

# NEAR-FIELD DRIPPING AND THERMAL MODELS

*Presented by*  
**Debra L. Hughson**  
**210/522-3805 (dhughson@swri.edu)**  
**Center for Nuclear Waste Regulatory Analyses**

**May 25, 1999**  
**San Antonio, Texas**

**DOE/NRC Technical Exchange on**  
**Total System Performance Assessments for Yucca Mountain**

# **IMPORTANCE TO PERFORMANCE ASSESSMENT**

---

- **Differences in the Amount of Seepage Into the Emplacement Drifts and Onto WPs Lead to Calculated Radionuclide Releases That Vary by Several Orders of Magnitude.**
- **Seepage Into Drifts and Onto WPs Is a Complex Process With Large Uncertainties. Both DOE and NRC Performance Assessments Use a Much Simplified Approach to Seepage Abstraction. Given the Large Uncertainties It Is Desirable to Err on the Conservative Side.**

## **CONCERNS**

---

- **Data Needed to Characterize Heterogeneity Have Not Been Collected in the Main Repository Block**
- **Existing Models Do Not Capture the Scales of Variability**
- **Degradation of Emplacement Drifts Is Neglected**
- **Several Thousands of Years of WP Performance Are Gained by Assuming No Dripping Occurs During the Thermal Period**

# OUTLINE

---

- **Seepage Into Drifts Process Model**
  - **Model scales and fracture properties**
  - **Drift degradation**
- **Thermal Abstraction**
  - **Neglecting seepage during thermal period**



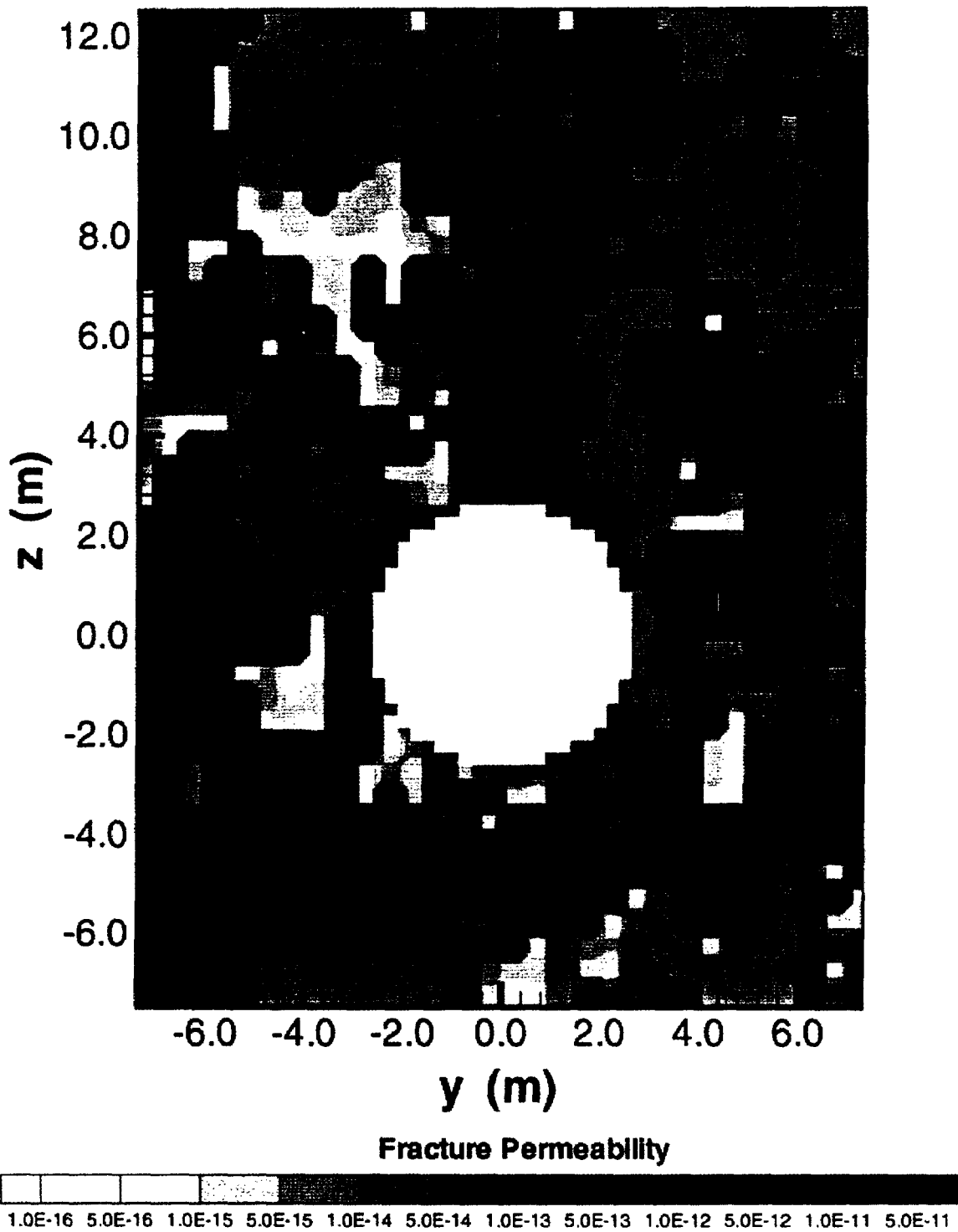


Figure 2-58b. Simulated Heterogeneous-Permeability Field for Vertical Slice 2 of the 3-D Block

