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426.1 87/08/11 W.K.

- 1 -

Dr. Malcolm D. Siegel
Division 6431
Sandia National Laboratories
Albuquerque, NM 87185

Dear Dr. Siegel:

SUBJECT: PLUTONIUM THERMOCHEMISTRY NETWORK

Dr. Garvin at the NBS has completed the calculations for the second set of Pu data I sent him (enclosed). I sent him data for a total of 35 reactions involving Pu. Most of the data were selected using the evaluation of Schwab and Felmy rather than Lemire and Tremaine, which is used in the ASD. I did this because the evaluation of Schwab and Felmy is more thorough and recent, and the experimental data were easier to trace. Nevertheless, the results calculated by the CATCH System generally show fairly good agreement with the ASD data (as of November 3, 1986), with the exception of PuO₂(OH)(am) and the fluoride complexes. The reactions involving Pu-fluoride complexes had very poor fits. Dr. Garvin provided additional data as they were needed, such as for the ligands. Dr. Garvin indicated that data for additional Pu-nitrate and phosphate complexes are available, and we may wish to include them for completeness sake.

Please forward the results to Sid Phillips if you believe they are beneficial.

Sincerely,

ORIGINAL SIGNED BY

Walton R. Kelly
Geochemistry Section
Technical Review Branch
Division of High-Level Waste Management
Office of Nuclear Material Safety
and Safeguards

Enclosure: As stated

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WM Project: WM-
PDR yes
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- 2 -

OFFICIAL CONCURRENCE AND DISTRIBUTION RECORD

LETTER TO: Dr. Malcolm D. Siegel
Division 6431
Sandia National Laboratories
Albuquerque, NM 87185

FROM: Walton R. Kelly
Gechemistry Section
Technical Review Branch
Division of High-Level Waste Management
Office of Nuclear Material Safety
and Safeguards

SUBJECT: PLUTONIUM THERMOCHEMISTRY NETWORK

DATE:

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CONCURRENCES

ORGANIZATION/CONCUREE	INITIALS	DATE CONCURRED
WKelly/HLTR/lw	<u>WRK</u>	87/08/12

Original sent out by: LW 8/12/87

SEE NOTES AFTER THE LISTING OF AUXILIARY DATA FOR EXPLANATION OF ENTRIES.

COMPOUND	MOLAR MASS g.mol ⁻¹	DFH0 +- SIGMA kJ.mol ⁻¹	DFG0 +- SIGMA kJ.mol ⁻¹	S0 +- SIGMA J.(mol.K) ⁻¹	REACTIONS
Pu+3(Ao)	239.0504	-592.036+- 2.092	-578.725+- 3.258	-184.514+- 8.368	14 15 17 56 56 56 13 16 12
76FUG/OET Pu+4(Ao)	239.0498	-536.389+- 2.959	-481.656+- 3.271	-388.783+-14.800	54 54 54 14 15
76FUG/OET Pu(Cs)	239.0520	(.000+- .0001)	(.000+- .0001)	56.149+- .418	
76FUG/RAN Pu(Cr)	239.0520	(.000+- .0001)			
76FUG/RAN PuO2(Cr)	271.0508	-1055.800+- .800	-997.642+- .813	66.130+- .260	57 57 57 18 19
78GUR/OEI, vol. 4. Unc. on S from gef. PuO2+(Ao)	271.0503	-914.752+- 7.073	-850.121+- 7.504	-20.920+- 8.400	60 60 60 30 32
76FUG/OET. At 1 atm. PuO2+2(Ao)	271.0497	-822.282+- 6.616	-757.169+- 3.319	-87.876+-24.830	55 55 55 17 30 16
76FUG/OET. At 1 atm. PuOH+3(Ao)	256.0577		-716.275+- 3.421		1
✓ PuO2(OH)(Am)	288.0581		-1056.470+- 9.608		51
Pu(OH)2+2(Ao)	273.0656		-949.184+- 3.835		2
Pu(OH)3+(Ao)	290.0735		-1167.533+- 3.836		3
Pu(OH)4(Am)	307.0814		-1425.762+- 6.836		50
Pu(OH)4(Ao)	307.0814		-1368.752+- 5.977		4
(PuO2)2(OH)2+2(Ao)	576.1152		-1941.726+- 6.714		8
(PuO2)4(OH)7+(Ao)	1203.2540		-4522.808+-13.364		9
PuF+3(Ao)	258.0488		-789.706+- 3.336		7
PuF2+2(Ao)	277.0477		-1088.206+- 3.526		45
PuF3(Cr)	296.0472	-1585.736+- 2.929	-1515.949+- 2.934	126.106+- .377	58 58 58 20 21
PuF4(Cr)	315.0456	-1846.399+- 2.092	-1752.702+- 2.099	147.250+- .370	59 59 59 27 28
83FUG/PAR ✓ PuO2F+(Ao)	290.0487		-1044.889+- 3.435		46
PuCl+2(Ao)	274.5039		-709.976+- 3.474		44
✓ PuCl+3(Ao)	274.5034		-613.767+- 3.279		5
PuCl2+2(Ao)	309.9569		-740.508+- 3.315		6
PuO2Cl+(Ao)	306.5033		-888.420+- 3.358		10
PuO2Cl2(Ao)	341.9568		-1015.271+- 3.472		11
Pu(OH)2.5Cl0.5(Cr)	299.2969		-1151.893+- 6.829		49
PuSO4+(Ao)	335.1091		-1338.778+- 3.410		33
PuSO4+2(Ao)	335.1085		-1253.169+- 3.423		35
PuO2SO4(Ao)	367.1084		-1519.192+- 3.777		37
Pu(SO4)2(Cr)	431.1672		-2012.316+- 4.444		52
Pu(SO4)2(Ao)	431.1672		-2019.102+- 3.867		36

