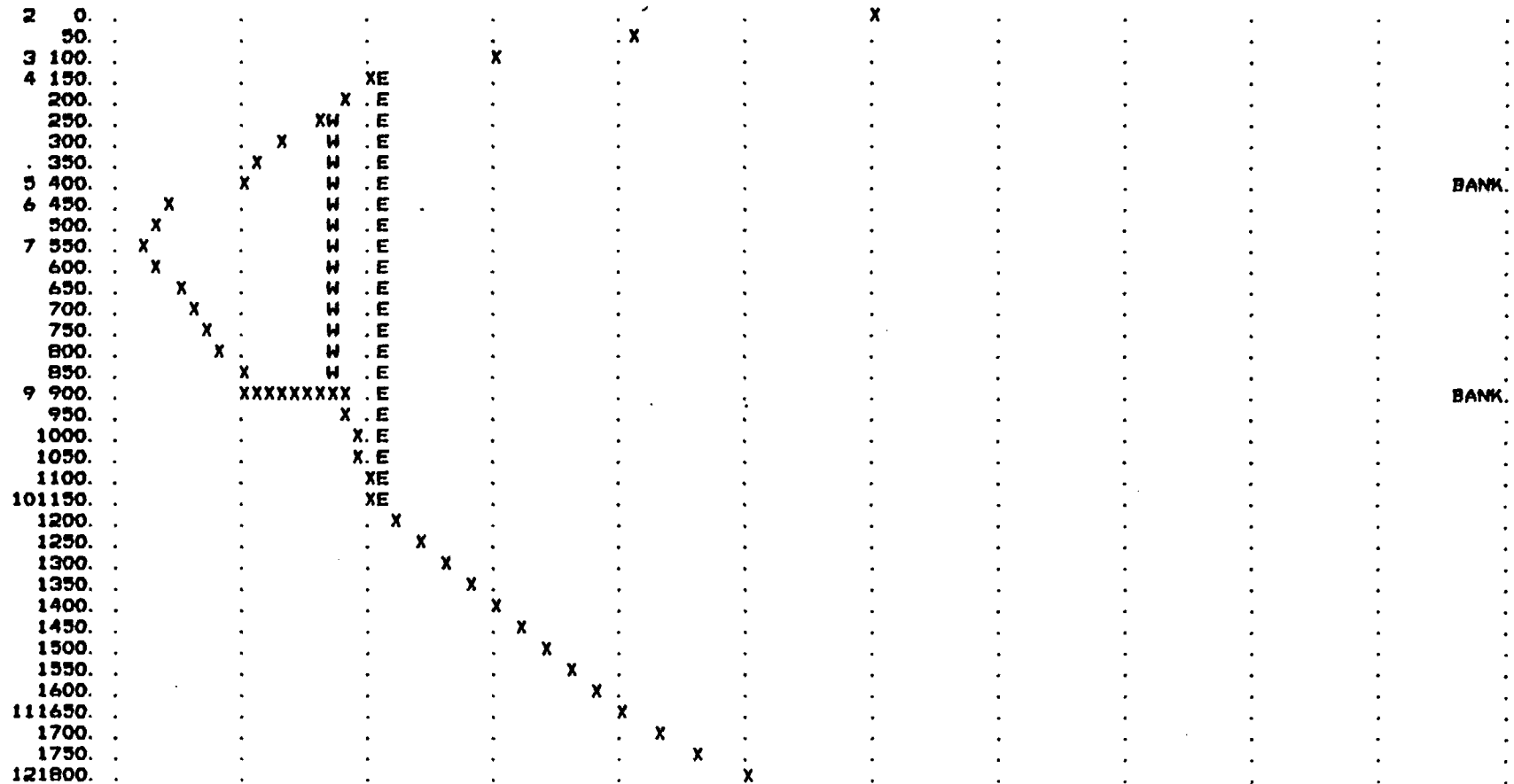
Sh. 23A. 7

PLOTTED POINTS (BY PRIORITY)-B=BOTTOM BRIDGE, T=TOP BRIDGE, X=GROUND, W=WATER SUR, E=ENERGY GRADIENT, C=CRITICAL WSEL

JTK 4/9/87  
 HM 5/19/87

ELEV 4070. 4080. 4090. 4100. 4110. 4120. 4130. 4140. 4150. 4160. 4170.

STA-FEET



NRD= 0 ELLC= 9999999.00 ELTRD= 9999999.00

EL(I), STA(I)

4130.00	0.00	4100.00	80.00	4090.00	170.00	4080.00	400.00	4074.00	455.00
4072.00	570.00	4080.00	880.00	4088.00	925.00	4090.00	1150.00	4110.00	1640.00
4120.00	1820.00								

CROSS SECTION 4.00  
 STREAM DISCHARGE = 100000 CFS  
 DISCHARGE = 100000.

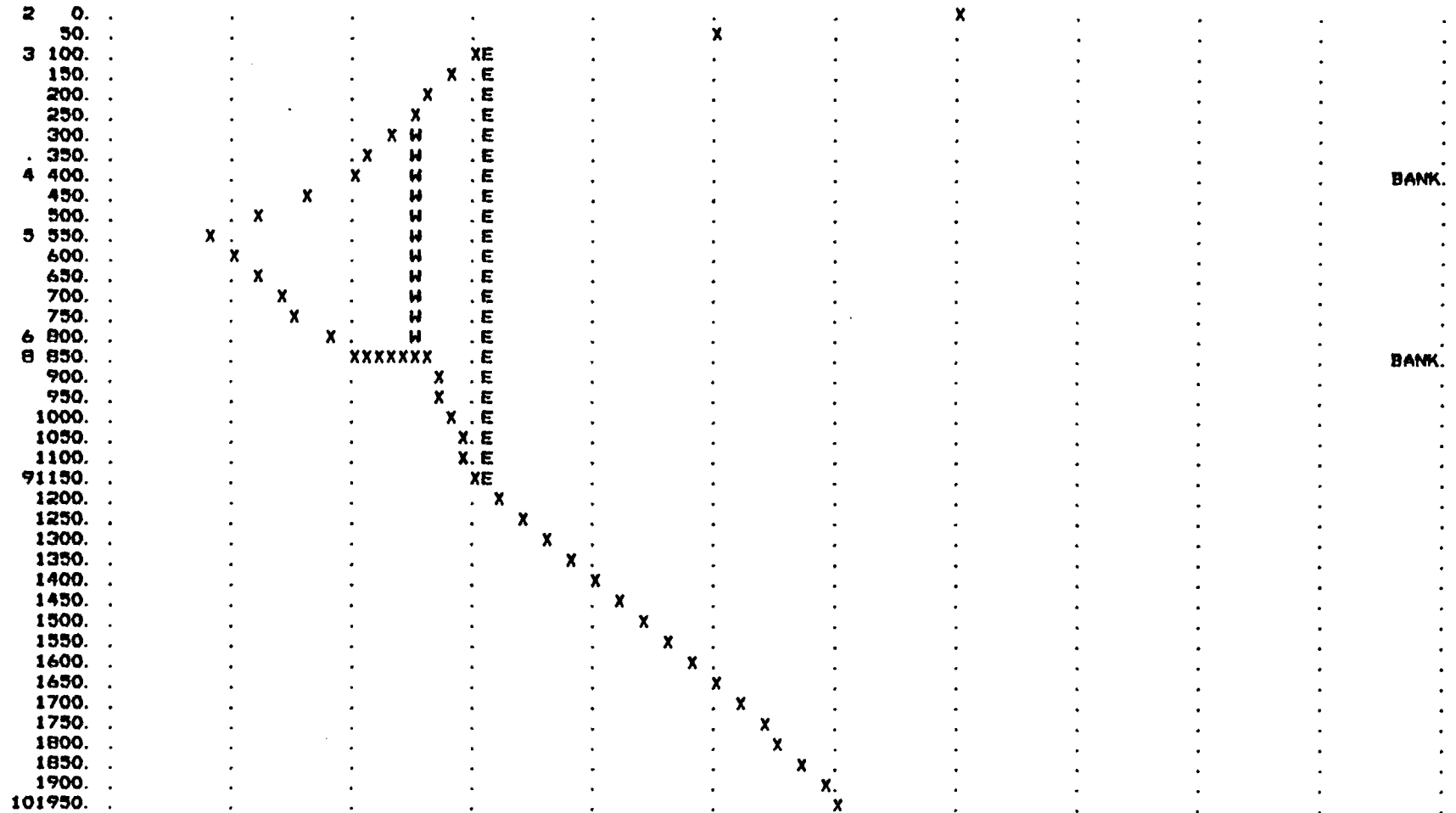
Sh. 23A. 8

JW 4/9/87  
 HM 5/14/87

PLOTTED POINTS (BY PRIORITY)-B-BOTTOM BRIDGE, T-TOP BRIDGE, X-GROUND, W-WATER SUR, E-ENERGY GRADIENT, C-CRITICAL WSEL

ELEV 4060. 4070. 4080. 4090. 4100. 4110. 4120. 4130. 4140. 4150. 4160.

STA-FEET



NRD= 0 ELLC= 9999999.00 ELTRD= 9999999.00

EL(I), STA(I)

4130.00	0.00	4090.00	100.00	4080.00	385.00	4068.00	530.00	4078.00	800.00
4080.00	840.00	4086.00	870.00	4090.00	1165.00	4120.00	1930.00		



6.00	2450.	.	I	LWEM	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.
	2500.	.	I	LWEM	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.
	2550.	.	I	LWE M	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.
	2600.	.	I	LWE M	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.
	2650.	.	I	LWE M	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.
	2700.	.	I	LWE M	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.
	2750.	.	ILWCE	M	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.
	2800.	.	I	LW E M	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.
7.00	2850.	.	I	LWE M	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.

Sh. 23A.10

FTK 4/9/87  
 HM 5/19/87



*Sh. 23A.11*

*JK 4/9/87*  
*HM 5/19/87*

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 HEC2 RELEASE DATED NOV 76 UPDATED MAY 1984  
 ERROR CORR - 01, 02, 03, 04, 05, 06  
 MODIFICATION - 50, 51, 52, 53, 54, 55, 56  
 \*\*\*\*\*

NOTE- ASTERISK (\*) AT LEFT OF CROSS-SECTION NUMBER INDICATES MESSAGE IN SUMMARY OF ERRORS LIST

DISCHARGE = 100000 CFS

SUMMARY PRINTOUT

SECNO	Q	CWSEL	CRWS	GLOB	GCH	GROB	GLOBP	GCHP	GROBP	VLOB	VCH	VRDB
1.000	100000.00	4096.62	4096.93	1630.48	98369.52	0.00	1.63	98.37	0.00	6.94	18.45	0.00
2.000	100000.00	4086.00	4088.26	3041.58	96207.13	751.29	3.04	96.21	0.75	9.41	22.87	8.37
* 2.500	100000.00	4085.89	4085.89	539.68	98821.49	638.82	0.54	98.82	0.64	6.23	16.91	6.67
* 3.000	100000.00	4086.53	4086.53	3036.91	96301.13	661.97	3.04	96.30	0.66	6.18	18.01	5.51
* 4.000	100000.00	4085.43	4085.43	2292.56	97350.02	357.43	2.29	97.35	0.36	5.46	18.48	4.86
5.000	100000.00	4079.07	4081.16	1154.80	97746.55	1098.65	1.15	97.75	1.10	5.62	21.07	11.06
* 5.500	100000.00	4079.53	4079.53	1257.50	98261.48	481.02	1.26	98.26	0.48	7.77	16.16	3.48
* 6.000	100000.00	4080.22	4080.22	828.76	95413.52	3757.72	0.83	95.41	3.76	6.23	15.19	4.51
7.000	100000.00	4068.38	4071.24	1632.62	96258.91	2108.48	1.63	96.26	2.11	10.01	23.89	5.90

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Sh. 23A.12

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DISCHARGE = 100000 CFS

SUMMARY PRINTOUT

JTK 4/9/87  
MM 5/14/87

SECNO	KRATIO	AREA	CWSEL	ELMIN	DEPTH	DIFWSX	HV	TOPWID	BSTA	ENDST	K*CHSL	10K*B
1.000	0.00	5567.30	4096.62	4080.00	16.62	0.00	5.21	613.87	79.03	692.91	0.00	89.92
2.000	1.45	4618.70	4086.00	4074.00	12.00	-10.63	7.87	677.82	272.14	949.96	-9.84	188.46
* 2.500	1.13	6027.91	4085.89	4073.00	12.89	-0.11	4.39	713.70	270.56	984.27	-3.33	86.56
* 3.000	1.55	5957.95	4086.53	4072.00	14.53	0.65	4.87	667.06	249.70	916.76	-3.33	72.42
* 4.000	1.73	5761.97	4085.43	4068.00	17.43	-1.11	5.17	636.77	230.36	867.13	-12.50	72.43
5.000	1.50	4944.67	4079.07	4064.00	15.07	-6.35	6.76	753.31	135.88	889.18	-9.09	163.81
* 5.500	0.75	6382.18	4079.53	4062.00	17.53	0.46	4.00	936.04	142.08	1078.13	-8.00	82.81
* 6.000	2.29	7249.86	4080.22	4062.00	18.22	0.69	3.43	1204.65	67.23	1271.87	0.00	79.43
7.000	2.02	4550.32	4068.38	4056.00	12.38	-11.84	8.56	1195.60	167.53	1363.13	-15.00	323.77

SUMMARY OF ERRORS AND SPECIAL NOTES

CAUTION	SECNO=	2.500	PROFILE=	1	CRITICAL DEPTH ASSUMED
CAUTION	SECNO=	2.500	PROFILE=	1	PROBABLE MINIMUM SPECIFIC ENERGY
CAUTION	SECNO=	2.500	PROFILE=	1	20 TRIALS ATTEMPTED TO BALANCE WSEL
CAUTION	SECNO=	3.000	PROFILE=	1	CRITICAL DEPTH ASSUMED
CAUTION	SECNO=	3.000	PROFILE=	1	PROBABLE MINIMUM SPECIFIC ENERGY
CAUTION	SECNO=	3.000	PROFILE=	1	20 TRIALS ATTEMPTED TO BALANCE WSEL
CAUTION	SECNO=	4.000	PROFILE=	1	CRITICAL DEPTH ASSUMED
CAUTION	SECNO=	4.000	PROFILE=	1	PROBABLE MINIMUM SPECIFIC ENERGY
CAUTION	SECNO=	4.000	PROFILE=	1	20 TRIALS ATTEMPTED TO BALANCE WSEL
CAUTION	SECNO=	5.500	PROFILE=	1	CRITICAL DEPTH ASSUMED
CAUTION	SECNO=	5.500	PROFILE=	1	PROBABLE MINIMUM SPECIFIC ENERGY
CAUTION	SECNO=	5.500	PROFILE=	1	20 TRIALS ATTEMPTED TO BALANCE WSEL
CAUTION	SECNO=	6.000	PROFILE=	1	CRITICAL DEPTH ASSUMED
CAUTION	SECNO=	6.000	PROFILE=	1	PROBABLE MINIMUM SPECIFIC ENERGY
CAUTION	SECNO=	6.000	PROFILE=	1	20 TRIALS ATTEMPTED TO BALANCE WSEL

JTK 4/9/87  
HM 5/19/87

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PAGE 1

*Sh. 23A.14*

*JK 4/9/87*  
*HM 5/19/87*

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HEC2 RELEASE DATED NOV 76 UPDATED MAY 1984  
ERROR CORR - 01, 02, 03, 04, 05, 06  
MODIFICATION - 50, 51, 52, 53, 54, 55, 56  
\*\*\*\*\*

\*\*\*\*\*  
 \* WATER SURFACE PROFILES \*  
 \* VERSION OF NOVEMBER 1976 \*  
 \* UPDATED MAY 1984 \*  
 \* \*  
 \* RUN DATE 16-APR-87 TIME 15:57:34 \*  
 \*\*\*\*\*

\*\*\*\*\*  
 \* U. S. ARMY CORPS OF ENGINEERS \*  
 \* THE HYDROLOGIC ENGINEERING CENTER \*  
 \* 609 SECOND STREET, SUITE D \*  
 \* DAVIS, CALIFORNIA 95616 \*  
 \* (916) 440-2105 (FTS) 448-2105 \*  
 \*\*\*\*\*

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X   X  XXXXXXX  XXXXX          XXXXX
X   X  X        X   X          X   X
X   X  X        X           X   X
XXXXXXXX XXXX   X           XXXXX XXXXX
X   X  X        X           X
X   X  X        X   X          X
X   X  XXXXXXX  XXXXX          XXXXXXX

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UMTRA - Green River

sh. 23 B.1

supercritical  
 flow

using 7 cross sections  
 adjusted by MKE

JK  
 4/16/87





JTK 4/16/87  
HM 5/19/87

SECNO	DEPTH	CWSEL	CRWS	WSELK	EG	HV	HL	QLOSS	BANK ELEV
G	GLOB	GCH	GRGB	ALOB	ACH	AROB	VOL	TWA	LEFT/RIGHT
TIME	VLOB	VCH	VROB	XNL	XNCH	XNR	WTN	ELMIN	SSTA
SLOPE	XLOBL	XLCH	XLOBR	ITRIAL	IDC	ICONT	CORAR	TOPWID	ENDST

\*PROF 1

CRITICAL DEPTH TO BE CALCULATED AT ALL CROSS SECTIONS

CCHV= 0.100 CEHV= 0.300

\*SECNO 1.000

3840 SECTION NOT HIGH ENOUGH	4347.487	4154.000	4080.000	4154.000	4083.000				14
3840 SECTION NOT HIGH ENOUGH	4347.487	4204.000	4080.000	4204.000	4083.000				14
3840 SECTION NOT HIGH ENOUGH	4347.487	4254.000	4080.000	4254.000	4083.000				14
3840 SECTION NOT HIGH ENOUGH	4347.487	4304.000	4080.000	4304.000	4083.000				14
1.00	16.62	4096.62	4096.93	4074.00	4101.83	5.21	0.00	0.00	4090.00
100000.	1630.	98370.	0.	235.	5332.	0.	0.	0.	4102.00
0.00	6.94	18.45	0.00	0.045	0.035	0.000	0.000	4080.00	79.03
0.008992	0.	0.	0.	0	35	11	0.00	613.87	692.91

\*SECNO 2.000

3301 HV CHANGED MORE THAN HVINS

2.00	12.91	4086.91	4088.81	0.00	4094.27	7.35	7.35	0.21	4080.00
100000.	4194.	94467.	1339.	429.	4241.	153.	73.	9.	4080.00
0.01	9.77	22.27	8.73	0.045	0.035	0.050	0.000	4074.00	255.68
0.016802	730.	610.	510.	6	11	0	0.00	688.72	944.40

\*SECNO 2.500

3301 HV CHANGED MORE THAN HVINS

3685 20 TRIALS ATTEMPTED WSEL, CWSEL  
3693 PROBABLE MINIMUM SPECIFIC ENERGY  
3720 CRITICAL DEPTH ASSUMED

2.50	13.21	4086.21	4086.21	0.00	4090.54	4.33	4.03	2.99	4080.00
100000.	615.	98987.	398.	97.	5902.	70.	117.	15.	4080.00
0.01	6.37	16.77	5.67	0.045	0.035	0.050	0.000	4073.00	268.93
0.008412	350.	350.	300.	20	5	0	0.00	713.67	982.60

CCHV= 0.200 CEHV= 0.500

\*SECNO 3.000

3685 20 TRIALS ATTEMPTED WSEL, CWSEL  
3693 PROBABLE MINIMUM SPECIFIC ENERGY



Sh. 23B. 5

FTK 4/16/87  
MM 5/14/87

SECNO	DEPTH	CWSEL	CRISW	WSELK	EG	HV	HL	DLOSS	BANK ELEV
G	GLOB	GCH	GROB	ALOB	ACH	AROB	VOL	TWA	LEFT/RIGHT
TIME	VLOB	VCH	VROB	XNL	XNCH	XNR	WTN	ELMIN	SSTA
SLOPE	XLOBL	XLCH	XLOBR	ITRIAL	IDC	ICONT	CORAR	TOPWID	ENDST

3720 CRITICAL DEPTH ASSUMED  
 3.00 15.34 4087.34 4087.34 0.00 4092.09 4.74 2.95 3.09 4080.00  
 100000. 4129. 94972. 900. 620. 5314. 152. 170. 21. 4080.00  
 0.02 6.66 17.87 5.94 0.045 0.035 0.050 0.000 4072.00 231.13  
 0.007189 365. 380. 380. 20 8 0 0.00 690.17 921.30

\*SECNO 4.000  
 3685 20 TRIALS ATTEMPTED WSEL, CWSEL  
 3693 PROBABLE MINIMUM SPECIFIC ENERGY  
 3720 CRITICAL DEPTH ASSUMED

4.00 18.08 4086.08 4086.08 0.00 4091.12 5.04 2.27 0.54 4080.00  
 100000. 3080. 96435. 485. 527. 5267. 93. 214. 26. 4080.00  
 0.02 5.84 18.31 5.23 0.045 0.035 0.050 0.000 4068.00 211.67  
 0.007115 315. 318. 320. 20 11 0 0.00 664.36 876.03

\*SECNO 5.000

5.00 18.32 4082.32 4083.06 0.00 4087.06 4.74 3.91 0.15 4076.00  
 100000. 6775. 92838. 387. 769. 5166. 112. 277. 35. 4076.00  
 0.03 8.81 17.97 3.46 0.045 0.035 0.050 0.000 4064.00 83.98  
 0.010323 470. 460. 440. 5 8 0 0.00 1015.12 1099.10

CCHV= 0.100 CEHV= 0.300  
 \*SECNO 5.500

3301 HV CHANGED MORE THAN HVINS

5.50 16.18 4078.18 4079.53 0.00 4083.90 5.72 3.06 0.10 4071.00  
 100000. 1062. 98786. 152. 115. 5122. 40. 309. 40. 4076.00  
 0.04 9.28 19.29 3.83 0.045 0.035 0.050 0.000 4062.00 148.09  
 0.014836 230. 250. 290. 7 8 0 0.00 778.23 926.32

\*SECNO 6.000

3301 HV CHANGED MORE THAN HVINS

3685 20 TRIALS ATTEMPTED WSEL, CWSEL  
 3693 PROBABLE MINIMUM SPECIFIC ENERGY  
 3720 CRITICAL DEPTH ASSUMED

6.00 18.96 4080.96 4080.96 0.00 4084.43 3.47 2.86 0.78 4074.00  
 100000. 1120. 95803. 3076. 166. 6287. 748. 348. 46. 4078.00  
 0.04 6.73 15.24 4.11 0.045 0.035 0.050 0.000 4062.00 62.16  
 0.007992 150. 270. 280. 20 11 0 0.00 1232.53 1294.70

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PAGE 5

Sh. 23B.6

JTK 4/16/87  
HM 5/14/87

SECNO	DEPTH	CWSEL	CRISW	WSELK	EQ	HV	HL	QLOSS	BANK	ELEV
Q	QLOB	QCH	GRQB	ALQB	ACH	AROB	VOL	TWA	LEFT/RIGHT	
TIME	VLOB	VCH	VRQB	XNL	XNCH	XNR	WTN	ELMIN	SSTA	
SLOPE	XLOBL	XLCH	XLOBR	ITRIAL	IDC	ICONT	CORAR	TOPWID	ENDST	

\*SECNO 7.000

3301 HV CHANGED MORE THAN HVINS

7.00	12.11	4068.11	4071.22	0.00	4077.77	9.65	6.04	0.62	4064.00	
100000.	1512.	96985.	1503.	144.	3838.	255.	400.	57.	4066.00	
0.05	10.50	25.27	5.90	0.045	0.035	0.050	0.000	4056.00	172.02	
0.038679	385.	400.	410.	7	14	0	0.00	1182.01	1354.03	

CROSS SECTION 3.00  
 STREAM DISCHARGE = 100000 CFS  
 DISCHARGE = 100000.

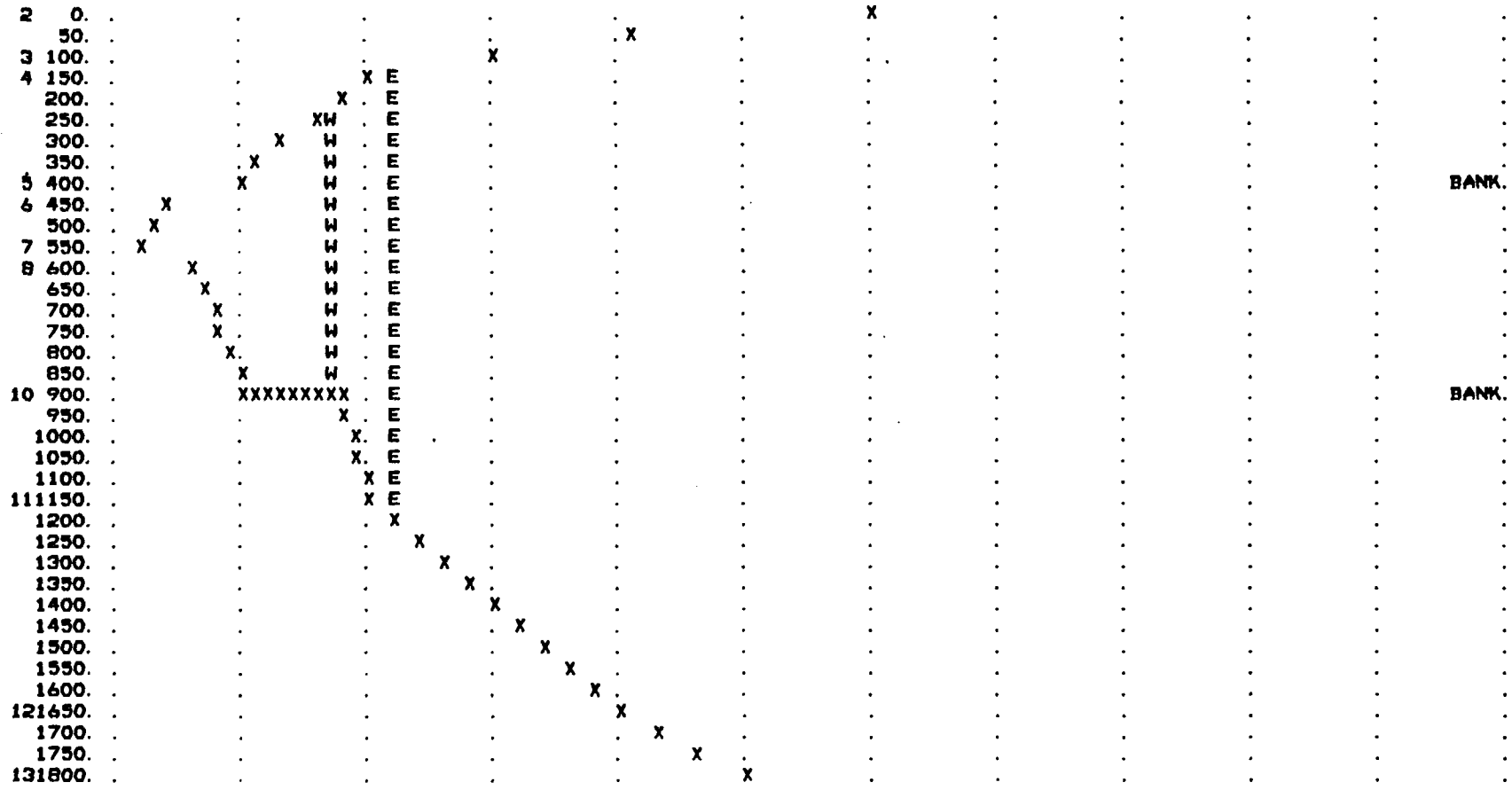
Sh. 23B.7

JFK 4/16/87  
 HM 5/19/87

PLOTTED POINTS (BY PRIORITY)-B=BOTTOM BRIDGE, T=TOP BRIDGE, X=GROUND, W=WATER SUR, E=ENERGY GRADIENT, C=CRITICAL WSEL

ELEV 4070. 4080. 4090. 4100. 4110. 4120. 4130. 4140. 4150. 4160. 4170.

STA- FEET



NRD= 0 ELLC= 9999999.00 ELTRD= 9999999.00

EL(I), STA(I)

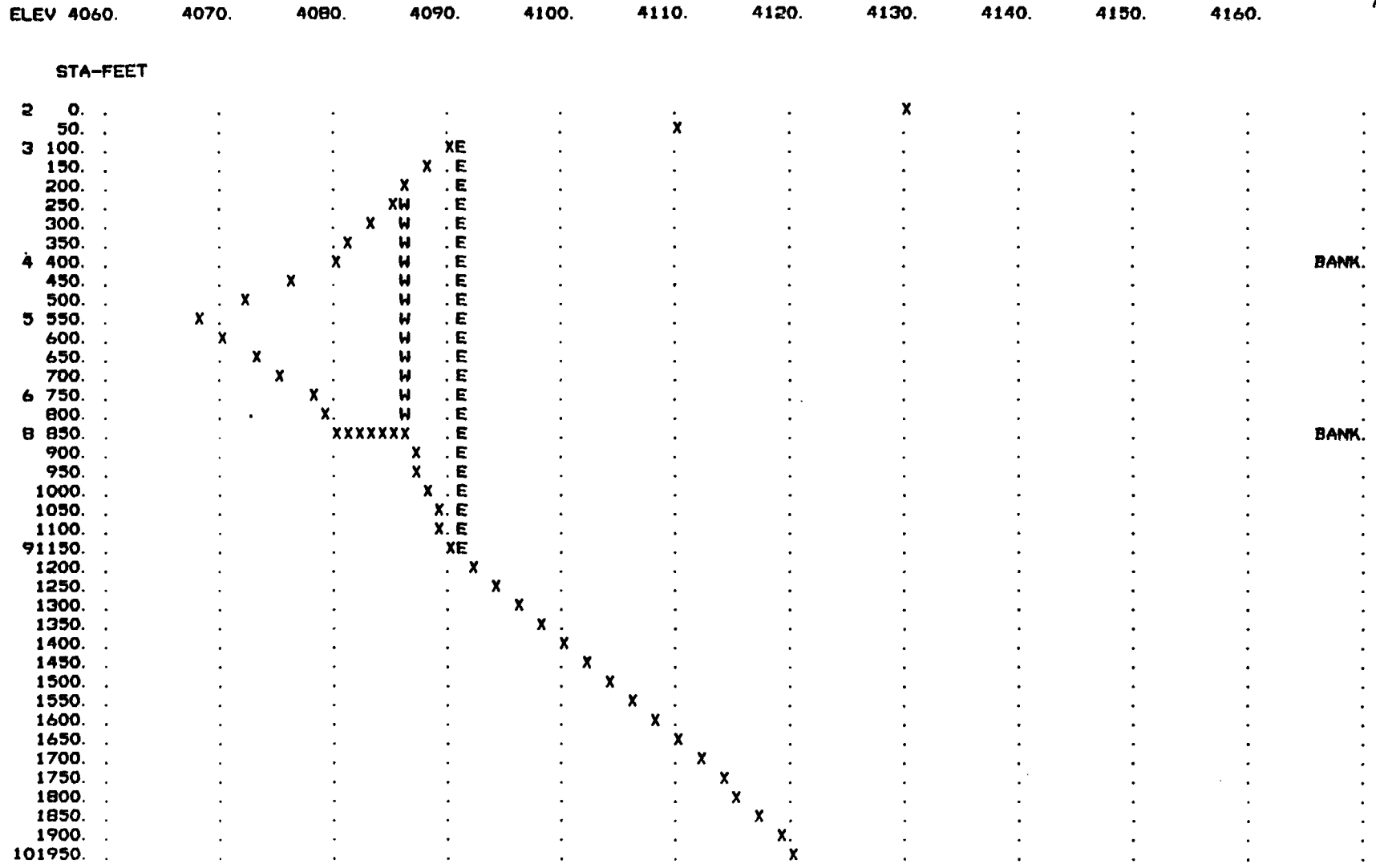
4130.00	0.00	4100.00	80.00	4090.00	170.00	4080.00	400.00	4074.00	455.00
4072.00	570.00	4076.00	620.00	4080.00	880.00	4088.00	925.00	4090.00	1150.00
4110.00	1640.00	4120.00	1820.00						

CROSS SECTION 4.00  
 STREAM DISCHARGE = 100000 CFS  
 DISCHARGE= 100000.

Sh. 23B.8

JTK 4/16/87  
 HM 5/19/87

PLOTTED POINTS (BY PRIORITY)-B=BOTTOM BRIDGE, T=TOP BRIDGE, X=GROUND, W=WATER SUR, E=ENERGY GRADIENT, C=CRITICAL WSEL



NRD= 0 ELLC= 9999999.00 ELTRD= 9999999.00

EL(I), STA(I)

4130.00	0.00	4090.00	100.00	4080.00	385.00	4068.00	530.00	4078.00	750.00
4080.00	840.00	4086.00	870.00	4090.00	1165.00	4120.00	1930.00		





Sh. 23B.11

JTK 4/16/87  
HM 5/19/87

\*\*\*\*\*  
HEC2 RELEASE DATED NOV 76 UPDATED MAY 1984  
ERROR CORR - 01, 02, 03, 04, 05, 06  
MODIFICATION - 50, 51, 52, 53, 54, 55, 56  
\*\*\*\*\*

NOTE- ASTERISK (\*) AT LEFT OF CROSS-SECTION NUMBER INDICATES MESSAGE IN SUMMARY OF ERRORS LIST

DISCHARGE = 100000 CFS

SUMMARY PRINTOUT

SECNO	Q	CWSEL	CRWS	GLOB	QCH	GRQB	GLOBP	QCMP	GRQBP	VLOB	VCH	VROB
1.000	100000.00	4096.62	4096.93	1630.48	98369.52	0.00	1.63	98.37	0.00	6.94	18.45	0.00
2.000	100000.00	4086.91	4088.81	4193.84	94467.47	1338.69	4.19	94.47	1.34	9.77	22.27	8.73
* 2.500	100000.00	4086.21	4086.21	614.70	98987.43	397.86	0.61	98.99	0.40	6.37	16.77	5.67
* 3.000	100000.00	4087.34	4087.34	4128.52	94971.57	899.91	4.13	94.97	0.90	6.66	17.87	5.94
* 4.000	100000.00	4086.08	4086.08	3080.27	96435.16	484.55	3.08	96.44	0.48	5.84	18.31	5.23
5.000	100000.00	4082.32	4083.06	6775.17	92837.50	387.33	6.78	92.84	0.39	8.81	17.97	3.46
5.500	100000.00	4078.18	4079.53	1062.46	98786.02	151.53	1.06	98.79	0.15	9.28	19.29	3.83
* 6.000	100000.00	4080.96	4080.96	1120.24	95803.27	3076.48	1.12	95.80	3.08	6.73	15.24	4.11
7.000	100000.00	4068.11	4071.22	1512.11	96984.69	1503.22	1.51	96.98	1.50	10.50	25.27	5.90

16-APR-87 15:57:35

PAGE 7

DISCHARGE = 100000 CFS

Sh. 23B. 12

SUMMARY PRINTOUT

JFK 4/16/87  
MM 5/19/87

SECNO	KRATIO	AREA	CWSEL	ELMIN	DEPTH	DIFWSX	HV	TOPWID	SSTA	ENDST	K*CHSL	10K*B
1.000	0.00	5567.30	4096.62	4080.00	16.62	0.00	5.21	613.87	79.03	692.91	0.00	89.92
2.000	1.37	4823.97	4086.91	4074.00	12.91	-9.71	7.35	688.72	255.68	944.40	-9.84	168.02
* 2.500	1.19	6068.58	4086.21	4073.00	13.21	-0.70	4.33	713.67	268.93	982.60	-2.86	84.12
* 3.000	1.64	6085.87	4087.34	4072.00	15.34	1.13	4.74	690.17	231.13	921.30	-2.63	71.89
* 4.000	1.13	5886.97	4086.08	4068.00	18.08	-1.26	5.04	664.36	211.67	876.03	-12.58	71.15
5.000	1.20	6047.20	4082.32	4064.00	18.32	-3.76	4.74	1015.12	83.98	1099.10	-8.70	103.23
5.500	1.20	5276.52	4078.18	4062.00	16.18	-4.14	5.72	778.23	148.09	926.32	-8.00	148.36
* 6.000	0.78	7202.15	4080.96	4062.00	18.96	2.78	3.47	1232.53	62.16	1294.70	0.00	79.92
7.000	2.20	4236.59	4068.11	4056.00	12.11	-12.84	9.65	1182.01	172.02	1354.03	-15.00	386.79



## SUMMARY OF ERRORS AND SPECIAL NOTES

CAUTION	SECNO=	2.500	PROFILE= 1	CRITICAL DEPTH ASSUMED
CAUTION	SECNO=	2.500	PROFILE= 1	PROBABLE MINIMUM SPECIFIC ENERGY
CAUTION	SECNO=	2.500	PROFILE= 1	20 TRIALS ATTEMPTED TO BALANCE WSEL
CAUTION	SECNO=	3.000	PROFILE= 1	CRITICAL DEPTH ASSUMED
CAUTION	SECNO=	3.000	PROFILE= 1	PROBABLE MINIMUM SPECIFIC ENERGY
CAUTION	SECNO=	3.000	PROFILE= 1	20 TRIALS ATTEMPTED TO BALANCE WSEL
CAUTION	SECNO=	4.000	PROFILE= 1	CRITICAL DEPTH ASSUMED
CAUTION	SECNO=	4.000	PROFILE= 1	PROBABLE MINIMUM SPECIFIC ENERGY
CAUTION	SECNO=	4.000	PROFILE= 1	20 TRIALS ATTEMPTED TO BALANCE WSEL
CAUTION	SECNO=	6.000	PROFILE= 1	CRITICAL DEPTH ASSUMED
CAUTION	SECNO=	6.000	PROFILE= 1	PROBABLE MINIMUM SPECIFIC ENERGY
CAUTION	SECNO=	6.000	PROFILE= 1	20 TRIALS ATTEMPTED TO BALANCE WSEL

Sh. 23B. 13

FTR 4/16/87  
HM 5/19/87



\*\*\*\*\*  
 \* WATER SURFACE PROFILES \*  
 \* VERSION OF NOVEMBER 1976 \*  
 \* UPDATED MAY 1984 \*  
 \*  
 \* RUN DATE 21-APR-87 TIME 11:30:48 \*  
 \*\*\*\*\*

\*\*\*\*\*  
 \* U. S. ARMY CORPS OF ENGINEERS \*  
 \* THE HYDROLOGIC ENGINEERING CENTER \*  
 \* 609 SECOND STREET, SUITE D \*  
 \* DAVIS, CALIFORNIA 95616 \*  
 \* (916) 440-2105 (FTS) 448-2105 \*  
 \*\*\*\*\*

Sh. 23C. 2

X	X	XXXXXXXX	XXXXXX		XXXXX
X	X	X	X	X	X
X	X	X	X	X	X
XXXXXXXX	XXXX	X		XXXXX	XXXXXX
X	X	X	X	X	X
X	X	X	X	X	X
X	X	XXXXXXXX	XXXXXX		XXXXXXX

FR 4/21/87  
 HM 5/19/87

Sh. 23C.3

\*\*\*\*\*  
 HEC2 RELEASE DATED NOV 76 UPDATED MAY 1984  
 ERROR CORR - 01, 02, 03, 04, 05, 06  
 MODIFICATION - 50, 51, 52, 53, 54, 55, 56  
 \*\*\*\*\*

JPK 4/21/87  
 NM 5/19/87

T1 UMTRA - GREEN RIVER - LOCAL PMF  
 T2 WATER SURFACE PROFILE ON BROWN WASH  
 T3 DISCHARGE = 100000 CFS

J1	ICHECK	ING	NINV	IDIR	STRT	METRIC	HVINS	Q	WSEL	FG
	0.	0.	0.	1.	0.009000	0.00	0.0	100000.	4085.000	0.000
J2	NPROF	IPLT	PRFVS	XSECV	XSECH	FN	ALLDC	IBW	CHNIM	ITRACE
	-1.000	0.000	0.000	0.000	0.000	0.000	-1.000	0.000	0.000	0.000
J3	VARIABLE CODES FOR SUMMARY PRINTOUT									
	38.000	43.000	1.000	2.000	13.000	14.000	15.000	35.000	60.000	59.000
	55.000	26.000	56.000	0.000	38.000	58.000	25.000	1.000	42.000	8.000
	51.000	10.000	4.000	53.000	54.000	33.000	5.000	0.000	0.000	0.000
NC	0.045	0.050	0.035	0.100	0.300	0.000	0.000	0.000	0.000	0.000
X1	2.000	11.000	380.000	900.000	350.000	300.000	350.000	0.000	0.000	0.000
GR	4114.000	0.000	4090.000	200.000	4080.000	380.000	4074.000	400.000	4074.000	430.000
GR	4078.000	510.000	4080.000	600.000	4080.000	900.000	4094.000	990.000	4094.000	1170.000
GR	4120.000	1890.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
X1	2.500	12.000	300.000	960.000	365.000	380.000	380.000	0.000	0.000	0.000
GR	4110.000	0.000	4090.000	250.000	4080.000	300.000	4073.000	420.000	4076.000	500.000
GR	4076.000	560.000	4078.000	620.000	4078.000	800.000	4080.000	960.000	4091.000	1000.000
GR	4096.000	1330.000	4110.000	1700.000	0.000	0.000	0.000	0.000	0.000	0.000
NC	0.000	0.000	0.000	0.200	0.500	0.000	0.000	0.000	0.000	0.000
X1	3.000	12.000	400.000	880.000	315.000	320.000	318.000	0.000	0.000	1.000
GR	4130.000	0.000	4100.000	80.000	4090.000	170.000	4080.000	400.000	4074.000	455.000
GR	4072.000	570.000	4076.000	620.000	4080.000	880.000	4088.000	925.000	4090.000	1150.000
GR	4110.000	1640.000	4120.000	1820.000	0.000	0.000	0.000	0.000	0.000	0.000
X1	4.000	9.000	385.000	840.000	470.000	440.000	460.000	0.000	0.000	1.000
GR	4130.000	0.000	4090.000	100.000	4080.000	385.000	4068.000	530.000	4078.000	750.000
GR	4080.000	840.000	4086.000	870.000	4090.000	1165.000	4120.000	1930.000	0.000	0.000



21-APR-87 11:30:49

Sh. 23C.5  
PAGE 3

SECNO	DEPTH	CWSEL	CRWS	WSELK	EQ	HV	HL	DLOSS	BANK ELEV
Q	GLOB	QCH	GRQB	ALOB	ACH	AROB	VOL	TWA	LEFT/RIGHT
TIME	VLOB	VCH	VROB	XML	XNCH	XNR	WTN	ELMIN	SSTA
SLOPE	XLOBL	XLCH	XLOBR	ITRIAL	IDC	ICONT	CORAR	TOPWID	ENDST

JTK 4/21/87  
HM 5/14/87

\*PROF 1

CRITICAL DEPTH TO BE CALCULATED AT ALL CROSS SECTIONS

CCHV= 0.100 CEHV= 0.300

\*SECNO 2.000

2.00	14.47	4088.47	4088.91	4085.00	4093.43	4.95	0.00	0.00	4080.00
100000.	5314.	92989.	1696.	646.	5057.	231.	0.	0.	4080.00
0.00	8.22	18.39	7.35	0.045	0.035	0.050	0.000	4074.00	227.47
0.009061	0.	0.	0.	0	11	4	0.00	727.01	954.48

\*SECNO 2.500

3301 HV CHANGED MORE THAN HVINS

3685 20 TRIALS ATTEMPTED WSEL, CWSEL  
3693 PROBABLE MINIMUM SPECIFIC ENERGY  
3720 CRITICAL DEPTH ASSUMED

2.50	13.14	4086.14	4086.14	0.00	4090.55	4.40	3.09	0.37	4080.00
100000.	604.	99005.	391.	94.	5856.	69.	48.	6.	4080.00
0.01	6.40	16.91	5.70	0.045	0.035	0.050	0.000	4073.00	269.28
0.008639	350.	350.	300.	20	11	0	0.00	713.07	982.34

CCHV= 0.200 CEHV= 0.500

\*SECNO 3.000

3685 20 TRIALS ATTEMPTED WSEL, CWSEL  
3693 PROBABLE MINIMUM SPECIFIC ENERGY  
3720 CRITICAL DEPTH ASSUMED

3.00	15.35	4087.35	4087.35	0.00	4092.09	4.73	2.98	3.11	4080.00
100000.	4135.	94963.	901.	621.	5318.	152.	101.	12.	4080.00
0.01	6.66	17.86	5.93	0.045	0.035	0.050	0.000	4072.00	230.93
0.007170	365.	380.	380.	20	8	0	0.00	690.42	921.35

\*SECNO 4.000

3685 20 TRIALS ATTEMPTED WSEL, CWSEL  
3693 PROBABLE MINIMUM SPECIFIC ENERGY  
3720 CRITICAL DEPTH ASSUMED

4.00	18.08	4086.08	4086.08	0.00	4091.12	5.04	2.27	0.55	4080.00
100000.	3080.	96435.	485.	527.	5267.	93.	144.	17.	4080.00
0.02	5.84	18.31	5.23	0.045	0.035	0.050	0.000	4068.00	211.67
0.007115	315.	318.	320.	20	11	0	0.00	664.36	876.03

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Sh. 23C.6  
PAGE 4

JTK  
4/21/97  
HM 5/19/87

SECNO Q TIME SLOPE	DEPTH GLOB VLOB XLOBL	CWSEL GCH VCH XLCH	CRISW GROB VROB XLOBR	WSELK ALOB XNL ITRIAL	EQ ACH XNCH IDC	HV AROB XNR ICONT	HL VOL WTN CORAR	LOSS TWA ELMIN TOPWID	BANK ELEV LEFT/RIGHT SSTA ENDST
*SECNO 5.000									
5.00	18.32	4082.32	4083.06	0.00	4087.06	4.74	3.91	0.15	4076.00
100000.	6775.	92838.	387.	769.	5166.	112.	207.	26.	4076.00
0.02	8.81	17.97	3.46	0.045	0.035	0.050	0.000	4064.00	83.98
0.010323	470.	460.	440.	5	8	0	0.00	1015.12	1099.10

CCHV= 0.100 CEHV= 0.300  
\*SECNO 5.500

3301 HV CHANGED MORE THAN HVINS

5.50	16.18	4078.18	4079.53	0.00	4083.90	5.72	3.06	0.10	4071.00
100000.	1062.	98786.	152.	115.	5122.	40.	240.	31.	4076.00
0.03	9.28	19.29	3.83	0.045	0.035	0.050	0.000	4062.00	148.09
0.014836	230.	250.	290.	7	8	0	0.00	778.23	926.32

\*SECNO 6.000

3301 HV CHANGED MORE THAN HVINS

3685 20 TRIALS ATTEMPTED WSEL, CWSEL  
3693 PROBABLE MINIMUM SPECIFIC ENERGY  
3720 CRITICAL DEPTH ASSUMED

6.00	18.96	4080.96	4080.96	0.00	4084.43	3.47	2.86	0.78	4074.00
100000.	1120.	95803.	3076.	166.	6287.	748.	278.	37.	4078.00
0.03	6.73	15.24	4.11	0.045	0.035	0.050	0.000	4062.00	62.16
0.007992	150.	270.	280.	20	11	0	0.00	1232.53	1294.70

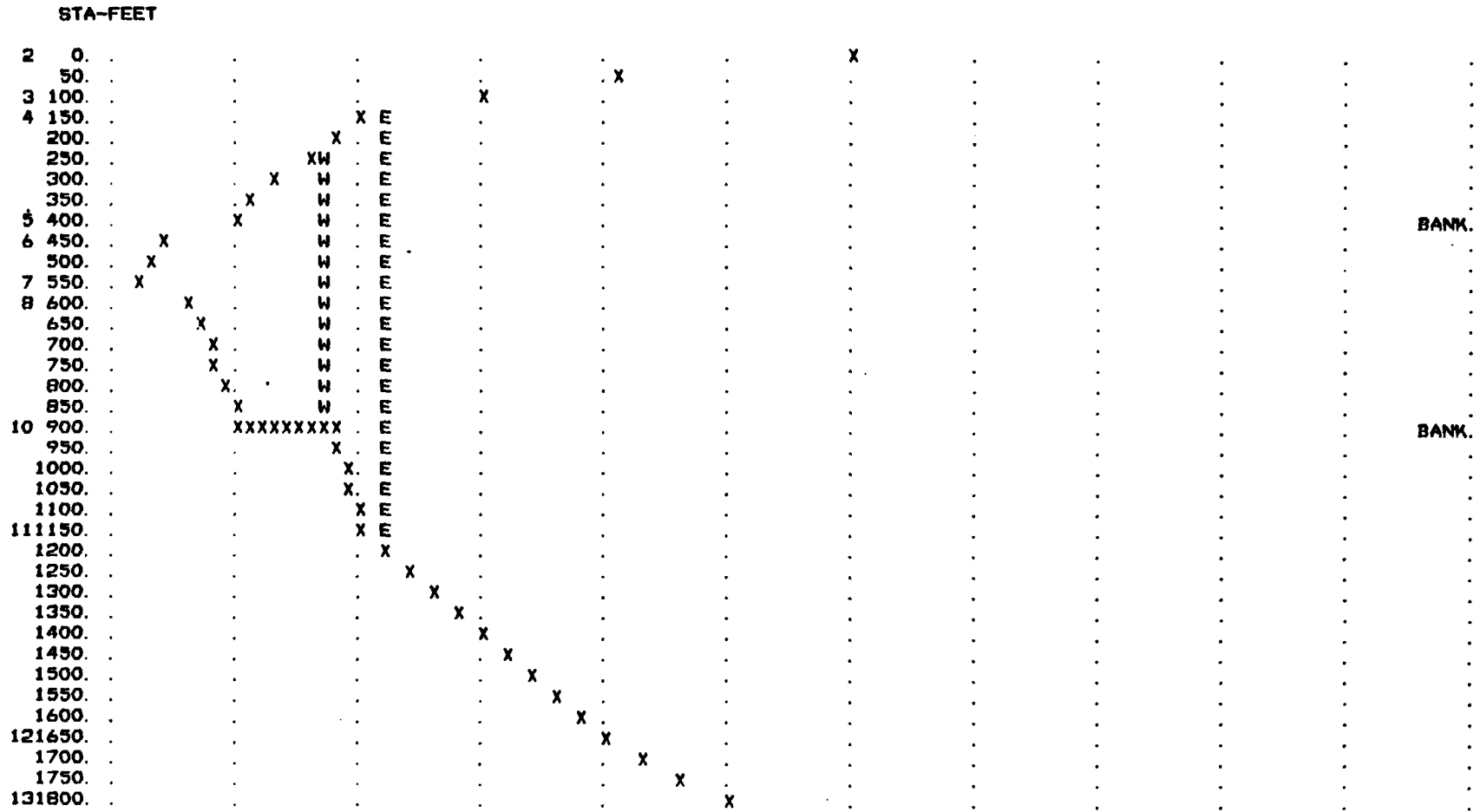
CROSS SECTION 3.00  
 STREAM DISCHARGE = 100000 CFS  
 DISCHARGE= 100000.

Sh. 23C.7

JTK 4/24/87  
 HM 5/19/87

PLOTTED POINTS (BY PRIORITY)-B=BOTTOM BRIDGE, T=TOP BRIDGE, X=GROUND, W=WATER SUR, E=ENERGY GRADIENT, C=CRITICAL WSEL

ELEV 4070. 4080. 4090. 4100. 4110. 4120. 4130. 4140. 4150. 4160. 4170.



NRD= 0 ELLC= 9999999.00 ELTRD= 9999999.00

EL(I), STA(I)	4130.00	4072.00	4110.00	4100.00	4090.00	4120.00	4130.00	4140.00	4150.00	4160.00	4170.00
	0.00	570.00	1640.00	80.00	170.00	880.00	4080.00	400.00	4074.00	455.00	
				620.00	4080.00	4088.00	925.00	4090.00	1150.00		
				1820.00							



CROSS SECTION 4.00  
 STREAM DISCHARGE = 100000 CFS  
 DISCHARGE = 100000.

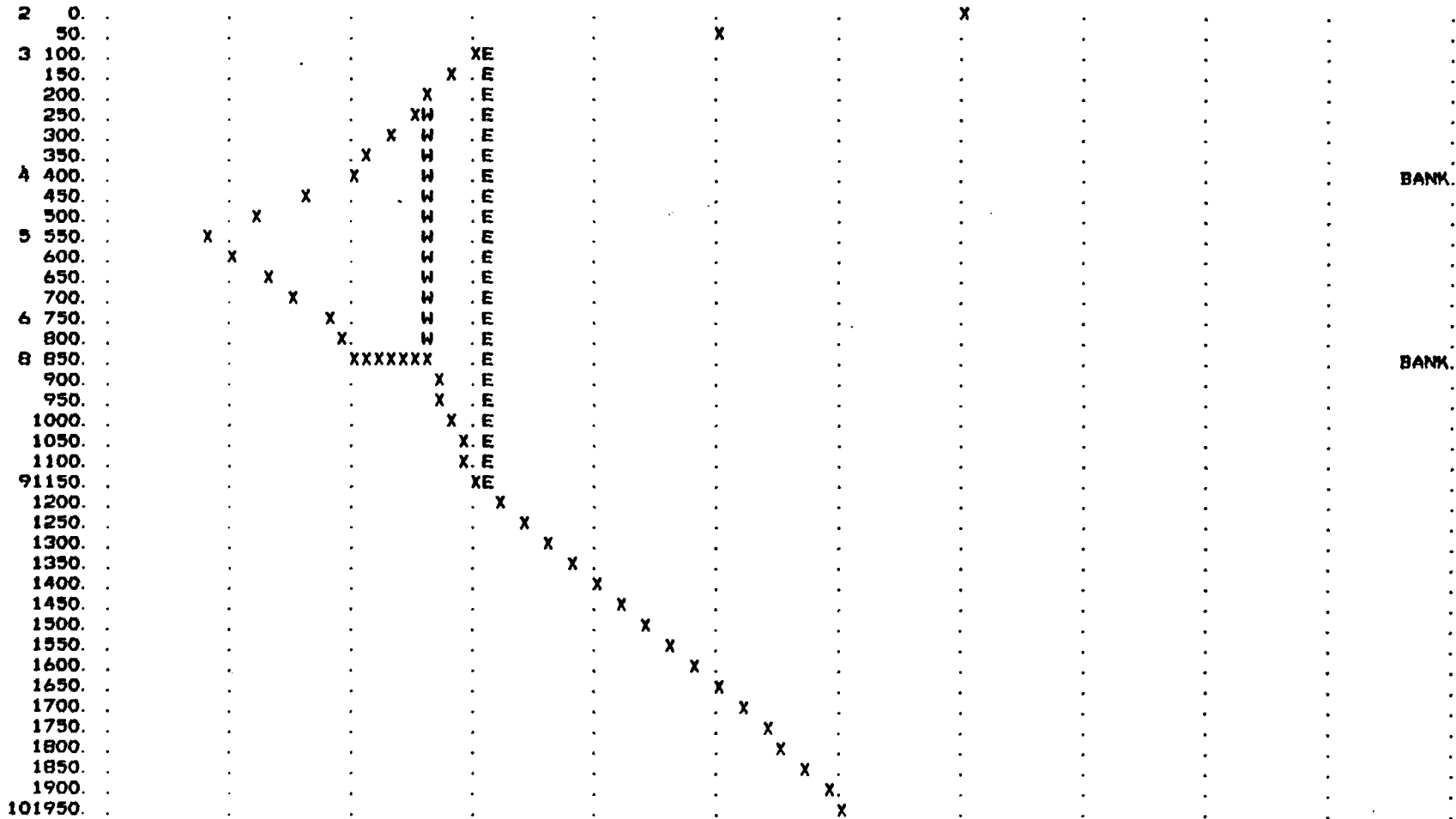
Sh. 23C.8

JFK  
 4/21/87  
 KM 5/14/87

PLOTTED POINTS (BY PRIORITY)-B=BOTTOM BRIDGE, T=TOP BRIDGE, X=GROUND, W=WATER SUR, E=ENERGY GRADIENT, C=CRITICAL WSEL

ELEV 4060. 4070. 4080. 4090. 4100. 4110. 4120. 4130. 4140. 4150. 4160.