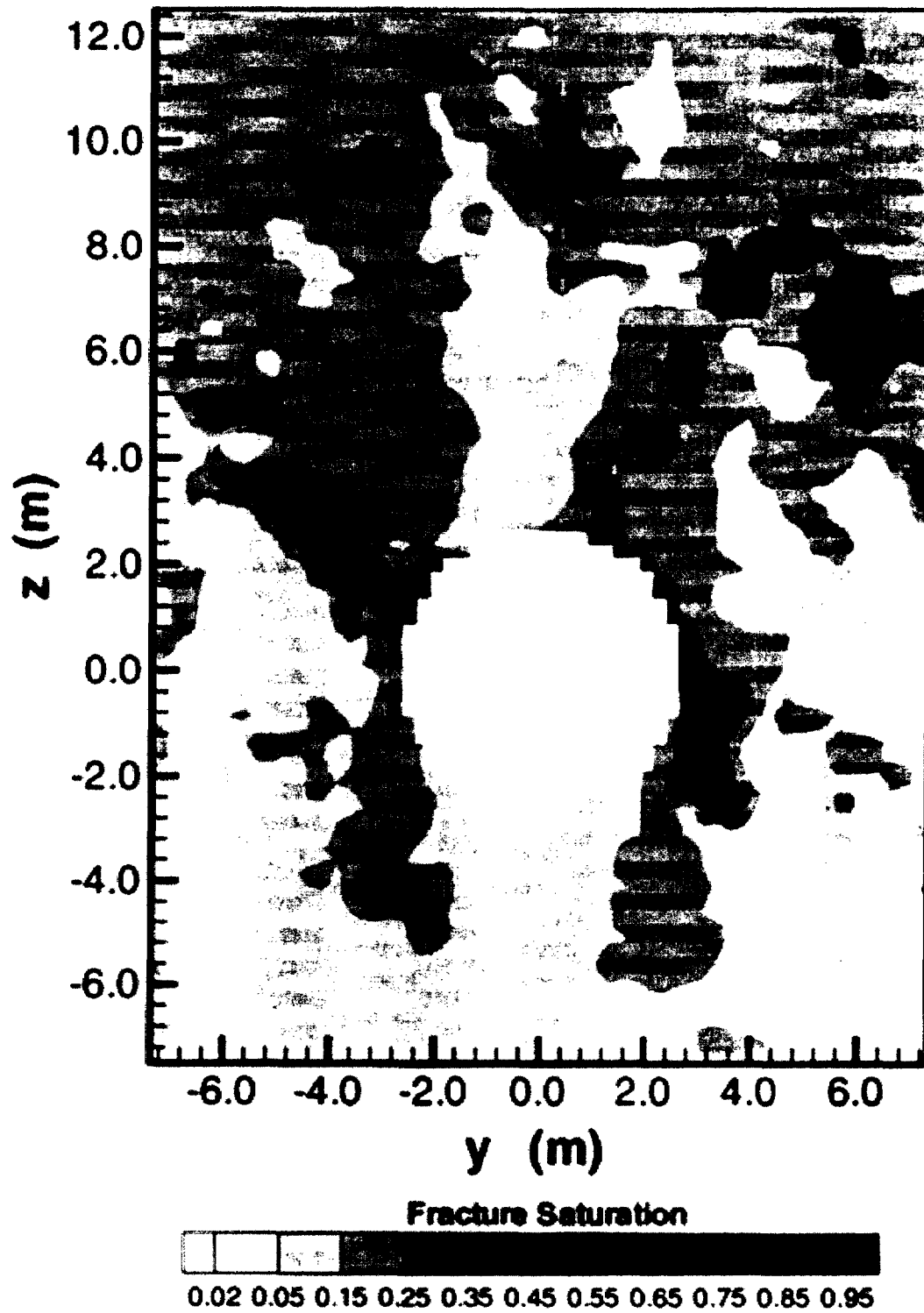
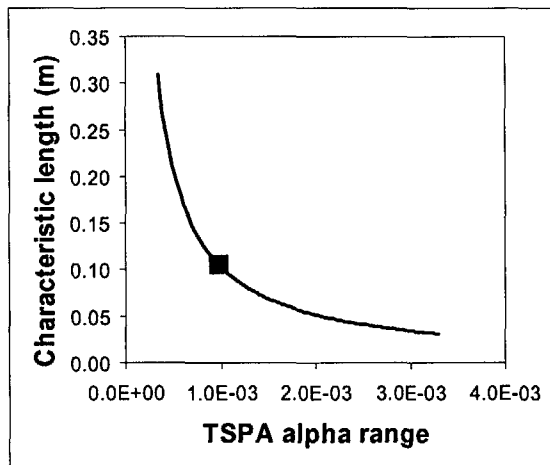


