



Department of Energy
Washington, DC 20585

MAY 27 1988

Mr. Robert Browning, Director
Division of High-Level Waste Management
Office of Nuclear Material Safety
and Safeguards
U. S. Nuclear Regulatory Commission
Washington, D.C. 20555

Dear Mr. Browning:

Enclosed with this letter is a copy of Study Plan No. 8.3.1.15.1.5 entitled, "Excavation Investigations", prepared by the Nevada Nuclear Waste Storage Investigations (NNWSI) Project. This study plan corresponds to the study of the same number in the Consultation Draft Site Characterization Plan (SCP/CD) for the Yucca Mountain Site in Nevada. The plan describes the testing to be performed in one shaft, during the construction phase of the Exploratory Shaft Facility (ESF).

The Department of Energy (DOE) is currently re-evaluating the testing planned for the ESF as a part of the completion process of the SCP. Details of some activities may change as a result of this completion process and will be reflected in the statutory SCP as well as in revisions to the appropriate study plans.

The DOE has reviewed the plan for consistency with the content requirements for study plans as given in Attachment B to the Summary of the NRC/DOE Meeting on the Level-of-Detail for Site Characterization Plans and Study Plans (May 7-8, 1986). The DOE is submitting this plan for NRC review and comment as agreed in that meeting.

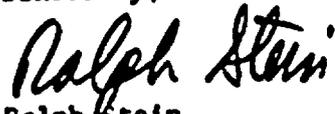
The DOE anticipates that NRC will review this plan as described in the NRC review procedure dealing with study plan review. These procedures specify that NRC will notify DOE in writing when their acceptance review is completed, notify DOE of any objections to the plan at the conclusion of the three month start work review, and provide the complete package of review comments within six months of the review initiation, if the NRC elects to perform a technical review of this plan.

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If you have any questions, please call Dr. Donald Alexander of my staff on 586-4889

Sincerely,



Ralph Stein
Acting Associate Director for
Systems Integration and Regulations
Office of Civilian Radioactive Waste
Management

Attachment

cc:

E. Kay, RW-1
S. Kale, RW-20
T. Isaacs, RW-40
C. Gertz, NNWSI

bcc:

S. Brocoum, RW-221
I. Alterman, RW-221
D. Alexander, RW-332
S. Singal, RW-332
M. Blanchard, NNWSI
D. Dobson, NNWSI
M. Fendleton, SAIC/LV
K. Czyscinski, Weston

EXCAVATION INVESTIGATION STUDY PLAN
SANDIA NATIONAL LABORATORIES
NNWSI GEOTECHNICAL PROJECTS DIVISION 6313
JANUARY 22,1988

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STUDY PLAN FOR WATER MOVEMENT TEST
Site Characterization Plan Study 8.3.1.2.2.2

1.0 Purpose and Objectives of Study

1.1 Purpose

The purpose of this study is to determine the rate of water movement downward through the unsaturated zone beneath Yucca Mountain, using measurements of chloride concentrations and chlorine isotopic compositions in samples of soil and tuff collected as part of the site characterization program. The objective of one phase of this study is to determine an upper bound on the amount of water that enters Yucca Mountain by infiltration. The objective of the second phase is to time water movements in the unsaturated zone by measuring chlorine-36/total chlorine ratios in samples that will be collected as the exploratory shaft is mined. The 301,000-yr half-life of chlorine-36 is useful for tracing water movements between 50,000 and 2,000,000 yr and is most useful between 100,000 and 1,000,000 yr.

1.2 Use of Results

The data from this test will be used as part of the information required by the Nevada Nuclear Waste Storage Investigations (NNWSI) Project to calculate releases to the accessible environment. These data will help establish an accurate model of the hydrologic characteristics of the unsaturated zone at Yucca Mountain. The hydrologic model will be used to compute radioactivity releases to the accessible environment as part of the repository performance assessment.

Another use of the data will be to estimate the rate of technetium-99 movement through the unsaturated zone. The technetium-99 is likely to be in the chemical form TcO_4^- , which, like chloride, is a nonsorbing geochemical form. The rate of movement of technetium will be no faster than the chlorine-36 rate of movement.

1.3 Resolution of Performance Issues

The rationale for the NNWSI site characterization program is presented in Section 8.1 of the NNWSI Site Characterization Plan (SCP). The issues-based strategy was guided first by an issue

identification procedure and then by performance allocation to define the activities needed to resolve the issues. The issues were divided into performance issues and design issues. The work in this study plan applies only to performance issues.

The primary issues that will use the data from this study are the following:

Issue 1.6: Will the site meet the performance objective for pre-waste-emplacment ground-water travel time as required by 10 CFR 60.113?

Issue 1.1: Will the mined geologic disposal system meet the system performance objective for limiting radionuclide material to the accessible environment as required by 10 CFR 60.112 and 40 CFR 191.13?

Important information required in the resolution of both of these issues will be derived from measurements of the ground-water velocities and fluxes in the unsaturated zone.

1.4 Tie to Regulations

As indicated in the discussion of performance issues, this study could provide support concerning compliance with several key regulations. The Department of Energy's siting guidelines [10 CFR 960.4-1-2(b)(1)] specify that a pre-waste-emplacment ground-water travel time greater than 10,000 yr along any path of likely radionuclide travel from the disturbed zone to the accessible environment would be a favorable condition. The long travel times that this test can measure will bear directly on the evaluation of this favorable condition. The data may be used to determine the nature and rates of hydrologic processes that have occurred during the Quaternary Period, which are specified in 10 CFR 960.4-2-1(b)(2). The sampling procedure for this test (see Section 3.1 below) is designed to detect stratigraphically influenced changes in the rate of water movement through the unsaturated zone. Such changes, if detected, will be used for validating the modeling of the geohydrologic system that is required in 10 CFR 960.4-2-1(b)(3). All of the above information will be used to support the higher level findings on the geohydrology disqualifying and qualifying conditions specified in 10 CFR 960.4-2-1(a) and (d).

The second major source of regulatory requirements is the technical criteria of the US Nuclear Regulatory Commission (NRC). In 10 CFR 60.113(a)(2), the NRC requires that the pre-waste-emplacment ground-water travel time along the fastest path of likely radionuclide travel from the disturbed zone to the accessible environment shall be at least 1,000 yr. The NRC also specifies that the geologic repository system performance following permanent closure shall conform to the applicable environmental standards for radioactivity as established by the Environmental Protection Agency

(10 CFR 60.112). The hydrologic flux in the unsaturated zone is an important component of the total system performance assessment, and the measurements in this study are part of the site characterization process to determine the unsaturated-zone flux.