STA-FEET



NRD= 0 ELLC= 9999999.00 ELTRD= 9999999.00

EL(I), STA(I)

4130.00	0.00	4090.00	100.00	4080.00	385.00	4068.00	530.00	4078.00	750.00
4080.00	840.00	4086.00	870.00	4090.00	1165.00	4120.00	1930.00		

PROFILE FOR STREAM DISCHARGE = 100000 CFS

Sh. 23C.9

PLOTTED POINTS (BY PRIORITY)-E-ENERGY, W-WATER SURFACE, I-INVERT, C-CRITICAL W. S., L-LEFT BANK, R-RIGHT BANK, M-LOWER END STA

JTK 4/21/87  
HM 5/14/87

ELEVATION SECND	4060. CUMDIS	4070.	4080.	4090.	4100.	4110.	4120.	4130.	4140.	4150.
2.00	0.		I	L	WC	E				
	50.		I	L	WC	E				
	100.		I	L	W	E				
	150.		I	L	WC	E				
	200.		I	L	W	E				
	250.		I	L	W	E				
	300.		I	L	WC	E				
2.50	350.		I	L	W	E				
	400.		I	L	W	E				
	450.		I	L	W	E				
	500.		I	L	W	E				
	550.		I	L	W	E				
	600.		I	L	W	E				
	650.		I	L	W	E				
	700.		I	L	W	E				
3.00	750.		I	L	W	E				
	800.		I	L	W	E				
	850.		I	L	W	E				
	900.		I	L	W	E				
	950.		I	L	W	E				
4.00	1000.		I	L	W	E				
	1050.		I	L	W	E				
	1100.		I	L	W	E				
	1150.		I	L	W	E				
	1200.		I	L	W	E				
	1250.		I	L	WC	E				
	1300.		I	L	W	E				
	1350.		I	L	W	E				
	1400.		I	L	WC	E				
	1450.		I	L	W	E				
5.00	1500.		I	L	WC	E				
	1550.		I	L	WC	E				
	1600.		I	LR	WC	E				
	1650.		I	L	WC	E				
	1700.		I	L	R	WC	E			
	1750.		I	L	R	WC	E			
5.50	1800.		I	L	R	WC	E			
	1850.		I	L	R	WC	E			
	1900.		I	L	R	WC	E			
	1950.		I	L	R	W	E			
6.00	2000.		I	L	R	WC	E			
	2050.		I	L	R	W	E			

*Sh. 23C.10*

*JR 4/21/87  
HM 4/19/87*

\*\*\*\*\*  
 HEC2 RELEASE DATED NOV 76 UPDATED MAY 1984  
 ERROR CORR - 01, 02, 03, 04, 05, 06  
 MODIFICATION - 50, 51, 52, 53, 54, 55, 56  
 \*\*\*\*\*

NOTE- ASTERISK (\*) AT LEFT OF CROSS-SECTION NUMBER INDICATES MESSAGE IN SUMMARY OF ERRORS LIST

DISCHARGE = 100000 CFS

SUMMARY PRINTOUT

	SECNO	Q	CWSEL	CRWS	GLOB	GCH	GROB	GLOBP	GCHP	GROBP	VLOB	VCH	VROB
	2.000	100000.00	4088.47	4088.91	5314.26	92989.40	1696.34	5.31	92.99	1.70	8.22	18.39	7.35
*	2.500	100000.00	4086.14	4086.14	604.33	99004.52	391.15	0.60	99.00	0.39	6.40	16.91	5.70
*	3.000	100000.00	4087.35	4087.35	4135.43	94963.16	901.42	4.14	94.96	0.90	6.66	17.86	5.93
*	4.000	100000.00	4086.08	4086.08	3080.27	96435.16	484.55	3.08	96.44	0.48	5.84	18.31	5.23
	5.000	100000.00	4082.32	4083.06	6775.17	92837.50	387.33	6.78	92.84	0.39	8.81	17.97	3.46
	5.500	100000.00	4078.18	4079.53	1062.46	98786.02	151.53	1.06	98.79	0.15	9.28	19.29	3.83
*	6.000	100000.00	4080.96	4080.96	1120.24	95803.27	3076.48	1.12	95.80	3.08	6.73	15.24	4.11

21-APR-87 11:30:49

Sh. 23C-11

PAGE 6

DISCHARGE = 100000 CFS

SUMMARY PRINTOUT

JTK 4/21/87  
HM 5/14/87

SECNO	KRATID	AREA	CWSEL	ELMIN	DEPTH	DIFWSX	HV	TOPWID	SSTA	ENDST	K*CHSL	10K*B
2.000	0.00	5933.66	4088.47	4074.00	14.47	0.00	4.95	727.01	227.47	954.48	0.00	90.61
* 2.500	1.09	6018.59	4086.14	4073.00	13.14	-2.33	4.40	713.07	269.28	982.34	-2.86	86.39
* 3.000	1.61	6091.74	4087.35	4072.00	15.35	1.21	4.73	690.42	230.93	921.35	-2.63	71.70
* 4.000	1.13	5886.97	4086.08	4068.00	18.08	-1.27	5.04	664.36	211.67	876.03	-12.58	71.15
5.000	1.20	6047.20	4082.32	4064.00	18.32	-3.76	4.74	1015.12	83.98	1099.10	-8.70	103.23
5.500	1.20	5276.52	4078.18	4062.00	16.18	-4.14	5.72	778.23	148.09	926.32	-8.00	148.36
* 6.000	0.78	7202.15	4080.96	4062.00	18.96	2.78	3.47	1232.53	62.16	1294.70	0.00	79.92

Sh. 23C.12

SUMMARY OF ERRORS AND SPECIAL NOTES

CAUTION	SECNO=	2.500	PROFILE=	1	CRITICAL DEPTH ASSUMED
CAUTION	SECNO=	2.500	PROFILE=	1	PROBABLE MINIMUM SPECIFIC ENERGY
CAUTION	SECNO=	2.500	PROFILE=	1	20 TRIALS ATTEMPTED TO BALANCE WSEL
CAUTION	SECNO=	3.000	PROFILE=	1	CRITICAL DEPTH ASSUMED
CAUTION	SECNO=	3.000	PROFILE=	1	PROBABLE MINIMUM SPECIFIC ENERGY
CAUTION	SECNO=	3.000	PROFILE=	1	20 TRIALS ATTEMPTED TO BALANCE WSEL
CAUTION	SECNO=	4.000	PROFILE=	1	CRITICAL DEPTH ASSUMED
CAUTION	SECNO=	4.000	PROFILE=	1	PROBABLE MINIMUM SPECIFIC ENERGY
CAUTION	SECNO=	4.000	PROFILE=	1	20 TRIALS ATTEMPTED TO BALANCE WSEL
CAUTION	SECNO=	6.000	PROFILE=	1	CRITICAL DEPTH ASSUMED
CAUTION	SECNO=	6.000	PROFILE=	1	PROBABLE MINIMUM SPECIFIC ENERGY
CAUTION	SECNO=	6.000	PROFILE=	1	20 TRIALS ATTEMPTED TO BALANCE WSEL

JJK 4/21/87  
HM 5/14/87

Calculation Cover Sheet



Contract No. 5057

Discipline Earth Sci

Calc. No. 10-539-01-00<sup>01</sup>

No. of Sheets 10 / 11

Project UMTRA - Green River

Feature PMP for Erosion Protection

Item SOS Disposal Site

Sources of Data

- ③ Nelson J. D., et al "Methodologies for evaluating long-term Stabilization Designs of Uranium Mill Tailings Impoundments", prepared for Division of Waste Management, U.S. NRC, NRC FIN 80279, NUREG/CR-0600 ORNL/TM-10067, June, 1986.

Sources of Formulae & References

- ① TAC "Green River, draft Rap, site conceptual design Civil Engineering Calculations - Vol. 2", MKE Document No 5057-GRN-C-04-00062-00, 1987.
- ② Hanson et al, "Probable Maximum Precipitation Estimates, Colorado River and Great Basin Drainages, Hydrometeorological Report No. 49, prepared by the National Weather Service, Office of Hydrology, for the U.S. Department of Commerce and U.S. Dept. of the Army, Silver Spring, Maryland.

Preliminary Calc.

Final Calc.

Supersedes Calc. No.     

Rev. No.	Revision	Calculation By	Date	Checked By	Date	Approved By	Date
1	Changed to Final Calc	Martin J. Cochran	11-11-87	PK Chen	7/11/87	PK Chen	7/11/87
0	Checked effect of incorrect site location (Sh. 4 & 5)	FB Guros	9/18/87	PK Chen	9/18/87	PK Chen	9/18/87
0		James Kam	4/23/87	Martin J. Cochran	5/18/87	PK Chen	7/18/87

Project UMTKA - Green River  
Feature Hydrology  
Item PMP for pile design

Contract No. 5057  
Designed JK  
Checked MJG

Sheet 1  
File No. \_\_\_\_\_  
Date 4/22/87  
Date 5/18/87

Purpose: To derive a rainfall intensity frequency duration curve from the local 6-hr. PMP for the SOS disposal site

Summary of Results:

The derivation of precipitation data by TAC (ref. 1) from ref. 2 has been checked (sh. 2-7) and applied to the plotting of the rainfall intensity vs. duration curve (sh. 10). The parameters of a curve which best fits the data are determined as

$$\text{Log}(I) = 1.81 - 0.31 [\text{Log}(T_c)]^{1.77}$$

where  $I$  = rainfall intensity

$T_c$  = Time of concentration

The above equation can be entered into the computer program used for erosion protection design at the SOS disposal site

DATE 1/14/87 SUBJECT GRN - SOS disposal site SHEET 1  
 BY Dey CHKD. MJG 5/18/87 JOB NO. 05057010106  
PMP Calculations

Reference 1

III Calculations and Analysis

The table below contains the step-by-step procedure for determining the local-PMP for the Green River-SOS disposal site.

Table 6.3A.—Local-storm PMP computation, Colorado River, Great Basin and California drainages. For drainage average depth PMP. Go to table 6.3B if areal variation is required.

Drainage Green River SOS Disposal Site Area mi<sup>2</sup> (km<sup>2</sup>)  
 Latitude 38°58'58" Longitude 110°08'20" Minimum Elevation 4134 (ft) (m)

Steps correspond to those in sec. 6.3A.

1. Average 1-hr 1-mi<sup>2</sup> (2.6-km<sup>2</sup>) PMP for drainage [fig. 4.5]. 8.5 in. (mm)
2. a. Reduction for elevation. [No adjustment for elevations up to 5,000 feet (1,524 m): 5% decrease per 1,000 feet (305 m) above 5,000 feet (1,524 m)]. X
- b. Multiply step 1 by step 2a. 8.5 in. (mm)
3. Average 6/1-hr ratio for drainage [fig. 4.7]. 1.2

	Duration (hr)									
	1/4	1/2	3/4	1	2	3	4	5	6	
4. Durational variation for 6/1-hr ratio of step 3 [table 4.4].	<u>74</u>	<u>89</u>	<u>95</u>	<u>100</u>	<u>110</u>	<u>115</u>	<u>118</u>	<u>119</u>	<u>120</u>	<u>X</u>
5. <u>1-mi<sup>2</sup></u> (2.6-km <sup>2</sup> ) PMP for indicated durations [step 2b X step 4].	<u>6.3</u>	<u>7.6</u>	<u>8.1</u>	<u>8.5</u>	<u>9.4</u>	<u>9.8</u>	<u>10.0</u>	<u>10.1</u>	<u>10.2</u>	<u>in. (mm)</u>
6. Areal reduction [fig. 4.9].	<u>X</u>									
7. Areal reduced PMP [steps 5 X 6].	<u>6.3</u>	<u>7.6</u>	<u>8.1</u>	<u>8.5</u>	<u>9.4</u>	<u>9.8</u>	<u>10.0</u>	<u>10.1</u>	<u>10.2</u>	<u>in. (mm)</u>
8. Incremental PMP [successive subtraction in step 7].	largest 2nd 3rd 4th 5th least <u>8.5 0.9 0.4 0.2 0.1 0.1 in. (mm)</u> 6.3 1.3 0.5 0.4 } 15-min. increments									

checked FTK  
4/22/87



DATE 1/14/87

SUBJECT GEN - SOS disposal site  
PMP Calculations

SHEET NO. -

BY V. Day CHKD. MJF 5/18/87

JOB NO. 05051010106

III Calculations and Analysis - cont.

Reference 1

9. Time sequence of incremental PMP according to:

HMR No. 5

Hourly increments  
[table 4.7].

0.1 0.4 8.5 0.9 0.2 0.1 (20) ~~(10)~~

Four largest 15-min.  
increments [table 4.8].

6.3 1.3 0.5 0.4 (20) ~~(10)~~

Reference: Hansen, et al., 1977

IV Conclusions and Recommendations

A one-hour PMP rainfall value of 8.5" will be used in all related calculations. In some cases, a peak 5-minute intensity will be determined and converted to a maximum one-hour intensity. Likewise the 8.5" will be divided into 5-minute intervals in order to develop a rainfall hydrograph for estimating runoff.

checked JK

4/22/87

DATE 1/14/87  
BY V. Dery CHKD. MJE 5/18/87

SUBJECT GRN - SOS disposal site  
PMP Calculations

SHEET NO. 1  
JOB NO. OSOS101D106

II. Procedure, cont.

Approximate location of Green River SOS disposal area  
V = B.5"

Reference 1

Note: some "latitude" ties are incorrectly positioned on 110°, 115° and 120° Meridians

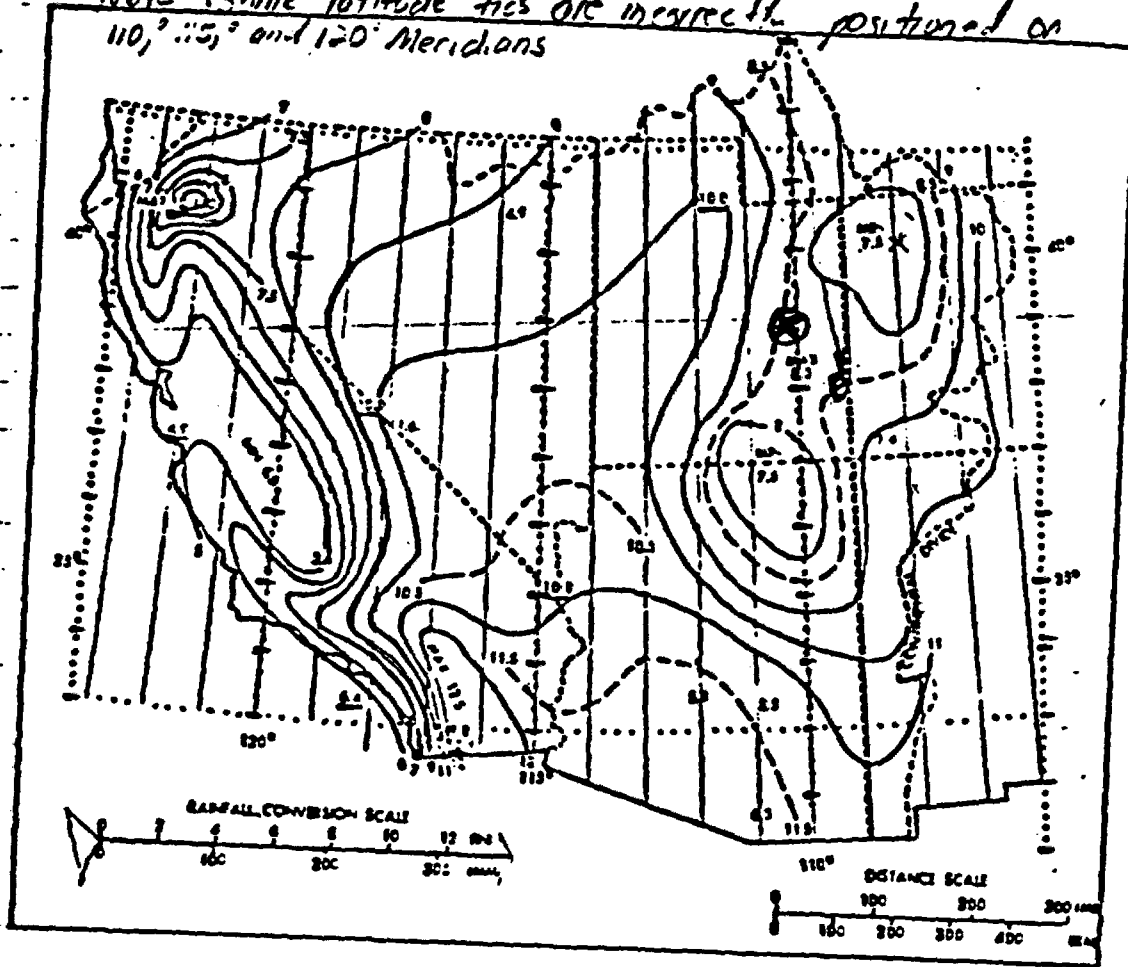


Figure 4.5 - Local-storm PMP for 1 mi<sup>2</sup> (2.6 km<sup>2</sup>) 1 hr. Directly applicable for locations between sea level and 5000 ft (1524 m). Elevation adjustment must be applied for locations above 5000 ft.

Reference: Hanson, et. al., 1977

NOTE: (X) INDICATES ACTUAL SITE LOCATION.  
HOWEVER, THE VALUE FOR LOCAL STORM  
PMP FROM THIS FIGURE REMAINS B.5"  
AS USED IN THIS CALC.

Checked  
JTK  
4/22/87

FBG 9-18-87  
PVL 9-18-87

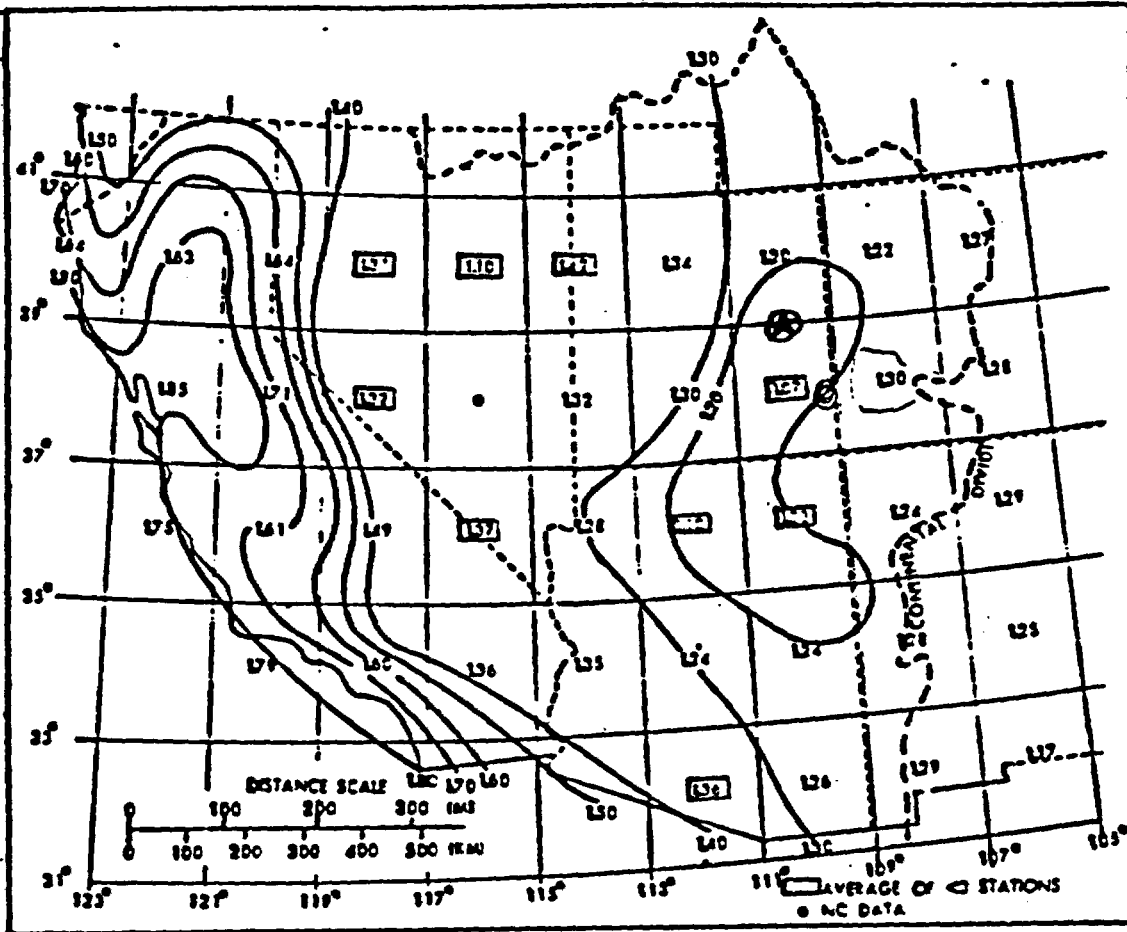
DATE 1/14/87 MF 5/14/87 SUBJECT GLN-SOS disposal site  
 BY V Day CHKD. \_\_\_\_\_ PMP Calculations

Sh. 5  
 SHEET NO. \_\_\_\_\_  
 JOB NO. OS05010106

II Procedure, cont.

Approximate location of Green River SOS disposal site;  $V = 1.20$

Reference 1



DATE 1/14/87

SUBJECT GRN-50's disposal site

SHEET NO. \_\_\_\_\_

BY V. Dery CHKD. M/L 5/14/87

PMP Calculations

JOB NO. 05051010106

II. Procedure, cont.

Reference 1

Table 4.4.—Durational variation of 1-mi<sup>2</sup> (2.6-km<sup>2</sup>) local-storm PMP in percent of 1-hr PMP (see figure 4.3)

checked  
JTK  
9/22/87

6/1-hr ratio	Duration (hr)								
	1/4	1/2	3/4	1	2	3	4	5	6
1.1	86	93	97	100	107	109	110	110	110
1.2	74	89	95	100	110	115	118	119	120
1.3	74	89	95	100	114	121	125	128	130
1.4	63	83	93	100	118	126	132	137	140
1.5	63	83	93	100	121	132	140	145	150
1.6	43	70	87	100	124	138	147	154	160
1.8	43	70	87	100	130	149	161	171	180
2.0	43	70	87	100	137	161	175	188	200

Reference: Hansen et al., 1977

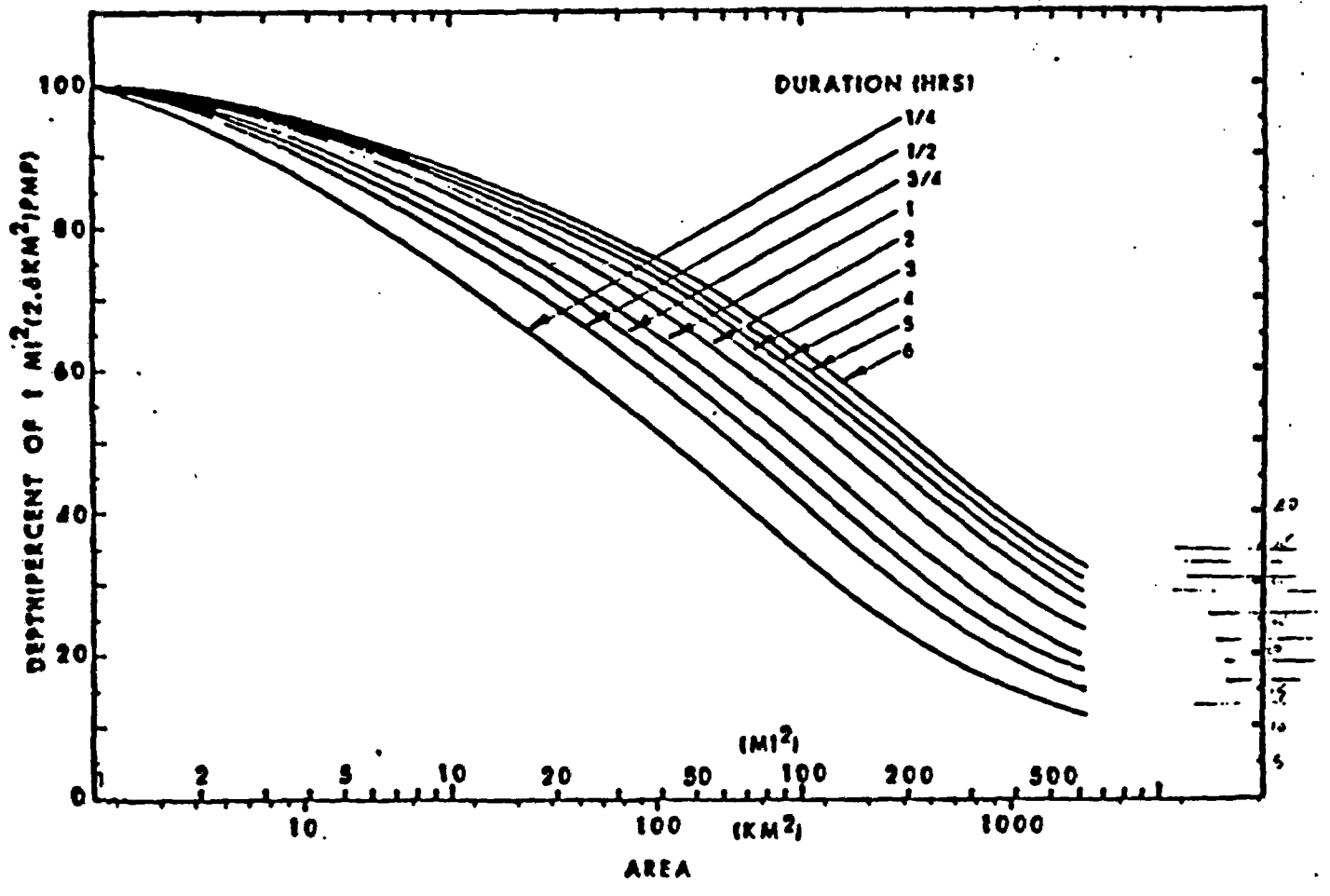


Figure 4.9.—Adopted depth-area relations for local-storm PMP.

Reference: Hansen, et al., 1977

DATE 1/14/87

SUBJECT GEN-505 disposal site  
PMP Calculations

SHEET NO. 5h. 7

BY V. Dery, OHKD. MJE 5/10/87

JOB NO. 05051010106

II. Procedure, cont.

Reference 1

Table 4.7.--Time sequence for hourly incremental PMP in 6-hr storm

Increment	Sequence Position	
	HMR No. 5 <sup>1</sup>	EM1110-2-1411 <sup>2</sup>
Largest hourly amount	Third	Fourth
2nd largest	Fourth	Third
3rd largest	Second	Fifth
4th largest	Fifth	Second
5th largest	First	Last
least	Last	First

- <sup>1</sup>U. S. Weather Bureau 1947.
- <sup>2</sup>U. S. Corps of Engineers 1952.

Reference: Hansen, et al., 1977

Table 4.8.--Time sequence for 15-min incremental PMP within 1 hr.

Increment	Sequence Position
Largest 15-min amount	First
2nd largest	Second
3rd largest	Third
least	Last

Reference: Hansen, et al., 1977

Note: The 15-minute distribution calculated in this analysis has been superseded by the 5-minute distribution sequence presented in the TAD (DOE, 1986).

Checked  
JFK

4/22/87

Project UNITRA - Green River  
Feature Hydrology  
Item PMP for pile design

Contract No. 5057  
Designed FTK  
Checked MJB

Sheet 82  
File No. \_\_\_\_\_  
Date 4/22/87  
Date 5/18/87

From Sh. 2 local PMP vs. duration (TAC's calculation)

Duration (min)	PMP (in)	Intensity (in/hr)
15	6.3	25.2
30	7.6	15.2
45	8.1	10.8
60	8.5	8.5
120	9.4	4.7
180	9.8	3.3
240	10.0	2.5

For durations smaller than 15 min, refer to Table on sh. 8b.  
from reference 3

2.5	2.3	56.1
5.0	3.8	45.9
10.0	5.3	31.6

PMP distribution for various rainfall durations Sheet B 6

10 Reference 3

JTK 4/22/87

to six hours although the majority of the precipitation falls within the first three hours of the storm. In order to reflect the durational and geographical differences between sites, ratios between the 6-hour general type storm and the 1-hour thunderstorm (6/1-hr ratios) were determined and are presented in Figure 2.4 for the southwest United States. Similar information is available in HMR 51 and HMR 55 (NWS, 1979 and 1984). Figure 2.4 indicates that the 6/1-hr ratios range from 1.1 to 2.0 and that a single depth-duration relation is not regionally applicable. Therefore, the 6/1-hr ratio is site specific and varies with drainage basin area. Furthermore, the lower the 6/1-hr ratio, the greater the local-storm PMP percentage that falls in the initial period of the storm.

For determining the PMF for a watershed or reclaimed site with small drainage areas, the rainfall intensity corresponding to the time of concentration must be determined. In order to determine the PMP rainfall intensity, the incremental PMP rainfall depths for a specific site must first be derived. The PMP rainfall depths can be estimated as a percent of the PMP values for both the 1-hour thunderstorm and the 6-hour general-type storm. Table 2.1 presents the rainfall duration and percent PMP values (thunderstorms ranging in duration from 2.5 to 60 minutes) for determining appropriate rainfall depths in the Colorado River basin (NWS, 1977 and NRC, 1985). Similar rainfall duration and PMP percentage relations can be developed for the northwest states (HMR 43), for the midwestern and eastern states (HMR 51) and for the region between the continental divide and the 103° meridian (HMR 55) as shown in Figure 2.2.

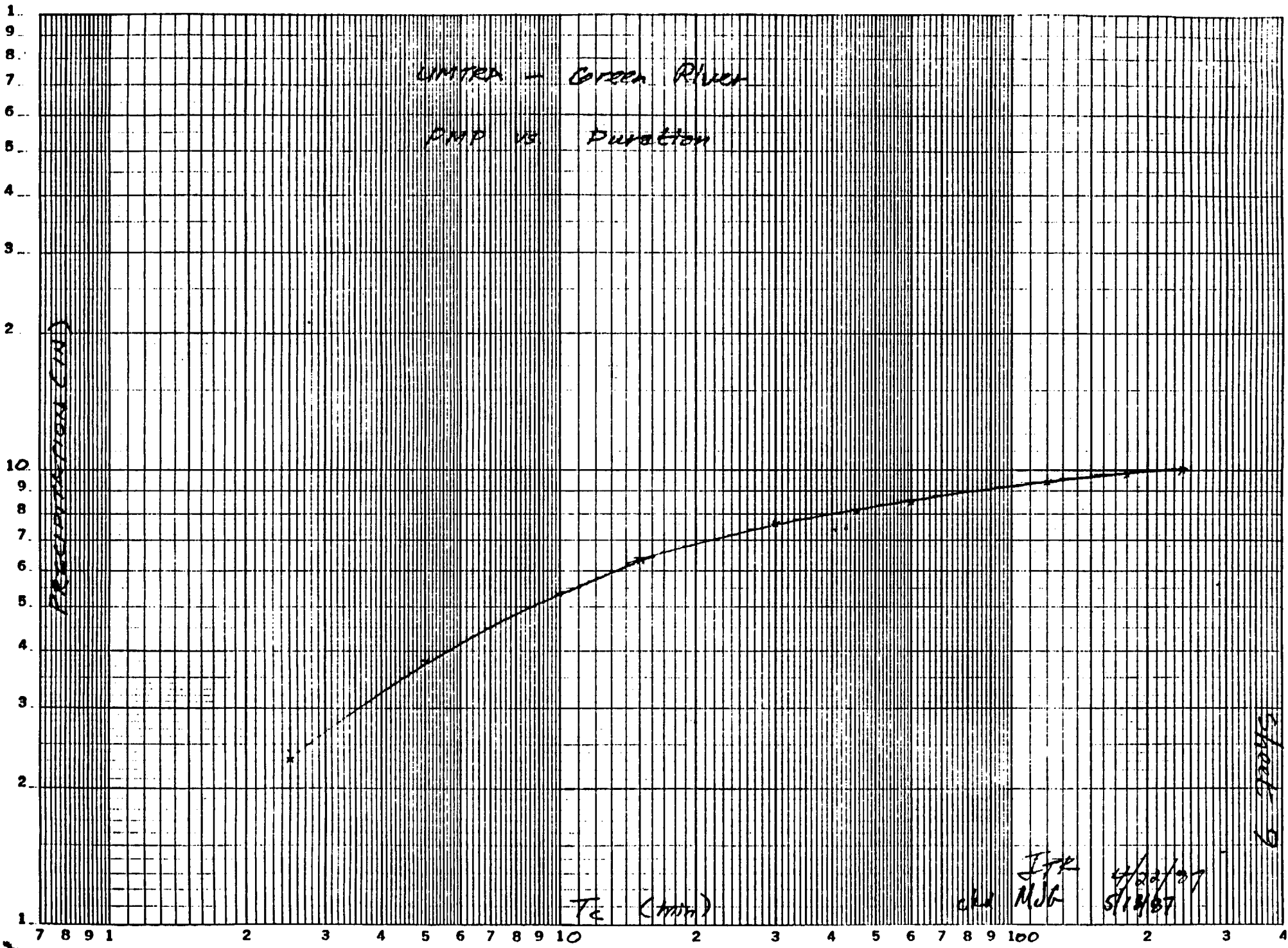
Table 2.1 Percent of Probable Maximum Precipitation for Various Rainfall Durations in the Colorado River Drainage Area.

Rainfall Duration min.	% of 1-hour PMP*
2.5	27.5
5	45
10	62
15	74
20	82
30	89
45	95
60	100

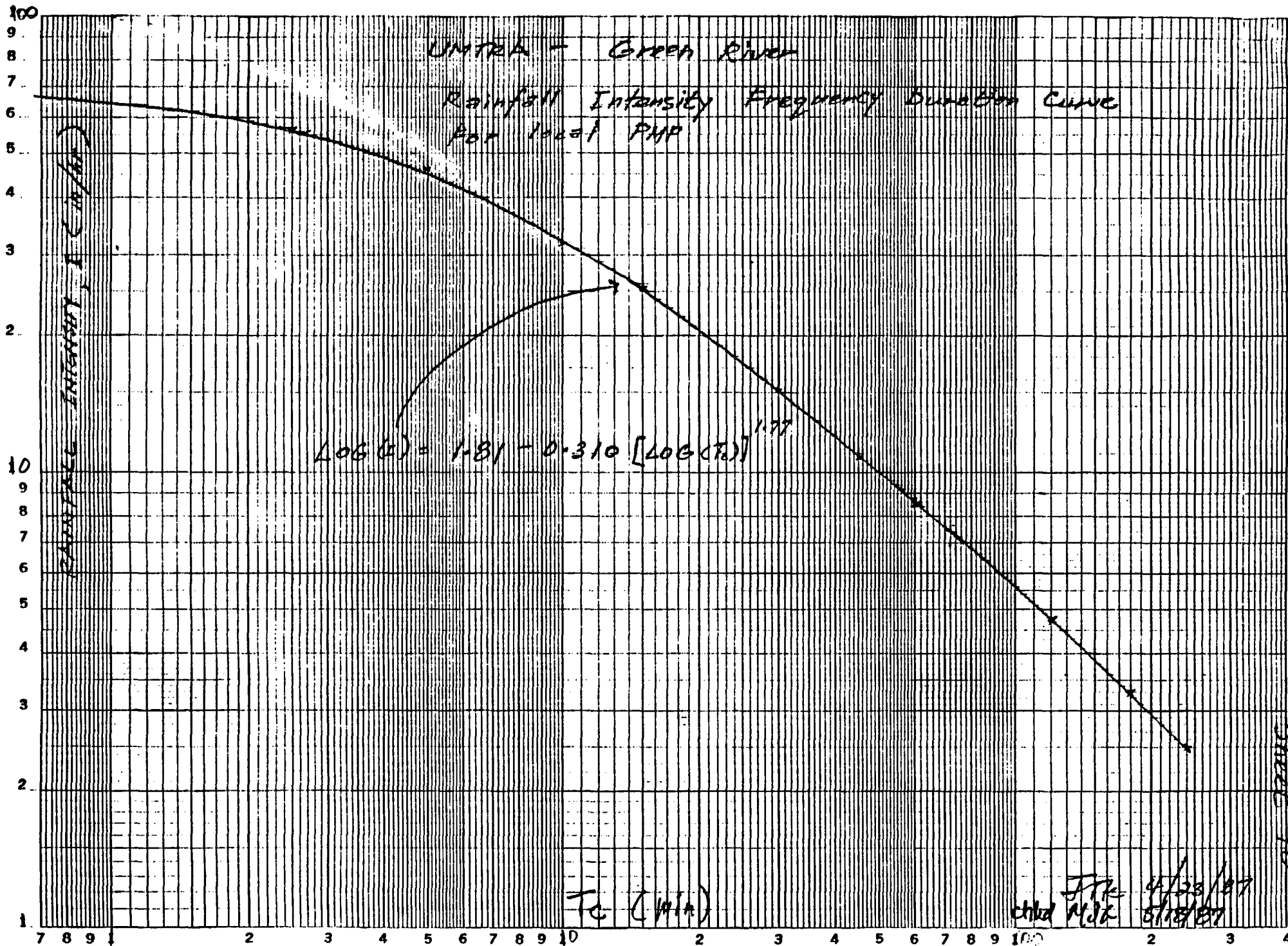
\*The 1-hour, 1 square mile local storm is derived using 6/1-hour ratios from 1.2 to 1.3.

Source: NWS, 1977 and NRC, 1985.

*cdl Martin Goodwin 5/18/87*







Calculation Cover Sheet



Contract No. 5057

Discipline Earth Sci

Calc. No. 10-534-01-009  
 No. of Sheets 110

Project

UMTRA - Green River

Feature

Hydrology

Item

Flood Frequency Analysis (10-YR & 25-YR)

Sources of Data

Sources of Formulae & References

- ① Haan, C.T. "Hydrology and sedimentology of surface mined lands"
- ② Miller J F et al. "Precipitation - frequency Atlas of the Western United States, NOAA ATLAS 2 vol. VI - Utah - U.S. Dept. of Commerce, NOAA, National Weather Service", 1973.
- ③ McCuen R.H., "A Guide to Hydrologic Analysis using SCS Methods", Prentice - Hall, Inc., 1982

Preliminary Calc.

Final Calc.

Supersedes Calc. No. \_\_\_\_\_

Rev. No.	Revision	Calculation By	Date	Checked By	Date	Approved By	Date
1	Changed to Final Calc	Martin J. Conrath	11-11-87	PK Cla	11/11/87	PK Cla	11/11/87
0		Janus Kam	5/1/87	HM	7/17/87	PK Cla	7/29/87



Project UNTEA - Green River  
Feature Hydrology  
Item Flooding Potential on Browns Wash

Contract No. 5057  
Designed JK  
Checked HM

Sheet 1  
File No. \_\_\_\_\_  
Date 5/1/07  
Date June 09, 12

Purpose: to determine the discharges in the Browns Wash resulting from the 10-yr and 25-yr 24-hr storm at the vicinity of the existing tailings pile. From the peak discharge, the maximum water level was derived.

Summary of Results:

The peak flows for the 10-yr and 25-yr 24 hr. storms are determined to be 11,300 and 15,300 cfs, respectively. The max. water level elevation resulting from these floods at Sta. 5+5 and 6+0 is estimated to be at 4078.35'.





Project UMTRA - COLLEA RIVER  
Feature Hydrology  
Item Flood frequency Analysis

Contract No. 5257  
Designed JTK  
Checked HM

Sheet 2  
File No. \_\_\_\_\_  
Date 4/28/87  
Date 7/16/87

Assume design life of project = 6 months =  $\frac{1}{2}$  yr.

i.e. excavation and clean-up of existing pile will take approx. 6 months.

By 
$$p = 1 - (1 - 1/T)^n$$

where  $p$  = probability that a  $T$ -yr. event will be equalled or exceeded at least once in an  $n$ -year period

$T$  = Design return period (yr)

$n$  = Design life of project (yr)

for  $T = 25$ -yr event,  $n = \frac{1}{2}$  yr.

$$p = 1 - (1 - 1/25)^{\frac{1}{2}}$$
$$= 0.02$$

If design life of project is extended to 1 yr. i.e.  $n = 1$  yr.  
and  $T = 25$ -yr event

$$p = 1 - (1 - 1/25)$$
$$= 0.04$$

$\therefore$  If the design is based on a 25-yr. event, at least 95% sure that this storm event will not be equalled or exceeded in either a 6-month or 1-yr period.





Project

UMTRA - Green River

Contract No.

5057

Sheet

3

Feature

Hydrology

Designed

JK

File No.

4/28/87

Item

Flood Frequency Analysis

Checked

HM

Date

7/16/87

Values of P for various T and n

		T		
		10-yr	25-yr	50-yr
n	1/2 yr	0.05	0.02	0.01
	1 yr.	0.10	0.04	0.02





Project

UMTRA - Green River

Contract No.

5057

Sheet

4

Feature

Hydrology

Designed

JK

File No.

4/28/87

Item

Flood Frequency Analysis

Checked

HM

Date

7/16/87

From figures on Sh. 11-18, the following precipitation values are tabulated:

Precipitation (inches)		Return Period				
		2-yr.	10-yr.	25-yr.	50-yr.	100-yr
Duration	1-hr.	.58 <sup>1)</sup>	.90 <sup>3)</sup>	1.10 <sup>3)</sup>	1.20 <sup>3)</sup>	1.47 <sup>2)</sup>
	6-hr.	.75	1.20	1.40	1.60	1.80
	24-hr.	.90	1.60	1.95	2.25	2.50

from sh. 6 ref. ②

$$\begin{aligned}
 1) Y_2 &= 2\text{-yr } 1\text{-hr. estimated value} \\
 &= -0.011 + 0.942 [ .75 (.75/.90) ] \\
 &= 0.58 \text{ " }
 \end{aligned}$$

$$\begin{aligned}
 2) Y_{100} &= 100\text{-yr } 1\text{-hr. estimated value} \\
 &= 0.494 + 0.755 [ 1.80 (1.80/2.50) ] \\
 &= 1.47 \text{ " }
 \end{aligned}$$

3) from plot on Sh. 10 : Precipitation depth vs. return period



Project UMTRA - Green River  
 Feature Hydrology  
 Item Flood Frequency Analysis

Contract No. 5057 Sheet 52  
 Designed JTK File No. \_\_\_\_\_  
 Checked KM Date 4/28/87  
 Date 7/16/87

Using data on sh. 4, plot data on precipitation depth-duration diagram on sh. 7 and 8

Precipitation (inches)

Hr.	Cumulative		Incremental		Incre. Sequence	
	25-yr.	50-yr.	25-yr.	50-yr.	25-yr.	50-yr.
6	1.40	1.60	1.40	1.60	0.15	0.20
12	1.70	1.90	0.30	0.30	0.30	0.30
18	1.80	2.10	0.10	0.20	0.10	0.15
24	1.95	2.25	0.15	0.15	0.05	0.06
7			1.10	1.20	0.05	0.07
8			0.10	0.10	0.05	0.07
9			0.05	0.10	0.05	0.10
10			0.05	0.07	0.05	0.10
11			0.05	0.07	0.10	0.10
12			0.05	0.06	1.10	1.20
11:05	.32	.35	.32	.35	.03	.04
11:10	.50	.54	.18	.19	.04	.04
11:15	.63	.68	.13	.14	.04	.04
11:20	.71	.77	.08	.09	.04	.04
11:25	.79	.86	.08	.09	.04	.04
11:30	.87	.95	.08	.09	.04	.05
11:35	.91	1.00	.04	.05	.08	.09
11:40	.95	1.04	.04	.04	.08	.09
11:45	.99	1.08	.04	.04	.08	.09
11:50	1.03	1.12	.04	.04	.13	.14
11:55	1.07	1.16	.04	.04	.18	.19
12:00	1.10	1.20	.03	.04	.32	.35

from chart on sh. 7

from Table: adjustment factors to obtain n-min estimate from 1-hr vol. sh. 9



Project UMTRA - Green River  
 Feature Hydrology  
 Item Flood frequency analysis

Contract No. 5257 Sheet 56  
 Designed JKL File No. \_\_\_\_\_  
 Checked HM Date 4/29/87  
 Date 2/16/87

Precipitation (inches)

10-yr

Hr.	Cumulative	Incremental	Incremental Sequence
			0.10
6	1.20	1.20	[ 1.20 ]
12	1.40	0.20	0.20
18	1.50	0.10	0.10
24	1.60	0.10	0.10
7		0.90	0.05
8	from chart on sh. 7	0.10	0.05
9		0.05	0.05
10		0.05	0.05
11		0.05	0.10
12		0.05	[ 0.90 ]
11:05	.26	.26	.02
11:10	.41	.15	.03
11:15	.51	.10	.03
11:20	.58	.07	.03
11:25	.65	.07	.04
11:30	.71	.06	.04
11:35	.75	.04	.06
11:40	.79	.04	.07
11:45	.82	.03	.07
11:50	.85	.03	.10
11:55	.88	.03	.15
12:00	.90	.02	.26

(P. 54)  
 SES curve  
 curve is to  
 to pick  
 peak hr.  
 between  
 11 and 12

from  
 Table:  
 adjustment  
 factors to  
 obtain n-10  
 estimates from  
 1-hr. values  
 Sh. 9







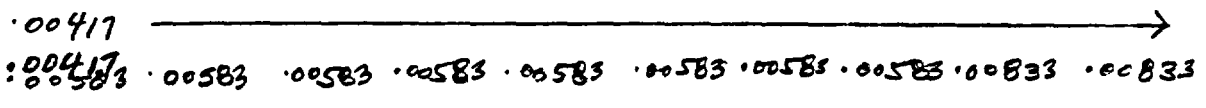
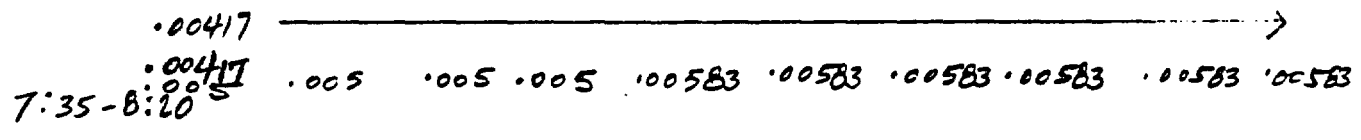
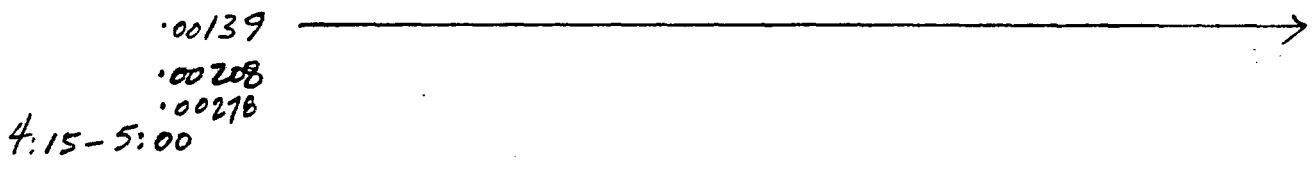
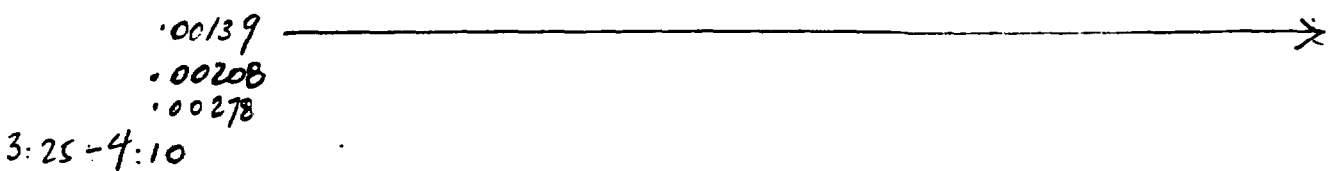
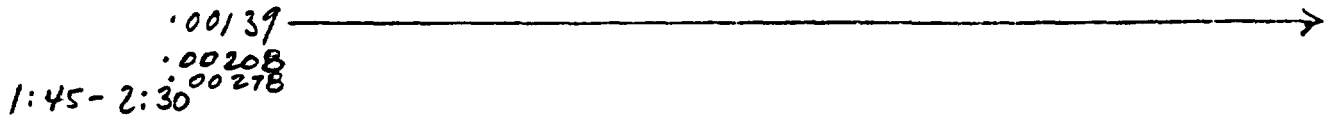
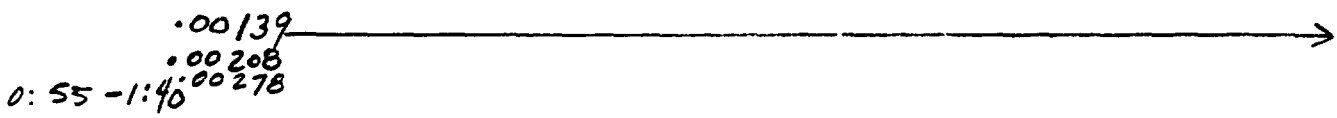
Project UMTRA - Green River  
Feature Hydrology  
Item Flood Frequency Analysis

Contract No. 5057  
Designed FK  
Checked HM  
File No. \_\_\_\_\_  
Date 4/30/87  
Date 7/16/87

$\Delta t = 5 \text{ min.}$

Precipitation distribution for 10-yr 24 hr.  
Precipitation distribution for 25-yr 24 hr.  
Precipitation distribution for 50-yr 24 hr.

0-0:50



Project UMTRA - Green River  
 Feature Hydrology  
 Item Flood Frequency Analysis

Contract No. 5057  
 Designed JTK  
 Checked HM  
 File No. \_\_\_\_\_  
 Date 4/30/87  
 Date 7/16/87

Precipitation distribution for 10-yr 24 hr.  $\Delta t = 5 \text{ min}$   
 Precipitation distribution for 25-yr 24 hr. (Continued)  
 Precipitation distribution for 50-yr 24 hr.

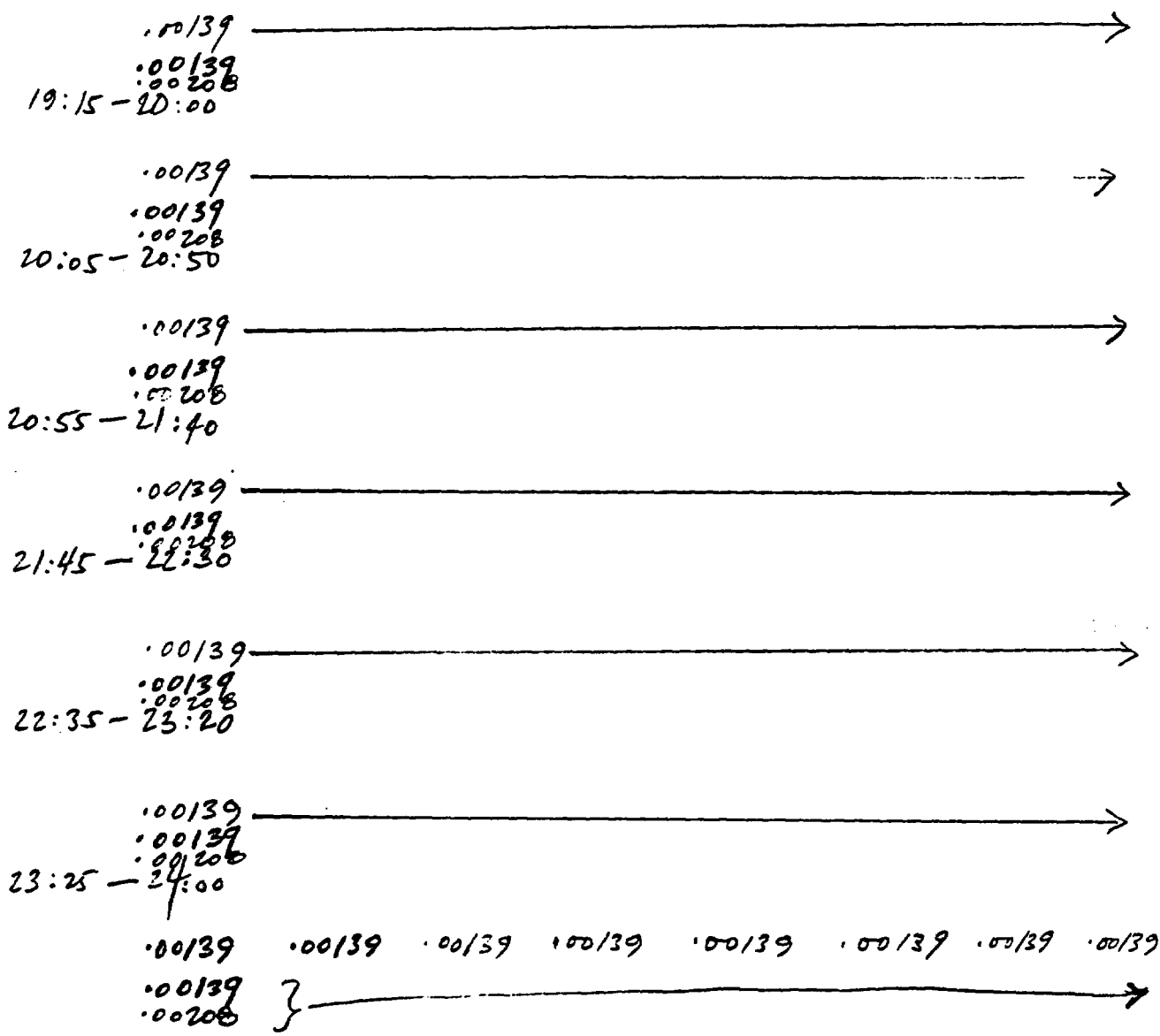
9:15 - 10:00	.00417									
10:05 - 10:50	.00417 .00833									
10:55 - 11:40	.00833 .00833 .00833									
11:45 - 12:30	.00833	.00833	.02	.03	.03	.03	.04	.04	.06	.07
	.00833 .00833	.00833	.03	.04	.04	.04	.04	.04	.08	.08
12:35 - 13:20	.07	.10	.15	.26	.00278					
	.08 .09	.13	.18	.32	.00417					
	.09	.14	.19	.35	.00417					
13:25 - 14:10	.00278 .00417 .00417									
14:15 - 15:00	.00278 .00417 .00417									
15:05 - 15:50	.00278 .00417 .00417									
15:55 - 16:40	.00278 .00417 .00417									
16:45 - 17:30	.00278 .00417 .00417									
17:35 - 18:20	.00278 .00417 .00417									
	.00278	.00278	.00278	.00278	.00278	.00278	.00139	.00139	.00139	.00139
	.00417	.00417	.00417	.00417	.00417	.00417	.00139	.00139	.00139	.00139



Project UMTRA - Green River  
 Feature Hydrology  
 Item Flood Frequency Analysis

Contract No. 5257 File No. \_\_\_\_\_  
 Designed JTK Date 4/20/87  
 Checked HM Date 7/10/87

Precipitation distribution for 10-yr 24 hr.  $\Delta t = 5 \text{ min}$   
 (continued)  
 Precipitation distribution for 25 yr 24 hr.  
 Precip. Dist. for 50 yr 24 hr.



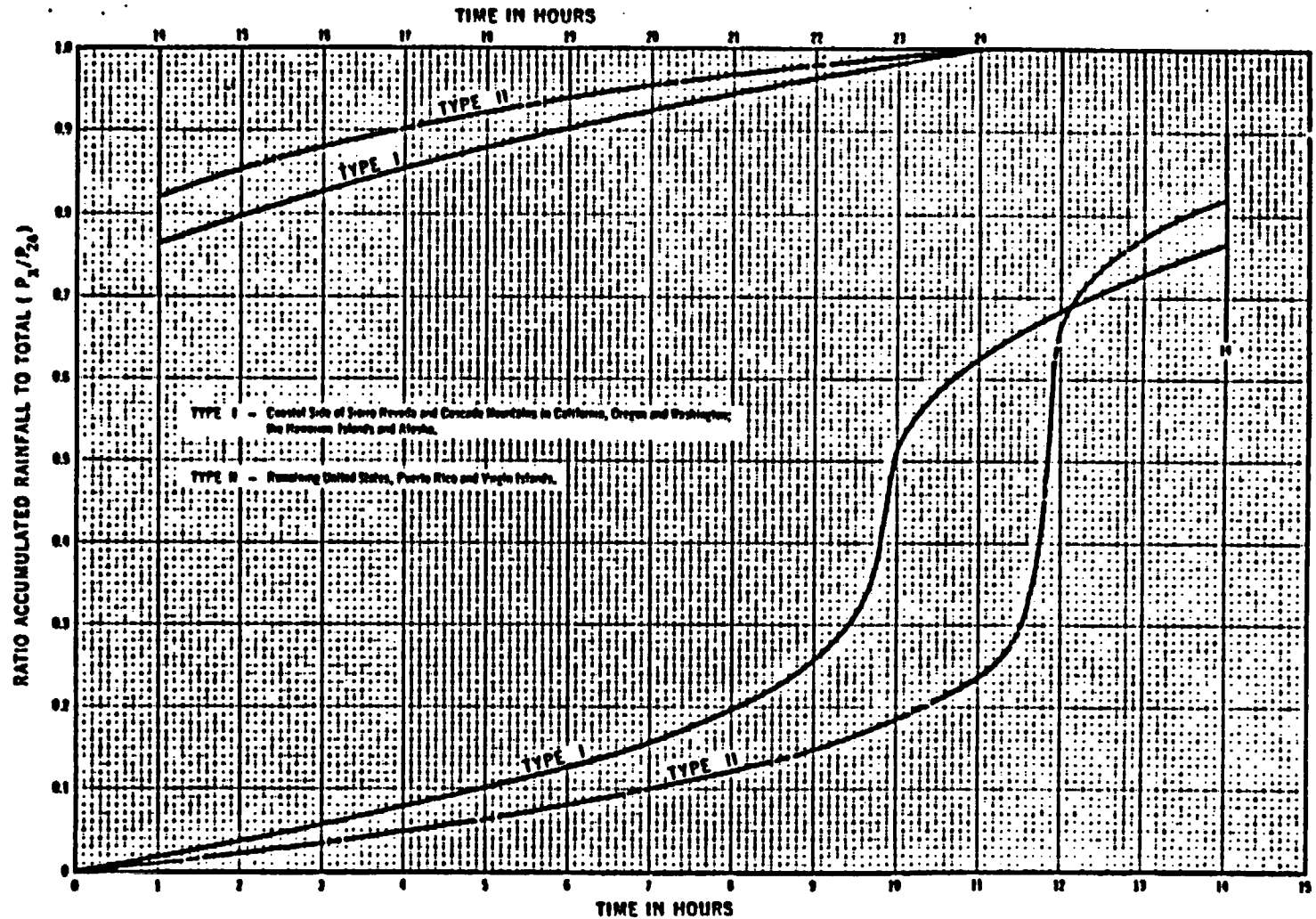
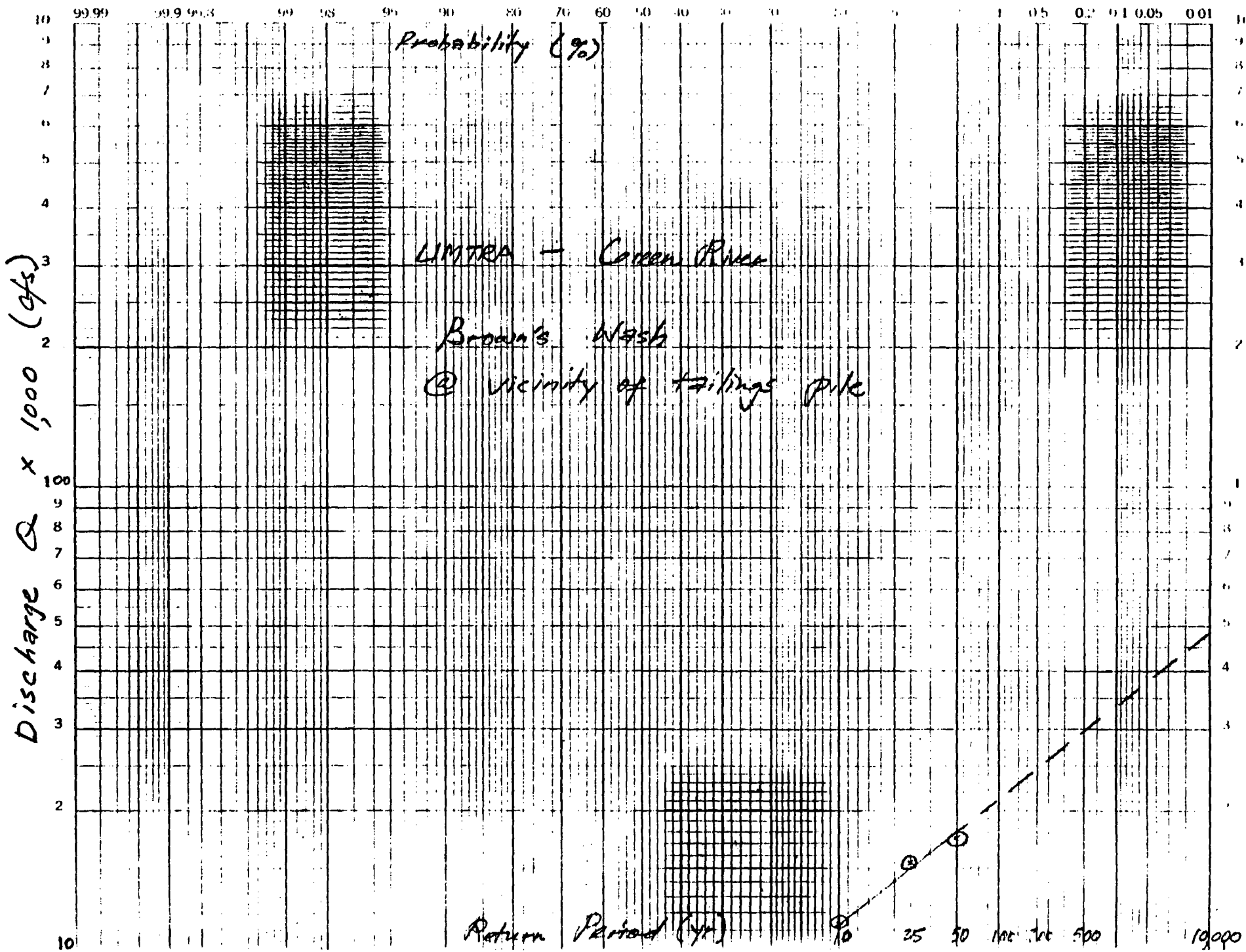


Figure 2. Twenty-four hour rainfall distributions (SCS).