Figure 2-71a. Calculated Saturation Profiles in Fracture Continuum on Slice 1 of the 3-D Block at  $t = t_p = 1$  Year

# BASE CASE PARAMETERS AND PHYSICAL INTERPRETATION

---



**Fracture Permeability**  
 $k_s = 10^{-14}, 10^{-13}, 10^{-12} \text{ m}^2$

**Fracture Alpha Parameter**  
 $\alpha = 3.3\text{E-}4, 9.7\text{E-}4, 3.3\text{E-}3 \text{ Pa}^{-1}$

*pore size distribution*

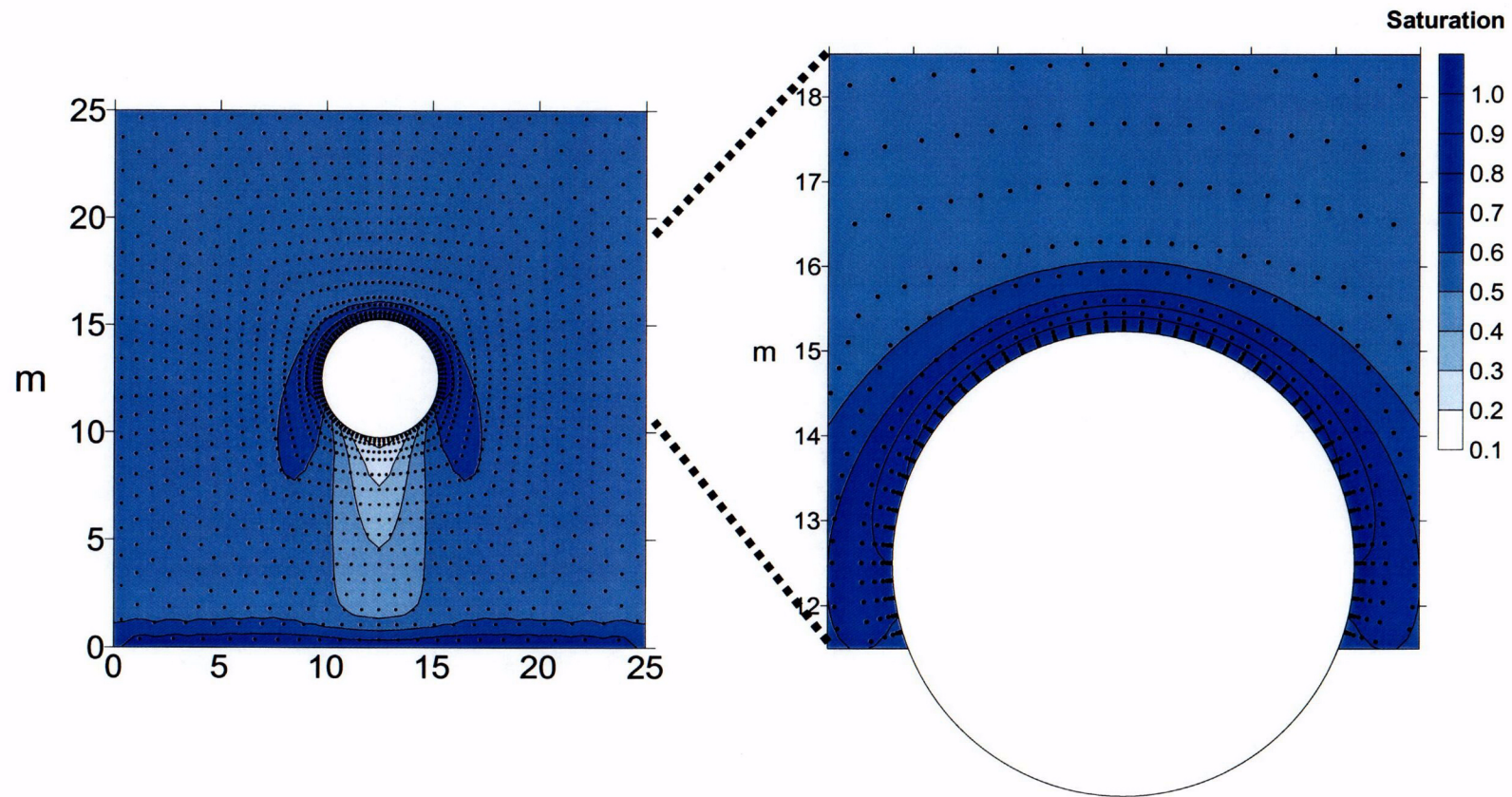
**Threshold Percolation Flux**

$$q^* = \frac{k_s}{\vartheta}$$

$\vartheta$  Is Dimensionless Potential, a Function of  $\alpha$  and Drift Radius

