Exelon Generation Company, LLC Quad Cities Nuclear Power Station 22710 206<sup>th</sup> Avenue North Cordova, IL 61242-9740

www.exeloncorp.com

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U. S. Nuclear Regulatory Commission ATTN: Document Control Desk Washington, D.C. 20555

> Quad Cities Nuclear Power Station, Unit 1 Facility Operating License No. DPR-29 NRC Docket Number 50-254

Subject: Core Operating Limits Report for Quad Cities Unit 1 Cycle 18A (Revision 1)

Reference: Letter from Timothy J. Tulon (Exelon Generation Company, LLC) to U. S. NRC, "Core Operating Limits Report for Quad Cities Unit 1 Cycle 18A," dated May 29, 2003.

In accordance with Technical Specifications Section 5.6.5.d, enclosed is Revision 1 of the Core Operating Limits Report (COLR) for Quad Cities Unit 1 Cycle 18A.

Revision 1 reflects the results of further licensing analyses that were recently performed for Unit 1 Cycle 18A. Specifically, a statistical Rod Withdrawal Error (RWE) analysis was performed that resulted in updated operating limits for Minimum Critical Power Ratio when cycle exposure is greater than 2200 MWD/MT. This revision to the COLR is applicable until the end of Cycle 18A, which is scheduled to conclude in March 2005.

Should you have any questions concerning this letter, please contact Mr. W. J. Beck at (309) 227-2800.

Respectfully

Timothy J. Tulon Site Vice President Quad Cities Nuclear Power Station

Attachment A: Core Operating Limits Report for Quad Cities Unit 1 Cycle 18A (Revision 1)

cc: Regional Administrator – NRC Region III NRC Senior Resident Inspector – Quad Cities Nuclear Power Station

ADDI

Exelon.

Nuclear

### Attachment A

# **Core Operating Limits Report**

for

# Quad Cities Unit 1 Cycle 18A

(Revision 1)

Exel<sup>u</sup>n... Nuclear

# Core Operating Limits Report (COLR)

for

Quad Cities Unit 1 Cycle 18A



# Issuances of Changes Summary

Affected Section	Affected Pages	Summary of Changes	Revision	Issue Date
All I	AII	Original Issue for Cycle 18A	0	5/2003
References Section 2 Section 3 Section 5	2, 4, 10, 11, 12, 16, 17, 19	<ul> <li>Update MCPR section with results from statistical RWE analysis.</li> <li>Remove distinction between "BASE CASE" and "FWHOOS/FFWTR" cases (DLO and SLO) such that the "BASE CASE" now includes coverage for FWHOOS/FFWTR.</li> <li>Update Table 5-1 with recalculated PLUOOS administrative limits.</li> </ul>	1	8/2003

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### References

- 1. Exelon Generation Company, LLC and MidAmerican Energy Company, Docket No. 50-254, Quad Cities Nuclear Power Station, Unit 1 Facility Operating License, License No. DPR-29.
- 2. Generic Letter 88-16, Letter from D. M. Crutchfield to All Power Reactor Licensees and Applicants, Concerning the Removal of Cycle-Specific Parameter Limits from Tech Specs, October 3, 1988.
- 3. Global Nuclear Fuel, 0000-0014-8357-SRLR, Rev. 0, "Supplemental Reload Licensing Report for Quad Cities 1 Q1M16 Cycle 18A," May 2003.
- 4. GE-NE-J11-03912-00-01-R1, "Dresden 2 and 3 Quad Cities 1 and 2 Equipment Out-Of-Service and Legacy Fuel Transient Analysis," November 2001.
- 5. BNDQ:02-026, Revision 0, "Determination of Q1C18 MICROBURN GE14 LHGR Limits," July 10, 2002.
- 6. GE DRF C51-00217-01, "Instrument Setpoint Calculation Nuclear Instrumentation, Rod Block Monitor, Commonwealth Edison Company, Quad Cities 1 & 2," December 14, 1999.
- 7. QDC-03-08, "Unit One OPL-3 for Q1C18A," April 1, 2003.
- 8. QDC-02-18, "OPL-3 for Quad Cities Unit 1 Cycle 18," April 25, 2002.
- 9. EMF-2563(P), Revision 1, "Fuel Mechanical Design Report Exposure Extension for ATRIUM-9B Fuel Assemblies at Dresden, Quad Cities, and LaSalle Units", August 2001.
- 10. BNDG:02-001, Revision 0, "Determination of Generic MCPR<sub>F</sub> Limits," May 17, 2002.
- 11. NEDE-24011-P-A-14, General Electric Standard Application for Reactor Fuel (GESTAR II) and US Supplement, June 2000.
- 12. NF0300028, Revision 0, "Quad Cities 1 Cycle 18A FRED Form," March 26, 2003.
- 13. NF-MW:02-0413, "Approval of GE Evaluation of Dresden and Quad Cities Pressure Regulator Out of Service Analysis," October 22, 2002.
- 14. NFM-MW:02-0274, "Approval of GE Evaluation of MSIV out of Service for Dresden and Quad Cities", August 2, 2002.
- 15. BNDQ:03-022, Revision 0, "Quad Cities Unit 1 Cycle 18A Composite LHGR Curve Generation for Bundle 2647," May 2003.
- 16. BNDQ:03-024, Revision 0, "Quad Cities Unit 1 Cycle 18A Generation of the Revision 0 Core Operating Limits Report (COLR)," May 23, 2003.
- 17. GE-NE-0000-0018-5044-R0, "Statistically Based Rod Withdrawal Error Analysis For Dresden and Quad Cities," July 2003.
- BNDQ:03-052, Revision 0, "Q1C18A Core Operating Limits Report (COLR) Revision 1 Creation," August 2003.