COMPOUND	MOLAR MASS g.mol ⁻¹	DFH0 +- SIGMA kJ.mol ⁻¹	DFG0 +- SIGMA kJ.mol ⁻¹	SO +- SIGMA J.(mol.K) ⁻¹	REACTIONS
Pu(SO4)2-(Ao)	431.1678		-2093.411+- 3.825		34
PuNO3+2(Ao)	301.0558		-694.171+- 3.495		38
PuNO3+3(Ao)	301.0553		-595.952+- 3.350		41
PuO2NO3+(Ao)	333.0552		-868.045+- 4.426		43
Pu(NO3)2+(Ao)	363.0613		-807.327+- 3.761		39
Pu(NO3)2+2(Ao)	363.0607		-709.688+- 3.421		42
Pu(NO3)3(Ao)	425.0667		-918.203+- 4.524		40
PuH2PO4+2(Ao)	336.0381		-1724.442+- 3.637		47
Pu(HPO4)2(Am)	431.0106		-2827.946+- 4.869		53
Pu(H2PO4)2+(Ao)	433.0259		-2865.699+- 4.520		48

AUXILIARY DATA USED IN SOLUTION

COMPOUND	MOLAR MASS g.mol ⁻¹	DFH0 +- UNC. kJ.mol ⁻¹	DfG0 +- UNC. kJ.mol ⁻¹	S0 +- UNC. J.(mol.K) ⁻¹
O2(G) 86WAG	31.9988	.000+- .000		
O2(Gs) 86WAG	31.9988	.000+- .000	.000+- .000	205.043+- .005
H+(Ao) CONVENTION	1.0074	.000+- .000	.000+- .000	
H2(G) 86WAG	2.0159	.000+- .000	.000+- .000	
OH-(Ao) 86WAG	17.0079		-157.269+- .040	
H2O(L) 86WAG	18.0153	-285.830+- .040	-237.189+- .040	
H2O(G) 86WAG	18.0153	-241.826+- .040		
F-(Ao) 86WAG	18.9990	-335.350+- .650	-281.560+- .650	
F2(G) 86WAG	37.9968	.000+- .000		
F2(Gs) HF(G)	37.9968	.000+- .000	.000+- .000	202.682+- .005
HF(G) 86WAG	20.0063	-273.300+- .700		
Cl-(Ao) 86WAG	35.4536		-131.251+- .100	
SO4-2(Ao) 86WAG	96.0587		-744.100+- .400	
HSO4-(Ao) (87COX/WAG), DFG CALC.	97.0661		-755.413+- 1.000	
SF4(G) FROM [76PAR/WAG]	108.0536	-788.684+- 4.184		
SF6(G) FROM [76PAR/WAG]	146.0504	-1220.766+- 1.004		
NO3-(Ao) CODATA BULL. 10 FOR ION ENTROPY. DHF FROM TN-270-3 84COD	62.0055		-110.876+- .400	
HPO4-2(Ao)	95.9804		-1096.100+- 1.500	
H2PO4-(Ao) 87COX/WAG, DFG CALC (DG)	96.9878		-1137.267+- 1.500	