# BOUNDARY LAYER FORMED WITH MEDIAN

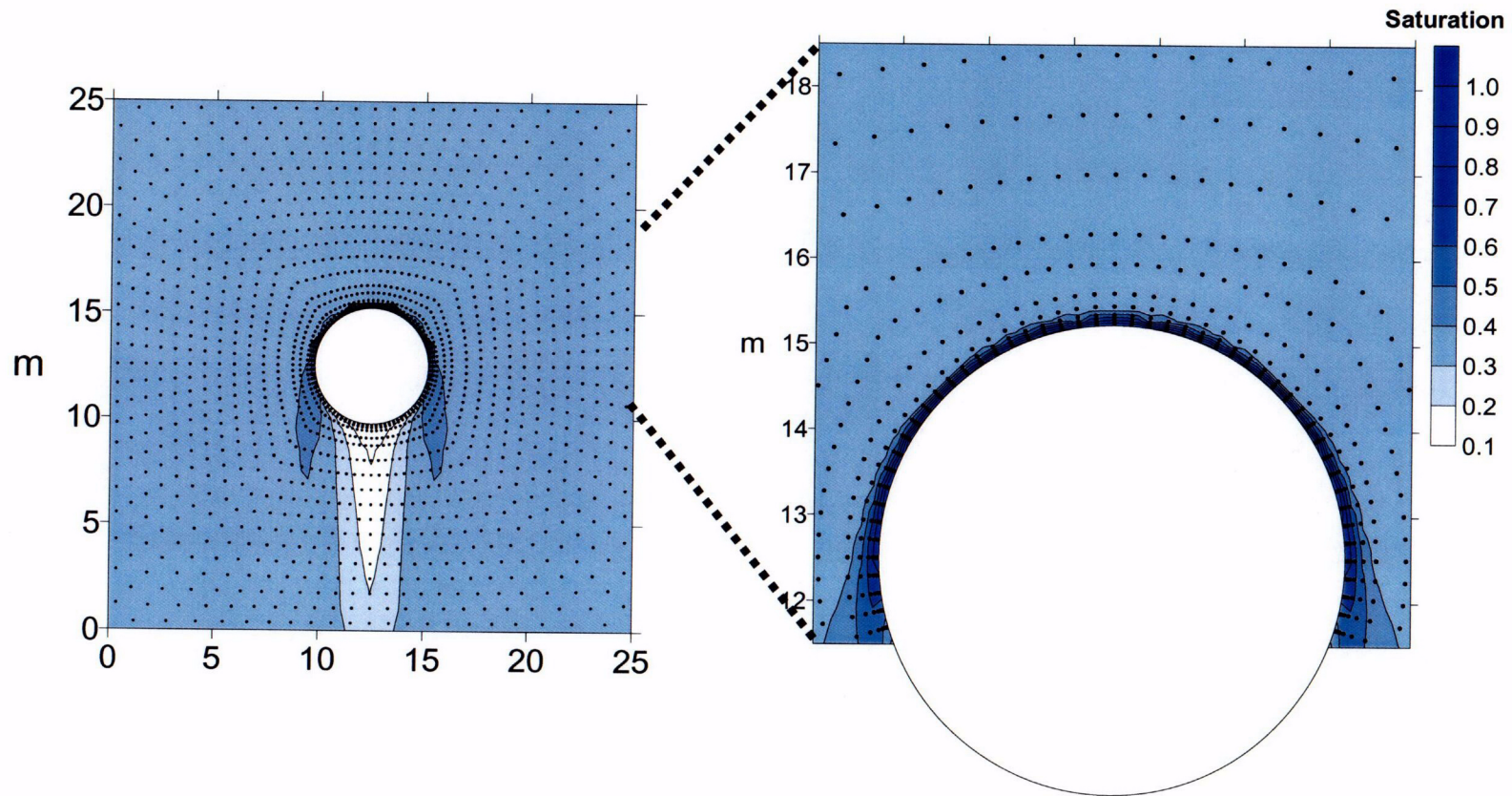
$$\alpha = 9.7 \times 10^{-4} \text{ Pa}^{-1}$$