# **1.** Average Planar Linear Heat Generation Rate

### **1.1** Technical Specification Reference

Sections 3.2.1 and 3.4.1

### 1.2 Description

Tables 1-1 and 1-2 are used to determine the maximum average planar linear heat generation rate (MAPLHGR) limit for each fuel type. Limits listed in Tables 1-1 and 1-2 are for dual reactor recirculation loop operation (DLO).

For single reactor recirculation loop operation (SLO), the MAPLHGR limits given in Tables 1-1 and 1-2 must be multiplied by a SLO MAPLHGR multiplier. The SLO MAPLHGR multipliers are given in Table 1-3 by fuel type.

	ear Heat Generation Rate (MAPLHGR) for C) ATRIUM-9B Fuel
Bundle Type 5, ATRM9-P9DATB348-	wing fuel bundle types: 11G6.5-SPC100T-9WR-144-T6-2444 11G6.5-SPC100T-9WR-144-T6-2445
Applicable Refere	nce Number(s): 3
Planar Average Exposure (GWD/MT)	MAPLHGR Limit (kW/ft)
0.00	13.52
17.25	13.52
70.00	7.84

Table 1-2: Maximum Average Planar Line GNF GE	
Applicable to the follow Bundle Type 16, GE14-P10DNA Bundle Type 17, GE14-P10DNA Bundle Type 1, GE14-P10DNA	B411-14GZ-100T-145-T6-2564 B409-15GZ-100T-145-T6-2565
Applicable Referen	nce Number(s): 3
Planar Average Exposure (GWD/MT)	MAPLHGR Limit (kW/ft)
0.00	11.68
16.00	11.68
44.09	9.16
55.12	8.09
63.50	6.97
70.00	4.36

Table 1-3: Maximum Average Planar L SLO Multipliers f	near Heat Generation Rate (MAPLHGR) or All Fuel Types
Applicable Refere	nce Number(s): 3
Fuel Product Line	SLO MAPLHGR Multiplier
ATRIUM-9B	0.84
GE14	0.77

### 2. Minimum Critical Power Ratio

### 2.1 Technical Specification Reference

Sections 3.2.2, 3.4.1, and 3.7.7.

### 2.2 Description

The MCPR limit for a specific fuel type/condition is determined by choosing the maximum CPR limit from the pool of applicable limits. The sections below provide the method for determining the applicable MCPR limit in any case. Linear interpolation is to be used to determine values from the following tables for flow/power conditions not specifically listed: 2-3, 2-4, 2-5, and 2-7. Rated core thermal power is 2957 MWth and rated core flow is 98 Mlb/hr.

#### 2.2.1 Manual Flow Control (MFC) MCPR Limits

The operating limit MCPR (OLMCPR) for operation in the manual flow control mode is determined from either Section 2.2.1.1 or 2.2.1.2, whichever is greater at the given power and flow condition.

#### 2.2.1.1 MFC Power-Dependent MCPR (MCPR<sub>P</sub>)

For operation at less than 38.5% of rated core thermal power, the OLMCPR as a function of core thermal power (MCPR<sub>P</sub>) is shown in Table 2-3. For operation at greater than 38.5% of rated core thermal power, the OLMCPR as a function of core thermal power is determined by multiplying the applicable EOOS condition limit as shown in Table 2-1 or 2-2 (see Section 2.2.3) by the applicable MCPR multiplier, K<sub>P</sub>, given in Table 2-3. For operation at exactly 38.5% of rated core thermal power, the OLMCPR as a function of core thermal power is the maximum of either of the two aforementioned methods evaluated at 38.5% of rated core thermal power.

#### 2.2.1.2 MFC Flow-Dependent MCPR (MCPR<sub>F</sub>)

The OLMCPR as a function of flow (MCPR<sub>F</sub>) is determined from either Table 2-4 or Table 2-5 depending on the EOOS condition. The MCPR<sub>F</sub> limit is independent of the flow control mode of the reactor.

#### 2.2.2 Automatic Flow Control (AFC) MCPR Limits

The operating limit MCPR (OLMCPR) in the automatic flow control mode is to be determined from either Section 2.2.2.1 or 2.2.2.2, whichever is greater at the given power and flow condition.