2.0 Rationale for Use of Chlorine-36 and Chloride to Trace Water Movement in the Unsaturated Zone at Yucca Mountain

2.1 Estimates of Rates of Water Movement from Hydrologic Data

Determining the rate of water movement through the unsaturated zone at Yucca Mountain is one of the most important tasks for assessing the future performance of a nuclear waste repository, but it is a very difficult task. Montazer and Wilson (1984) discuss the data on water movement available through 1984. Their hydrologic terminology is used in this study plan, as it is in the NNWSI SCP. Estimates of downward flux through the potential repository host rock, the moderately to densely welded portion of the Topopah Spring Member of the Paintbrush Tuff formation, range from 1×10^{-7} to 0.2 mm/yr. These estimates were based on hydraulic gradient and effective permeability data derived from one borehole and from cores recovered from holes at more than one location. Analyses of geothermal heat-flux data from the same tuff unit indicate that the net hydrologic flux may be upward at a rate of 1 to 2 mm/yr, possibly from vapor-phase transport. Montazer and Wilson (1984) state that the hydrologic flux through the tuffaceous beds of Calico Hills, which underlie the host rock, is likely to be variable, but less than about 0.006 mm/yr downward, as estimated from measurements of effective hydraulic conductivities from core samples that included the zeolitic facies of this unit.

The hydrologic flux estimates outlined in the preceding discussion do not give a definitive picture of the rate of water movement to be expected through the unsaturated zone. If the flux through the Topopah Spring Member is assumed to be about 0.2 mm/yr downward, then estimates of ground-water travel time through the unsaturated zone are greater than 100,000 yr. Such estimates indicate that chlorine-36 techniques would provide data useful for hydrologic modeling.

2.2 Radiometric Determinations of Rates of Water Movement

Direct measurements of the rate of water movement through the unsaturated zone would be of great value. Radiometric methods are one potential technique for making such measurements. Determinations of tritium and carbon-14 in the unsaturated zone are discussed in the hydrochemistry study plan. The 5,730-yr half-life of carbon-14 permits dating to ages of 60,000 yr under favorable conditions. Other radiometric dating techniques have been considered. A survey of such techniques given by Phillips (1984) indicates that radiometric dating with iodine-129 may be possible for waters older than 10^6 years. The applicability of this technique to waters moving through the unsaturated zone at Yucca Mountain may be limited by the lack of a useful iodine-129 source.

The technique chosen to determine the water travel time through the unsaturated zone in this study is the measurement of chlorine-36 as a function of depth. Chlorine is deposited globally both in precipitation and in dry fallout. The source of most of the chlorine in this fallout is sea salt lofted into the troposphere by surface winds. A very small fraction of chlorine atoms in the fallout consists of chlorine-36, which results from cosmic ray reactions with argon in the atmosphere. The chlorine-36 half-life of 301,000 yr is appropriate for the travel times calculated from the hydrologic data. Geochemical properties of chlorine make it a useful tracer of subterranean water movements (Bentley et al. 1986). Chlorine is so electronegative that it exists as the nonvolatile chloride ion under most geohydrologic conditions. Bentley et al. (1986) state that chloride ions are among the least sorbed ions on solid surfaces because of their negative charge and small radius. Measurements of chlorine-36 discussed in Bentley et al. (1986) indicate the validity of using this technique for tracing water movements over long times.

At Yucca Mountain the technique discussed in this study plan will measure chloride carried into the tuff by meteoric water and now present in pore water or on the surfaces of the tuffs. This chloride traces the movement of water in the liquid phase through the unsaturated zone. Chlorine originally present in the tuffs (the chlorine-36 component of which should have decayed to negligible amounts at the present) may be included in the samples. Most of this chlorine may be chemically bound. Short leaching times should help minimize the introduction of this chlorine into the samples for the chlorine-36 measurements.

Measurements to aid in interpreting the chlorine-36 data include chloride concentration with depth and stable chlorine isotope ratios. The chloride concentration profile is expected to be relatively uniform, if the water movement in the unsaturated zone is uniform. Deviations in the chloride concentration profile may result from nonuniform evaporation or from mingling of waters caused by localized cross-cutting features. These data may help confirm patterns of nonuniform flow in the chlorine-36 data. The stable chlorine isotope ratio measurements may indicate that detectable differences can be observed in the chlorine-35/chlorine-37 ratio, depending on the origin of the chlorine. Such differences have been reported recently (Desaulniers et al. 1986). At Yucca Mountain, the chlorine-35/chlorine-37 studies may show that chlorine of meteoric origin has one ratio whereas chlorine originally present in the tuff has a different ratio. The chlorine-36 content associated with chlorine of meteoric origin is the only quantity of interest. Measurements of chlorine-35/chlorine-37 ratios in the samples for chlorine-36 analysis can be compared with the ratio determined for chlorine of meteoric origin and with the ratio measured for chlorine from tuff to correct the chlorine-36/chlorine ratio to that which should be observed in chlorine of meteoric origin.

The specific activity of chlorine-36 in the environment is so low that measurements of the chlorine-36 isotopic abundance have not been feasible, with a few exceptions, until the recent development of tandem accelerator mass spectrometric analyses. The sensitivity of this technique currently is approximately one atom of chlorine-36 in 10^{15} atoms of chlorine. The sample size required for these measurements is 10 mg of chloride or more. The background chlorine-36/chlorine ratio in surficial deposits of alluvium at Yucca Mountain has been measured in this work to be approximately 5×10^{-13} , which is more than 100 times greater than the limit of this technique. Any samples collected in which chlorine-36 has undergone detectable radioactive decay will result in chlorine-36/chlorine ratios lower than that of the cosmogenic background. Radiometric determinations are limited to samples that have been isolated from isotopic exchange with cosmogenic sources of chlorine-36.

Several recent studies suggest that chlorine-36 may be a suitable indicator of the rate of water movement. Andrews et al. (1986) used the chlorine-36/chlorine ratio to estimate ground-water residence times at the Stripa mine in Sweden and formulated conceptual ground-water flow paths to explain the evolution of the ratio.

Norris et al. (1987) used measurements of chlorine-36 in soil samples from two locations near Yucca Mountain to determine the infiltration of precipitation during the past quarter century and to examine the differences in surficial hydrologic infiltration between the two sites. The source of the chlorine-36 measured in this work was not from cosmic ray reactions with argon in the atmosphere. Instead, the chlorine-36 was deposited globally as fallout from high-yield nuclear weapons tests that were conducted at the surface of the Pacific Ocean between 1952 and 1962. The data can be interpreted in terms of an infiltration rate at Yucca Wash, located to the east of Yucca Mountain, of 1.8 mm/yr during the past quarter century. This value represents an in situ measurement of flux that is valuable in establishing the upper bound for the amount of water flowing downward through the unsaturated zone.