C-01

# BOUNDARY LAYER FORMED WITH MAXIMUM

$$\alpha = 3.3 \times 10^{-3} \text{ Pa}^{-1}$$



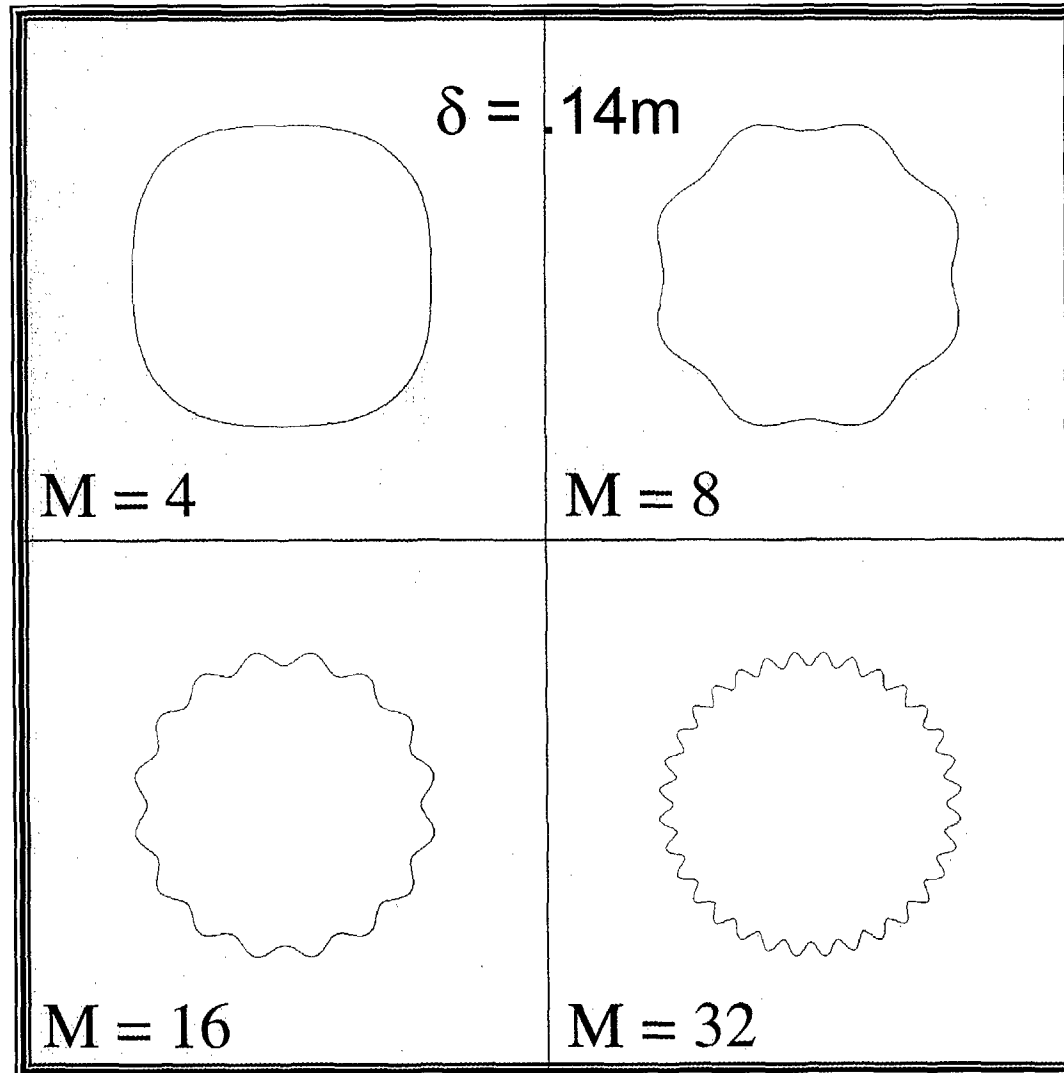
C-02

# **COMMENTS ON SCALE AND HETEROGENEITY**

---

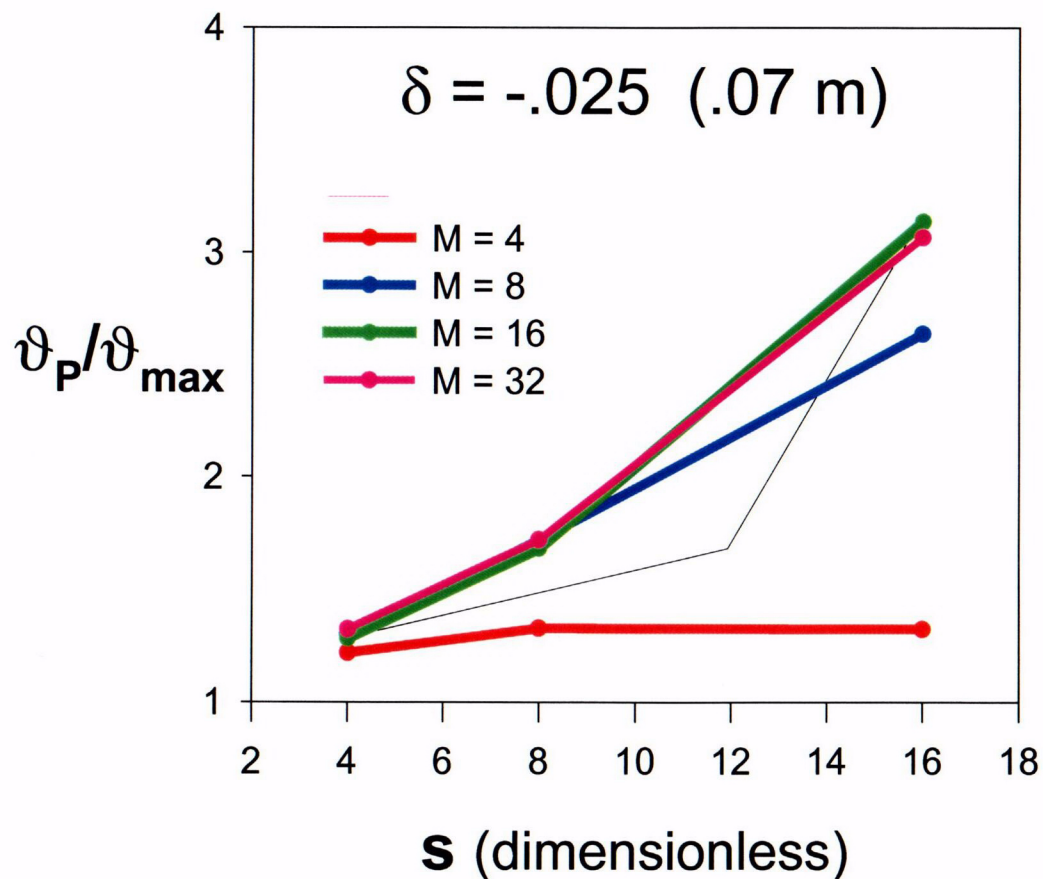
- **Model Scales and Fracture Properties**
