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Initial Issue

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# CALCULATION TITLE PAGE

# CALCULATION NUMBER: PSAT 3019CF.QA.05

CALCULATION TITLE: Fuel Handling Accident Dose for Vermont Yankee

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#### Purpose

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The purpose of this calculation is to provide an analysis of the Fuel Handling Accident (FHA) for Vermont Yankee. This update provides (1) implementation of the Reference 1 (AST) source terms and (2) both offsite and control room doses.

#### **Summary of Results**

Table 1 - FHA Summary of Dose Results (TEDE in Rem/Applicable Reference 1 Limit)

Case	Control Room	EAB	LPZ
0% Ground-Level Release, 24-Hour Decay	0.15305/5	0.47194/6.3	< 0.47194/6.3
20% Ground-Level Release, 24-Hour Decay	3.14204/5	1.59761/6.3	<1.59761/6.3
0% Ground-Level Release, 96-Hour Decay	0.10708/5	0.27413/6.3	< 0.27413/6.3
20% Ground-Level Release, 96-Hour Decay	2.19841/5	0.92799/6.3	< 0.92799/6.3

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This table shows that all cases meet the applicable limits at all locations. Appendix B explains that in order to have acceptable control room doses without any containment credit (i.e., 100% ground level release), a miminum of 14 days' decay is needed.

#### Methodology

This dose analysis fully complies with NRC Regulatory Guide 1.183 (Reference 1). Following accident initiation (either at 24 or 96 hours after shutdown), the radionuclide inventory from the damaged fuel pins is assumed to leak out to the environment instantaneously (even though releases to the environment could be assumed to occur over a 2-hour period according to Reference 1).

Credit is taken for the plant stack in achieving an elevated release for at least a portion of the activity released from the damaged fuel. In one case, 100% of the activity is assumed to be released to the environment from the plant stack; in a second case, 20% of the activity is assumed to be released to the environment at ground level and 80% is assumed to be released to the environment at ground level and 80% is assumed to be released to the environment from the plant stack. In no case is SGTS filtration credited. Due to these simplifying, conservative assumptions, a spreadsheet is used to calculate the control room, EAB, and LPZ doses.

The time duration that corresponds to the 20% release of activity to the environment at ground level (were a two-hour release to be considered as opposed to an instantaneous release) is different depending on release assumptions. If the activity release rate were assumed to be uniform, the 20% release would correspond to  $0.2 \times 120$  minutes = 24 minutes out of the two hours. If the activity release were assumed to correspond to a constant fractional release rate and 99% of the release were assumed to occur over two hours, the 20% release would correspond to [ln(0.8)/ln(0.01)] x 120 minutes = 6 minutes out of the two hours. Either of these two assumptions would be consistent with Reference 1.

Releases account for:

- a 1.02 multiplier on licensed power,
- a radial peaking factor of 1.65,
- 5% gap activity (except 10% for Kr85 and 8% for I131),
- a pin failure fraction of 0.571% corresponding to 2.1 assemblies out of 368 assemblies,
- an overall iodine DF of 200 and an infinite DF for other radionuclides except for noble gas.

The TEDE values obtained from the revised analysis are compared with the 6.3 rem FHA TEDE limit for offsite doses and the 5 rem TEDE limit for the control room (Reference 1).

#### Assumptions

Assumption 1: The accident is assumed to occur either 24 hours or 96 hours after shutdown. Consequently, core inventories were calculated that correspond to each decay time.

Justification: Fuel handling would not begin before 24 hours after shutdown. 96 hours after shutdown is more typical.

Assumption 2: The release to the environment from the refueling floor occurs within two hours.

Justification: Reference 1

Assumption 3: The DF in the refueling pool does not exceed 200 for iodine. No DF is applied to noble gas, and the DF for other radionuclides is assumed to be infinite.

Justification: Reference 1

Assumption 4: Credit is taken for containment, collection, and elevated release of at least 80% of the activity escaping the fuel pool. No credit is needed (or taken) for SGTS filters.

Justification: As can be seen from the results summary, the ground level release is limited to 20% of the activity released from the fuel pool.

#### References

- 1. "Alternative Radiological Source Terms for Evaluating Design Basis Accidents at Nuclear Power Reactors", US NRC Regulatory Guide 1.183, Revision 0, July 2000
- 2. PSAT 3019CF.QA.03, "DESIGN DATA BASE FOR APPLICATION OF THE REVISED DBA SOURCE TERM TO VERMONT YANKEE", Revision 0
- 3. RADDECAY Version 3, Grove Engineering, Inc., 1990.
- 4. VY Calculation VYC-2260, "Bounding Core Inventories of Actinides and Fission Products for Design-Basis Applications at 1950 MWt" Revision 0
- 5. S. L. Humphries et al, "RADTRAD: A Simplified Model for Radionuclide Tansport and Removal and Dose Estimation", NUREG/CR-6604, Sandia National Laboratories, December 1997.

#### **Design Inputs**

Design Input Data (Reference 2 for all inputs, Item numbers given in brackets)

Power Level: 1950 MWt [8.1]

Core inventory at shutdown: see Item 1.1 of Reference 2 Total number of fuel assemblies in core: 368 assemblies [1.2] Number of damaged assemblies: 2.1 [2.4] Gap release fractions:

Radio-nuclide	Release
Group	Fraction from
-	Gap to
	Coolant
Kr-85	10%
Other NG	5%
I-131	8%
Other Iodines	5%

[2.5]

Peaking factor: 1.65 [2.6]

Control Room Free Volume: 41,533.75 ft<sup>3</sup> [3.4]

X/Q values in sec/m<sup>3</sup>:

EAB:	1.7E-3 (ground-level)	
	2.03E-4 (1 <sup>st</sup> half-hour elevated), 1.54E-3 (2 <sup>nd</sup> half-hour	
	elevated), 9.17E-5 (remainder elevated) [5.1	I)
LPZ:	*	-
CR:	5.89E-3 (ground-level)	
•	2.39E-4 (1 <sup>st</sup> half-hour elevated), 1.05E-6 (2 <sup>nd</sup> half-hour	
	elevated), 8.7E-7 (remainder elevated) [5.3	۶ <b>]</b>
		-

\*LPZ dose not necessary since release is limited to two hours and EAB is more limiting

Breathing Rate in m<sup>3</sup>/s (from start of release): 3.5E-4 [5.4]

Iodine Species: 99.85% elemental, 0.15% organic\*\* [2.7]

**\*\*** Iodine chemical form not critical since control room filters are not used. Elemental iodine DF adjusted to obtain overall iodine of DF of 200 per Reference 1. No DF applied to organic iodine.