#### 2.2.2.1 AFC Power-Dependent MCPR

For operation at less than 38.5% of rated core thermal power, the OLMCPR as a function of core thermal power (MCPR<sub>P</sub>) is shown in Table 2-7. For operation at greater than 38.5% of rated core thermal power, the OLMCPR as a function of core thermal power is determined by multiplying the applicable EOOS condition limit as shown in Table 2-6 by the applicable MCPR multiplier, K<sub>P</sub>, given in Table 2-7. For operation at exactly 38.5% of rated core thermal power, the OLMCPR as a function of core thermal power, the OLMCPR as a function of core thermal power is the maximum of either of the two aforementioned methods evaluated at 38.5% of rated core thermal power.

#### 2.2.2.2 AFC Flow-Dependent MCPR

The OLMCPR as a function of flow (MCPR<sub>F</sub>) is determined from either Table 2-4 or Table 2-5 depending on the EOOS condition. The MCPR<sub>F</sub> limit is independent of the flow control mode of the reactor.

#### 2.2.3 Option A and Option B

OLMCPR values have been determined based upon two assumed core average scram times – Option A which assumes the Technical Specification 20% insertion core average scram time and Option B which assumes a core average 20% insertion scram time equal to 0.694 seconds.

Option A OLMCPR values may be utilized if the core average 20% insertion scram time is less than or equal to the Technical Specification required time. Reload analyses performed by Global Nuclear Fuel (GNF) for cycle 18A Option A MCPR limits utilized a 20% core average insertion time of 0.900 seconds (References 7 and 8).

Option B OLMCPR values may be utilized if the core average 20% insertion scram time is less than or equal to 0.694 seconds (References 7 and 8).

If the core average scram insertion time does not meet the Option B criteria, but is less than the Option A criteria, the appropriate OLMCPR value may be determined from a linear interpolation between the Option A and Option B limits with standard mathematical rounding to two decimal places. When performing a linear interpolation to determine MCPR limits, ensure that the time used for Option A is 0.900 seconds, which is the 20% insertion time utilized by GNF in the reload analyses. For manual flow control operation, Option A based OLMCPRs are found in Table 2-1 while Option B based OLMCPRs are contained in Table 2-2. For automatic flow control operation only Option A based OLMCPRs are available and are given in Table 2-6 (no adjustment for core average scram time is available for AFC mode).

#### 2.2.4 Recirculation Pump Motor Generator Settings

Quad Cities Unit 1 Cycle 18A was analyzed with a maximum core flow runout of 110% of rated core flow. Therefore, the recirculation pump motor generator scoop tube mechanical and electrical stops must be set to maintain core flow less than 110% of rated core flow, which is equivalent to 107.8 Mlb/hr (1.10 \* 98.0 Mlb/hr), for all runout events (Reference 12). A maximum core flow runout of 110% of rated core flow is consistent with what was used in the analysis presented in Reference 4.

		nual Flow Cont			是國家認知
	Applica	ble Reference Num			Manual Anna and Anna
EOOS Combination <sup>M3</sup>	Fuel Type	<2200 MWD/MT	Cycle Expo >2200 MWD/MT & <eor<sup>11-2128 MWD/MT</eor<sup>	EOR <sup>(1)</sup> -2128 MWD/MT & EOR	≥EOR <sup>[1]</sup> (Coastdown)
	GE14	1.55	1.55	1.63	1.63
Base Case	ATRIUM-98	1.52	1.52	1.61	1.61
	GE14	1.56	1.56	1.64	1.64
Base Case SLO	ATRIUM-98	1.53	1.53	1.62	1.62
TD0000[2]	GE14	1.72	1.72	1.72	1.74 <sup>[3]</sup>
TBPOOS <sup>[2]</sup>	ATRIUM-98	1.68	1.68	1.68	1.70[3]
	GE14	1.73	1.73	1.73	1.75 <sup>[3]</sup>
TBPOOS SLO <sup>[2]</sup>	ATRIUM-98	1.69	1.69	1.69	1.71 <sup>[3]</sup>
	GE14	1.61	1.61	1.63	1.63
TCV Slow Closure	ATRIUM-98	1.55	1.55	1.61	1.61
	GE14	1,62	1.62	1.64	1.64
TCV Slow Closure SLO	ATRIUM-9B	1.56	1.56	1.62	1.62
PLUCOC	GE14	1.64	1.64	1.64	1.64
PLUOOS -	ATRIUM-9B	1.58	1.58	1.61	1.61
	GE14	1.65	1.65	1.65	1.65
PLUOOS SLO	ATRIUM-9B	1.59	1.59	1.62	1.62
TOMO	GE14	1.55	1.55	1.63	1.63
TCV Stuck Closed	ATRIUM-98	1.52	1.52	1.61	1.61
	GE14	1.56	1.56	1.64	1.64
TCV Stuck Closed SLO	ATRIUM-9B	1.53	1.53	1.62	1.62

Notes for Table 2-1:

1.