McCuen R. H., "A Guide to Hydrologic Analysis using SCS Methods"  
Prentice - Hall, Inc. 1982.

Sheet 55



Probability (%)

LIMTRA - Carron River

Brown's Wash

@ vicinity of tailings pile

Discharge  $Q \times 1000$  (cfs)

Return Period (yr)

Sheet 59

Table 11. Equations for estimating 1-hr values in Utah with statistical parameters for each equation

Region of applicability*	Equation	Corr. coeff.	No. of stations	Mean of computed stn. values (inches)	Standard error of estimate (inches)
Utah south of the Unitas east of Wasatch, and east and south of Boulder and Pine Valley Mountains (1)	$Y_2 = -0.011 + 0.942[(X_1)(X_1/X_2)]$	0.95	86	0.72	0.085
	$Y_{100} = 0.494 + 0.755[(X_3)(X_3/X_4)]$	.90	85	1.96	.290
Most of western Utah (2)	$Y_2 = 0.005 + 0.852[(X_1)(X_1/X_2)]$	.89	65	0.41	.047
	$Y_{100} = 0.322 + 0.789[(X_3)(X_3/X_4)]$	.87	65	1.25	.196
Northeast and northwest corners of Utah (3)	$Y_2 = 0.019 + 0.711[(X_1)(X_1/X_2)]$ + 0.001Z	.82	98	0.40	.031
	$Y_{100} = 0.338 + 0.670[(X_3)(X_3/X_4)]$ + 0.001Z	.80	79	1.04	.141

\* Numbers in parentheses refer to geographic regions shown in figure 18. See text for more complete description.

List of variables

- $Y_2$  = 2-yr 1-hr estimated value
- $Y_{100}$  = 100-yr 1-hr estimated value
- $X_1$  = 2-yr 6-hr value from precipitation-frequency maps
- $X_2$  = 2-yr 24-hr value from precipitation-frequency maps
- $X_3$  = 100-yr 6-hr value from precipitation-frequency maps
- $X_4$  = 100-yr 24-hr value from precipitation-frequency maps
- Z = point elevation in hundreds of feet

Procedures for estimating 1-hr (60-min) precipitation-frequency values. Multiple-regression screening techniques were used to develop equations for estimating 1-hr values. Factors considered in the screening process were restricted to those that could be determined easily from the maps of this Atlas or from generally

the Wasatch Range, and east and south of the Boulder and Pine Valley Mountains (Region 1, fig. 18). The second region is most of western Utah and is labeled Region 2 on figure 18. Northeastern Utah north of the Unitas and the northwestern tip of Utah (Region 3, fig. 18) comprises the third region. Equations to provide estimates for the 1-hr duration for 2- and 100-yr return periods are shown in table 11. Also listed are the statistical parameters associated with each equation. In these equations, the variable  $[(X_1)(X_1/X_2)]$  or  $[(X_3)(X_3/X_4)]$  can be regarded as the 6-hr value times the slope of the line connecting the 6- and 24-hr values for the appropriate return period.

As with any separation into regions, the boundary can only be a function of a zone of transition between

Dr. 4/1/77  
 ref (2)  
 SH. 6  
 for 4/21/77

precipitation occurring within these months, but the investigations mentioned in the preceding paragraph indicate that these maps will approximate the values that would be obtained by using a data series made up of precipitation events that are exclusively rain. Since data for only part of the year were used, these maps have been labeled with the appropriate probabilities rather than with a return period in years (figs. 31-42).

- $Y_{100}$  = 100-yr 1-hr estimated value
- $X_1$  = 2-yr 6-hr value from precipitation-frequency
- $X_2$  = 2-yr 24-hr value from precipitation-frequency
- $X_3$  = 100-yr 6-hr value from precipitation-frequency
- $X_4$  = 100-yr 24-hr value from precipitation-frequency
- $Z$  = point elevation in hundreds of feet

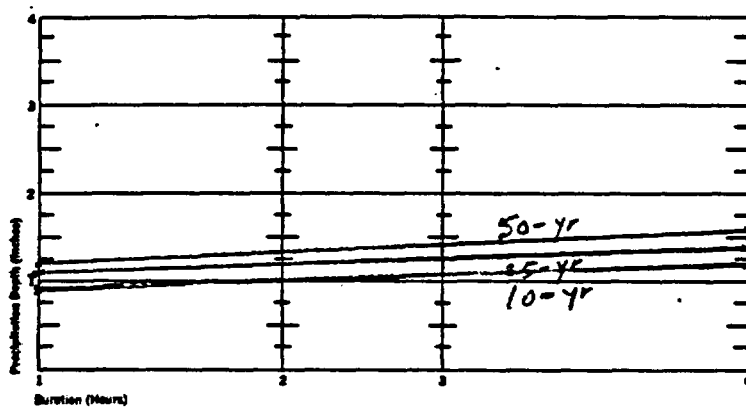
sh. 7

### Procedures for Estimating Values for Durations Other Than 6 and 24 Hrs

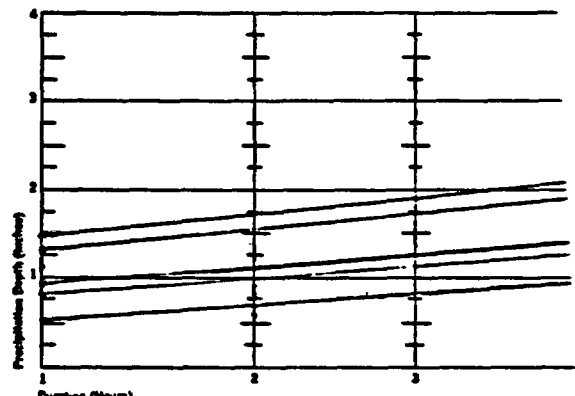
The isopluvial maps in this Atlas are for 6- and 24-hr durations. For many hydrologic purposes, values for other durations are necessary. Such values can be estimated using the 6- and 24-hr maps and the empirical methods outlined in the following sections. The procedures detailed below for obtaining 1-, 2-, and 3-hr estimates were developed specifically for this Atlas. The procedures for obtaining estimates for less than 1-hr duration and for 12-hr duration were adopted from *Weather Bureau Technical Paper No. 40* (U.S. Weather Bureau 1961) only after investigation demonstrated their applicability to data from the area covered by this Atlas.

Procedures for estimating 1-hr (60-minute) frequency values. Multiple-regression screening tests to develop equations for estimating 1-hr values in the screening process were restricted to those determined easily from the maps of this Atlas available topographic maps.

The 11 western states were separated into regions. The regions were chosen on the basis of climatological homogeneity and are general river basins separated by prominent divides. Topographic regions are partially within Utah. For use as an overlay on the precipitation-frequency regions are outlined in figure 18. The first region is that portion of the State south of the Unita Mountains.



(A)



(B)

Figure 15. Precipitation depth-duration diagram (1- to 6-hr).  
 a. Utah south of the Unita Mountains, east of the Wasatch Range, and east and south of the Boulder and Pine Valley Mountains. (Region 1, fig. 18).

b. Most of western Utah. (Region 2, fig. 18).

ref. (2)

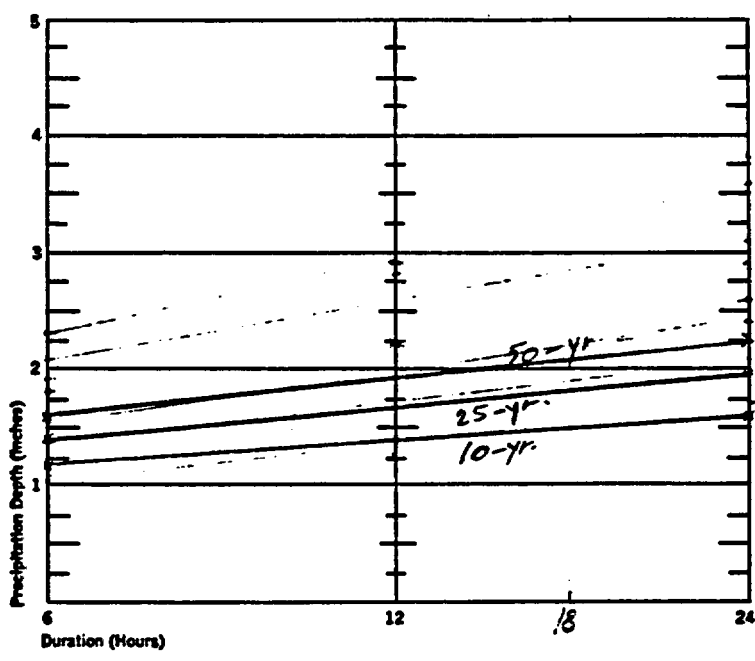
JFK 4/27 87  
 HM 6/12/87

Sk. 3

ref (2)

Figure 16. Precipitation depth-duration diagram (6- to 24-hr).

200 4/29/37  
 MW 5/1/37



**Illustration of Use Maps, Diagrams, &**

To illustrate the use figures 19 to 30 for the de These values are shown i read from the maps should of figure 6 because (1) n series of maps as are lab registration differences ir values in table 13 (fig. 17 subjectively. On this nor what above the line, so th (as shown by the strikeou adopted in preference to th

The 2- and 100-yr 1 from the equations applic The 2-yr 1-hr value is e: values from table 13); the (100-yr 6- and 24-hr valu values on figure 6 and co can obtain estimates for r

The 2- and 3-hr val gram of figure 15 or equa for the desired return pe points on the nomogram straight line. Read the esti of the connecting line an example is shown in figur: 100-yr 2-hr (1.82 in.) ar italics on table 13.

Estimates of 1-hr precipitation-frequency values for return periods between 2 and 100 yrs. The 1-hr values for the 2- and 100-yr return periods can be plotted on the nomogram of figure 6 to obtain values for return periods greater than 2 yrs or less than 100 yrs. Draw a straight line connecting the 2- and 100-yr values and read the desired return-period value from the nomogram.

Estimates for 2- and 3-hr (120- and 180-min) precipitation-frequency values. To obtain estimates of precipitation-frequency values for 2 or 3 hrs, plot the 1- and 6-hr values from the Atlas on the appropriate nomogram of figure 15. Draw a straight line connecting the 1- and 6-hr values, and read the 2- and 3-hr values from the nomogram. This nomogram is independent of return period. It was developed using data from the same regions used to develop the 1-hr equations.

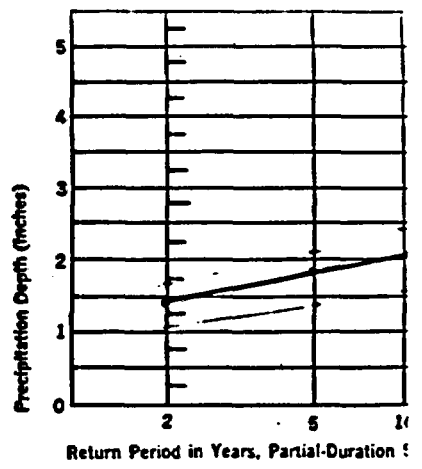
The mathematical solution from the data used to develop figure 15 gives the following equations for estimating the 2- and 3-hr values:

For Region 1,	2-hr = 0.341 (6-hr) + 0.659 (1-hr)	(3)
figure 18	3-hr = 0.569 (6-hr) + 0.431 (1-hr)	(4)
For Region 2,	2-hr = 0.299 (6-hr) + 0.701 (1-hr)	(5)



can obtain estimates for return periods of 5, 10, 25, and 50 yrs.

The 2- and 3-hr values can be estimated by using the nomogram of figure 15 or equations (3) and (4). The 1- and 6-hr values for the desired return period are obtained as above. Plot these points on the nomogram of figure 15 and connect them with a straight line. Read the estimates for 2 or 3 hrs at the intersections of the connecting line and the 2- and 3-hr vertical lines. An example is shown in figure 17b for the 100-yr return period. The 100-yr 2-hr (1.82 in.) and 100-yr 3-hr (1.95 in.) values are in italics on table 13.



ues for return  
- the 2- and  
10<sub>yr</sub> -m of figure 6  
2 yrs or less than  
and 100-yr values  
he nomogram.  
nin) precipitation-  
pitation-frequency  
es from the Atlas  
aw a straight line  
2- and 3-hr values  
endent of return  
ne regions used to

used to develop  
nating the 2- and

- 1.659 (1-hr) (3)
- 1.431 (1-hr) (4)
- 1.701 (1-hr) (5)
- 1.474 (1-hr) (6)
- 1.750 (1-hr) (7)
- 1.533 (1-hr) (8)

-frequency values.  
t values from the  
imates at the  
h the 12-hr

estimates for dura-  
le 12 to the 1-hr

	.29	.16	.12	
Duration (min)	5	10	15	30
Ratio to 1-hr	0.29	0.45	0.57	0.79

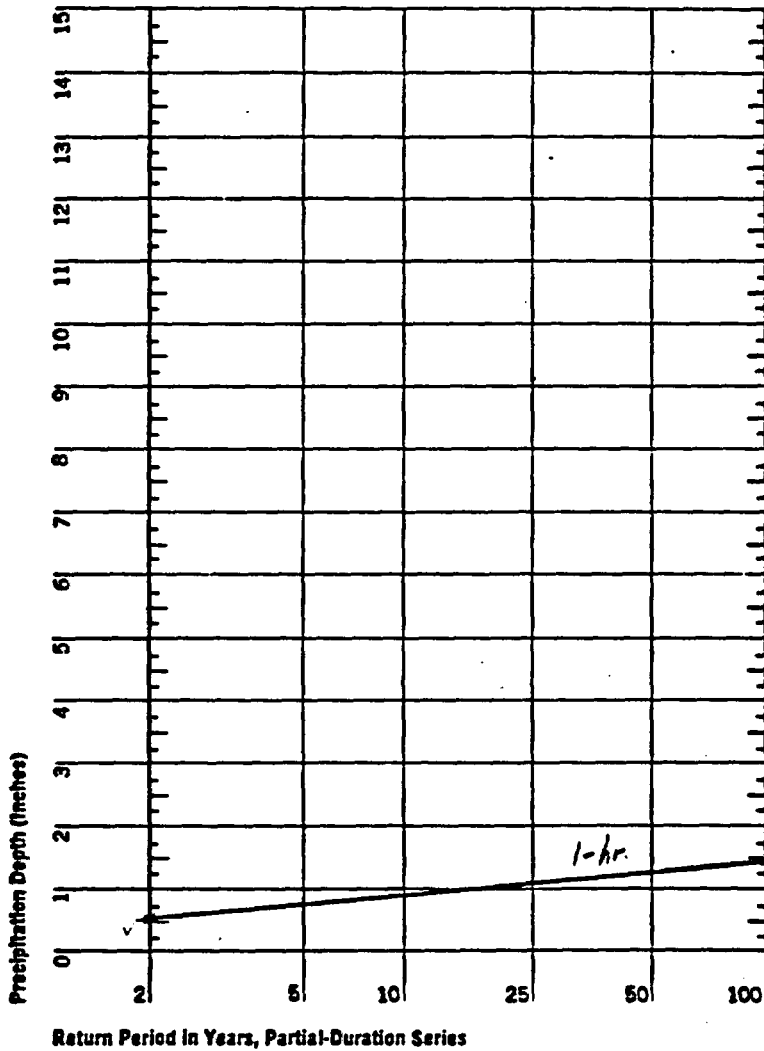
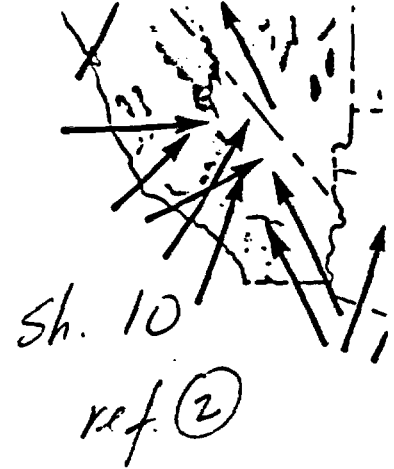
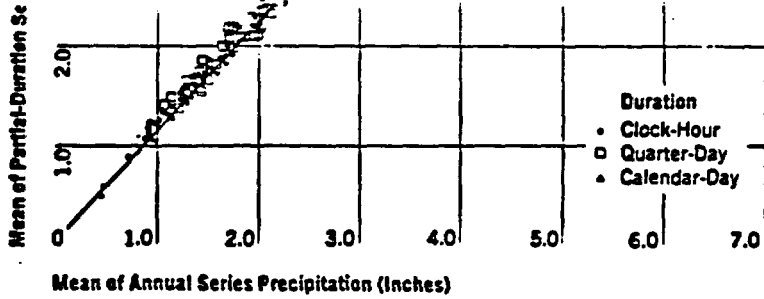
(Adopted from U.S. Weather Bureau Technical Paper No. 40, 1961.)

(A)  
Sh. 7  
ref. (2)  
JTK 4/27  
HM 6/18/87

	1-hr	2-hr
2-yr	0.65	
5-yr		
10-yr		
25-yr		
50-yr		
100-yr	1.63	1.82

Table 12. Adjustment factors to obtain n-min estimates from 1-hr values

Table 13. Precipitation data for computed for town of



portant. Next, an examination was made in the direction of topographic and meteorologic correlation to moisture sources. Each factor is a measure of some physical reality, and each is subject to variation in the precipitation-frequency relationship.

Finally, various climatologic factors were considered. The procedure used in the regression analysis was a multiple-regression analysis. The computer program was capable of handling a large number of independent variables for as many as 100. The number of variables screened was between 60 and 100. This does not mean that completely different factors could be screened. Some factors might involve different measures of slope might be over different orientations. In each instance, the computer selected the most critical factor.

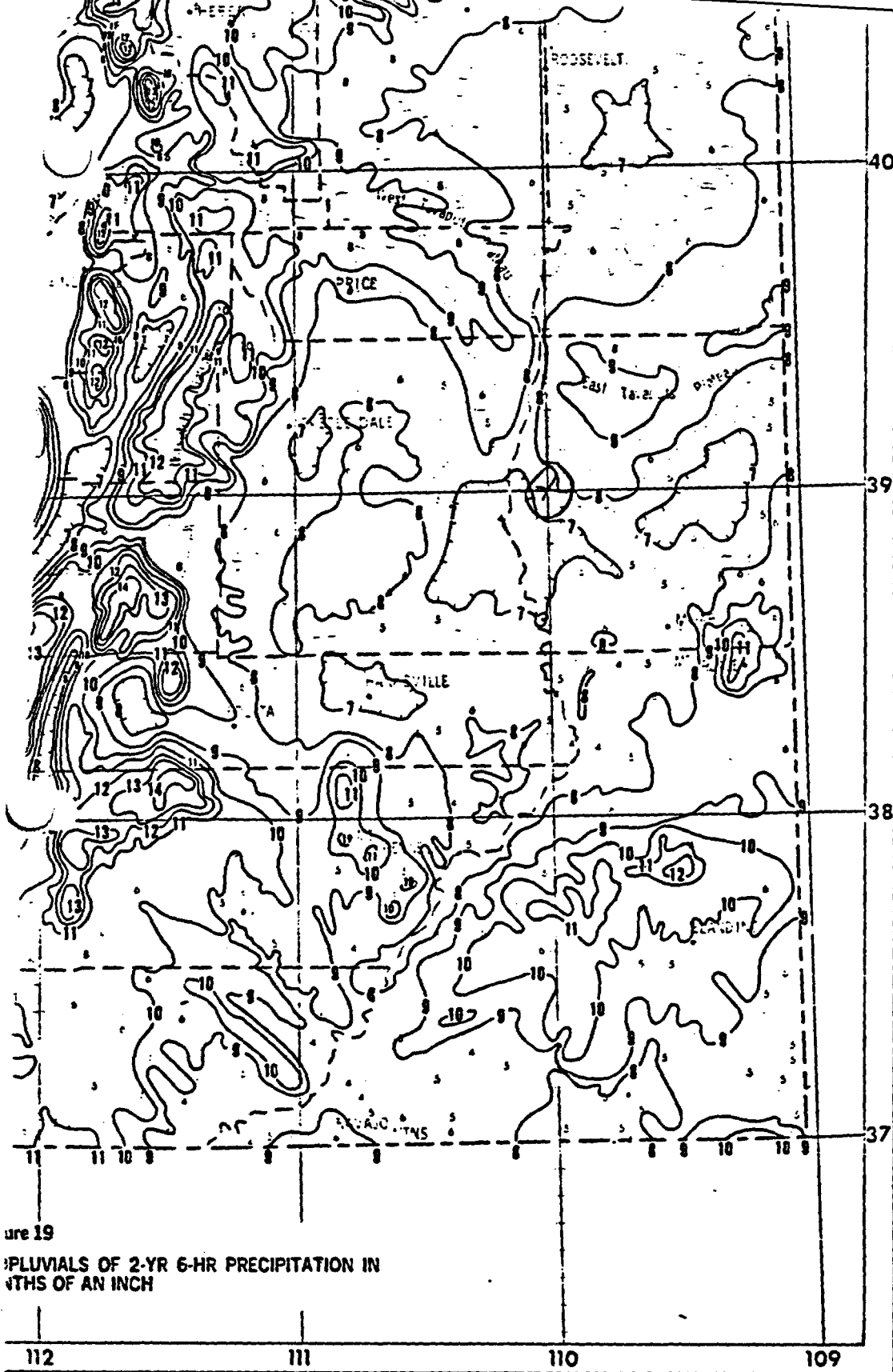
Although the computer program was used during the regression analysis, the results of the computations to use logarithms, combinations of any or all of the factors were selected. The single variable most highly correlated with the precipitation-frequency value under investigation was selected. The variable that, combined with the other factors, would explain the greatest variation in the precipitation-frequency values. The third, fourth, fifth, and sixth variables were selected in a similar manner. The

Figure 6. Precipitation depth versus return period for partial-duration series.

JFK

4/29/57

HM 6/18/87



Ch. 11  
ref. (2)

File  
4/29/35  
HM 6/18/87

PPT  
2-yr 6hr. = .75"  
✓

Figure 19  
ISOPLETHS OF 2-YR 6-HR PRECIPITATION IN  
TENTHS OF AN INCH

112                      111                      110                      109

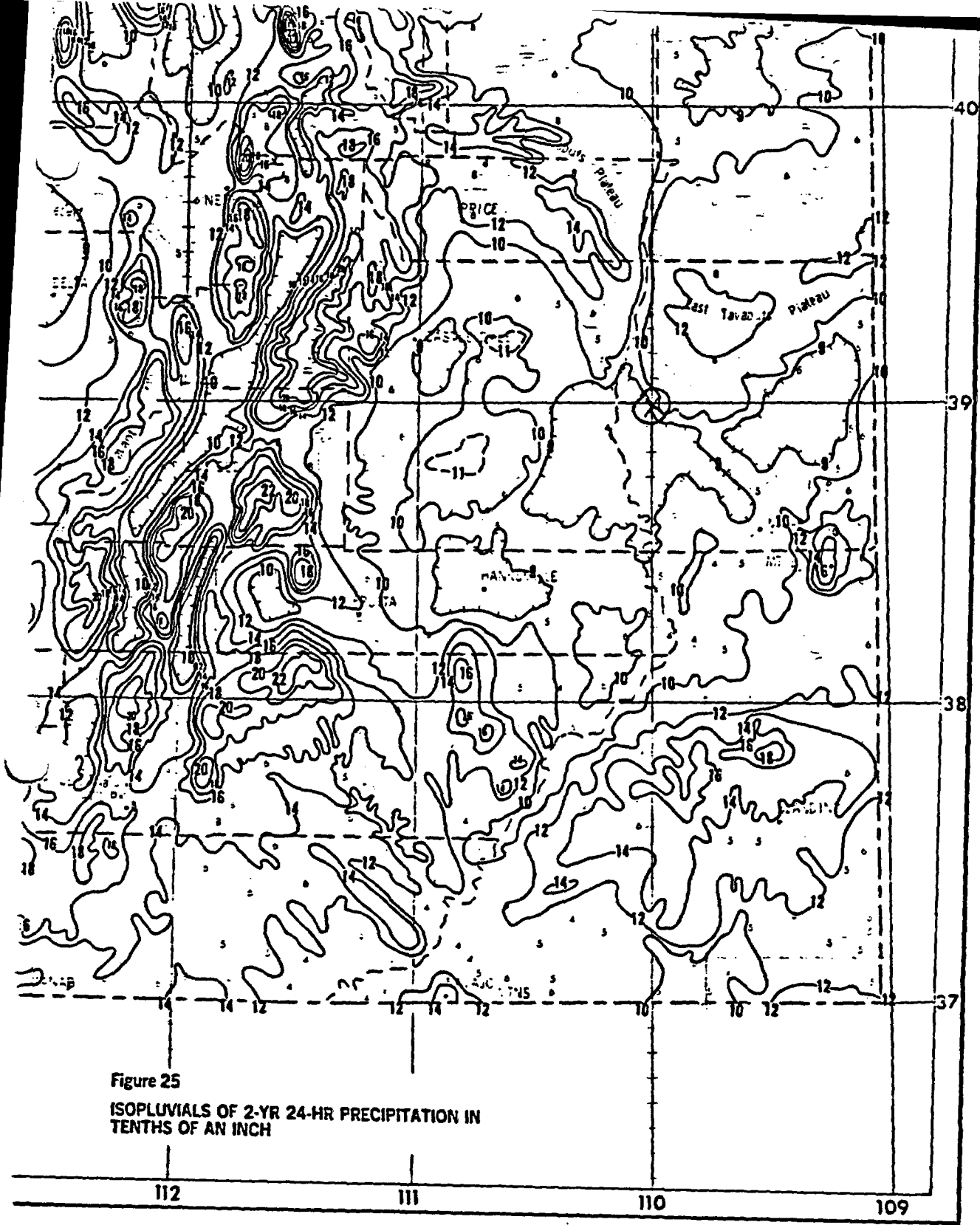
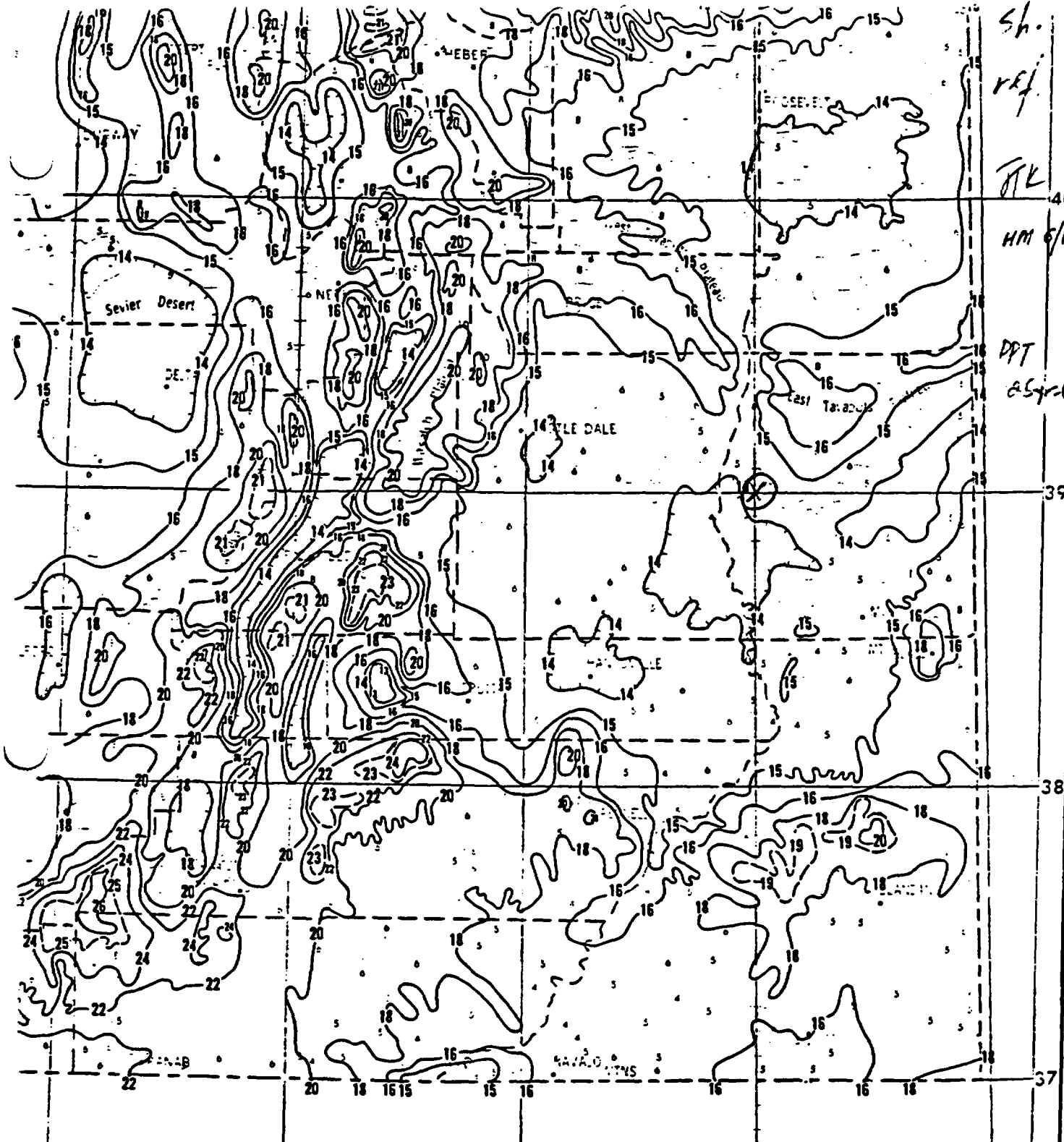


Figure 25  
 ISOPLUVIALS OF 2-YR 24-HR PRECIPITATION IN  
 TENTHS OF AN INCH

sh. 12  
 ref (2)

File  
 4/23/87  
 HM 6/18/87

PPT = .9  
 2-yr 24hr ✓



Sh. 13  
 ref. (2)  
 JK 4/29/87  
 HM 6/16/87  
 DPT = 1.1  
 & S. r. l. h. v

Figure 22  
 ISOPLUVIALS OF 25-YR 6-HR PRECIPITATION IN  
 TENTHS OF AN INCH

0 40  
 MILES

113 112 111 110 109  
 37 38 39 40

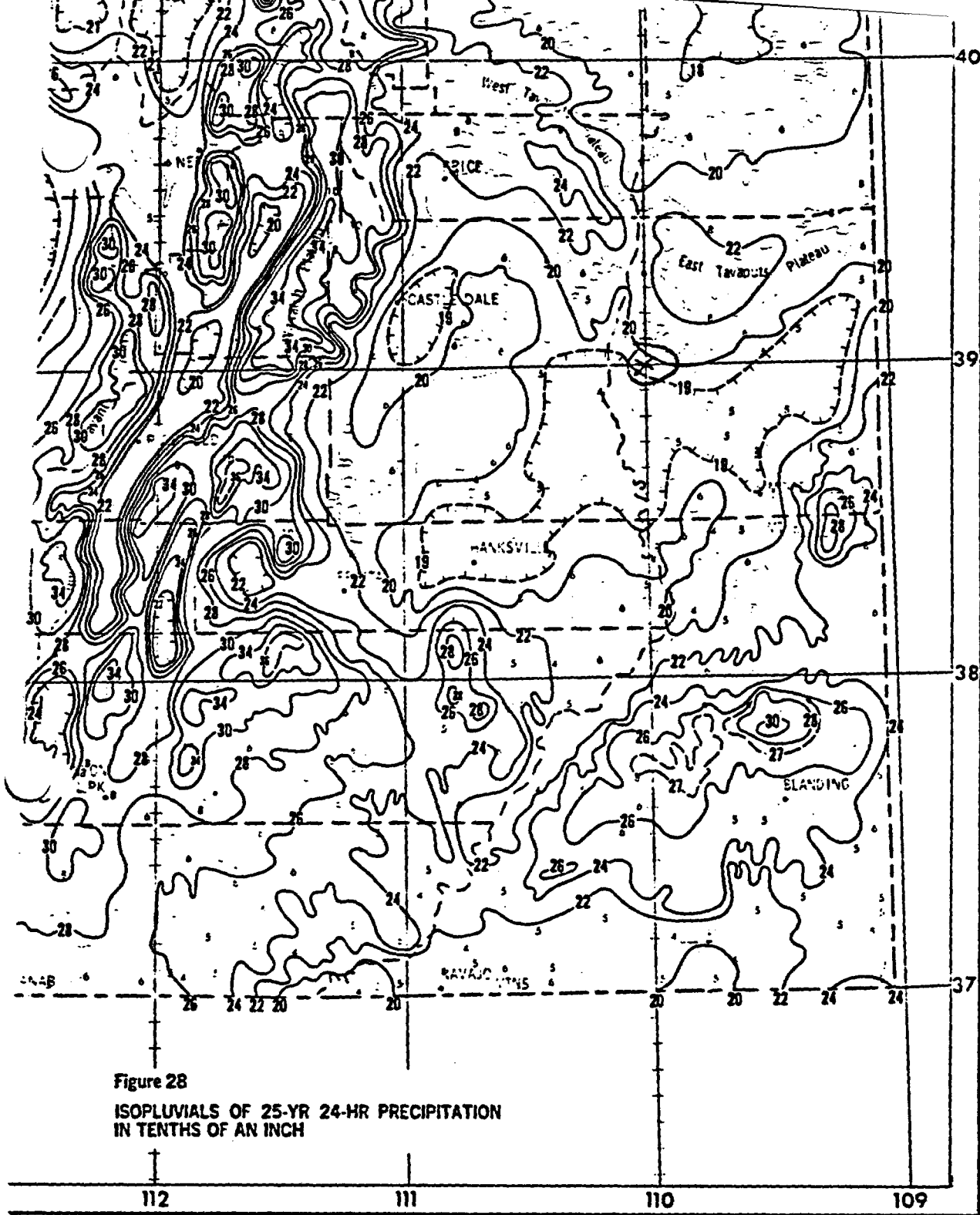


Figure 28  
 ISOPLUVIALS OF 25-YR 24-HR PRECIPITATION  
 IN TENTHS OF AN INCH

Sh. 14  
 ref. ②

JFK 4/29/87  
 HMB 5/12/87

PPT = 1.95"  
 25-yr 24hr ✓

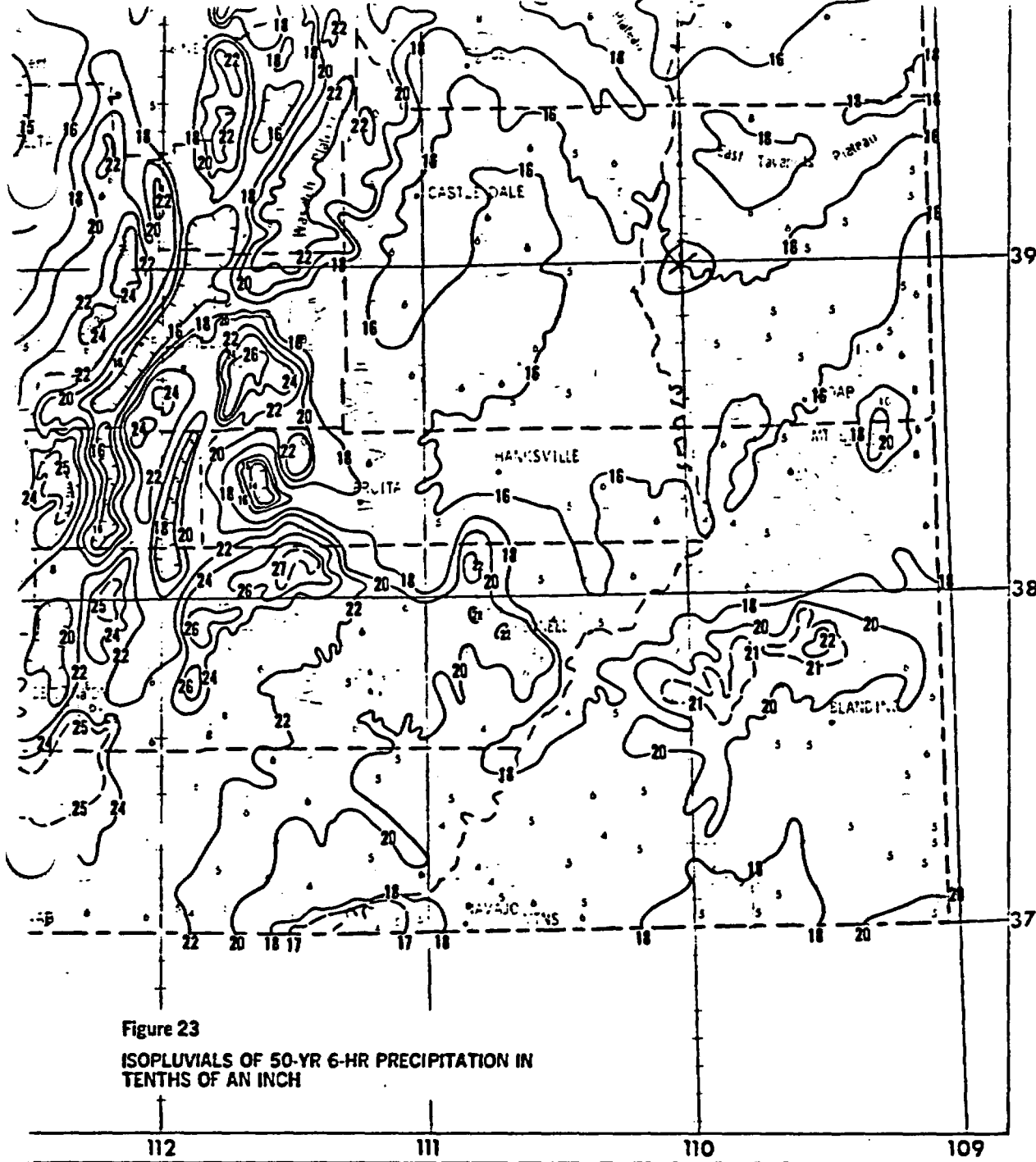


Figure 23  
 ISOPLUVIALS OF 50-YR 6-HR PRECIPITATION IN  
 TENTHS OF AN INCH

Sh. 15  
 ref (2)  
 JTK 9/29/1  
 HM 6/12/57  
 FST = 1.5"  
 50yr Sh. ✓

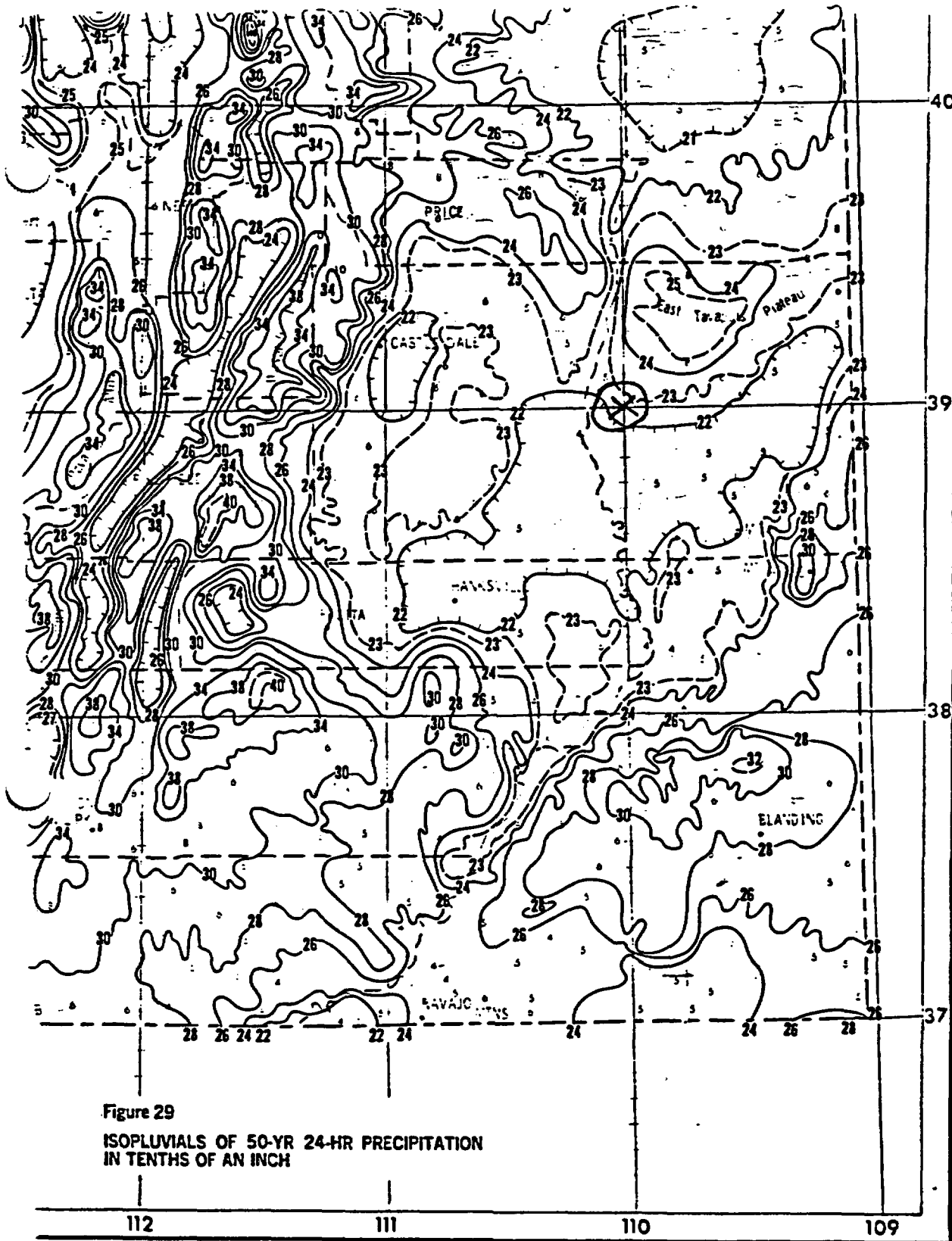


Figure 29  
 ISOPLUVIALS OF 50-YR 24-HR PRECIPITATION  
 IN TENTHS OF AN INCH

Sh. 16

ref. (2)

File 4/29/87

HM 6/18/87

PPT 50-yr 24hr = 2.2: ✓

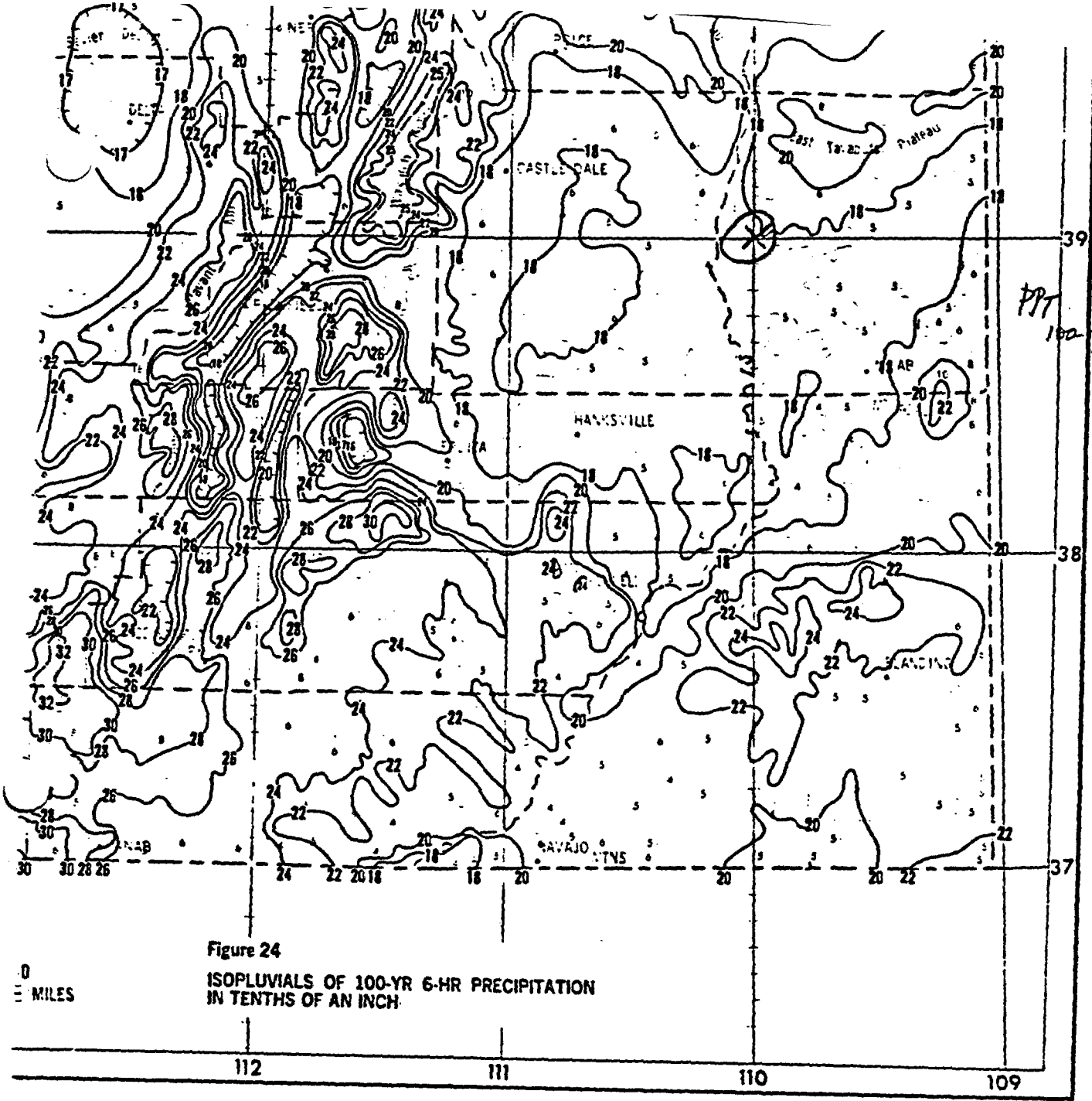
112

111

110

109





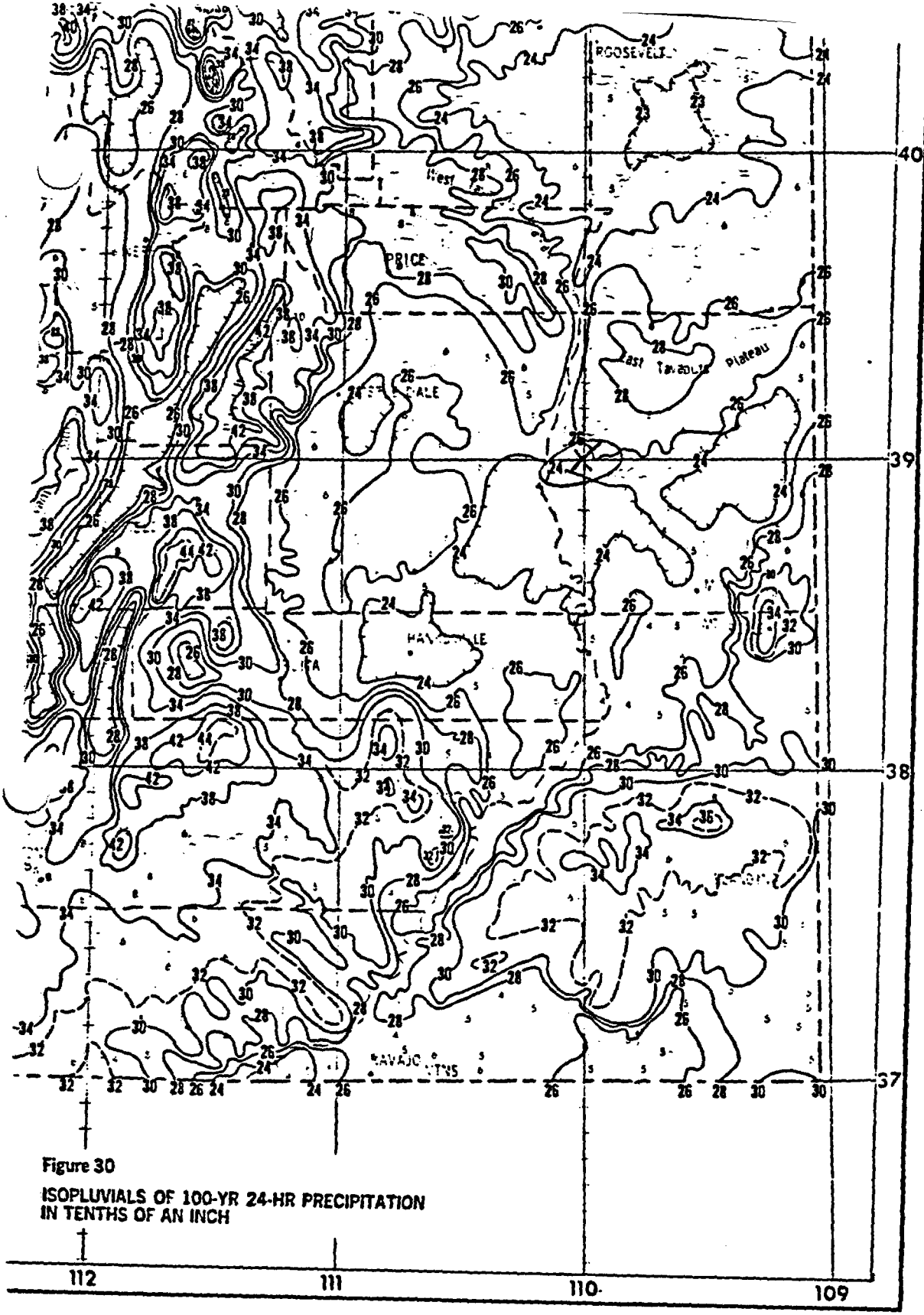
Sh. 17

ref. (2)

JFK 4/29/4  
 HMS 1/18/8

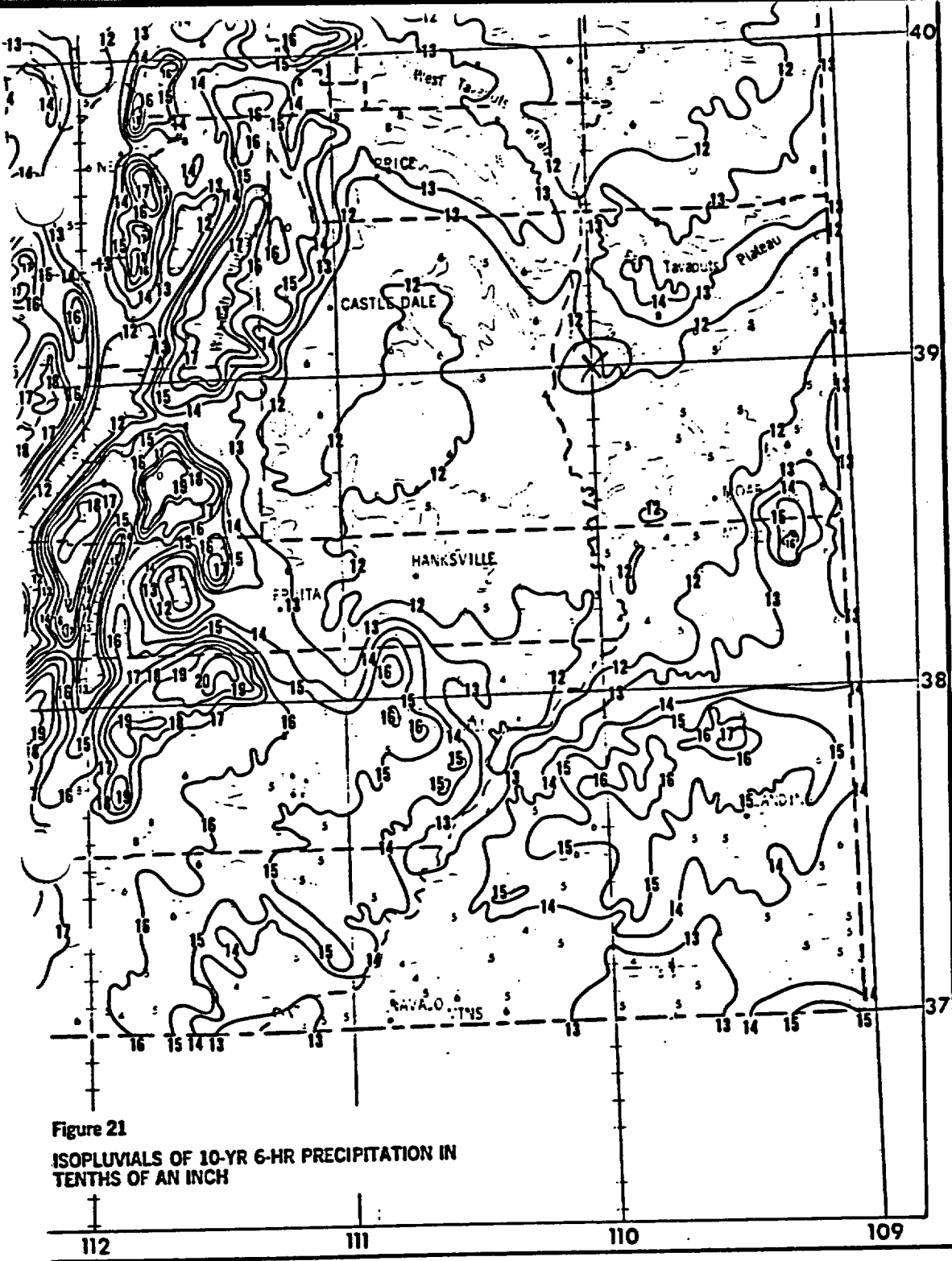
= 1.8"

PPT  
 100-yr 6-hr. ✓



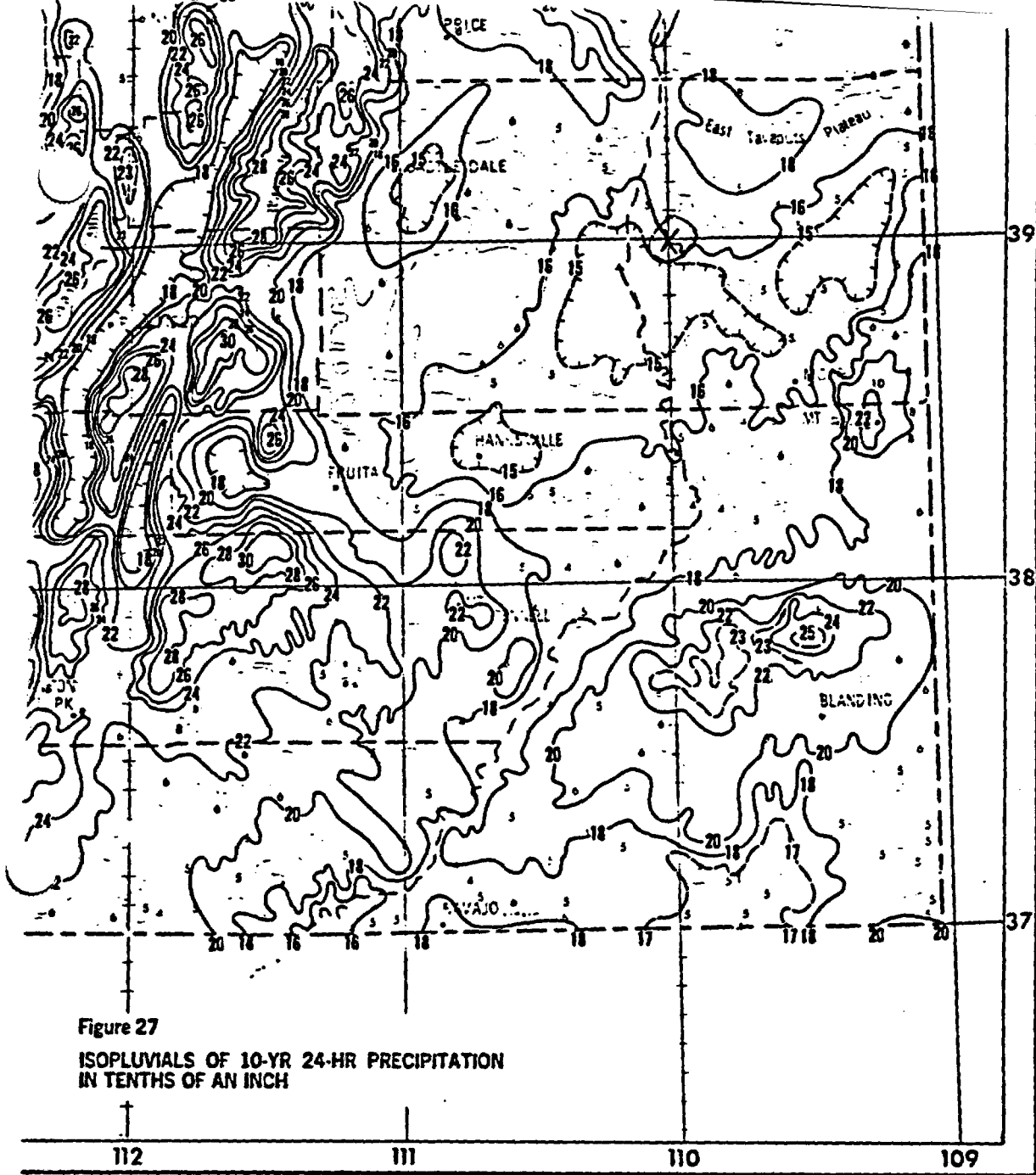
Sh. 18  
 ref (2)  
 FR 4/21/8  
 HM 6/18/8;  
 PPT<sub>100-yr. 24hr</sub> = 2.5 ✓

Figure 30  
 ISOPLUVIALS OF 100-YR 24-HR PRECIPITATION  
 IN TENTHS OF AN INCH



Sh: 19  
 ref. (2)  
 JTK 4/29/8  
 HM 6/18/8  
 PPT = 1.2"  
 10yr 6hr. ✓

**Figure 21**  
**ISOPLUVIALS OF 10-YR 6-HR PRECIPITATION IN**  
**TENTHS OF AN INCH**



Sh. 20 A  
 ref. (2)  
 JTK 4/29/87  
 PPT<sub>10 yr. 24hr</sub> = 1.6" ✓  
 HM 6/18/87

Figure 27  
 ISOPLUVIALS OF 10-YR 24-HR PRECIPITATION  
 IN TENTHS OF AN INCH

112                      111                      110                      109

Project UNTRA - GULL RIVER  
Feature Hydrology  
Item Flooding Potential on Browns Wash

Contract No. 5057  
Designed JTK  
Checked HM

Sheet 20 B  
File No. \_\_\_\_\_  
Date 4/30/87  
Date 7/16/87

Using the precipitation data derived on Sh. 52-5e, the same drainage model and time of concentration from MKE Calc. No. 10-539-02-00 on sheet 5

the peak discharges for the 10-yr and 25-yr 24 hr. storms are computed using the computer program HEC 1. The results of the computer runs are presented on Sh. 21A - 23B.