The mechanisms of water transport in the unsaturated zone are of interest for appropriate modeling of radionuclide transport. However, the chlorine-36/chlorine data from this study are unlikely to discriminate between fracture flow and porous flow because the chloride that is measured can result from water flow by a combination of mechanisms. The chlorine-36/chlorine data may shed light on the mechanism of water flow only if rapid fracture flow dominates to the extent that bomb pulse chlorine-36 is observed at great depths or if the hydrologic flow is so slow that hydrologists would describe the mechanism as porous flow.

2.3 Constraints on Chlorine-36 Studies

Analytical and Sampling Constraints

The specific activity of chlorine-36 present in tuff samples from Yucca Mountain, as in typical samples from other environments, is too small to permit direct measurements of the radioactive decay of chlorine-36. Conventional mass spectrometry can be used to measure chlorine-36/chlorine ratios as low as 10^{-10} , but the ratios in Yucca Mountain are approximately 5×10^{-13} for samples with contemporary cosmogenic chlorine-36. Therefore, the only feasible technique for this study is tandem accelerator mass spectrometry. The 10 mg of chloride required for the chlorine-36/chlorine measurement will be leached from crushed tuff samples, as described in Section 3 of this study plan. The chloride content of tuff samples from the Paintbrush Tuff formation at Yucca Mountain necessitates collecting about 40 kg of rock per sample. The collection process should involve little or no contact of water with the sample to be collected, to avoid inadvertent removal of the chloride before the leaching process that is part of the analysis procedure.

These constraints led to the necessity for using tuff samples collected as the exploratory shaft is mined. Some water will be used in the drilling and blasting operations, but large rubble pieces can be chosen to minimize any wetting of the major part of the rubble volume. This study could not be performed with core samples from conventional surface-based drilling, in which water is used as the lubricant for the drilling bit.

Samples will be collected from the exploratory shaft as shown in Figure 1. The sampling locations indicated were selected on the basis of stratigraphic data from USW G-4. The strata might be factors in controlling the downward movement of water through the unsaturated zone penetrated by the exploratory shaft. The chlorine-36 half-life constrains the interpretation of the data to water movements that have taken longer than 30,000 yr, because too little chlorine-36 decay has occurred to be detectable for younger times. Measurements of samples collected from the upper part of the exploratory shaft may give no useful data because of this threshold limitation. The half-life of chlorine-36 also constrains the measurements of age differences between samples to those that are greater than 30,000 yr. The data from deeper samples should provide information about water movement in the tuff above the repository horizon as well as below it.

The impact of this study on the potential repository site will be negligible. Each sample will require that about 40 kg of rubble be used for analysis. Preliminary plans call for the water used to construct the exploratory shaft to be tagged with 20 ppm of bromide. This will permit detection and correction for approximately 10 ppm of chlorine in that water. Some samples for chloride profile studies may be at shallow depths (<10 m) in locations of potential infiltration, but these locations will be selected after a field study of Yucca Mountain.

DEPTH, m (ft)	LITHOLOGY
ALLUVIUM	
TIVA CANYON MEMBER	WELDED, DEVITRIFIED TUFF
35.9 (118.0)	PARTIALLY WELDED VITRIC WEATHERED
BEDDED TUFF	BEDDED TUFF, VITRIC
YUCCA MT. 51.3 (168.2)	NONWELDED, VITRIC (PAH C.)
AND PAH 87.3 (188.0)	BEDDED TUFF, VITRIC (POORLY CONSOLIDATED)
CANYON MEMBERS	
71.1 (233.4)	CAVROCK ZONE, WELDED, CRYSTAL RICH
80.9 (265.6)	WELDED, DEVITRIFIED TUFF, VAPOR-PHASE CRYSTALLIZATION ZONE
121.0 (400.0)	WELDED, >10% LITHOPHYSAL CAVITIES
128.0 (420.0)	WELDED, SPARSE LITHOPHYSAE
143.2 (470.0)	
TOPOPAH SPRING MEMBER	WELDED, DEVITRIFIED TUFF, COMMON TO ABUNDANT LITHOPHYSAL CAVITIES (UP TO 40%)
207.2 (680.0)	WELDED, DEVITRIFIED TUFF, RARE LITHOPHYSAE; SOME HIGH-ANGLE FRACTURES PRESENT
235.0 (770.0)	WELDED, DEVITRIFIED TUFF, LITHOPHYSAL CAVITIES 2-30%; SPLINTERY AND CONCHOIDAL-TYPE PARTING COMMON THROUGHOUT INTERVAL. LOWER CONTACT GRADATIONAL.
343.7 (1127.9)	
381.0 (1250.0)	WELDED, DEVITRIFIED TUFF; LITHOPHYSAL CAVITIES EXTREMELY RARE TO ABSENT
394.0 (1293.0)	WELDED, PARTLY VITRIC, ZEOLITIC AND ARGILLIC
401.2 (1316.8)	WELDED TUFF VITROPHYRE
410.0 (1345.4)	MOD. WELDED TO NONWELDED, VITRIC
420.0 (1377.8)	NON- TO PARTLY WELDED, PARTLY ZEOLITIC
428.7 (1406.8)	BEDDED AND NONWELDED TUFF, SLIGHTLY TO MOD. ZEOLITIC
434.7 (1426.3)	BEDDED & NONWELDED TUFF ZEOLITE
443.4 (1456.6)	
TUFFS OF CALICO HILLS	NONWELDED TUFF, ZEOLITIC
451.1 (1480.0)	

NOT TO SCALE

Figure 1. USW G-4 stratigraphic column with proposed chlorine-36 sampling locations shown as circles. Total sampling depth will be constrained by the depth of the Exploratory Shaft Facility.

The analytical techniques for this study are available and are described in Section 3 of this plan. Cosmogenic chlorine-36 in samples of Yucca Mountain alluvium has been measured (Norris et al. 1987). The tandem accelerator mass spectrometric measurements have to be performed when the apparatus is available. There are a sufficient number of tandem accelerator users that a wait of several months can be expected. Exploratory shaft operations are not affected by this wait.

Chlorine-36 can be produced underground from neutron capture by chlorine-35. The neutrons result from the presence of uranium and thorium and their decay chains. Some neutrons come from spontaneous fission of the first members of the decay chains. The remainder are produced by (α, n) reactions on light elements. Calculations will be performed to determine whether in situ production of chlorine-36 will limit the interpretation of the data from this test to travel times shorter than the two million years permitted by the chlorine-36 half-life and current analytical techniques.

2.4 Potential for Interference with the Chlorine-36 Studies

The interferences to which this study is susceptible from exploratory shaft operations are due to the use of water, which has been discussed above, and the introduction of chlorine that could alter the in situ chlorine-36/chlorine ratio. The explosives used in mining the exploratory shaft may contain chlorine with negligible chlorine-36. Samples for this study will be collected to minimize the possibility of contamination from chlorine in the explosives.

3.0 Description of Chlorine-36 Study

The key parameter to be measured in this study is the ratio of chlorine-36 to total chlorine as a function of depth in the exploratory shaft at Yucca Mountain. Location of the exploratory shaft is shown in Figure 2.