EOR refers to the end of rated power operation - the all-rods-out condition at 100% rated power and 100% rated flow. TBPOOS cases include a +0.03 OLMCPR penalty for operation below analysis basis dome pressure per page 24 of 2.

Reference 4. TBPOOS cases which cover operation in coast down conditions include a +0.02 OLMCPR penalty per page 22 of 3. Reference 4.

All EOOS combinations presented here, including the BASE CASE and BASE CASE SLO, account for both normal feedwater temperature operation and operation with FFWTR/FHOOS. 4.

		ual Flow Cont ble Reference Num				
	Applica		Cycle Expos	sure Range		
EOOS Combination <sup>43</sup>	Fuel Type	<2200 MWD/MT	≥2200 MWD/MT & <eor<sup>II-2128 MWD/MT</eor<sup>	>EOR <sup>[1]</sup> -2128 MWD/MT & <eor< th=""><th colspan="2">≥EOR<sup>[1]</sup> (Coastdown)</th></eor<>	≥EOR <sup>[1]</sup> (Coastdown)	
	GE14	1.44	1.47	1.47	1.47	
Base Case	ATRIUM-9B	1.44	1.47	1.47	1.47	
D 01-0	GE14	1,45	1.48	1.48	1.48	
Base Case SLO	ATRIUM-9B	1.45	1.48	1.48	1.48	
TBPOOS <sup>121</sup>	GE14	1.55	1.55	1.55	1.57 <sup>[3]</sup>	
IBPOOS-	ATRIUM-98	1.51	1.51	1.51	1.53 <sup>[3]</sup>	
	GE14	1.56	1.56	1.56	1.58 <sup>[3]</sup>	
TBPOOS SLO <sup>21</sup>	ATRIUM-98	1.52	1.52	1.52	1.54 <sup>[3]</sup>	
	GE14	1.44	1.47	1.47	1.47	
TCV Slow Closure	ATRIUM-98	1.44	1.47	1.47	1.47	
	GE14	1.45	1.48	1.48	1.48	
TCV Slow Closure SLO	ATRIUM-9B	145	1.48	1,48	1.48	
<b>DU1000</b>	GE14	1.47	1.47	1.47	1.47	
PLUOOS	ATRIUM-98	1.44	1.47	1.47	1.47	
	GE14	1.48	1.48	1.48	1.48	
PLUOOS SLO	ATRIUM-98	1.45	1.48	1.48	1.48	
TOM Charle Classe	GE14	1.44	1.47	1.47	1.47	
TCV Stuck Closed	ATRIUM-98	1.44	1.47	1.47	1.47	
	GE14	1.45	1.48	1.48	1.48	
TCV Stuck Closed SLO	ATRIUM-98	1.45	1.48	1.48	1.48	

Notes for Table 2-2:

1.

EOR refers to the end of rated power operation - the all-rods-out condition at 100% rated power and 100% rated flow. TBPOOS cases include a +0.03 OLMCPR penalty for operation below analysis basis dome pressure per page 24 of 2. Reference 4.

TBPOOS cases which cover operation in coast down conditions include a +0.02 OLMCPR penalty per page 22 of 3.

Reference 4. All EOOS combinations presented here, including the BASE CASE and BASE CASE SLO, account for both normal feedwater temperature operation and operation with FFWTR/FHOOS. 4.

		App	licable R	eference	Number(s	s): 4, 3						
			Core Thermal Power (% Rated)									
EOOS Combination	Core Flow (% Rated)	0	<b>25</b>	38.5	38.5	45	60	70	70	≥100		
		Operati	ng Limit	MCPR <sup>III</sup>	<b>C</b>	perating	y Limit MC	PR Mul	iplier, K <sub>P</sub>	<b>11</b>		
Base Case	<b>\$60</b>	3.16	2.58	2.27	1.32	1.28	1,15	N/A	N/A	1.00		
Dase Case	>60	3.77	2.99	2.56	1.92	1,20		NA	11/A			
	<b>≤</b> 60	3.17	2.59	2.28	1.32	1.28	1.15	N/A	N/A	4.00		
Base Case SLO	>60	3.78	3.00	2.57		1.20	1.19		N/A	1.00		
TBPOOS	≤60	5.55	3.77	2.82	1.37	1.28	1.15	N/A	N/A	1.00		
	>60	6.79	4.62	3.45								
	. ≤60	5.56	3.78	2.83	1.37	1.28	1.15	N/A	N/A	1.00		
TBPOOS SLO	>60	6.80	4.63	3.46			1.15					
TCV Slow Closure	≤60	5.55	3.77	2.82	1.64	N/A	1,45	1.26	1.11	1,00		
ICV Slow Closure	>60	6.79	4.62	3.45	1.04		later a					
TCV Slow Closure	≲60	5.56	3.78	2.83		NUA	N/A 1,45	1.26	1.11	1.00		
SLO	>60	6.80	4.63	3.46	1,64	N/A		1.20				
	60	5.55	3.77	2.82		N/A	1.45	1.26	1.11	1.00		
PLUOOS	>60	6.79	4.62	3.45	1.64							
	≤60	5.56	3.78	2.83	1.64	N/A	1.45	1.26	4.44	1.00		
PLUOOS SLO	>60	6.80	4.63	3.46	1.04	N/A	1.45		1.11			
TCV Stuck Closed	≤60	3.16	2.58	2.27	1.32	1.28	1.15	N/A	N/A	1.00		
ILY SLUCK CHOSED	>60	3.77	2.99	2.56	1.02	1.20		N/A	N/A			
TCV Stuck Closed	≲60	3.17	2.59	2.28		4 90		N/A	NUA	+ 00		
SLÓ	>60	3.78	3.00	2.57	1,32	1.40	1.28 1.15		N/A	1.00		

