1	Appendix G
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5	NRC Staff Evaluation of Severe
6	Accident Mitigation Alternatives
7	for the R.E. Ginna Nuclear Power Plant
8	in Support of License Renewal Application

1	Appendix G
2	
3	NRC Staff Evaluation of Severe
4	Accident Mitigation Alternatives
5	for the R.E. Ginna Nuclear Power Plant
6	in Support of License Renewal Application
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9	G.1 Introduction
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11	Rochester Gas and Electric (RG&E) submitted an assessment of severe accident mitigation
12	alternatives (SAMAs) for the R.E. Ginna (Ginna) Nuclear Power Plant as part of the Ginna
13	Environmental Report (ER) (RG&E 2002). This assessment was based on the most recent
14	Ginna probabilistic safety assessment (PSA) available at that time, a plant-specific offsite
15	consequence analysis performed using the MELCOR Accident Consequence Code System 2
16	(MACCS2) code, and insights from the Ginna Individual Plant Examination for External Events
17	(IPEEE) (RG&E 1997a, 1998a, 1998b, 1998c). In identifying and evaluating potential SAMAs,
18	RG&E considered SAMA analyses performed for other operating plants that have submitted
19	license renewal applications, as well as industry and U.S. Nuclear Regulatory Commission
20	(NRC) documents that discuss potential plant improvements, such as NUREG-1560 (NRC
21	1997a) and NUREG-1742 (NRC 2002a). RG&E also identified SAMAs that were dominant
22	contributors to core damage frequency (CDF) and large early release frequency (LERF) based

sed on the plant-specific PSA. RG&E assessed the costs and benefits associated with each of the 23 potential SAMAs and concluded that two of the candidate SAMAs evaluated are potentially cost 24 beneficial for Ginna. 25

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27 Based on a review of the SAMA assessment, the NRC issued a request for additional information (RAI) to RG&E by letter dated December 26, 2002 (NRC 2002a). Key questions 28 29 concerned (1) dominant risk contributors at Ginna and the SAMAs that address these contributors, (2) the impact on dose consequences if all release categories were considered 30 rather than just large early release categories, (3) the potential impact of uncertainties on the 31 study results, and (4) detailed information on several specific candidate SAMAs. RG&E 32 submitted additional information on January 31, 2003, and February 28, 2003, in response to 33 the RAI (RG&E 2003a, 2003b). The February 28, 2003, response included a completely 34 revised SAMA analysis (Section 4.14 and Appendix E of the ER) based on an updated version 35 of the PSA. In these responses, RG&E provided tables containing the results of importance 36 analyses, revised results based on the removal of scrubbing of fission product releases, and an 37 assessment of the impacts of uncertainties. RG&E's responses addressed the staff's concerns 38 and reaffirmed that only two SAMAs would be cost beneficial. 39

- 40
- 41 An assessment of SAMAs for Ginna is presented as follows.

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G.2 Estimate of Risk for Ginna

RG&E's estimates of offsite risk at Ginna are summarized in Section G.2.1. The summary is followed by the staff's review of RG&E's risk estimates in Section G.2.2.

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G.2.1 RG&E's Risk Estimates

Two distinct analyses are combined to form the basis for the risk estimates used in the SAMA 8 analysis: (1) the Ginna Level 1 and 2 PSA model, which is an updated version of the Individual 9 10 Plant Examination (IPE) (RG&E 1994, 1997b, 1997c), and (2) a supplemental analysis of offsite consequences and economic impacts (essentially a Level 3 PSA model) developed specifically 11 12 for the SAMA analysis. The Level 1 and 2 PSA used as the basis for the SAMA analysis is the most recent PSA model of record, and is referred to as Version 4.2. The scope of the Ginna 13 14 PSA does not include full consideration of seismic events. However, the dominant fire and internal flooding sequences are included in the PSA. 15

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The baseline CDF for the purpose of the SAMA evaluation is approximately 4×10^{-5} per year. 17

The CDF is based on the risk assessment for internally initiated events at power and at 18

shutdown, and the dominant external events, specifically, fire and internal flooding at power. 19

20 RG&E did not include the contribution of risk from seismic events within the Ginna risk

21 estimates. It is RG&E's position that due to the recent and extensive evaluations and

modifications performed as part of IPEEE and Seismic Qualification Utility Group (SQUG) 22

23 activities, seismic events have been adequately addressed and need not be explicitly treated in the SAMA analysis (additional discussion provided in Section G.2.2). 24

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The breakdown of CDF by initiating event/accident type is provided in Table G-1. Internal 26 27 events at power contribute about 33 percent of the total CDF and are composed of (1) steam generator tube ruptures (15 percent of the total), (2) loss of coolant accidents (LOCAs) less 28 than 5 cm (2 in.) (6 percent of the total), (3) station blackout (SBO) (5 percent of the total), 29 (4) LOCAs greater than 5 cm (2 in.) (2 percent of the total), and (5) interfacing system LOCAs 30

and anticipated transient without scram (ATWS) (each about 1 percent of the total) (RG&E 31

2003b). Shutdown events represent about 17 percent of the total CDF (RG&E 2003b). 32 External event initiators represent about 50 percent of the total CDF and are composed of fire 33

initiators (28 percent of the total CDF) and floods (22 percent of the total CDF) (RG&E 2003b). 34

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36 The Level 2 PSA model has also been updated since the IPE. As described in the RAI

responses (RG&E 2003b), results from the previous detailed Level 2 analysis were converted to 37 the simplified LERF methodology described in NUREG/CR-6595 (NRC 1999a). In the updated 38

1	Table G-1.	R.E. Ginna N	Nuclear Power	Plant Core	Damage Fre	equency (Revisio	on 4.2 of PSA)
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Contributor	CDF (per year)	Percent of Total CDF
Internal Events – At Power		
Transients	1.0 x 10 ⁻⁶	3
Station Blackout (SBO)	2.1 x 10 ⁻⁶	5
Anticipated transient without scram (ATWS)	2.0 x 10 ⁻⁷	1
Steam generator tube rupture (SGTR)	6.0 x 10 ⁻⁶	15
Loss of coolant accidents (LOCAs) <2 inches	2.6 x 10⁻ ⁶	6
LOCAs >2 inches	7.0 x 10 ⁻⁷	2
Interfacing system LOCA (ISLOCA)	2.5 x 10 ⁻⁷	1
Internal Events – Shutdown	6.8 x 10⁻ ⁶	17
CDF from internal events	2.0 x 10⁻⁵	50
External Events		
Fire	1.1 x 10 ⁻⁵	28
Flood	8.8 x 10 ⁻⁶	22
CDF from external events	2.0 x 10 ⁻⁵	50
Total CDF	4.0 x 10 ⁻⁵	100

analysis, the 25 source term categories (STCs) used in the IPE were rebinned into 11 release
 category bins, each of which was assigned a representative source term based on the original
 MAAP analyses performed for the IPE. The conditional probabilities and release characteristics
 associated with each release category were provided in response to an RAI (RG&E 2003b). An
 explanation of the binning process and a mapping of the STCs to release category bins was
 also provided (RG&E 2003c).