To perform a sensitivity analysis of the model, the times of concentration for the sub-basins 6, 7, 8 and 9 are adjusted (see Sh. 25) and the discharge for the 10-yr flood is recomputed (see Sh. 24A-24F)

As a result, the peak discharge became 10,900 cfs compared with the previous 11,300 cfs. Since the difference is insignificant, the more conservative 11,300 cfs. was used to derive the water surface profile at the site.

In addition, the flow length for routing the combined flow from Subbasins 7 and 8 to station 9 is actually 2,000 ft instead of 32,736 ft (used in earlier computer runs) (see Map, Sh. 25). Results using 2,000 ft are printed on Sh. 25B-<sup>5E</sup> indicating insignificant difference in the peak flow rate at the disposal sites. In all cases, <sup>storm</sup> 11,300 cfs will be a conservative value for the 10-yr; likewise for the 25-yr storm with estimated flow of 15,300 cfs.



Project UMTRA - Green River  
 Feature Hydrology  
 Item Flooding potential on Brown's Wash

Contract No. 5057  
 Designed JTK  
 Checked HM  
 Sheet 20C  
 File No. \_\_\_\_\_  
 Date 6/12/87  
 Date 7/14/87

Using peak discharges of 11,300 and 15,300 cfs for the 10-yr and 25-yr storms respectively, a water surface profile analysis was done using HEC2 at the vicinity of the site using the same cross sections as those in MKE Calc. No. 10-539-02-00.

In addition, New cross sections 0.6, 0.8, 6.5 and 6.8 are incorporated into the model to simulate flow through the upstream railroad crossing and the downstream culverts shown respectively on Sh. 19 of MKE Calc. No. 10-539-02-00. The geometry of the above new cross sections are shown on Sh. 26 and Sh. 29.

Results show that the water level for sections 5.5 and 6.0 will reach approx. 4077', thus will inundate the downstream side of the existing pile end in the area where the retention basin will be located (See Sh. 32 and 33). Therefore, a berm is proposed to be built to elevation 4080' as indicated on Sh. 19 MKE Calc. No. 10-539-02-00, to keep the floodwater out. The HEC2 runs were repeated assuming the existence of the berm at sections 5.5 and 6.0. Results of the analysis are shown on Sh. 34 and 35 and the water surface profiles are plotted on Sh. 30 and 31.



Project UMTRA - Caddo River  
 Feature Hydrology  
 Item Flooding potential on Brown's Wash

Contract No. 5757  
 Designed JTK  
 Checked HM

Sheet 20D  
 File No. \_\_\_\_\_  
 Date 6/12/87  
 Date 7/16/87

It was shown, by building a berm to elevation 4080', that the maximum water level during the peak 10-yr and 25-yr storms will be retained in the main channel of Brown's Wash with a residual freeboard of about 2 feet.





44 LU 0 ✓ 0.2 ✓  
 45 UD 0.73 ✓  
 46 KK ST12 COMBINE BAS. 1&2 FLOWS ✓  
 47 HC 2 ✓

Sh. 21B

HEC-1 INPUT

PAGE 2 JTK 4/30/07  
 HM 7/18/07

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

48 KK 3,4 FLOW 1,2 FROM STA.1,2 TO 3,4  
 49 RK 2E400 .032 ✓ .04 ✓ TRAP 0 0.45  
 50 KK BAS4 ✓  
 51 KM 10YR 24HR ✓  
 52 BA 6.4 ✓  
 53 LU 0 ✓ 0.2 ✓  
 54 UD 0.75  
 55 KK BAS3 ✓  
 56 KM 10YR 24HR ✓  
 57 BA 12.1 ✓  
 58 LU 0 ✓ 0.2 ✓  
 59 UD .96 ✓  
 60 KK ST34 COMBINE FLOWS 3,4  
 61 HC 3 ✓  
 62 KK 5,6 FLOW 3,4 FROM STA.3,4 TO 5,6  
 63 RK 53856 .015 ✓ .04 ✓ TRAP 0 0.03  
 64 KK BAS5 ✓  
 65 KM 10YR 24HR  
 66 BA 20.7 ✓  
 67 LU 0 ✓ 0.2 ✓  
 68 UD 1.73  
 69 KK BAS6 ✓  
 70 KM 10YR 24HR ✓  
 71 BA 11.8 ✓  
 72 LU 0 ✓ 0.2 ✓  
 73 UD 0.95  
 74 KK ST56 ✓ COMBINE FLOWS 5,6 ✓  
 75 HC 3 ✓  
 76 KK 7,8 FLOW 5,6 FROM STA.5,6 TO 7,8  
 77 RK 6336 0.005 .04 ✓ TRAP 0 0.025  
 78 KK BAS8  
 79 KM 10YR 24HR  
 80 BA 0.5 ✓  
 81 LU 0 0.2 ✓  
 82 UD 0.52  
 83 KK BAS7  
 84 KM 10YR 24HR  
 85 BA 12.2 ✓  
 86 LU 0 0.2 ✓  
 87 UD 1.22

HEC-1 INPUT

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

88 KK ST78 COMBINE FLOWS 7,8  
 89 HC 3 ✓

88 KK ST78 COMBINE FLOWS 7,8  
 89 HC 3 ✓  
 90 KK 9 FLOWS 7,8 FROM STA. 7,8 TO 9  
 91 RK 32735 0.01 .04 TRAP 0 0.05  
 92 KK BAS9  
 93 KM 10YR 24HR  
 94 BA 11.3 ✓  
 95 LU 0 0.2 ✓  
 96 UD 1.39 ✓  
 97 KK ST9 COMBINE FLOWS  
 98 HC 2 ✓  
 99 ZZ

Sh. 21C  
 JTK 4/30/87  
 HM 7/16/87

1  
 \*\*\*\*  
 FLOOD HYDROGRAPH PACKAGE HEC-1 (IBM XT 512K VERSION) -FEB 1, 1985  
 U.S. ARMY CORPS OF ENGINEERS, THE HYDROLOGIC ENGINEERING CENTER, 609 SECOND STREET, DAVIS, CA. 95616  
 \*\*\*\*

UMTRA - GREEN RIVER - BROWN WASH  
 10 - YR 24-HR STORM

5 10 OUTPUT CONTROL VARIABLES  
 IPRINT 5 PRINT CONTROL  
 IPLOT 0 PLOT CONTROL  
 OSCAL 0. HYDROGRAPH PLOT SCALE

17 HYDROGRAPH TIME DATA  
 NMIN 5 MINUTES IN COMPUTATION INTERVAL  
 IDATE 1 0 STARTING DATE  
 ITIME 0000 STARTING TIME  
 N2 300 NUMBER OF HYDROGRAPH ORDINATES  
 NDDATE 2 0 ENDING DATE  
 NDTIME 0055 ENDING TIME  
 COMPUTATION INTERVAL .08 HOURS  
 TOTAL TIME BASE 24.92 HOURS

1 ENGLISH UNITS

RUNOFF SUMMARY  
 FLOW IN CUBIC FEET PER SECOND  
 TIME IN HOURS, AREA IN SQUARE MILES

OPERATION	STATION	PEAK FLOW	TIME OF PEAK	AVERAGE FLOW FOR MAXIMUM PERIOD			BASIN AREA	MAXIMUM STAGE	TIME OF MAX STAGE
				6-HOUR	24-HOUR	72-HOUR			
+	HYDROGRAPH AT								
+		BAS1	1100.	12.50	196.	49.	47.	2.60	
+	HYDROGRAPH AT								
+		BAS2	2151.	12.58	414.	103.	100.	5.50	
	2 COMBINED AT								
		ST12	3234.	12.50	610.	152.	147.	8.10	
	ROUTED TO								
+		3,4	2963.	12.83	609.	153.	147.	8.10	
+	HYDROGRAPH AT								
		BAS4	2456.	12.58	482.	120.	116.	6.40	

+	HYDROGRAPH AT	BAS3	3799.	12.75	911.	228.	219.	12.10
+	3 COMBINED AT	ST34	9028.	12.75	2001.	501.	482.	25.60
	ROUTED TO	5,6	6387.	14.17	1958.	501.	483.	25.60
+	HYDROGRAPH AT	BAS5	3857.	13.50	1535.	389.	375.	20.70
+	HYDROGRAPH AT	BAS6	3738.	12.75	888.	222.	214.	11.80
+	3 COMBINED AT	ST56	10307.	14.00	4312.	1113.	1072.	59.10
+	ROUTED TO	7,8	10213.	14.17	4295.	1112.	1071.	59.10
+	HYDROGRAPH AT	BAS8	250.	12.33	38.	9.	9.	.50
+	HYDROGRAPH AT	BAS7	3117.	13.00	917.	230.	221.	12.20
+	3 COMBINED AT	ST78	11283.	14.17	5226.	1351.	1301.	71.80
+	ROUTED TO	9	10640.	14.75	5119.	1346.	1297.	71.80
+	HYDROGRAPH AT	BAS9	2571.	13.17	847.	213.	205.	11.30
+	2 COMBINED AT	ST9	11314.	14.67	5838.	1559.	1502.	83.10

Sh. 21 D

JK 4/30/8  
HM 7/16/07

\*\*\* NORMAL END OF HEC-1 \*\*\*

\*\*\*\*  
 FLOOD HYDROGRAPH PACKAGE HEC-1 (IBM XT 512K VERSION) -FEB 1, 1985  
 U.S. ARMY CORPS OF ENGINEERS, THE HYDROLOGIC ENGINEERING CENTER, 609 SECOND STREET, DAVIS, CA. 95616  
 \*\*\*\*

*UMTRA - Green River*

*Sh. 22 A*

THIS HEC-1 VERSION CONTAINS ALL OPTIONS EXCEPT ECONOMICS, AND THE NUMBER OF PLANS ARE REDUCED TO 3

*JFK 4/30/87*  
*HAI 7/12/87*

1

HEC-1 INPUT

PAGE 1

LINE	ID	1	2	3	4	5	6	7	8	9	10
1	ID	UMTRA - GREEN RIVER - BROWN WASH									
2	ID	25 - YR 24-HR STORM									
3	IT	5			300						
4	IN	5									
5	IO	5									
6	KK	BAS1 SUB-BASIN 1									
7	KM	25-YR 24-HR									
8	BA	2.6									
9	PB	1.95									
10	PI	.00208	.00208	.00208	.00208	.00208	.00208	.00208	.00208	.00208	.00208
11	PI	.00208	.00208	.00208	.00208	.00208	.00208	.00208	.00208	.00208	.00208
12	PI	.00208	.00208	.00208	.00208	.00208	.00208	.00208	.00208	.00208	.00208
13	PI	.00208	.00208	.00208	.00208	.00208	.00208	.00208	.00208	.00208	.00208
14	PI	.00208	.00208	.00208	.00208	.00208	.00208	.00208	.00208	.00208	.00208
15	PI	.00208	.00208	.00208	.00208	.00208	.00208	.00208	.00208	.00208	.00208
16	PI	.00208	.00208	.00208	.00208	.00208	.00208	.00208	.00208	.00208	.00208
17	PI	.00208	.00208	.00417	.00417	.00417	.00417	.00417	.00417	.00417	.00417
18	PI	.00417	.00417	.00417	.00417	.00417	.00417	.00417	.00417	.00417	.00417
19	PI	.00417	.00417	.00417	.00417	.00417	.00417	.00417	.00417	.00417	.00417
20	PI	.00417	.00417	.00417	.00417	.00417	.00417	.00417	.00417	.00417	.00417
21	PI	.00417	.00417	.00417	.00417	.00417	.00417	.00417	.00417	.00417	.00417
22	PI	.00833	.00833	.00833	.00833	.00833	.00833	.00833	.00833	.00833	.00833
23	PI	.00833	.00833	.03	.04	.04	.04	.04	.04	.08	.08
24	PI	.08	.13	.18	.32	.00417	.00417	.00417	.00417	.00417	.00417
25	PI	.00417	.00417	.00417	.00417	.00417	.00417	.00417	.00417	.00417	.00417
26	PI	.00417	.00417	.00417	.00417	.00417	.00417	.00417	.00417	.00417	.00417
27	PI	.00417	.00417	.00417	.00417	.00417	.00417	.00417	.00417	.00417	.00417
28	PI	.00417	.00417	.00417	.00417	.00417	.00417	.00417	.00417	.00417	.00417
29	PI	.00417	.00417	.00417	.00417	.00417	.00417	.00417	.00417	.00417	.00417
30	PI	.00417	.00417	.00417	.00417	.00417	.00417	.00417	.00417	.00417	.00417
31	PI	.00417	.00417	.00417	.00417	.00417	.00417	.00139	.00139	.00139	.00139
32	PI	.00139	.00139	.00139	.00139	.00139	.00139	.00139	.00139	.00139	.00139
33	PI	.00139	.00139	.00139	.00139	.00139	.00139	.00139	.00139	.00139	.00139
34	PI	.00139	.00139	.00139	.00139	.00139	.00139	.00139	.00139	.00139	.00139
35	PI	.00139	.00139	.00139	.00139	.00139	.00139	.00139	.00139	.00139	.00139
36	PI	.00139	.00139	.00139	.00139	.00139	.00139	.00139	.00139	.00139	.00139
37	PI	.00139	.00139	.00139	.00139	.00139	.00139	.00139	.00139	.00139	.00139
38	PI	.00139	.00139	.00139	.00139	.00139	.00139	.00139	.00139	.00139	.00139
39	LU	0	0.2								
40	LD	.66									
41	KK	BAS2									
42	KM	25YR 24HR									
43	BA	5.5									

44 LU 0 0.2  
 45 UD 0.73  
 46 KK ST12 COMBINE BAS. 1&2 FLOWS  
 47 HC 2

HEC-1 INPUT

Sh. 22 B

JFK 4' 197  
 HM 7/15/20

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

48 KK 3,4 FLOW 1,2 FROM STA. 1,2 TO 3,4  
 49 RK 26400 .032 .04 TRAP 0 0.45

50 KK BAS4  
 51 KM 25YR 24HR  
 52 BA 5.4  
 53 LU 0 0.2  
 54 UD 0.75

55 KK BAS3  
 56 KM 25YR 24HR  
 57 BA 12.1  
 58 LU 0 0.2  
 59 UD .95

60 KK ST34 COMBINE FLOWS 3,4  
 61 HC 3

62 KK 5,6 FLOW 3,4 FROM STA. 3,4 TO 5,6  
 63 RK 53856 .015 .04 TRAP 0 0.03

64 KK BAS5  
 65 KM 25YR 24HR  
 66 BA 20.7  
 67 LU 0 0.2  
 68 UD 1.73

69 KK BAS6  
 70 KM 25YR 24HR  
 71 BA 11.8  
 72 LU 0 0.2  
 73 UD 0.95

74 KK ST56 COMBINE FLOWS 5,6  
 75 HC 3

76 KK 7,8 FLOW 5,6 FROM STA. 5,6 TO 7,8  
 77 RK 6336 0.005 .04 TRAP 0 0.025

78 KK BAS8  
 79 KM 25YR 24HR  
 80 BA 0.5  
 81 LU 0 0.2  
 82 UD 0.52

83 KK BAS7  
 84 KM 25YR 24HR  
 85 BA 12.2  
 86 LU 0 0.2  
 87 UD 1.22

HEC-1 INPUT

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

88 KK ST78 COMBINE FLOWS 7,8  
 89 HC 3

88 KK ST78 COMBINE FLOWS 7,8  
 89 HC 3

90 KK 9 FLOWS 7,8 FROM STA.7,8 TO 9  
 91 RK 32736 0.01 .04 TRAP 0 0.05

92 KK BAS9  
 93 KM 25YR 24HR  
 94 BA 11.3  
 95 LU 0 0.2  
 96 UD 1.39

97 KK ST9 COMBINE FLOWS  
 98 HC 2  
 99 ZZ

Sh. 22 C

JTK 4/30/87  
 HM 7/1.. 7

1

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 FLOOD HYDROGRAPH PACKAGE MEC-1 (IBM XT 512K VERSION) -FEB 1,1985  
 U.S. ARMY CORPS OF ENGINEERS, THE HYDROLOGIC ENGINEERING CENTER, 609 SECOND STREET, DAVIS, CA. 95616  
 \*\*\*\*

UNTRA - GREEN RIVER - BROWN WASH  
 25 - YR 24-HR STORM

5 IO OUTPUT CONTROL VARIABLES  
 IPRNT 5 PRINT CONTROL  
 IPLOT 0 PLOT CONTROL  
 QSCAL 0. HYDROGRAPH PLOT SCALE

IT HYDROGRAPH TIME DATA  
 NMIN 5 MINUTES IN COMPUTATION INTERVAL  
 IDATE 1 0 STARTING DATE  
 ITIME 0000 STARTING TIME  
 NI 300 NUMBER OF HYDROGRAPH ORDINATES  
 NDATE 2 0 ENDING DATE  
 NDTIME 0055 ENDING TIME

COMPUTATION INTERVAL .08 HOURS  
 TOTAL TIME BASE 24.92 HOURS

ENGLISH UNITS

1

RUNOFF SUMMARY  
 FLOW IN CUBIC FEET PER SECOND  
 TIME IN HOURS, AREA IN SQUARE MILES

OPERATION	STATION	PEAK FLOW	TIME OF PEAK	AVERAGE FLOW FOR MAXIMUM PERIOD			BASIN AREA	MAXIMUM STAGE	TIME OF MAX STAGE
				6-HOUR	24-HOUR	72-HOUR			
+									
+	HYDROGRAPH AT								
	BAS1	1391.	12.50	252.	63.	61.	2.60		
+	HYDROGRAPH AT								
	BAS2	2720.	12.58	532.	133.	128.	5.50		
+	2 COMBINED AT								
	ST12	4893.	12.58	784.	196.	189.	8.10		
+	ROUTED TO								
	3,4	3818.	12.75	783.	196.	189.	8.10		
+	HYDROGRAPH AT								
	BAS4	3107.	12.58	619.	155.	149.	6.40		

+	HYDROGRAPH AT	BAS3	4827.	12.75	1171.	293.	282.	12.10
	3 COMBINED AT							
+		ST34	11516.	12.75	2573.	644.	620.	25.60
	ROUTED TO							
		5,6	8063.	14.00	2518.	645.	621.	25.60
+	HYDROGRAPH AT	BAS5	4938.	13.50	1973.	501.	482.	20.70
+	HYDROGRAPH AT	BAS6	4746.	12.75	1142.	286.	275.	11.80
+	3 COMBINED AT							
		ST56	13491.	13.92	5555.	1431.	1378.	59.10
+	ROUTED TO							
		7,8	13388.	14.00	5538.	1430.	1376.	59.10
+	HYDROGRAPH AT	BAS8	316.	12.33	48.	12.	12.	.50
+	HYDROGRAPH AT	BAS7	3975.	13.00	1179.	295.	284.	12.20
+	3 COMBINED AT							
		ST78	15083.	14.00	6738.	1737.	1674.	71.80
+	ROUTED TO							
		9	14159.	14.50	6592.	1732.	1669.	71.80
+	HYDROGRAPH AT	BAS9	3285.	13.17	1088.	273.	263.	11.30
+	2 COMBINED AT							
		ST9	15289.	14.42	7554.	2006.	1932.	83.10

Sh.22D

JTK 4/30/87  
HM 7/16/

\*\*\* NORMAL END OF HEC-1 \*\*\*





44 LU 0 0.2  
 45 UD 0.73  
 46 KK ST12 COMBINE BAS. 1&2 FLOWS  
 47 HC 2

HEC-1 INPUT

Sh. 23 B.

PAGE 2  
 JTK 5/1/97  
 HM 7/17/27

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

48 KK 3,4 FLOW 1,2 FROM STA. 1,2 TO 3,4  
 49 RK 26400 .032 .04 TRAP 0 0.45

50 KK BAS4  
 51 KM 50YR 24HR  
 52 BA 6.4  
 53 LU 0 0.2  
 54 UD 0.75

55 KK BAS3  
 56 KM 50YR 24HR  
 57 BA 12.1  
 58 LU 0 0.2  
 59 UD .96

60 KK ST34 COMBINE FLOWS 3,4  
 61 HC 3

62 KK 5,6 FLOW 3,4 FROM STA. 3,4 TO 5,6  
 63 RK 53856 .015 .04 TRAP 0 0.03

64 KK BAS5  
 65 KM 50YR 24HR  
 66 BA 20.7  
 67 LU 0 0.2  
 68 UD 1.73

69 KK BAS6  
 70 KM 50YR 24HR  
 71 BA 11.8  
 72 LU 0 0.2  
 73 UD 0.95

74 KK ST56 COMBINE FLOWS 5,6  
 75 HC 3

76 KK 7,8 FLOW 5,6 FROM STA. 5,6 TO 7,8  
 77 RK 6336 0.005 .04 TRAP 0 0.025

78 KK BAS8  
 79 KM 50YR 24HR  
 80 BA 0.5  
 81 LU 0 0.2  
 82 UD 0.52

83 KK BAS7  
 84 KM 50YR 24HR  
 85 BA 12.2  
 86 LU 0 0.2  
 87 UD 1.22

HEC-1 INPUT

PAGE 3

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

88 KK ST78 COMBINE FLOWS 7,8

89 HC 3  
 90 KK 9 FLOWS 7,8 FROM STA.7,8 TO 9  
 91 RK 32736 0.01 .04 TRAP 0 0.05  
 92 KK BAS9  
 93 KM 50YR 24HR  
 94 BA 11.3  
 95 LU 0 0.2  
 96 UD 1.39  
 97 KK ST9 COMBINE FLOWS  
 98 HC 2  
 99 ZZ

Sh. 23 C

JTK 5/1/87  
 HM 7/17/87

1

\*\*\*\*

FLOOD HYDROGRAPH PACKAGE HEC-1 (IBM XT 512K VERSION) -FEB 1, 1985  
 U.S. ARMY CORPS OF ENGINEERS, THE HYDROLOGIC ENGINEERING CENTER, 609 SECOND STREET, DAVIS, CA. 95616

\*\*\*\*

UMTRA - GREEN RIVER - BROWN WASH  
 50 - YR 24-HR STORM

5 10

OUTPUT CONTROL VARIABLES

IPRNT 5 PRINT CONTROL  
 IPLOT 0 PLOT CONTROL  
 QSCAL 0. HYDROGRAPH PLOT SCALE

IT

HYDROGRAPH TIME DATA

NMIN 5 MINUTES IN COMPUTATION INTERVAL  
 IDATE 1 0 STARTING DATE  
 ITIME 0000 STARTING TIME  
 NQ 300 NUMBER OF HYDROGRAPH ORDINATES  
 NDDATE 2 0 ENDING DATE  
 NOTIME 0055 ENDING TIME

COMPUTATION INTERVAL .08 HOURS  
 TOTAL TIME BASE 24.92 HOURS

ENGLISH UNITS

1

RUNOFF SUMMARY  
 FLOW IN CUBIC FEET PER SECOND  
 TIME IN HOURS, AREA IN SQUARE MILES

OPERATION	STATION	PEAK FLOW	TIME OF PEAK	AVERAGE FLOW FOR MAXIMUM PERIOD			BASIN AREA	MAXIMUM STAGE	TIME OF MAX STAGE
				6-HOUR	24-HOUR	72-HOUR			
HYDROGRAPH AT	BAS1	1538.	12.50	260.	70.	67.	2.60		
HYDROGRAPH AT	BAS2	3010.	12.50	592.	148.	142.	5.50		
2 COMBINED AT	ST12	4533.	12.50	871.	218.	210.	8.10		
ROUTED TO	3,4	4271.	12.83	871.	218.	210.	8.10		
HYDROGRAPH AT	BAS4	3440.	12.50	688.	172.	166.	6.40		

+	HYDROGRAPH AT	BAS3	5349.	12.75	1301.	325.	313.	12.10
+	3 COMBINED AT	ST34	12773.	12.75	2850.	715.	689.	26.60
	ROUTED TO	5,6	9155.	14.00	2803.	716.	690.	26.60
+	HYDROGRAPH AT	BAS5	5482.	13.50	2192.	557.	536.	20.70
+	HYDROGRAPH AT	BAS6	5260.	12.75	1269.	317.	306.	11.80
+	3 COMBINED AT	ST56	15248.	13.92	6181.	1590.	1532.	59.10
+	ROUTED TO	7,8	15197.	14.00	6164.	1589.	1531.	59.10
+	HYDROGRAPH AT	BAS8	349.	12.33	54.	13.	13.	.50
+	HYDROGRAPH AT	BAS7	4409.	13.00	1310.	328.	316.	12.20
+	3 COMBINED AT	ST78	17160.	13.92	7499.	1931.	1860.	71.80
	ROUTED TO	9	16068.	14.50	7348.	1926.	1855.	71.80
+	HYDROGRAPH AT	BAS9	3544.	13.17	1209.	304.	293.	11.30
+	2 COMBINED AT	ST9	17385.	14.42	8424.	2230.	2148.	83.10

Sh. 23 D

JTK 5/1/87  
HM 7/17/87

\*\*\* NORMAL END OF HEC-1 \*\*\*



19	FI	.00417	.00417	.00417	.00417	.00417	.00417	.00417	.00417	.0
0417	.00417	.00417	.00417	.00417	.00417	.00417	.00417	.00417	.00417	.0
20	FI	.00417	.00417	.00417	.00417	.00417	.00417	.00417	.00417	.0
00417	.00417	.00417	.00417	.00417	.00417	.00417	.00417	.00417	.00417	.0
21	FI	.00417	.00417	.00417	.00417	.00417	.00417	.00417	.00417	.0
00417	.00417	.00417	.00417	.00417	.00417	.00417	.00417	.00417	.00417	.0
22	FI	.00833	.00833	.00833	.00833	.00833	.00833	.00833	.00833	.0
00833	.00833	.00833	.00833	.00833	.00833	.00833	.00833	.00833	.00833	.0
23	FI	.00833	.00833	.02	.03	.03	.03	.03	.03	.0
004	.04	.06	.07	.07	.10	.15	.26	.00278	.00278	.0
24	FI	.07	.10	.15	.26	.00278	.00278	.00278	.00278	.0
0278	.00278	.00278	.00278	.00278	.00278	.00278	.00278	.00278	.00278	.0
25	FI	.00278	.00278	.00278	.00278	.00278	.00278	.00278	.00278	.0
0278	.00278	.00278	.00278	.00278	.00278	.00278	.00278	.00278	.00278	.0
26	FI	.00278	.00278	.00278	.00278	.00278	.00278	.00278	.00278	.0
0278	.00278	.00278	.00278	.00278	.00278	.00278	.00278	.00278	.00278	.0
27	FI	.00278	.00278	.00278	.00278	.00278	.00278	.00278	.00278	.0
0278	.00278	.00278	.00278	.00278	.00278	.00278	.00278	.00278	.00278	.0
28	FI	.00278	.00278	.00278	.00278	.00278	.00278	.00278	.00278	.0
0278	.00278	.00278	.00278	.00278	.00278	.00278	.00278	.00278	.00278	.0
29	FI	.00278	.00278	.00278	.00278	.00278	.00278	.00278	.00278	.0
0278	.00278	.00278	.00278	.00278	.00278	.00278	.00278	.00278	.00278	.0
30	FI	.00278	.00278	.00278	.00278	.00278	.00278	.00278	.00278	.0
0278	.00278	.00278	.00278	.00278	.00278	.00278	.00278	.00278	.00278	.0
31	FI	.00278	.00278	.00278	.00278	.00278	.00278	.00278	.00278	.0
0139	.00139	.00139	.00139	.00139	.00139	.00139	.00139	.00139	.00139	.0
32	FI	.00139	.00139	.00139	.00139	.00139	.00139	.00139	.00139	.0
0139	.00139	.00139	.00139	.00139	.00139	.00139	.00139	.00139	.00139	.0
33	FI	.00139	.00139	.00139	.00139	.00139	.00139	.00139	.00139	.0
0139	.00139	.00139	.00139	.00139	.00139	.00139	.00139	.00139	.00139	.0
34	FI	.00139	.00139	.00139	.00139	.00139	.00139	.00139	.00139	.0
0139	.00139	.00139	.00139	.00139	.00139	.00139	.00139	.00139	.00139	.0
35	FI	.00139	.00139	.00139	.00139	.00139	.00139	.00139	.00139	.0
0139	.00139	.00139	.00139	.00139	.00139	.00139	.00139	.00139	.00139	.0
36	FI	.00139	.00139	.00139	.00139	.00139	.00139	.00139	.00139	.0
0139	.00139	.00139	.00139	.00139	.00139	.00139	.00139	.00139	.00139	.0
37	FI	.00139	.00139	.00139	.00139	.00139	.00139	.00139	.00139	.0
0139	.00139	.00139	.00139	.00139	.00139	.00139	.00139	.00139	.00139	.0
38	FI	.00139	.00139	.00139	.00139	.00139	.00139	.00139	.00139	.0
0139	.00139	.00139	.00139	.00139	.00139	.00139	.00139	.00139	.00139	.0
39	LU	0	0.2							
40	UD	.66								
41	KK	BAS2								
42	KM	10YR 24HR								
43	BA	5.5								
44	LU	0	0.2							
45	UD	0.73								
46	KK	ST12	COMBINE BAS. 1&2 FLOWS							
47	HC	2								

Sh. 24B  
 JTK 6/11/87  
 HM 7/17/87

48	FK	3,4	FLOW 1,2 FROM STA. 1,2 TO 3,4			
49	RK	26400	.032	.04	TRAP	0
50	KK	BAS4				
51	KM	10YR 24HR				
52	BA	6.4				
53	LU	0	0.2			
54	UD	0.75				
55	KK	BAS3				
56	KM	10YR 24HR				
57	BA	12.1				
58	LU	0	0.2			
59	UD	.96				
60	KK	ST34	COMBINE FLOWS 3,4			
61	HC	3				
62	KK	5,6	FLOW 3,4 FROM STA. 3,4 TO 5,6			
63	RK	53856	.015	.04	TRAP	0
64	KK	BAS5				
65	KM	10YR 24HR				
66	BA	20.7				
67	LU	0	0.2			
68	UD	1.73				
69	KK	BAS6				
70	KM	10YR 24HR				
71	BA	11.8				
72	LU	0	0.2			
73	UD	0.84				
74	KK	ST56	COMBINE FLOWS 5,6			
75	HC	3				

Sh. 24c

JK 5/11/87

HM 7/7/87

0.03

1985

78	KK	BAS8		
79	KM		10YR 24HR	
80	BA	0.5		
81	LU	0	0.2	
82	UD	0.42		
83	KK	BAS7		
84	KM		10YR 24HR	
85	BA	12.2		
86	LU	0	0.2	
87	UD	1.09		

*3h. 24h*  
*JKK 1/17/87*  
*HM 7/17/87*

HEC-1 INPUT

PAGE 3

LINE	ID	1	2	3	4	5	6
7	8	9	10				
88	KK	ST78	COMBINE FLOWS 7,8				
89	HC	3					
90	KK	9	FLOWS 7,8 FROM STA.7,8 TO 9				
91	RK	32736	0.01	.04		TRAP	0
92	KK	BAS9					
93	KM		10YR 24HR				
94	BA	11.3					
95	LU	0	0.2				
96	UD	1.47					
97	KK	ST9	COMBINE FLOWS				
98	HC	2					
99	ZZ						

0.05

1

\*\*\*\*\*  
FLOOD HYDROGRAPH PACKAGE HEC-1 (IBM XT 512K VE

RSION) -FEB 1, 1985

U.S. ARMY CORPS OF ENGINEERS, THE HYDROLOGIC ENGINEERING CENTER  
609 SECOND STREET, DAVIS, CA. 95616

\*\*\*\*\*

Sh. 24-E

UMTRA - GREEN RIVER - BROWN WASH

10 - YR 24-HR STORM

Jrk 6/10/87  
HM 7/17/87

5 IO

OUTPUT CONTROL VARIABLES

IPRNT	5	PRINT CONTROL
IPLOT	0	PLOT CONTROL
QSCAL	0.	HYDROGRAPH PLOT SCALE

IT

HYDROGRAPH TIME DATA

NMIN	5	MINUTES IN COMPUTATION INTERVAL
IDATE	1 0	STARTING DATE
ITIME	0000	STARTING TIME
NQ	300	NUMBER OF HYDROGRAPH ORDINATES
NDDATE	2 0	ENDING DATE
NDTIME	0055	ENDING TIME

COMPUTATION INTERVAL	.08 HOURS
TOTAL TIME BASE	24.92 HOURS

ENGLISH UNITS

1

ILES

RUNOFF SUMMARY  
FLOW IN CUBIC FEET PER SECOND  
TIME IN HOURS, AREA IN SQUARE M

PERIOD	BASIN OPERATION AREA	MAXIMUM STATION STAGE	PEAK TIME OF FLOW MAX STAGE	TIME OF PEAK	AVERAGE FLOW FOR MAXIM	
					6-HOUR	24-HOUR
72-HOUR						
+	HYDROGRAPH AT					
+	47. 2.60	BAS1	1100.	12.50	196.	49.
+	HYDROGRAPH AT					
+	100. 5.50	BAS2	2151.	12.58	414.	103.
+	2 COMBINED AT					
+	147. 8.10	ST12	3234.	12.50	610.	152.
+	ROUTED TO					
+	147. 8.10	3,4	2963.	12.83	609.	153.
+	HYDROGRAPH AT					
+	116. 6.40	BAS4	2456.	12.58	482.	120.
+	HYDROGRAPH AT					
+	219. 12.10	BAS3	3799.	12.75	911.	228.
+	3 COMBINED AT					
+	482. 26.60	ST34	9028.	12.75	2001.	501.



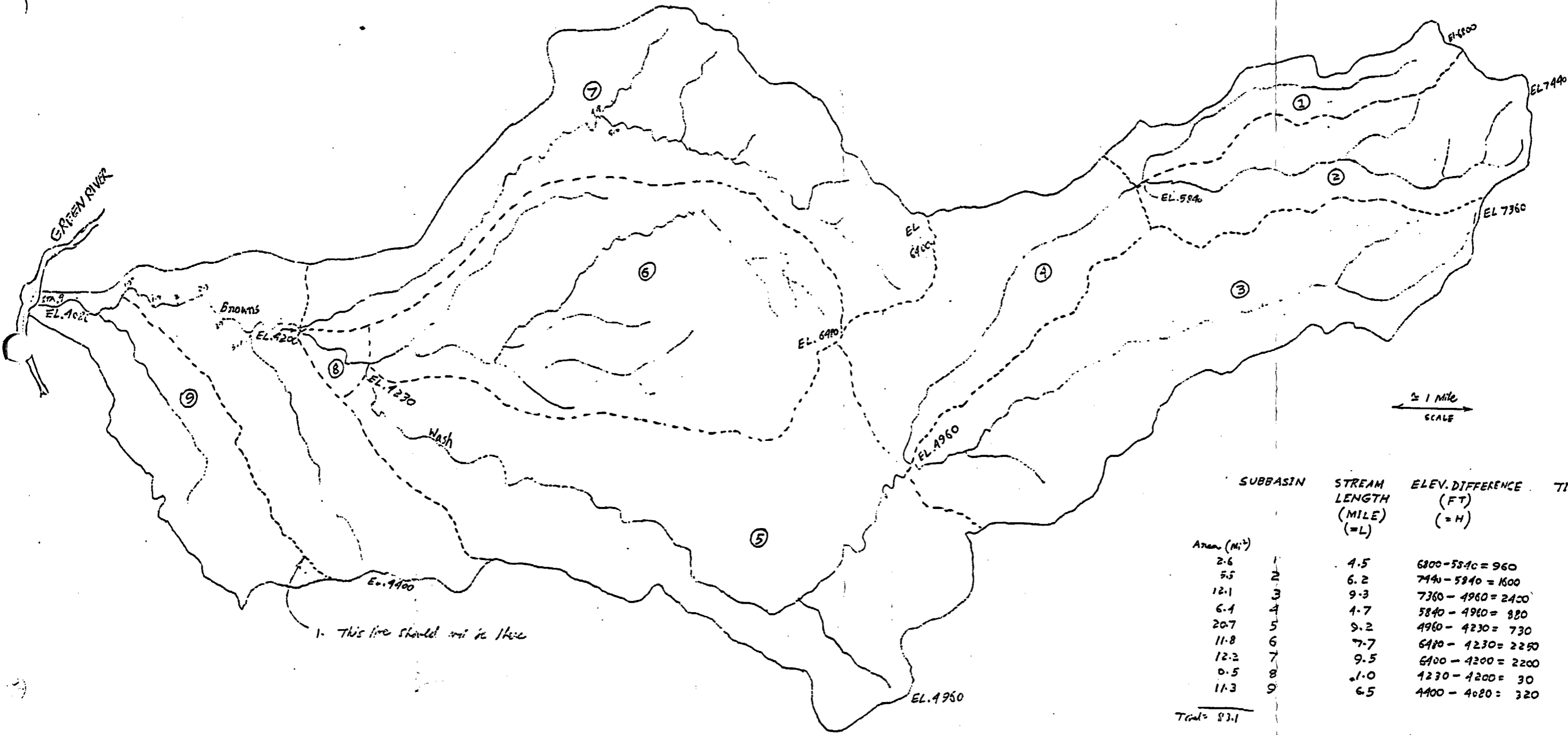
+		ROUTED TO	5,6	6387.	14.17	1958.	501.
	483.	26.60					
+		HYDROGRAPH AT	BAS5	3857.	13.50	1535.	389.
	375.	20.70					
+		HYDROGRAPH AT	BAS6	4136.	12.67	888.	222.
	214.	11.80					
+		3 COMBINED AT	ST56	10090.	14.00	4308.	1113.
	1072.	59.10					
+		ROUTED TO	7,8	9999.	14.17	4292.	1112.
	1071.	59.10					
+		HYDROGRAPH AT	BAS8	289.	12.25	38.	9.
	9.	.50					
+		HYDROGRAPH AT	BAS7	3438.	12.92	918.	230.
	221.	12.20					
+		3 COMBINED AT	ST78	10838.	14.17	5220.	1351.
	1301.	71.80					
+		ROUTED TO	9	10150.	14.75	5111.	1346.
	1297.	71.80					
+		HYDROGRAPH AT	BAS9	2446.	13.25	845.	213.
	205.	11.30					
+		2 COMBINED AT	ST9	10882.	14.75	5847.	1559.
	1502.	83.10					

\*\*\* NORMAL END OF HEC-1 \*\*\*

*S/L 247*

*JPK 1/11/87  
HM 7/17/87*

Sh. 25 A  
 HM 6/11/87  
 JTC 7/14/87



SUBBASIN	STREAM LENGTH (MILE) (=L)	ELEV. DIFFERENCE (FT) (=H)	TIME OF CONC. (HR) (=T <sub>C</sub> ) = $\frac{11.9L^2}{H}$
1	4.5	6800 - 5840 = 960	1.04
2	6.2	7440 - 5840 = 1600	1.25
3	9.3	7360 - 4960 = 2400	1.70
4	4.7	5840 - 4960 = 880	1.14
5	9.2	4960 - 4230 = 730	2.66
6	7.7	6480 - 4230 = 2250	1.40
7	9.5	6400 - 4200 = 2200	1.81
8	1.0	4230 - 4200 = 30	0.70
9	6.5	4400 - 4020 = 380	2.45
Total = 83.1			

0.84 → 1.04  
 1.09 → 1.25  
 0.42 → 0.70  
 1.47 → 1.70

Sh. 258

\*\*\*\*  
FLOOD HYDROGRAPH PACKAGE HEC-1 (IBM XT 512K VERSION) -FEB 1, 1985  
U.S. ARMY CORPS OF ENGINEERS, THE HYDROLOGIC ENGINEERING CENTER, 609 SECOND STREET, DAVIS, CA. 95616  
\*\*\*\*

JK 6/26/87  
HM 7/17/87

THIS HEC-1 VERSION CONTAINS ALL OPTIONS EXCEPT ECONOMICS, AND THE NUMBER OF PLANS ARE REDUCED TO 3

HEC-1 INPUT

PAGE 1

LINE	ID	1	2	3	4	5	6	7	8	9	10
1	ID	UMTRA - GREEN RIVER - BROWN WASH									
2	ID	10 - YR 24-HR STORM									
3	IT	5				300					
4	IN	5									
5	IO	5									
6	KK	BAS1 SUB-BASIN 1									
7	KM	10-YR 24-HR									
8	BA	2.6									
9	PB	1.6									
10	PI	.00139	.00139	.00139	.00139	.00139	.00139	.00139	.00139	.00139	.00139
11	PI	.00139	.00139	.00139	.00139	.00139	.00139	.00139	.00139	.00139	.00139
12	PI	.00139	.00139	.00139	.00139	.00139	.00139	.00139	.00139	.00139	.00139
13	PI	.00139	.00139	.00139	.00139	.00139	.00139	.00139	.00139	.00139	.00139
14	PI	.00139	.00139	.00139	.00139	.00139	.00139	.00139	.00139	.00139	.00139
15	PI	.00139	.00139	.00139	.00139	.00139	.00139	.00139	.00139	.00139	.00139
16	PI	.00139	.00139	.00139	.00139	.00139	.00139	.00139	.00139	.00139	.00139
17	PI	.00139	.00139	.00417	.00417	.00417	.00417	.00417	.00417	.00417	.00417
18	PI	.00417	.00417	.00417	.00417	.00417	.00417	.00417	.00417	.00417	.00417
19	PI	.00417	.00417	.00417	.00417	.00417	.00417	.00417	.00417	.00417	.00417
20	PI	.00417	.00417	.00417	.00417	.00417	.00417	.00417	.00417	.00417	.00417
21	PI	.00417	.00417	.00417	.00417	.00417	.00417	.00417	.00417	.00417	.00417
22	PI	.00833	.00833	.00833	.00833	.00833	.00833	.00833	.00833	.00833	.00833
23	PI	.00833	.00833	.02	.03	.03	.03	.04	.04	.06	.07
24	PI	.07	.10	.15	.26	.00278	.00278	.00278	.00278	.00278	.00278
25	PI	.00278	.00278	.00278	.00278	.00278	.00278	.00278	.00278	.00278	.00278
26	PI	.00278	.00278	.00278	.00278	.00278	.00278	.00278	.00278	.00278	.00278
27	PI	.00278	.00278	.00278	.00278	.00278	.00278	.00278	.00278	.00278	.00278
28	PI	.00278	.00278	.00278	.00278	.00278	.00278	.00278	.00278	.00278	.00278
29	PI	.00278	.00278	.00278	.00278	.00278	.00278	.00278	.00278	.00278	.00278
30	PI	.00278	.00278	.00278	.00278	.00278	.00278	.00278	.00278	.00278	.00278
31	PI	.00278	.00278	.00278	.00278	.00278	.00278	.00139	.00139	.00139	.00139
32	PI	.00139	.00139	.00139	.00139	.00139	.00139	.00139	.00139	.00139	.00139
33	PI	.00139	.00139	.00139	.00139	.00139	.00139	.00139	.00139	.00139	.00139
34	PI	.00139	.00139	.00139	.00139	.00139	.00139	.00139	.00139	.00139	.00139
35	PI	.00139	.00139	.00139	.00139	.00139	.00139	.00139	.00139	.00139	.00139
36	PI	.00139	.00139	.00139	.00139	.00139	.00139	.00139	.00139	.00139	.00139
37	PI	.00139	.00139	.00139	.00139	.00139	.00139	.00139	.00139	.00139	.00139
38	PI	.00139	.00139	.00139	.00139	.00139	.00139	.00139	.00139	.00139	.00139
39	LU	0	0.2								
40	UD	.66									
41	KK	BAS2									
42	KM	10YR 24HR									

42 KM 10YR 24HR  
 43 BA 5.1  
 44 LU 0 0.2  
 45 UD 0.75  
 46 KK ST12 COMBINE BAS. 1&2 FLOWS  
 47 HC 2

sh. 25c



JKK 6/6/57  
 HM 7/17/57

PAGE 2

HEC-1 INPUT

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

48 KK 3,4 FLOW 1,2 FROM STA.1,2 TO 3,4  
 49 RK 26400 .032 .04 TRAP 0 0.45

50 KK BAS4  
 51 KM 10YR 24HR  
 52 BA 6.4  
 53 LU 0 0.2  
 54 UD 0.75

55 KK BAS3  
 56 KM 10YR 24HR  
 57 BA 12.1  
 58 LU 0 0.2  
 59 UD .76

60 KK ST34 COMBINE FLOWS 3,4  
 61 HC 3

62 KK 5,6 FLOW 3,4 FROM STA.3,4 TO 5,6  
 63 RK 53856 .015 .04 TRAP 0 0.03

64 KK BAS5  
 65 KM 10YR 24HR  
 66 BA 20.7  
 67 LU 0 0.2  
 68 UD 1.75

69 KK BAS6  
 70 KM 10YR 24HR  
 71 BA 11.9  
 72 LU 0 0.2  
 73 UD 0.84

74 KK ST56 COMBINE FLOWS 5,6  
 75 HC 3

76 KK 7,8 FLOW 5,6 FROM STA.5,6 TO 7,8  
 77 RK 6336 0.005 .04 TRAP 0 0.025

78 KK BAS8  
 79 KM 10YR 24HR  
 80 BA 0.5  
 81 LU 0 0.2  
 82 UD 0.42

83 KK BAS7  
 84 KM 10YR 24HR  
 85 BA 12.2  
 86 LU 0 0.2  
 87 UD 1.09

HEC-1 INPUT

PAGE 3

00 STG COMBINE FLOWS 7,8  
 01 21000 0.01 1.04 TRAP 0 0.05  
 02  
 03 BASIN  
 04 10YR 24HR  
 05 11.0  
 06 0 0.2  
 07 1.47  
 08 STG COMBINE FLOWS  
 09  
 10  
 11

Sh. 25

JTK 6/26/87  
 HM 7/17/87

\*\*\*\*  
 FLOOD HYDROGRAPH PACKAGE HEC-1 (IBM XT 512K VERSION) -FEB 1, 1985  
 U.S. ARMY CORPS OF ENGINEERS, THE HYDROLOGIC ENGINEERING CENTER, 609 SECOND STREET, DAVIS, CA. 95616  
 \*\*\*\*

UMTRA - GREEN RIVER - BROWN WASH  
 10 - YR 24-HR STORM

5 IO OUTPUT CONTROL VARIABLES

IPRNT 5 PRINT CONTROL  
 IPLOT 0 PLOT CONTROL  
 QSCALE 0. HYDROGRAPH PLOT SCALE

IT HYDROGRAPH TIME DATA

NMIN 5 MINUTES IN COMPUTATION INTERVAL  
 IDATE 1 0 STARTING DATE  
 ITIME 0000 STARTING TIME  
 NIQ 300 NUMBER OF HYDROGRAPH ORDINATES  
 NDDATE 0 0 ENDING DATE  
 NDTIME 0055 ENDING TIME

COMPUTATION INTERVAL .08 HOURS  
 TOTAL TIME BASE 24.92 HOURS

ENGLISH UNITS

RUNOFF SUMMARY  
 FLOW IN CUBIC FEET PER SECOND  
 TIME IN HOURS, AREA IN SQUARE MILES

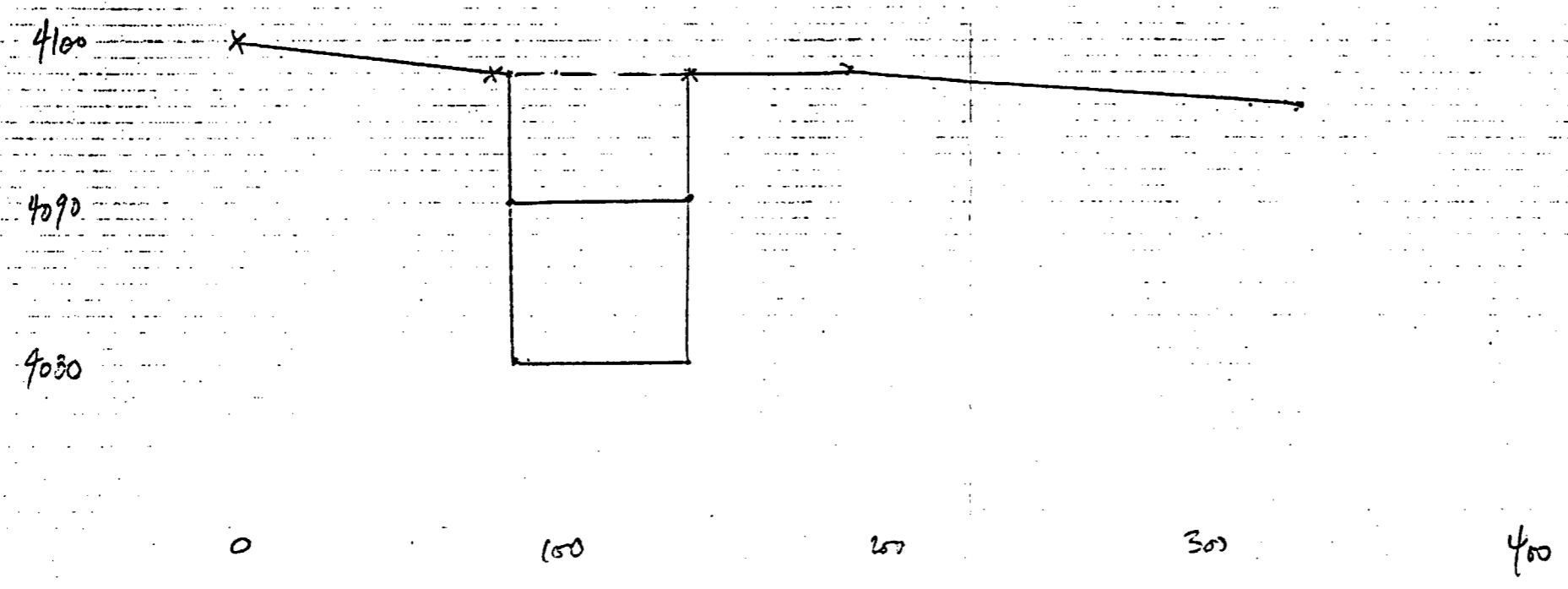
OPERATION	STATION	PEAK FLOW	TIME OF PEAK	AVERAGE FLOW FOR MAXIMUM PERIOD			BASIN AREA	MAXIMUM STAGE	TIME OF MAX STAGE
				6-HOUR	24-HOUR	72-HOUR			
+									
+	HYDROGRAPH AT								
	BAS1	1100.	12.50	196.	49.	47.	2.60		
+	HYDROGRAPH AT								
	BAS2	2151.	12.50	414.	103.	100.	5.50		
+	2 COMBINED AT								
	ST12	3234.	12.50	610.	152.	147.	8.10		
+	ROUTED TO								
	3,4	2963.	12.50	609.	153.	147.	8.10		

+	HYDROGRAPH AT	BAS4	2152.	13.50	482.	120.	116.	6.40
+	HYDROGRAPH AT	BAS3	3779.	12.70	911.	228.	219.	12.10
+	3 COMBINED AT	ST34	9028.	12.70	2001.	501.	482.	26.60
+	ROUTED TO	5,6	6387.	14.17	1958.	501.	483.	26.60
+	HYDROGRAPH AT	BAS5	3857.	13.50	1535.	389.	375.	20.70
+	HYDROGRAPH AT	BAS6	4136.	12.67	888.	222.	214.	11.80
+	3 COMBINED AT	ST56	10070.	14.00	4308.	1113.	1072.	59.10
+	ROUTED TO	7,8	9999.	14.17	4292.	1112.	1071.	59.10
+	HYDROGRAPH AT	BAS8	289.	12.25	38.	9.	9.	.50
+	HYDROGRAPH AT	BAS7	3438.	12.92	918.	230.	221.	12.20
+	3 COMBINED AT	ST78	10838.	14.17	5220.	1351.	1301.	71.80
+	ROUTED TO	9	10224.	14.50	5140.	1349.	1299.	71.80
+	HYDROGRAPH AT	BAS9	2446.	13.25	845.	213.	205.	11.30
+	2 COMBINED AT	ST9	11240.	14.42	5945.	1561.	1504.	83.10

Sh. 25  
 JTK  
 6/26/87  
 HM 7/17/87

\*\*\* NORMAL END OF HEC-1 \*\*\*

Sections 0.6  $\leq$  0.8



JTK 6/8/87  
HM 7/17/87

DATE 2/2/87  
BY RP CHKD. \_\_\_\_\_

SUBJECT GRN SURFACE WATER FLOOD STUDIES  
HYDRAULIC ANALYSIS

SHEET NO. 7  
JOB NO. \_\_\_\_\_

Sh. 27

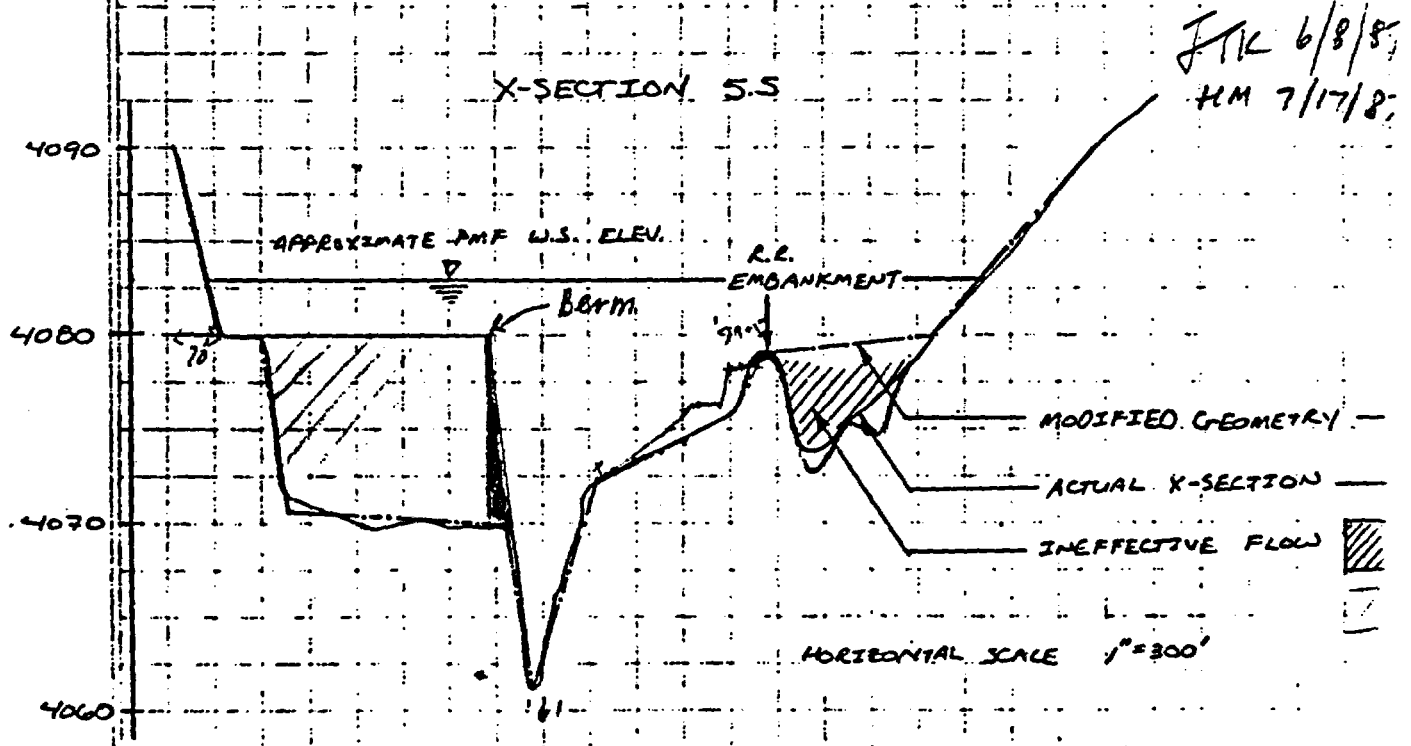
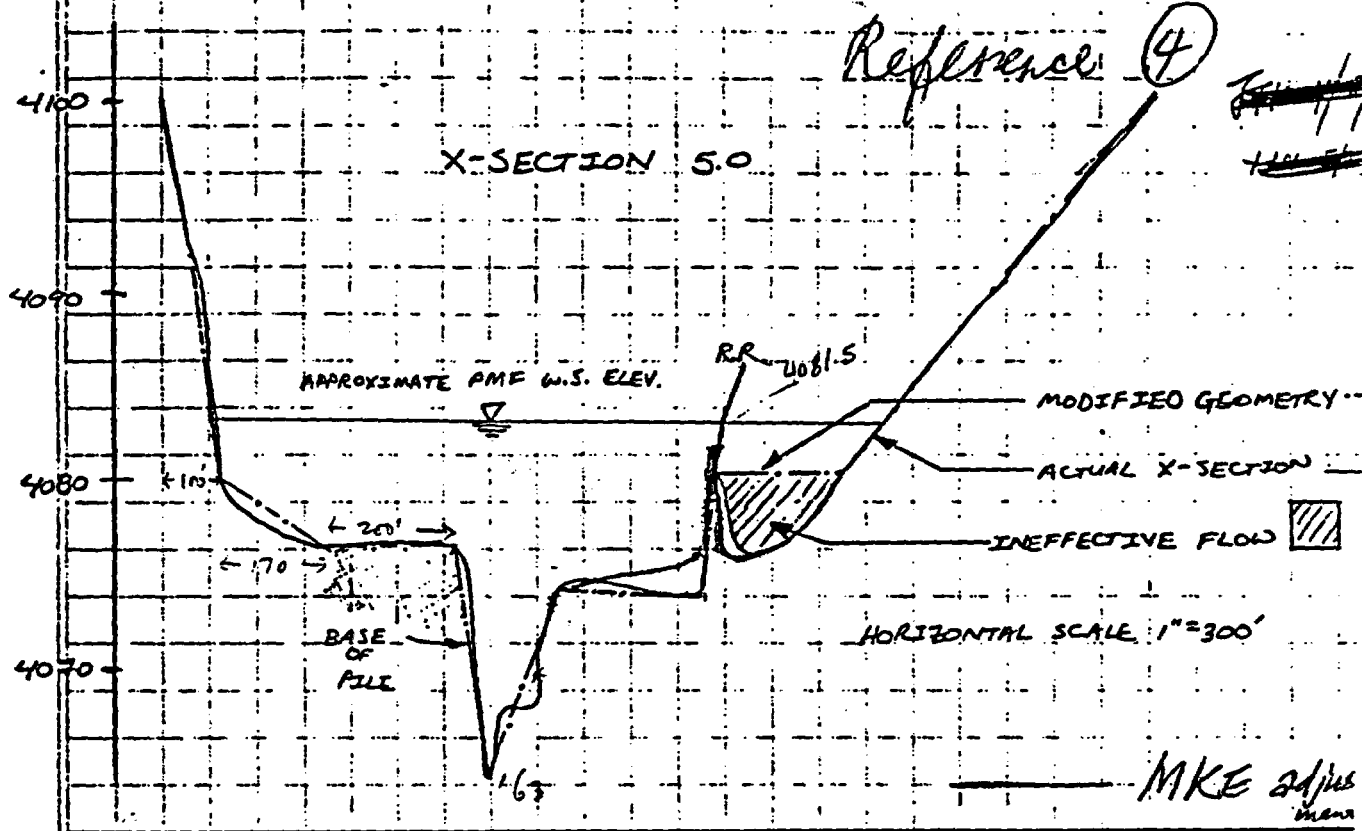


