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114 - 114 - CHEMISTRY COORDINATOR: EMERGENCY PLAN-POSITION SPECIFIC PROCEDURE

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| Section 1: Release Data | | | | | | |
|---|---|-----------------------------|--|--|--|--|
| Time of release commencen | nent into river (T ₁) | · | | | | |
| Time of release termination (| (T ₂) | • | | | | |
| Duration of release $(T_3 = T_2 - T_3)$ | T ₁ , expressed in hours) | Hours | | | | |
| Sample location(s) | | | | | | |
| NOTE: Complete PA | RT I, II, or III based on location o | of sample. | | | | |
| Section 2: Determination of | of Radionuclides (from Part IV) | | | | | |
| EC fraction for all radionuclid | es at Danville (S _d) | | | | | |
| Section 3: Times of Arrival | at Danville | | | | | |
| | Transit Time to Danville (from Table 1) | Time of Arrival at Danville | | | | |
| Leading Edge | hrs | | | | | |
| Peak Concentration | hrs | | | | | |
| ailing Edgehrs | | | | | | |

PART I: Complete this part if the results are for a sample obtained directly from the SSES Cooling Tower Blowdown Discharge (CTBD) line. Otherwise, proceed to Part II of this tab. Upon completion of Part I, proceed to Part IV.

| Radionuclides in Sample | Co-60 | Sr-91 | Mo-99 | Te-132 | I-131 | 1-133 | I-134 | I-135 | Cs-134 | Cs-136 | Cs-137 | Ba-139 | Ba-140 | Ba-141 | Np-239 |
|---|-------|-------|-------|--------|-------|-------|-------|-------|--------|--------|--------|--------|--------|--------|--------|
| Radionuclide Activity Concentrations (C _I) of the Sample (μCi/ml) | | | | | | | | | | | | | 333 | | |
| EC Values (L _I) for Radionuclides (μCi/ml) ¹ | 3E-6 | 2E-5 | 2E-5 | 9E-6 | 1E-6 | 7E-6 | 4E-4 | 3E-5 | 9E-7 | 6E-6 | 1E-6 | 2E-4 | 8E-6 | , 3E-4 | 2E-5 |
| EC Fractions (F _I) of Radionuclides ² | | | | | | | | | | | | | | | • |

- 1 The EC (effluent concentration) values (L_i) are obtained from Table 2, Column 2 of Appendix B to 10CFR20. These EC values correspond to the PAG value (50 mrem CEDE) for river water at Danville.
- Obtain the EC fractions (F_i) by dividing each radionuclide concentration (C_i) by its corresponding EC value (L_i) as follows: $F_i = C/L_i$. The EC fractions are those for the water entering the Susquehanna River from the SSES discharge.

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|----|-----|----|---|
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Complete this part if the results are for a sample obtained from a waste stream entering directly into the SSES Cooling Tower Blowdown Discharge (CTBD) line. This includes results for a sample obtained from the SSES Spray Pond or from the SSES Liquid Radwaste System. Otherwise, proceed to Part III of this tab. Upon completion of Part II and Part II (continued), proceed to Part IV.

| Flow Rate (F ₁) of Waste Stream into the CTBD line (gpm) ¹ | |
|---|--|
| Flow Rate (F ₂) of CTBD line (gpm) ² | |
| Dilution Factor (D ₂) for the CTBD line ³ | |

- Obtain the flow rate (F₁) for the waste stream entering the CTBD line. If the waste stream is the SSES Spray Pond, its flow rate into the CTBD line may be determined as follows: a) Obtain the spray pond level from the Control Room, and b) Using the spray pond level, obtain the flow rate (F₁) for the spray pond from Table 2.
- 2 Obtain the flow rate (F₂) of the CTBD line from the TSC Chemistry Coordinator or TSC Coordinator, if possible. If the actual flow rate can't be obtained from the TSC Coordinator or TSC Chemistry Coordinator, assume that it is 5,000 gpm.
- 3 The dilution factor (D₂) for the CTBD line is obtained by dividing the sum of the waste stream and CTBD line flow rates (F_1+F_2) by the waste stream flow rate (F_1) as follows: D₂ = (F_1+F_2)/ F_1 .