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The offsite consequences and economic impact analyses use the MELCOR MACCS2 code, Version 1.12, to determine the offsite risk impacts on the surrounding environment and public. Inputs for this analysis include plant-specific and site-specific input values for core radionuclide inventory, source term and release characteristics, site meteorological data, projected population distribution (within a 80-km [50-mi] radius) for the year 2030, emergency response evacuation modeling, and economic data.

In the ER, RG&E estimated the dose to the population within 80 km (50 mi) of the Ginna site to
 be approximately 0.163 person-sievert (Sv) (16.300 person-rem) per year (RG&E 2003b). The
 breakdown of the total population dose by containment release mode is summarized in

Table G-2. Bypass events (steam generator tube rupture [SGTR] and interfacing system loss-of-coolant accident [ISLOCA]) and late containment failures dominate the population dose risk at Ginna.

Table G-2. Breakdown of Population Dose by Containment Release Mode

Containment Release Mode	Person-Sv Per Year	Person-Rem Per Year	Percent Contribution
SGTR ^(a)	0.063	6.3	39
ISLOCAs	0.044	4.4	27
Early containment failure	0.020	2.0	12
Late containment failure ^(b)	0.030	3.0	19
No containment failure	0.006	0.6	3
Total	0.163	16.300	100
(a) Includes thermally induced SGTR.			
(b) Includes contribution from shutdown events.			

G.2.2 Staff's Review of RG&E Risk Estimates

RG&E's determination of offsite risk at Ginna is based on the following three major elements of analysis:

- the Level 1 and 2 risk models that form the bases for the 1994 IPE and 1997 IPEEE submittals (RG&E 1994, 1997a, 1997b, 1997c, 1998a, 1998b, 1998c)
- the major modifications to the IPE model that have been incorporated in the Ginna PSA
- the MACCS2 analyses performed to translate fission product release frequencies from the level 2 PSA model into offsite consequence measures.
- Each of these analyses was reviewed to determine the acceptability of RG&E's risk estimates for the SAMA analysis, as summarized below.

The staff's review of the Ginna IPE is described in an NRC report dated September 16, 1997 (NRC 1997b). In that review, the staff evaluated the methodology, models, data, and assumptions used to estimate the CDF and characterize containment performance and fission product releases. The staff concluded that RG&E's analyses met the intent of Generic Letter 88-20 (NRC 1988); that is, the IPE was of adequate quality to be used to look for design or operational vulnerabilities. The staff's review primarily focused on the licensee's ability to examine Ginna for severe accident vulnerabilities and not specifically on the detailed findings or

quantification estimates. Overall, the staff believed that the Ginna IPE was of adequate quality
to be used as a tool in searching for areas with high potential for risk reduction and to assess
such risk reductions, especially when the risk models are used in conjunction with insights,
such as those from risk importance, sensitivity, and uncertainty analyses.

- In the IPE, RG&E identified five vulnerabilities as follows:
- 1. <u>Relays for steam generator low-level actuation of auxiliary feedwater (AFW)</u>. The relays for this signal must be energized to actuate the AFW; however, they are currently powered by a non-safety bus that is unavailable upon a loss of offsite power.
- 2. <u>ISLOCA through penetration 111</u>. A LOCA outside containment through penetration 111 fails all residual heat removal (RHR) due to the low elevation of the RHR pump pits.
- 3. <u>Standby AFW system out-of-service activities</u>. Currently, both trains of this system can be taken out of service for up to 7 days; however, it is credited for providing steam generator cooling water for certain LOCAs outside containment.
- 4. <u>Charging pump suction</u>. Upon loss of dc control power or instrument air, the charging pump suction line fails to open the volume control tank, which may be empty because its supply source will have been eliminated as a result of the loss of power or air.
- 5. <u>Intermediate building ventilation</u>. The preferred AFW pumps are located in the basement of
 the intermediate building, which is ventilated via either building exhaust fans or natural
 circulation from a fire door opening; however, only one train of the exhaust fans is powered
 by the emergency diesel generators.

In an RAI, the staff questioned the current status of these vulnerabilities and whether any 28 unresolved vulnerabilities were included in the SAMA evaluation. In response to the RAI, 29 RG&E stated that items 1 and 3 had been resolved through plant modifications. Items 2 and 4, 30 although considered by RG&E to be adequately addressed based on further review under the 31 IPE program, are covered by SAMAs 3, 4, and 5. RG&E indicated that item 5 was originally 32 identified as a result of overly conservative assumptions in the PSA model, and based on a 33 34 more realistic assessment, it was reduced to a no-action status (RG&E 2003a). The staff inquired further about the conservative assumptions contained in the model. During a 35 36 telephone conversation, RG&E explained that there are two methods of accomplishing ventilation within the intermediate building: (1) natural circulation via Fire Door F36 and (2) 37 38 forced ventilation by the intermediate building exhaust fans (NRC 2003). Because only one train of the exhaust fans are diesel generator-backed, the three AFW pumps rely on the 39 passive cooling in an SBO event in which the diesel generator is inoperable. A reanalysis of the 40

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building's ventilation determined that no active cooling is required for AFW; therefore, this item
is no longer an item of concern.

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4 The IPE also identified an issue associated with the dc electrical configuration that could result 5 in a common mode failure of the pressurizer power-operated relief valves (PORVs). This was 6 corrected during a subsequent outage.

- A comparison of internal events risk profiles between the IPE and the PSA used in the SAMA analysis indicates a decrease of approximately 3.7 x 10⁻⁵ per year in the total CDF (about a factor of two). The reduction is attributed to plant and modeling improvements that have been implemented at Ginna since the IPE was submitted. A summary listing of those changes that resulted in the greatest impact on the total CDF was provided in response to an RAI (RG&E 2003b), and include:
- Relocated the service water (SW) piping that ran through the two battery rooms. This change eliminates the potential loss of both battery rooms due to failure to isolate SW
 line breaks in this area, which was the largest contributing CDF sequence.
- Modified procedures to avoid situations in which both trains of standby auxiliary
 feedwater (SAFW) could be taken out of service at the same time, thereby improving
 the ability to provide steam generator cooling in the event of a high-energy line break in
 the intermediate or turbine building.
 - Revised the "Alternate Shutdown for Control Complex Fire" procedure to also apply to relay room floods. Previously, the procedure only addressed fire.
 - Developed a new procedure to instruct plant personnel to manually close the Bus 18 breakers to prevent a SBO condition in the event of a worst-case fire.
 - Updated generic data sources for initiating events, including the use of WCAP-15210 (WEC 1999) and NUREG/CR-5750 (NRC 1999b).
 - Added plant-specific data for component failure rates, test and maintenance unavailabilities, and initiating event frequencies, and refined the Bayesian updating process.
 - Increased frequencies for loss of offsite power to include all severe weather events, and included ISLOCAs whose frequencies previously fell below the threshold level for detailed analyses.
 - Draft NUREG-1437, Supplement 14