FIGURE 4.0 X-SECTION PLOTS

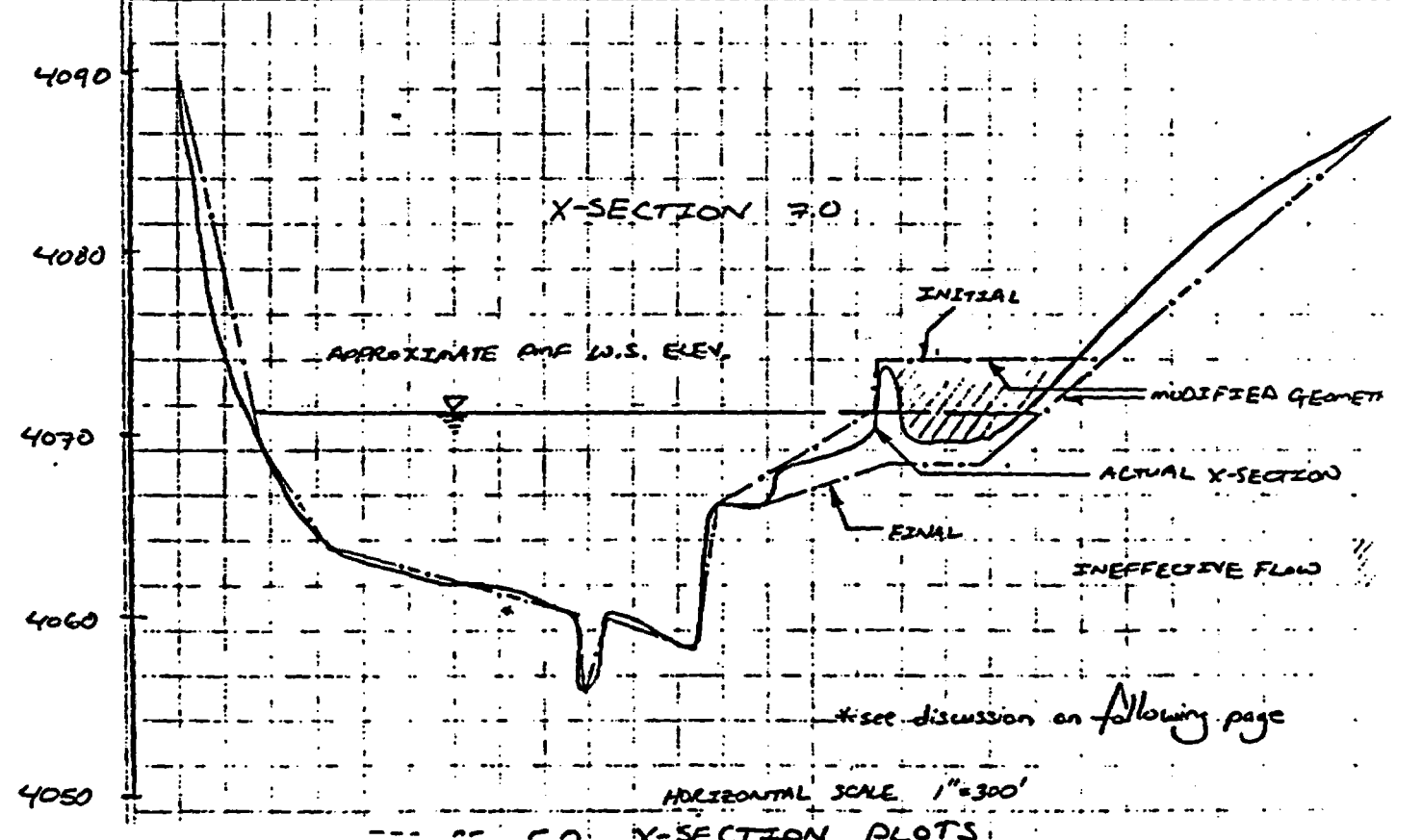
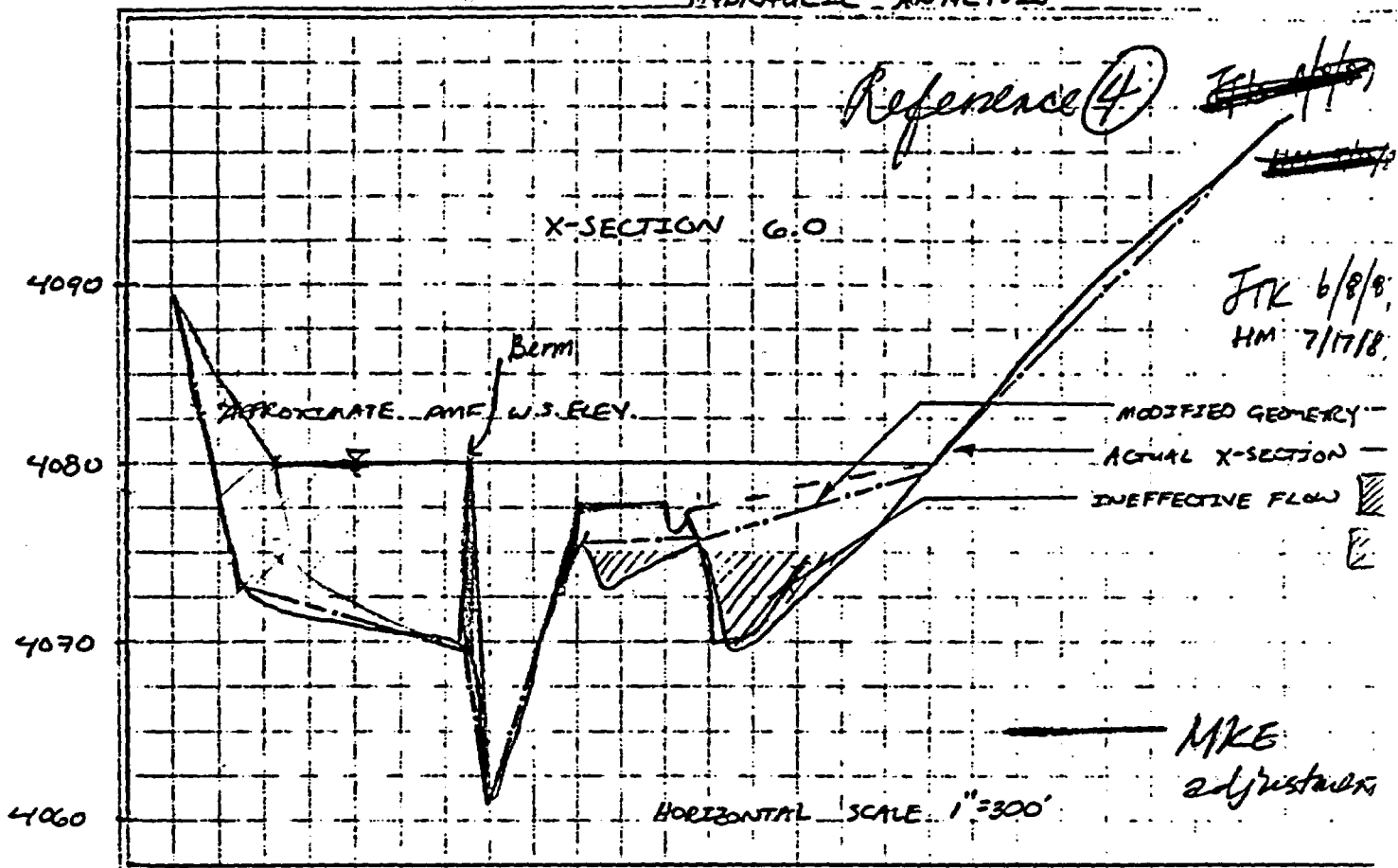


DATE 2/7/87  
BY RP CHKD. \_\_\_\_\_

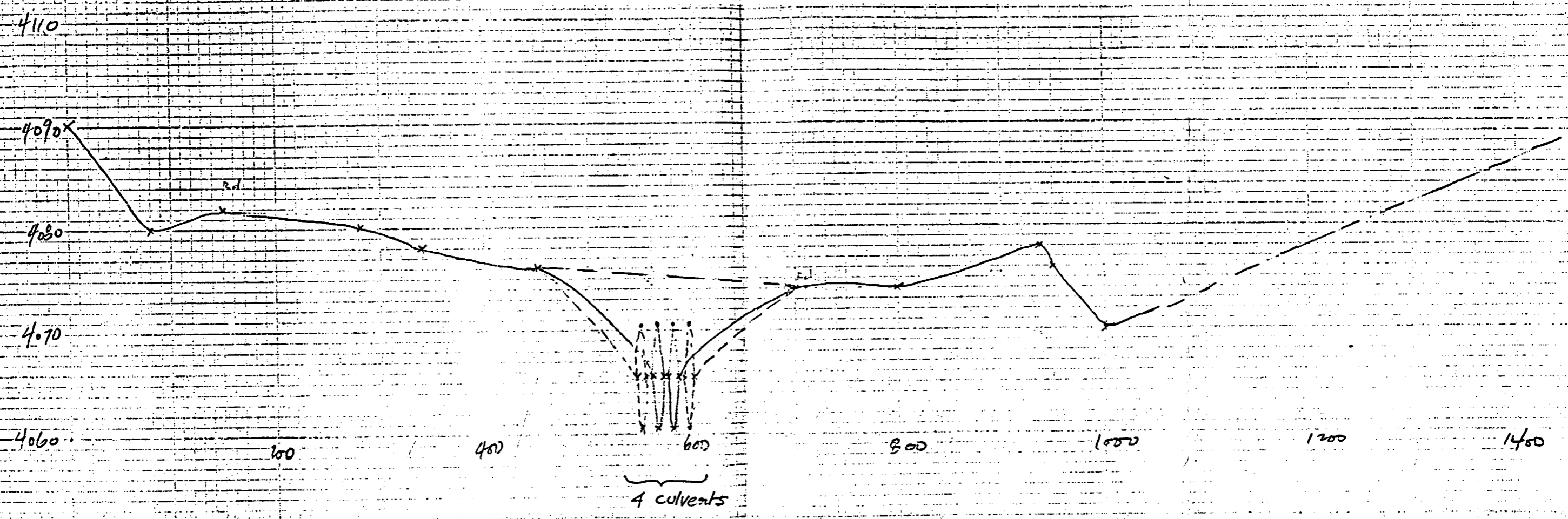
SUBJECT CRN, SURFACE-WATER  
FLOOD STUDIES  
HYDRAULIC ANALYSIS

~~4/1/87~~  
SHEET NO. 28  
JOB NO. \_\_\_\_\_

Reference (4) ~~JFK 6/8/87~~  
~~HM 7/17/87~~



Sections 6.5  $\frac{1}{2}$  6.8



JTK 6/8/87  
HM 7/17/87

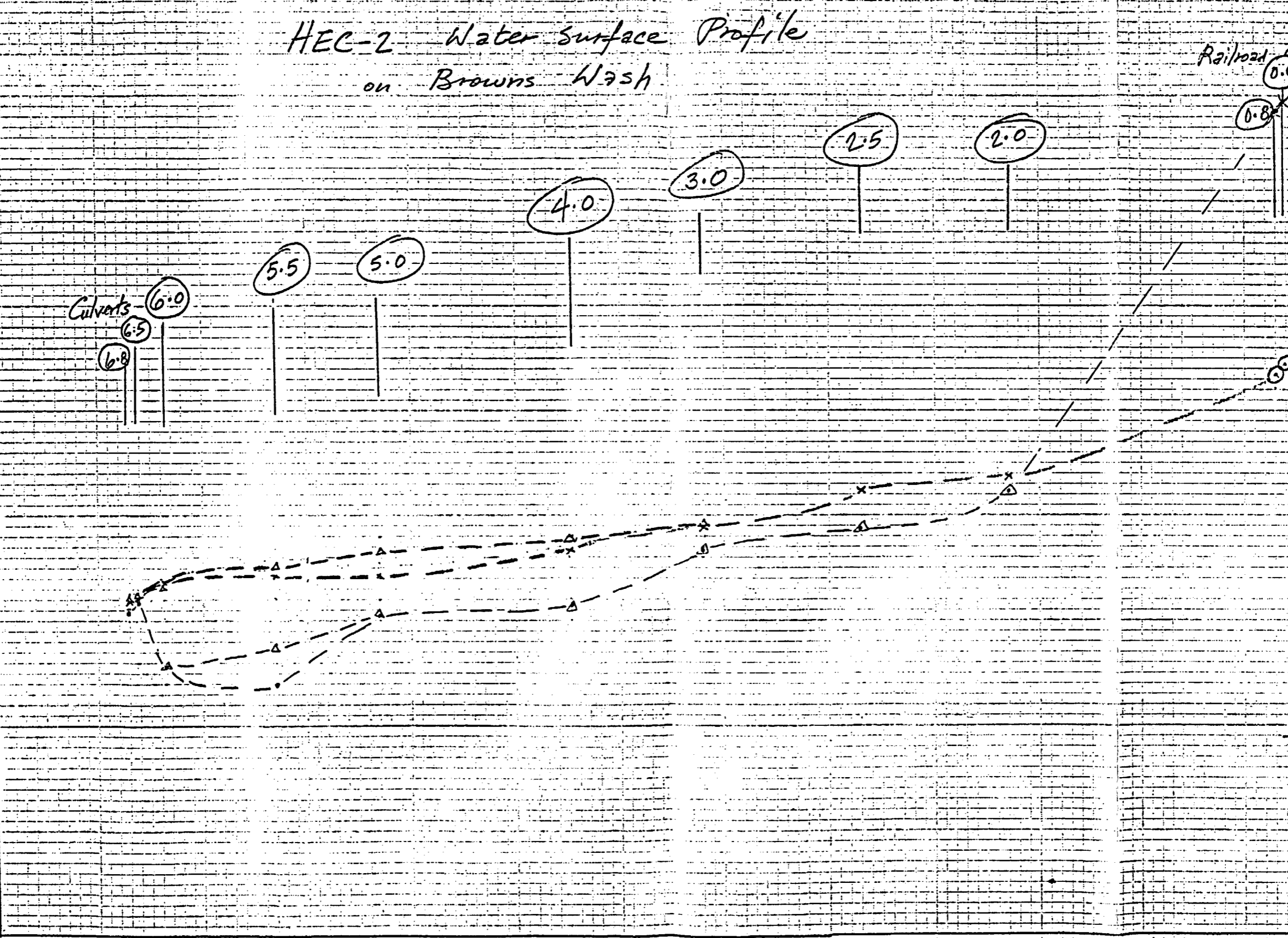
10-yr-24-hr.

Q = 11,300 cfs

# HEC-2 Water surface Profile on Browns Wash

Elevation, ft MSL

4100  
4090  
4080  
4070  
4060



Railroad Crossing

0.6

0.8

--- Actual (without berm)

x Subcritical

○ Supercritical

-.-.- critical (with berm)

—△— with berm (4080') @ stations 5.5 & 6.0

-△-△- critical (with berm)

Distance in ft. from downstream reference station

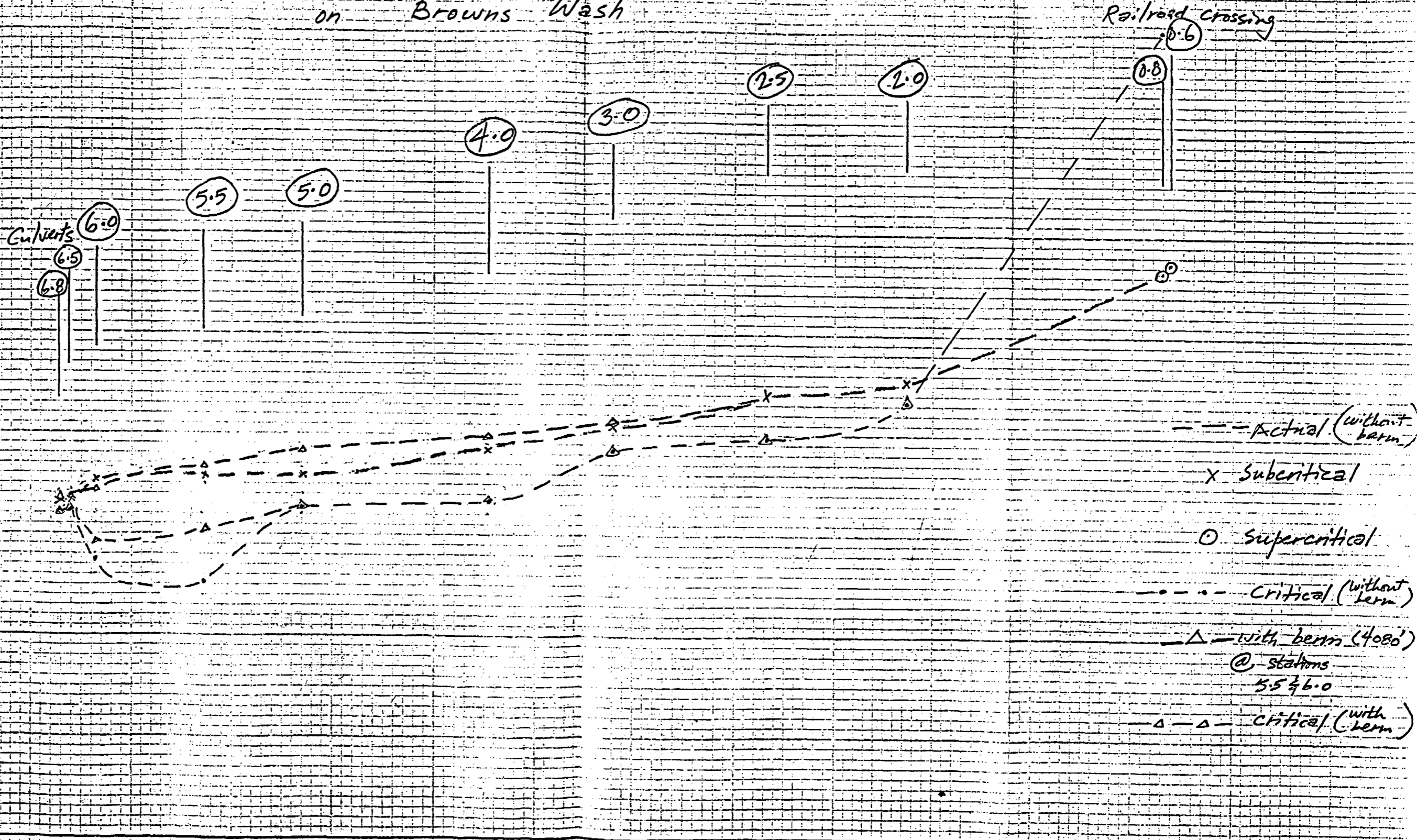
JK 6/8/87  
HM 7/17/87

25-yr 24 hr

Q = 15,300 cfs

# HEC-2 Water Surface Profile on Browns Wash

Elevation, ft  
MSL  
4100  
4090  
4080  
4070  
4060



Distance in ft. from downstream reference station

JFK 6/8/87  
HM 7/17/87



Sh. S. A

\*\*\*\*\*  
 HEC2 RELEASE DATED NOV 76 UPDATED MAY 1984  
 ERROR CORR - 01, 02, 03, 04, 05, 06  
 MODIFICATION - 50, 51, 52, 53, 54, 55, 56  
 \*\*\*\*\*

*Subcritical profile  
 with upstream railroad crossing  
 and downstream culverts  
 (4 functioning)*

T1 UMTRA - GREEN RIVER - 10-YR 24 HR  
 T2 WATER SURFACE PROFILE IN BROWN WASH  
 T3 DISCHARGE = 11300 CFS

J1	ICHECK	ING	NINV	IDIR	STRT	METRIC	HVINS	Q	WSEL	FG
	Q.	0.	0.	0.	0.009000	0.00	0.0	11300.	4074.000	0.000
J2	NPROF	IPLDT	PRFVS	XSECV	XSECH	FN	ALLDC	IBW	CHNIM	ITRACE
	-1.000	0.000	0.000	0.000	0.000	0.000	-1.000	0.000	0.000	0.000
J3	VARIABLE CODES FOR SUMMARY PRINTOUT									
	38.000	43.000	1.000	2.000	13.000	14.000	15.000	35.000	60.000	59.000
	55.000	26.000	56.000	0.000	38.000	58.000	25.000	1.000	42.000	8.000
	51.000	10.000	4.000	53.000	54.000	33.000	5.000	0.000	0.000	0.000
NC	0.045	0.050	0.024	0.300	0.500	0.000	0.000	0.000	0.000	0.000
X1	6.800	25.000	150.000	700.000	0.000	0.000	0.000	0.000	0.000	0.000
BT	25.000	0.000	4090.000	4090.000	80.000	4080.000	4080.000	150.000	4082.000	4082.000
BT	280.000	4080.000	4080.000	340.000	4078.000	4078.000	450.000	4076.000	4076.000	545.000
BT	4075.200	4065.500	550.000	4075.500	4070.500	555.000	4075.200	4065.500	560.000	4075.200
BT	4065.500	565.000	4075.000	4070.500	570.000	4075.000	4065.500	575.000	4075.000	4065.500
BT	580.000	4075.000	4070.500	585.000	4075.000	4065.500	590.000	4074.900	4065.500	595.000
BT	4074.900	4070.500	600.000	4074.800	4065.500	700.000	4074.000	4074.000	800.000	4074.000
BT	4074.000	936.000	4078.000	4078.000	950.000	4076.000	4076.000	1000.000	4070.000	4070.000
BT	1070.000	4070.000	4070.000	1885.000	4100.000	4100.000	0.000	0.000	0.000	0.000
QR	4090.000	0.000	4080.000	80.000	4082.000	150.000	4080.000	280.000	4078.000	340.000
QR	4076.000	450.000	4065.500	545.000	4060.500	550.000	4065.500	555.000	4065.500	560.000
QR	4060.500	565.000	4065.500	570.000	4065.500	575.000	4060.500	580.000	4065.500	585.000
QR	4065.500	590.000	4060.500	595.000	4065.500	600.000	4074.000	700.000	4074.000	800.000
QR	4078.000	936.000	4076.000	950.000	4070.000	1000.000	4070.000	1070.000	4100.000	1885.000
X1	6.500	0.000	0.000	0.000	20.000	20.000	20.000	0.000	0.400	0.000
X2	0.000	0.000	0.000	0.000	0.000	0.000	0.000	1.000	0.000	0.000

FTK 6/11/87  
 HM 7/17/87



11-JUN-87 09:05:31

PAGE 3

Sh. 32C

JTK 6/11/87  
HM 7/17/87

SECNO	DEPTH	CWSEL	CRWS	WSELK	EQ	HV	HL	CLOSS	BANK ELEV
0	GLOB	GCH	GROB	ALOB	ACH	AROB	VOL	TWA	LEFT/RIGHT
TIME	VLOB	VCH	VROB	XLN	XNCH	XNR	WTN	ELMIN	BSTA
SLOPE	XLOBL	XLCH	XLOBR	ITRIAL	IDC	ICONT	CORAR	TOPWID	ENDST

\*PROF 1

CRITICAL DEPTH TO BE CALCULATED AT ALL CROSS SECTIONS

CCHV= 0.300 CEHV= 0.500  
\*SECNO 6.800

3265 DIVIDED FLOW

3370 NORMAL BRIDGE, NRD= 25 MIN ELTRD= 4070.00 MAX ELLC= 4100.00

6.80	15.44	4075.94	4075.30	4074.00	4076.61	0.67	0.00	0.00	4082.00
11300.	0.	2777.	8523.	0.	420.	1301.	0.	0.	4074.00
0.00	0.00	6.61	6.55	0.000	0.024	0.050	0.000	4060.50	450.53
0.009005	0	0.	0.	0	14	4	-1366.45	696.38	1231.40

\*SECNO 6.500

3265 DIVIDED FLOW

3370 NORMAL BRIDGE, NRD= 25 MIN ELTRD= 4070.00 MAX ELLC= 4100.40

6.50	15.19	4076.09	4075.53	0.00	4076.85	0.77	0.19	0.05	4082.40
11300.	0.	3134.	8166.	0.	422.	1188.	1.	0.	4074.40
0.00	0.00	7.43	6.87	0.000	0.024	0.050	0.000	4060.90	452.85
0.010362	20.	20.	20.	2	18	0	-1301.00	676.28	1224.45

CCHV= 0.100 CEHV= 0.300  
\*SECNO 6.000

3301 HV CHANGED MORE THAN HVINS

6.00	14.84	4076.84	4072.83	0.00	4077.02	0.18	0.11	0.06	4074.00
11300.	28.	11272.	0.	28.	3321.	0.	5.	1.	4078.00
0.01	1.02	3.39	0.00	0.045	0.035	0.000	0.000	4062.00	90.46
0.000602	70.	70.	70.	2	14	0	0.00	582.97	673.43

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Sh. 32 D

FTK 6/11/87  
HM 7/17/87

SECNO	DEPTH	CWSEL	CRWS	WSELK	EG	HV	HL	QLOSS	BANK ELEV
Q	GLOB	GCH	GRDB	ALGB	ACH	AROB	VOL	TWA	LEFT/RIGHT
TIME	VLOB	VCH	VROB	XML	XNCH	XNR	WTN	ELMIN	SSTA
SLOPE	XLOBL	XLCH	XLOBR	ITRIAL	IDC	ICONT	CDRAR	TOPWID	ENDST
*SECNO 5.500									
5.50	15.04	4077.04	4071.85	0.00	4077.15	0.10	0.12	0.01	4071.00
11300.	101.	11196.	3.	81.	4317.	9.	29.	5.	4076.00
0.04	1.25	2.59	0.35	0.045	0.035	0.050	0.000	4062.00	153.14
0.000337	150.	270.	280.	2	17	0	0.00	754.27	907.41
CCHV= 0.200 CEHV= 0.500									
*SECNO 5.000									
5.00	13.04	4077.04	4075.68	0.00	4077.55	0.51	0.20	0.20	4076.00
11300.	31.	11267.	1.	24.	1968.	1.	47.	9.	4076.00
0.05	1.32	5.73	1.12	0.045	0.035	0.050	0.000	4064.00	224.40
0.003797	230.	250.	290.	2	13	0	0.00	654.03	878.43
*SECNO 4.000									
4.00	10.38	4078.38	4075.67	0.00	4078.97	0.59	1.38	0.04	4080.00
11300.	0.	11300.	0.	0.	1837.	0.	67.	15.	4080.00
0.07	0.00	6.15	0.00	0.000	0.035	0.000	0.000	4068.00	404.61
0.002417	470.	460.	440.	2	14	0	0.00	362.37	766.97
*SECNO 3.000									
3.00	7.38	4079.38	4078.40	0.00	4080.26	0.88	1.15	0.14	4080.00
11300.	0.	11300.	0.	0.	1504.	0.	79.	18.	4080.00
0.08	0.00	7.51	0.00	0.000	0.035	0.000	0.000	4072.00	405.74
0.005974	315.	318.	320.	1	14	0	0.00	433.54	839.28
CCHV= 0.100 CEHV= 0.300									
*SECNO 2.500									
3301 HV CHANGED MORE THAN HVINS									
2.50	8.15	4081.15	4079.17	0.00	4081.45	0.30	1.13	0.06	4080.00
11300.	3.	11295.	2.	3.	2556.	2.	97.	23.	4080.00
0.10	0.95	4.42	0.84	0.045	0.035	0.050	0.000	4073.00	294.28
0.001783	365.	380.	380.	2	9	0	0.00	669.89	964.16
*SECNO 2.000									
2.00	7.88	4081.88	4081.21	0.00	4082.60	0.73	1.03	0.13	4080.00
11300.	77.	11199.	24.	32.	1630.	11.	114.	27.	4080.00
0.12	2.40	6.87	2.14	0.045	0.035	0.050	0.000	4074.00	346.08
0.005724	350.	350.	300.	2	10	0	0.00	566.03	912.11



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Sh. 32E

FTK 6/16/87  
HM 7/17/87

SECNO	DEPTH	CWSEL	CRISW	WSELK	EQ	HV	HL	DLOSS	BANK ELEV
G	GLOB	GCH	GRGB	ALOB	ACH	AROB	VOL	TWA	LEFT/RIGHT
TIME	VLOB	VCH	VROB	XNL	XNCH	XNR	WTN	ELMIN	SSTA
SLOPE	XLOBL	XLCH	XLOBR	ITRIAL	IDC	ICONT	CORAR	TOPWID	ENDST

CCHV= 0.300 CEHV= 0.500  
 \*SECNO 0.600  
 3280 CROSS SECTION 0.80 EXTENDED 3.41 FEET

3301 HV CHANGED MORE THAN HVINS

3370 NORMAL BRIDGE.NRD= 8 MIN ELTRD= 4096.00 MAX ELLC= 4100.00

7185 MINIMUM SPECIFIC ENERGY  
3720 CRITICAL DEPTH ASSUMED

0.80	19.41	4099.41	4099.41	0.00	4101.23	1.82	2.59	0.55	4098.00
11300.	231.	7156.	3913.	47.	618.	408.	133.	33.	4098.00
0.13	4.92	11.59	9.58	0.015	0.015	0.015	0.000	4080.00	23.52
0.003311	650.	650.	400.	0	10	0	-432.00	306.49	330.00

\*SECNO 0.600  
 3280 CROSS SECTION 0.60 EXTENDED 3.38 FEET

3370 NORMAL BRIDGE.NRD= 8 MIN ELTRD= 4096.00 MAX ELLC= 4100.40

7185 MINIMUM SPECIFIC ENERGY  
3720 CRITICAL DEPTH ASSUMED

0.60	19.38	4099.78	4099.78	0.00	4101.57	1.80	0.06	0.01	4098.40
11300.	212.	7365.	3723.	45.	637.	402.	134.	34.	4098.40
0.13	4.73	11.56	9.27	0.015	0.015	0.015	0.000	4080.40	24.94
0.003163	20.	20.	20.	0	10	0	-410.41	305.06	330.00

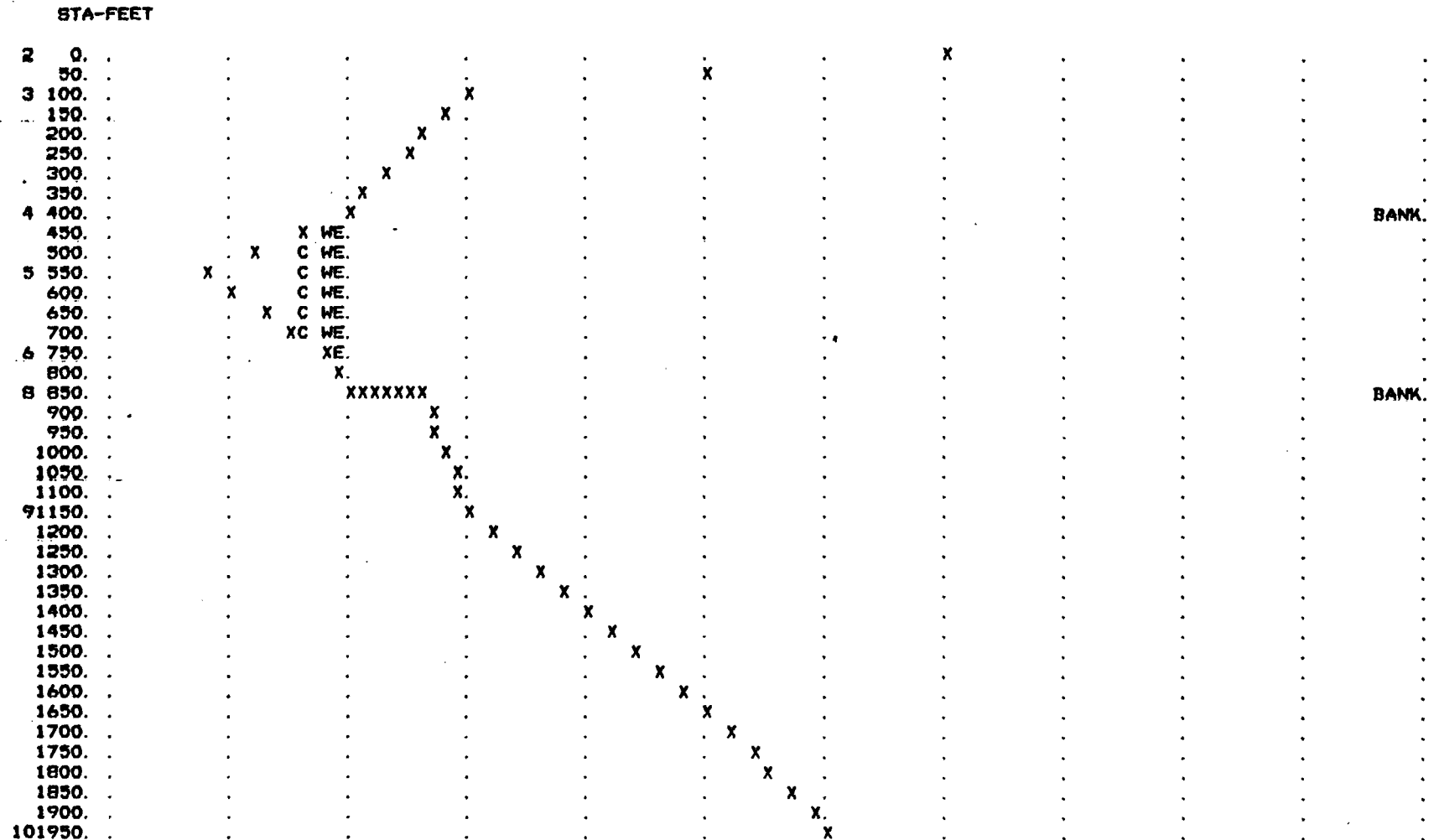
CROSS SECTION 4.00  
 STREAM DISCHARGE = 11300 CFS  
 DISCHARGE = 11300.

sh.32 F

JTK 6/11/87  
 HM 7/17/87

PLOTTED POINTS (BY PRIORITY)-B=BOTTOM BRIDGE, T=TOP BRIDGE, X=GROUND, W=WATER SUR, E=ENERGY GRADIENT, C=CRITICAL WSEL

ELEV 4060. 4070. 4080. 4090. 4100. 4110. 4120. 4130. 4140. 4150. 4160.



NRD= 0 ELLC= 9999999.00 ELTRD= 9999999.00

EL(I), STA(I)	4130.00	0.00	4090.00	100.00	4080.00	385.00	4068.00	530.00	4078.00	730.00
	4080.00	840.00	4086.00	870.00	4090.00	1165.00	4120.00	1930.00		

Sh. 32 G

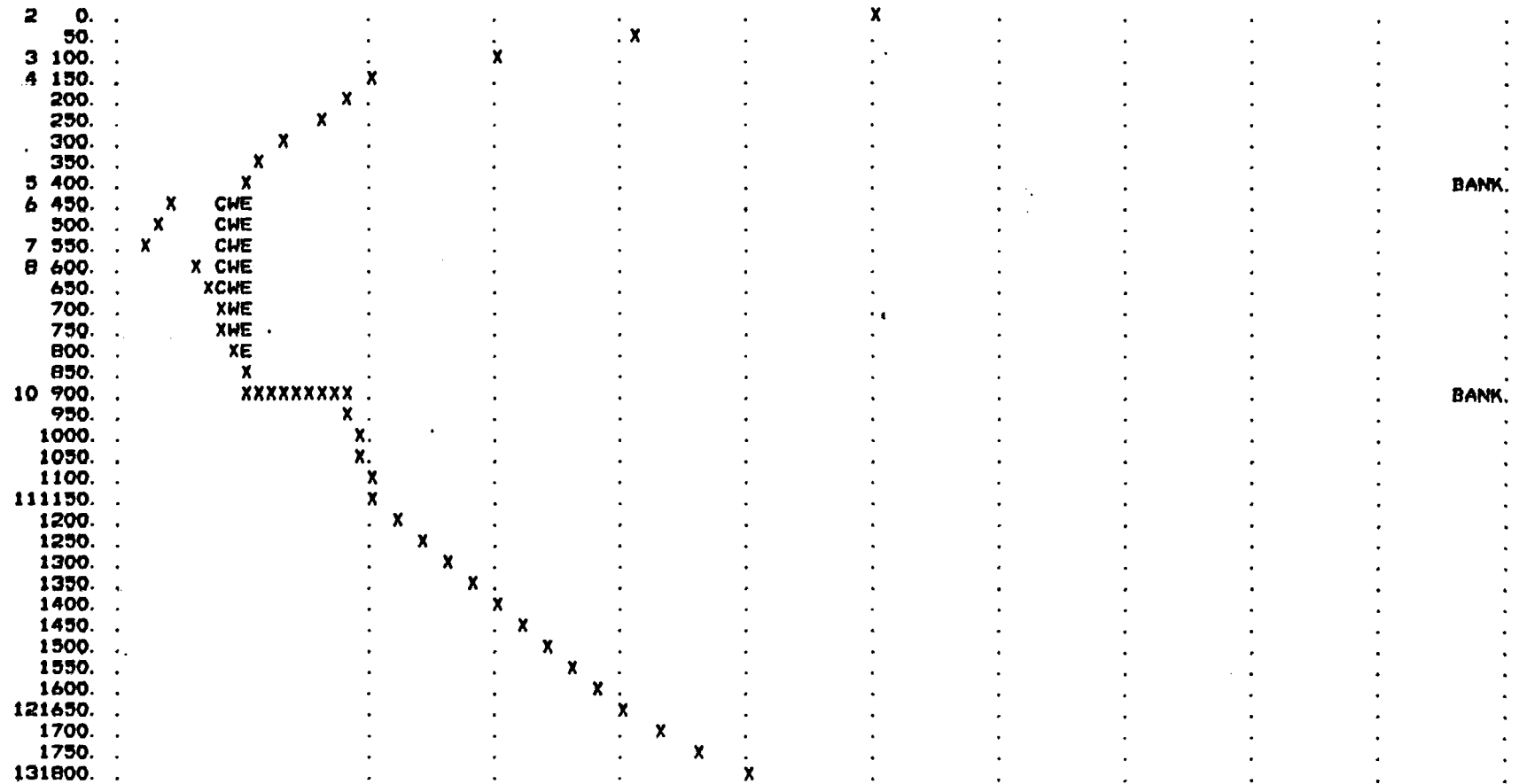
CROSS SECTION 3.00  
 STREAM DISCHARGE = 11300 CFS  
 DISCHARGE= 11300.

JK 6/11/87  
 MM 7/17/87

PLOTTED POINTS (BY PRIORITY)-B=BOTTOM BRIDGE, T=TOP BRIDGE, X=GROUND, W=WATER SUR, E=ENERGY GRADIENT, C=CRITICAL WSEL

ELEV 4070. 4080. 4090. 4100. 4110. 4120. 4130. 4140. 4150. 4160. 4170.

STA-FEET



NRD= 0 ELLC= 9999999.00 ELTRD= 9999999.00

EL(I), STA(I)

4130.00	0.00	4100.00	80.00	4090.00	170.00	4080.00	400.00	-4074.00	455.00
4072.00	570.00	4076.00	620.00	4080.00	880.00	4088.00	925.00	4090.00	1150.00
4110.00	1640.00	4120.00	1820.00						

Sh. 32 H

File 6/11/87  
MM 7/17/87

PROFILE FOR STREAM DISCHARGE = 11300 CFS

PLOTTED POINTS (BY PRIORITY)-E-ENERGY, W-WATER SURFACE, I-INVERT, C-CRITICAL W.S., L-LEFT BANK, R-RIGHT BANK, M-LOWER END STA

ELEVATION SECD	4060. CUMDIS	4065.	4070.	4075.	4080.	4085.	4090.	4095.	4100.	4105.
6.80	0.	I			R . C W E		L			M
6.50	50.	I			R . C W E		L			M
6.00	100.	I			C L . E R					M
	150.	I			C L . E R					M
	200.	I			C L . E R					M
	250.	I			C . E					M
	300.	I			L C C . R E					M
5.50	350.	I			L C C . R E					M
	400.	I			L C C . R E					M
	450.	I			L C C . R E					M
	500.	I			L C C . R W E					M
	550.	I			C . R W E					M
5.00	600.	I			C . R W E					M
	650.	I			C L W E					M
	700.	I			C L W E					M
	750.	I			C L W E					M
	800.	I			C . W E					M
	850.	I			C . W E					M
	900.	I			C . W E					M
	950.	I			C . W E					M
	1000.	I			C . W E L					M
4.00	1050.	I			C . W E L					M
	1100.	I			C . W E L					M
	1150.	I			C . W E L					M
	1200.	I			C . W E L					M
	1250.	I			C . W E L					M
	1300.	I			C . W E					M
3.00	1350.	I			C W E					M
	1400.	I			C W E					M
	1450.	I			C W E					M
	1500.	I			C W E					M
	1550.	I			C W E					M
	1600.	I			C L W E					M
	1650.	I			C L W E					M
	1700.	I			C L E					M
2.50	1750.	I			C L W E					M
	1800.	I			C L W E					M
	1850.	I			C L W E					M
	1900.	I			C W E					M
	1950.	I			C W E					M
	2000.	I			L C W E					M
	2050.	I			L C W E					M
2.00	2100.	I			L C W E					M
	2150.	I			L C W E					M
	2200.	I			L C W E					M
	2250.	I			L C W E					M
	2300.	I			L C W E					M
	2350.	I			L C W E					M
	2400.	I			L C W E					M

	2450.	.	.	.	.	.	.	.
	2500.	.	.	.	.	.	.	.
	2550.	.	.	.	.	.	.	.
	2600.	.	.	.	.	.	.	.
	2650.	.	.	.	.	.	.	.
	2700.	.	.	.	.	.	.	.
	2750.	.	.	.	.	.	.	.
0.80	2800.	.	.	.	.	.	.	.
0.60	2850.	.	.	.	.	.	.	.

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Sh. 32 I

JK 6/11/87  
HM 7/17/87

Sh. 32J

FTU 6/11/87  
HM 7/17/87

\*\*\*\*\*  
 HEC2 RELEASE DATED NOV 76 UPDATED MAY 1984  
 ERROR CORR - 01,02,03,04,05,06  
 MODIFICATION - 50,51,52,53,54,55,56  
 \*\*\*\*\*

NOTE- ASTERISK (\*) AT LEFT OF CROSS-SECTION NUMBER INDICATES MESSAGE IN SUMMARY OF ERRORS LIST

DISCHARGE = 11300 CFS

SUMMARY PRINTOUT

SECNO	Q	CWSEL	CRWS	GLOB	GCH	GROB	GLOBP	GCHP	GROBP	VLOB	VCH	VROB
6.800	11300.00	4075.94	4075.30	0.00	2777.36	8522.64	0.00	24.58	75.42	0.00	6.61	6.55
6.500	11300.00	4076.09	4075.53	0.00	3134.29	8165.71	0.00	27.74	72.26	0.00	7.43	6.87
6.000	11300.00	4076.84	4072.83	28.26	11271.75	0.00	0.25	99.75	0.00	1.02	3.39	0.00
5.500	11300.00	4077.04	4071.85	101.23	11195.56	3.21	0.90	99.08	0.03	1.25	2.59	0.35
5.000	11300.00	4077.04	4075.68	31.29	11267.29	1.42	0.28	99.71	0.01	1.32	5.73	1.12
4.000	11300.00	4078.38	4075.67	0.00	11300.00	0.00	0.00	100.00	0.00	0.00	6.15	0.00
3.000	11300.00	4079.38	4078.40	0.00	11300.00	0.00	0.00	100.00	0.00	0.00	7.51	0.00
2.500	11300.00	4081.15	4079.17	3.11	11294.88	2.01	0.03	99.95	0.02	0.95	4.42	0.84
2.000	11300.00	4081.88	4081.21	76.65	11198.89	24.47	0.68	99.11	0.22	2.40	6.87	2.14
* 0.800	11300.00	4099.41	4099.41	230.87	7155.75	3913.39	2.04	63.33	34.63	4.92	11.59	9.58
* 0.600	11300.00	4099.78	4099.78	211.88	7364.91	3723.21	1.88	65.18	32.95	4.73	11.56	9.27

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Sh. 32 K

JTK 6/11/87  
HM 7/17/87

DISCHARGE = 11300 GFS

SUMMARY PRINTOUT

SECNO	KRATIO	AREA	CWSEL	ELMIN	DEPTH	DIFWSX	HV	TOPWID	SSTA	ENDST	K*CHSL	10K#6
6.800	0.00	1720.64	4075.94	4060.50	15.44	0.00	0.67	696.38	450.53	1231.40	0.00	90.05
6.500	0.93	1610.49	4076.09	4060.90	15.19	0.14	0.77	676.28	452.85	1224.45	20.00	103.62
6.000	4.15	3348.91	4076.84	4062.00	14.84	0.76	0.18	582.97	90.46	673.43	15.72	6.02
5.500	1.34	4406.83	4077.04	4062.00	15.04	0.20	0.10	754.27	153.14	907.41	0.00	3.37
5.000	0.30	1992.62	4077.04	4064.00	13.04	0.00	0.51	654.03	224.40	878.43	8.00	37.97
4.000	1.25	1836.77	4078.38	4068.00	10.38	1.34	0.59	362.37	404.61	766.97	8.70	24.17
3.000	0.64	1503.85	4079.38	4072.00	7.38	1.00	0.88	433.54	405.74	839.28	12.58	59.74
2.500	1.83	2561.21	4081.15	4073.00	8.15	1.76	0.30	669.89	294.28	964.16	2.63	17.83
2.000	0.56	1673.19	4081.88	4074.00	7.88	0.73	0.73	566.03	346.08	912.11	2.86	57.24
* 0.800	1.31	1072.91	4099.41	4080.00	19.41	17.53	1.82	306.49	23.52	330.00	9.23	33.11
* 0.600	1.02	1083.59	4099.78	4080.40	19.38	0.36	1.80	305.06	24.94	330.00	20.00	31.63

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PAGE B

Sh. 32L

JTC 6/11/87

HM 7/17/87

SUMMARY OF ERRORS AND SPECIAL NOTES

CAUTION	SECNO=	0.800	PROFILE= 1	CRITICAL DEPTH ASSUMED
CAUTION	SECNO=	0.800	PROFILE= 1	MINIMUM SPECIFIC ENERGY
CAUTION	SECNO=	0.600	PROFILE= 1	CRITICAL DEPTH ASSUMED
CAUTION	SECNO=	0.600	PROFILE= 1	MINIMUM SPECIFIC ENERGY



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sh. 32 M

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HEC2 RELEASE DATED NOV 76 UPDATED MAY 1984  
ERROR CORR - 01,02,03,04,05,06  
MODIFICATION - 50,51,52,53,54,55,56  
\*\*\*\*\*

JTK 6/11/87  
HM 7/1/87

Sh. 33A

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 HEC2 RELEASE DATED NOV 76 UPDATED MAY 1984  
 ERROR CORR - 01,02,03,04,05,06  
 MODIFICATION - 50,51,52,53,54,55,56  
 \*\*\*\*\*

JTK 6/11/87  
 HM 7/14/87

T1 UMTRA - GREEN RIVER - 25-YR 24 HR  
 T2 WATER SURFACE PROFILE IN BROWN WASH  
 T3 DISCHARGE = 15300 CFS

J1	ICHECK	ING	NINV	IDIR	STRT	METRIC	HVINS	Q	WSEL	FG
	0.	0.	0.	0.	0.009000	0.00	0.0	15300.	4074.000	0.000
J2	NPROF	IPL0T	PRFVS	XSECV	XSECH	FN	ALLDC	IBW	CHNIM	ITRACE
	-1.000	0.000	0.000	0.000	0.000	0.000	-1.000	0.000	0.000	0.000
J3	VARIABLE CODES FOR SUMMARY PRINTOUT									
	38.000	43.000	1.000	2.000	13.000	14.000	15.000	35.000	60.000	59.000
	55.000	26.000	56.000	0.000	38.000	58.000	25.000	1.000	42.000	8.000
	51.000	10.000	4.000	53.000	54.000	33.000	5.000	0.000	0.000	0.000
NC	0.045	0.050	0.024	0.300	0.500	0.000	0.000	0.000	0.000	0.000
X1	6.800	25.000	150.000	700.000	0.000	0.000	0.000	0.000	0.000	0.000
BT	25.000	0.000	4090.000	4090.000	80.000	4080.000	4080.000	4080.000	150.000	4082.000
BT	280.000	4080.000	4080.000	340.000	4078.000	4078.000	450.000	4076.000	4076.000	545.000
BT	4073.500	4065.500	550.000	4075.500	4070.500	555.000	4075.200	4065.500	560.000	4075.200
BT	4065.500	565.000	4075.000	4070.500	570.000	4075.000	4065.500	575.000	4075.000	4065.500
BT	580.000	4075.000	4070.500	585.000	4075.000	4065.500	590.000	4074.900	4065.500	595.000
BT	4074.900	4070.500	600.000	4074.800	4065.500	700.000	4074.000	4074.000	800.000	4074.000
BT	4074.000	936.000	4078.000	4078.000	950.000	4076.000	4076.000	1000.000	4070.000	4070.000
BT	1070.000	4070.000	4070.000	1885.000	4100.000	4100.000	0.000	0.000	0.000	0.000
QR	4090.000	0.000	4080.000	80.000	4082.000	150.000	4080.000	280.000	4078.000	340.000
QR	4076.000	450.000	4065.500	545.000	4060.500	550.000	4065.500	555.000	4065.500	560.000
QR	4060.500	565.000	4065.500	570.000	4065.500	575.000	4060.500	580.000	4065.500	585.000
QR	4065.500	590.000	4060.500	595.000	4065.500	600.000	4074.000	700.000	4074.000	800.000
QR	4078.000	936.000	4076.000	950.000	4070.000	1000.000	4070.000	1070.000	4100.000	1885.000
X1	6.500	0.000	0.000	0.000	20.000	20.000	20.000	0.000	0.400	0.000
X2	0.000	0.000	0.000	0.000	0.000	0.000	1.000	0.000	0.000	0.000

NC	0.045	0.050	0.035	0.100	0.300	0.000	0.000	0.000	0.000	0.000
X1	6.000	8.000	110.000	890.000	70.000	70.000	70.000	0.000	0.000	0.000
GR	4090.000	0.000	4074.000	110.000	4070.000	490.000	4062.000	525.000	4078.000	685.000
GR	4078.000	890.000	4080.000	1265.000	4100.000	1885.000	0.000	0.000	0.000	0.000
X1	5.500	11.000	180.000	890.000	150.000	280.000	270.000	0.000	0.000	0.000
GR	4090.000	0.000	4080.000	80.000	4080.000	140.000	4071.000	180.000	4070.000	530.000
GR	4062.000	570.000	4073.000	680.000	4076.000	890.000	4079.000	940.000	4080.000	1200.000
GR	4090.000	1460.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
NC	0.000	0.000	0.000	0.200	0.500	0.000	0.000	0.000	0.000	0.000
X1	5.000	10.000	270.000	876.000	230.000	290.000	250.000	0.000	0.000	0.000
GR	4100.000	0.000	4080.000	95.000	4076.000	270.000	4076.000	470.000	4064.000	530.000
GR	4074.000	635.000	4076.000	876.000	4082.000	890.000	4082.000	1090.000	4110.000	1885.000
X1	4.000	9.000	385.000	840.000	470.000	440.000	460.000	0.000	0.000	1.000
GR	4130.000	0.000	4090.000	100.000	4080.000	385.000	4068.000	530.000	4078.000	750.000
GR	4080.000	840.000	4086.000	870.000	4090.000	1165.000	4120.000	1930.000	0.000	0.000
X1	3.000	12.000	400.000	880.000	315.000	320.000	318.000	0.000	0.000	1.000
GR	4130.000	0.000	4100.000	80.000	4090.000	170.000	4080.000	400.000	4074.000	455.000
GR	4072.000	570.000	4076.000	620.000	4080.000	880.000	4088.000	925.000	4090.000	1150.000
GR	4110.000	1640.000	4120.000	1820.000	0.000	0.000	0.000	0.000	0.000	0.000
NC	0.000	0.000	0.000	0.100	0.300	0.000	0.000	0.000	0.000	0.000
X1	2.500	12.000	300.000	960.000	365.000	380.000	380.000	0.000	0.000	0.000
GR	4110.000	0.000	4090.000	250.000	4080.000	300.000	4073.000	420.000	4076.000	500.000
GR	4076.000	560.000	4078.000	620.000	4078.000	800.000	4080.000	960.000	4091.000	1000.000
GR	4096.000	1330.000	4110.000	1700.000	0.000	0.000	0.000	0.000	0.000	0.000
X1	2.000	11.000	380.000	900.000	350.000	300.000	350.000	0.000	0.000	0.000
GR	4114.000	0.000	4090.000	200.000	4080.000	380.000	4074.000	400.000	4074.000	430.000
GR	4078.000	510.000	4080.000	600.000	4080.000	900.000	4094.000	990.000	4094.000	1170.000
GR	4120.000	1890.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
NC	0.015	0.015	0.015	0.300	0.500	0.000	0.000	0.000	0.000	0.000
X1	0.800	8.000	85.000	140.000	650.000	400.000	650.000	0.000	0.000	0.000
BT	8.000	0.000	4100.000	4100.000	80.000	4098.000	4098.000	85.000	4098.000	4098.000
BT	86.000	4098.000	4090.000	139.000	4098.000	4090.000	140.000	4098.000	4098.000	190.000
BT	4098.000	4098.000	330.000	4096.000	4096.000	0.000	0.000	0.000	0.000	0.000
GR	4100.000	0.000	4098.000	80.000	4098.000	85.000	4080.000	86.000	4080.000	139.000
GR	4098.000	140.000	4098.000	190.000	4096.000	330.000	0.000	0.000	0.000	0.000
X1	0.600	0.000	0.000	0.000	20.000	20.000	20.000	0.000	0.400	0.000
X2	0.000	0.000	0.000	0.000	0.000	0.000	1.000	0.000	0.000	0.000
EJ	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000

JTK

6/11/87  
HM 7/17/87

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Sh. 33C

File 4/11/87  
HM 7/17/87

SECNO	DEPTH	CWSEL	CRWS	WSELK	EQ	HV	HL	CLOSS	BANK ELEV
0	GLOB	GCH	GROB	ALOB	ACH	AROB	VOL	TWA	LEFT/RIGHT
TIME	VLOB	VCH	VROB	XNL	XNCH	XNR	WTN	ELMIN	SSTA
SLOPE	XLOBL	XLCH	XLOBR	ITRIAL	IDC	ICONT	CORAR	TOPWID	ENDST

\*PRQF 1

CRITICAL DEPTH TO BE CALCULATED AT ALL CROSS SECTIONS

CCHV= 0.300 CEHV= 0.500  
\*SECNO 6.800

3265 DIVIDED FLOW

3370 NORMAL BRIDGE, NRD= 25 MIN ELTRD= 4070.00 MAX ELLC= 4100.00

6.80	16.03	4076.53	4075.90	4074.00	4077.32	0.79	0.00	0.00	4082.00
15300.	0.	4358.	10942.	0.	574.	1575.	0.	0.	4074.00
0.00	0.00	7.59	6.95	0.000	0.024	0.050	0.000	4060.50	420.94
0.009036	0.	0.	0.	0	13	5	-1366.77	766.07	1247.35

\*SECNO 6.500

3265 DIVIDED FLOW

3370 NORMAL BRIDGE, NRD= 25 MIN ELTRD= 4070.00 MAX ELLC= 4100.40

6.50	15.77	4076.67	4076.14	0.00	4077.57	0.91	0.20	0.06	4082.40
15300.	0.	4686.	10614.	0.	564.	1449.	1.	0.	4074.40
0.00	0.00	8.31	7.32	0.000	0.024	0.050	0.000	4060.90	435.36
0.010556	20.	20.	20.	2	13	0	-1305.78	733.78	1240.23

CCHV= 0.100 CEHV= 0.300  
\*SECNO 6.000

3301 HV CHANGED MORE THAN HVINS

6.00	15.51	4077.51	4073.52	0.00	4077.77	0.26	0.14	0.06	4074.00
15300.	56.	15244.	0.	42.	3699.	0.	6.	1.	4078.00
0.01	1.33	4.12	0.00	0.045	0.035	0.000	0.000	4062.00	85.88
0.000782	70.	70.	70.	2	13	0	0.00	594.21	680.09

Sh. 33D

JFK 6/11/87  
MM 7/17/87

SECNO	DEPTH	CWSEL	CRISW	WSELK	EG	HV	HL	DLOSS	BANK ELEV
G	GLOB	GCH	GROB	ALOB	ACH	AROB	VOL	TWA	LEFT/RIGHT
TIME	VLOB	VCH	VRQB	XNL	XNCH	XNR	WTN	ELMIN	SSTA
SLOPE	XLOBL	XLCH	XLOBR	ITRIAL	IDC	ICONT	CORAR	TOPWID	ENDST
<b>*SECNO 5.500</b>									
5.50	15.78	4077.78	4072.56	0.00	4077.93	0.15	0.15	0.01	4071.00
15300.	154.	15131.	15.	102.	4842.	27.	32.	6.	4076.00
0.03	1.50	3.13	0.56	0.045	0.035	0.050	0.000	4062.00	149.85
0.000420	150.	270.	280.	2	18	0	0.00	769.89	919.74
CCHV= 0.200 CEHV= 0.500									
<b>*SECNO 5.000</b>									
5.00	13.79	4077.79	4076.38	0.00	4078.39	0.61	0.23	0.23	4076.00
15300.	126.	15169.	6.	70.	2419.	4.	54.	10.	4076.00
0.04	1.80	6.27	1.53	0.045	0.035	0.050	0.000	4064.00	191.85
0.003459	230.	250.	290.	2	13	0	0.00	688.32	880.17
<b>*SECNO 4.000</b>									
4.00	11.19	4079.19	4076.66	0.00	4079.98	0.78	1.50	0.09	4080.00
15300.	0.	15300.	0.	0.	2153.	0.	78.	16.	4080.00
0.04	0.00	7.11	0.00	0.000	0.035	0.000	0.000	4068.00	394.71
0.003069	470.	460.	440.	2	14	0	0.00	409.11	803.82
<b>*SECNO 3.000</b>									
3.00	8.36	4080.36	4079.23	0.00	4081.30	0.94	1.24	0.08	4080.00
15300.	1.	15299.	0.	1.	1963.	0.	93.	19.	4080.00
0.07	0.76	7.80	0.67	0.045	0.035	0.050	0.000	4072.00	391.73
0.005163	315.	318.	320.	2	14	0	0.00	490.29	882.02
CCHV= 0.100 CEHV= 0.300									
<b>*SECNO 2.500</b>									
3301 HV CHANGED MORE THAN HVINS									
2.50	9.02	4082.02	4079.80	0.00	4082.39	0.37	1.03	0.06	4080.00
15300.	14.	15278.	9.	10.	3131.	7.	116.	24.	4080.00
0.09	1.33	4.88	1.19	0.045	0.035	0.050	0.000	4073.00	289.91
0.001657	365.	380.	380.	2	16	0	0.00	677.42	967.34
<b>*SECNO 2.000</b>									
2.00	8.62	4082.62	4081.64	0.00	4083.47	0.86	0.94	0.15	4080.00
15300.	175.	15069.	56.	62.	2015.	22.	137.	29.	4080.00
0.10	2.83	7.48	2.53	0.045	0.035	0.050	0.000	4074.00	332.74
0.005108	350.	350.	300.	2	9	0	0.00	584.14	916.88

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JTK  
6/11/87  
HM 7/17/87

SECNO	DEPTH	CWSEL	CRWS	WSELK	EQ	HV	HL	QLOSS	BANK ELEV
G	GLOB	GCH	GROB	ALOB	ACH	AROB	VOL	TWA	LEFT/RIGHT
TIME	VLOB	VCH	VRQB	XLN	XNCH	XNR	WTN	ELMIN	SSTA
SLOPE	XLOBL	XLCH	XLOBR	ITRIAL	IDC	ICONT	CDRAR	TOPWID	ENDST

CCHV= 0.300 CEHV= 0.500  
 \*SECNO 0.800  
 3280 CROSS SECTION 0.80 EXTENDED 4.21 FEET

3301 HV CHANGED MORE THAN HVINS

3370 NORMAL BRIDGE.NRD= 8 MIN ELTRD= 4096.00 MAX ELLC= 4100.00

7185 MINIMUM SPECIFIC ENERGY

3720 CRITICAL DEPTH ASSUMED

0.80	20.21	4100.21	4100.21	0.00	4102.35	2.14	2.43	0.64	4098.00
15300.	731.	8033.	6536.	108.	661.	560.	161.	35.	4098.00
0.12	6.79	12.14	11.68	0.015	0.015	0.015	0.000	4080.00	0.00
0.003320	650.	650.	400.	0	11	0	-432.00	330.00	330.00

\*SECNO 0.600  
 3280 CROSS SECTION 0.60 EXTENDED 4.16 FEET

3370 NORMAL BRIDGE.NRD= 8 MIN ELTRD= 4096.00 MAX ELLC= 4100.40

7185 MINIMUM SPECIFIC ENERGY

3720 CRITICAL DEPTH ASSUMED

0.60	20.16	4100.56	4100.56	0.00	4102.69	2.13	0.07	0.00	4098.40
15300.	679.	8328.	6293.	103.	680.	550.	161.	35.	4098.40
0.12	6.56	12.24	11.44	0.015	0.015	0.015	0.000	4080.40	0.00
0.003253	20.	20.	20.	0	11	0	-410.41	330.00	330.00

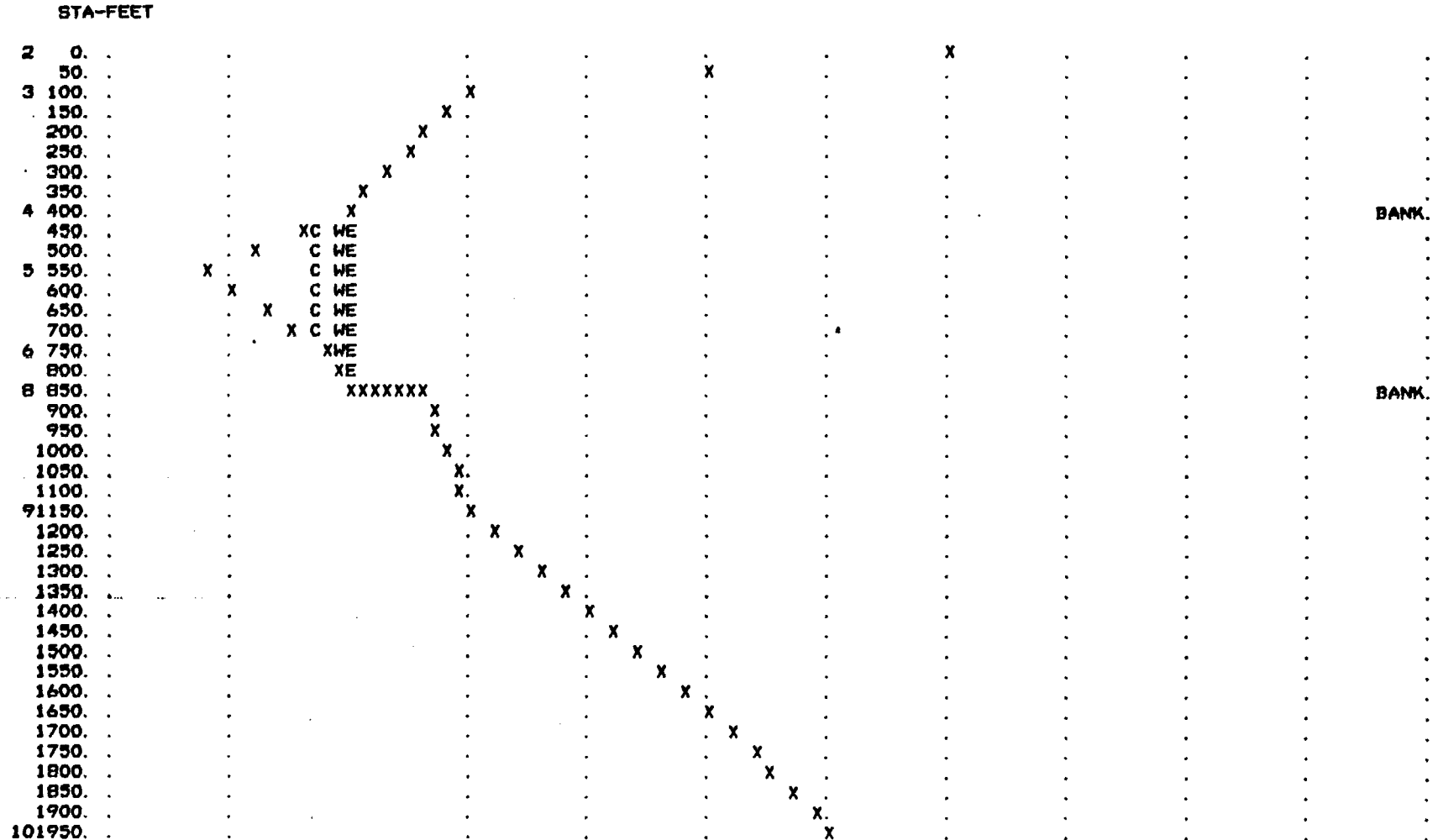
CROSS SECTION 4.00  
 STREAM DISCHARGE = 15300 CFS  
 DISCHARGE = 15300.