3.1 Sample Collection

Most of the sample collection will be performed as the exploratory shaft is mined. The principal borehole (USW G-4) stratigraphy was used to select sampling depths on the basis of lithology and stratification that might be significant for hydrologic characteristics. When there were no stratigraphic features to guide the selection of sampling intervals, the maximum interval between samples was set arbitrarily at 30 m (100 ft). The locations of samples are shown in Figure 1. The depths of sampling are subject to minor modifications to account for the dip of the beds between USW G-4 and exploratory shaft 1 (ES-1) and because the stratigraphy at ES-1 may not be exactly the same as that at USW G-4. The data from the Shaft-Wall Mapping Test (see geologic study plans) will be monitored to ensure that the blasting rounds will be sampled where significant lithologic changes occur.

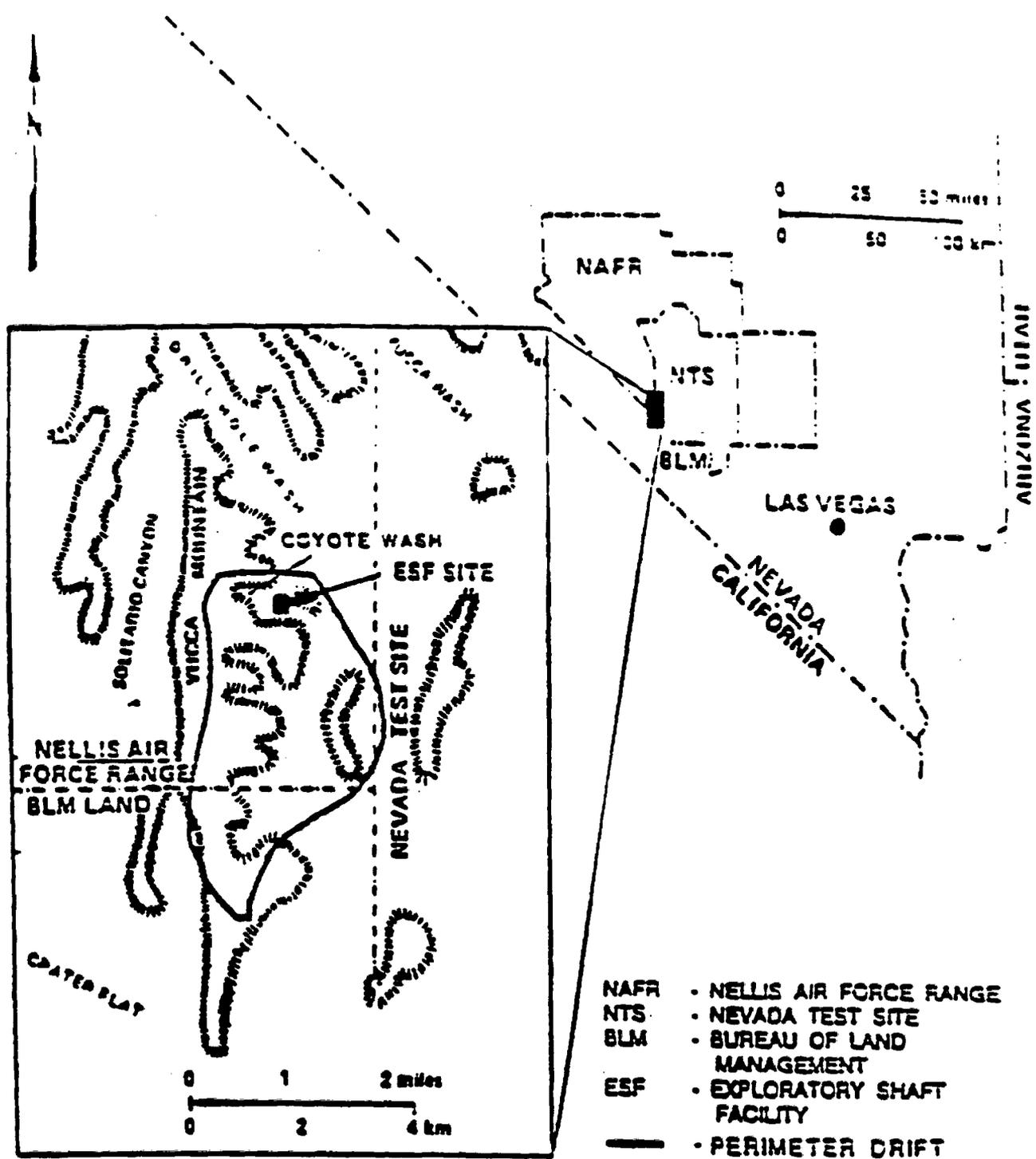


Figure 2. Relationship of the exploratory shaft facility to the Yucca Mountain site.

Sampling will be performed in accordance with the procedures that will be developed by the NNWSI Sample Overview Committee.

After each designated round, a geologist will descend to the working face of ES-1 to select rubble pieces larger than 130 mm (6 in.) in diameter for transport to the surface before the customary washdown. At the surface, the rubble may be segregated into a special container. A 208-L (55-gal) barrel will be packed with 100 to 200 kg (220 to 440 lb) of rubble and labeled with the depth from which the rubble was collected.

Accidental contamination of samples with chlorine-36 is not expected to be a problem. Chlorine-36, unlike carbon-14, is not transported in the vapor phase. No special atmospheric protection is necessary during sample preparation. Quantities of chlorine-36 produced from nuclear reactors or particle accelerators are not stocked routinely where the chlorine-36 sample preparation is likely to be performed.

Most chlorine that might accidentally contaminate the samples from ES-1 would come from chloride ions in the well J-13 water used in construction and from chlorine in the explosives that will be used during shaft-sinking operations. Therefore, the selection of larger pieces of rubble and the postponement of the customary washdown after blasting are two steps taken to mitigate potential sample contamination problems. The chloride content of well J-13 water is approximately 10 mg/L. The water used underground will be tagged with a sodium bromide tracer. The bromide concentration of the well J-13 water will be increased to 20 ppm, which is $\geq 10^3$ times the natural bromide concentration. The bromide content of the rubble selected for chlorine-36 analysis will be measured to permit the calculation of the chloride that might have been introduced from well J-13 water. Finally, a chlorine analysis of all the explosives used during the mining operations will be obtained and used to set a bound on the maximum amount of chlorine that could contaminate the samples from explosives.

The introduction of chlorine from well J-13 water and from explosives is expected to result in at most a minor perturbation in the data because the quantities of chlorine are small. Explosives customarily contain chlorine as a minor or a trace constituent. A problem more difficult to evaluate is the downward movement of water used in construction, which may leach chloride from tuff below the working depth before samples are collected for this test. Selecting rubble pieces with large diameters may ameliorate this problem, because water flow into the interior of an intact piece of tuff is slow. If the data indicate that leaching before sample collection is a problem, additional samples can be obtained by using horizontal dry coring techniques. The shaft liner and the surrounding tuff can be penetrated to a depth where the downward flow of water used in construction is unlikely to be a problem.