NOTES ON DELTA HF(298), DELTA GF(298) AND S(298)

VALUES ARE PRODUCED IN A SIMULTANEOUS SOLUTION OF THE REACTIONS LISTED SEPARATELY, EITHER BY LEAST SQUARES OR LEAST SUMS. THE REACTIONS IN WHICH A COMPOUND APPEARS AND WHICH ARE USED IN SETTING ITS PROPERTIES ARE LISTED BY NUMBER.

COMPOUNDS ARE LISTED ACCORDING TO THE STANDARD ORDER OF ARRANGEMENT (APPROXIMATELY).

THE PARENTHETICAL EXPRESSION AT THE RIGHT-HAND END OF A CHEMICAL FORMULA SHOWS THE PHYSICAL STATE OF, OR THE MEDIUM CONTAINING THE COMPOUND. COMMON ABBREVIATIONS ARE:

C = CRYSTALLINE, L = LIQUID, G = GASEOUS, OR, FOR ELEMENTS IN THEIR REFERENCE STATES, CS, LS, AND GS.

AM = AMORPHOUS, GL = GLASSY, A = HYPOTHETICAL STANDARD STATE, M = 1, IN AQUEOUS SOLUTION.

AO = AQUEOUS, UNDISSOCIATED, AU = AQUEOUS, UNSPECIFIED CONCENTRATION, USUALLY DILUTE.

250 H2O, ETC. = SOLUTION OF SPECIFIED CONCENTRATION., D:=DIFFERENTIAL (PARTIAL MOLAL) PROPERTY.

FORMULA WEIGHTS ARE ON THE 1981 ATOMIC WEIGHT SCALE.

SIGMA = 1 STANDARD DEVIATION. (NOT DEFINED FOR LEAST SUMS). THE MAGNITUDE OF SIGMA REFLECTS THE OVER-ALL FIT OF THE NETWORK. WHEN SIGMAS ARE USED IN THE USUAL SQUARE-ROOT-OF-SUM-OF-SQUARES FORMULA TO PREDICT THE STD. DEV. OF A PROPERTY, THE RESULT IS TOO LARGE BECAUSE PROPERTIES ARE HIGHLY CORRELATED. SEE LIST OF REACTIONS FOR BETTER ESTIMATES.