Sh. 33 f

PLOTTED POINTS (BY PRIORITY)-B=BOTTOM BRIDGE, T=TOP BRIDGE, X=GROUND, W=WATER SUR, E=ENERGY GRADIENT, C=CRITICAL WSEL

ELEV 4060. 4070. 4080. 4090. 4100. 4110. 4120. 4130. 4140. 4150. 4160.

FTK 6/11/87  
 MM 7/17/87



NRD= 0 ELLC= 9999999.00 ELTRD= 9999999.00

EL(I), STA(I)	4130.00	4090.00	100.00	4080.00	385.00	4068.00	530.00	4078.00	750.00
	4080.00	840.00	4086.00	870.00	4090.00	1165.00	4120.00	1930.00	

CROSS SECTION 3.00  
 STREAM DISCHARGE = 15300 CFS  
 DISCHARGE= 15300.

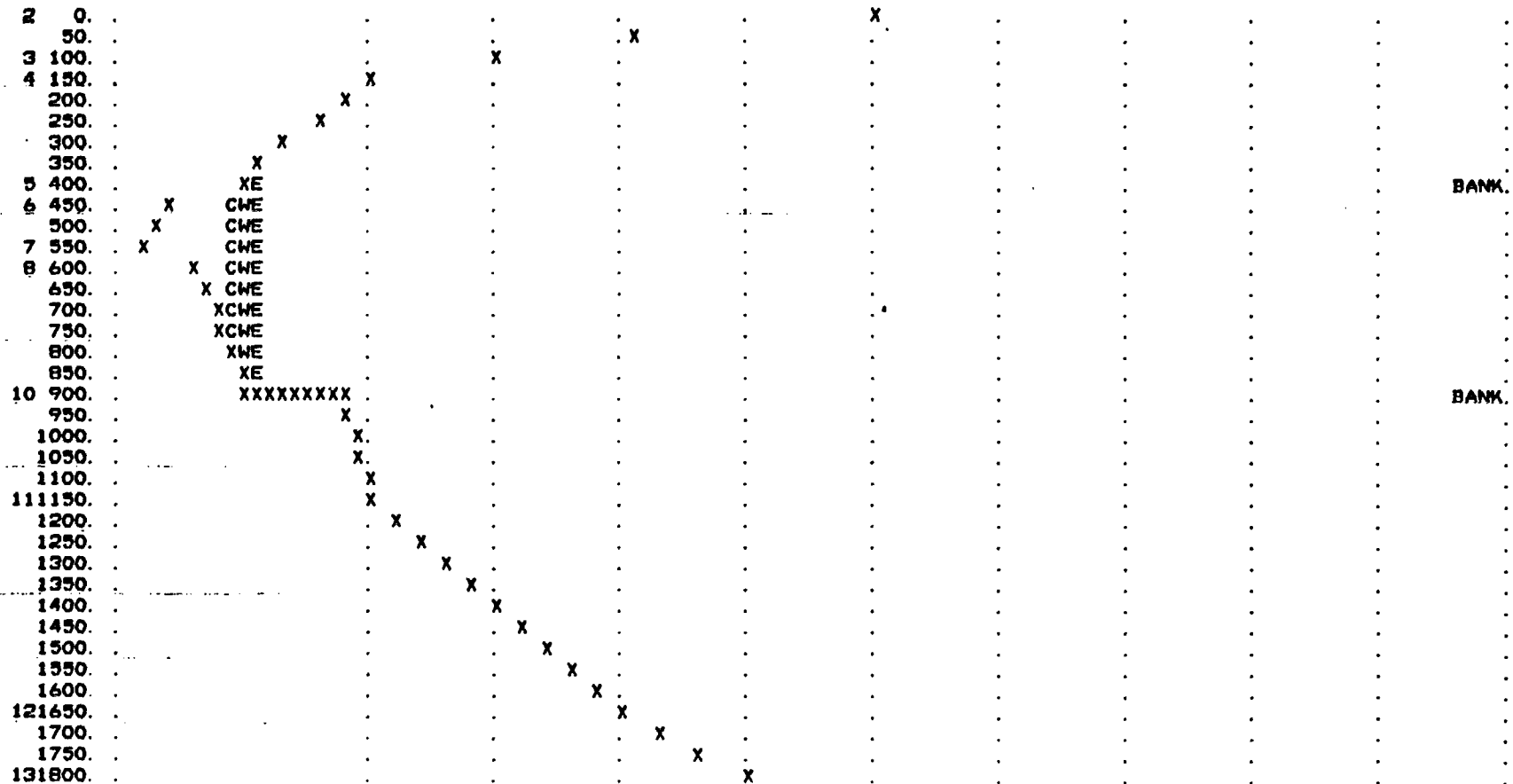
sh. 336

PLOTTED POINTS (BY PRIORITY)-B=BOTTOM BRIDGE, T=TOP BRIDGE, X=GROUND, W=WATER SUR, E=ENERGY GRADIENT, C=CRITICAL WSEL

JR 6/11/87  
 HM 7/17/87

ELEV 4070. 4080. 4090. 4100. 4110. 4120. 4130. 4140. 4150. 4160. 4170.

STA-FEET



NRD= 0 ELLC= 9999999.00 ELTRD= 9999999.00

EL(I), STA(I)

4130.00	0.00	4100.00	80.00	4090.00	170.00	4080.00	400.00	4074.00	455.00
4072.00	570.00	4076.00	620.00	4080.00	880.00	4088.00	925.00	4090.00	1150.00
4110.00	1640.00	4120.00	1820.00						



Sh. 33 H

PROFILE FOR STREAM DISCHARGE = 15300 CFS

PLOTTED POINTS (BY PRIORITY)-E-ENERGY, W-WATER SURFACE, I-INVERT, C-CRITICAL W. S., L-LEFT BANK, R-RIGHT BANK, M-LOWER END STA

JK 6/11/87  
HM 7/17/87

ELEVATION SECNO	4060. CUMDIS	4065.	4070.	4075.	4080.	4085.	4090.	4095.	4100.	4105.
6.80	0.	I			R. C W E		L			M
6.50	50.	I			R. C W E		L			M
6.00	100.	I			CL	W E				M
	150.	I			C	W E				M
	200.	I			LC	W E				M
	250.	I			L C	R W E				M
	300.	I			L C	R W E				M
	350.	I			L C	R E E				M
5.50	400.	I		L	L C	R E E				M
	450.	I		L	L C	R E E				M
	500.	I		L	L C	R E E				M
	550.	I			L C R	R E E				M
	600.	I			L C R	W E				M
5.00	650.	I			LC	W E				M
	700.	I			C	W E				M
	750.	I			CL	W E				M
	800.	I			C L W E					M
	850.	I			C L W E					M
	900.	I			C L W E					M
	950.	I			C	W E				M
	1000.	I			C	W E				M
	1050.	I			C	W E				M
4.00	1100.	I			C	W E				M
	1150.	I			C	W E				M
	1200.	I			C	W E				M
	1250.	I			C	W E				M
	1300.	I			C	W E				M
	1350.	I			C	W E				M
3.00	1400.	I			C	W E				M
	1450.	I			C	W E				M
	1500.	I			C	W E				M
	1550.	I			C	W E				M
	1600.	I			C	W E				M
	1650.	I			C	W E				M
	1700.	I			C	W E				M
	1750.	I			C	W E				M
2.50	1800.	I			C	W E				M
	1850.	I			C	W E				M
	1900.	I			LC	W E				M
	1950.	I			LC	W E				M
	2000.	I			L C	W E				M
	2050.	I			L C	W E				M
	2100.	I			L	C W E				M
2.00	2150.	I			L	C W E				M
	2200.	I			L	C W E				M
	2250.	I			L	C W E				M
	2300.	I			L	C W E				M
	2350.	I			L	C W E				M
	2400.	I			L	C W E				M



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Sh.33 J

FTK 6/11/87  
HM 7/17/87

\*\*\*\*\*  
 HEC2 RELEASE DATED NOV 76 UPDATED MAY 1984  
 ERROR CORR - 01, 02, 03, 04, 05, 06  
 MODIFICATION - 50, 51, 52, 53, 54, 55, 56  
 \*\*\*\*\*

NOTE- ASTERISK (\*) AT LEFT OF CROSS-SECTION NUMBER INDICATES MESSAGE IN SUMMARY OF ERRORS LIST

DISCHARGE = 15300 CFS

SUMMARY PRINTOUT

SECNO	Q	CWSEL	CRWS	GLOB	GCH	OROB	GLOBP	GCHP	OROBP	VLOB	VCH	VROB
6.800	15300.00	4076.53	4075.90	0.00	4357.75	10942.25	0.00	28.48	71.52	0.00	7.59	6.95
6.500	15300.00	4076.67	4076.14	0.00	4685.81	10614.19	0.00	30.63	69.37	0.00	8.31	7.32
6.000	15300.00	4077.51	4073.52	56.44	15243.56	0.00	0.37	99.63	0.00	1.33	4.12	0.00
5.500	15300.00	4077.78	4072.56	153.72	15131.33	14.95	1.00	98.90	0.10	1.50	3.13	0.56
5.000	15300.00	4077.79	4076.38	125.69	15168.60	5.70	0.82	99.14	0.04	1.80	6.27	1.53
4.000	15300.00	4079.19	4076.66	0.00	15300.00	0.00	0.00	100.00	0.00	0.00	7.11	0.00
3.000	15300.00	4080.36	4079.23	1.12	15298.63	0.24	0.01	99.99	0.00	0.76	7.80	0.67
2.500	15300.00	4082.02	4079.80	13.57	15277.64	8.79	0.09	99.85	0.06	1.33	4.88	1.19
2.000	15300.00	4082.62	4081.64	175.36	15068.67	55.98	1.15	98.49	0.37	2.83	7.48	2.53
* 0.800	15300.00	4100.21	4100.21	731.39	8032.54	6536.07	4.78	52.50	42.72	6.79	12.14	11.68
* 0.600	15300.00	4100.56	4100.56	678.74	8328.02	6293.25	4.44	54.43	41.13	6.56	12.24	11.44

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DISCHARGE = 15300 CFS

SUMMARY PRINTOUT

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JFK 6/11/87  
HM 7/17/87

SECND	KRATIO	AREA	CWSEL	ELMIN	DEPTH	DIFWSX	HV	TOPWID	SSTA	ENDST	K*CHSL	10K*5
6.800	0.00	2149.03	4076.53	4060.50	16.03	0.00	0.79	766.07	420.94	1247.35	0.00	90.36
6.500	0.93	2013.38	4076.67	4060.90	15.77	0.14	0.91	733.78	435.36	1240.23	20.00	105.56
6.000	3.67	3741.08	4077.51	4062.00	15.51	0.84	0.26	594.21	85.88	680.09	15.72	7.82
5.500	1.36	4970.57	4077.78	4062.00	15.78	0.27	0.15	769.89	149.85	919.74	0.00	4.20
5.000	0.35	2492.06	4077.79	4064.00	13.79	0.00	0.61	688.32	191.85	880.17	8.00	34.59
4.000	1.06	2152.63	4079.19	4068.00	11.19	1.41	0.78	409.11	394.71	803.82	8.70	30.69
3.000	0.77	1964.47	4080.36	4072.00	8.36	1.17	0.94	490.29	391.73	882.02	12.58	51.63
2.500	1.77	3149.01	4082.02	4073.00	9.02	1.66	0.37	677.42	289.91	967.34	2.63	16.57
2.000	0.57	2099.45	4082.62	4074.00	8.62	0.60	0.86	584.14	332.74	916.88	2.86	51.08
* 0.800	1.24	1328.64	4100.21	4080.00	20.21	17.59	2.14	330.00	0.00	330.00	9.23	33.20
* 0.600	1.01	1333.96	4100.56	4080.40	20.16	0.35	2.13	330.00	0.00	330.00	20.00	32.53

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Sh. 33 L

SUMMARY OF ERRORS AND SPECIAL NOTES

CAUTION	SECNO=	0.800	PROFILE= 1	CRITICAL DEPTH ASSUMED
CAUTION	SECNO=	0.800	PROFILE= 1	MINIMUM SPECIFIC ENERGY
CAUTION	SECNO=	0.600	PROFILE= 1	CRITICAL DEPTH ASSUMED
CAUTION	SECNO=	0.600	PROFILE= 1	MINIMUM SPECIFIC ENERGY

JFK 6/17/87  
HM 7/17/87

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Sh. 33M

\*\*\*\*\*  
HEC2 RELEASE DATED NOV 76 UPDATED MAY 1984  
ERROR CORR - 01,02,03,04,05,06  
MODIFICATION - 50,51,52,53,54,55,56  
\*\*\*\*\*

JTK 6/11/87  
HM 7/17/87

Sh. 34A

FTK 4/11/87  
HM 7/17/87

\*\*\*\*\*  
MEC2 RELEASE DATED NOV 76 UPDATED MAY 1984  
ERROR CORR - 01, 02, 03, 04, 05, 06  
MODIFICATION - 50, 51, 52, 53, 54, 55, 56  
\*\*\*\*\*

T1 UMTRA - GREEN RIVER - 10-YR 24 HR  
T2 WATER SURFACE PROFILE IN BROWN WASH  
T3 DISCHARGE = 11300 CFS

J1	ICHECK	ING	NINV	IDIR	STRT	METRIC	HVINS	Q	WSEL	FG
	0.	0.	0.	0.	0.009000	0.00	0.0	11300.	4074.000	0.000
J2	NPROF	IPL0T	PRFVS	XSECV	XSECH	FN	ALLDC	IBW	CHNIM	ITRACE
	-1.000	0.000	0.000	0.000	0.000	0.000	-1.000	0.000	0.000	0.000
J3	VARIABLE CODES FOR SUMMARY PRINTOUT									
	38.000	43.000	1.000	2.000	13.000	14.000	15.000	35.000	60.000	59.000
	55.000	26.000	56.000	0.000	38.000	58.000	25.000	1.000	42.000	8.000
	51.000	10.000	4.000	53.000	54.000	33.000	5.000	0.000	0.000	0.000

NC	0.045	0.050	0.024	0.300	0.500	0.000	0.000	0.000	0.000	0.000
X1	6.800	19.000	150.000	700.000	0.000	0.000	0.000	0.000	0.000	0.000
BT	19.000	0.000	4090.000	4090.000	80.000	4080.000	4080.000	4080.000	150.000	4082.000
BT	280.000	4080.000	4080.000	340.000	4078.000	4078.000	450.000	4076.000	4076.000	560.000
BT	4075.200	4065.500	565.000	4075.000	4070.500	570.000	4075.000	4065.500	575.000	4075.000
BT	4065.500	580.000	4075.000	4070.500	585.000	4075.000	4065.500	700.000	4074.000	4074.000
BT	800.000	4074.000	4074.000	936.000	4078.000	4078.000	950.000	4076.000	4076.000	1000.000
BT	4070.000	4070.000	1070.000	4070.000	4070.000	1885.000	4100.000	4100.000	0.000	0.000
GR	4090.000	0.000	4080.000	80.000	4082.000	150.000	4080.000	280.000	4078.000	340.000
GR	4076.000	450.000	4065.500	560.000	4060.500	565.000	4065.500	570.000	4065.500	575.000
GR	4060.500	580.000	4065.500	585.000	4074.000	700.000	4074.000	800.000	4078.000	936.000
GR	4076.000	950.000	4070.000	1000.000	4070.000	1070.000	4100.000	1885.000	0.000	0.000
X1	6.500	0.000	0.000	0.000	20.000	20.000	20.000	0.000	0.400	0.000
X2	0.000	0.000	0.000	0.000	0.000	0.000	1.000	0.000	0.000	0.000
NC	0.045	0.050	0.035	0.100	0.300	0.000	0.000	0.000	0.000	0.000
X1	6.000	9.000	180.000	890.000	70.000	70.000	70.000	0.000	0.000	0.000
GR	4090.000	0.000	4083.000	110.000	4080.000	180.000	4080.000	500.000	4062.000	540.000
GR	4074.000	685.000	4078.000	890.000	4080.000	1265.000	4100.000	1885.000	0.000	0.000

Subcritical profile  
with upstream railroad crossing  
and downstream culverts (2 functioning)  
with berm @ 4080' for sections 5-55/6-0





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sh. 34 c

SECNO	DEPTH	CWSEL	CRHS	WSELK	EG	HV	HL	CLOSS	BANK	ELEV
G	GLOB	GCH	GROB	ALOB	ACH	AROB	VOL	TWA	LEFT/RIGHT	
TIME	VLOB	VCH	VROB	XML	XNCH	XNR	WTN	ELMIN	SSTA	
SLOPE	XLOBL	XLCH	XLOBR	ITRIAL	IDC	ICQNT	CORAR	TOPWID	ENDST	

Jrk 6/11/87  
HM 7/17/87

\*PROF 1

CRITICAL DEPTH TO BE CALCULATED AT ALL CROSS SECTIONS

CCHV= 0.300 CEHV= 0.500

\*SECNO 6.800

3265 DIVIDED FLOW

3370 NORMAL BRIDGE, NRD= 19 MIN ELTRD= 4070.00 MAX ELLC= 4100.00

6.80	15.56	4076.06	4075.46	4074.00	4076.74	0.68	0.00	0.00	4082.00
11300.	0.	2307.	8993.	0.	357.	1356.	0.	0.	4074.00
0.00	0.00	6.46	6.63	0.000	0.024	0.050	0.000	4060.50	446.46
0.009008	0.	0.	0.	0	14	4	-1267.76	708.94	1234.75

\*SECNO 6.500

3265 DIVIDED FLOW

3370 NORMAL BRIDGE, NRD= 19 MIN ELTRD= 4070.00 MAX ELLC= 4100.40

6.50	15.31	4076.21	4075.78	0.00	4076.99	0.78	0.20	0.05	4082.40
11300.	0.	2540.	8760.	0.	349.	1241.	1.	0.	4074.40
0.00	0.00	7.27	7.06	0.000	0.024	0.050	0.000	4060.90	452.03
0.010704	20.	20.	20.	2	14	0	-1211.22	685.52	1227.74

CCHV= 0.100 CEHV= 0.300

\*SECNO 6.000

6.00	14.62	4076.62	4072.91	0.00	4077.34	0.72	0.34	0.01	4080.00
11300.	0.	11300.	0.	0.	1665.	0.	3.	1.	4078.00
0.00	0.00	6.79	0.00	0.000	0.035	0.000	0.000	4062.00	507.50
0.002783	70.	70.	70.	2	20	0	0.00	312.10	819.59

\*SECNO 5.500

5.50	15.48	4077.48	4073.65	0.00	4077.92	0.44	0.55	0.03	4080.00
11300.	0.	11283.	17.	0.	2123.	18.	15.	3.	4076.00
0.02	0.00	5.32	0.96	0.000	0.035	0.050	0.000	4062.00	518.40
0.001551	150.	270.	280.	2	12	0	0.00	396.24	914.65

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JK 6/11/87  
HM 7/17/87

SECNO Q TIME SLOPE	DEPTH GLOB VLOB XLOBL	CWSEL GCH VCH XLCH	CRISW GROB VROB XLOBR	WSELK ALOB XNL ITRIAL	EG ACH XNCH IDC	HV AROB XNR ICONT	HL VOL WTN CORAR	QLOSS TWA ELMIN TOPWID	BANK LEFT/RIGHT SSTA ENDST	ELEV
CCHV= 0.200 CEHV= 0.500										
*SECNO 5.000										
5.00	14.04	4078.04	4075.34	0.00	4078.33	0.29	0.39	0.03	4076.00	
11300.	118.	11170.	12.	90.	2569.	10.	29.	6.	4076.00	
0.03	1.31	4.35	1.16	0.045	0.035	0.050	0.000	4064.00	181.02	
0.001535	230.	250.	290.	0	14	0	0.00	704.75	885.76	
*SECNO 4.000										
4.00	10.74	4078.74	4075.69	0.00	4079.25	0.51	0.81	0.11	4080.00	
11300.	0.	11300.	0.	0.	1974.	0.	53.	12.	4080.00	
0.06	0.00	5.72	0.00	0.000	0.035	0.000	0.000	4068.00	400.17	
0.002049	470.	460.	440.	0	11	0	0.00	383.35	783.52	
*SECNO 3.000										
3.00	7.59	4079.59	4078.40	0.00	4080.36	0.78	0.98	0.13	4080.00	
11300.	0.	11300.	0.	0.	1599.	0.	67.	15.	4080.00	
0.07	0.00	7.07	0.00	0.000	0.035	0.000	0.000	4072.00	403.77	
0.005110	315.	318.	320.	2	14	0	0.00	449.51	853.28	
CCHV= 0.100 CEHV= 0.300										
*SECNO 2.500										
2.50	8.17	4081.17	4079.32	0.00	4081.47	0.30	1.06	0.05	4080.00	
11300.	3.	11295.	2.	3.	2570.	2.	85.	20.	4080.00	
0.09	0.95	4.39	0.85	0.045	0.035	0.050	0.000	4073.00	294.17	
0.001750	365.	380.	380.	2	10	0	0.00	670.08	964.24	
*SECNO 2.000										
2.00	7.88	4081.88	4081.10	0.00	4082.61	0.72	1.01	0.13	4080.00	
11300.	77.	11198.	25.	32.	1632.	11.	102.	25.	4080.00	
0.11	2.40	6.86	2.14	0.045	0.035	0.050	0.000	4074.00	345.99	
0.005693	350.	350.	300.	2	9	0	0.00	566.16	912.15	
CCHV= 0.300 CEHV= 0.500										
*SECNO 0.800										
3280 CROSS SECTION		0.80 EXTENDED		3.41 FEET						

sh. 34 E

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JK 6/11/87  
HM 7/17/87

SECNO	DEPTH	CWSEL	CRWS	WSELK	EO	HV	HL	DLOSS	BANK ELEV
G	GLOB	GCH	GROB	ALOB	ACH	AROB	VOL	TWA	LEFT/RIGHT
TIME	VLOB	VCH	VRGB	XML	XNCH	XNR	WTN	ELMIN	SSTA
SLOPE	XLOBL	XLCH	XLOBR	ITRIAL	IDC	ICONT	CRAR	TOPWID	ENDST

3301 HV CHANGED MORE THAN HVINS

3370 NORMAL BRIDGE, NRD= B MIN ELTRD= 4096.00 MAX ELLC= 4100.00

7185 MINIMUM SPECIFIC ENERGY

3720 CRITICAL DEPTH ASSUMED

0.80	19.41	4099.41	4099.41	0.00	4101.23	1.82	2.58	0.55	4098.00
11300.	231.	7156.	3913.	47.	618.	408.	121.	31.	4098.00
0.12	4.92	11.59	9.58	0.015	0.015	0.015	0.000	4080.00	23.52
0.003311	650.	650.	400.	0	10	0	-432.00	306.49	330.00

\*SECNO 0.600

3280 CROSS SECTION 0.60 EXTENDED 3.38 FEET

3370 NORMAL BRIDGE, NRD= B MIN ELTRD= 4096.00 MAX ELLC= 4100.40

7185 MINIMUM SPECIFIC ENERGY

3720 CRITICAL DEPTH ASSUMED

0.60	19.38	4099.78	4099.78	0.00	4101.57	1.80	0.06	0.01	4098.40
11300.	212.	7365.	3723.	45.	637.	402.	122.	31.	4098.40
0.12	4.73	11.56	9.27	0.015	0.015	0.015	0.000	4080.40	24.94
0.003163	20.	20.	20.	0	10	0	-410.41	305.06	330.00

CROSS SECTION 4.00  
 STREAM DISCHARGE = 11300 CFS  
 DISCHARGE = 11300.

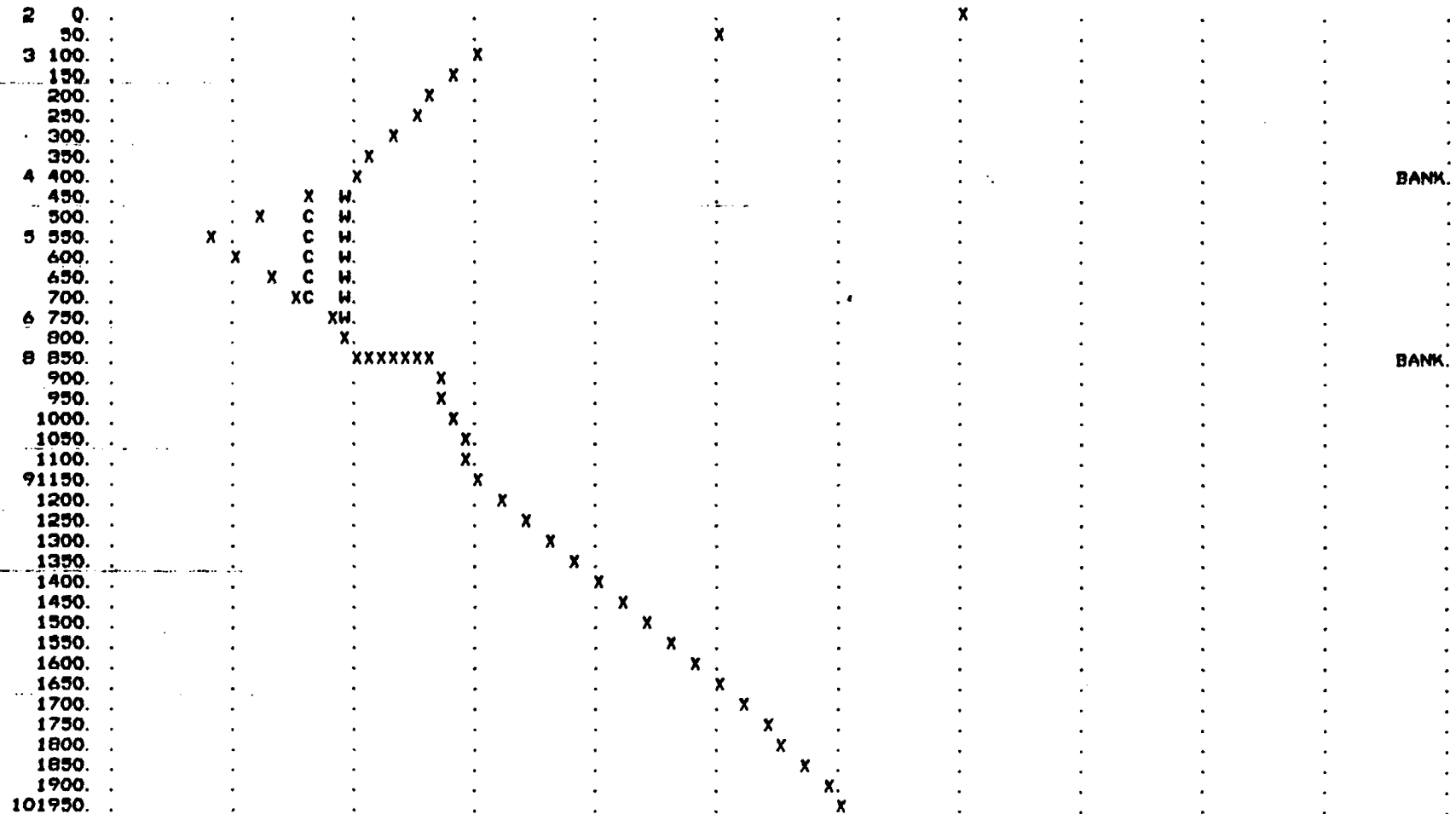
Sh. 34 F

PLOTTED POINTS (BY PRIORITY)-B=BOTTOM BRIDGE, T=TOP BRIDGE, X=GROUND, W=WATER SUR, E=ENERGY GRADIENT, C=CRITICAL WSEL

JTK 6/11/87  
 HM 7/17/87

ELEV 4060. 4070. 4080. 4090. 4100. 4110. 4120. 4130. 4140. 4150. 4160.

STA-FEET



NRD= 0 ELLC= 9999999.00 ELTRD= 9999999.00

EL(I), STA(I)

4130.00	0.00	4090.00	100.00	4080.00	385.00	4068.00	530.00	4078.00	750.00
4080.00	840.00	4086.00	870.00	4090.00	1165.00	4120.00	1930.00		

Sh. 34 G

JK 6/11/87

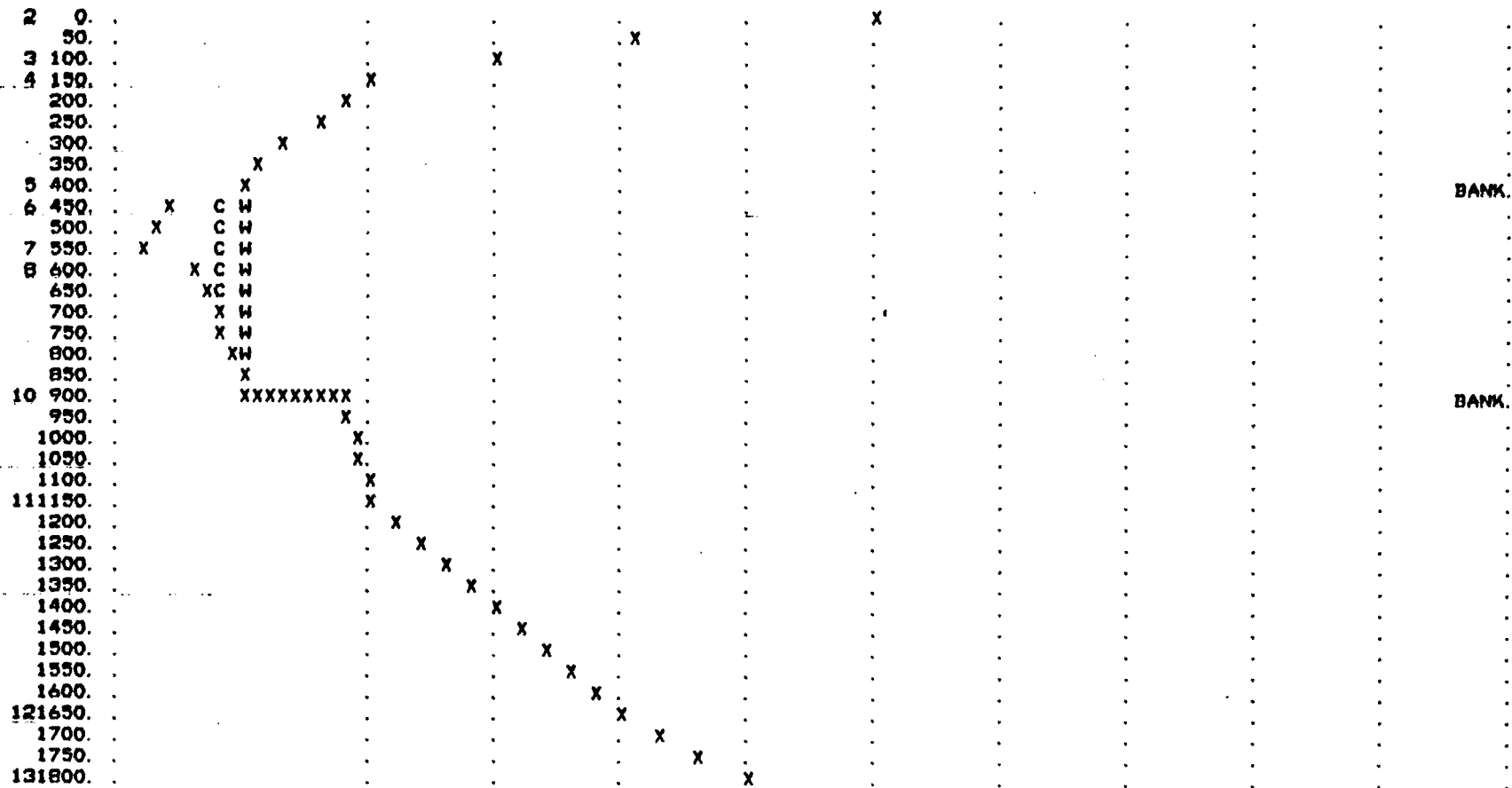
HM 7/17/87

CROSS SECTION 3.00  
 STREAM DISCHARGE = 11300 CFS  
 DISCHARGE = 11300.

PLOTTED POINTS (BY PRIORITY)-B=BOTTOM BRIDGE, T=TOP BRIDGE, X=GROUND, W=WATER SUR, E=ENERGY GRADIENT, C=CRITICAL WSEL

ELEV 4070. 4080. 4090. 4100. 4110. 4120. 4130. 4140. 4150. 4160. 4170.

STA-FEET



NRD= 0 ELLC= 9999999.00. ELTRD= 9999999.00

EL(I), STA(I)

4130.00	0.00	4100.00	80.00	4090.00	170.00	4080.00	400.00	4074.00	455.00
4072.00	570.00	4076.00	620.00	4080.00	880.00	4088.00	925.00	4090.00	1150.00
4110.00	1640.00	4120.00	1820.00						

PROFILE FOR STREAM DISCHARGE = 11300 CFS

sh. 84H

PLOTTED POINTS (BY PRIORITY)-E-ENERGY, W-WATER SURFACE, I-INVERT, C-CRITICAL W. S., L-LEFT BANK, R-RIGHT BANK, M-LOWER END STA

JFK 6/11/87  
HM 7/17/87

ELEVATION SECNO	4060. CUMDIS	4065.	4070.	4075.	4080.	4085.	4090.	4095.	4100.	4105.
6.80	0.	I			R . CWE		L			M
6.50	50.	I			R . WE		L			M
6.00	100.	I			C . W ER		L			M
	150.	I			C . WE		L			M
	200.	I			C . WE		L			M
	250.	I			C . WE		L			M
	300.	I			C C . R WE		L			M
	350.	I			C C . R WE		L			M
5.50	400.	I			C C . R WE		L			M
	450.	I			C . R WE L					M
	500.	I			C . R WE L					M
	550.	I			C . R LE					M
	600.	I			C . R LE					M
5.00	650.	I			.CL WE					M
	700.	I			.C L WE					M
	750.	I			.C L WE					M
	800.	I			.C L E					M
	850.	I			.C L E					M
	900.	I			.C L WE					M
	950.	I			.C WE					M
	1000.	I			.C WE					M
	1050.	I			.C WEL					M
4.00	1100.	I			.C WEL					M
	1150.	I			.C WEL					M
	1200.	I			.C WEL					M
	1250.	I			.C WE					M
	1300.	I			.C WE					M
	1350.	I			.C WE					M
3.00	1400.	I			.C WLE					M
	1450.	I			.C WE					M
	1500.	I			.C WE					M
	1550.	I			.C WE					M
	1600.	I			.C LWE					M
	1650.	I			.C LWE					M
	1700.	I			.C L E					M
	1750.	I			.C L WE					M
2.50	1800.	I			.CL WE					M
	1850.	I			.CL E					M
	1900.	I			.C WE					M
	1950.	I			.C WE					M
	2000.	I			.LC WE					M
	2050.	I			.LC WE					M
	2100.	I			.L C WE					M
2.00	2150.	I			.L C WE					M
	2200.	I			.L CW E					M
	2250.	I			.L CW E					M
	2300.	I			.L CW E					M
	2350.	I			.L C WE					M
	2400.	I			.L C WE					M



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Sh. 34 J

\*\*\*\*\*  
HEC2 RELEASE DATED NOV 76 UPDATED MAY 1984  
ERROR CORR - 01, 02, 03, 04, 05, 06  
MODIFICATION - 50, 51, 52, 53, 54, 55, 56  
\*\*\*\*\*

JTK 6/11/87  
HM 7/17/87

NOTE- ASTERISK (\*) AT LEFT OF CROSS-SECTION NUMBER INDICATES MESSAGE IN SUMMARY OF ERRORS LIST

DISCHARGE = 11300 CFS

SUMMARY PRINTOUT

SECNO	Q	CWSEL	CRWS	GLOB	GCH	GRDB	GLOBR	GCHP	GRDBP	VLOB	VCH	VROB
6.800	11300.00	4076.06	4075.46	0.00	2306.61	8993.39	0.00	20.41	79.59	0.00	6.46	6.63
6.500	11300.00	4076.21	4075.78	0.00	2540.02	8759.98	0.00	22.48	77.52	0.00	7.27	7.06
6.000	11300.00	4076.62	4072.91	0.00	11300.00	0.00	0.00	100.00	0.00	0.00	6.79	0.00
5.500	11300.00	4077.48	4073.65	0.00	11282.59	17.41	0.00	99.85	0.15	0.00	5.32	0.96
5.000	11300.00	4078.04	4075.34	118.35	11170.12	11.52	1.05	98.85	0.10	1.31	4.35	1.16
4.000	11300.00	4078.74	4075.69	0.00	11300.00	0.00	0.00	100.00	0.00	0.00	5.72	0.00
3.000	11300.00	4079.59	4078.40	0.00	11300.00	0.00	0.00	100.00	0.00	0.00	7.07	0.00
2.500	11300.00	4081.17	4079.32	3.24	11294.67	2.10	0.03	99.95	0.02	0.95	4.39	0.85
2.000	11300.00	4081.88	4081.10	76.98	11198.45	24.57	0.68	99.10	0.22	2.40	6.86	2.14
* 0.800	11300.00	4099.41	4099.41	230.87	7155.75	3913.39	2.04	63.33	34.63	4.92	11.59	9.58
* 0.600	11300.00	4099.78	4099.78	211.88	7364.91	3723.21	1.88	65.18	32.95	4.73	11.56	9.27



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DISCHARGE = 11300 CFS

SUMMARY PRINTOUT

SECND	KRATIO	AREA	CWSEL	ELMIN	DEPTH	DIFWSX	HV	TOPWID	SSTA	ENDST	K*CHSL	10X*8
6.800	0.00	1713.43	4076.06	4060.50	15.56	0.00	0.68	708.94	446.46	1234.75	0.00	90.08
6.500	0.92	1590.26	4076.21	4060.90	15.31	0.14	0.78	685.52	452.03	1227.74	20.00	107.04
6.000	1.96	1665.21	4076.62	4062.00	14.62	0.42	0.72	312.10	507.50	819.59	15.72	27.83
5.500	1.34	2140.74	4077.48	4062.00	15.48	0.85	0.44	396.24	518.40	914.65	0.00	15.51
5.000	1.01	2668.98	4078.04	4064.00	14.04	0.56	0.29	704.75	181.02	885.76	8.00	15.35
4.000	0.87	1973.86	4078.74	4068.00	10.74	0.70	0.51	383.35	400.17	783.52	8.70	20.49
3.000	0.63	1598.92	4079.59	4072.00	7.59	0.84	0.78	449.51	403.77	853.28	12.58	51.10
2.500	1.71	2575.93	4081.17	4073.00	8.17	1.58	0.30	670.08	294.17	964.24	2.63	17.50
2.000	0.55	1676.09	4081.88	4074.00	7.88	0.72	0.72	566.16	345.99	912.15	2.86	56.93
* 0.800	1.31	1072.91	4099.41	4080.00	19.41	17.53	1.82	306.49	23.52	330.00	9.23	33.11
* 0.600	1.02	1083.59	4099.78	4080.40	19.38	0.36	1.80	305.06	24.94	330.00	20.00	31.63

Sh. 34 K

JFK 6/11/87  
HM 7/17/87

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SUMMARY OF ERRORS AND SPECIAL NOTES

CAUTION SECNO= 0.800 PROFILE= 1 CRITICAL DEPTH ASSUMED  
CAUTION SECNO= 0.800 PROFILE= 1 MINIMUM SPECIFIC ENERGY

CAUTION SECNO= 0.600 PROFILE= 1 CRITICAL DEPTH ASSUMED  
CAUTION SECNO= 0.600 PROFILE= 1 MINIMUM SPECIFIC ENERGY

sh. 34 L

JTK 6/11/87  
HM 7/17/87

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Sh. 34M

\*\*\*\*\*  
HEGZ RELEASE DATED NOV 76 UPDATED MAY 1984  
ERROR CORR - 01, 02, 03, 04, 05, 06  
MODIFICATION - 50, 51, 52, 53, 54, 55, 56  
\*\*\*\*\*

JTC 6/11/87  
HM 7/17/87

\*\*\*\*\*  
 HEC2 RELEASE DATED NOV 76 UPDATED MAY 1984  
 ERROR CORR - 01, 02, 03, 04, 05, 06  
 MODIFICATION - 50, 51, 52, 53, 54, 55, 56  
 \*\*\*\*\*

JTK 6/11/87  
 HM 7/17/87

T1 UMTRA - GREEN RIVER - 25-YR 24 HR  
 T2 WATER SURFACE PROFILE IN BROWN WASH  
 T3 DISCHARGE = 15300 CFS

J1	ICHECK	ING	NINV	IDIR	STRT	METRIC	HVINS	Q	WSEL	FG
	0.	0.	0.	0.	0.009000	0.00	0.0	15300.	4074.000	0.000
J2	NPROF	IPLOT	PRFVS	XSECV	XSECH	FN	ALLDC	IBW	CHNIM	ITRACE
	-1.000	0.000	0.000	0.000	0.000	0.000	-1.000	0.000	0.000	0.000

J3 VARIABLE CODES FOR SUMMARY PRINTOUT

	38.000	43.000	1.000	2.000	13.000	14.000	15.000	35.000	60.000	59.000
	55.000	26.000	56.000	0.000	38.000	58.000	25.000	1.000	42.000	8.000
	51.000	10.000	4.000	53.000	54.000	33.000	5.000	0.000	0.000	0.000

NC	0.045	0.050	0.024	0.300	0.500	0.000	0.000	0.000	0.000	0.000	0.000
X1	6.800	19.000	150.000	700.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
BT	19.000	0.000	4090.000	4090.000	80.000	4080.000	4080.000	4080.000	150.000	4082.000	4082.000
BT	280.000	4080.000	4080.000	340.000	4078.000	4078.000	450.000	4076.000	4076.000	4076.000	560.000
BT	4075.200	4065.500	565.000	4075.000	4070.500	570.000	4075.000	4065.500	575.000	4075.000	4075.000
BT	4065.500	580.000	4075.000	4070.500	585.000	4075.000	4065.500	700.000	4074.000	4074.000	4074.000
BT	800.000	4074.000	4074.000	936.000	4078.000	4078.000	950.000	4076.000	4076.000	4076.000	1000.000
BT	4070.000	4070.000	1070.000	4070.000	4070.000	1885.000	4100.000	4100.000	0.000	0.000	0.000
QR	4090.000	0.000	4080.000	80.000	4082.000	150.000	4080.000	280.000	4078.000	4078.000	340.000
QR	4076.000	450.000	4065.500	560.000	4060.500	565.000	4065.500	570.000	4065.500	4065.500	575.000
QR	4060.500	580.000	4065.500	585.000	4074.000	700.000	4074.000	800.000	4078.000	4078.000	936.000
QR	4076.000	950.000	4070.000	1000.000	4070.000	1070.000	4100.000	1885.000	0.000	0.000	0.000
X1	6.500	0.000	0.000	0.000	20.000	20.000	20.000	0.000	0.000	0.400	0.000
X2	0.000	0.000	0.000	0.000	0.000	0.000	1.000	0.000	0.000	0.000	0.000
NC	0.045	0.050	0.035	0.100	0.300	0.000	0.000	0.000	0.000	0.000	0.000
X1	6.000	9.000	180.000	890.000	70.000	70.000	70.000	0.000	0.000	0.000	0.000
QR	4090.000	0.000	4083.000	110.000	4080.000	180.000	4080.000	500.000	4062.000	4062.000	540.000
QR	4074.000	685.000	4078.000	890.000	4080.000	1265.000	4100.000	1885.000	0.000	0.000	0.000



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sh. 35c

JFK 6/11/87  
MM 7/17/87

SECNO	DEPTH	CWSEL	CRWS	WSELK	EQ	HV	HL	QLOSS	BANK	ELEV
G	GLOB	GCH	GROB	ALOB	ACH	AROB	VOL	TWA	LEFT/RIGHT	
TIME	VLOB	VCH	VROB	XML	XNCH	XNR	WTN	ELMIN	SSTA	
SLOPE	XLOBL	XLCH	XLOBR	ITRIAL	IDC	ICONT	CORAR	TOPWID	ENDST	

\*PROF 1

CRITICAL DEPTH TO BE CALCULATED AT ALL CROSS SECTIONS

CCHV= 0.300 CEHV= 0.500

\*SECNO 6.800

3265 DIVIDED FLOW

3370 NORMAL BRIDGE, NRD= 19 MIN ELTRD= 4070.00 MAX ELLC= 4100.00

6.80	16.13	4076.63	4076.01	4074.00	4077.43	0.80	0.00	0.00	4082.00
15300.	0.	3907.	11393.	0.	508.	1622.	0.	0.	4074.00
0.00	0.00	7.69	7.02	0.000	0.024	0.050	0.000	4060.50	415.60
0.009061	0.	0.	0.	0	17	5	-1267.76	778.04	1249.99

\*SECNO 6.500

3265 DIVIDED FLOW

3370 NORMAL BRIDGE, NRD= 19 MIN ELTRD= 4070.00 MAX ELLC= 4100.40

6.50	15.86	4076.76	4076.30	0.00	4077.69	0.93	0.20	0.06	4082.40
15300.	0.	4129.	11171.	0.	489.	1494.	1.	0.	4074.40
0.00	0.00	8.44	7.48	0.000	0.024	0.050	0.000	4060.90	430.22
0.010814	20.	20.	20.	2	17	0	-1212.77	745.29	1242.77

CCHV= 0.100 CEHV= 0.300

\*SECNO 6.000

6.00	15.09	4077.09	4074.57	0.00	4078.19	1.10	0.45	0.05	4080.00
15300.	0.	15300.	0.	0.	1816.	0.	4.	1.	4078.00
0.00	0.00	8.42	0.00	0.000	0.035	0.000	0.000	4062.00	506.46
0.004227	70.	70.	70.	2	12	0	0.00	336.99	843.45

\*SECNO 5.500

3301 HV CHANGED MORE THAN HVINS

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Sh. 35 D

SECNO Q TIME SLOPE	DEPTH GLOB VLOB XLOBL	CWSEL GCH VCH XLCH	CRISW GROB VROB XLOBR	WSELK ALOB XNL ITRIAL	EQ ACH XNCH IDC	HV AROB XNR ICONT	HL VDL WTN CORAR	CLOSS TWA ELMIN TOPWID	BANK ELEV LEFT/RIGHT SSTA ENDST
5.50	16.35	4078.35	4075.14	0.00	4078.95	0.60	0.71	0.05	4080.00
15300.	0.	15236.	64.	0.	2447.	46.	17.	4.	4076.00
0.02	0.00	6.23	1.39	0.000	0.035	0.050	0.000	4062.00	515.50
0.001779	150.	270.	280.	2	9	0	0.00	413.64	929.15
CCHV= 0.200		CEHV= 0.500							
*SECNO 5.000									
5.00	15.05	4079.05	4076.48	0.00	4079.38	0.33	0.38	0.05	4076.00
15300.	326.	14942.	32.	203.	3184.	22.	34.	7.	4076.00
0.03	1.60	4.69	1.42	0.045	0.035	0.050	0.000	4064.00	136.57
0.001342	230.	250.	290.	2	17	0	0.00	754.07	890.64
*SECNO 4.000									
4.00	11.71	4079.71	4076.71	0.00	4080.36	0.65	0.81	0.16	4080.00
15300.	0.	15300.	0.	0.	2370.	0.	65.	13.	4080.00
0.05	0.00	6.46	0.00	0.000	0.035	0.000	0.000	4068.00	388.53
0.002443	470.	460.	440.	2	11	0	0.00	438.33	826.86
*SECNO 3.000									
3.00	8.62	4080.62	4079.22	0.00	4081.45	0.83	1.00	0.09	4080.00
15300.	4.	15295.	1.	4.	2086.	1.	81.	17.	4080.00
0.06	0.98	7.33	0.87	0.045	0.035	0.050	0.000	4072.00	385.82
0.004211	315.	318.	320.	2	14	0	0.00	497.65	883.47
CCHV= 0.100		CEHV= 0.300							
*SECNO 2.500									
2.50	9.07	4082.07	4079.80	0.00	4082.43	0.36	0.93	0.05	4080.00
15300.	14.	15277.	9.	11.	3164.	8.	104.	22.	4080.00
0.08	1.33	4.83	1.19	0.045	0.035	0.050	0.000	4073.00	289.67
0.001600	365.	380.	380.	2	16	0	0.00	677.85	967.52
*SECNO 2.000									
2.00	8.64	4082.64	4081.66	0.00	4083.49	0.85	0.91	0.15	4080.00
15300.	177.	15066.	57.	63.	2026.	23.	125.	27.	4080.00
0.10	2.82	7.44	2.52	0.045	0.035	0.050	0.000	4074.00	332.36
0.005014	350.	350.	300.	2	9	0	0.00	584.66	917.01

JTK 6/11/87  
MM 7/17/87

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Sh. 35 E

JTIL 6/11/87  
HM 7/17/87

SECNO	DEPTH	CWSEL	CRISW	WSELK	E0	HV	HL	GLOSS	BANK ELEV
G	GLOB	GCH	GROB	ALOB	ACH	AROB	VOL	TWA	LEFT/RIGHT
TIME	VLOB	VCH	VROB	XLN	XLNCH	XNR	WTN	ELMIN	SSTA
SLOPE	XLOBL	XLCH	XLOBR	ITRIAL	IDC	ICONT	CORAR	TOPWID	ENDST

CCHV= 0.300 CEHV= 0.500  
 \*SECNO 0.800  
 3280 CROSS SECTION 0.80 EXTENDED 4.21 FEET

3301 HV CHANGED MORE THAN HVINS

3370 NORMAL BRIDGE.NRD= 8 MIN ELTRD= 4096.00 MAX ELLC= 4100.00

7185 MINIMUM SPECIFIC ENERGY

3720 CRITICAL DEPTH ASSUMED									
0.80	20.21	4100.21	4100.21	0.00	4102.35	2.14	2.41	0.65	4098.00
15300.	731.	8033.	6536.	108.	661.	560.	149.	33.	4098.00
0.11	6.79	12.14	11.68	0.015	0.015	0.015	0.000	4080.00	0.00
0.003320	650.	650.	400.	0	11	0	-432.00	330.00	330.00

\*SECNO 0.600  
 3280 CROSS SECTION 0.60 EXTENDED 4.16 FEET

3370 NORMAL BRIDGE.NRD= 8 MIN ELTRD= 4096.00 MAX ELLC= 4100.40

7185 MINIMUM SPECIFIC ENERGY

3720 CRITICAL DEPTH ASSUMED									
0.60	20.16	4100.56	4100.56	0.00	4102.69	2.13	0.07	0.00	4098.40
15300.	679.	8328.	6293.	103.	680.	550.	150.	33.	4098.40
0.11	6.56	12.24	11.44	0.015	0.015	0.015	0.000	4080.40	0.00
0.003253	20.	20.	20.	0	11	0	-410.41	330.00	330.00



CROSS SECTION 4.00  
 STREAM DISCHARGE = 15300 CFS  
 DISCHARGE= 15300.