  - **Heterogeneity in the alpha parameter within the boundary layer may be important**
- **Drift Degradation and Wall Irregularity: What Happens If the Boundary Layer Shape Is Perturbed?**

# MODEL SHAPES FOR DRIFT DEGRADATION





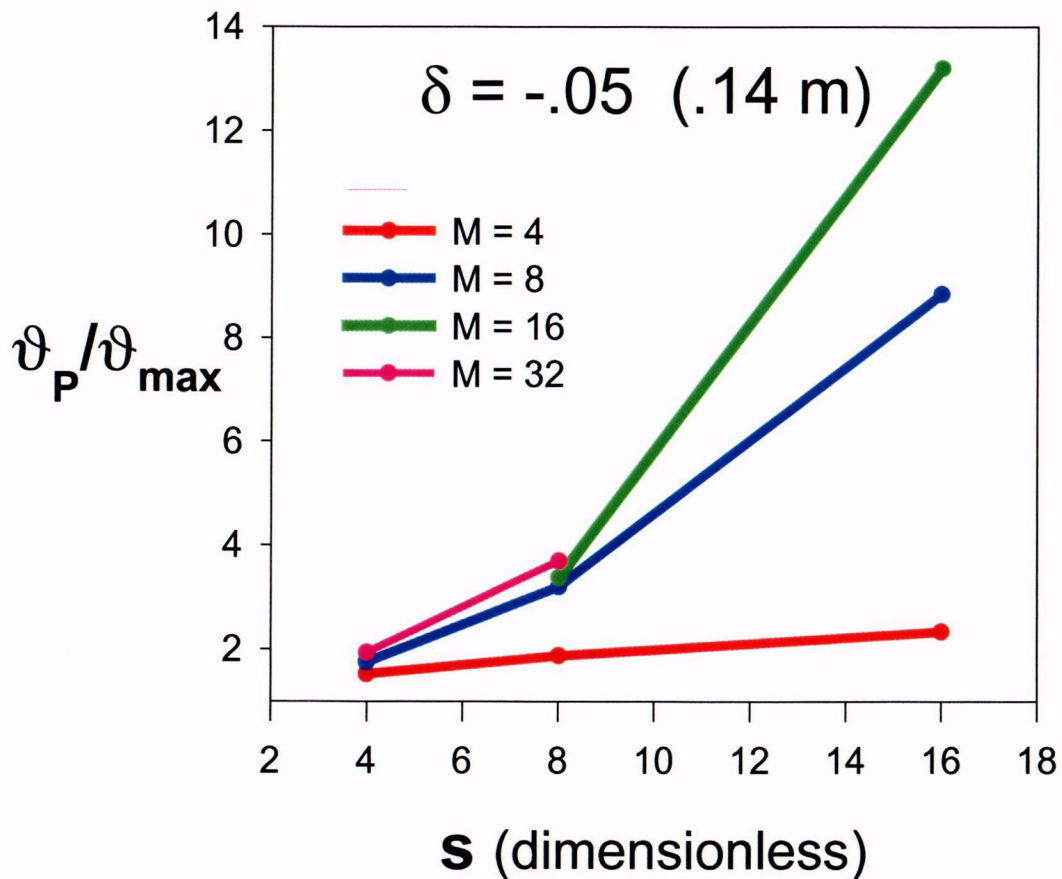
# FACTOR BY WHICH THRESHOLD PERCOLATION FLUX IS DECREASED