Some samples for measuring the chloride profile at depths to a few meters below the surface may be collected independently of the exploratory shaft mining operations, particularly if the hole for the exploratory shaft collar is excavated in a way that precludes obtaining samples at known depths. These data will aid in interpreting the chlorine-36 data by providing a source term for the expected quantity of meteoric chloride.

Any water encountered in sufficient volume during the construction of the exploratory shaft will be sampled and analyzed for chlorine-36. Pore water samples will be analyzed for chlorine-36 if sufficient volume can be obtained (see SCP Section 8.3.1.2.2.8, Hydrochemistry).

3.2 Measurement of Chlorine-36/Chlorine Ratio

The chlorine-36/chlorine ratio will be measured in the tuff samples collected from ES-1. A subcontractor will be chosen to prepare the rock samples and perform the analyses of chlorine-36, because a highly specialized technique is used (Elmore et al. 1984a). The rubble selected for the chlorine-36/chlorine ratio measurements will be crushed. The bromide content will be measured to determine the quantity of chloride from well J-13 water in the sample, and the crushed rock will be contacted with chloride-free water. Silver nitrate will be added to the water to precipitate about 50 mg of silver chloride. This precipitate will then be analyzed for the chlorine-36/chlorine ratio in a tandem accelerator mass spectrometer.

Descriptions of the apparatus and the techniques currently being used for tandem accelerator mass spectrometric analyses of chlorine-36 are given in Elmore et al. (1984a). Chlorine in the form of silver chloride is accelerated first as negative ions to eliminate interferences from argon-36, which does not form negative ions. The chlorine ions pass through an argon gas stripper in the center of the tandem accelerator. Ions with a charge of +7 are selected for mass analysis in a 90 degree magnetic analyzer. Chlorine-35 and chlorine-37 are measured in a multiplate gas ionization detector. Measurement of energy loss in this detector permits separation of chlorine-36 ions from interfering sulfur-36 ions. Measurements of chlorine-36 with precisions as good as +5% have been obtained. The data in this study plan, from analyses performed on a routine basis, are expected to be measured with a one standard deviation (σ) precision of +10%.

All activities in this study plan will be conducted at Quality Assurance Level I. Technical procedures will be written for sampling and analysis activities.

3.3 Analysis and Interpretation of Isotope Data

Table 1 summarizes the parameters that will be measured in this study and provides expected values. The range of expected values

for the chlorine-36/chlorine ratio is determined at the upper end by the contemporary quantity of cosmogenic chlorine-36 and at the lower end by the sensitivity of the tandem accelerator mass spectrometric technique. The bromide will be added as a tracer to tag the water used in the exploratory shaft; the maximum quantity added will be 20 ppm. The ion chromatography sensitivity limit is 20 ppb. The limit on the sample collection depth is determined by the total depth of the exploratory shaft. The final part of this test is the analysis and interpretation of the data.

TABLE 1. PARAMETERS MEASURED IN THIS TEST

<u>Procedure</u>	<u>Parameter Measured</u>	<u>Expected Value</u>
Tandem accelerator mass spectrometry	Chlorine-36/chlorine	1 to 600 x 10 ⁻¹⁵
Ion chromatography	Total bromide	≤20 ppm
Linear measurement	Depth of samples in ES	≤457 m (<1500 ft)
ASTM mercuric nitrate titration	Chloride concentration	1 to 1000 mg/kg rock
Conventional mass spectrometry	Chlorine-37/chlorine-35	-1 to 3 per mil relative to standard mean ocean chloride

The techniques used to obtain the chlorine-36/chlorine isotope ratios from tandem accelerator mass spectrometry measurements are documented in a paper by Elmore et al. (1984b). That paper discusses the calculation of the ratio of chlorine-36 to chlorine-35 + chlorine-37 in the sample, in a National Bureau of Standards (NBS) chlorine-36 standard, and in a reagent blank. The isotope ratios are corrected for mass fractionation, for background, and for interferences arising from the presence of sulfur-36. The NBS chlorine-36/chlorine ratios are used to normalize the ratios in the samples for inaccuracies introduced by the tandem accelerator. The value of the final chlorine-36/chlorine ratio in the sample is calculated as the mean of the corrected and normalized ratios from a sequence of measurements, weighted by the uncertainty of each determination.

Interpretation of the chlorine-36 data in terms of the rate of water movement through the unsaturated zone will require the consideration of processes that differentiate chloride movement from water movement. One process is that of anion exclusion. Positively charged components in the subterranean mineralogic environment can exclude negatively charged ions, which causes the anionic tracer to

move slightly faster than tritiated water (Daniels 1983). The second aspect of chloride movement that is important for hydrologic modeling is the nonvolatile character of these anions. If water movement through the unsaturated zone should be in downward pulses through the matrix in the liquid phase, followed by upward movement in the vapor phase, the chloride ions would move only in the liquid phase. The chlorine-36 decay data, then, might show an age that results from mixing chloride ions from more than one pulse. The data in this case still would be useful for calculating the average travel time of a radioactive waste nuclide such as technetium-99, which is expected to be transported in water as the TcO_4^- ion. Like chloride, the pertechnetate ion is both nonvolatile and nonsorbing.

A premise of data interpretation for this study is that the chlorine-36 fallout has been constant throughout the Quaternary Period. Experimental evidence bearing on this premise is being sought in ice cores from Camp Century, Greenland (Elmore et al. 1984a). A perturbation in the constancy of the chlorine-36 fallout occurred between 1952 and 1962. High-yield nuclear weapons tests at sea level in the Pacific Ocean resulted in significantly increased global fallout of chlorine-36. This "bomb pulse" has been used to measure infiltration that occurred during the past 30 yr into the top few meters of sandy loam in New Mexico (Bentley et al. 1986) and into alluvium at Yucca Mountain (Norris et al. 1987). Hydrologic flow at Yucca Mountain may occur through fractures in tuff and by some lateral flow, particularly through the Tiva Canyon and Pah Canyon Members. If chlorine-36 values higher than background are encountered in samples from the exploratory shaft, the data will be examined to determine if fracture flow or lateral flow might account for the inclusion of "bomb pulse" chlorine-36.

The ratio of chlorine-36 to chlorine as a function of depth will be correlated with the measured chloride concentration profile and with detailed data on fracture orientation and frequency. Regions of nonuniformity in the chloride concentration profile indicate nonuniform flow rates, and such nonuniform flow rates might be observable in the chlorine-36/chlorine profile. The data concerning fracture characteristics and distributions, to be provided by the US Geological Survey (USGS), will be studied as one possible explanation for the nonuniform flow.