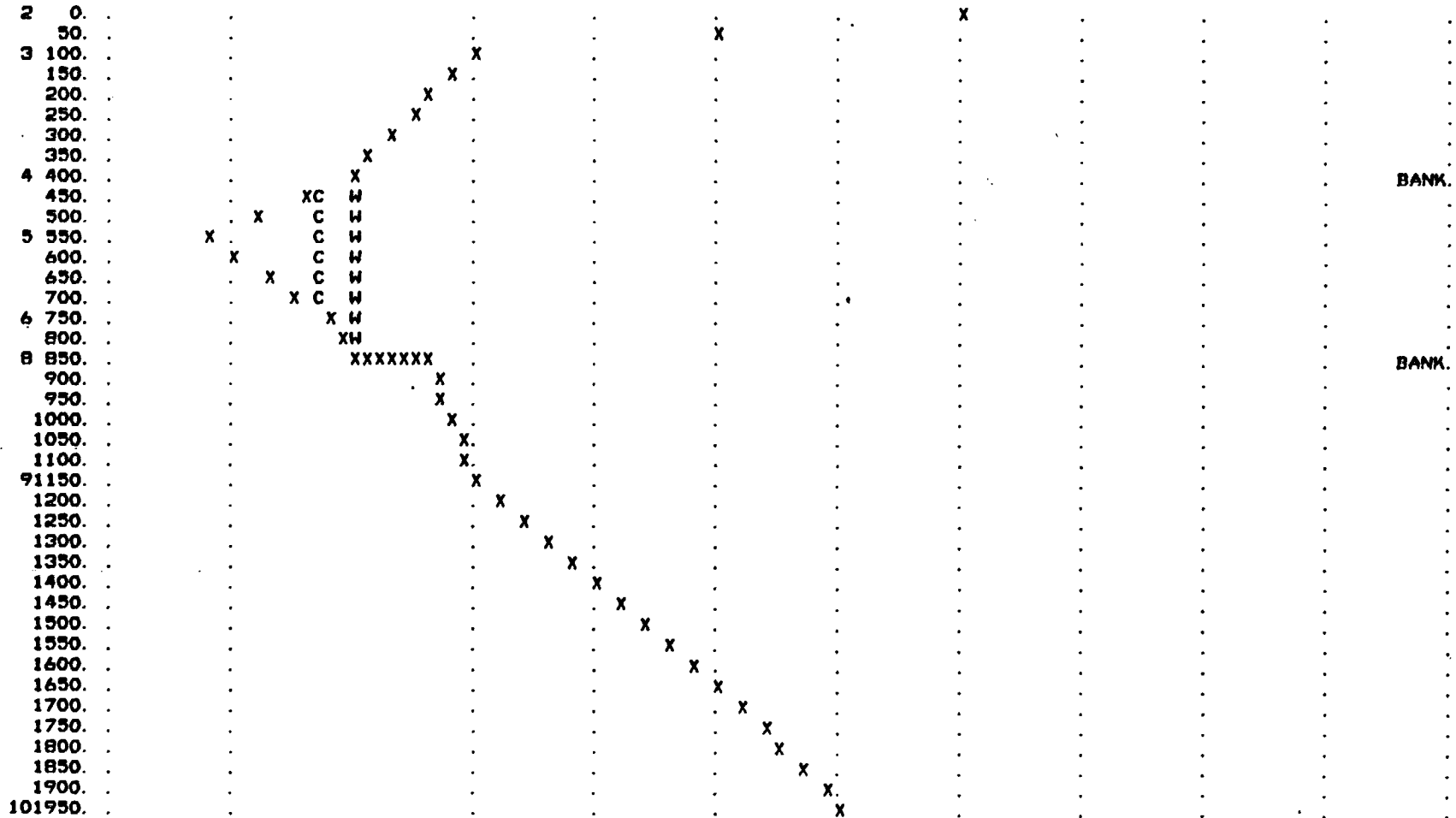
sh. 35 F

JFK 6/11/87  
 HM 7/11/87

PLOTTED POINTS (BY PRIORITY)-B=BOTTOM BRIDGE, T=TOP BRIDGE, X=GROUND, W=WATER SUR, E=ENERGY GRADIENT, C=CRITICAL WSEL

ELEV 4060. 4070. 4080. 4090. 4100. 4110. 4120. 4130. 4140. 4150. 4160.

STA- FEET



NRD= 0 ELLC= 9999999.00 ELTRD= 9999999.00

EL(I), STA(I)

4130.00	0.00	4090.00	100.00	4080.00	385.00	4068.00	530.00	4078.00	750.00
4080.00	840.00	4086.00	870.00	4090.00	1165.00	4120.00	1930.00		

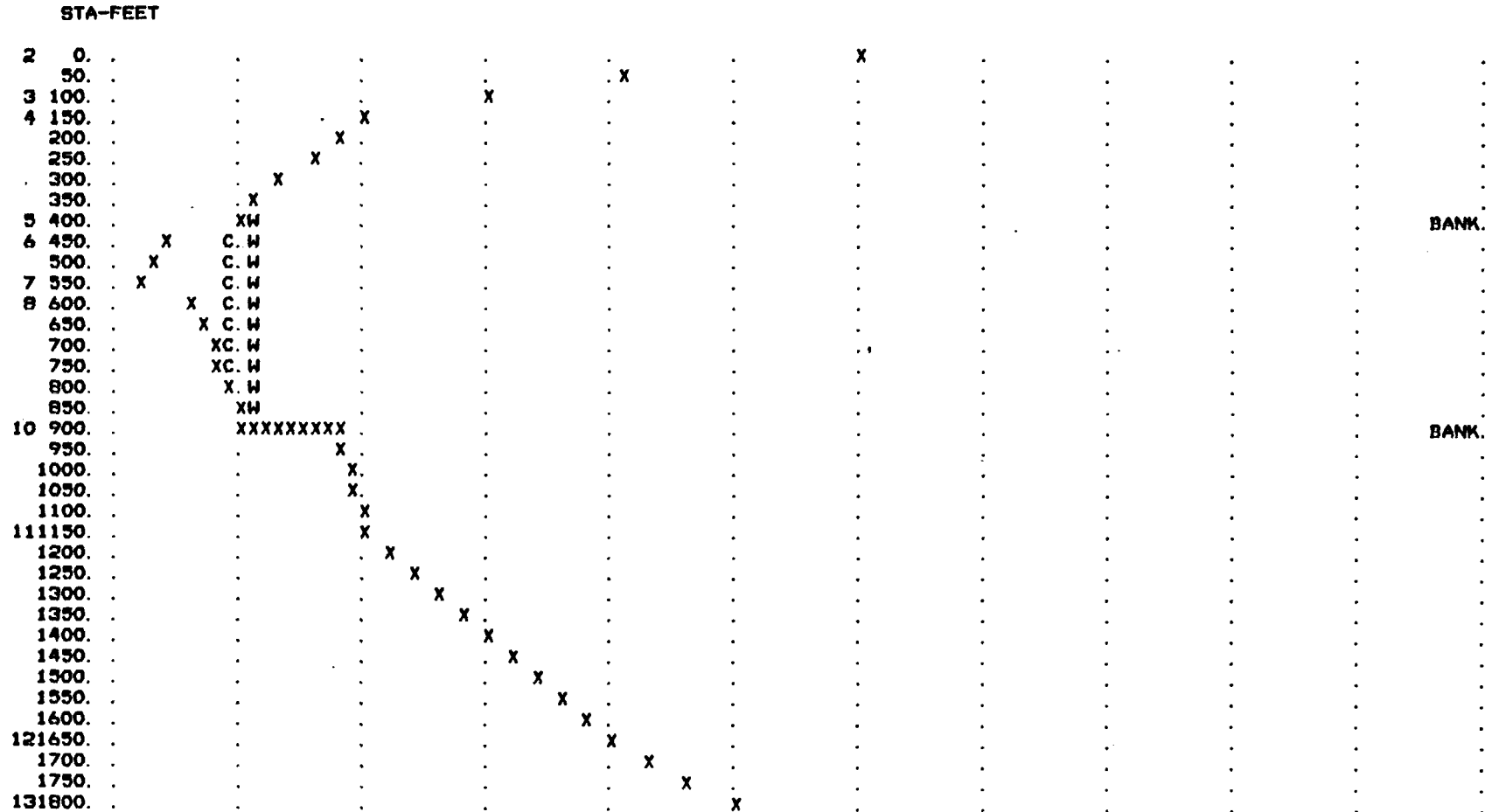
CROSS SECTION 3.00  
 STREAM DISCHARGE = 15300 CFS  
 DISCHARGE = 15300.

Sh. 35G

PLOTTED POINTS (BY PRIORITY)-B=BOTTOM BRIDGE, T=TOP BRIDGE, X=GROUND, W=WATER SUR, E=ENERGY GRADIENT, C=CRITICAL WSEL

Flw 6/11/87  
 11m 7/17/87

ELEV 4070. 4080. 4090. 4100. 4110. 4120. 4130. 4140. 4150. 4160. 4170.



NRD= 0 ELLC= 9999999.00 ELTRD= 9999999.00

EL(I), STA(I)

4130.00	0.00	4100.00	80.00	4090.00	170.00	4080.00	400.00	4074.00	455.00
4072.00	570.00	4076.00	620.00	4080.00	880.00	4088.00	925.00	4090.00	1150.00
4110.00	1640.00	4120.00	1820.00						

Sh. 35 H

PROFILE FOR STREAM DISCHARGE = 15300 CFS

JFK 6/11/87  
HM 7/17/87

PLOTTED POINTS (BY PRIORITY)-E-ENERGY, W-WATER SURFACE, I-INVERT, C-CRITICAL W. S., L-LEFT BANK, R-RIGHT BANK, M-LOWER END STA

ELEVATION SECND	4060. CUMDIS	4065.	4070.	4075.	4080.	4085.	4090.	4095.	4100.	4105.
6.80	0.	I			R. CHE		L			M
6.50	50.	I			R. CHE		L			M
6.00	100.				C. WE	L				M
	150.	I			C. WE	L				M
	200.	I			C. WE	L				M
	250.	I			C. R WE	L				M
	300.	I			C R WE	L				M
	350.	I			CR WE	L				M
5.50	400.	I			CR WE	L				M
	450.	I			CR WE			M		
	500.	I			CR WE			M		
	550.	I			C L E			M		
	600.	I			C L WE			M		
5.00	650.	I			LC WE			M		
	700.	I			C L WE				M	
	750.	I			CL WE				M	
	800.	I			CL E					M
	850.	I			CL WE					M
	900.	I			C L WE					M
	950.	I			C L WE					M
	1000.	I			C L WE					M
4.00	1050.	I			C WE					M
	1100.	I			C WE					M
	1150.	I			C WE					M
	1200.	I			C WE					M
	1250.	I			C WE					M
	1300.	I			C LWE					M
	1350.	I			C LWE					M
3.00	1400.	I			C LWE					M
	1450.	I			CL WE					M
	1500.	I			CL WE					M
	1550.	I			CL WE					M
	1600.	I			CL WE					M
	1650.	I			CL WE					M
	1700.	I			CL E					M
	1750.	I			C WE					M
2.50	1800.	I			C WE					M
	1850.	I			C WE					M
	1900.	I			LC WE					M
	1950.	I			LC WE					M
	2000.	I			LC WE					M
	2050.	I			LC WE					M
	2100.	I			L C WE					M
2.00	2150.	I			L C WE					M
	2200.	I			L C WE					M
	2250.	I			L C WE					M
	2300.	I			L C WE					M
	2350.	I			L C WE					M
	2400.	I			L C WE					M



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SH. 35 J

\*\*\*\*\*  
HEC2 RELEASE DATED NOV 76 UPDATED MAY 1984  
ERROR CORR - 01, 02, 03, 04, 05, 06  
MODIFICATION - 50, 51, 52, 53, 54, 55, 56  
\*\*\*\*\*

JTE 6/11/87  
MM 7/17/87

NOTE- ASTERISK (\*) AT LEFT OF CROSS-SECTION NUMBER INDICATES MESSAGE IN SUMMARY OF ERRORS LIST

DISCHARGE = 15300 CFS

SUMMARY PRINTOUT

SECNO	Q	CWSEL	CRWS	GLOB	GCH	GR0B	GLOBP	GCHP	GR0BP	VLOB	VCH	VR0B
6.800	15300.00	4076.63	4076.01	0.00	3907.04	11392.96	0.00	25.54	74.46	0.00	7.69	7.02
6.500	15300.00	4076.76	4076.30	0.00	4128.80	11171.20	0.00	26.99	73.01	0.00	8.44	7.48
6.000	15300.00	4077.09	4074.37	0.00	15300.00	0.00	0.00	100.00	0.00	0.00	8.42	0.00
5.500	15300.00	4078.35	4075.14	0.00	15235.94	64.06	0.00	99.58	0.42	0.00	6.23	1.39
5.000	15300.00	4079.05	4076.48	326.05	14942.21	31.75	2.13	97.66	0.21	1.60	4.69	1.42
4.000	15300.00	4079.71	4076.71	0.00	15300.00	0.00	0.00	100.00	0.00	0.00	6.46	0.00
3.000	15300.00	4080.62	4079.22	4.27	15294.80	0.93	0.03	99.97	0.01	0.98	7.33	0.87
2.500	15300.00	4082.07	4079.80	14.23	15276.55	9.21	0.09	99.85	0.06	1.33	4.83	1.19
2.000	15300.00	4082.64	4081.66	177.48	15065.86	56.65	1.16	98.47	0.37	2.82	7.44	2.52
* 0.800	15300.00	4100.21	4100.21	731.39	8032.54	6536.07	4.78	52.50	42.72	6.79	12.14	11.68
* 0.600	15300.00	4100.56	4100.56	678.74	8328.02	6293.25	4.44	54.43	41.13	6.56	12.24	11.44

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Sh. 35 K

DISCHARGE = 15300 CFS

SUMMARY PRINTOUT

JFK 6/11/87  
HM 7/17/87

SECNO	KRATIO	AREA	CWSEL	ELMIN	DEPTH	DIFWSX	HV	TOPWID	SSTA	ENDBT	K*CHSL	10K*8
6.800	0.00	2130.55	4076.63	4060.50	16.13	0.00	0.80	778.04	415.60	1249.99	0.00	90.61
6.500	0.92	1983.00	4076.76	4060.90	15.86	0.13	0.93	745.29	430.22	1242.77	20.00	108.14
6.000	1.60	1816.33	4077.09	4062.00	15.09	0.33	1.10	336.99	506.46	843.45	15.72	42.27
5.500	1.54	2493.08	4078.35	4062.00	16.35	1.26	0.60	413.64	515.50	929.15	0.00	17.79
5.000	1.15	3409.97	4079.05	4064.00	15.05	0.70	0.33	754.07	136.57	890.64	8.00	13.42
4.000	0.74	2367.58	4079.71	4068.00	11.71	0.66	0.65	438.33	388.53	826.86	8.70	24.43
3.000	0.76	2091.46	4080.62	4072.00	8.62	0.91	0.83	497.65	385.82	883.47	12.58	42.11
2.500	1.62	3182.60	4082.07	4073.00	9.07	1.45	0.36	677.85	289.67	967.52	2.63	16.00
2.000	0.56	2111.85	4082.64	4074.00	8.64	0.57	0.85	584.66	332.36	917.01	2.86	50.14
* 0.800	1.23	1328.64	4100.21	4080.00	20.21	17.57	2.14	330.00	0.00	330.00	9.23	33.20
* 0.600	1.01	1333.96	4100.56	4080.40	20.16	0.35	2.13	330.00	0.00	330.00	20.00	32.53

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sh. 35 L

SUMMARY OF ERRORS AND SPECIAL NOTES

CAUTION	SECNO=	0.800	PROFILE= 1	CRITICAL DEPTH ASSUMED
CAUTION	SECNO=	0.800	PROFILE= 1	MINIMUM SPECIFIC ENERGY
CAUTION	SECNO=	0.600	PROFILE= 1	CRITICAL DEPTH ASSUMED
CAUTION	SECNO=	0.600	PROFILE= 1	MINIMUM SPECIFIC ENERGY

JTk 6/11/87  
NM 7/17/87

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SH 35 M

\*\*\*\*\*  
HEC2 RELEASE DATED NOV 76 UPDATED MAY 1984  
ERROR CORR - 01,02,03,04,05,06  
MODIFICATION - 50,51,52,53,54,55,56  
\*\*\*\*\*

JTK 6/11/87  
HM 7/17/87



Calculation Cover Sheet



Contract No. 5057

Discipline Earth Sci

Calc. No. 10-551-01-00

No. of Sheets 42 43 *KJ*

Project

UMTRA - Green River

Feature

Flood Analysis - Brown's Wash

Item

Hydrologic and Hydraulic analysis of 100yr. storm

Sources of Data

Sources of Formulae & References

- ① Flood Analysis - Brown Wash (Hydrologic and Hydraulic analysis of PMF)  
MKE DOC. NO. 5057-GRN-C-01-00215-00, Calc. No. 10-539-02-60
- ③ Miller J. F. et al. "Precipitation - Frequency Atlas of the Western United States, NOAA ATLAS 2 Vol. VI - Utah - U.S. Dept. of Commerce, NOAA, National Weather Service", 1973.
- ② Flood Frequency Analysis (10-yr & 25-yr) MKE DOC. NO. 5057-GRN-C-01-00216-00, Calc. No. 10-534-01-00.

Preliminary Calc.

Final Calc.

Supersedes Calc. No. \_\_\_\_\_

Rev. No.	Revision	Calculation By	Date	Checked By	Date	Approved By	Date
		<u>James Kam</u>	<u>10/8/87</u>	<u>HM</u>	<u>10/21/87</u>	<u>P.K. [Signature]</u>	<u>11/3/87</u>

Project UMTRA - Green River  
 Feature Hydrology  
 Item Flooding Potential on Brown Wash

Contract No. 5057 Sheet 1  
 Designed JK File No. \_\_\_\_\_  
 Checked HM Date 10/7/87  
 Date 04/19/87

Purpose: To determine the discharge in the Brown's Wash resulting from the 100-yr 24-hr. storm at the vicinity of the existing tailings pile. Based on the computed peak discharge, the maximum water level was derived.

Summary of Results:

Peak flow resulting from the 100-yr 24 hr. at the tailings pile location has been determined to be 24,510 cfs. Maximum water level elevations at different stations are listed as follows:-

Sta.	Water level elevations (ft)	
	without berm	with berm (4080') @ Sta. 5.5 to 6.0
6.0	4078.8	4077.7
5.5	4079.2	4080.7
5.0	4079.2	4081.4
4.0	4080.6	4081.8
3.0	4081.9	4082.5
2.5	4083.7	4083.9

Project UMTRCA - Green River  
 Feature Hydrology  
 Item Flood Frequency Analysis

Contract No. 5057  
 Designed FTK  
 Checked HM

Sheet 2  
 File No. \_\_\_\_\_  
 Date 10/7/87  
 Date 04/14/87

The precipitations for the 100 yr storm with different durations were taken from ref. ③ and are listed on sh. 3. Precipitation distribution is derived on sh. 4 thru. 7, and is used in the HEC1 analysis of flood routing through the Brown's Wash Watershed upstream of the tailing pile. The watershed characteristics used in the simulation is identical to that described in ref. ① for the PMF analysis.

Based on the HEC1 analysis (see sh. 12-16) a peak flow of 24,510 cfs was computed for the 100 yr - 14 hr. storm.

This flow was entered into the HEC2 computer run to determine the maximum water surface profile. Description of the cross sections used in the HEC2 analysis is contained in ref. ②. The water surface profiles with and without the berm (4080') @ sta. 5.5 & 6.0 are presented on sh. 38 and sh. 26 respectively.

The extent of the inundated areas is shown on Plate 1.

Project UMTA - Green River  
 Feature Hydrology  
 Item Flood Frequency Analysis

Contract No. 5057  
 Designed JK  
 Checked HM

Sheet 3  
 File No. \_\_\_\_\_  
 Date 4/23/87  
 Date 7/11/87

MKE DOC.# 5057-GRN-C-01-00216-00

Ref. (2) JK 10/7/87  
 HM 02/19/87

From figures on Sh. 11-18, the following precipitation values are tabulated:

Precipitation (inches)		Return Period				
		2-yr.	10-yr.	25-yr.	50-yr.	100-yr.
Duration	1-hr.	.58 <sup>1)</sup>	.90 <sup>3)</sup>	1.10 <sup>3)</sup>	1.20 <sup>3)</sup>	1.47 <sup>2)</sup>
	6-hr.	.75	1.20	1.40	1.60	1.80
	24-hr.	.90	1.60	1.95	2.25	2.50

from sh. 8a ref. (3)

$$\begin{aligned}
 1) Y_2 &= 2\text{-yr } 1\text{-hr. estimated value} \\
 &= -0.011 + 0.942 [ .75 (.75/.90) ] \\
 &= 0.58 \text{ " }
 \end{aligned}$$

$$\begin{aligned}
 2) Y_{100} &= 100\text{-yr } 1\text{-hr. estimated value} \\
 &= 0.494 + 0.755 [ 1.80 (1.80/2.50) ] \\
 &= 1.47 \text{ " }
 \end{aligned}$$

3) from plot on Sh. 11 : Precipitation depth vs. return period



Project UMTRA - Green River  
 Feature Hydrology  
 Item Flood Frequency Analysis

Contract No. 5057  
 Designed JTK  
 Checked HM  
 File No. \_\_\_\_\_  
 Date 4/28/87  
 Date 7/16/87

JTK 10/7/87

HM Oct 14/87

Using data on sh. 3, plot data on precipitation depth-duration diagram on sh. 8b and 9

Precipitation (inches)

Hr.	Cumulative			Incremental			Incre. Sequence		
	25-yr.	50-yr.	100-yr.	25-yr.	50-yr.	100-yr.	25-yr.	50-yr.	100-yr.
6	1.40	1.60	1.80	1.40	1.60	1.80	0.15	0.20	0.20
12	1.70	1.90	2.20	0.30	0.30	0.40	1.40	1.60	1.80
18	1.80	2.10	2.30	0.10	0.20	0.10	0.30	0.30	0.40
24	1.95	2.25	2.50	0.15	0.15	0.20	0.10	0.15	0.10

7				1.10	1.20	1.47	0.05	1.06	0.05
8				0.10	0.10	0.10	0.05	0.07	0.05
9				0.05	0.10	0.08	0.05	0.07	0.05
10				0.05	0.07	0.05	0.05	1.10	0.08
11				0.05	0.07	0.05	0.10	0.10	0.10
12				0.05	0.06	0.05	1.10	1.20	1.47

from chart on sh. 8 b

11:05	.32	.35	.32	.35	.03	.04	.05
11:10	.50	.54	.16	.19	.04	.04	.05
11:15	.63	.68	.13	.14	.04	.04	.05
11:20	.71	.77	.08	.09	.04	.04	.05
11:25	.79	.86	.08	.09	.04	.04	.05
11:30	.87	.95	.08	.09	.04	.05	.05
11:35	.91	1.00	.04	.05	.08	.09	.06
11:40	.95	1.04	.04	.04	.08	.09	.10
11:45	.99	1.08	.04	.04	.08	.09	.11
11:50	1.03	1.12	.04	.04	.13	.14	.11
11:55	1.07	1.16	.04	.04	.18	.19	.18
12:00	1.10	1.20	.03	.04	.32	.35	.23

from Table: adjusted factors to obtain h-min estimates from 1-hr value sh. 10

Project UNITRA - Green River  
 Feature Hydrology  
 Item Flood Frequency Analysis

Contract No. 5057 File No. \_\_\_\_\_  
 Designed JK Date 10/2/87  
 Checked HM Date Oct 19/87

$\Delta t = 5 \text{ min.}$

0 - 0:50

.00278 —————→

0:55 - 1:40

.00278 .00278 —————→

1:45 - 2:30

.00278 —————→

2:35 - 3:20

.00278 —————→

3:25 - 4:10

.00278 —————→

4:15 - 5:00

.00278 —————→

5:05 - 5:50

.00278 —————→

5:55 - 6:40

.00278 .00278 .0042 .0042 —————→

6:45 - 7:30

0.0042 —————→

7:35 - 8:20

0.0042 —————→

8:25 - 9:10

0.0042 —————→ 0.0067 0.0067



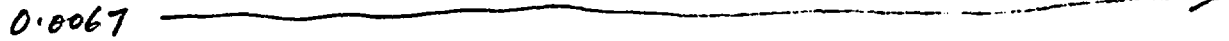
Project UMTRA - Great River  
 Feature Hydrology  
 Item Flood Frequency Analysis

Contract No. 5057  
 Designed JK  
 Checked HM

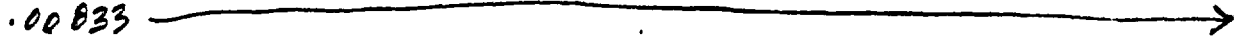
Sheet 6  
 File No. \_\_\_\_\_  
 Date 10/2/87  
 Date OK 11/87

Precipitation distribution for 100 yr-24 hr.

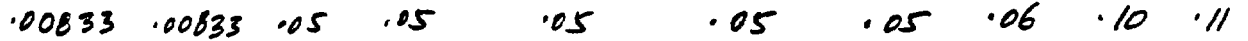
9:15 - 10:00



10:05 - 10:50



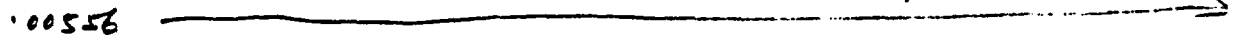
10:55 - 11:40



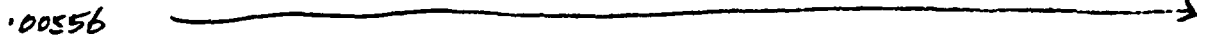
11:45 - 12:30



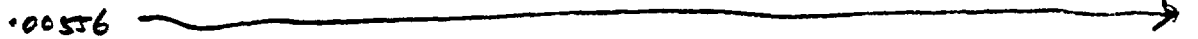
12:35 - 13:20



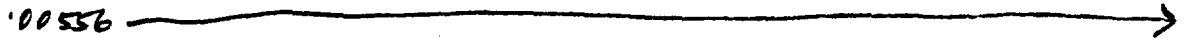
13:25 - 14:10



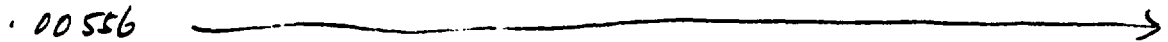
14:15 - 15:00



15:05 - 15:50



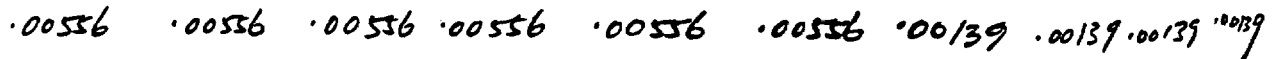
15:55 - 16:40



16:45 - 17:30



17:35 - 18:20

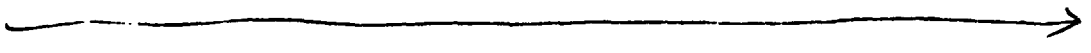


Project NMTRA - Green River  
Feature Hydrology  
Item Flood Frequency Analysis

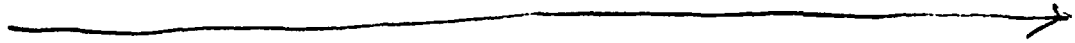
Contract No. 5057  
Designed JTK  
Checked HM

Sheet 7  
File No. \_\_\_\_\_  
Date 10/2/87  
Date Oct 19/87

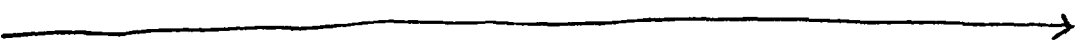
18:25 - 19:10

.00139 

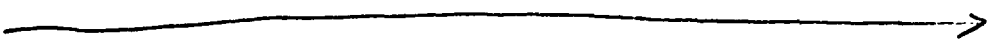
19:15 - 20:00

.00139 

20:05 - 20:50

.00139 

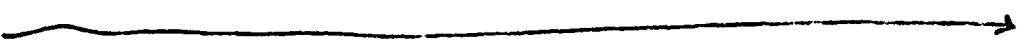
20:55 - 21:40

.00139 

21:45 - 22:30

.00139 

22:35 - 23:20

.00139 

23:25 - 24:10

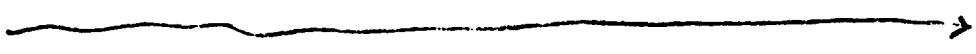
.00139 



Table 11. Equations for estimating 1-hr values in Utah with statistical parameters for each equation

Region of applicability*	Equation	Corr. coeff.	No. of stations	Mean of computed stn. values (inches)	Standard error of estimate (inches)
Utah south of the Unita east of Wasatch, and east and south of Boulder and Pine Valley Mountains (1)	$Y_2 = -0.011 + 0.942[(X_1)(X_1/X_2)]$	.95	86	0.72	0.085
	$Y_{100} = 0.49 + 0.755[(X_3)(X_3/X_4)]$	.90	85	1.96	.290
Most of western Utah (2)	$Y_2 = 0.005 + 0.852[(X_1)(X_1/X_2)]$	.89	65	0.41	.047
	$Y_{100} = 0.322 + 0.789[(X_3)(X_3/X_4)]$	.87	65	1.25	.196
Northeast and northwest corners of Utah (3)	$Y_2 = 0.019 + 0.711[(X_1)(X_1/X_2)] + 0.001Z$	.82	98	0.40	.031
	$Y_{100} = 0.338 + 0.670[(X_3)(X_3/X_4)] + 0.001Z$	.80	79	1.04	.141

\* Numbers in parentheses refer to geographic regions shown in figure 18. See text for more complete description.

List of variables

- $Y_2$  = 2-yr 1-hr estimated value
- $Y_{100}$  = 100-yr 1-hr estimated value
- $X_1$  = 2-yr 6-hr value from precipitation-frequency maps
- $X_2$  = 2-yr 24-hr value from precipitation-frequency maps
- $X_3$  = 100-yr 6-hr value from precipitation-frequency maps
- $X_4$  = 100-yr 24-hr value from precipitation-frequency maps
- Z = point elevation in hundreds of feet

Procedures for estimating 1-hr (60-min) precipitation-frequency values. Multiple-regression screening techniques were used to develop equations for estimating 1-hr values. Factors considered in the screening process were restricted to those that could be determined easily from the maps of this Atlas or from generally available topographic maps.

the Wasatch Range, and east and south of the Boulder and Pine Valley Mountains (Region 1, fig. 18). The second region is most of western Utah and is labeled Region 2 on figure 18. Northeastern Utah north of the Unita and the northwestern tip of Utah (Region 3, fig. 18) comprises the third region. Equations to provide estimates for the 1-hr duration for 2- and 100-yr return periods are shown in table 11. Also listed are the statistical parameters associated with each equation. In these equations, the variable  $[(X_1)(X_1/X_2)]$  or  $[(X_3)(X_3/X_4)]$  can be regarded as the 6-hr value times the slope of the line connecting the 6- and 24-hr values for the appropriate return period.

As with any separation into regions, the boundary can only be considered as the sharpest portion of a zone of transition between

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FRK 4/27/87

Sh. 8a.

values regard-  
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ay occurring  
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investigations  
use maps will  
using a data  
clusively rain.  
se maps have  
ner than with

id 24-hr dura-  
ther durations  
6- and 24-hr

precipitation occurring within these months, but the investigations mentioned in the preceding paragraph indicate that these maps will approximate the values that would be obtained by using a data series made up of precipitation events that are exclusively rain. Since data for only part of the year were used, these maps have been labeled with the appropriate probabilities rather than with a return period in years (figs. 31-42).

- $X_2$  = 2-yr 1-hr estimated value
- $Y_{100}$  = 100-yr 1-hr estimated value
- $X_2$  = 2-yr 6-hr value from precipitation-frequency
- $X_6$  = 2-yr 24-hr value from precipitation-frequency
- $X_6$  = 100-yr 6-hr value from precipitation-frequency
- $X_6$  = 100-yr 24-hr value from precipitation-frequency
- $Z$  = point elevation in hundreds of feet

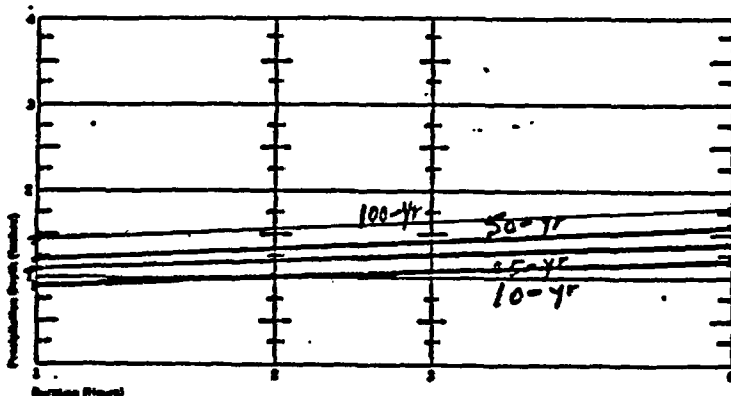
Sh. 8b.

### Procedures for Estimating Values for Durations Other Than 6 and 24 Hrs

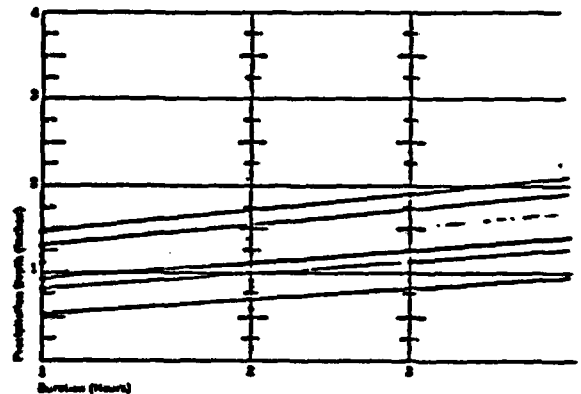
The isopluvial maps in this Atlas are for 6- and 24-hr durations. For many hydrologic purposes, values for other durations are necessary. Such values can be estimated using the 6- and 24-hr maps and the empirical methods outlined in the following sections. The procedures detailed below for obtaining 1-, 2-, and 3-hr estimates were developed specifically for this Atlas. The procedures for obtaining estimates for less than 1-hr duration and for 12-hr duration were adopted from *Weather Bureau Technical Paper No. 40* (U.S. Weather Bureau 1961) only after investigation demonstrated their applicability to data from the area covered by this Atlas.

Procedures for estimating 1-hr (60-min) frequency values. Multiple-regression screening tests to develop equations for estimating 1-hr values. In the screening process were restricted to those determined easily from the maps of this Atlas available topographic maps.

The 11 western states were separated into 11 regions. The regions were chosen on the basis of climatological homogeneity and are generally river basins separated by prominent divides. The graphic regions are partially within Utah. For use as an overlay on the precipitation-frequency regions are outlined in figure 18. The first region is that portion of the State south of the Unita M



(A)



(B)

Figure 15. Precipitation depth-duration diagram (1- to 6-hr).  
 a. Utah south of the Unita Mountains, east of the Wasatch Range, and east and south of the Boulder and Pine Valley Mountains. (Region 1, fig. 18).

b. Most of western Utah. (Region 2, fig. 18).

Ref. (3) JTK 10/1/89  
 HM 6/14/87  
 JTK 4/27/87  
 HM 6/12/87

Sh. 9

JTK 10/7/87  
HM 04/14/87  
121  
(3)

Figure 16. Precipitation depth-duration diagram (6- to 24-hr).

JTK 4/27/87  
HM 5/13/87

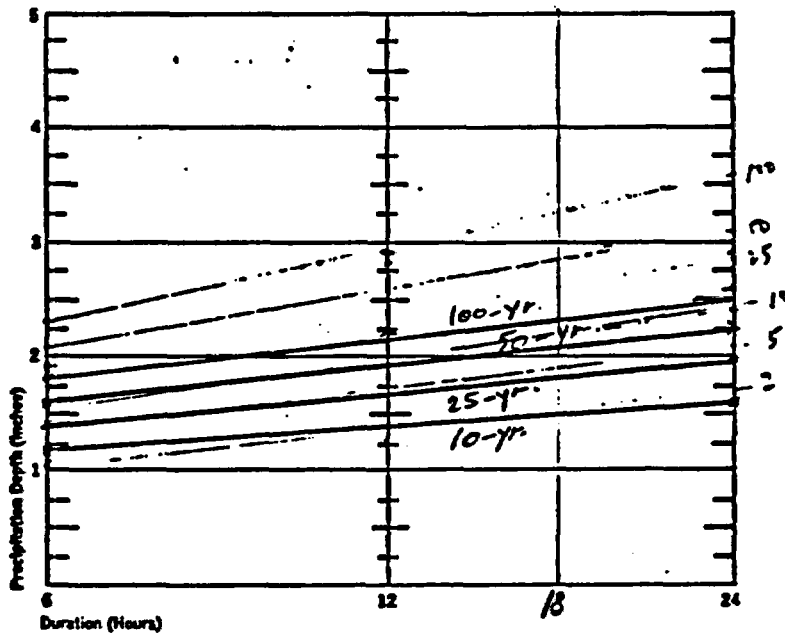


Illustration of Use Maps, Diagrams, a

To illustrate the use figures 19 to 30 for the do These values are shown in read from the maps should of figure 6 because (1) n series of maps as are lab registration differences in between isolines is diffic values in table 13 (fig. 17. subjectively. On this nom what above the line, so th (as shown by the strikeout adopted in preference to th

The 2- and 100-yr 1 from the equations applic The 2-yr 1-hr value is es values from table 13); the (100-yr 6- and 24-hr valu values on figure 6 and co can obtain estimates for re

The 2- and 3-hr valu gram of figure 15 or equat for the desired return pe: points on the nomogram straight line. Read the esti of the connecting line as example is shown in figur 100-yr 2-hr (1.82 in.) an italics on table 13.

Estimates of 1-hr precipitation-frequency values for return periods between 2 and 100 yrs. The 1-hr values for the 2- and 100-yr return periods can be plotted on the nomogram of figure 6 to obtain values for return periods greater than 2 yrs or less than 100 yrs. Draw a straight line connecting the 2- and 100-yr values and read the desired return-period value from the nomogram.

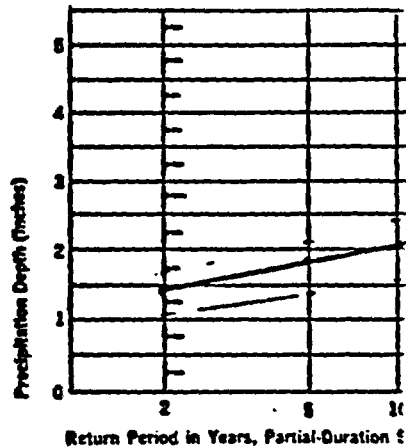
Estimates for 2- and 3-hr (120- and 180-min) precipitation-frequency values. To obtain estimates of precipitation-frequency values for 2 or 3 hrs, plot the 1- and 6-hr values from the Atlas on the appropriate nomogram of figure 15. Draw a straight line connecting the 1- and 6-hr values, and read the 2- and 3-hr values from the nomogram. This nomogram is independent of return period. It was developed using data from the same regions used to develop the 1-hr equations.

The mathematical solution from the data used to develop figure 15 gives the following equations for estimating the 2- and 3-hr values:

For Region 1, 2-hr = 0.341 (6-hr) + 0.659 (1-hr) (3)  
figure 18 3-hr = 0.569 (6-hr) + 0.431 (1-hr) (4)  
For Region 2, 2-hr = 0.299 (6-hr) + 0.701 (1-hr) (5)

can obtain estimates for return periods of 5, 10, 25, and 50 yrs.

The 2- and 3-hr values can be estimated by using the nomogram of figure 15 or equations (3) and (4). The 1- and 6-hr values for the desired return period are obtained as above. Plot these points on the nomogram of figure 15 and connect them with a straight line. Read the estimates for 2 or 3 hrs at the intersections of the connecting line and the 2- and 3-hr vertical lines. An example is shown in figure 17b for the 100-yr return period. The 100-yr 2-hr (1.82 in.) and 100-yr 3-hr (1.95 in.) values are in italics on table 13.



(A)

Sh. 10

ref. (3)

JFK 4/29  
HM 6/18/67

values for return  
es for the 2- and  
ogram of figure 6  
2 yrs or less than  
and 100-yr values  
he nomogram.  
in) precipitation-  
itation-frequency  
es from the Atlas  
w a straight line  
- and 3-hr values  
endent of return  
e regions used to  
used to develop  
nating the 2- and

- .659 (1-hr) (3)
- 1.431 (1-hr) (4)
- .701 (1-hr) (5)
- .474 (1-hr) (6)
- 1.750 (1-hr) (7)
- .33 (1-hr) (8)

equency values.  
values from the  
r estimates at the  
with the 12-hr  
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le 12 to the 1-hr

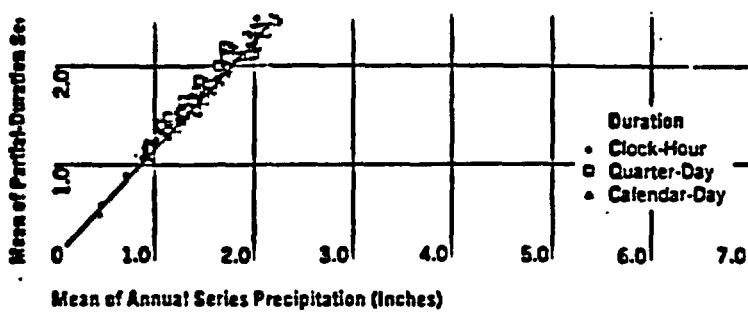
	.29	.16	.12	
Duration (min)	5	10	15	30
Ratio to 1-hr	0.29	0.45	0.57	0.79

(Adopted from U.S. Weather Bureau Technical Paper No. 40, 1961.)

	1-hr	2-hr
2-yr	0.65	
5-yr		
10-yr		
25-yr		
50-yr		
100-yr	1.63	1.82

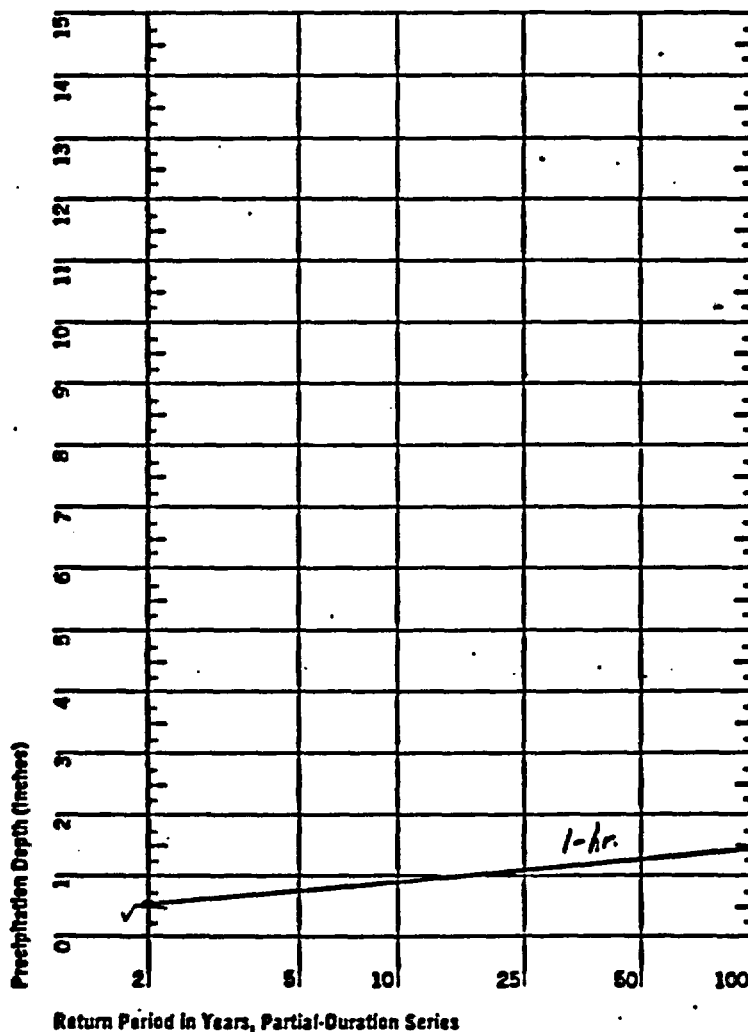
Table 12. Adjustment factors to obtain n-min estimates from 1-hr values

Table 13. Precipitation data for town computed for town



Sh. 11

ref. (3)



portant. Next, an examination was topographic and meteorologic con: direction to moisture sources. Eac: ure of some physical reality, and c to variation in the precipitation-fre:

Finally, various climatological could be indexes of variation of th were considered. The procedure u equations was a multiple-regression ess was done by computer using computer program was capable of pendent variables for as many lo. The number of variables screened between 60 and 100. This does n: pletely different factors could be i factors might involve different mea measures of slope might be over di ent orientations. In each instance, computer to select the most critical factor.

Although the computer progr ear during the regression analysis, i computations to use logarithms, po binations of any or all of the la selected the single variable most hig tation-frequency value under inves select the variable that, combined lected, would explain the greatest v: quency values. The third, fourth, & selected in a similar manner. The

Figure 6. Precipitation depth versus return period for partial-duration series.

JTK  
4/29/57  
HM 6/18/87



HEC-1 INPUT

Sh. 13

LINE	ID	1	2	3	4	5	6	7	8	9	10
48	KK	3.4									
49	RK	26400	.032	.04				0	0.45		
50	KK	BAS4									
51	KM	100YR 24HR									
52	BA	6.4									
53	LU	0	0.2								
54	UD	0.75									
55	KK	BAS3									
56	KM	100YR 24HR									
57	BA	12.1									
58	LU	0	0.2								
59	UD	.96									
60	KK	ST34									
61	HC	3									
62	KK	5.6									
63	RK	53856	.015	.04				0	0.03		
64	KK	BAS5									
65	KM	100YR 24HR									
66	BA	20.7									
67	LU	0	0.2								
68	UD	1.73									
69	KK	BAS6									
70	KM	100YR 24HR									
71	BA	11.8									
72	LU	0	0.2								
73	UD	0.95									
74	KK	ST56									
75	HC	3									
76	KK	7.8									
77	RK	6336	0.005	.04				0	0.025		
78	KK	BAS8									
79	KM	100YR 24HR									
80	BA	0.5									
81	LU	0	0.2								
82	UD	0.52									
83	KK	BAS7									
84	KM	100YR 24HR									
85	BA	12.2									
86	LU	0	0.2								
87	UD	1.22									

JFK 10/5/87  
HM 02/14/87

HEC-1 INPUT

LINE	ID.	1	2	3	4	5	6	7	8	9	10
88	KK	ST78	COMBINE FLOWS 7,8								
89	HC	3									
90	KK	9	FLOWS 7,8 FROM STA. 7,8 TO 9								
91	RK	32736	0.01	.04				TRAP	0	0.05	
92	KK	BAS9									
93	KM	100YR 24HR									
94	BA	11.3									
95	LU	0	0.2								
96	UD	1.39									
97	KK	ST9	COMBINE FLOWS								
98	HC	2									
99	ZZ										

Sh. 14

File 10/5/87

HM 06/19/87



\*\*\*\*\*  
 \* FLOOD HYDROGRAPH PACKAGE (HEC-1) \*  
 \* FEBRUARY 1981 \*  
 \* REVISED 30 OCT 81 \*  
 \* \*  
 \* RUN DATE

UMTRA - GREEN RIVER - BROWN WASH  
 100 - YR 24 - HR STORM

5 ID OUTPUT CONTROL VARIABLES  
 IPRNT 5 PRINT CONTROL  
 IPLOT 0 PLOT CONTROL  
 GSCAL 0. HYDROGRAPH PLOT SCALE

IT HYDROGRAPH TIME DATA  
 NMIN 5 MINUTES IN COMPUTATION INTERVAL  
 IDATE 1 0 STARTING DATE  
 ITIME 0000 STARTING TIME  
 NQ 300 NUMBER OF HYDROGRAPH ORDINATES  
 NDDATE 2 0 ENDING DATE  
 NDTIME 0055 ENDING TIME

COMPUTATION INTERVAL 0.08 HOURS  
 TOTAL TIME BASE 24.92 HOURS

ENGLISH UNITS  
 DRAINAGE AREA SQUARE MILES  
 PRECIPITATION DEPTH INCHES  
 LENGTH, ELEVATION FEET  
 FLOW CUBIC FEET PER SECOND  
 STORAGE VOLUME ACRE-Feet  
 SURFACE AREA ACRES  
 TEMPERATURE DEGREES FAHRENHEIT

\*\*\*\*\*  
 \* U. S. ARMY CORPS OF ENGINEERS \*  
 \* THE HYDROLOGIC ENGINEERING CENTER \*  
 \* 609 SECOND STREET \*  
 \* DAVIS, CALIFORNIA 95616 \*  
 \*

*Sh. 15*

*JTK 10/5/87*  
*NM 06/14/87*

RUNOFF SUMMARY  
FLOW IN CUBIC FEET PER SECOND  
TIME IN HOURS, AREA IN SQUARE MILES

Sh. 16

JK 10/5/87  
HM 11/4/87

OPERATION	STATION	PEAK FLOW	TIME OF PEAK	AVERAGE FLOW FOR MAXIMUM PERIOD			BASIN AREA	MAXIMUM STAGE	TIME OF MAX STAGE
				6-HOUR	24-HOUR	72-HOUR			
HYDROGRAPH AT	BAS1	1932.	12.50	354.	89.	85.	2.60		
HYDROGRAPH AT	BAS2	3782.	12.58	750.	187.	181.	5.50		
2 COMBINED AT	ST12	5702.	12.50	1104.	276.	266.	8.10		
ROUTED TO	3, 4	5411.	12.75	1103.	276.	266.	8.10		
HYDROGRAPH AT	BAS4	4325.	12.58	872.	218.	210.	6.40		
HYDROGRAPH AT	BAS3	6743.	12.75	1649.	412.	397.	12.10		
3 COMBINED AT	ST34	16194.	12.67	3624.	906.	873.	26.60		
ROUTED TO	5, 6	12835.	13.83	3571.	908.	875.	26.60		
HYDROGRAPH AT	BAS5	6932.	13.50	2777.	705.	679.	20.70		
HYDROGRAPH AT	BAS6	6628.	12.75	1608.	402.	387.	11.80		
3 COMBINED AT	ST56	21136.	13.75	7866.	2016.	1941.	59.10		
ROUTED TO	7, 8	21058.	13.92	7848.	2015.	1941.	59.10		
HYDROGRAPH AT	BAS8	438.	12.33	68.	17.	16.	0.50		
HYDROGRAPH AT	BAS7	5566.	13.00	1660.	416.	400.	12.20		
3 COMBINED AT	ST78	23980.	13.83	9544.	2448.	2357.	71.80		
ROUTED TO	9	22675.	14.33	9411.	2443.	2353.	71.80		
HYDROGRAPH AT	BAS9	4605.	13.17	1532.	385.	371.	11.30		
2 COMBINED AT	ST9	24510.	14.33	10780.	2828.	2724.	83.10		

\*\*\* NORMAL END OF HEC-1 \*\*\*

Sh. 17

*Subentical profile  
with upstream railroad crossing  
and downstream culverts  
(4 functioning)*

\*\*\*\*\*  
HEC2 RELEASE DATED NOV 76 UPDATED MAY 1984  
ERROR CORR - 01,02,03,04,05,06  
MODIFICATION - 50,51,52,53,54,55,56  
\*\*\*\*\*

T1 UMTRA - GREEN RIVER - 100-YR 24 HR  
T2 WATER SURFACE PROFILE IN BROWN WASH  
T3 DISCHARGE = 24510 CFS

J1	ICHECK	ING	NINV	IDIR	STRT	METRIC	HVINS	Q	WSEL	FR
	0.	0.	0.	0.	0.009000	0.00	0.0	24510.	4074.000	0.000
J2	NPROF	IPLOT	PRFVS	XSECV	XSECH	FN	ALLDC	IBW	CHNIM	ITRACE
	-1.000	0.000	0.000	0.000	0.000	0.000	-1.000	0.000	0.000	0.000
J3	VARIABLE CODES FOR SUMMARY PRINTOUT									
	38.000	43.000	1.000	2.000	13.000	14.000	15.000	35.000	60.000	59.000
	55.000	26.000	56.000	0.000	38.000	58.000	25.000	1.000	42.000	8.000
	51.000	10.000	4.000	53.000	54.000	33.000	5.000	0.000	0.000	0.000
NC	0.045	0.050	0.024	0.300	0.500	0.000	0.000	0.000	0.000	0.000
X1	6.800	25.000	150.000	700.000	0.000	0.000	0.000	0.000	0.000	0.000
BT	25.000	0.000	4090.000	4090.000	80.000	4080.000	4080.000	4080.000	150.000	4082.000
BT	280.000	4080.000	4080.000	340.000	4078.000	4078.000	4078.000	450.000	4076.000	4076.000
BT	4075.500	4065.500	550.000	4075.500	4070.500	555.000	4075.200	4065.500	560.000	4075.200
BT	4065.500	565.000	4075.000	4070.500	570.000	4075.000	4065.500	575.000	4075.000	4065.500
BT	580.000	4075.000	4070.500	585.000	4075.000	4065.500	590.000	4074.900	4065.500	595.000
BT	4074.900	4070.500	600.000	4074.800	4065.500	700.000	4074.000	4074.000	800.000	4074.000
BT	4074.000	936.000	4078.000	4078.000	950.000	4076.000	4076.000	1000.000	4070.000	4070.000
BT	1070.000	4070.000	4070.000	1885.000	4100.000	4100.000	0.000	0.000	0.000	0.000
QR	4090.000	0.000	4080.000	80.000	4082.000	150.000	4080.000	280.000	4078.000	340.000
QR	4076.000	450.000	4065.500	545.000	4065.500	550.000	4065.500	555.000	4065.500	560.000
QR	4060.500	565.000	4065.500	570.000	4065.500	575.000	4060.500	580.000	4065.500	585.000
QR	4065.500	590.000	4060.500	595.000	4065.500	600.000	4074.000	700.000	4074.000	800.000
QR	4078.000	936.000	4076.000	950.000	4070.000	1000.000	4070.000	1070.000	4100.000	1885.000
X1	6.500	0.000	0.000	0.000	20.000	20.000	20.000	0.000	0.400	0.000
X2	0.000	0.000	0.000	0.000	0.000	0.000	1.000	0.000	0.000	0.000

*JFK 10/6/87  
HM 02/14/87*

NC	0.045	0.050	0.035	0.100	0.300	0.000	0.000	0.000	0.000	0.000	0.000
X1	6.000	8.000	110.000	890.000	70.000	70.000	70.000	0.000	0.000	0.000	0.000
GR	4090.000	0.000	4074.000	110.000	4070.000	490.000	4062.000	525.000	4078.000	685.000	0.000
GR	4078.000	890.000	4080.000	1265.000	4100.000	1885.000	0.000	0.000	0.000	0.000	0.000
X1	5.500	11.000	180.000	890.000	150.000	280.000	270.000	0.000	0.000	0.000	0.000
GR	4090.000	0.000	4080.000	80.000	4080.000	140.000	4071.000	180.000	4070.000	530.000	0.000
GR	4062.000	570.000	4073.000	680.000	4076.000	890.000	4079.000	940.000	4080.000	1200.000	0.000
GR	4090.000	1460.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
NC	0.000	0.000	0.000	0.200	0.500	0.000	0.000	0.000	0.000	0.000	0.000
X1	5.000	10.000	270.000	876.000	230.000	290.000	250.000	0.000	0.000	0.000	0.000
GR	4100.000	0.000	4080.000	95.000	4076.000	270.000	4076.000	470.000	4064.000	530.000	0.000
GR	4074.000	635.000	4076.000	876.000	4082.000	890.000	4082.000	1090.000	4110.000	1885.000	0.000
X1	4.000	9.000	385.000	840.000	470.000	440.000	460.000	0.000	0.000	0.000	1.000
GR	4130.000	0.000	4090.000	100.000	4080.000	385.000	4068.000	530.000	4078.000	750.000	0.000
GR	4080.000	840.000	4086.000	870.000	4090.000	1165.000	4120.000	1930.000	0.000	0.000	0.000
X1	3.000	12.000	400.000	880.000	315.000	320.000	318.000	0.000	0.000	0.000	1.000
GR	4130.000	0.000	4100.000	80.000	4090.000	170.000	4080.000	400.000	4074.000	455.000	0.000
GR	4072.000	570.000	4076.000	620.000	4080.000	880.000	4088.000	925.000	4090.000	1150.000	0.000
GR	4110.000	1640.000	4120.000	1820.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
NC	0.000	0.000	0.000	0.100	0.300	0.000	0.000	0.000	0.000	0.000	0.000
X1	2.500	12.000	300.000	960.000	365.000	380.000	380.000	0.000	0.000	0.000	0.000
GR	4110.000	0.000	4090.000	250.000	4080.000	300.000	4073.000	420.000	4076.000	500.000	0.000
GR	4076.000	560.000	4078.000	620.000	4078.000	800.000	4080.000	960.000	4091.000	1000.000	0.000
GR	4096.000	1330.000	4110.000	1700.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
X1	2.000	11.000	380.000	900.000	350.000	300.000	350.000	0.000	0.000	0.000	0.000
GR	4114.000	0.000	4090.000	200.000	4080.000	380.000	4074.000	400.000	4074.000	430.000	0.000
GR	4078.000	510.000	4080.000	600.000	4080.000	900.000	4094.000	990.000	4094.000	1170.000	0.000
GR	4120.000	1890.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
NC	0.015	0.015	0.015	0.300	0.500	0.000	0.000	0.000	0.000	0.000	0.000
X1	0.800	8.000	85.000	140.000	650.000	400.000	650.000	0.000	0.000	0.000	0.000
BT	8.000	0.000	4100.000	4100.000	80.000	4098.000	4098.000	85.000	4098.000	4098.000	0.000
BT	86.000	4098.000	4090.000	139.000	4098.000	4090.000	140.000	4098.000	4098.000	190.000	0.000
BT	4098.000	4098.000	330.000	4096.000	4096.000	0.000	0.000	0.000	0.000	0.000	0.000
GR	4100.000	0.000	4098.000	80.000	4098.000	85.000	4080.000	86.000	4080.000	139.000	0.000
GR	4098.000	140.000	4098.000	190.000	4096.000	330.000	0.000	0.000	0.000	0.000	0.000
X1	0.600	0.000	0.000	0.000	20.000	20.000	20.000	0.000	0.400	0.000	0.000
X2	0.000	0.000	0.000	0.000	0.000	0.000	1.000	0.000	0.000	0.000	0.000
EJ	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000

JK  
10/6/87  
HM 02/14/87

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JTK 10/6/87  
HM Oct 14/87

SECNO	DEPTH	CWSEL	CRISW	WSELK	EQ	HV	HL	CLOSS	BANK	ELEV
Q	QLOB	QCH	QROB	ALOB	ACH	AROB	VDL	TWA	LEFT	RIGHT
TIME	VLOB	VCH	VROB	XNL	XNCH	XNR	WTN	ELMIN	BSTA	
SLOPE	XLOBL	XLCH	XLOBR	ITRIAL	IDC	ICONT	CORAR	TOPWID	ENDST	

\*PROF 1

CRITICAL DEPTH TO BE CALCULATED AT ALL CROSS SECTIONS

CCHV= 0.300 CEHV= 0.500  
\*SECNO 6.800

3265 DIVIDED FLOW

3370 NORMAL BRIDGE, NRD= 25 MIN ELTRD= 4070.00 MAX ELLC= 4100.00

6.80	17.08	4077.58	4076.91	4074.00	4078.63	1.05	0.00	0.00	4082.00	
24510.	0.	8355.	16155.	0.	899.	2127.	0.	0.	4074.00	
0.00	0.00	9.29	7.60	0.000	0.024	0.050	0.000	4060.50	362.88	
0.008946	0.	0.	0.	0	13	6	-1366.77	896.09	1276.03	

\*SECNO 6.500

3265 DIVIDED FLOW

3370 NORMAL BRIDGE, NRD= 25 MIN ELTRD= 4070.00 MAX ELLC= 4100.40

6.50	16.80	4077.70	4077.23	0.00	4078.90	1.20	0.19	0.08	4082.40	
24510.	0.	8703.	15807.	0.	867.	1971.	1.	0.	4074.40	
0.00	0.00	10.04	8.02	0.000	0.024	0.050	0.000	4060.90	378.44	
0.010460	20.	20.	20.	2	13	0	-1305.78	861.24	1268.34	

CCHV= 0.100 CEHV= 0.300  
\*SECNO 6.000

3301 HV CHANGED MORE THAN HVINS

6.00	16.76	4078.76	4074.75	0.00	4079.20	0.44	0.22	0.08	4074.00	
24510.	176.	24302.	33.	78.	4575.	54.	7.	2.	4078.00	
0.00	2.25	5.31	0.60	0.045	0.035	0.050	0.000	4062.00	77.26	
0.001484	70.	70.	70.	2	14	0	0.00	935.70	1032.96	

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JFK 10/6/87  
HM oct 11/87

SECND Q TIME SLOPE	DEPTH GLOB VLOB XLOBL	CWSEL GCH VCH XLCH	CRISW GROB VROB XLOBR	WSELK ALOB XNL ITRIAL	EQ ACH XNCH IDC	HV AROB XNR ICONT	HL VOL WTN CORAR	GLOSS TWA ELMIN TOPWID	BANK ELEV LEFT/RIGHT SSTA ENDST
*SECND 5.500									
5.50	17.19	4079.19	4073.92	0.00	4079.45	0.26	0.23	0.02	4071.00
24510.	296.	24128.	86.	149.	5837.	89.	41.	7.	4076.00
0.02	1.99	4.13	0.96	0.045	0.035	0.050	0.000	4062.00	143.62
0.000573	150.	270.	280.	2	14	0	0.00	844.88	988.50

CCHV= 0.200 CEHV= 0.500  
\*SECND 5.000

3301 HV CHANGED MORE THAN HVINS

5.00	15.19	4079.19	4077.52	0.00	4080.00	0.81	0.28	0.28	4076.00
24510.	564.	23921.	26.	223.	3270.	12.	68.	12.	4076.00
0.03	2.53	7.31	2.15	0.045	0.035	0.050	0.000	4064.00	130.34
0.003146	230.	250.	290.	2	14	0	0.00	753.10	883.45

\*SECND 4.000

4.00	12.60	4080.60	4078.58	0.00	4081.81	1.21	1.61	0.20	4080.00
24510.	5.	24505.	1.	5.	2772.	1.	101.	18.	4080.00
0.05	0.92	8.84	0.82	0.045	0.035	0.050	0.000	4068.00	367.94
0.003902	470.	460.	440.	2	16	0	0.00	475.05	842.99

\*SECND 3.000

3.00	9.91	4081.91	4080.54	0.00	4083.17	1.26	1.33	0.02	4080.00
24510.	90.	24401.	20.	42.	2706.	10.	121.	22.	4080.00
0.06	2.15	9.02	1.91	0.045	0.035	0.050	0.000	4072.00	356.13
0.004504	315.	318.	320.	2	19	0	0.00	534.60	890.73

CCHV= 0.100 CEHV= 0.300  
\*SECND 2.500

3301 HV CHANGED MORE THAN HVINS

2.50	10.66	4083.66	4080.87	0.00	4084.18	0.52	0.94	0.07	4080.00
24510.	65.	24403.	42.	34.	4218.	24.	152.	27.	4080.00
0.07	1.93	5.79	1.72	0.045	0.035	0.050	0.000	4073.00	281.68
0.001567	365.	380.	380.	2	14	0	0.00	691.64	973.32

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SECNO	DEPTH	CWSEL	CRIBS	WSELK	EG	HV	HL	GLOSS	BANK ELEV
Q	GLOB	GCH	GRDB	ALOB	ACH	AROB	VOL	TWA	LEFT/RIGHT
TIME	VLOB	VCH	VROB	XML	XNCH	XNR	WTN	ELMIN	SSTA
SLOPE	XLOBL	XLCH	XLOBR	ITRIAL	IDC	ICONT	CORAR	TOPWID	ENDST

\*SECNO 2.000

3301 HV CHANGED MORE THAN HVINS

2.00	10.11	4084.11	4082.94	0.00	4085.21	1.10	0.85	0.18	4080.00
24510.	534.	23805.	170.	152.	2790.	54.	181.	33.	4080.00
0.09	3.50	8.53	3.13	0.045	0.035	0.050	0.000	4074.00	305.93
0.004311	350.	350.	300.	2	10	0	0.00	620.53	926.46

CCHV= 0.300 CEHV= 0.500

\*SECNO 0.800

3280 CROSS SECTION 0.80 EXTENDED 5.71 FEET

3301 HV CHANGED MORE THAN HVINS

3370 NORMAL BRIDGE.NRD= 8 MIN ELTRD= 4096.00 MAX ELLC= 4100.00

7185 MINIMUM SPECIFIC ENERGY

3720 CRITICAL DEPTH ASSUMED

0.80	21.71	4101.71	4101.71	0.00	4104.60	2.89	2.14	0.89	4098.00
24510.	2547.	9498.	12464.	235.	744.	844.	215.	39.	4098.00
0.10	10.84	12.77	14.76	0.015	0.015	0.015	0.000	4080.00	0.00
0.003139	650.	650.	400.	0	10	0	-432.00	330.00	330.00

\*SECNO 0.600

3280 CROSS SECTION 0.60 EXTENDED 5.64 FEET

3370 NORMAL BRIDGE.NRD= 8 MIN ELTRD= 4096.00 MAX ELLC= 4100.40

7185 MINIMUM SPECIFIC ENERGY

3720 CRITICAL DEPTH ASSUMED

0.60	21.64	4102.04	4102.04	0.00	4104.92	2.88	0.06	0.00	4098.40
24510.	2452.	9884.	12174.	230.	762.	832.	215.	39.	4098.40
0.10	10.68	12.97	14.63	0.015	0.015	0.015	0.000	4080.40	0.00
0.003140	20.	20.	20.	0	10	0	-410.41	330.00	330.00

JFK 10/6/87  
HM 04/14/87

CROSS SECTION 4.00  
 STREAM DISCHARGE = 24510 CFS  
 DISCHARGE= 24510.