PART II (Continued)

| Radionuclides in Sample | Co-60 | Sr-91 | Mo-99 | Te-132 | I-131 | 1-133 | 1-134 | I-135 | Cs-134 | Cs-136 | Cs-137 | Ba-139 | Ba-140 | Ba-141 | Np-239 |
|--|-------|-------|-------|--------|-------|-------|-------|-------|--------|--------|--------|--------|--------|--------|--------|
| Radionuclide Activity Concentrations (C _i) of the Sample (μCi/ml) | | | | | | | | | | | | | | | |
| Expected Radionuclide Activity Concentration (E₂) in the CTBD Line (μCi/ml) ⁴ | | | | | | | | | | | | | | | |
| EC Values (L _I) for Radionuclides (μCi/ml) ⁵ | 3E-6 | 2E-5 | 2E-5 | 9E-6 | 1E-6 | 7E-6 | 4E-4 | 3E-5 | 9E-7 | 6E-6 | 1E-6 | 2E-4 | 8E-6 | 3E-4 | 2E-5 |
| EC Fractions (F _I) of Radionuclides ⁶ | | | | | | | | | | | | | | | |

- Obtain the radionuclide concentrations expected (E_2) in the CTBD line by dividing the radionuclide concentrations (C_1) by the CTBD line dilution factor (D_2) as follows: $E_2 = C_1/D_2$.
- 5 The EC (effluent concentration) values (L_I) are obtained from Table 2, Column 2 of Appendix B to 10CFR20. These EC values correspond to the PAG value (50 mrem CEDE) for river water at Danville.
- Obtain the EC fractions (F_1) by dividing each expected radionuclide concentration (E_2) by its corresponding EC value (L_1) as follows: $F_1 = E_2/L_1$. The EC fractions are those for the water entering the Susquehanna River from the SSES discharge.

PART III: Complete this part if the results are for a sample obtained from a waste stream entering into the Spray Pond before being released to the SSES Cooling Tower Blowdown Discharge (CTBD) line. Upon completion of Part III and Part III (continued), proceed to Part IV.

| Volume (V) of Release into the Spray Pond (gallons) ¹ | |
|---|--|
| SSES Spray Pond Level ² | |
| Dilution Factor (D₁) for the Spray Pond³ | |
| Flow Rate (F ₁) of Spray Pond into the CTBD line (gpm) ⁴ | |
| Flow Rate (F₂) of CTBD line (gpm) ⁵ | |
| Dilution Factor (D₂) for the CTBD line ⁶ | |

- 1 Obtain the volume of the release to the Spray Pond from the TSC Chemistry Coordinator or TSC Coordinator.
- 2 Obtain the SSES Spray Pond level from the Control Room.
- Obtain the dilution factor (D₁) for the Spray Pond by dividing 2E7 by the volume (V) of the release into the Spray Pond as follows: $D_1 = 2E7/V$.
- 4 Obtain the flow rate (F₁) from the SSES Spray Pond from Table 2. (Spray Pond level is obtained from the Control Room, see Step 2.).
- 5 Obtain the flow rate (F₂) of the CTBD line from the TSC Chemistry Coordinator or TSC Coordinator, if possible. If the actual flow rate can't be obtained from the TSC Coordinator or TSC Chemistry Coordinator, assume that it is 5,000 gpm.
- Obtain the dilution factor (D₂) for the CTBD line by dividing the sum of the Spray Pond (waste stream) and CTBD line flow rates (F_1+F_2) by the Spray Pond flow rate (F_1) as follows: $D_2 = (F_1 + F_2)/F_1$.

PART III (Continued)

| Radionuclides in Sample | Co-60 | Sr-91 | Mo-99 | Te-132 | 1-131 | 1-133 | I-134 | I-135 | Cs-134 | Cs-136 | Cs-137 | Ba-139 | Ba-140 | Ba-141 | Np-239 |
|--|-------|-------|-------|--------|-------|-------|-------|-------|--------|--------|--------|--------|--------|--------|--------|
| Radionuclide Activity Concentrations (C _i) of the Sample (µCi/ml) | | | | | | | | | | | | | | | |
| Expected Radionuclide Activity Concentration (E ₁) in the Spray Pond (μCi/ml) ⁷ | | | | | | | | | | | | | | | |
| Expected Radionuclide Activity Concentration (E ₂) in the CTBD Line (μCi/ml) ⁸ | | | | | | | | | | | | | | | • |
| EC Values (L _I) for Radionuclides (μCi/ml) ⁹ | 3E-6 | 2E-5 | 2E-5 | 9E-6 | 1E-6 | 7E-6 | 4E-4 | 3E-5 | 9E-7 | 6E-6 | 1E-6 | 2E-4 | 8E-6 | 3E-4 | 2E-5 |
| EC Fractions (F _i) of Radionuclides ¹⁰ | | | | | | | | | | | | | | | |