C-03



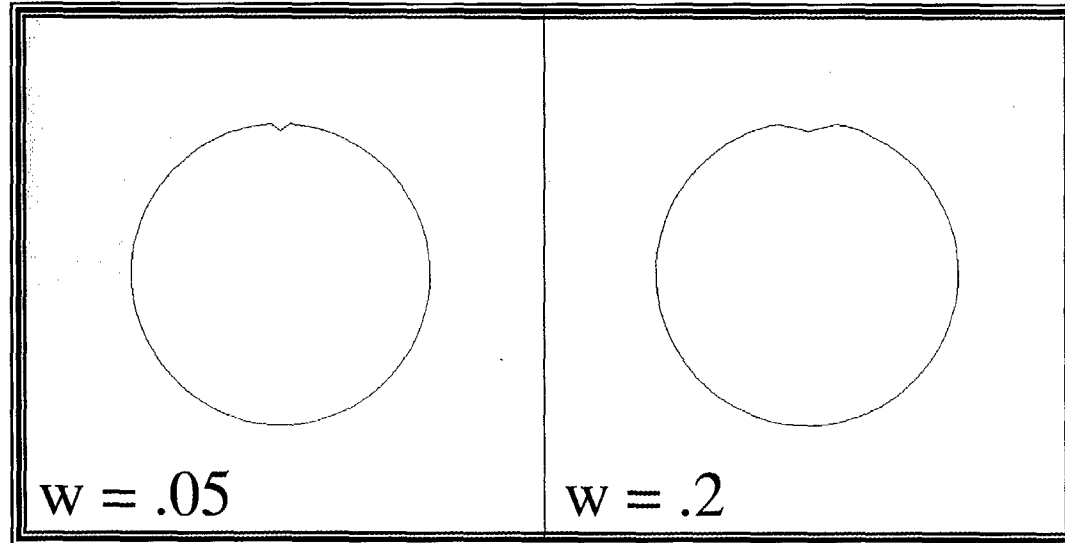
# FACTOR BY WHICH THRESHOLD PERCOLATION FLUX IS DECREASED