#### Calculation

Core inventories at one or four days after shutdown are calculated using the RADDECAY Code (Reference 3). The gap activity of noble gas and iodine (set at 99.85% elemental, 0.15% organic per References 1 and 2) is added from the core to the gap.

The starting point of the calculation was the t = 0 shutdown inventories (Ci/MWt) from Reference 2, Item 1.1. RADDECAY was then run starting with the t = 0 inventories for the noble gas and iodine isotopes. Given the activity (Ci or Ci/MWt) of an isotope at t = 0, RADDECAY calculates the curies or Ci/MWt at any subsequent time of that isotope and its daughters. To get the total curies of the isotope of interest one must add the curies resulting from its direct decay plus the curies resulting from decay in chains in which it is a daughter product.

For Kr83m, Kr85, Kr85m, I133 and I134, there were no shutdown activities listed for certain of their parent nuclides (Br83, Br85, Te133, Te133m, and Te134). These were obtained directly from Reference 4. In all cases, the activity contribution from these additional nuclides is negligible except for Br83 to Kr83m and Te134 to I134. While the parents contributed markedly to the activity for Kr83m and I134, the EAB and CR dose contribution for both of these nuclides is zero to five significant figures; therefore, the contributions have no significance for the dose.

The final activities are shown in Table 2.

Nuclide	Shutdown	Adjusted	24 Hours	96 Hours
Br83	4.24E+03	*	*	*
Kr83m	4.24E+03	same	15.6	nceligible
Br85	9.61E+03	*	*	*
Kr85m	9.71E+03	same	239	negligible
Kr85	5.05E+02	1.01E+03	1010	1009
Kr87	1.94E+04	same	0.038	negligible
Kr88	2.75E+04	same	72.3	negligible
Kr89	3.46E+04	same	negligible	negligible
Tel31m	4.31E+03		*	*
I131	2.85E+04	4.56E+04	42105	32776
Xe131m	3.18E+02	same	327	338
Te132	3.97E+04	+	*	*
<b>I</b> 132	4.05E+04	same	33065	17466
Te133m	2.30E+04	*	*	*
Te133	3.39E+04	*	*	*
I133	5.79E+04	same	26656	2420
Xe133m	1.76E+03	same	1594	766
Xe133	5.78E+04	same	55528	40184
Te134	5.31E+04	*	*	*
I134	6.43E+04	same	negligible	negligible
I135	5.39E+04	same	4351	2.3
Xe135m	1.14E+04	same	negligible	negligible
Xe135	2.33E+04	same	15285	106
Xe137	5.07E+04	same	negligible	negligible
Xe138	5.05E+04	same	negligible	negligible
* Considered	d as parent onl	У		

#### Table 2 – Core Inventories (per MWt) for FHA

These activities are compared to those calculated as part of the check calculation in Appendix A (see Table A-1).

The offsite X/Qs are from Reference 2 as previously noted. A weighted-average X/Q is calculated depending on the percentage of activity released with the elevated release CR and EAB X/Q and the ground-level release CR and EAB X/Q. Cases for both zero and 20% ground release are considered. As noted under Methodology, if it is assumed that the normalized release to the environment is linear (i.e., 0.5 per hour for two hours), then the 20% ground-level X/Q means that the ground-level release lasted 0.4 hours or 24 minutes. If a constant fractional release rate is assumed such that 99% is released in two hours (2.3 per hour), then the 20% ground-level X/Q means that the ground level release lasted approximately 0.1 hour or 6 minutes.

So using the database (Reference 2) values as follows for the CR:

Stack (fumig):	2.39E-4
Stack (norm):	1.05E-6 (1/2 hour), 8.7E-7 (1 hour)
RB siding:	5.89E-3

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the "zero" case would just use a weighted average  $0.25 \times 2.39E-4 + 0.25 \times 1.05E-6 + 0.5 \times 8.7E-7 = 6.04E-5$ , while the "20%" case would use a weighted average of  $0.2 \times 5.89E-3 + 0.25 \times 2.39E-4 + 0.25 \times 1.05E-6 + 0.3 \times 8.7E-7 = 1.24E-3$ .

In like manner, for the EAB dose:

Stack (fumig):	2.03E-4
Stack (norm):	1.54E-4 (1/2 hour), 9.17E-5 (1 hour)
Ground-level:	1.7E-3

the "zero" case would just use a weighted average  $0.25 \times 2.03E-4 + 0.25 \times 1.54E-4 + 0.5 \times 9.17E-5 = 1.35E-4$ , while the "20%" case would use a weighted average of  $0.2 \times 1.7E-3 + 0.25 \times 2.03E-4 + 0.25 \times 1.54E-4 + 0.3 \times 9.17E-5 = 4.57E-4$ .

The breathing rate of  $3.5E-4 \text{ m}^3/\text{s}$  is taken from Reference 2.

Note that no credit is taken for the SGTS filtration.

#### Results

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An EXCEL spreadsheet calculation has been carried out to obtain the results for each of four cases (0% and 20% elevated release for 24 hours and 96 hours decay). The spreadsheet is constructed as follows:

Rows 1 and 2: Title and headings for X/Q values (EAB and CR)

Denston Damas () (11/4) and sumting for an estated

RUW J.	Reactor Power (WWW) accounting for uncertainties
Row 4:	Control Room free volume $(ft^3)$
Row 5:	Release fraction (fraction of total inventory released during the accident)
	RF = 0.05 x (no. of damaged assemblies/total no. of fuel assemblies in core)
	$RF = 0.05 \times 2.1 / 368 = 2.85E-4$
Row 6:	Radial power peaking factor
Column 1:	Radionuclides, with distinction between iodine chemical forms
Column 2:	Decayed core inventory (24 hours or 96 hours, as appropriate)
Column 3:	Whole Body DCF, equal to "Cloudshine Effective" from Ref. 5 after conversion to rem-m <sup>3</sup> /Ci-sec
Column 4:	CEDE DCF, equal to "Inhaled Chronic Effective" from Ref. 5 after conversion to rem/Ci
Column 5:	TEDE DCF = (Whole Body DCF) + (CEDE DCF x Breathing Rate)
Column 6:	CR TEDE DCF = (Whole Body DCF x (CR Volume) <sup><math>0.338</math></sup> /1173) + (CEDE DCF x
	Breathing Rate)
	This CR DCF differs from the TEDE DCF as it includes a finite volume correction
	for the Whole Body dose taken from Ref 1. CR volume must be in ft <sup>3</sup> .
Row 6: Column 1: Column 2: Column 3: Column 4: Column 5: Column 6:	RF = 0.05 x 2.1 /368 = 2.85E-4 Radial power peaking factor Radionuclides, with distinction between iodine chemical forms Decayed core inventory (24 hours or 96 hours, as appropriate) Whole Body DCF, equal to "Cloudshine Effective" from Ref. 5 after conversion to rem-m <sup>3</sup> /Ci-sec. CEDE DCF, equal to "Inhaled Chronic Effective" from Ref. 5 after conversion to rem/Ci TEDE DCF = (Whole Body DCF) + (CEDE DCF x Breathing Rate) CR TEDE DCF = (Whole Body DCF) + (CEDE DCF x Breathing Rate) CR TEDE DCF = (Whole Body DCF x (CR Volume) <sup>0.338</sup> /1173) + (CEDE DCF x Breathing Rate) This CR DCF differs from the TEDE DCF as it includes a finite volume correction for the Whole Body dose taken from Ref. 1. CR volume must be in ft <sup>3</sup> .