Table 2-4: Flow Dependent OLN and All Operating Conditions	ICPR (MCPR <sub>F</sub> ) for All Fuel Types Except TCV Stuck Closed <sup>[1,2]</sup>
Applicable Reference	e Number(s): 10, 3, 4
Core Flow (% Rated)	MCPR <sub>F</sub> <sup>[3]</sup>
110.0	1.22
100.0	1.22
0.0	1.86

This table is not applicable to TCV Stuck Closed operating conditions.

This table is applicable to both Manual Flow Control and Automatic Flow Control operation. 2. 2

Values are to be linearly interpolated between listed core flow values.

	ACPR (MCPR <sub>F</sub> ) for All Fuel Types Operating Conditions <sup>11,21</sup>
Applicable Reference	e Number(s): 10, 3, 4
Core Flow (% Rated)	MCPR <sub>F</sub> <sup>31</sup>
110.0	1.27
108.9	1.27
0.0	1.97
Notes for Table 2-5:	

This table is applicable to TCV Stuck Closed operating conditions only.

This table is applicable to both Manual Flow Control and Automatic Flow Control operation. Values are to be linearly interpolated between listed core flow values. 2

	Table 2-6 for	<b>Automatic Flor</b>	am Time Based w Control Opera nce Number(s): 3,4	tion	
EOOS Combination <sup>[2,3]</sup>	Fuel Type		Cycle Expo ≥2200 MWD/MT & <eor<sup>M-2128 MWD/MT</eor<sup>		≥EOR <sup>(1)</sup> (Coastdown)
Base Case	GE14 ATRIUM-9B	1.73 1.70	1.86 1.86	1.86 1.86	1.86 1.86

Notes for Table 2-6:

EOR refers to the end of rated power operation - the all-rods-out condition at 100% rated power and 100% rated flow.

Operation in Automatic Flow Control mode with TCV Slow Closure, TCV Stuck Closed, or PLUOOS is not an allowed 2 condition.

Operation in Automatic Flow Control mode with an MSIVOOS or a pressure regulator OOS is not an allowed condition.

•		Appli	cable Referen	nce Number	(s): 4, 3			
	Core		ې د د د د د د ورو د د . د د د د د د د د د د د د د	Core Then	nal Power	(% Rated)	a second and a second as a second as	يە مەربەر يىلى
EOOS Combination <sup>[1,3]</sup>	Flow	0	25	38.5	38.5	45	60	≥100
Company	(% Rated)	Rated) Operating Limit MCPR Operating Limit MCPR						
Base Case	≤60	3.16	2.58	2.27	4.00 4.00	4.00	1.15	
	>60	3.77	2.99	2.56	1.32	1.28	1.10	1.00

condition.

Values are to be linearly interpolated between listed core thermal power values.

Operation in Automatic Flow Control mode with an MSIVOOS or a pressure regulator OOS is not an allowed condition.

## 3. Linear Heat Generation Rate

### **3.1** Technical Specification Reference

Section 3.2.3.

### 3.2 Description

The linear heat generation rate (LHGR) limit is the product of the LHGR limit from Tables 3-1, 3-2, 3-3 or 3-4 (depending of the fuel type) and the minimum of either the power dependent LHGR multiplication factor, LHGRFAC<sub>P</sub>, the flow dependent LHGR multiplication factor, LHGRFAC<sub>F</sub> or the single loop operation (SLO) multiplication factor. The applicable LHGRFAC<sub>P</sub> limit is to be determined from Table 3-5 or Table 3-8 depending on the flow control mode in use. The applicable LHGRFAC<sub>F</sub> limit is to be determined from Table 3-5 or 3-7, depending on the EOOS status. The SLO multiplication factor can be found in Table 3-9.