3.4 Accuracy and Precision of Water Velocity Determinations

The chlorine-36 concentration data, when plotted against sample depth, provide a measure of water velocity down through the unsaturated zone, if a vertical flow path is assumed. The accuracy of the measurement from this test depends on the rate of water movement down through the unsaturated tuff. For velocities less than 5 mm/yr, the accuracy is high. It decreases for higher water velocities until the practical limit of the test is reached at water velocities of about 10 mm/yr. For water velocities greater than 10 mm/yr, the shorter lived nuclides discussed in Section 2.2 will be used. The following statistical analysis shows the sensitivity of this technique.

Power curves were used to estimate the probability of detecting small water movement velocities from chlorine-36/chlorine ratio measurements at the depths indicated in Figure 1. The analysis is based on a constant water flow rate throughout the volume penetrated by ES-1. A null hypothesis was tested, namely that the rate of water flow through the unsaturated zone is greater than or equal to 15 mm/yr (which corresponds to a slope of $-1.5 \times 10^{-4} \text{ m}^{-1}$ or greater when the natural logarithm of the chlorine-36/chlorine ratio is plotted versus depth). Figure 3 shows a plot of velocity versus power. Power is the probability of rejecting the null hypothesis, when the null hypothesis is false. The significance level of 0.05 implies a 5% chance of erroneously rejecting the null hypothesis. The three curves in the figure are labeled with the $\pm 1\sigma$ values of the individual data points.

The curves in Figure 3 show the probability that the measured data can distinguish between an actual velocity, shown on the abscissa, and the selected hypothetical velocity (greater than or equal to 15 mm/yr in this case). The curves show this probability for different uncertainties associated with the measured data. As the actual velocity approaches the hypothetical velocity, it becomes more likely that the two velocities cannot be distinguished. For example, when the actual velocity is 10 mm/yr, there is a 36% chance that the data will indicate a velocity greater than or equal to 15 mm/yr. However, when the actual velocity is less than about 5 mm/yr, there is essentially no chance that the data will indicate a velocity greater than 15 mm/yr.

Figure 4 shows a plot of the expected half-width of a symmetric 95% confidence interval for the average velocity. This plot shows that a velocity of 1 mm/yr can be estimated within a few percent. However, for a velocity of 5 mm/yr the error associated with the 95% confidence interval will be about ± 2 mm/yr with $\pm 1\sigma = 10\%$ measurement errors, which are expected, and will be considerably larger as the measurement errors increase. The maximum flux is expected to be 0.2 mm/yr for a saturation of 0.65 and a porosity of 0.14 (Montazer and Wilson 1984), which is approximately equal to a water velocity of 2 mm/yr. Figure 4 shows that water velocities less than 2 mm/yr will be measured with small uncertainties.

3.5 Equipment and Services Required

Two special facilities are required at the ES-1 site. One is a box at the surface (see Table 2) into which the rubble collected at a particular depth can be poured. The purpose of this box is to separate the sample material from the spoils pile until the sample can be packed in 208-L (55-gal) barrels. The second facility required at the ES-1 site is a metering device (Table 2) to introduce a definite, small quantity of water tracer into all water that is used for mining ES-1. In practice, a bromide tracer will be

POWER OF TEST WITH SIGNIFICANCE LEVEL = 0.05

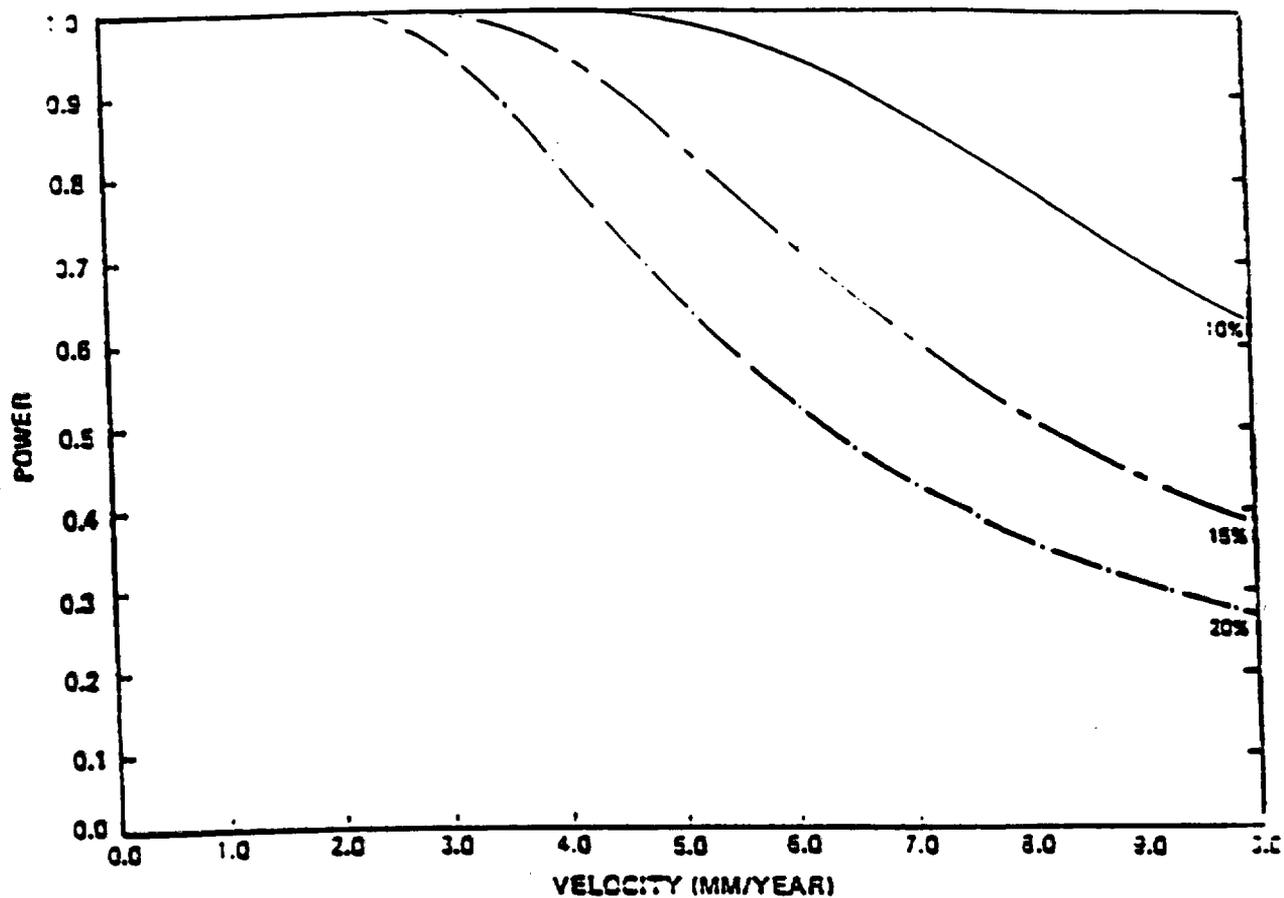


Figure 3. Power curves for measurements of the chlorine-36/total chlorine ratio. The curves are labeled with the $\pm 1\sigma$ values (in percentages) of the individual data points.