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Column 7:	EAB TEDE = (Ci/MWt) x (Power Level) x (Release Fraction) x (Peaking Factor) $\bar{x}$ (Appropriate Nuclide Multiplier of 1.0 for noble gas, 0.0015 for organic iodine, or 0.9985 divided by DF = 285 for elemental iodine) x (EAB X/O) x (TEDE DCF)
Column 8:	CR TEDE = (Ci/MWt) x (Power Level) x (Release Fraction) x (Peaking Factor) x (Appropriate Nuclide Multiplier of 1.0 for noble gas, 0.0015 for organic iodine, or 0.9985 divided by DF = 285 for elemental iodine) x (CR X/Q) x (CR TEDE DCF)

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The "appropriate nuclide multipilers" are 1.0 for the noble gases, 0.0015 for organic iodine, and (1.0 - 0.0015)/(refueling pool DF) for the elemental iodine. The refueling pool DF for elemental iodine is calculated as follows:

- 1. Assume an effective DF of 200.
- 2. The fraction of the iodine inventory released from the pool is 1/200 = 0.005. Of this, 0.0015 is for organics, so the elemental iodine release fraction is 0.0035.
- 3. DF =  $1.0/0.0035 \approx 285$ .

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The spreadsheet results for 24 hour decay before the fuel handling accident are shown in Tables 3 and 4 for 0% ground level release and 20% ground level release, respectively. Corresponding results for 96 hours after shutdown appear in Tables 5 and 6. Control room and EAB doses are explicitly calculated; and because the release occurs within two hours, the EAB doses are bounding for the LPZ.

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Table 3. Doses after a Fuel Handling Accident (0% ground-level release, 24-hour decay).

VY FHA (24 hrs)		EAB	CR				
X/Qs =		1.35E-04	6.04E-05	$sec/m^3$ (0	% release at grou	nd level)	
Power =	1950	MWt			-		
CR Vol =	41533.75	ft <sup>3</sup>					
Rel Frac. =	2.85E-04						
Peaking =	1.65	WB	CEDE	TEDE	CR TEDE	EAB	CR
Nuclide	Ci/MW	DCF	DCF	DCF	DCF	TEDE	TEDE
Kr83m	1.56 <del>E+</del> 01	1.49E-05	. 0	1.5E-05	5E-07	0.00000	0.00000
Kr85m	2.39E+02	0.0277	0	0.0277	0.0009	0.00082	0.00001
Kr85	1.01E+03	4.40E-04	0	0.00044	1E-05	0.00006	0.00000
Kr87	3.80E-02	0.1524	0	0.1524	0.0047	0.00000	0.00000
Kr88	7.23E+01	0.3774	0	0.3774	0.0117	0.00338	0.00005
Kr89	0.00E+00	0.323	0	0.323	0.01	0.00000	0.00000
Xe131m	0.00E+00	0.00149	0	0.00149	5E-05	0.00000	0.00000
Xe133m	0.00E+00	0.00507	0	0.00507	0.0002	0.00000	0.00000
Xe133	5.30E+04	0.00577	0	0.00577	0.0002	0.03787	0.00053
Xe135m	0.00E+00	0.07548	0	0.07548	0.0023	0.00000	0.00000
Xe135	1.45E+04	0.04403	0	0.04403	0.0014	0.07903	0.00110
Xe137	0.00E+00	0.0303	0	0.0303	0.0009	0.00000	0.00000
Xe138	0.00E+00	0.199	0	0.199	0.0062	0.00000	0.00000
I131Org	4.21E+04	0.06734	32893	11.5799	11.515	0.09054	0.04028
I132Org	3.31E+04	0.4144	381.1	0.54779	0.1462	0.00336	0.00040
I133Org	2.67E+04	0.10878	5846	2.15488	2.0495	0.01067	0.00454
I134Org	0.00E+00	0.481	131.35	0.52697	0.0609	0.00000	0.00000
I135Org	4.35E+03	0.3069	1228.4	0.73684	0.4395	0.00060	0.00016
I131Elem	4.21E+04	0.06734	32893	11.5799	11.515	0.21147	0.09408
I132Elem	3.31E+04	0.4144.	381.1	0.54779	0.1462	0.00786	0.00094
II33Elem	2.67E+04	0.10878	5846	2.15488	2.0495	0.02491	0.01060
I134Elem	0.00E+00	0.481	131.35	0.52697	0.0609	0.00000	0.00000
I135Elem	4.35E+03	0.3069	1228.4	0.73684	0.4395	0.00139	0.00037
					Total TEDE=	0.47194	0.15305

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# Table 4. Doses after a Fuel Handling Accident (20% ground level release, 24-hour decay).