PLUTONIUM EQUILIBRIA, (PLUTO12.CYBR) KELLY

NO.	REACTION	PROP. MEAS.	OBSVD. +/- UNC.	RESID. (OB-CAL)	STD. DEV.	AVE. FIT	WT.	STD. RES.	REFERENCE
		kJ/mol or J/(mol.K)							
17	$\text{Pu}+3(\text{Ao}) + 2 \text{H}_2\text{O}(\text{L}) = \text{PuO}_2+2(\text{Ao}) + \text{H}+(\text{Ao}) + 1.5 \text{H}_2(\text{G})$ Combination of DG for $\text{Pu}+4(\text{ao}) = \text{Pu}+3(\text{ao}) + \text{PuO}_2+2(\text{ao})$ with DG for the $\text{Pu}+3/\text{Pu}+4$ couple in 1 M HClO_4 , and assigning the value to the stand. state.	DG=	295.93	0.63	.000		-1.0	76FUG/OET	
18	$\text{Pu}(\text{Cr}) + \text{O}_2(\text{G}) = \text{PuO}_2(\text{Cr})$ Combustion of alpha Pu, based on [58HOL/MUL] and [57POP/IOA].	DH=-	1055.8	0.8	.000		-1.0	78GUR/UEI	
19	$\text{PuO}_2(\text{Cr})$ Low Temp. Cp meas.	S=	66.13	0.26	.000		-1.0	76FLO/OSB	
20	$\text{Pu}(\text{Cr}) + 1.5 \text{F}_2(\text{G}) = \text{PuF}_3(\text{Cr})$ Selected value, based on $\text{DH}(\text{ppt})$ of $\text{PuF}_3:0.4\text{K}20$	DH=-	1585.7	2.9	.000		-1.0	83FUG/PAR	
21	$\text{PuF}_3(\text{Cr})$ Calorimetric, on 242Pu. CONSTRAINT - SOLVED EXACTLY.	S=	126.11	0.38	.000		INF	740SB/FLO	
22	$4 \text{PuF}_3(\text{Cr}) + \text{O}_2(\text{G}) = 3 \text{PuF}_4(\text{Cr}) + \text{PuO}_2(\text{Cr})$ Estim. from equilib. 783-1073 K, following [66RAN]. 2d law analysis (?) LISTED FOR INFORMATION ONLY.	DH=	-190.4	20.9	61.682		.0	83FUG/PAR	
23	$\text{PuF}_4(\text{Cr}) = \text{Pu}+4(\text{Ao}) + 4 \text{F}-(\text{Ao})$ Estim., assuming same DsolH as for $\text{UF}_4(\text{cr})$ LISTED FOR INFORMATION ONLY.	DH=	-18.4	12.6	12.980		.0	83FUG/PAR	
24	$\text{PuO}_2(\text{Cr}) + 4 \text{HF}(\text{G}) = \text{PuF}_4(\text{Cr}) + 2 \text{H}_2\text{O}(\text{G})$ Based on equilib. at 673-873 K [45JOH]. LISTED FOR INFORMATION ONLY.	DH=	-178.2	20.9	2.813		.0	83FUG/PAR	
25	$\text{Pu}+4(\text{Ao}) + 2 \text{H}_2(\text{G}) + 2 \text{F}_2(\text{G}) = \text{PuF}_4(\text{Cr}) + 4 \text{H}+(\text{Ao})$ Estim. from $\text{D}(\text{DFH}(\text{MF}_4, \text{cr}) - \text{DFH}(\text{M}+4, \text{ao}))$ vs. ionic radius for the series Th, U, Pu. LISTED FOR INFORMATION ONLY.	DH=-	1319.6	13.0	-9.623		.0	83FUG/PAR	
26	$2 \text{PuF}_4(\text{Cr}) + \text{SF}_4(\text{G}) = 2 \text{PuF}_3(\text{Cr}) + \text{SF}_6(\text{G})$ Estim. from lack of reaction at 773 K [61JOH/FIS] LISTED FOR INFORMATION ONLY.	DH=	-10.5	20.9	-99.705		.0	83FUG/PAR	
27	$\text{Pu}(\text{Cr}) + 2 \text{F}_2(\text{G}) = \text{PuF}_4(\text{Cr})$ Selected value, based on estim. from equilib. data, using $\text{S}(\text{PF}_4, \text{cr}) = 147.2 \text{ J/mol.K}$ CONSTRAINT - SOLVED EXACTLY.	DH=-	1846.4	2.1	.000		INF	83FUG/PAR	