- Updated the human reliability analysis to provide detailed evaluations of more events in lieu of screening values.
 - Removed conservatism for common cause failures that can induce initiators such as loss of service water, component cooling water, and instrument/service air.
- Added fires, internal floods, and shutdown risk models to the fault trees to enable their solution and risk ranking. Removed loss of spent fuel pool cooling and fuel-handling accidents and analyzed separately, because they do not lead to core damage.
- The modeling changes from the IPE version to the current PSA are significant. Some contributors such as transients (previously a 25 percent contribution to internal events CDF) were significantly reduced. For example, the use of updated event frequencies significantly decreased the CDF from large LOCA, and plant changes such as a modification to the service water piping in battery rooms eliminated the largest contributor to CDF. Given the magnitude of the plant and model changes, the overall reduction in CDF appears to be reasonable.
- 17 The IPE CDF value for Ginna is comparable to most of the original IPE values estimated for 18 other pressurized water reactors (PWRs) with a large dry containment. Figure 11.6 of 19 NUREG-1560 shows that the IPE-based total internal events CDF for two-loop Westinghouse 20 plants ranges from 5 x 10⁻⁵ to 1.2 x 10⁻⁴ per reactor-year (NRC 1997a). The internal events 21 CDF based on the latest PSA (approximately 1.3 x 10⁻⁵ per year for events at power) is lower 22 than the IPE values for other two-loop plants. However, it is recognized that other plants in 23 addition to Ginna have reduced the values for CDF subsequent to the IPE submittals through 24 25 modeling and hardware changes.
- 26 The staff considered the peer review performed for the Ginna PSA, and the potential impact of 27 the peer review findings on the SAMA evaluation. In response to an RAI (RG&E 2003b), RG&E 28 described the recent peer review of the Ginna PSA model. In preparation for a Westinghouse 29 Owners Group peer review, an assessment of the Ginna PSA was performed by RG&E, the 30 findings of which resulted in Revision 4.1. Revision 4.1 of the PSA model was reviewed by the 31 Westinghouse Owners Group in May 2002. As a result of the peer review, RG&E updated the 32 PSA to correct the most significant findings and observations. The updated model is referred to 33 34 as Revision 4.2. According to RG&E, a few of the peer review comments were not incorporated into the current version of the PSA; however, those comments were evaluated and judged to 35 36 have minimal impact of the plant CDF and no impact on the SAMA analysis (RG&E 2003c). Two high-level peer review items that were not addressed in the PSA but that could impact the 37 38 SAMA analysis relate to the use of fission product scrubbing factors in the determination of source terms for bypass events. RG&E explicitly addressed these comments in the SAMA 39 analysis by removing credit for scrubbing. 40

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1 Ginna has two reactor coolant pumps (RCPs), each equipped with qualified high-temperature 2 O-rings. The staff questioned RG&E regarding the model used to evaluate RCP seal LOCAs during loss-of-seal cooling events (NRC 2002a, 2003). The model used in Revision 4.2 is a 3 composite based on (1) the original Westinghouse RCP Seal LOCA model developed in 4 WCAP-10541 (WEC 1986), (2) the RCP Seal LOCA model employed by the NRC in NUREG-5 1150 (NRC 1990), (3) the Rhodes-based Brookhaven National Laboratory model, and (4) the 6 most recent Westinghouse RCP Seal LOCA model described in WCAP-15603 (RG&E 2003c). 7 RG&E noted that if the Rhodes model was used, the CDF would be higher by less 8 than1 percent (RG&E 2003c). Based on RG&E's response, which supports use of the current 9 model, the staff concludes that no new SAMA candidates would have evolved from application 10 of the Rhodes model. 11

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RG&E submitted an IPEEE in January 1997 (RG&E 1997c) in response to Supplement 4 of 13 Generic Letter 88-20. This was followed by a submittal that included the fire analysis 14 (RG&E 1998a). RG&E did not identify any vulnerabilities to severe accident risk in regard to 15 the external events related to seismic, fire, or other external events. The Ginna hurricane, 16 tornado, and high winds analyses show that the plant is adequately designed or procedures 17 exist to cope with the effects of these natural events. Additionally, the Ginna IPEEE 18 demonstrated that transportation and nearby facility accidents were not considered to be 19 significant vulnerabilities at the plant. However, a number of areas were identified for 20 improvement in both the seismic and fire areas as discussed below. In a letter dated December 21 21, 2000, the staff concluded that the submittal met the intent of Supplement 4 to Generic 22 23 Letter 88-20, and that the licensee's IPEEE process is capable of identifying the most likely 24 severe accidents and severe accident vulnerabilities (NRC 2000). A strength noted in the IPEEE submittal was that Ginna is an Systematic Evaluation Program (SEP) plant and was 25 subjected to a detailed review for SEP, much of which is applicable to IPEEE. 26 27

The Ginna IPEEE does not provide the means to determine the numerical estimates of the CDF 28 contributions from seismic initiators. The seismic portion of the IPEEE consisted of a reduced-29 scope seismic evaluation using the methodology for Seismic Margins Assessment, described in 30 Electric Power Research Institute NP-6041 (EPRI 1988). Since initial plant licensing, Ginna has 31 undergone a number of programs addressing seismic design issues, one of which was the 32 SEP. Under this and other programs, RG&E conducted extensive reevaluations of, and made 33 34 upgrades to, structures, systems, and equipment at Ginna, using a 0.2g Regulatory Guide 1.60 spectrum as seismic input (NRC 1973). These efforts have extended seismic capacity of Ginna 35 36 beyond the original seismic design basis.

1 During the IPEEE seismic analysis, RG&E identified five vulnerabilities: 2 • The house heating boiler, which is located near the service water pumps in the 3 screenhouse, was not anchored. It could shift and damage the attached natural gas 4 line. 5 6 7 · There are several locations where block wall failures could result in the release of combustibles: an oxygen line in the auxiliary building, a hydrogen line and valve station 8 in the intermediate building, and hydrogen cylinders in the turbine building. 9 10 • There are two fire suppression systems that could be actuated by block wall failures: 11 12 (1) the manual deluge system in the relay room and (2) both a manual deluge system and a pre-action sprinkler system on elevation 253 in the intermediate building. 13 14 Block walls are used as fire barriers throughout the plant. The walls whose failure could 15 impact the fire protection of safety-related equipment are those separating the service 16 building from the intermediate building (column line 3), and those separating the turbine 17 building from intermediate building (column line F). 18 19 The two reactor coolant pump oil collecting tanks in the containment basement were not 20 reviewed during the seismic walkdown because the containment was inaccessible. 21 22 23 These issues were later resolved as a part of the Ginna's IPEEE Fire Analysis by either design evaluations or design changes (RG&E 1998a). 24 25 Additionally, seismic issues were identified for 52 items of equipment (NRC 2002b). Fourteen 26 of these were resolved as part of the closeout of unresolved safety issue (USI) A-46 (NRC 27 1987). In response to an RAI, RG&E indicated that the remaining 38 items have been resolved, 28 and outlined the resolution of all 38 items, a majority of which were resolved by plant 29 modification (RG&E 2003c). Typical modifications included installation of restraints, hangers, 30 anchorages, and modifications of anchorages. 31 32 33 RG&E noted that one item still remains open: seismically induced flooding resulting from the 34 failure of the Reactor Makeup Water Tank (RMWT) and the Monitor Tank (RG&E 2003a). In response to a staff inquiry regarding why this vulnerability was not addressed in the SAMA 35 analysis, RG&E indicated that a modification to address this contributor is planned for 36 implementation in 2005 (NRC 2003). Various design options are being evaluated, including 37 38 installation of leak-tight, removable curb around the RHR sub-basement entrance to a level that would neither pose a flooding danger to the safety injection pumps nor allow the RMWT and 39 Monitor Tank contents to enter the sub-basement (RG&E 2003c). This item has been entered 40