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	VY FHA (24 hrs)		VY FHA (24 hrs) EAB CR					
	Ground Level X/Qs =		4.57E-04	1.24E-03	sec/m3 (2	0% release at g	round level	)
	Power =	1950	MW(t)					
	CR Vol =	41533.75	ft3					
	Rel Fract =	2.85E-04				•,		
	Pcaking =	1.65	WB	CEDE	TEDE	CR TEDE	EAB	CR
	Nuclide	Ci/MW	DCF	DCF	DCF	DCF	TEDE	TEDE
·:,	Kr83m	1.56E+01	1.49E-05		1.5E-05	5E-07	.0.00000	0.00000
	Kr85m	2.39E+02	0.0277	0	0.0277	0.0009	0.00277	0.00023
	Kr85	1.01E+03	4.40E-04	0	0.00044	1 <b>E-05</b>	0.00019	0.00002
	Kr87	3.80E-02	0.1524	0	0.1524	0.0047	0.00000	0.00000
	Kr88	7.23E+01	0.3774	0	0.3774	0.0117	0.01143	0.00096
	Kr89	0.00E+00	0.323	0	0.323	0.01	0.00000	0.00000
	Xe131m	0.00E+00	0.00149	0	0.00149	5E-05	0.00000	0.00000
	Xe133m	0.00E+00	0.00507	0	0.00507	0.0002	0.00000	0.00000
	Xe133	5.30E+04	0.00577	0	0.00577	0.0002	0.12820	0.01079
	Xe135m	0.00E+00	0.07548	0	0.07548	0.0023	0.00000	0.00000
	Xe135	1.45E+04	0.04403	0	0.04403	0.0014	0.26754	0.02252
	Xe137	0.00E+00	0.0303	0	0.0303	0.0009	0.00000	0.00000
	Xe138	0.00E+00	0.199	. 0	0.199	0.0062	0.00000	0.00000
	I131Org	4.21E+04	0.06734	32893	11.5799	11.515	0.30648	0.82691
	I132Org	3.31E+04	0.4144	381.1	0.54779	0.1462	0.01139	0.00825
	I133Org	2.67E+04	0.10878	5846	2.15488	2.0495	0.03611	0.09318
	I134Org	0.00E+00	0.481	131.35	0.52697	0.0609	0.00000	0.00000
	I135Org	4.35E+03	0.3069	1228.4	0.73684	0.4395	0.00202	0.00326
	I131Elem	4.21E+04	0.06734	32893	11.5799	11.515	0.71585	1.93140
	I132Elem	3.31E+04	0.4144	381.1	0.54779	0.1462	0.02659	0.01926
	I133Elem	2.67E+04	0.10878	5846	2.15488	2.0495	0.08433	0.21763
	I134Elem	0.00E+00	0.481	131.35	0.52697	0.0609	0.00000	0.00000
	I135Elem	4.35E+03	0.3069	1228.4	0.73684	0.4395	0.00471	0.00762
					•	Total TEDE	1.59761	3.14204

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Table 5. Doses after a Fuel Handling Accident (0% ground level release, 96-hour decay).

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	VY FHA	(96 hrs)	EAB	CR					
	Ground Lev	rel X/Qs =	1.35E-04	6.04E-05	sec/m <sup>3</sup> (0%	release at ground	l level)		
	Power =	1950	MWt						
	CR Vol =	41533.8	ft <sup>3</sup>						
	Rel Frac. =	2.85E-04							
	Peaking =	1.65	WB	CEDE	TEDE	CR TEDE	EAB	CR	
	Nuclide	Ci/MW	DCF	DCF	DCF	DCF	TEDE	TEDE	
in the second of	Kr83m	O	1.49E-05		1.5E-05	SE-07	0.00000	0.00000	وري المحاطية المتعادية
	Kr85m	0	0.0277	0	0.0277	0.0009	0.00000	0.00000	
	Kr85	1009	4.40E-04	0	0.00044	1E-05	0.00005	0.00000	
	Kr87	0	0.1524	0	0.1524	0.0047	0.00000	0.00000	
	Kr88	0	0.3774	0	0.3774	0.0117	0.00000	0.00000	
	Kr89	0	0.323	0	0.323	0.01	0.00000	0.00000	
	Xe131m	338	0.00149	0	0.00149	5E-05	0.00006	0.00000	
	Xe133m	766	0.00507	0	0.00507	0.0002	0.00048	0.00001	
	Xe133	40184	0.00577	0	0.00577	0.0002	0.02871	0.00040	
	Xe135m	0	0.07548	0	0.07548	0.0023	0.00000	0.00000	
	Xe135	106	0.04403	0	0.04403	0.0014	0.00058	0.00001	
	Xe137	0	0.0303	0	0.0303	0.0009	0.00000	0.00000	
	Xe138	0	0.199	0	0.199	0.0062	0.00000	0.00000	• .
	I131Org	32776	0.06734	32893	11.5799	11.515	0.07048	0.03135	
	I132Org	17466	0.4144	381.1	0.54779	0.1462	0.00178	0.00021	
	I133Org	2420	0.10878	5846	2.15488	2.0495	0.00097	0.00041	
	I134Org	0	0.481	131.35	0.52697	0.0609	0.00000	0.00000	
	I135Org	2.3	0.3069	1228.4	0.73684	0.4395	0.00000	0.00000	
	I131Elem	32776	0.06734	32893	11.5799	11.515	0.16461	0.07323	
	I132Elem	17466	0.4144	381.1	0.54779	0.1462	0.00415	0.00050	
	I133Elem	2420	0.10878	5846	2.15488	2.0495	0.00226	0.00096	
	I134Elem	0	0.481	131.35	0.52697	0.0609	0.00000	0.00000	
	I135Elem	2.3	0.3069	1228.4	0.73684	0.4395	0.00000	0.00000	
						Total TEDE=	0.27413	0.10708	

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Table 6. Doses after a Fuel Handling Accident (20% ground level release, 96-hour decay).