EXPECTED HALF-WIDTH OF 95% CONFIDENCE INTERVAL

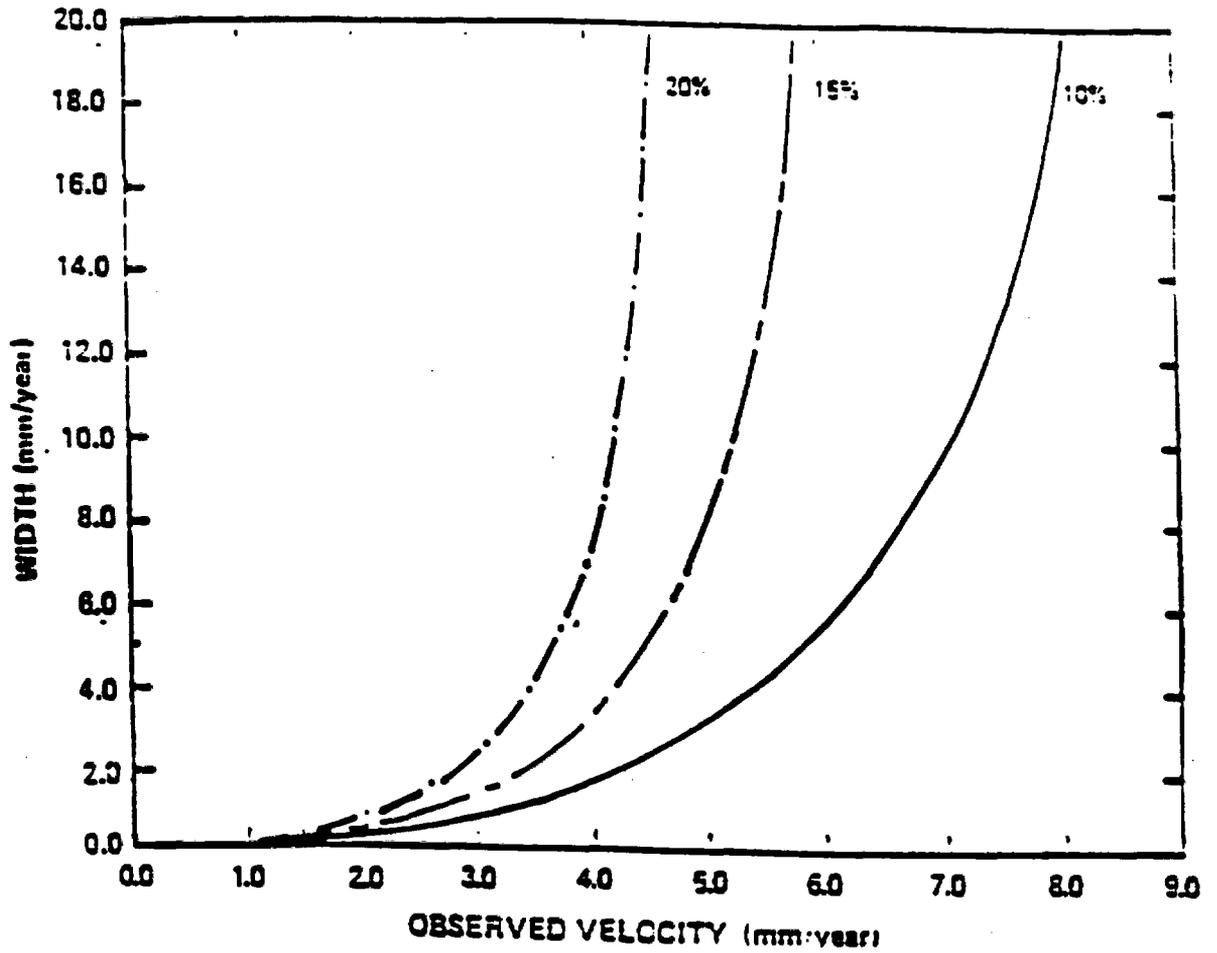


Figure 4. Confidence intervals for measurements of the chlorine-36/total chlorine ratio. The curves are labeled with the $\pm 1\sigma$ values (in percentages) of the individual data points.

Table 2. Instrumentation. Equipment. Materials. and Services for This Test

Item	Quantity	Description	Procurement Method
1. Box for rubble	1	Nonstandard	Designed and constructed by tester's organization
2. Water tracer metering system	1	Nonstandard	Designed and constructed by tester's organization
3. Water tracer. NaBr	1,120 kg	Standard	Tester's organization purchase order
4. 208-L (55-gal.) barrels	≤60	Standard	Tester's organization purchase order

SERVICES LIST

1. Depth of designated blasting round		Standard	Shaft-sinking subcontractor
2. Geologist to select and pack rubble pieces for chlorine-36 analysis (about 40 hours total)			Fenix and Scisson
3. Extract chloride from rubble; analyze for chlorine-36, chloride, and bromide; interpret data		Nonstandard	Tester's organization subcontractor

bromide tracer will be added to all well J-13 water used at the exploratory shaft site. A surge tank is likely to be the apparatus of choice for this application. Water samples will be analyzed periodically to verify the water tracer concentration. Water used at the surface for site preparation and dust control also will be tagged with a suitable tracer.

3.6 Representativeness of Velocity Determinations from the Exploratory Shaft

A question can be raised concerning the representativeness of the data from the exploratory shaft when it is extrapolated over the entire area of the repository, because the exploratory shaft allows access to only one point in the area. In the relatively unfaulted portion of Yucca Mountain, spatial results are expected to be fairly uniform. If downward water movement tends to be episodic with either short or long periodicity, interpretation of chlorine-36/chlorine ratios at different depths may be complicated. However, Montazer and Wilson (1984) indicate that such pulses are likely to occur only in the shallow unsaturated zone.

Representativeness of results is also influenced by the degree to which water transport occurs in the matrix of the tuff versus fractures. If most recharge occurs through major structural features as suggested in the conceptual model of Montazer and Wilson (1984), spatial variability may be large. Washes and other areas underlain by structural features would be likely to provide higher velocities, whereas relatively nonfaulted areas would provide lower velocities. The data of most concern to predictions of repository performance are those from the repository level and below. The potential variability in water velocities is therefore unlikely to cause significant changes in the determination of water movement by chlorine-36 tracer studies because the effects of temporal changes in infiltration are likely to be manifested only at shallow depths.