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1 into the Plant Change Request (PCR) system and is being tracked in the Commitment and Action Tracking System as item 10602 (RG&E 2003a). 2 3 The Ginna IPEEE fire assessment used a PSA approach to systematically and successively 4 evaluate fire hazards and their associated risks. The analysis was performed in three phases. 5 The first two phases, consisting of qualitative and quantitative screening steps, used methods 6 that are consistent with the Fire-Induced Vulnerability Evaluation methodology, which was 7 approved for use in NUREG-1407 for screening. The third phase was a detailed fire PSA, 8 which was performed for fire areas and fire zones that were not screened. A quantification for 9 fire events in the IPEEE indicated that the contribution to plant CDF from fire was about 3 x 10⁻⁵ 10 per year. 11 12 Based on the analysis, RG&E concluded that there were no fire-induced vulnerabilities. 13 However, several plant and procedural modifications were identified as a result of the analysis. 14 The following modification was implemented and was credited in the analysis: 15 16 Fuses will be installed on control circuits routed in the screen house associated with the 17 functioning of 4160 VAC circuit breakers. The fuses will be designed to open if 18 grounding occurs during a fire, thus permitting the protective function of the circuit 19 breakers to remain intact. 20 21 22 Several other modifications were identified by the licensee at the time of the IPEEE submittal. 23 specifically: 24 25 an operating procedure enhancement for performing local recovery of the pressurizer heaters if control of the heaters is lost from the control room (the pressurizer heaters are 26 one means of providing long-term reactor coolant system [RCS] circulation) 27 28 • insertion of a warning in the alternate shutdown procedure ER-FIRE-1 to indicate that, in 29 the event of a spurious opening of motor-operated valve (MOV) 857B (which fails RHR 30 shutdown cooling), this valve can be closed locally 31 32 33 installation of additional sealed containers for transient combustibles storage in the 34 auxiliary building basement 35 36 spurious opening of MOVs 850A and 850B due to hot shorts can lead to draining of the refueling water storage tank (RWST) volume into the containment sump 37 38 installation of a local pressure gauge to permit RWST level measurement in the event of 39 fire-induced damage to level instrumentation. 40

1 2 3 4 5 6 7	In response to NRC questions on the IPEEE submittal, RG&E performed a detailed update of the fire risk study that included explicitly modeling operator actions and fire suppression systems. As a result, the above modifications were no longer risk significant and were dismissed. The results of the update were documented in RG&E's response to an RAI (RG&E 1999). The staff reviewed the response and concluded that the licensee's submittals met the intent of the IPEEE process.
8	Since the time of the IPEEE, further changes to the fire and internal flood analyses have been
9	made. In response to an RAI, RG&E delineated the significant changes made to these
10	analyses since the submission of the IPEEE. The changes include:
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12	 The installed fire suppression systems have been explicitly modeled in the fault trees.
13	
14	 Several human error events have been added, and a few were deleted to reflect more
15	detailed modeling of specific fire events.
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17	The model has been revised to reflect a December 2000 plant modification to the
18	service water piping in battery rooms, which eliminated the largest contributing CDF
19	sequence.
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21	Several human error events for floods have been subjected to detailed human error
22	analysis to yield more accurate values for their probabilities.
23	- Soveral flooding initiator frequencies have been revised as well as some new ones
24 25	 Several flooding initiator frequencies have been revised as well as some new ones added to model certain zone-specific floods in greater detail.
25 26	added to model certain zone-specific hoods in greater detail.
20 27	Based on the current PSA, the contribution to the total CDF from fires is comparable to the CDF
28	contribution from internal events (approximately 1 x 10^{-5} per year). As such, in an RAI the staff
29	inquired whether specific SAMAs were considered that might reduce the risk due to fire
30	(NRC 2002a). In response, RG&E stated that six of the eight candidate SAMAs (SAMA
31	numbers 1, 2, 3, 4, 6, and 7) address elements of internal fire (RG&E 2003a).
32	
33	Because RG&E included contributions from fire and floods in its base case evaluation, and due
34	to the extensive efforts made during the IPEEE and SQUG processes to address seismic
35	issues, the staff finds RG&E's consideration of external events to be acceptable.
36	
37	Given that RG&E incorporated all relevant and significant comments from the Westinghouse
38	Owners Group peer review and revised the SAMA analysis accordingly, that RG&E
39	satisfactorily addressed staff questions regarding the PSA (RG&E 2003a, 2003b, 2003c), and
40	that the CDF falls within the range of contemporary CDFs for Westinghouse plants with large

1 dry containments, the staff concludes that the Level 1 and 2 PSA is of sufficient quality to 2 support the SAMA evaluation.

3

The staff reviewed the process used by RG&E to extend the containment performance (Level 2) 4 portion of the PSA to an assessment of offsite consequences (essentially a Level 3 PSA). This 5 process included consideration of the source terms used to characterize fission product 6 7 releases for the applicable containment release category and the major input assumptions used in the offsite consequence analyses. The MACCS2 code was used to estimate offsite 8 consequences. Plant-specific input to the code includes the Ginna reactor core radionuclide 9 inventory, emergency evacuation modeling, release category source terms, site-specific 10 meteorological data, and projected population distribution within a 80-km (50-mi) radius for the 11 12 year 2030. This information is provided in Appendix E of the Ginna ER (RG&E 2002).

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RG&E used source term release fractions for 11 different release classes defined for Ginna. 14 Tables 3 and 4 of the RAI responses provide a breakout of the source terms by release 15 category (RG&E 2003b). The frequencies of the various release classes are based on an 16 updated version of the IPE, developed consistent with the methodology described in 17 NUREG/CR-6595. In the updated analysis, the 25 STCs used in the IPE were rebinned into 11 18 release category bins, each of which was assigned a representative source term based on the 19 original MAAP analyses performed for the IPE. The binning and assignment of source terms 20 appears to have been performed in a consistent manner; that is, the release category bins 21 generally contain STCs with similar release characteristics and timing and are assigned a 22 source term consistent with these characteristics. A sensitivity study was performed for a 23 24 10 percent increase in the quantity of fission products released. (The core inventory was increased by 10 percent while maintaining the release fractions.) This resulted in a 7 percent 25 increase in the population dose. RG&E used the 10 percent larger source term as input into 26 MACCS2 for the base case. The staff concludes that the assignment of source terms is 27 acceptable for use in the SAMA analysis. 28