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	VY FHA	(96 hrs)	EAB	CR					
	Ground Le	vel X/Qs =	4.57E-04	1.24E03	sec/m3 (2	0% release at gro	ound level)		
	Power =	1950	MW(t)						
	CR Vol =	41533.8	ft3						
	Rel Fract =	2.85E-04							
	Peaking =	1.65	WB	CEDE	TEDE	CR	EAB	CR	
	Nuclide	Ci/MW	DCF	DCF	DCF	DCF	TEDE	TEDE	
and the second second second second	Kr83m	A State	1:49E-05		- 1.5E=05-	5E-07-	0.00000	-0:00000	
	Kr85m	0	0.0277	··· 0	0.0277	0.0009	0.00000	0.00000	
	Kr85	1009	4.40E-04	0	0.00044	1E-05	0.00019	0.00002	
	Kr87	0	0.1524	0	0.1524	0.0047	0.00000	0.00000	
	Kr88	0	0.3774	0	0.3774	0.0117	0.00000	0.00000	
	Kr89	0	0.323	0	0.323	0.01	0.00000	0.00000	
	Xe131m	338	0.00149	0	0.00149	5E-05	0.00021	0.00002	
	Xe133m	766	0.00507	0.	0.00507	0.0002	0.00163	0.00014	
	Xe133	40184	0.00577	0	0.00577	0.0002	0.09720	0.00818	
	Xe135m	0	0.07548	0	0.07548	0.0023	0.00000	0.00000	
	Xe135	106	0.04403	0	0.04403	0.0014	0.00196	0.00016	
	Xe137	0	0.0303	0	0.0303	0.0009	0.00000	0.00000	
	Xe138		0.199	0	0.199	0.0062	0.00000	0.00000	
	I131Org	32776	0.06734	32893	11.5799	11.515	0.23858	0.64369	
	I132Org	17466	0.4144	381.1	0.54779	0.1462	0.00601	0.00436	
	I133Org	2420	0.10878	5846	2.15488	2.0495	0.00328	0.00846	
	I134Org	0	0.481	131.35	0.52697	0.0609	0.00000	0.00000	
	I135Org	2.3	0.3069	1228.4	0.73684	0.4395	0.00000	0.00000	
	I131Elem	32776	0.06734	32893	11.5799	11.515	0.55723	1.50345	
	I132Elem	17466	0.4144	381.1	0.54779	0.1462	0.01405	0.01018	
	I133Elem	2420	0.10878	5846	2.15488	2.0495	0.00766	0.01976	
	I134Elem	0	0.481	131.35	0.52697	0.0609	0.00000	0.00000	
	I135Elem	2.3	0.3069	1228.4	0.73684	0.4395	0.00000	0.00000	
						Total TEDE=	0.92799	2.19841	

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Reference 1 states that the control room dose limit is 5 rem TEDE and that the offsite dose limit for the FHA is 6.3 rem TEDE. The results from Tables 3 through 6 can be compared to these limits. Note that there is considerable margin for the control room doses and for the EAB and LPZ doses.

#### Conclusions

The FHA control room and offsite doses are well within their Reference 1 limits if the ground level release is limited. Even if 20% of the release is at ground level, the limits are not exceeded, with either 24 or 96 hours of decay prior to the start of the accident.

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#### Appendix A - Check Calculation Using the STARDOSE Computer Code

This appendix provides a check calculation for the FHA analysis for VY using the STARDOSE computer code (Reference A-1). The analysis makes use of the same dose conversion factors (DCFs) as used in the dose calculation spreadsheets provided in the main body of the calculation.

The release is assumed to occur on the refueling floor, and the activity release to the environment is designed to be complete within two hours. For cases involving ground-level release, the assumption is made that a fractional release rate necessary to release 99% of the activity to the environment in two hours (i.e., 0.0384 per minute) occurs for six minutes at the start of the accident. Beyond that time (i.e., for the next 0.5 hours, for the next 0.5 hours after that, and finally for the last 0.9 hours), the elevated release X/Qs are used in decending order of magnitude for both the EAB dose and the CR dose. Fractional release rates are then varied to obtain a average absolute release rate of 0.5 per hour for the next hour (i.e., 0.0125 per minute for the first half of that one hour and then 0.02 per minute for the last half of that one hour) and finally to release the remaining 30% of the activity withing the last 0.9 hours (0.063 per minute). By so doing, 20% of the activity is released within the first six minutes (ground-level release), 25% within the next half-hour, another 25% within the half-hour after that, and then finally, 29% during the remaining 0.9 hours (leaving 1% not released). This is a conservative interpretation of the Reference A-2 requirement that the release be complete within two hours, and it is consistent with the X/Q averaging done in the main body of the calculation.

For cases not involving ground-level release, the intent is to release 25% within the first halfhour, 25% within the next half-hour, and 49% within the final one hour (leaving 1% not released). The corresponding fractional release rates are 0.0096 per minute, 0.01335 per minute, and 0.065 per minute, respectively.

The control room dose calculation is continued for a minimum of 22 hours after the end of the release. With a fresh air intake rate of 3700 cfm and a control room volume of 4.15E4  $ft^3$  (Reference A-3), the room turnover rate is 0.09 per minute which means nearly 120 volume changes in 22 hours. Continuing the dose calculation for 22 hours the end of the release ensures that the control room dose is fully accumulated.

#### **STARDOSE Calculation**

The model in STARDOSE consists of three control volumes. The first control volume is the gap (nominally 100  $ft^3$ ), the second is the reactor building (RB) refueling floor (also nominally 100  $ft^3$ ), and the third is the control room (4.15E4  $ft^3$  per Reference A-3). Note that the nominal 100  $ft^3$  volumes are used to conveniently calculate exchange rates.

The core power is assumed to be 1950 MWt as in the main body of the calculation. The gap activity of noble gas, iodine (set at 100% organic because the iodine form is not relevant without filters in the control room), and tellurium (as an iodine precursor) is added from the core to the gap over the first 0.01 hours of the analysis. It is added at 8.25 core inventories per hour so that the release is 8.25%. This 8.25% is to account for a "base" gap fraction of 5% (Reference A-2)

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and a peaking factor of 1.65 (Reference A-3). Note, however, that because the gap activities for Kr-85 and I-131 are respectively 10% and 8% per Reference A-2, the inventories of these two radionuclides in the attached STARDOSE LIBFILE1.TXT file were increased by a factor of 2 and 8/5, respectively, as compared to the activities given in Reference A-3.

Once the activity has been established in the gap, it is allowed to decay until 23.9833 or 95.9833 hours, as appropriate. It is then released to the RB at 0.571 cfm (0.571% per minute) for 0.0167 hours (one minute) so that the assumed 0.571% of the assemblies are represented as in the main body of the calculation. A filter efficiency of 0.995 is used to account for the water DF of 200 applied to the iodine. Since tellurium was also released to provide additional iodine during the decay period, a filter efficiency of 0.99999 is used to prevent its subsequent release to the RB (although a small amount would be present). No other particulates are assumed to be released in the STARDOSE model because (per Reference A-2), the scrubbing DF is assumed to be infinite for that activity.

All of this activity is in the RB by 24 hours or 96 hours, as appropriate. At 24/96 hours, the release to the environment is assumed to begin at the rates specifed above. Note that no credit for SGTS filtration is taken.

The X/Qs are from Reference A-3 but displaced by 24 or 96 hours, as appropriate. The breathing rate of  $3.5E-4 \text{ m}^3$ /sec is also taken from Reference A-3.

As for the control room, a fresh air intake rate of 3700 cfm (Reference A-3) and an occupancy factor of unity are used.

Four cases are run (as in the main body of the calculation): 0% and 20% ground-level release and 24- and 96-hour decay times.