Table 3-1: LHGR Lim GE14-P10DNAB411-14GZ-1	nits for Bundle Type 00T-145-T6-2564 (Type 16)
Applicable Referen	ce Number(s): 5
Nodal Exposure (GWD/MT)	LHGR Limit (kW/ft) <sup>[1]</sup>
0.00	13.40
12.50	13.40
15.20	13.05
24.00	11.95
47.00	9.10
56.25	8.00
62.85	5.00
Notes for Table 3-1:	

1. Values are to be linearly interpolated between listed nodal exposure values.

	Z-100T-145-T6-2565 (Type 17) erence Number(s): 5
	LHGR Limit (kW/ft) <sup>[1]</sup>
0.00	13.40
12.50	13.40
15.00	13.05
18.70	12.60
27.50	11.50
56.00	8.00
62.50	5.00

1. Values are to be linearly interpolated between listed nodal exposure values.

		ce Number(s)	6-2647 (Type 1)	
Nodal Exposure (GWD/MT)			LHGR Limit (KW/ft) <sup>[1]</sup>	
0.00		· · ·	13.40	
11.02			13.40	
13.22	. ]		12.91	
16.53	· .		12.91	
55.11			8.20	
60.62		·	5.62	· .
61.71			5.00	

1. Values are to be linearly interpolated between listed nodal exposure values.

Table 3-4: LHGR Limits f ATRM9-P9DATB348-11G6.5-SPC100T-4 ATRM9-P9DATB360-11G6.5-SPC100	9WR-144-T6-2444 (Type 5) and
Applicable Reference N	
Nodal Exposure (GWD/MT)	LHGR Limit (kW/ft) <sup>[1]</sup>
0.00	14.40
15.00	14.40
64.30	7.90

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-	· ·	Appli	cable Refe	erence Nur	nber(s): 4	, 3	· · ·		
		Core Thermal Power (% Rated)							
EOOS Combination	Core Flow (% Rated)	Ô	25	38.5	38.5	70	70	<b>B</b> D	≥100
				L L	IGRFAC	Multiplier	14		
Base Case	ĨĂ	0.50	0.56	0.59	<b>D.6</b> 8	N/A	N/A	0.86	1.00
Base Case SLO	All	0.50	0.56	0.59	0.68	N/A	N/A	0.86	1.00
TBPOOS	≤60	0.22	0.39	0.48	0.54	0.54 N/A	N/A	N/A	1.00
IBPOUS	>60	0.33	0.39	0.42					
TBPOOS SLO	≤60	0.22	0.39	0.48	0.54	N/A	N/A	N/A	1.00
IBPOUS SLU	>60	0.33	0.39	0.42					
TCV Slow Closure	<i>≤</i> 60	0.22	0.39	0.48	0.54	.54 0.73	0.78	N/A	1.00
TOV CION CIOSUIS	>60	0.33	0.39	0.42					
TCV Slow Closure	≤60	0.22	0.39	0.48	0.54	0.54 0.73	0.78	N/A	1.00
SLO	>60	0.33	0.39	0.42					
PLUOOS	<i>≤</i> 60	0.22	0.39	0.48	0.54	0.54 0.73	0.78	N/A	1.00
	>60	0.33	0.39	0.42					
PLUOOS SLO	≤60	0.22	0.39	0.48	0.54	0.54 0.73	0.78	0.78 N/A	1.00
	>60	0.33	0.39	0.42	0.04		0.10		
TCV Stuck Closed	All	0.50	0.56	0.59	0.68	N/A	N/A	0.86	1.00
TCV Stuck Closed SLO	ILA	0.50	0.56	0.59	0.68	N/A	N/A	0.86	1.00

Notes for Table 3-5:

1. 2.

Values are to be linearly interpolated between listed core power values. The LHGR multiplier for any core power/flow condition is the limiting of the LHGRFAC<sub>P</sub>, LHGRFAC<sub>F</sub>, and SLO Multiplier (if applicable).

Applicable Reference Number(s): 4, 3					
Core Flow (% Rated)					
0.0	0.28				
30.0	0.55				
40.0	0.64				
50.0	0.77				
80.0	1.00				
≥100.0	1.00				

This table is <u>not</u> applicable to TCV Stuck Closed operating conditions. This table is applicable to both Manual Flow Control and Automatic Flow Control operation. Values are to be linearly interpolated between listed core flow values. 2

3.

The LHGR multiplier for any core powerflow condition is the limiting of the LHGRFACP, LHGRFACP, and SLO Multiplier (if 4. applicable).

Table 3-7: LHGRFACF Multipliers for TCV Stuck Closed Conditions <sup>(1,3)</sup> Applicable Reference Number(s): 4         Core Flow (% Rated)									
							0.0	i tradicio	0.14
							30.0	; ·	0.41
40.0	, ·	0.50							
50.0		0.63							
80.0		0.86							
98.3	· · · · · · · · · · · · · · · · · · ·	1.00							
≥100.0		1.00							
Nieles for Table 8 7									

Notes for Table 3-7:

This table is applicable to TCV Stuck Closed operating conditions only. 1.

Values are to be linearly interpolated between listed core flow values. 2.

This table is applicable to both Manual Flow Control and Automatic Flow Control operation. 3.

The LHGR multiplier for any core powerflow condition is the limiting of the LHGRFAC, LHGRFAC, and SLO Multiplier (If 4. applicable).