NO.	REACTION	PROP. MEAS.	OBSVD. +/- UNC.	RESID. (OB-CAL)	STD. DEV.	AVE. FIT	WT.	STD. RES.	REFERENCE
		kJ/mol or J/(mol.K)							
28	PuF4(Cr) Low temp. Cp meas.	S=	147.25	0.37	.000		-1.0		750SB/FLO
29	Pu(Cr) + 2 F2(G) = PuF4(Cr) Selected value, based on estimate from equilib. data using S(PuF4, cr) = 161.9 J/mol.K est. from PuF4-PuF6 equilib. LISTED FOR INFORMATION ONLY.	DH=-	1778.2	1.0	68.199		.0		66RAN
30	PuO2+(Ao) + H+(Ao) = PuO2+2(Ao) + 0.5 H2(G)	DH=	92.47	2.50	.000		-1.0		76FUG/OET
31	PuO2+(Ao) + H+(Ao) = PuO2+2(Ao) + 0.5 H2(G) FROM EMF IN 1 M HClO4, CORR. TO STD. STATE E/U=1.016. NOT USED, NOT CONSISTENT WITH ESTIM. FROM NPO2+ AND THE RXN PU+4 + PUO2+ = PU+3 + PUO2+2. LISTED FOR INFORMATION ONLY.	DG=	97.91	5.00	4.958		.0		76FUG/OET
	PuO2+(Ao)	S=	-20.92	8.40	.000		-1.0		76FUG/OET
33	Pu+3(Ao) + HS04-(Ao) = PuS04+(Ao) + H+(Ao)	DG=	-4.64	0.10	.000		-1.0		78UAS/BAG
34	Pu+3(Ao) + 2 HS04-(Ao) = Pu(S04)2-(Ao) + 2 H+(Ao)	DG=	-3.86	0.12	.000		-1.0		78UAS/BAG
35	Pu+4(Ao) + HS04-(Ao) = PuS04+2(Ao) + H+(Ao)	DG=	-16.10	0.12	.000		-1.0		76BAG/RAM
36	Pu+4(Ao) + 2 HS04-(Ao) = Pu(S04)2(Ao) + 2 H+(Ao)	DG=	-26.62	0.50	.000		-1.0		76BAG/RAM
37	PuO2+2(Ao) + HS04-(Ao) = PuO2S04(Ao) + H+(Ao)	DG=	-6.61	1.50	.000		-1.0		76PAT/RAM
38	Pu+3(Ao) + NO3-(Ao) = PuNO3+2(Ao) From analysis of Pu complexes in nitric acid hydrazine nitrate mixtures (at 20 C). Kaso = 5.9+-0.5	DG=	-4.57	1.20	.000		-1.0		59SHE/TIM
39	Pu+3(Ao) + 2 NO3-(Ao) = Pu(NO3)2+(Ao) From analysis of Pu complexes in nitric acid hydrazine nitrate mixtures (at 20 C). Kaso = 14.3+- 0.8	DG=	-6.85	1.70	.000		-1.0		59SHE/TIM
40	Pu+3(Ao) + 3 NO3-(Ao) = Pu(NO3)3(Ao) From analysis of Pu complexes in nitric acid hydrazine nitrate mixtures (at 20 C). Kaso = 14.4 +-0.8	DG=	-6.85	2.90	.000		-1.0		59SHE/TIM