The LIBFILE1.TXT file of Attachment A-1, common to all AST STARDOSE runs, contains the radionuclide input data. The core inventories listed in Column 5 are from Reference A-3 (with the Kr-85 and I-131 inventories increased by a factor of 2 and 8/5, as described above). The Dose Conversion Factors (Column 8 for whole body and Column 12 for CEDE) are the same as in the main body of the calculation. Decay constants (per second) come from Reference A-4.

Input files are provided as Attachments A-2 through A-5.

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Output file excerpts are provided in the Results section below. The core inventory in the gap at the start of the gap release is shown in the following table for comparison to the values in the main body of the calculation. Note that the agreement is good except for Kr83m and, to a lesser extent, for Xe131m and Xe133m. This is because the daughter ingrowth formulation in STARDOSE is less sophisticated than for the RADDECAY code used in the main body of the calculation. However, the important daughter ingrowth contributions are properly represented in STARDOSE, and the three dose contributors just mentioned have very little impact on the overall dose calculation.

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## Table A-1

## Gap Inventory Comparison (Ci/MWt at Stated Time, No Peaking, Multipliers for Kr85 and I131 Included)

	Nuclide	24 Hours*	24 Hours**	96 Hours*	96 Hours**	
	Kr83m	15.6	1	negligible	0	
	Kr85m	239	219	negligible	0	
	K185	1010	1007	1009	1007	
	Kr87	0.038	0.04	negligible	0	
	Kr88	72.3	72	negligible	0	
and the second	· · · · Kr89 · · · ·	negligible		negligible "		 ويعمون بالمعرف مرابده
	I131	42105	42207	32776	32883	
	Xe131m	327	300	338	252	
	I132	33065	32945	17466	17218	
	I133	26656	26107	2420	2393	
	Xe133m	1594	1299	766	527	
	Xe133	55528	55571	40184	40466	
	I134	negligible	0	negligible	0	
	1135	4351	4563	2.3	3	
	Xe135m	negligible	· 0	negligible	0	
	Xe135	15285	15540	106	116	
	Xe137	negligible	0	negligible	0	
	Xe138	negligible	0	negligible	0	
	*Main body **STARDO	of calculation SE	<b></b> .	_		-

#### Results

# Excerpt from STARDOSE output corresponding to Attachment 2 INPUT.DAT (0% ground-level release, 24-hour decay):

#### Control\_Room

	thyroid	wbody	skin	CEDE
Total dose:	4.90E+000	1.92E-003	8.89E-002	1.51E-001
Noble gas	0.00E+000	1.75E-003	8.69E-002	0.00E+000
Org iodine	4.90E+000	1.63E-004	1.98E-003	1.51E-001

environment

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EAB dose:	thyroid 1.05E+001	wbody 1.31E-001	skin 1.89E-001	CEDE 3.24E-001	
Wahle and a	thyrd_eab	wbody_eab	skin_eab	CEDE_eab	
Org iodine	0.00E+000 1.05E+001	1.20E-001	1.85E-001 4.09E-003	0.00E+000 3.24E-001	

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# Excerpt from STARDOSE output corresponding to Attachment 3 INPUT.DAT (20% ground-level release, 24-hour decay):

Control\_Room

	thyroid	wbody	skin	CEDE
Total dose:	1.03E+002	4.08E-002	1.89E+000	3.18E+000
Noble gas	0.00E+000	3.73E-002	1.84E+000	0.00E+000
Org iodine	1.03E+002	3.57E-003	4.27E-002	3.18E+000

#### environment

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	· · · · · · · ·	thyroid T	wbody	skin	CEDE
EAB	dose:	3.70E+001	4.73E-001	6.77E-001	1.14E+000
		thyrd eab	wbody eab	skin eab	CEDE eab

Noble gas	0.00E+000	4.31E-001	6.61E-001	0.00E+000
Org iodine	3.70E+001	4.15E-002	1.54E-002	1.14E+000

# Excerpt from STARDOSE output corresponding to Attachment 4 INPUT.DAT (0% ground-level release, 96-hour decay):

#### Control\_Room

	thyroid	wbody	skin	CEDE
Total dose:	3.50E+000	4.91E-004	2.75E-002	1.07E-001
Noble gas	0.00E+000	4.16E-004	2.67E-002	0.00E+000
Org iodine	3.50E+000	7.52E-005	7.94E-004	1.07E-001

environment

EAB dose:	thyroid 7.52E+000	wbody 3.38E-002	skin 5.91E-002	CEDB 2.30E-001
	thyrd_eab	wbody_eab	skin_eab	CEDE_eab
Noble gas	0.00E+000	2.88E-002	5.75E-002	0.00 <u>E</u> +000
Org iodine	7.52E+000	4.94E-003	1.63E-003	2.30E-001

# Excerpt from STARDOSE output corresponding to Attachment 5 INPUT.DAT (20% ground-level release, 96-hour decay):

Control\_Room

	thyroid	wbody	skin	CEDE
Total dose:	7.36E+001	1.04E-002	5.80E-001	2.25E+000
Noble gas	0.00E+000	8.75E-003	5.63E-001	0.00E+000
Org iodine	7.36E+001	1.64E-003	1.73E-002	2.25E+000

#### environment

EAB dose:	thyroid 2.64E+001	wbody 1.20E-001	skin 2.08E-001	CEDE 8.05E-001
	thyrd eab	wbody eab	skin_eab	CEDE_eab
Noble gas	0.00E+000	1.01E-001	2.02E-001	0.00E+000
Org iodine	2.64E+001	1.92E-002	6.22E-003	8.05E-001

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Table A-2 summarizes offsite and control room dose results for all four cases:

Case	24 hour or	0% or 20%	EABJEDE	EAB TEDE	CR TEDEN	CR TEDE
	96 hour	ground-level	(Main Body)	(STARDOSE)	(Main Body)	(STARDOSE)
	decay?	release	(UHENE)			
A	24	0	0.472	0.455	0.153	0.153
B	24	20	1.598	1.613	8333343111	3.22
. C.		0 - 5.0	0.274	0.264	0 108	0.108
D	96	20	0.928	0.925	2.20	2.26

Table A-2 – Doses for the FHA Analysis (in rem)

#### Conclusions

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The dose agreement for all cases is excellent. The STARDOSE runs confirm the results from the main body of the calculation.

Reference A-2 states that the control room dose limit is 5 rem TEDE and that the offsite dose limit for the FHA is 6.3 rem TEDE. The results from Table A-2 can be compared to these limits.