Table 3-8: LHGRFAC <sub>P</sub> Multipli	ers for Automatic Flow Control
Applicable Refere	nce Number(s): 4
Core Thermal Power (% Rated)	LHGRFAC <sub>p</sub> <sup>(1,2)</sup>
0.0	0.00
50.0	0.50
≥100.0	1.00
Notes for Table 3-8:	

Values are to be linearly interpolated between listed core thermal power values. 1.

The LHGR multiplier for any core power/flow condition is the limiting of the LHGRFACP, LHGRFACP, and SLO Multiplier (If 2 applicable).

Applicable Refere	ence Number(s): 3
Fuel Product Line	SLO LHGR Multiplier <sup>(1)</sup>
ATRIUM-9B	0.84
GE14	0.77

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# 4. Control Rod Withdrawal Block Instrumentation

### 4.1 Technical Specification Reference

Table 3.3.2.1-1

# 4.2 Description

The rod block monitor upscale instrumentation setpoints are determined from the relationships shown below (Reference 6).

Table 4-1: Rod Block Monitor Upscale Instrumentation Setpoints <sup>(3)</sup> Applicable Reference Number(s): 6					
Rod Block Monitor Upscale Trip Function	Allowable Value <sup>11,21</sup>				
Two Recirculation Loop Operation	0.65 W <sub>d</sub> + 56.1%				
Single Recirculation Loop Operation	0.65 W <sub>d</sub> + 51.4%				
RWE is analyzed for unblocked conditions.	duce a rated core flow of 98.0 Mib/hr. e rod withdrawal event (RWE) licensing analysis because the to exceed the allowable value for a recirculation loop drive flow				

## 5. Allowed Modes of Operation

### 5.1 Technical Specification Reference

Bases Sections 3.2.2, 3.2.3, and 3.7.7

### 5.2 Description

The Allowed Modes of Operation with combinations of Equipment Out-of-Service are as described below:

11231	able Reference Number(s): 3, 4, 7, 8, 11, 13, 14 Operating Region					
EOOS Combinations <sup>[1,2,3]</sup>	Standard		MELLLA	Coastdown		
Base Case	Yes	Yes	Yes	Yes		
Base Case SLO	Yes	Yes	Yes	Yes		
TBPOOS	Yes	Yes	Yes	Yes		
TBPOOS SLO	Yes	Yes	Yes	Yes		
TCV Slow Closure <sup>[6]</sup>	Yes	Yes	Yes	Yes		
TCV Slow Closure <sup>16]</sup> SLO	Yes	Yes	Yes	Yes		
PLUOOS <sup>[7]</sup>	Yes	Yes	Yes	Yes		
PLUOOS SLO	Yes	Yes	Yes	Yes		
TCV Stuck Closed	Yes	Yes	Yes	Yes		
TCV Stuck Closed SLO	Yes	Yes	Yes	Yes		
tes for Table 5-1: Each OOS Option may be combine methodology are met) with all TIPS LPRM calibration frequency of 2500 sets a 120°F reduction in feedwate Reduction was analyzed for the end A single MSIV may be taken OOS (thermal power is maintained ≤75% All OOS Options support 1 Turbine	available at startup fro D Effective Full Power i temperature througho ire cycle). shut) under any and a of 2957 MWth (Refere	om a refuel outage and Hours (EFPH) (2000 El out the cycle was analyz II OOS Options except nces 14 and 3).	up to 50% of the LPi FPH +25%). For ope ted (Final Feedwate) Automatic Flow Con	RMs OOS with an Ination under all limit Temperature Irol, so long as core		

 All OOS Options support 1 Turbine Bypass Valve OOS, if the OPL-3 assumed opening profile for the Turbine Bypass system is met. If the OPL-3 (References 7 and 8) opening profile is not met, or if more than one Turbine Bypass Valve is OOS, utilize the TBPOOS condition.

4. Coastdown operation is defined as any cycle exposure beyond the full power, all rods out condition with plant power slowly lowering to a lesser value while core flow is held constant (Reference 11 Section 4.3.1.2.8). Up to a 15% overpower is analyzed per Reference 4.

5. Increased Core Flow (ICF) is supported to 108% of rated core flow.

 For operation with a pressure regulator out-of-service (PROOS), the TCV Slow Closure limits should be applied (Reference 13) and the operational notes from Reference 13 reviewed. PROOS in conjunction with TCV Slow Closure is not an analyzed out-of-service combination.

7. If the Base Case limit set is being used and the PLU is taken OOS for a surveillance and the reactor is maintained at 280% rated core thermal power and 280% of rated core flow during the PLUOOS period, an administrative limit on FDLRX/MFLPD and MFLCPR can be used instead of the PLUOOS thermal limit set. The FDLRX/MFLPD administrative limit to be used is 0.98 for all scram speeds. The MFLCPR administrative limit is 0.94 for Option A scram times, 0.97 for Option B scram times, and 0.97 for scram times less than or equal to 0.731 seconds but greater than the Option B time. (Reference 16).