NO.	REACTION	PROP. MEAS.	OBSVD.	+ - UNC.	RESID. (OB-CAL)	STD. DEV.	AVE. FIT	WT.	STD. RES.	REFERENCE
		kJ/mol or J/(mol.K)								
41	$\text{Pu}+4(\text{Ao}) + \text{NO}_3-(\text{Ao}) = \text{PuNO}_3+3(\text{Ao})$	DG-	-3.42	0.60	.000		-1.0			76BAG/RAH
42	$\text{Pu}+4(\text{Ao}) + 2 \text{NO}_3-(\text{Ao}) = \text{Pu}(\text{NO}_3)_2+2(\text{Ao})$	DG-	-6.28	0.60	.000		-1.0			76BAG/RAH
43	$\text{PuO}_2+2(\text{Ao}) + \text{NO}_3-(\text{Ao}) = \text{PuO}_2\text{NO}_3+(\text{Ao})$	DG-	0.0	2.9	.000		-1.0			65MAZ/SEV
44	$\text{Pu}+3(\text{Ao}) + \text{Cl}-(\text{Ao}) = \text{PuCl}+2(\text{Ao})$	DG-	0.0	1.2	.000		-1.0			56WAR/WEL
45	$\text{Pu}+4(\text{Ao}) + 2 \text{F}-(\text{Ao}) = \text{PuF}_2+2(\text{Ao})$	DG-	-43.43	0.20	.000		-1.0			76BAG/RAH
46	$\text{PuO}_2+2(\text{Ao}) + \text{F}-(\text{Ao}) = \text{PuO}_2\text{F}+(\text{Ao})$	DG-	-6.16	0.60	.000		-1.0			76PAT/RAH
47	$\text{Pu}+3(\text{Ao}) + \text{H}_2\text{PO}_4-(\text{Ao}) = \text{PuH}_2\text{PO}_4+2(\text{Ao})$	DG-	-8.45	0.60	.000		-1.0			71MOS
48	$\text{Pu}+3(\text{Ao}) + 2 \text{H}_2\text{PO}_4-(\text{Ao}) = \text{Pu}(\text{H}_2\text{PO}_4)_2+(\text{Ao})$	DG-	-12.44	0.90	.000		-1.0			71MOS
49	$\text{Pu}(\text{OH})_2.5\text{Cl}.5(\text{Cr}) = \text{Pu}+3(\text{Ao}) + 2.5 \text{OH}-(\text{Ao}) + 0.5 \text{Cl}-(\text{Ao})$	DG-	114.37	6.00	.000		-1.0			50BUS/COU
	$\text{Pu}(\text{OH})_4(\text{Am}) = \text{Pu}+4(\text{Ao}) + 4 \text{OH}-(\text{Ao})$	DG-	315.03	6.00	.000		-1.0			49KAS
51	$\text{PuO}_2(\text{OH})(\text{Am}) = \text{PuO}_2+(\text{Ao}) + \text{OH}-(\text{Ao})$	DG-	49.08	6.00	.000		-1.0			49KRA/DAM
52	$\text{Pu}(\text{SO}_4)_2(\text{Cr}) = \text{Pu}+4(\text{Ao}) + 2 \text{SO}_4-2(\text{Ao})$ Combination of selections for Pu(SO4)2, Pu+4(ao) [76FUG/OET] and SO4-2(ao) [78COD]	DG-	42.46	2.90	.000		-1.0			78COR/OHA
53	$\text{Pu}(\text{HPO}_4)_2(\text{Am}) = \text{Pu}+4(\text{Ao}) + 2 \text{HPO}_4-2(\text{Ao})$ $\text{Pu}(\text{HPO}_4)_2(\text{am}) = \text{Pu}(\text{HPO}_4)_2 \cdot x\text{H}_2\text{O}(\text{gel})$	DG-	154.09	2.00	.000		-1.0			49KIN
54	$\text{Pu}(\text{Cs}) = \text{Pu}+4(\text{Ao})$ CONSTRAINT - SOLVED EXACTLY.	HGS-	0.000	0.000	.000					INF
55	$\text{Pu}(\text{Cs}) + \text{O}_2(\text{Gs}) = \text{PuO}_2+2(\text{Ao})$ CONSTRAINT - SOLVED EXACTLY.	HGS-	0.000	0.000	.000					INF
56	$\text{Pu}(\text{Cs}) = \text{Pu}+3(\text{Ao})$ CONSTRAINT - SOLVED EXACTLY.	HGS-	0.000	0.000	.000					INF
	$\text{Pu}(\text{Cs}) + \text{O}_2(\text{Gs}) = \text{PuO}_2(\text{Cr})$ CONSTRAINT - SOLVED EXACTLY.	HGS-	0.000	0.000	.000					INF
58	$\text{Pu}(\text{Cs}) + 1.5 \text{F}_2(\text{Gs}) = \text{PuF}_3(\text{Cr})$ CONSTRAINT - SOLVED EXACTLY.	HGS-	0.000	0.000	.000					INF
59	$\text{Pu}(\text{Cs}) + 2 \text{F}_2(\text{Gs}) = \text{PuF}_4(\text{Cr})$ CONSTRAINT - SOLVED EXACTLY.	HGS-	0.000	0.000	.000					INF
60	$\text{Pu}(\text{Cs}) + \text{O}_2(\text{Gs}) = \text{PuO}_2+(\text{Ao})$ CONSTRAINT - SOLVED EXACTLY.	HGS-	0.000	0.000	.000					INF

NOTES ON THE LISTING OF THE REACTIONS

REACTION NOS. MATCH THOSE GIVEN WITH THE SOLUTION FOR FORMATION PROPERTIES. STATISTICS FOR REACTIONS ARE BASED ON THAT SOLUTION.

THE REACTIONS LISTED HERE MAY FORM SEVERAL INDEPENDENT NETWORKS. IF SO, THEY WERE SOLVED SEPARATELY.