For the limiting case of only 24 hour's decay and 20% ground-level release, the FHA control room dose represents about 63% of the 5-rem limit. The EAB dose has almost a factor four margin.

#### References

A-1. "STARDOSE Model Report", Polestar Applied Technology, Inc., PSATCI09.03, January 1997

A-2. "Alternative Radiological Source Terms for Evaluating Design Basis Accidents at Nuclear Power Reactors", US NRC Regulatory Guide 1.183, Revision 0, July 2000

A-3. PSAT 3019CF.QA.03, "Design Data Base for Application of the Revised DBA Source Term to Vermont Yankee", Revision 0

A-4. NUREG/CR-5106 (Manual for TACT5 – Version SAIC 9/23/87), File MLWRICRP.30

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PSA. JO19CF.	.QA.05	<b>;</b> ,•				Attac	ent	A-1 – L	BFILE	1.TXT					
n isotopes :	20 niso	tope ar	oups	11						Kev U		24 24 3			
			<u>-</u>												
Kr83m N_Gas I 0	NONE NONE 0 0	4.248+	03	1.048-	04	0	1.49E-	05	0	0	0	Ő	0	0	0
Kr85m N_Gas 1 0	NONE NONE 0 0	9.71B+	03	4.39E-	05	0	0.0277	7	0	0	0.05	0	0.22	0	0
Kr85 N_Gas I 0 (	NONE NONE 0 0	1.01E+	03	2.04E-	09	0	4.40E-	•04	0	0	0.05	0	0.22	0	0
Kr87 N_Gas J	NONE NONE	1.94E+	04	1.528-	04	0	0.1524	ł	0	0	0.34	0	1.48	0	0
Kr88 N_Gas 1	NONE NONE	2.75B+	04	6.88E-	05	0	0.3774	ŧ	0	0	0.08	0	0.35	0	0
Kr89 N_Gas I	NONE NONE	3.46E+	04	3.63E-	03	0	0.323	0	0	0.35	0	1.52	0	0	0
Xel31m 1	N_Gas NONE	NONE	3.18E+	02	6.68E·	-07	0	0.0014	9	0	0	0.02	0	0.04	0
Xe133m 1	N_Gas NONE	NONE	1.76E+	03	3.49E	-06	0	0.0050	7	0	0	0.03	0	0.13	0
Xe133 N_Gas	11330rg	NONE	5.78E+	04	1.52B-	-06	0	0.0057	7	0	0	0.01	0	0.04	0
Xe135m 1	N_Gas NONE	NONE	1.14E+	04	7.40E	-04	0	0.0754	8	0	0	Q.02	0	0.09	0
Xe135 N_Gas	11350rg	NONE	2.33E+	04	2.09E	-05	0	0.0440	3	<b>o</b> .	0	0.06	0	0.26	0
Xe137 N_Gas I	NONE NONE	5.07E+	04	2.96B-	03	0	0.0303	Ì	0	0	0.46	Ø	2	0.	0
Xe138 N_Gas I	NONE NONE	5.05E+	04	6.80E-	04	0	0.199	0	0	0.15	0	0.65	0	0	0
I1310rg (	Org_I Tel31	.m	NONE	4.57B+	04	9.96E-	07	108040	0	0.0673	4	0	0	0.03	32893
1132Org	Org_I Tel32	NONE	4.05E+	04	8.27B	-05	6438	0.4144	ł	0	0	Q.11	381.1	0.48	0
11330rg (	Org_I NONE	Xe133	5.79B+	04	9.228	-06	179820	)	0.1087	78	0	Ø	0.09	5846	0.39
I1340rg (	Org_I NONE	NONE	6.43E+	04	2.23E	-04	1065.6	;	0.481	0	0	0.14	131.35	i	0.61
I1350rg (	Org_I NONE	V Xe135	5.39B+	04	2.86B	-05	31302	0.3069	)	0	0	0.08	1228.4	Ł	0.35
0 ( Tel31m '	U O Tegro None	0 71310r	u a	4.31R-	.03	6.428-	-06	0	0	0	0	,` n'	0	•	0
0	0 0	,0	7			41-46H)-		~	-	~	5		5	J	v
Tel32 TeGrp 1 0	NONE I1320 0 0	rg	3.978+	04	2.51E	-06	0	0	0	0	0	0	0	0	0

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Attachment A-2 – INPUT.DAT, 24 hr, 0% PSAT 3019CF.QA.05 Rev 0 edit time 0.0 0.01 23.9833 24.0 48.0 end\_edit\_time participating\_isotopes Kr83m Kr85m Kr85 Xel31m Xel33m Xel33 Kr87 Kr88 Kr89 Xe135m Xe135 Xe137 Xe138 11350rg I1320rg I1330rg I1340rg I1310rg **Tel31**m Te132 end\_participating\_isotopes core thermal power 1950 elemental fodine\_frac a set to a organize a contraction and the set of the set of the set of the set of the set 1.0 organic\_iodine\_frac 0.0 particulate\_iodine\_frac release\_frac to\_control\_volume GAP TimeN\_GasI\_GrpCsGrpTeGrpBaGrpNMtlsCeGrpLaGrpSrGrp0.018.258.2508.2500000 0 0 0 0 0 48 0 0 0 0 end\_to\_control\_volume end\_release\_frac end\_core control\_volume OBJ\_CV obj\_type name GAP air\_volume 100 water\_volume ۵ surface\_area has recirc filter false end\_control\_volume control\_volume OBJ CV obj\_type name RB air\_volume 100 water\_volume 0 surface\_area 0 has\_recirc\_filter false end\_control\_volume control\_volume OBJ\_CR obj\_type name Control Room air\_volume 4.15e+004 water\_volume . . . . ..... . . . --surface\_area 0 has\_recirc\_filter false breathing\_rate Time (hr) Value (cms) 48 0.00035 end\_breathing\_rate occupancy\_factor Time (hr) Value (frac) 48 1 end\_occupancy\_factor end\_control volume

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#### Attachment A-2 – INPUT.DAT, 24 hr, 0% Rev 0