- Obtain the radionuclide concentrations expected (E_1) in the Spray Pond by dividing the radionuclide concentrations (C_1) of the sample by the dilution factor (D_1) of the Spray Pond as follows: $E_1 = C_1/D_1$.
- Obtain the radionuclide concentrations expected (E_2) in the CTBD line by dividing the radionuclide concentrations (E_1) by the CTBD line dilution factor (D_2) as follows: $E_2 = E_1/D_2$.
- 9 The EC (effluent concentration) values (L_I) are obtained from Table 2, Column 2 of Appendix B to 10CFR20. These EC values correspond to the PAG value (50 mrem CEDE) for river water at Danville.
- 10 Obtain the EC fractions (F_1) by dividing each expected radionuclide concentration (E_2) by its corresponding EC value (L_1) as follows: $F_1 = E_2/L_1$. The EC fractions are those for the water entering the Susquehanna River from the SSES discharge.

PART IV: Complete this part using the results obtained from either Parts I, II, or III, as applicable.

| Undiluted Sum (S) of EC Fractions for all Radionuclides ¹ | |
|--|------|
| River Depth (R _{CR}) Read at the Control Room – 0C653 or ENVIR in PICSY ² | |
| Dispersion Factor to Danville (M) from Table 1 | · . |
| Diluted Sum (S _d) of EC Fractions for all Radionuclides at Danville ^{3,4} | |

- Obtain the undiluted sum (S) of EC fractions for all radionuclides by adding the EC fractions (F_i) for all radionuclides as follows: $S = \Sigma F_i$. Obtain the EC fractions from either Part I, II, or III, as appropriate.
- 2 If the river depth (R_{EL}) read at the SSES Environmental Lab is available, convert to the depth (R_{CR}) read at the Control Room as follows: $R_{CR} = 12 \times R_{EL} + 126$.
- Obtain the diluted sum (S_d) of EC fractions by dividing the undiluted sum (S) of EC fractions by the dispersion factor (M) as follows: $S_d = S/M$.
- 4 The diluted sum of EC fractions is at Danville after dilution of the SSES effluent by the Susquehanna River enroute.

TABLE 1

SUSQUEHANNA RIVER:

DEPTH - DISPERSION FACTOR - TRANSIT TIME TO DANVILLE

| RIVER DEPTH | DISPERSION AT DANVILLE | TR | ANSIT TIME (hou | ırs) |
|----------------|---------------------------|--------------|-----------------|---------------|
| (in)* | (M) | Leading Edge | Peak Conc | Trailing Edge |
| 144 | 136.4 | 68.7 | 74.3 | 141.2 |
| 150 | 155.5 | 64.8 | 70.3 | 136.5 |
| 156 | 179.2 | 61.1 | 66.5 | 131.9 |
| 162 | 208.3 | 57.2 | 62.3 | 127.2 |
| 168 | 281.3 | 45.9 | 52.4 | 112.9 |
| 174 | 250.6 | 35.5 | 41.2 | 99.7 |
| 180 | 261.5 | 34.5 | 40.0 | 95.6 |
| 186 | 277.8 | 33.0 | 38.3 | 90.2 |
| 192 | 297.3 | 31.4 | 36.4 | 84.0 |
| 198 | 323.6 | 29.5 | 34.3 | 76.7 |
| 204 | 366.7 | 26.9 | 31.3 | 66.7 |
| 210 | 456.6 | 23.0 | 27.2 | 52.7 |
| 216 | 588.2 | 20.0 | 24.0 | 40.8 |
| 222 | 869.6 | 16.5 | 20.5 | 27.5 |
| 228 | 980.4 | 15.3 | 19.3 | 24.3 |
| 234 | 1072 | 14.7 | 18.7 | 23.7 |
| 240 | 1174 | 14.2 | 18.2 | 23.0 |
| 246 | 1285 | 13.5 | 17.5 | 22.5 |
| 258 | 1567 | 12.2 | 16.2 | 21.0 |
| 270_ | 2058 | 10.7 | 14.7 | 19.5 |
| 282 | 2597 | 10.0 | 14.0 | 18.7 |
| 294 | 3068 | 9.8 | 13.8 | 18.3 |
| 306 | 3559 | 9.8 | <u> </u> | 18.0 |
| 318 | 4082 | 9.8 | 13.8 | 17.7 |
| 330 | 4651 | 9.7 | 13.7 | 17.2 |
| 342_ | 5236 | 9.7 | 13.7 | 16.8 |
| 354 | 5882 | 9.7 | 13.7 | 16.3 |
| 366 | 6536 | 9.5 | 13.5 | 16.0 |
| 378 | 7246 | 9.5 | 13.5 | 15.5 |
| 390 | 8000 | 9.3 | 13.3 | 15.0 |