The applicant used site-specific meteorological data processed from hourly measurements as 30 input to the MACCS2 code. Annual data from 1992 through 1994 were input into the MACCS2 31 code for the base case. The results showed that the total dose and cost results for the most 32 severe release category (ISLOCA) are within 12 percent of the average. The data from 1992 33 34 yielded results above the average for all release cases and, therefore, was selected and used as the input. Where data blocks were missing in the source files, supplementary information 35 36 was derived from meteorological data obtained from the National Oceanic and Atmospheric Administration from the Greater Rochester International Airport, approximately 24 km (15 mi) 37 38 west of Ginna. The staff notes that previous SAMA analyses results have shown little sensitivity to year-to-year differences in meteorological data and considers use of the 1992 data in the 39 base case to be reasonable. 40

The population distribution the applicant used as input to the MACCS2 analysis was estimated for the year 2030, based on the NRC geographic information system for 1990 (NRC 1997c), and the population growth rates were based on the 2000 county-level census data. A sensitivity study was performed by increasing the projected population for 2030 by 10 percent. This resulted in a greater than 20 percent increase for both offsite dose and economic costs. Due to this significant increase, RG&E used the 2030 population plus 10 percent in the base case analysis. The staff considers the methods and assumptions for estimating population reasonable and acceptable for purposes of the SAMA evaluation.

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The emergency evacuation model was modeled as a single evacuation zone extending 16 km (10 mi) from the plant. It was assumed that 95 percent of the population would move at an average speed of approximately 1.8 meters per second (6.0 ft per second) with a delayed start time of 2 hrs (7200 s). This assumption is conservative relative to the NUREG-1150 study (NRC 1990), which assumed evacuation of 99.5 percent of the population within the emergency planning zone. The evacuation assumptions and analysis are deemed reasonable and

16 acceptable for the purposes of the SAMA evaluation.

Much of the site-specific economic data were provided by specifying the data for each of the 13 counties surrounding the plant, to a distance of 50 miles. The SECPOP90 site input file was 20 manually updated to the 2000 timeframe (NRC 1997c). The agricultural economic data were 21 updated using available data from the 1997 Census of Agriculture supplemented by other data 22 available through other federal agencies (USDA 1999). These included per value of farm and 23 non-farm wealth, and fraction of farm wealth from improvements (e.g., buildings).

24

17

The staff concludes that the methodology used by RG&E to estimate the offsite consequences for Ginna, which includes the frequency-weighted contribution from all release categories, provides an acceptable basis from which to proceed with an assessment of risk reduction potential for candidate SAMAs. Accordingly, the staff based its assessment of offsite risk on the CDF and offsite doses reported by RG&E.

30

G.3 Potential Plant Improvements

31 32

> The process for identifying potential plant improvements, an evaluation of that process, and the improvements evaluated in detail by RG&E are discussed in this section.

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37

G.3.1 Process for Identifying Potential Plant Improvements

In the Ginna ER (RG&E 2003b), only eight candidate SAMAs were identified. However, a much
 broader set of SAMAs was considered by RG&E to arrive at these eight SAMAs. RG&E

1	elaborated on its process for identifying potential SAMAs in response to RAIs (RG&E 2003a,
2	2003b, 2003c). The process consisted of the following elements:
3	
4	 review of SAMA analyses performed for other operating plants that have submitted
5	license renewal applications, particularly Fort Calhoun Station
6	
7	 review of other NRC and industry documentation discussing potential plant
	improvements (e.g., NUREG-1560) (NRC 1997a)
8	improvements (e.g., NOREG-1500) (NRC 1997a)
9	no investigation that increases and a interaction that allow the second states of the sinteraction of the second
10	 review of potential improvements identified in the plant-specific risk analyses (IPE,
11	IPEEE, and subsequent PSA revisions)
12	
13	 a review of the Fussel-Vesely (F-V) and risk achievement worth (RAW) importance
14	measures, and the dominant CDF and LERF cut sets for Revision 4.2
15	
16	 insights provided by RG&E plant staff.
17	
18	Based on this process, 192 candidate SAMAs considered by previous applicants, plus several
19	plant-specific SAMAs based on the Ginna PSA were identified (RG&E 2003c). RG&E
20	performed a qualitative screening of the initial list of SAMAs and eliminated SAMAs from further
21	consideration using the following criteria:
21	consideration using the following chiena.
	The SAMA modifies factures not applies he cinne
23	 The SAMA modifies features not applicable to Ginna.
24	
25	The SAMA would involve major plant design and/or structural changes that would clearly
26	be well in excess (greater than two times) of the maximum attainable benefit (MAB).
27	
28	 The SAMA would provide only minimal risk reduction based on review of F-V and RAW.
29	
30	This qualitative screening process reduced the list to approximately 20 candidate SAMAs
31	(RG&E 2003c). These SAMAs were further defined and then reviewed based on the following
32	considerations:
33	
34	 ability to implement the change at Ginna (i.e., are there any design challenges or
35	physical limitations)
	physical limitations)
36	the shall as done there the transmitted as a Particular back as a defense of
37	 the risk reduction that would realistically be achieved
38	
39	 whether implementation of the change would increase vulnerabilities in other areas.
40	

This culminated in eight plant-specific candidate SAMAs. These eight SAMAs were further
evaluated, and two SAMAs were found to be potentially cost beneficial, as described below in
Sections G.4 and G.6. RG&E considered the impact of uncertainties on the results of the
SAMA analysis (RG&E 2003a). No additional SAMAs were judged to be cost beneficial
(RG&E 2003b).

6

7

G.3.2 Review of RG&E's Process

8 The preliminary review of the Ginna ER raised concerns regarding the process used to identify 9 potential SAMAs, and the completeness of the set of SAMAs considered. This was 10 satisfactorily resolved though the additional information provided by the applicant, as described 11 12 above. The staff also requested information regarding whether an importance analysis was used to confirm the adequacy of the SAMA identification process, and the portion of risk 13 represented by the dominant risk contributors. In response to the RAI, RG&E provided a 14 tabular listing of the contributors with the greatest potential for reducing risk as demonstrated by 15 F-V and RAW assigned to the event. This approach inherently considers the top 95 percent of 16 17 the CDF and LERF cut sets. RG&E also reviewed the dominant 50 CDF and LERF cut sets, which accounts for the top 45 percent of the CDF cut sets and 75 percent of the LERF cut sets 18 19 (RG&E 2003b). Based on this, the staff concludes that RG&E's efforts to identify potential SAMAs included consideration of areas that presented the greatest potential for reducing risk. 20 21 The list of eight SAMAs generally addressed the accident categories that are dominant CDF 22 contributors or issues that tend to have a large impact on a number of accident sequences at 23 Ginna.

In the original ER submittal, the estimated MAB was \$992,000 (RG&E 2002). During the screening process, SAMAs whose cost exceeded two times the MAB were removed from further consideration. The SAMA analysis was subsequently revised to address peer review comments, and that portion of the ER was resubmitted. As a result, the MAB increased to \$1.93 million. RG&E concluded that the increase in MAB did not result in the identification of any additional SAMAs. The staff agrees with this conclusion because the initial screening removed SAMAs that are estimated to cost \$2 million or more.