AIR JUNCTION junction\_type AIR SPACE downstream\_location CORE upstream GAP downstream has\_filter false flow\_rate Time (hr) Value (cfm) 48 1 end flow rate end\_junction junction AIR\_JUNCTION junction\_type 2 ... 2.1.2.2.2 ۰. downstream\_location GAP upstream downstream RB has filter true flow\_rate Time (hr) Value (cfm) 23.9833 0 0.571 24 48 0 end\_flow\_rate filter\_efficiency ElemIodine OrgIodine PartIodine Solubles Insolubles Time NobleGas 48 0 0 0.995 0 Ω 0.99999 end\_filter\_efficiency frac\_4\_daughter\_resusp Time NobleGas ElemIodine OrgIodine PartIodine Solubles Insolubles 0 0 0 0 0 48 0 end\_frac\_4\_daughter\_resusp reevolution\_rate Insolubles ElemIodine OrgIodine PartIodine Solubles Time NobleGas 0 0 0 Ο. 0 0 48 end reevolution\_rate end\_junction junction junction\_type AIR JUNCTION downstream\_location AIR SPACE upstream RB downstream environment has\_filter false flow\_rate Time (hr) Value (cfm) 24 0 24.5 0.96 a a sate a 25 . 1.335 - . . 26 6.5 48 0 end\_flow\_rate X\_over\_Q\_4\_site\_boundary Time (hr) Value (s/m\*3) 24 0 24.5 2.03e-4 25 1.54e-4 26 9.17e-5 0.0 48 end\_X\_over\_Q\_4\_site\_boundary X over Q 4 low population zone Time (hr) Value (s/m\*3)

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48 0.0 end\_X\_over\_Q\_4\_low\_population\_zone X\_over\_Q\_4\_ctrl\_room Time (hr) Value (s/m\*3) 24 0.0 24.5 2.39e-4 25 1.05e-6 26 8.70e-7 48 0.0 end\_X\_over\_Q\_4\_ctrl\_room end\_junction junction junction\_type AIR JUNCTION downstream\_location AIR SPACE upstream environment downstream Control Room has\_filter false flow\_rate Time (hr) Value (cfm) 48 3700 end\_flow\_rate end\_junction junction junction\_type AIR JUNCTION downstream location AIR SPACE upstream Control\_Room downstream environment has\_filter false flow\_rate ·-- . Time (hr) Value (cfm) 48 3700 end flow rate X\_over\_Q\_4\_ctrl\_room Time (hr) Value (s/m\*3) 48 0 end\_X\_over\_Q\_4\_ctrl\_room X\_over\_Q\_4\_site\_boundary Time (hr) Value (s/m\*3) 48 0 end\_X\_over\_Q\_4\_site\_boundary X\_over\_Q\_4\_low\_population\_zone Time (hr) Value (s/m\*3)48 0 end\_X\_over\_Q\_4\_low\_population\_zone end\_junction environment breathing\_rate\_sb Time (hr) Value (cms) 24 0.0 26 0.00035 48 0.0 end\_breathing\_rate\_sb breathing\_rate\_lpz Time (hr) Value (cms) 48 0.0 end\_breathing\_rate\_lpz end\_environment

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### Attachment A-3 – INPUT.DAT, 24 hr, 20% Rev 0

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#### Attachment A-4 – INPUT.DAT, 96 hr, 0% Rev 0

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#### Attachment A-5 – INPUT.DAT, 96 hr, 20% Rev 0

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Attachment A-5 – INPUT.DAT, 96 hr, 20% Rev 0

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#### Attachment A-4 – INPUT.DAT, 96 hr, 0% Rev 0

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#### Attachment A-4 – INPUT.DAT, 96 hr, 0% Rev 0

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#### Attachment A-5 – INPUT.DAT, 96 hr, 20% Rev 0

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#### Attachment A-5 – INPUT.DAT, 96 hr, 20% Rev 0

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Attachment A-5 - INPUT.DAT, 96 hr, 20% PSAT 3019CF.QA.05 Rev 0 edit time  $0.0 \ \overline{0}.01 \ 95.9833 \ 96.0 \ 120.0$ end\_edit\_time participating\_isotopes Kr83m Kr85m Kr85 Xel31m Xel33m Xel33 Kr87 Kr88 Kr89 Xe137 Xe138 Xe135m Xe135 I1310rg I1320rg I1330rg I1340rg I1350rg **Te131m** Te132 end\_participating\_isotopes core 1950 thermal\_power sing groups elemental\_iodine\_frac a ser and a second and a second a second a second a service and a service organic iodine frac 1.0 particulate\_iodine\_frac 0.0 release\_frac to\_control\_volume GAP Time N\_Gas I\_Grp CsGrp TeGrp BaGrp NMtls CeGrp LaGrp SrGrp 0.01 8.25 8.25 0 8.25 0 0 0 0 0 0 120 0 0 0 0 0 0 0 0 end\_to\_control\_volume end\_release\_frac end\_core control volume OBJ CV obj\_type GAP name air\_volume 100 water\_volume 0 surface\_area 0 has\_recirc\_filter false end\_control\_volume control volume OBJ\_CV obj\_type RB name air\_volume 100 water\_volume 0 surface\_area has\_recirc\_filter 0 false end\_control\_volume control\_volume obj\_type OBJ\_CR Control\_Room name air\_volume 4.15e+004water volume 0 surface\_area Ò has\_recirc\_filter false breathing\_rate Time (hr) Value (cms) 120 0.00035 end\_breathing rate occupancy\_factor Time (hr) Value (frac) 120 1 end\_occupancy\_factor end control volume junction

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Attachment A-5 - INPUT.DAT, 96 hr, 20% Rev 0

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Page B1 of 1 Rev 0

#### Appendix B - Minimum Decay Time Giving Acceptable Control Room Dose Results without Credit for Containment

From the main body of the calculation, one may note that for 24 hours of decay, about 88% of the control room dose is from I131 (Tables 3 and 4). With 96 hours of decay, it is 98% (Tables 5 and 6). At even later decay times (decay times that will give acceptable control room doses without any credit for containment), one may assume that the control room dose will be due entirely to I131.

At 96 hours, the CR dose is 2.2 rem with 20% ground-level release (Table 6). Nearly all of this 2.2 rem (except for less than 0.1 rem) is due to that 20% ground-level contribution. Therefore, the dose for 100% ground-level release would be about 11 rem (very slightly conservative) at 96 hours. To have the control room dose be less than the 5 rem control room dose limit at some later time, the I131 release would have to decrease to 5/11 (i.e., to 45%) of its inventory at 4 days. With a decay constant of about 1E-6 per second, this would require about 8E5 seconds or just over 9 days. Therefore, with a measure of conservatism, it can be confidently asserted that no containment would be needed after 14 days from the time of shutdown to have the control room dose be less than the 5 rem TEDE limit for the FHA.

QAP 6.1 Revision 0 4/28/95 Attachment 4 1

# Form QA-007 Document Transmittal/Receipt

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Form QA-023

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