Samples could be collected at other locations by using a new dry-drilling technique, reverse vacuum drilling (Whitfield 1985). Correlation of the chlorine-36 results with detailed stratigraphic mapping of fracture frequency data would not be possible to the extent that will be possible in the exploratory shaft. If spatially distributed data are likely to improve knowledge of the hydrologic flow through the unsaturated zone, this alternative method of sample collection could be used at a later date.

Another source of material for chlorine-36 analyses is perched water that might be encountered during the construction of the exploratory shaft. If the chloride content of the perched water is 10 ppm, as in well J-13 water, then 2 to 3 L per sample would be sufficient to obtain material for a chlorine-36 analysis. The data from these analyses might provide information about the rate of water flow in the unsaturated zone at Yucca Mountain.

4.0 Application of Results

4.1 Site Investigation

The work in this study plan will provide information for determining the ground-water travel time in the unsaturated zone at Yucca Mountain. Water movements will be characterized through measurements of the chloride concentrations and the chlorine-36/chlorine ratios, both as a function of depth below surface. Results from this study will be used in assessing water movement at the site. Information from chlorine-36 data may be used for inferring rates of fracture flow relative to matrix flow. The chlorine-36 vertical distribution may permit assessment of the role of convective water movement relative to dispersive movement. This study will be performed in parallel with USGS hydrochemistry studies and will precede USGS in situ tests. The groups working on these tests plan to exchange information as they progress. The use of rates of chlorine-36 migration as an upper bound on technetium-99 migration may also provide valuable confirmatory support to results from geochemical studies summarized in Section 8.2.2.4.2 of the SCP.

4.2 Resolution of Performance Issues

The application of results in the site investigation work can be tied directly to resolution of key performance assessment issues. The assessment of total system performance summarized in Section 8.2.2.1.1.1 of the SCP is dependent upon the ranges of potential flux passing through and below the repository level. An independent confirmation of flux estimates by rates of movement derived from chlorine-36 studies would provide valuable support to the transport and release predictions. Both containment by the waste package (SCP Section 8.2.2.1.1.4) and release from the engineered barrier system (SCP Section 8.3.2.1.1.5) are strongly dependent upon the rate of water movement through the repository horizon. Therefore, confirmation of low flux values by independent analytical studies will reduce uncertainties in meeting the waste package and engineered barrier system performance objectives.

As indicated in Section 2 of this study plan, confidence in meeting the 1,000-yr pre-waste-emplacment travel time requirement will increase if chlorine-36 samples below the repository horizon indicate rates of movement far too slow for a shorter travel time.

5.0 Schedule and Milestones

<u>Item</u>	<u>Date</u>
Develop water metering system for NaBr tracer	Constructed and operational by time of exploratory shaft site preparation
Commence sample collection	Start of exploratory shaft construction
Conclude sample collection	Completion of exploratory shaft to depth
Complete chlorine-36/chlorine ratio analyses	1 yr after completion of exploratory shaft to depth
Complete data interpretation and final report	21 months after exploratory shaft completed to depth

A chart showing the anticipated progress in this study is shown in Figure 5.

Milestone

R495	Infiltration rates from chlorine distributions at Yucca Mountain
M623	Final ESF chlorine-36 report

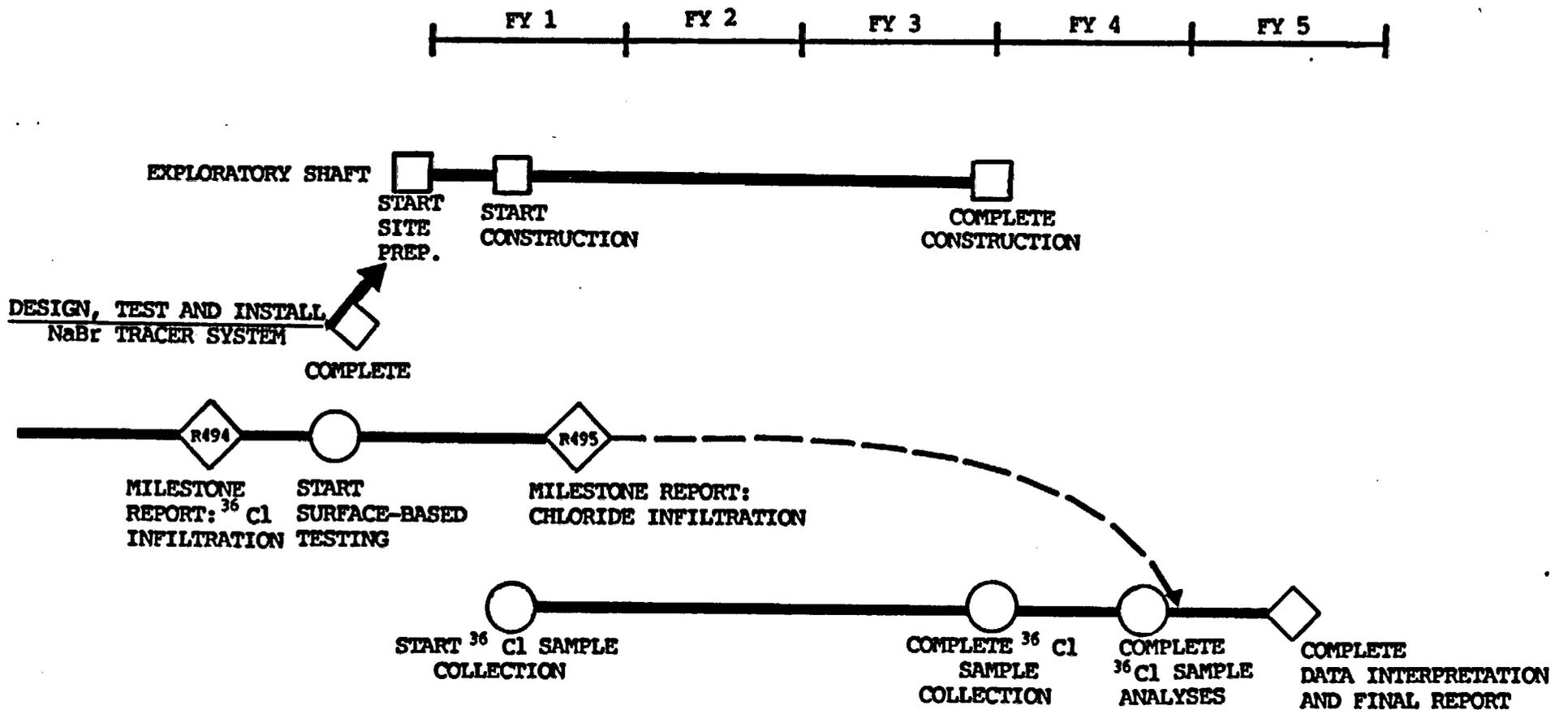


Figure 5. Anticipated progress in this study.

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