TABLE 2
DISCHARGE FROM SPRAY POND TO COOLING TOWER BLOWDOWN LINE

^{*} For depth readings found between depths stated above, round to closest figure. If value falls exactly between two depths reported above, round to the lesser value. EP-AD-000-138, Revision 7, Page 8 of 9

VS. SPRAY POND WATER SURFACE ELEVATION

| SPRAY POND | DISCHARGE RATE | | | | |
|------------------|----------------|--|--|--|--|
| WATER SURFACE | TO BLOWDOWN | | | | |
| ELEVATION | CONDUIT (I) | | | | |
| (feet above msl) | (gpm) | | | | |
| 678.5 | 0 | | | | |
| .6 | 541 | | | | |
| 7 | 1,530 | | | | |
| .8 | 2,849 | | | | |
| .9 | 4,445 | | | | |
| 679.0 | 6,213 | | | | |
| .1 | 8,166 | | | | |
| .2 | 10,271 | | | | |
| 3 | 12,525 | | | | |
| 4 | 14,804 | | | | |
| 5 | 14,964 | | | | |
| .6 | 15,123 | | | | |
| 7 | 15,279 | | | | |
| .8 | 15,434 | | | | |
| 9 | 15,588 | | | | |
| 680.0 | 15,740 | | | | |
| .1 | 15,891 | | | | |
| .2 | 16,040 | | | | |
| .3 | 16,188 | | | | |
| .4 | 16,334 | | | | |
| .5 | 16,480 | | | | |
| .6 | 16,624 | | | | |
| 7 | 16,766 | | | | |
| .8 | 16,907 | | | | |
| .9 | 17,048 | | | | |

| | | | | | |
|------------------|----------------|--|--|--|--|
| SPRAY POND | DISCHARGE RATE | | | | |
| WATER SURFACE | TO BLOWDOWN | | | | |
| ELEVATION | CONDUIT (I) | | | | |
| (feet above msl) | (gpm) | | | | |
| 681.0 | 17,187 | | | | |
| .1 | 17,325 | | | | |
| .2 | 17,462 | | | | |
| .3 | 17,598 | | | | |
| .4 | 17,733 | | | | |
| .5 | 17,867 | | | | |
| .6 | 18,000 | | | | |
| .7 | 18,131 | | | | |
| .8 | 18,262 | | | | |
| .9 | 18,392 | | | | |
| 682.0 | 18,521 | | | | |
| .1 | 18,649 | | | | |
| .2 | 18,777 | | | | |
| .3 | 18,903 | | | | |
| .4 | 19,029 | | | | |
| .5 | 19,154 | | | | |
| .6 | 19,278 | | | | |
| .7 | 19,401 | | | | |
| .8 | 19,523 | | | | |
| .9 | 19,645 | | | | |
| 683.0 | 19,766 | | | | |
| .1 | 19,886 | | | | |
| .2 | 20,005 | | | | |
| .3 | 20,124 | | | | |
| .4 | 20,242 | | | | |
| .5 | 20,359 | | | | |