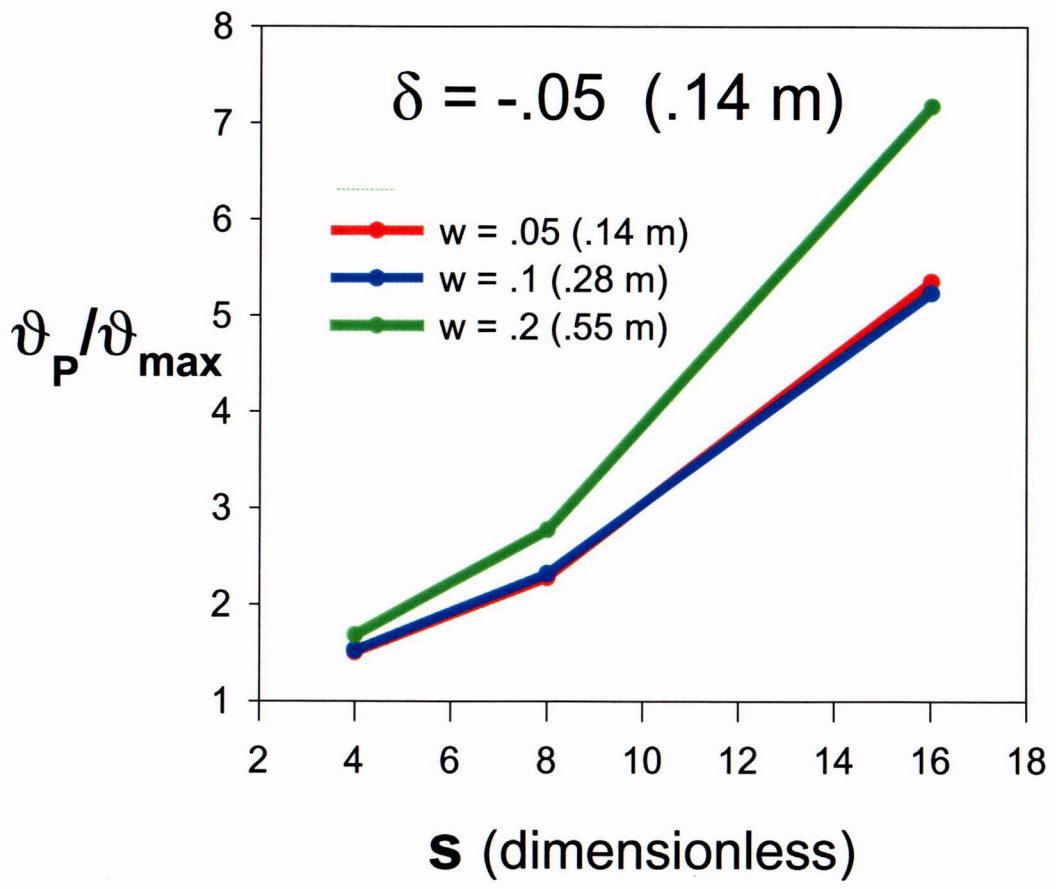
C-04

# MODEL SHAPES FOR DRIFT DEGRADATION

$$\delta = .14\text{m}$$

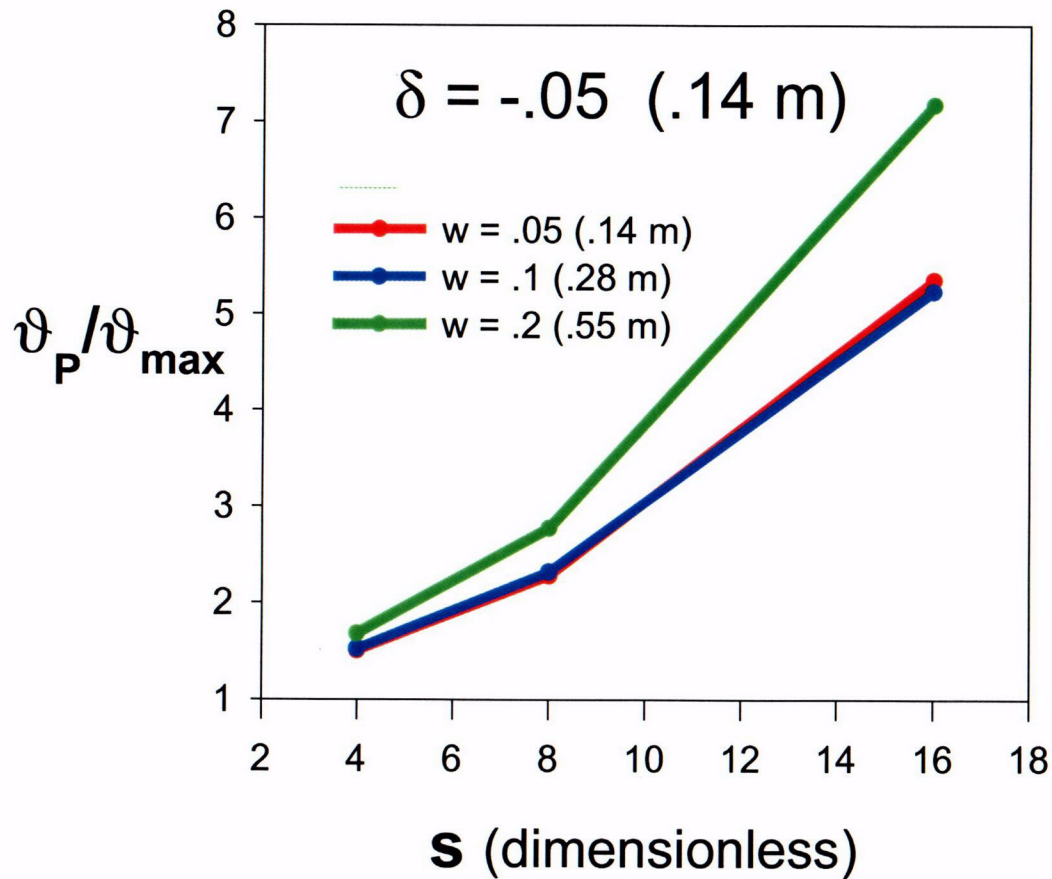


# FACTOR BY WHICH THRESHOLD PERCOLATION FLUX IS DECREASED



C-05

# FACTOR BY WHICH THRESHOLD PERCOLATION FLUX IS DECREASED



0-06

## COMMENTS ON DRIFT DEGRADATION

---

**Irregularities in the Range of 15 cm Can Result in Order of Magnitude Decreases in Threshold Percolation Flux for  $s$  Less Than 16. Note the Dramatic Increase in This Reduction Factor With Increasing  $s$ . Larger  $s$  Corresponds to the Larger  $\alpha$ , (i.e., smaller characteristic length scale, representative of the larger vertical fractures.)**

# **THERMAL-HYDROLOGICAL CONCERNS IN TSPA-VA**

---

- **TH Processes on Seepage Are Required for the Entire Repository Performance Period. TH Driven Flow Cannot Be Neglected for the Initial 5,000 years After Waste Emplacement**
- **Penetration of the Boiling Isotherm by Flow Down a Fracture Is Omitted. The Assumption That Water Will Not Contact the WP Until WP Temperature Decreases Below Boiling Is Not Conservative.**

## **SUPPORTING TECHNICAL BASIS**

---

- **Theoretical Analysis, O.M Phillips**
- **Numerical Simulations, K. Pruess**
- **Laboratory Scale Heater Experiments, R. Green.**
- **Field Scale Observations in the G-tunnel at Climax**