32

24

33 The staff questioned RG&E whether it considered some of the cost beneficial SAMAs identified at previous plants, specifically, the use of a portable generator to power steam generator level 34 instrumentation, and improvements to the reactor protection system logic to reduce the 35 likelihood of failure of two 125 VAC instrument buses causing the spurious opening of the 36 PORVs (NRC 2003). In a telephone conversation, RG&E stated that such vulnerabilities did not 37 exist at Ginna due to design differences, or that sufficient battery capacity existed. Ginna is a 38 4-hour coping plant but has 8-hour capacity batteries (NRC 2003). Based on a review of the 39 response, the staff agrees with this conclusion. 40

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1 The staff notes that the set of SAMAs submitted is not all inclusive, since additional, possibly

2 even less expensive, design alternatives can always be postulated. However, the staff

3 concludes that the benefits of any additional modifications are unlikely to exceed the benefits of

the modifications evaluated and that the alternative improvements would not likely cost less
 than the least expensive alternatives evaluated, when the subsidiary costs associated with

than the least expensive alternatives evaluated, when the subsidiary c
maintenance, procedures, and training are considered.

7

The staff concludes that RG&E used a systematic and comprehensive process for identifying
potential plant improvements for Ginna, and that the set of potential plant improvements
identified by RG&E is reasonably comprehensive and, therefore, is acceptable. This search
included reviewing insights from the IPE, IPEEE, and other plant-specific studies; reviewing
plant improvements in previous SAMA analyses; and using the knowledge and experience of its
PRA personnel.

13 14

16

15 G.4 Risk Reduction Potential of Plant Improvements

17 RG&E estimated the risk-reduction potential of the eight remaining SAMA candidates that were 18 applicable to Ginna. RG&E used model requantification to determine the potential benefits. The CDF and LERF reductions were estimated using the current version of the Ginna PSA 19 20 (Revision 4.2). The changes made to the PSA model to quantify the impact of each SAMA are detailed in Section E.3 of Appendix E to the Ginna ER (RG&E 2003b). Table G-3 provides a 21 22 summary of the assumptions used to estimate the risk reduction, the risk reduction in terms of 23 percent reduction in CDF and population dose, the total benefit (present value) of the averted risk, and the estimated implementation cost for each of the eight SAMAs. The determination of 24 the benefits for the various SAMAs is discussed in Section G.6. 25

In response to an RAI, RG&E considered the uncertainties associated with the calculated CDF.
 This matter is discussed further in Section G.6.2.

The staff has reviewed the bases used by RG&E for calculating the risk reduction for the various plant improvements, and concludes that the rationale and assumptions for estimating risk reduction are reasonable and generally conservative (i.e., the estimated risk reduction is higher than what would actually be realized). Accordingly, the staff based its estimates of averted risk for the various SAMAs on risk reduction estimates provided by RG&E.

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G.5 Cost Impacts of Candidate Plant Improvements

36 37

RG&E estimated the costs of implementing the eight candidate SAMAs through the application
 of engineering judgment and site-specific cost estimates. The cost estimates (presented in
 Section E.3 of Appendix E to the Ginna ER) conservatively did not include the cost of

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				cent Risk		
			Re	eduction	Total	Estimated
3	SAMA	Assumptions	CDF	Population Dose	Benefit (\$)	Cost (\$)
4	1. Obtain a skid-mounted,	The addition of a skid-mounted,	24.8	43.5	<u>(</u>) 944,000	400,000
5	480-V diesel generator	480-V diesel generator with the	24.0	43.5	944,000	400,000
6	that could be directly	same failure rate as the existing				
7	connected to one train of the	diesel generators and a				
8	safeguards buses in the	0.01 operator failure probability to				
9	event of a failure of the two	start and align the diesel				
10	existing diesel generators. ^(a)	generator can supply the				
		safeguards bus to reduce SBO				
		and induced SBO sequences.				
11	2. Obtain a third fire water	The addition of a diesel-driven	1.8	3.3	70,000	200,000
12	source that is independent of	pump of comparable size to the				
13	the existing suction source	existing motor- and diesel-driven				
14 15	for the motor- and diesel-	fire pumps can be connected to				
16	driven fire pumps to be used in the event of a total loss of	the existing fire system water piping and used for fire suppres-				
17	the screen house due to a	sion or as a source of suction to				
18	fire or flood or loss of all	the AFW pumps. The failure rate				
19	service water suction due to	of the new pump is assumed to				
20	environmental causes.	be the same as the existing				
		diesel-driven fire pump. A failure				
		rate of 0.1 is assumed for the				
		operator action to connect the				
		pump to the AFW system and				
		0.01 for the operator action to				
		align the pump to supply the fire				
04		system during fire events.	44.0	0.5	407 000	4 400 000
21 22	3. Add a standby charging	Conditions where charging pump	11.2	2.5	107,000	1,100,000
22	pump powered from a protected AC source and	A is out of service or directly failed, large floods that disable all				
24	located in the intermediate or	three charging pumps and a				
25	turbine building or SAFW	charging pump room fire can be				
26	pump building.	mitigated by an additional				
	1 1 3	charging pump that autostarts on				
		low flow or pressure. This pump				
		is assumed to be powered from				
		Bus 14.				

Table G-3. SAMA Cost/Benefit Screening Analysis

Table G-3. (contd)

				cent Risk		
				eduction	Total Benefit	Estimated
	SAMA	Assumptions	CDF	Population Dose	(\$)	Cost (\$)
charging manually This aliguused to r requiring procedur Shutdow Complex disabling charging	rocedures to allow pump B or C to be aligned to Bus 14. Inment could be nitigate fires entry into e "Alternative n for Control Fire" or fires train B, where the A pump is out of r fails to run. ^(a)	Manually aligning the B or C pump to Bus 14 can reduce all cut sets in which charging pump A is out of service or failed directly. A failure rate of 8.21 x 10^{-3} is used for aligning and starting the pump.	9.1	1.7	83,000	20,000
5. Add redu in the two to the RC LOCA in	indant check valves o RHR injection lines CS to prevent a the auxiliary which could not be	The ISLOCA frequency is reduced reflecting the new configuration where failure of the additional check valve, the current check valve and the MOV, or both check valves and an inadvertent opening of the MOV, or a spurious safety injection signal would result in an ISLOCA. This was applied to the two lines through Penetration 111. It was also assumed that for this penetration LERF is a third of CDF because a third of the Penetration 111 piping that would be exposed to RCS pressure is inside containment.	0.2	7.7	45,000	1,000,000
pump co	otor-driven AFW oling system to be lent of service water	All cut sets that involve a loss of all AFW due to a failure of the SW suction source or a global failure of the screen house equipment due to fire or flooding will no longer lead to core damage due to the availability of the motor-driven pumps.	1.8	< 1	13,000	200,000

-				cent Risk eduction	Total	Estimated
	SAMA	Assumptions	CDF	Population Dose	Benefit (\$)	Cost (\$)
-	7. Modify air-operated valve (AOV) 112C to fail close and AOV 112B to fail open on loss of instrument air. This change would allow the RWST to become the suction source for charging instead of the volume control tank (VCT).	All cut sets that contain the operator action to switch over the charging suction source from the VCT to the RWST can be reduced by setting this action to false (success).	2.0	< 1	14,000	50,000
	8. Reconfigure the PORV so they transfer automatically from instrument air to N2 on low pressure and convert N2 supply line AOV to DC powered MOV.	The nitrogen system is available to support the power-operated relief valves with a failure probability of 4.76×10^{-3} (the failure rate of the components in the nitrogen system). Nitrogen support system failures were not included. This is conservative in that including these failures would increase the failure probability of the nitrogen system.	1.6	< 1	24,000	400,000
-	(a) SAMAs judged to be cost benefic	the nitrogen system.				