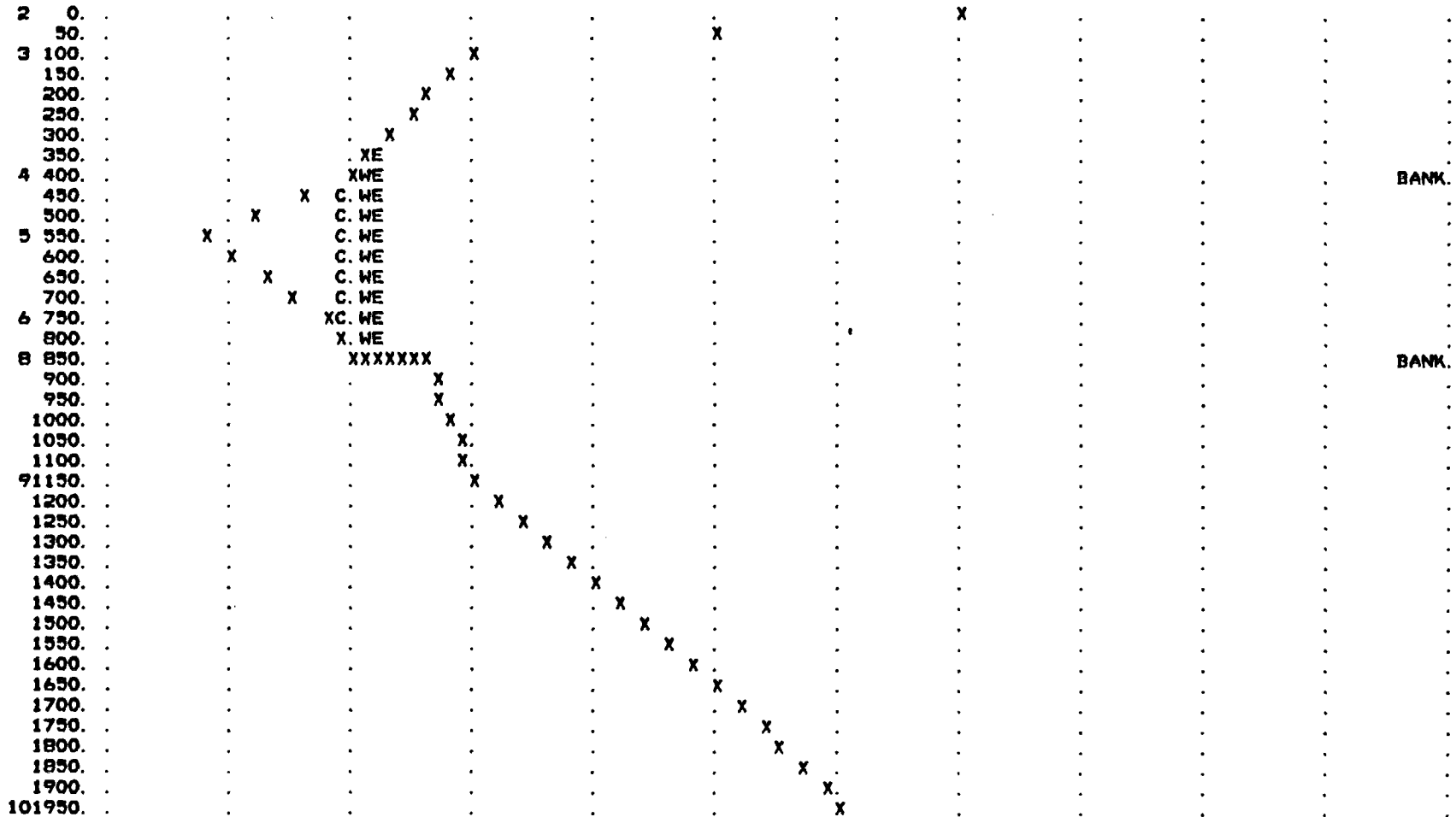
Sh. 22

PLOTTED POINTS (BY PRIORITY)-B=BOTTOM BRIDGE, T=TOP BRIDGE, X=GROUND, W=WATER SUR, E=ENERGY GRADIENT, C=CRITICAL WSEL

JKK 10/6/87  
 HM Oct 14/87

ELEV 4060. 4070. 4080. 4090. 4100. 4110. 4120. 4130. 4140. 4150. 4160.

STA-FEET



NRD= 0 ELLC= 9999999.00 ELTRD= 9999999.00

EL(I), STA(I)

4130.00	0.00	4090.00	100.00	4080.00	385.00	4068.00	530.00	4078.00	750.00
4080.00	840.00	4086.00	870.00	4090.00	1165.00	4120.00	1930.00		



CROSS SECTION 3.00  
 STREAM DISCHARGE = 24510 CFS  
 DISCHARGE= 24510.

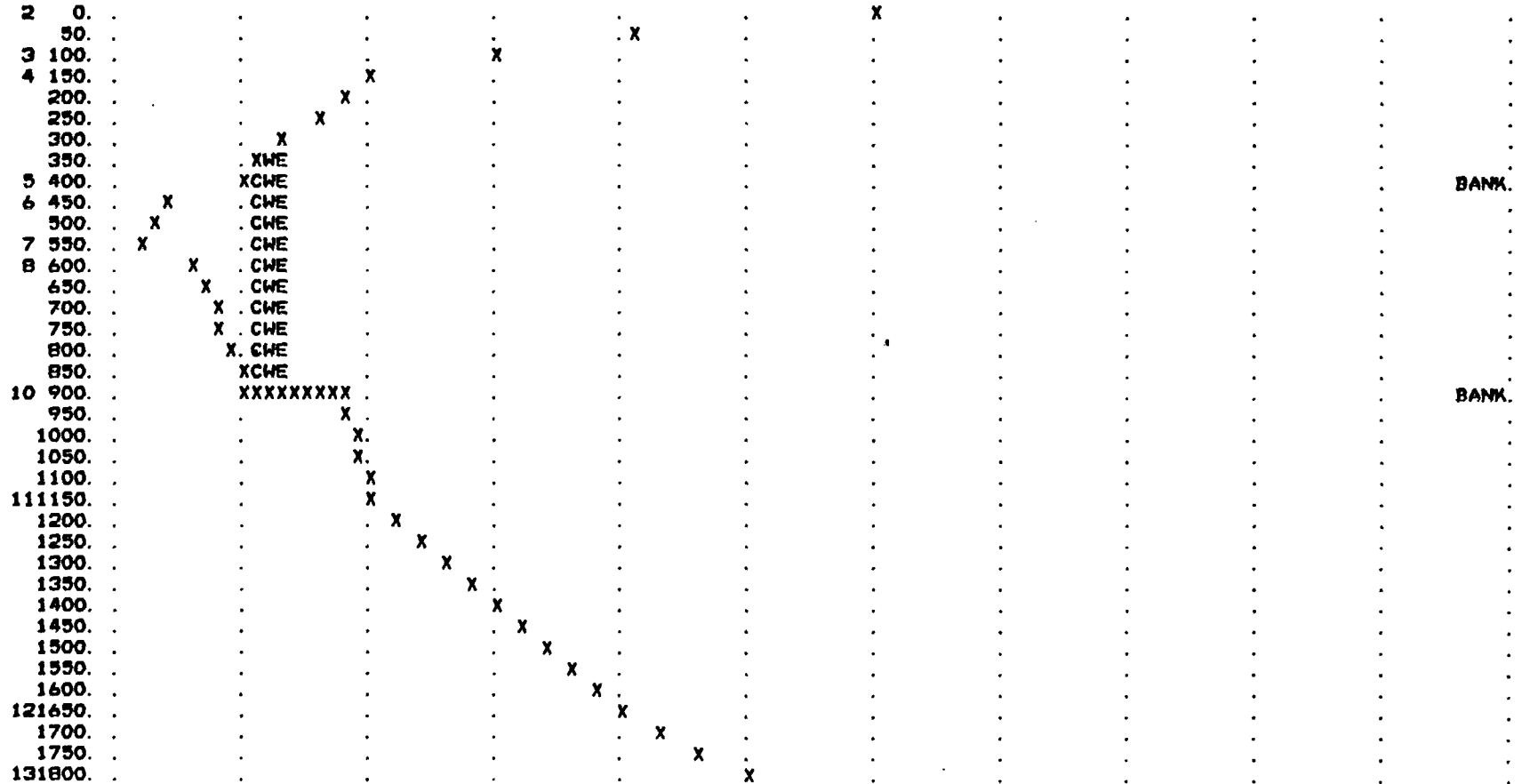
Sh. 23

JFK 10/6/87  
 HM Oct 19/87

PLOTTED POINTS (BY PRIORITY)-B=BOTTOM BRIDGE, T=TOP BRIDGE, X=GROUND, W=WATER SUR, E=ENERGY GRADIENT, C=CRITICAL WSEL

ELEV 4070. 4080. 4090. 4100. 4110. 4120. 4130. 4140. 4150. 4160. 4170.

STA-FEET



NRD= 0 ELLC= 9999999.00 ELTRD= 9999999.00

EL(I), STA(I)

4130.00	0.00	4100.00	80.00	4090.00	170.00	4080.00	400.00	4074.00	455.00
4072.00	570.00	4076.00	620.00	4080.00	880.00	4088.00	925.00	4090.00	1150.00
4110.00	1640.00	4120.00	1820.00						

PROFILE FOR STREAM DISCHARGE = 24510 CFS

Sh. 24

PLOTTED POINTS (BY PRIORITY)-E-ENERGY, W-WATER SURFACE, I-INVERT, C-CRITICAL W. S., L-LEFT BANK, R-RIGHT BANK, M-LOWER END STA

ELEVATION SECNO	4060. CUMDIS	4065.	4070.	4075.	4080.	4085.	4090.	4095.	4100.	4105.
6.80	0.	I			R.	CWE	L			M
6.50	50.	I			R.	CWE	L			M
6.00	100.	I			LC	RE				M
	150.	I			LC	RE				M
	200.	I			LC	RE				M
	250.	I			L	C.	R	WE.		M
	300.	I			L	C.	R	WE.		M
	350.	I			L	C.	R	WE.		M
5.50	400.	I			L	C.	R	WE.		M
	450.	I			L	C.	R	WE.		M
	500.	I			L	C.	R	WE.		M
	550.	I			L	CR	C	WE.		M
	600.	I			L	C	R	WE.		M
5.00	650.	I			L	LC	C	WE		M
	700.	I			L	LC	C	WE		M
	750.	I			L	LC	C	WE		M
	800.	I			L	LC	C	WE		M
	850.	I			L	LC	C	WE		M
	900.	I			L	LC	C	WE		M
	950.	I			L	LC	C	WE		M
	1000.	I			L	LC	C	WE		M
	1050.	I			L	LC	C	WE		M
4.00	1100.	I			L	LC	C	WE		M
	1150.	I			L	LC	C	WE		M
	1200.	I			L	LC	C	WE		M
	1250.	I			L	LC	C	WE		M
	1300.	I			L	LC	C	WE		M
	1350.	I			L	LC	C	WE		M
3.00	1400.	I			L	LC	C	WE		M
	1450.	I			L	LC	C	WE		M
	1500.	I			L	LC	C	WE		M
	1550.	I			L	LC	C	WE		M
	1600.	I			L	LC	C	WE		M
	1650.	I			L	LC	C	WE		M
	1700.	I			L	LC	C	WE		M
	1750.	I			L	LC	C	WE		M
2.50	1800.	I			L	LC	C	WE		M
	1850.	I			L	LC	C	WE		M
	1900.	I			L	LC	C	WE		M
	1950.	I			L	LC	C	WE		M
	2000.	I			L	LC	C	WE		M
	2050.	I			L	LC	C	WE		M
	2100.	I			L	LC	C	WE		M
2.00	2150.	I			L	LC	C	WE		M
	2200.	I			L	LC	C	WE		M
	2250.	I			L	LC	C	WE		M
	2300.	I			L	LC	C	WE		M
	2350.	I			L	LC	C	WE		M
	2400.	I			L	LC	C	WE		M

JFK  
10/6/87  
HM Oct 14/87

	2450.	.	.	.	.	I	.	.
	2500.	.	.	.	.	I	.	.
	2550.	.	.	.	.	I	.	.
	2600.	.	.	.	.	I	.	.
	2650.	.	.	.	.	I	.	.
	2700.	.	.	.	.	I	.	.
	2750.	.	.	.	.	I	.	.
0.80	2800.	.	.	.	.	I	.	.
0.60	2850.	.	.	.	.	I	.	.

L	.	CW	E	.	.	.	.	M	M
L	.	L	CW	E	.	.	.	M	M
.	L	.	L	CW	E	.	.	M	M
.	.	L	.	L	CW	E	.	M	M
.	.	.	L	.	L	CW	E	M	M
.	.	.	.	L	.	L	CW	E	M
.	.	.	.	.	L	.	L	CW	E
.	.	.	.	.	.	L	.	L	CW
.	.	.	.	.	.	.	L	.	L
.	.	.	.	.	.	.	.	L	.
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sh. 25

JHC  
10/6/87  
HM at 14/87

sh. 26

JFK 10/6/87  
HM Oct 11/87

\*\*\*\*\*  
HEC2 RELEASE DATED NOV 76 UPDATED MAY 1984  
ERROR CORR - 01, 02, 03, 04, 05, 06  
MODIFICATION - 50, 51, 52, 53, 54, 55, 56  
\*\*\*\*\*

NOTE- ASTERISK (\*) AT LEFT OF CROSS-SECTION NUMBER INDICATES MESSAGE IN SUMMARY OF ERRORS LIST

DISCHARGE = 24510 CFS

SUMMARY PRINTOUT

SECNO	Q	CWSEL	CRWS	GLOB	GCH	GROB	GLOBP	GCHP	GROBP	VLOB	VCH	VRQB	
6.800	24510.00	4077.58	4076.91	0.00	8355.28	16154.72	0.00	34.09	65.91	0.00	9.29	7.60	
6.500	24510.00	4077.70	4077.23	0.00	8703.36	15806.64	0.00	35.51	64.49	0.00	10.04	8.02	
6.000	24510.00	4078.76	4074.75	175.63	24301.58	32.79	0.72	99.15	0.13	2.25	5.31	0.60	
5.500	24510.00	4079.19	4073.92	296.22	24128.26	85.53	1.21	98.44	0.35	1.99	4.13	0.96	
5.000	24510.00	4079.19	4077.52	563.72	23920.70	25.58	2.30	97.60	0.10	2.53	7.31	2.15	
4.000	24510.00	4080.60	4078.58	4.71	24504.56	0.73	0.02	99.98	0.00	0.92	8.84	0.82	
3.000	24510.00	4081.91	4080.54	89.77	24400.66	19.57	0.37	99.55	0.08	2.15	9.02	1.91	
2.500	24510.00	4083.66	4080.87	64.79	24403.28	41.93	0.26	99.56	0.17	1.93	5.79	1.72	
2.000	24510.00	4084.11	4082.94	534.06	23805.47	170.47	2.18	97.13	0.70	3.50	8.53	3.13	
*	0.800	24510.00	4101.71	4101.71	2547.30	9498.32	12464.39	10.39	38.75	50.85	10.84	12.77	14.76
*	0.600	24510.00	4102.04	4102.04	2452.07	9883.73	12174.20	10.00	40.33	49.67	10.68	12.97	14.63

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PAGE 7

DISCHARGE = 24510 CFS

SUMMARY PRINTOUT

Sh. 27  
JFK 10/6/87  
HM old 11/87

SECNO	KRATIO	AREA	CWSEL	ELMIN	DEPTH	DIFWSX	HV	TOPWID	SSTA	ENDST	K*CHSL	10K*S
6.800	0.00	3026.37	4077.58	4060.50	17.08	0.00	1.05	896.09	362.88	1276.03	0.00	89.46
6.500	0.92	2838.68	4077.70	4060.90	16.80	0.12	1.20	861.24	378.44	1268.34	20.00	104.60
6.000	2.65	4707.16	4078.76	4062.00	16.76	1.06	0.44	955.70	77.26	1032.96	15.72	14.84
5.500	1.61	6075.21	4079.19	4062.00	17.19	0.42	0.26	844.88	143.62	988.50	0.00	5.73
5.000	0.43	3505.21	4079.19	4064.00	15.19	0.01	0.81	753.10	130.34	883.45	8.00	31.46
4.000	0.90	2778.38	4080.60	4068.00	12.60	1.41	1.21	475.05	367.94	842.99	8.70	39.02
3.000	0.93	2757.65	4081.91	4072.00	9.91	1.31	1.26	534.60	356.13	890.73	12.58	45.04
2.500	1.70	4275.74	4083.66	4073.00	10.66	1.76	0.52	691.64	281.68	973.32	2.63	15.67
2.000	0.60	2996.77	4084.11	4074.00	10.11	0.44	1.10	620.53	305.93	926.46	2.86	43.11
* 0.800	1.17	1823.16	4101.71	4080.00	21.71	17.60	2.89	330.00	0.00	330.00	9.23	31.39
* 0.600	1.00	1823.65	4102.04	4080.40	21.64	0.34	2.88	330.00	0.00	330.00	20.00	31.40

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SUMMARY OF ERRORS AND SPECIAL NOTES

CAUTION	SECNO=	0.800	PROFILE= 1	CRITICAL DEPTH ASSUMED
CAUTION	SECNO=	0.800	PROFILE= 1	MINIMUM SPECIFIC ENERGY
CAUTION	SECNO=	0.600	PROFILE= 1	CRITICAL DEPTH ASSUMED
CAUTION	SECNO=	0.600	PROFILE= 1	MINIMUM SPECIFIC ENERGY

Sh. 28

JTK 10/6/87  
HM 02/14/87

*Subcritical run*

*Sh. 29*

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HEC2 RELEASE DATED NOV 76 UPDATED MAY 1984  
ERROR CORR - 01, 02, 03, 04, 05, 06  
MODIFICATION - 50, 51, 52, 53, 54, 55, 56  
\*\*\*\*\*

*Jernu @ Jd. 6.0 ± 5.5  
(4080')*

*JRK 10/4/87  
HM NOV 02/87*

T1 UMTRA - GREEN RIVER - 100 YR  
T2 WATER SURFACE PROFILE IN BROWN WASH  
T3 DISCHARGE = 24510 CFS

J1 ICHECK INQ NINV IDIR STRT METRIC HVINS Q WSEL FQ  
0. 0. 0. 0. 0.009000 0.00 0.0 24510. 4074.000 0.000

J2 NPROF IPLOT PRFVS XSECV XSECH FN ALLDC IBW CHNIM ITRACE  
-1.000 0.000 0.000 0.000 0.000 0.000 -1.000 0.000 0.000 0.000

J3 VARIABLE CODES FOR SUMMARY PRINTOUT

38.000 43.000 1.000 2.000 13.000 14.000 15.000 35.000 60.000 59.000

55.000 26.000 56.000 0.000 38.000 58.000 25.000 1.000 42.000 8.000

51.000 10.000 4.000 53.000 54.000 33.000 5.000 0.000 0.000 0.000

NC	0.045	0.050	0.024	0.300	0.500	0.000	0.000	0.000	0.000	0.000
X1	6.800	19.000	150.000	700.000	0.000	0.000	0.000	0.000	0.000	0.000
BT	19.000	0.000	4090.000	4090.000	80.000	4080.000	4080.000	150.000	4082.000	4082.000
BT	280.000	4080.000	4080.000	340.000	4078.000	4078.000	450.000	4076.000	4076.000	560.000
BT	4075.200	4065.500	565.000	4075.000	4070.500	570.000	4075.000	4065.500	575.000	4075.000
BT	4065.500	580.000	4075.000	4070.500	585.000	4075.000	4065.500	700.000	4074.000	4074.000
BT	800.000	4074.000	4074.000	936.000	4078.000	4078.000	950.000	4076.000	4076.000	1000.000
BT	4070.000	4070.000	1070.000	4070.000	4070.000	1885.000	4100.000	4100.000	0.000	0.000
QR	4090.000	0.000	4080.000	80.000	4082.000	150.000	4080.000	280.000	4078.000	340.000
QR	4076.000	450.000	4065.500	560.000	4060.500	565.000	4065.500	570.000	4065.500	575.000
QR	4060.500	580.000	4065.500	585.000	4074.000	700.000	4074.000	800.000	4078.000	936.000
QR	4076.000	950.000	4070.000	1000.000	4070.000	1070.000	4100.000	1885.000	0.000	0.000

X1 6.500 0.000 0.000 0.000 20.000 20.000 20.000 0.000 0.400 0.000  
X2 0.000 0.000 0.000 0.000 0.000 0.000 1.000 0.000 0.000 0.000

NC 0.045 0.050 0.035 0.100 0.300 0.000 0.000 0.000 0.000 0.000  
X1 6.000 9.000 180.000 890.000 70.000 70.000 70.000 0.000 0.000 0.000  
QR 4090.000 0.000 4083.000 110.000 4080.000 180.000 4080.000 300.000 4062.000 540.000  
QR 4074.000 685.000 4078.000 890.000 4080.000 1265.000 4100.000 1885.000 0.000 0.000





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PAGE 3

Sh. 31  
JTK 10/6/87  
HM 11/02/87

SECNO	DEPTH	CWSEL	CRWS	WSELK	EG	HV	HL	LOSS	BANK ELEV
G	GLOB	GCH	GROB	ALOB	ACH	AROB	VOL	TWA	LEFT/RIGHT
TIME	VLOB	VCH	VROB	XML	XNCH	XNR	WTN	ELMIN	SSTA
SLOPE	XLOBL	XLCH	XLOBR	ITRIAL	IDC	ICONT	CORAR	TOPWID	ENDST

\*PROF 1

CRITICAL DEPTH TO BE CALCULATED AT ALL CROSS SECTIONS

CCHV= 0.300 CEHV= 0.500  
\*SECNO 6.800

3265 DIVIDED FLOW

3370 NORMAL BRIDGE, NRD= 19 MIN ELTRD= 4070.00 MAX ELLC= 4100.00

6.80	17.16	4077.66	4077.01	4074.00	4078.73	1.07	0.00	0.00	4082.00
24510.	0.	7950.	16560.	0.	831.	2169.	0.	0.	4074.00
0.00	0.00	9.56	7.64	0.000	0.024	0.050	0.000	4060.50	358.79
0.008931	0.	0.	0.	0	13	6	-1267.76	905.27	1278.05

\*SECNO 6.500

3265 DIVIDED FLOW

3370 NORMAL BRIDGE, NRD= 19 MIN ELTRD= 4070.00 MAX ELLC= 4100.40

6.50	16.87	4077.77	4077.34	0.00	4079.01	1.24	0.19	0.08	4082.40
24510.	0.	8185.	16325.	0.	790.	2009.	1.	0.	4074.40
0.00	0.00	10.36	8.13	0.000	0.024	0.050	0.000	4060.90	374.64
0.010618	20.	20.	20.	2	13	0	-1212.77	869.75	1270.22

CCHV= 0.100 CEHV= 0.300  
\*SECNO 6.000

3301 HV CHANGED MORE THAN HVINS

6.00	15.73	4077.73	4077.14	0.00	4079.96	2.23	0.66	0.30	4080.00
24510.	0.	24510.	0.	0.	2043.	0.	5.	1.	4078.00
0.00	0.00	11.99	0.00	0.000	0.035	0.000	0.000	4062.00	505.04
0.008328	70.	70.	70.	3	12	0	0.00	371.29	876.32

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Sh. 32

JTK 10/6/87  
HM 10/02/87

SECNO	DEPTH	CWSEL	CRWS	WSELK	EQ	HV	HL	QLOSS	BANK ELEV
Q	GLOB	GCH	GRDB	ALOB	ACH	AROB	VDL	TWA	LEFT/RIGHT
TIME	VLOB	VCH	VROB	XNL	XNCH	XNR	WTN	ELMIN	SSTA
SLOPE	XLOBL	XLCH	XLOBR	ITRIAL	IDC	ICONT	CDRAR	TOPWID	ENDST

\*SECNO 5.500

3301 HV CHANGED MORE THAN HVINS

5.50	18.69	4080.69	4076.98	0.00	4081.33	0.64	1.21	0.16	4080.00
24510.	96.	23319.	1095.	71.	3562.	476.	24.	6.	4076.00
0.01	1.35	6.55	2.30	0.045	0.035	0.050	0.000	4062.00	74.45
0.002784	150.	270.	280.	9	10	0	0.00	1143.57	1218.03

CCHV= 0.200 CEHV= 0.500

\*SECNO 5.000

5.00	17.39	4081.39	4077.39	0.00	4081.76	0.36	0.37	0.05	4076.00
24510.	1348.	22876.	287.	599.	4607.	266.	52.	12.	4076.00
0.03	2.25	4.97	1.08	0.045	0.035	0.050	0.000	4064.00	88.36
0.000919	230.	250.	290.	2	13	0	0.00	1038.66	1127.02

\*SECNO 4.000

4.00	13.77	4081.77	4078.53	0.00	4082.62	0.85	0.62	0.24	4080.00
24510.	63.	24437.	10.	45.	3306.	8.	99.	21.	4080.00
0.05	1.41	7.39	1.26	0.045	0.035	0.050	0.000	4068.00	334.48
0.002157	470.	460.	440.	2	14	0	0.00	314.38	848.86

\*SECNO 3.000

3.00	10.51	4082.51	4080.54	0.00	4083.53	1.02	0.83	0.08	4080.00
24510.	157.	24318.	34.	73.	2996.	18.	122.	25.	4080.00
0.06	2.17	8.12	1.93	0.045	0.035	0.050	0.000	4072.00	342.20
0.003184	315.	318.	320.	2	14	0	0.00	551.93	894.14

CCHV= 0.100 CEHV= 0.300

\*SECNO 2.500

3301 HV CHANGED MORE THAN HVINS

2.50	10.87	4083.87	4080.71	0.00	4084.35	0.49	0.77	0.05	4080.00
24510.	71.	24393.	46.	37.	4353.	27.	155.	30.	4080.00
0.08	1.90	5.60	1.69	0.045	0.035	0.050	0.000	4073.00	280.66
0.001410	365.	380.	380.	2	19	0	0.00	693.40	974.06

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SECNO	DEPTH	CHSEL	CRISW	WSELK	EQ	HV	HL	CLOSS	BANK ELEV
Q	QLOB	QCH	QROB	ALOB	ACH	AROB	VOL	TWA	LEFT/RIGHT
TIME	VLOB	VCH	VROB	XML	XNCH	XNR	WTN	ELMIN	SSTA
SLOPE	XLOBL	XLCH	XLOBR	ITRIAL	IDC	ICONT	CORAR	TOPWID	ENDST

Sh. 33

JTK 10/6/87  
HM 11/02/87

\*SECNO 2.000

3301 HV CHANGED MORE THAN HVINS

2.00	10.25	4084.25	4083.02	0.00	4085.29	1.04	0.77	0.17	4080.00
24510.	558.	23774.	178.	163.	2862.	58.	185.	35.	4080.00
0.09	3.43	8.31	3.06	0.045	0.035	0.050	0.000	4074.00	303.44
0.003950	350.	350.	300.	2	10	0	0:00	623.90	927.34

CCHV= 0.300 CEHV= 0.500

\*SECNO 0.800

3280 CROSS SECTION 0.80 EXTENDED 5.71 FEET

3301 HV CHANGED MORE THAN HVINS

3370 NORMAL BRIDGE, NRD= 8 MIN ELTRD= 4096.00 MAX ELLC= 4100.00

7185 MINIMUM SPECIFIC ENERGY

3720 CRITICAL DEPTH ASSUMED

0.80	21.71	4101.71	4101.71	0.00	4104.60	2.89	2.05	0.92	4098.00
24510.	2547.	9498.	12464.	235.	744.	844.	219.	42.	4098.00
0.10	10.84	12.77	14.76	0.015	0.015	0.015	0.000	4080.00	0.00
0.003139	650.	650.	400.	0	10	0	-432.00	330.00	330.00

\*SECNO 0.600

3280 CROSS SECTION 0.60 EXTENDED 5.64 FEET

3370 NORMAL BRIDGE, NRD= 8 MIN ELTRD= 4096.00 MAX ELLC= 4100.40

7185 MINIMUM SPECIFIC ENERGY

3720 CRITICAL DEPTH ASSUMED

0.60	21.64	4102.04	4102.04	0.00	4104.92	2.88	0.06	0.00	4098.40
24510.	2452.	9884.	12174.	230.	762.	832.	220.	42.	4098.40
0.10	10.68	12.97	14.63	0.015	0.015	0.015	0.000	4080.40	0.00
0.003140	20.	20.	20.	0	10	0	-410.41	330.00	330.00



4.35

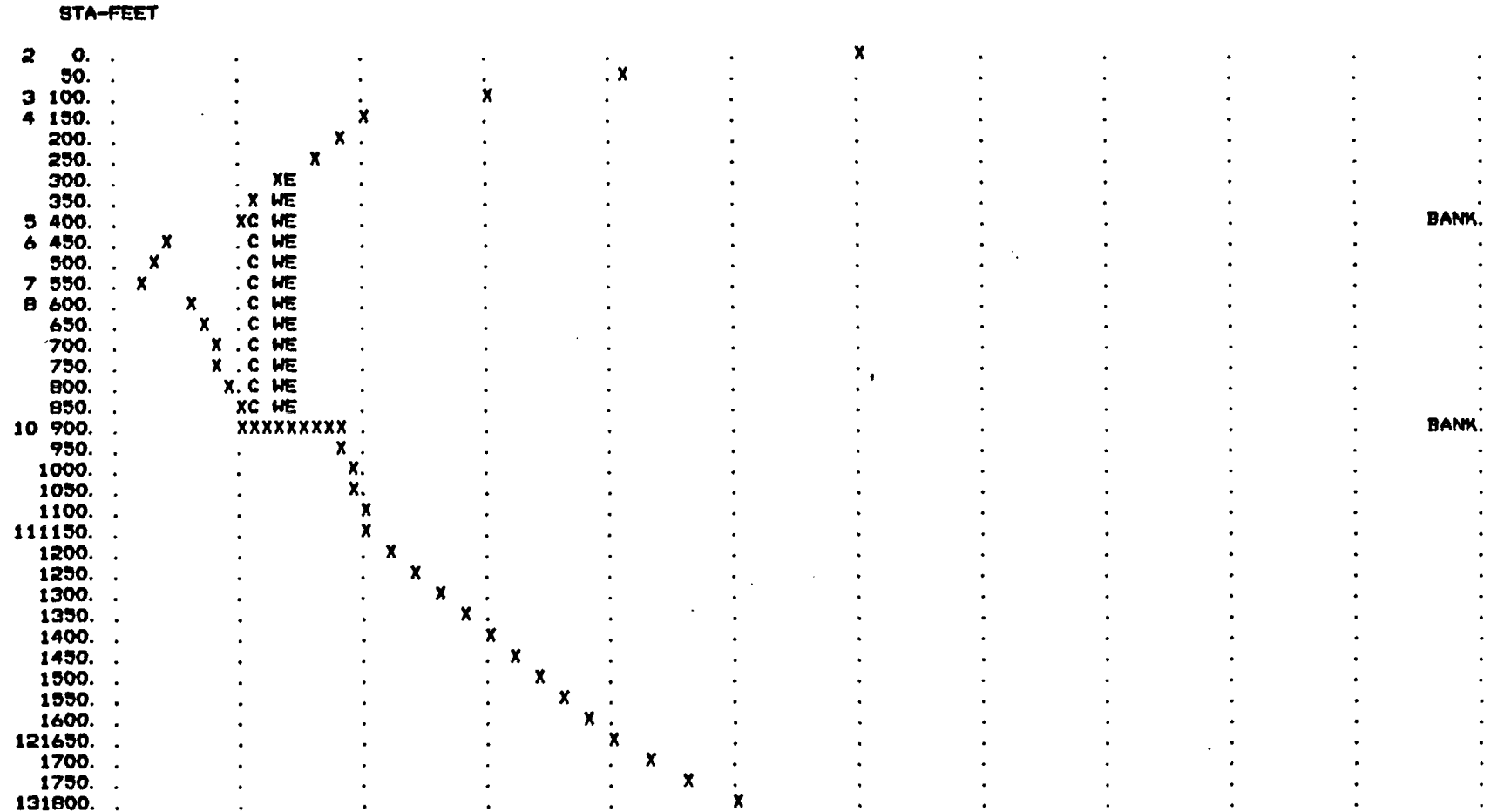
JRK 10/6/87

HN 10/02/87

CROSS SECTION 3.00  
STREAM DISCHARGE = 24510 CFS  
DISCHARGE= 24510.

PLOTTED POINTS (BY PRIORITY)-B=BOTTOM BRIDGE, T=TOP BRIDGE, X=GROUND, W=WATER SUR, E=ENERGY GRADIENT, C=CRITICAL WSEL

ELEV 4070. 4080. 4090. 4100. 4110. 4120. 4130. 4140. 4150. 4160. 4170.



NRD= 0 ELLC= 9999999.00 ELTRD= 9999999.00

EL(I), STA(I)										
4130.00	0.00	4100.00	80.00	4090.00	170.00	4080.00	400.00	4074.00	455.00	
4072.00	570.00	4076.00	620.00	4080.00	880.00	4088.00	925.00	4090.00	1150.00	
4110.00	1640.00	4120.00	1820.00							

PROFILE FOR STREAM DISCHARGE = 24310 CFS

Sh. 36

JFK 10/6/87

HM 11/02/87

PLOTTED POINTS (BY PRIORITY)-E-ENERGY, W-WATER SURFACE, I-INVERT, C-CRITICAL W. S., L-LEFT BANK, R-RIGHT BANK, M-LOWER END STA

ELEVATION SECD	4060. CUMDIS	4065.	4070.	4075.	4080.	4085.	4090.	4095.	4100.	4105.
6.80	0.	I			R.	CW E				M
6.50	50.	I			R.	CW E				M
6.00	100.	I				CWR	E			M
	150.	I				CR W	E			M
	200.	I				CR W	LE			M
	250.	I				C	WLE			M
	300.	I				RC	WE			M
	350.	I				RRC	LWE			M
5.50	400.	I				RRC	LWE			M
	450.	I				RRC	L			M
	500.	I				RRC	L			M
	550.	I				RRC	L			M
	600.	I				RRC	L			M
5.00	650.	I				L	C			M
	700.	I				L	C			M
	750.	I				L	C			M
	800.	I				L	C			M
	850.	I				L	C			M
	900.	I				L	C			M
	950.	I				L	C			M
	1000.	I				L	C			M
	1050.	I				L	C			M
4.00	1100.	I				L	C			M
	1150.	I				L	C			M
	1200.	I				L	C			M
	1250.	I				L	C			M
	1300.	I				L	C			M
	1350.	I				L	C			M
3.00	1400.	I				L	C			M
	1450.	I				L	C			M
	1500.	I				L	C			M
	1550.	I				L	C			M
	1600.	I				L	C			M
	1650.	I				L	C			M
	1700.	I				L	C			M
	1750.	I				L	C			M
2.50	1800.	I				L	C			M
	1850.	I				L	C			M
	1900.	I				L	C			M
	1950.	I				L	C			M
	2000.	I				L	C			M
	2050.	I				L	C			M
	2100.	I				L	C			M
2.00	2150.	I				L	C			M
	2200.	I				L	C			M
	2250.	I				L	C			M
	2300.	I				L	C			M
	2350.	I				L	C			M
	2400.	I				L	C			M

2450.	.	.	.	.	I	.	.	.	.	L	.	C	W	E	.	.	.	.	.	M
2500.	.	.	.	.	I	.	.	.	.	L	.	C	W	E	.	.	.	.	.	M
2550.	.	.	.	.	I	.	.	.	.	L	.	C	W	E	.	.	.	.	.	M
2600.	.	.	.	.	I	.	.	.	.	L	.	C	W	E	.	.	.	.	.	M
2650.	.	.	.	.	I	.	.	.	.	L	.	C	W	E	.	.	.	.	.	M
2700.	.	.	.	.	I	.	.	.	.	L	.	C	W	E	.	.	.	.	.	M
2750.	.	.	.	.	I	.	.	.	.	L	.	C	W	E	.	.	.	.	.	M
0.80 2800.	.	.	.	.	I	.	.	.	.	L	.	C	W	E	.	.	.	.	.	M
0.60 2850.	.	.	.	.	I	.	.	.	.	L	.	C	W	E	.	.	.	.	.	M

Sh. 37

JFK 10/6/87  
 H/M NY 02/87

Sh. 3B

JFK 10/6/87  
HM NOV 22/87

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HEC2 RELEASE DATED NOV 76 UPDATED MAY 1984  
ERROR CORR - 01, 02, 03, 04, 05, 06  
MODIFICATION - 50, 51, 52, 53, 54, 55, 56  
\*\*\*\*\*

NOTE- ASTERISK (\*) AT LEFT OF CROSS-SECTION NUMBER INDICATES MESSAGE IN SUMMARY OF ERRORS LIST

DISCHARGE = 24510 CFS

SUMMARY PRINTOUT

SECNO	Q	CWSEL	CRWS	GLOB	GCH	GROB	GLOBP	GCHP	GROBP	VLOB	VCH	VROB
6.800	24510.00	4077.66	4077.01	0.00	7949.83	16560.17	0.00	32.44	67.56	0.00	9.56	7.64
6.500	24510.00	4077.77	4077.34	0.00	8184.58	16325.42	0.00	33.39	66.61	0.00	10.36	8.13
6.000	24510.00	4077.73	4077.14	0.00	24510.00	0.00	0.00	100.00	0.00	0.00	11.99	0.00
5.500	24510.00	4080.69	4076.98	96.28	23319.14	1094.57	0.39	95.14	4.47	1.35	6.55	2.30
5.000	24510.00	4081.39	4077.39	1347.86	22875.57	286.58	5.50	93.33	1.17	2.25	4.97	1.08
4.000	24510.00	4081.77	4078.53	63.32	24436.81	9.87	0.26	99.70	0.04	1.41	7.39	1.26
3.000	24510.00	4082.51	4080.54	157.44	24318.25	34.32	0.64	99.22	0.14	2.17	8.12	1.93
2.500	24510.00	4083.87	4080.71	71.02	24393.02	45.96	0.29	99.52	0.19	1.90	5.60	1.69
2.000	24510.00	4084.25	4083.02	558.18	23773.65	178.17	2.28	97.00	0.73	3.43	8.31	3.06
* 0.800	24510.00	4101.71	4101.71	2547.30	9498.32	12464.39	10.39	38.75	50.85	10.84	12.77	14.76
* 0.600	24510.00	4102.04	4102.04	2452.07	9883.73	12174.20	10.00	40.33	49.67	10.68	12.97	14.63



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DISCHARGE = 24510 CFS

SUMMARY PRINTOUT

sh. 39

JJK 10/6/87  
MM

SECNO	KRATIO	AREA	CWSEL	ELMIN	DEPTH	DIFWSX	HV	TOPWID	SSTA	ENDST	K*CHSL	10K*B
6.800	0.00	2999.89	4077.66	4060.50	17.16	0.00	1.07	905.27	358.79	1278.05	0.00	89.31
6.500	0.92	2799.03	4077.77	4060.90	16.87	0.11	1.24	869.75	374.64	1270.22	20.00	106.18
6.000	1.13	2043.44	4077.73	4062.00	15.73	-0.04	2.23	371.29	505.04	876.32	15.72	83.28
5.500	1.73	4109.74	4080.69	4062.00	18.69	2.96	0.64	1143.57	74.45	1218.03	0.00	27.84
5.000	1.74	5471.48	4081.39	4064.00	17.39	0.70	0.36	1038.66	88.36	1127.02	8.00	9.19
4.000	0.65	3359.09	4081.77	4068.00	13.77	0.38	0.85	514.38	334.48	848.86	8.70	21.57
3.000	0.82	3086.58	4082.51	4072.00	10.51	0.74	1.02	551.93	342.20	894.14	12.58	31.84
2.500	1.50	4417.09	4083.87	4073.00	10.87	1.36	0.49	693.40	280.66	974.06	2.63	14.10
2.000	0.60	3082.59	4084.25	4074.00	10.25	0.38	1.04	623.90	303.44	927.34	2.86	39.50
* 0.800	1.12	1823.16	4101.71	4080.00	21.71	17.46	2.89	330.00	0.00	330.00	9.23	31.39
* 0.600	1.00	1823.65	4102.04	4080.40	21.64	0.34	2.88	330.00	0.00	330.00	20.00	31.40

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SUMMARY OF ERRORS AND SPECIAL NOTES

CAUTION	SECNO=	0.800	PROFILE= 1	CRITICAL DEPTH ASSUMED
CAUTION	SECNO=	0.800	PROFILE= 1	MINIMUM SPECIFIC ENERGY
CAUTION	SECNO=	0.600	PROFILE= 1	CRITICAL DEPTH ASSUMED
CAUTION	SECNO=	0.600	PROFILE= 1	MINIMUM SPECIFIC ENERGY

Sh. 40

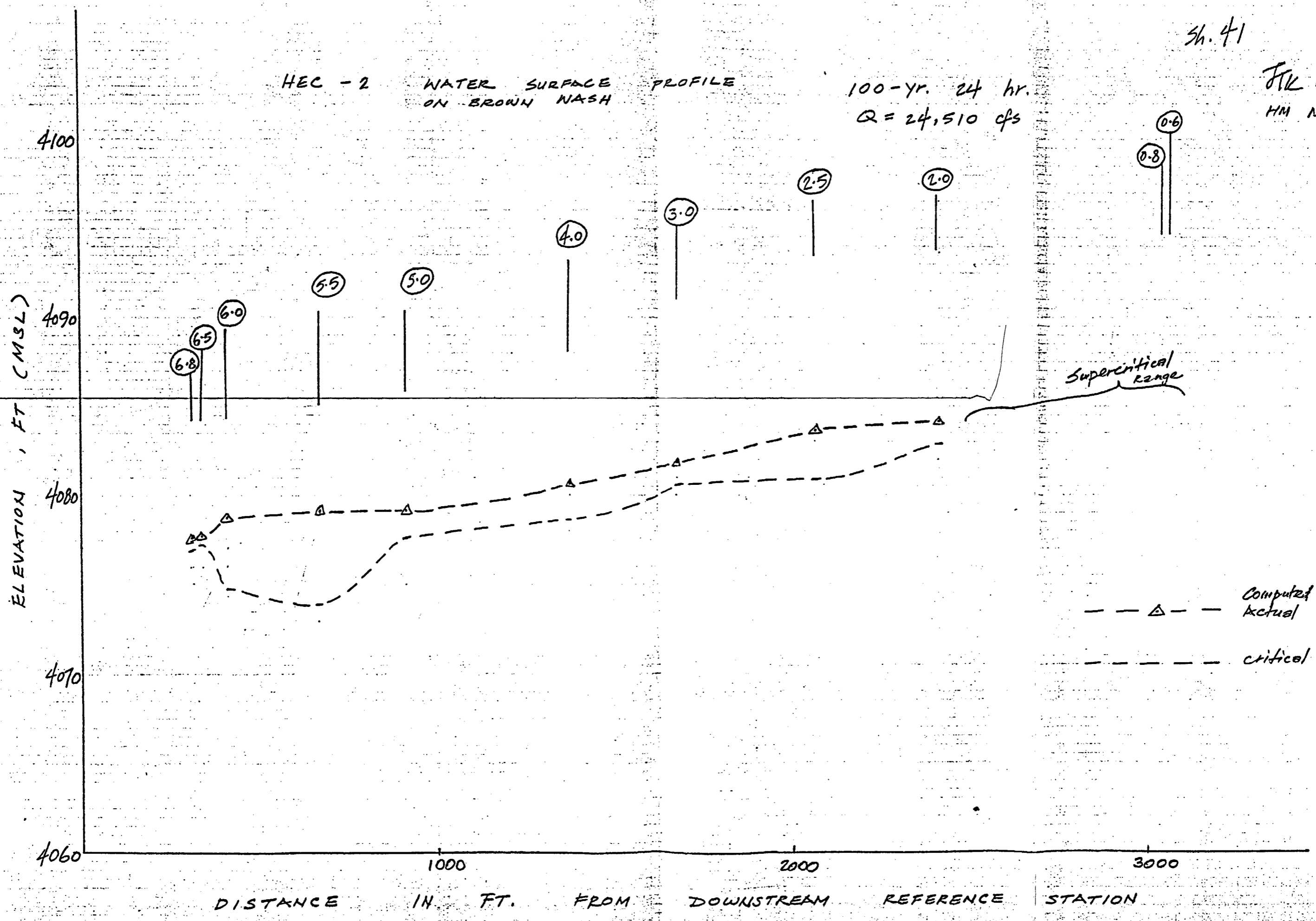
JTK 10/6/87  
HM NOV 02/87

Sh. 41

JTK 10/6/81  
HM MV 02/87

HEC - 2 WATER SURFACE PROFILE ON BROWN WASH PROFILE

100-yr. 24 hr.  
Q = 24,510 cfs



Supercritical range

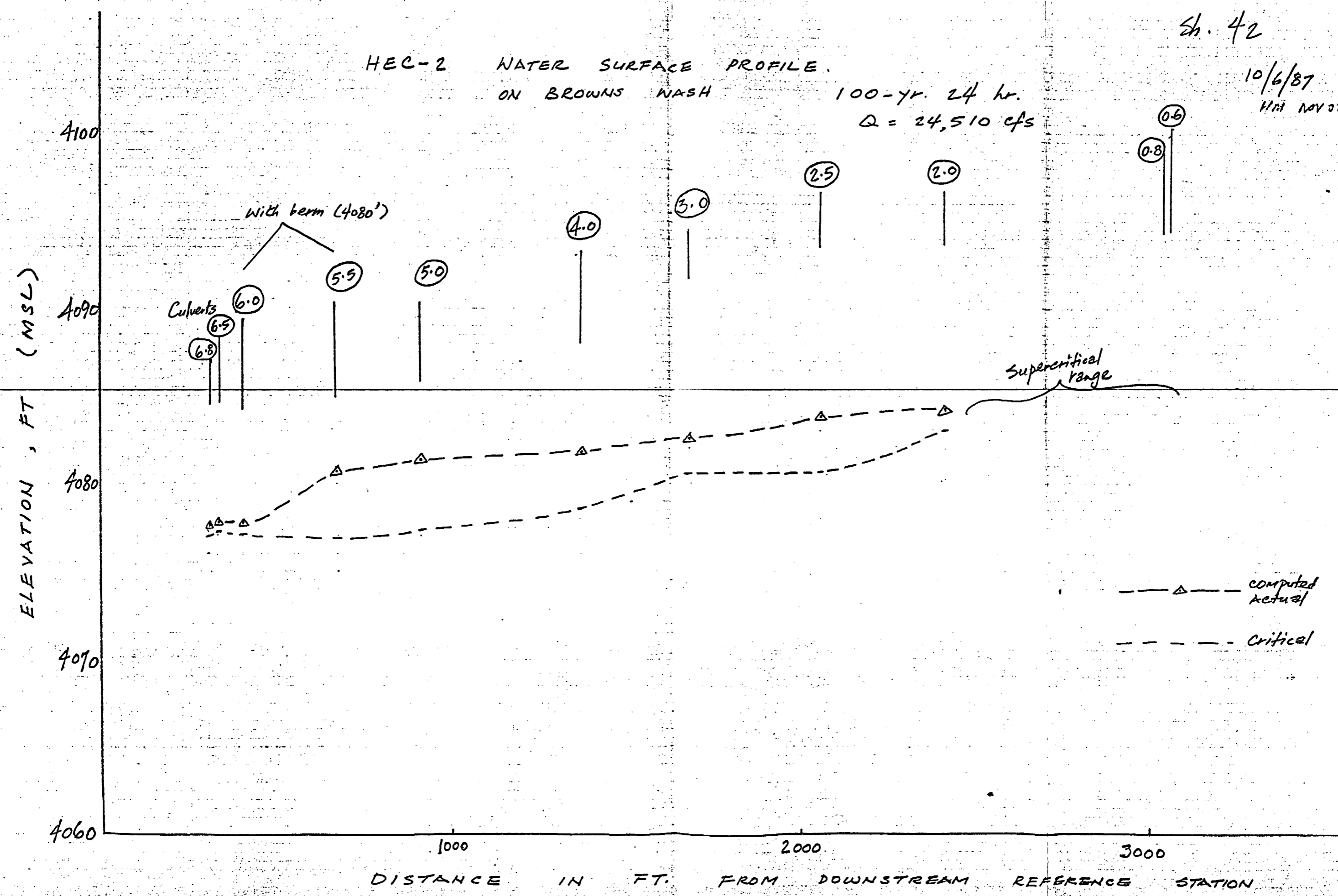
---△--- Computed Actual  
----- critical

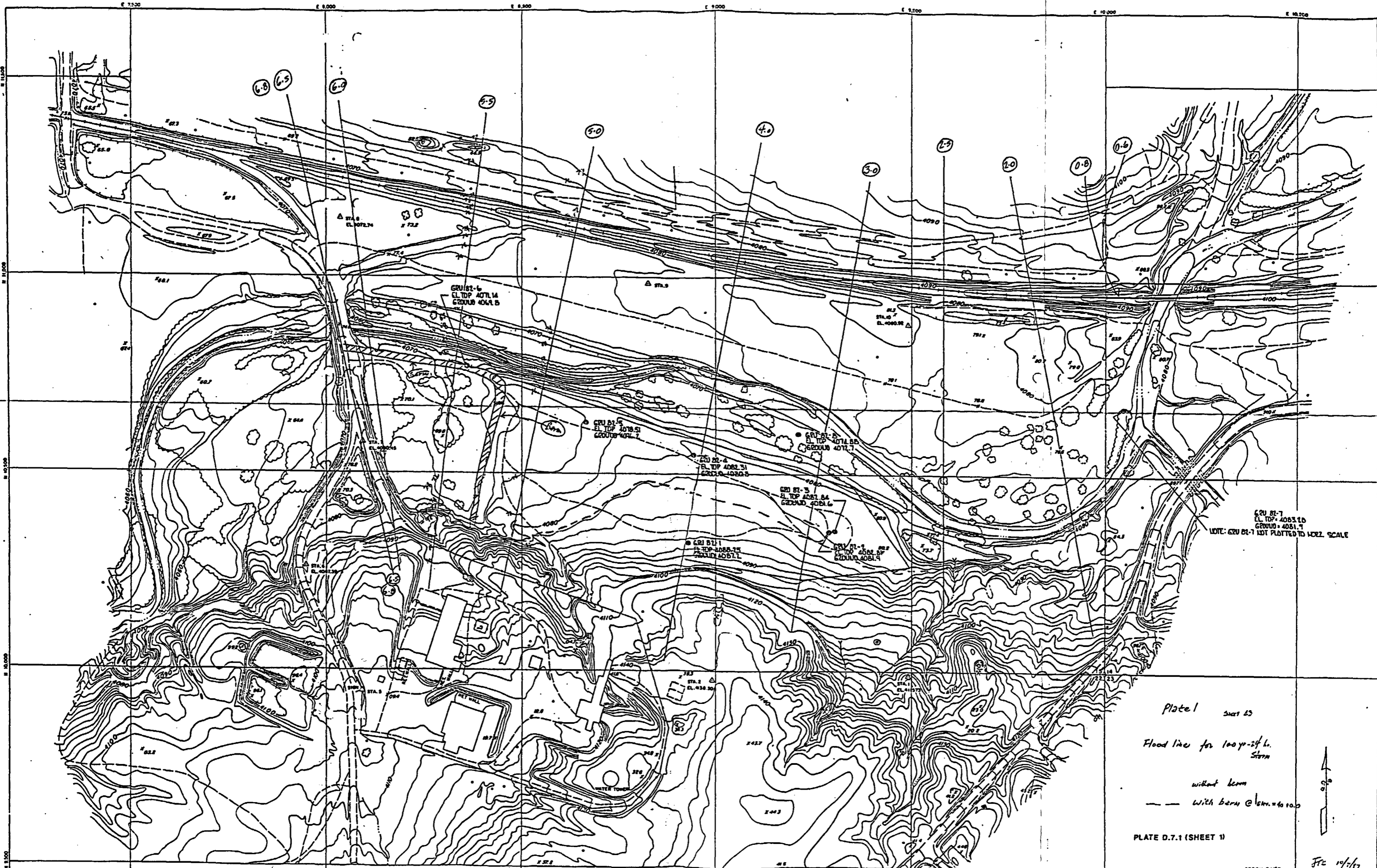
DISTANCE IN FT. FROM DOWNSTREAM REFERENCE STATION

HEC-2 WATER SURFACE PROFILE  
ON BROWNS WASH

100-YR. 24 hr.  
Q = 24,510 cfs

Sh. 42  
10/6/87  
H/M NOV 02/87





GRIST-7  
 EL TOP 4083.10  
 GROUND 4081.7  
 NOTE: GRIST-7 NOT PLOTTED TO VERT. SCALE

Plate 1 Sheet 13  
 Flood line for 100 yr-24 hr.  
 Storm  
 - - - - without berm  
 - - - - with berm @ elev. = 40.100

PLATE D.7.1 (SHEET 1)

GREEN RIVER FRZ 10/1/67  
HM 10/2/17

SHEET NO.	1
	2

SCALE 1" = 100'  
 CONTOUR INTERVAL 2'  
 PHOTOGRAPHY DATE JUL. 10, 1962