PRIOR TO SOLVING THE NETWORK, ALL ENTROPY REACTIONS ARE MULTIPLIED BY T/1000 TO PUT THEM ON THE SAME SCALE AS ENTHALPY AND FREE ENERGY REACTIONS. THIS FACTOR HAS BEEN REMOVED BEFORE PRINTING THE CATALOG OF REACTIONS. SEE ALSO DISCUSSION OF WEIGHTS, BELOW.

DEFINITIONS: NETWORKS CONTAIN ALL PROPERTIES THAT ARE OVERDETERMINED. SIDE CHAINS ARE SINGLE MEASUREMENTS THAT SPECIFY INDIVIDUAL PROPERTIES. CONSTRAINTS ARE EXACT RELATIONS BETWEEN TWO OR MORE PROPERTIES.

UNCERTAINTY SHOWN IN BRACKETS IS MACHINE-ASSIGNED. IT IS EQUAL TO 10 IN THE LEAST SIGNIFICANT DIGIT OF THE OBSERVATION, AND IS SUPPLIED WHEN NO ESTIMATE IS PROVIDED BY THE DATA ANALYST.

WT. = WEIGHT FOR THE REACTION. WT. IS POSITIVE FOR REACTIONS THAT ARE IN A NETWORK, AND IS -1 FOR CONSTRAINTS, SIDE-CHAINS AND UNUSED REACTIONS. WEIGHTS PRINTED ABOVE ARE APPLICABLE DIRECTLY TO ENTHALPY AND FREE ENERGY REACTIONS AND TO ENTROPY REACTIONS MULTIPLIED BY T/1000. FOR WEIGHTED SOLUTIONS, WT. IS LIMITED (USUALLY) TO THE RANGE 0.1 TO 20. IT IS EQUAL TO THE RECIPROCAL OF THE UNCERTAINTY OF THE REACTION AFTER ALLOWING FOR THE UNCERTAINTIES IN THE AUXILIARY DATA. CONSTRAINT REACTIONS ARE TREATED AS HAVING ZERO UNCERTAINTIES. IN THE SPECIAL CASE OF A SEQUENTIAL PAIR OF SOLUTIONS, WT. FOR THE SECOND IS EQUAL TO THE RECIPROCAL OF THE AVERAGE FIT OF THE FIRST.

RESID. = OBSERVED- PREDICTED VALUE.

STD.DEV. = 1 STANDARD DEVIATION FOR THE PREDICTED VALUE. NEITHER THE UNCERTAINTY OF THE REACTION NOR THOSE OF THE AUXILIARY DATA ARE INCLUDED EXCEPT TO THE EXTENT THAT THEY INFLUENCE THE WEIGHT USED IN THE SOLUTION.

AVE. FIT = (RESID. + UNCERTAINTY)/2, OR, IN SPECIAL CASES, = UNCERTAINTY/2. IT IS A COMBINED MEASURE OF CONSISTENCY AND EXPECTED ACCURACY.

STD. RES. IS THE RESIDUAL NORMALIZED TO UNITY AT ONE STD. DEVIATION (APPROXIMATELY) OF THE NETWORK. A VALUE LESS THAN 0.5 IS VERY GOOD. A VALUE GREATER THAN 2 MEANS A VERY POOR FIT. DEFINITIONS ARE:

STD.RES.(LEAST SUM) = $\text{RESID}(I) / ((\text{SUM}(\text{WT}(J) * \text{RESID}(J)) / \text{DF}) / \text{WT}(I))$

STD.RES.(LEAST SQUARES) = $\text{RESID}(I) / \text{SQRT}((\text{SPR} / \text{WT}(I)) - \text{SIGMA}(I) ** 2)$, WHERE $\text{SPR} = \text{SUM}(\text{WT}(J) * \text{RESID}(J) ** 2) / \text{DF}$. FOR BOTH CASES J RUNS OVER ALL REACTIONS, AND DF (DEGREES OF FREEDOM) = (NO. OF REACTIONS) - (NO. OF VARIABLES).

REACTIONS LABELED 'CONSTRAINT' ARE SOLVED EXACTLY, PER INSTRUCTIONS FROM THE DATA ANALYST.