Table G-3. (contd)

20

1 2

21 replacement power during extended outages required to implement the modifications, nor did 22 they include recurring maintenance and surveillance costs or contingency costs associated with 23 unforeseen implementation obstacles. Cost estimates typically included procedures, training, 24 and documentation, in addition to any hardware.

25 The staff reviewed the bases for the applicant's cost estimates. For certain improvements, the 26 27 staff also compared the cost estimates to estimates developed elsewhere for similar improvements, including estimates developed as part of other licensees' analyses of SAMAs for 28 operating reactors and advanced light-water reactors. Six of the eight SAMAs were screened 29 30 from further consideration on the basis that the expected implementation cost would be much 31 greater than the estimated risk reduction benefit. This is reasonable for these six SAMAs given 32 the relatively small estimated benefit (a maximum benefit of about \$107,000 among the six SAMAs), and the sizeable costs typically associated with hardware modifications. It is noted 33 34 that one SAMA (SAMA 7) involves a minimal hardware modification to two valve operators. However, the estimated benefit for this SAMA (\$14,000) is small in comparison to the 35 implementation costs (\$50,000), and the actual costs are likely to be higher when all cost 36 factors are included. The staff concludes that the cost estimates are sufficient and appropriate 37 38 for use in the SAMA evaluation.

G-19

1 2	G.6	Cost/Benefit Comparison
2 3 4	RG&E	's cost/benefit analysis and the staff's review are described in the following sections.
5 6	G.6.1	RG&E Evaluation
7 8 9 10	cost/b	ethodology used by RG&E was based primarily on NRC's guidance for performing enefit analysis (NRC 1997d). The guidance involves determining the net value for each according to the following formula:
11 12		Net Value = (APE + AOC + AOE + AOSC) - COE
13 14	where	,
15 16 17 18 19 20		 APE = present value of averted public exposure (\$) AOC = present value of averted offsite property damage costs (\$) AOE = present value of averted occupational exposure costs (\$) AOSC = present value of averted onsite costs (\$) COE = cost of enhancement (\$).
21 22 23 24	benefi	net value of a SAMA is negative, the cost of implementing the SAMA is larger than the t associated with the SAMA, and it is not considered cost beneficial. RG&E's derivation h of the associated costs is summarized below.
25 26	<u>Averte</u>	ed Public Exposure (APE) Costs
27 28	The A	PE costs were calculated using the following formula:
29 30 31 32 33	AF	 PE = Annual reduction in public exposure (Δperson-rem/reactor-year) x monetary equivalent of unit dose (\$2000 per person-rem) x present value conversion factor (10.76 based on a 20-year period with a 7 percent discount rate).
34 35 36 37 38 39 40	the pu health losses Thus, accide	ted in NUREG/BR-0184 (NRC 1997d), it is important to note that the monetary value of blic health risk after discounting does not represent the expected reduction in public risk due to a single accident. Rather, it is the present value of a stream of potential extending over the remaining lifetime (in this case, the renewal period) of the facility. it reflects the expected annual loss due to a single accident, the possibility that such an ent could occur at any time over the renewal period, and the effect of discounting these ial future losses to present value. For the purposes of initial screening, RG&E calculated

1	an APE of approximately \$350,000 for the 20-year license renewal period, which assumes
2	elimination of all severe accidents.
3	
4	Averted Offsite Property Damage Costs (AOC)
5	
6	The AOCs were calculated using the following formula:
7	
8	AOC = Annual CDF reduction
9	x offsite economic costs associated with a severe accident (on a per-event basis)
10	x present value conversion factor.
11	
12	For the purposes of initial screening, which assumes all severe accidents are eliminated, RG&E
13	calculated an annual offsite economic risk of about \$87,000 based on the Level 3 risk analysis.
14	This results in a discounted value of approximately \$932,000 for the 20-year license renewal
15	period.
16	
17	Averted Occupational Exposure (AOE) Costs
18	
19	The AOE costs were calculated using the following formula:
20	
21	AOE = Annual CDF reduction
22	x occupational exposure per core damage event
23	x monetary equivalent of unit dose
24	x present value conversion factor.
25	
26	RG&E derived the values for averted occupational exposure from information provided in
27	Section 5.7.3 of the regulatory analysis handbook (NRC 1997d). Best estimate values provided
28	for immediate occupational dose (3300 person-rem) and long-term occupational dose
29	(20,000 person-rem over a 10-year cleanup period) were used. The present value of these
30	doses was calculated using the equations provided in the handbook in conjunction with a
31	monetary equivalent of unit dose of \$2000 per person-rem, a real discount rate of 7 percent,
32	and a time period of 20 years to represent the license renewal period. For the purposes of
33	initial screening, which assumes all severe accidents are eliminated, RG&E calculated an AOE
34	of approximately \$15,000 for the 20-year license renewal period.
35	
36	

1 2	Averted Onsite Costs (AOSC)
2 3 4 5 6 7	Averted onsite costs (AOSC) include averted cleanup and decontamination costs and averted power replacement costs. Repair and refurbishment costs are considered for recoverable accidents only and not for severe accidents. RG&E derived the values for AOSC based on information provided in Section 5.7.6 of the regulatory analysis handbook (NRC 1997d).
8 9 10 11	RG&E divided this cost element into two parts: (1) the onsite cleanup and decontamination Cost, also commonly referred to as averted cleanup and decontamination costs, and (2) the replacement power cost.
12 13	Averted cleanup and decontamination costs (ACC) were calculated using the following formula:
14 15 16 17	ACC = Annual CDF reduction x present value of cleanup costs per core damage event x present value conversion factor.
18 19 20 21 22	The total cost of cleanup and decontamination subsequent to a severe accident is estimated in the regulatory analysis handbook to be 1.5×10^9 (undiscounted). This value was converted to present costs over a 10-year cleanup period and integrated over the term of the proposed license extension.
22 23 24	Long-term replacement power costs (RPC) were calculated using the following formula:
25 26 27 28 29 30	RPC = Annual CDF reduction x present value of replacement power for a single event x factor to account for remaining service years for which replacement power is required x reactor power scaling factor
31 32 33 34 35 36 37 38	RG&E based its calculations on the value of 490 MWe, and scaled down from the 910 MWe reference plant in NUREG/BR-0184 (NRC 1997d). Therefore, RG&E applied a power scaling factor of 490 MWe/910 MWe to determine the replacement power costs. For the purposes of initial screening, which assumes all severe accidents are eliminated, RG&E calculated an RPC of approximately \$169,000 for the 20-year license renewal period.
39	