# 6. Methodology References

The analytical methods used to determine the core operating limits shall be those previously reviewed and approved by the NRC (Technical Specification Section 5.6.5), specifically those described in the following documents:

- 1. ANF-1125 (P)(A) and Supplements 1 and 2, "Critical Power Correlation ANFB," April 1990.
- 2. ANF-524 (P)(A) Revision 2 and Supplements 1 and 2, "ANF Critical Power Methodology for Boiling Water Reactors," November 1990.
- 3. XN-NF-79-71 (P)(A) Revision 2 and Supplements 1, 2 & 3, "Exxon Nuclear Plant Transient Methodology for Bolling Water Reactors," March 1986.
- 4. XN-NF-80-19 (P)(A) Volume 1 Supplements 1 and 2, "Exxon Nuclear Methodology for Boiling Water Reactors Neutronic Methods for Design and Analysis," March 1993.
- 5. XN-NF-80-19 (P)(A) Volume 1 Supplement 3, Supplement 3 Appendix F, and Supplement 4, "Exxon Nuclear Methodology for Bolling Water Reactors," November 1990.
- 6. XN-NF-80-19 (P)(A) Volumes 2, 2A, 2B and 2C, "Exxon Nuclear Methodology for Boiling Water Reactors: EXEM BWR ECCS Evaluation Model," September 1982.
- 7. XN-NF-80-19 (P)(A) Volume 3 Revision 2, "Exxon Nuclear Methodology for Boiling Water Reactors, THERMEX: Thermal Limits Methodology Summary Description," January 1987.
- 8. XN-NF-80-19 (P)(A) Volume 4 Revision 1, "Exxon Nuclear Methodology for Boiling Water Reactors: Application of the ENC Methodology to BWR Reloads," June 1986.
- 9. XN-NF-85-67 (P)(A) Revision 1, "Generic Mechanical Design for Exxon Nuclear Jet Pump BWR Reload Fuel," September 1986.
- 10. ANF-913 (P)(A) Volume 1 Revision 1, and Volume 1 Supplements 2, 3, 4, "COTRANSA2: A Computer Program for Boiling Water Reactor Transients Analysis," August 1990.
- 11. XN-NF-82-06- (P)(A) Revision 1 and Supplements 2, 4 and 5, "Qualification of Exxon Nuclear Fuel for Extended Burnup," October 1986.
- 12. XN-NF-82-06- (P)(A) Supplement 1 Revision 2, "Qualification of Exxon Nuclear Fuel for Extended Burnup Supplement 1 Extended Burnup Qualification of ENC 9x9 BWR Fuel," May 1988.
- ANF-89-14(P)(A) Revision 1 and Supplements 1 & 2, "Advanced Nuclear Fuels Corporation Generic Mechanical Design for Advanced Nuclear Fuels Corporation 9X9 – IX and 9x9 – 9X BWR Reload Fuel," October 1991.
- 14. ANF-89-98 (P)(A), "Generic Mechanical Design Criteria for BWR Fuel Designs," Revision 1 and Revision 1 Supplement 1, May 1995.
- 15. ANF-91-048 (P)(A), "Advanced Nuclear Fuels Corporation Methodology for Boiling Water Reactors EXEM BWR ECCS Evaluation Model," January 1993.

- 16. Commonwealth Edison Company Topical Report NFSR-0091, "Benchmark of CASMO/ MICROBURN BWR Nuclear Design Methods," Revision 0 and Supplements on Neutronic Licensing Analysis (Supplement 1) and La Salle County Unit 2 benchmarking (Supplement 2), December 1991, March 1992, and May 1992, respectively.
- 17. EMF-85-74 (P) Revision 0 and Supplement 1(P)(A) and Supplement 2(P)(A), "RODEX2A (BWR) Fuel Rod Thermal-Mechanical Evaluation Model," February 1998.
- 18. NEDE-24011-P-A-14 Revision 14, "General Electric Standard Application for Reactor Fuel (GESTAR)," June 2000.
- 19. NEDC-32981P Revision 0, "GEXL96 Correlation for ATRIUM-9B Fuel", September 2000.
- 20. ANF-1125(P)(A), Supplement 1 Appendix E, "ANFB Critical Power Correlation Determination of ATRIUM-9B Additive Constant uncertainties," September 1998.
- 21. ANF-91-048(P)(A), Supplements 1 and 2, "BWR Jet Pump Model Revision for RELAX," October 1997.
- 22. Commonwealth Edison Topical Report NFSR-0085, Revision 0, "Benchmark of BWR Nuclear Design Methods," November 1990.
- 23. Commonwealth Edison Topical Report NFSR-0085, Supplement 1 Revision 0, "Benchmark of BWR Nuclear Design Methods Quad Cities Gamma Scan Comparisons," April 1991.
- 24. Commonwealth Edison Topical Report NFSR-0085, Supplement 2 Revision 0, "Benchmark of BWR Nuclear Design Methods Neutronic Licensing Analyses," April 1991.