- 1 Using the above equations, RG&E estimated the total present dollar value equivalent 2 associated with completely eliminating severe accidents at Ginna to be about \$1.93 million. 3 4 RG&E's Results 5 6 If the implementation costs were greater than the MAB, then the SAMA was screened from 7 further consideration. A more refined look at the costs and benefits was performed for the remaining SAMAs. If the expected cost for those SAMAs exceeded the calculated benefit, the 8 SAMA was considered not to be cost beneficial. The cost/benefit results for the individual 9 analysis of the eight SAMA candidates are presented in Table G-3. As a result, two of the 10 eight SAMAs were considered to be potentially cost beneficial: 11 12 • SAMA 1: Obtain a skid-mounted, 480-V diesel generator that could be directly 13 connected to one train of the safeguards buses in the event of a failure of the 14 two existing diesel generators. 15 16 • SAMA 4: Modify procedures to allow charging pump B or C to be manually aligned to 17 Bus 14. This alignment could be used to mitigate fires requiring entry into 18 procedure "Alternative Shutdown for Control Complex Fire" or fires disabling 19 train B, where the A charging pump is out of service or fails to run. 20 21 RG&E performed sensitivity analyses to evaluate the impact of parameter choices on the 22 23 analysis results (RG&E 2002, 2003a, 2003b). As discussed in Section 5.2.2.2, sensitivity cases 24 that assumed a 10 percent increase in the projected population and a 10 percent increase in 25 fission product releases were adopted in the baseline analysis. In addition, RG&E considered the impact on SAMA results if (1) a 3 percent discount rate (rather than 7 percent in the base 26 case) as recommended in NUREG/BR-0184 (NRC 1997d) was used, and (2) if the 95th 27 percentile values of the CDF were utilized in the cost/benefit analysis instead of the mean CDF. 28 These analyses did not result in a positive net benefit for any additional SAMAs. 29 30 RG&E stated in the Ginna ER that the two potentially cost beneficial SAMAs identified above do 31 not relate to adequately managing the effects of aging, and therefore, are not required to be 32 implemented pursuant to 10 CFR Part 54 (RG&E 2003b). However, RG&E stated that it will 33
- 34 35
- 36 G.6.2 Review of RG&E's Cost/Benefit Evaluation
- 37

The cost/benefit analysis performed by RG&E was based primarily on NUREG/BR-0184

consider implementation of these SAMAs through its current plant change process.

39 (NRC 1997d) and was executed consistent with this guidance.

In response to an RAI, RG&E considered the uncertainties associated with the calculated CDF
(Table G-4). If the 95th percentile values of the CDF were used in the cost/benefit analysis
instead of the mean CDF value used in the baseline analysis, the estimated benefits of the
SAMAs would increase by about a factor of two. Increasing the benefit by this factor would
have no impact on the conclusion of the SAMA evaluation; that is, even if the non-viable
SAMAs (those qualitatively screened out) were increased by a factor of two, the resulting cost
benefit would remain negative (RG&E 2003b).

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Table G-4.Uncertainty in the Calculated Core Damage Frequency
for R.E. Ginna Nuclear Power Plant

Percentile	CDF (per year)
5 th	2.05 x 10⁵
50 th	3.52 x 10⁵
mean	4.00 x 10 ⁻⁵
95 th	9.00 x 10⁻⁵

In addition, RG&E performed sensitivity analyses that addressed assumptions made in other
 parts of the cost/benefit analysis, including variations in discount rate, weather, population, and
 source terms. These were either adopted in the base case (e.g., population and source terms)
 or are bounded by the CDF uncertainty assessment.

The staff concludes that, with the exception of the two cost beneficial SAMAs, the costs of the SAMAs would be higher than the associated benefits. This conclusion is supported by uncertainty assessment and sensitivity analysis and upheld despite a number of additional uncertainties and non-quantifiable factors in the calculations, summarized as follows:

Uncertainty in the internal events CDF was not initially included in the calculations,
 which employed mean values to determine the benefits. The 95th percent confidence
 level for internal events CDF is approximately 2.25 times the best estimate CDF. Even
 upon considering the benefits at the 95th percentile value, no SAMAs were judged to be
 cost beneficial. Therefore, consideration of CDF uncertainty is not expected to alter the
 conclusions of the analysis.

- Seismic events were not included in the Ginna risk profile. However, seismic vulner abilities were addressed during the IPEEE and SQUG evaluations. Fire and flood
 events have been included within the scope of the SAMA evaluation. An increase in the
 benefits by a factor of two had no impact on the results of the evaluation.
- 39

 Risk reduction and cost estimates were generally found to be conservative. As such, uncertainty in the costs of any of the contemplated SAMAs would not likely have the effect of making them cost beneficial.

G.7 Conclusions

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RG&E evaluated approximately 200 SAMA candidates using the SAMA analyses as submitted
in support of licensing activities for other nuclear power plants, NRC and industry documents
discussing potential plant improvements, and the plant-specific insights from the Ginna IPE,
IPEEE, and current PSA model. A qualitative screening removed SAMA candidates that
(1) were not applicable at Ginna due to design differences, (2) had already been implemented
at Ginna, (3) were prohibitively expensive, or (4) did not provide a significant safety benefit.
Upon conclusion of this screening, eight SAMA candidates were retained for further evaluation.

- Using guidance in NUREG/BR-0184 (NRC 1997d), the current PSA model, and a Level 3 15 16 analysis developed specifically for SAMA evaluation, a maximum attainable benefit of about \$1.93 million was calculated, representing the total present-dollar-value equivalent associated 17 18 with completely eliminating severe accidents at Ginna. For the remaining eight SAMA candidates, a more detailed conceptual design and cost estimate were developed as shown in 19 20 Table 5-5. The cost-benefit analyses showed that two of the eight SAMA candidates were potentially cost beneficial. Upon completion of a 3 percent discount rate sensitivity study, no 21 additional SAMA candidates were determined to be cost beneficial. RG&E also considered the 22 23 benefits at the 95th percentile CDF value, and found that no additional SAMAs were cost beneficial. 24
- 25 26 The staff reviewed the RG&E analysis and concluded that the methods used and the implementation of those methods were sound. The treatment of SAMA benefits and costs, the 27 generally large negative net benefits, and the inherently small baseline risks support the 28 29 general conclusion that the SAMA evaluations performed by RG&E are reasonable and sufficient for the license renewal submittal. The unavailability of a seismic PSA model 30 31 precluded a quantitative evaluation of SAMAs specifically aimed at reducing risk of this initiator; 32 however, significant improvements have been realized as a result of the IPEEE and SQUG processes at Ginna that would minimize the likelihood of identifying cost beneficial 33 enhancements in this area. It is noted that one item still remains open: seismically induced 34 flooding resulting from the failure of the RMWT and the Monitor Tank. However, RG&E is 35 addressing this item through the PCR process and plans to implement a modification in 2005. 36 37
- Although two SAMA candidates appear to be cost beneficial, they do not relate to adequately managing the effects of aging during the period of extended operation. Therefore, they need not be implemented as part of the license renewal pursuant to 10 CFR Part 54.

1 G.8 References

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 renewal of operating licenses for nuclear power plants."

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