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May 29, 2003

SVP-03-073

U. S. Nuclear Regulatory Commission ATTN: Document Control Desk Washington, D.C. 20555

> Quad Cities Nuclear Power Station, Unit 1 Facility Operating License No. DPR-29 NRC Docket Number 50-254

Subject: Core Operating Limits Report for Quad Cities Unit 1 Cycle 18A

In accordance with Technical Specifications Section 5.6.5.d, enclosed is the Core Operating Limits Report (COLR) for Quad Cities Unit 1 Cycle 18A.

On May 20, 2003, Quad Cities Nuclear Power Station (QCNPS) Unit 1 was shutdown for a planned maintenance outage (Q1M16). During Q1M16, 233 Siemens Atrium 9B fuel bundles were replaced to address fuel performance concerns. As a result, a revised reload design, designated Cycle 18A, has been developed for Unit 1. The revised COLR for Unit 1 will be implemented prior to startup from Q1M16. QCNPS Unit 1 is currently scheduled to startup on May 29, 2003.

Should you have any questions concerning this letter, please contact Mr. W. J. Beck at (309) 227-2800.

Respectfully Timothy J. Tulon

Sile Vice President Quad Cities Nuclear Power Station

Attachment A: Core Operating Limits Report (COLR) for Quad Cities Unit 1 Cycle 18A

cc: Regional Administrator – NRC Region III NRC Senior Resident Inspector – Quad Cities Nuclear Power Station Attachment A

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Core Operating Limits Report

for

Quad Cities Unit 1 Cycle 18A

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# Exelon. Nuclear

# Core Operating Limits Report (COLR)

for

# Quad Cities Unit 1 Cycle 18A

# **Revision** 0

# Issuances of Changes Summary

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Affected Section	Affected Pages	Summary of Changes	Revision	Issue
All	All	Original Issue for Cycle 18A	0	5/2003

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- 4. GE-NE-J11-03912-00-01-R1. "Dresden 2 and 3 Quad Cities 1 and 2 Equipment Out-Of-Service

and Legacy Fuel Transient Analysis," November 2001.

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- 8. QDC-02-18, "OPL-3 for Quad Cities Unit 1 Cycle 18," April 25, 2002.
- 9. EMF-2563(P), Revision 1, "Fuel Mechanical Design Report Exposure Extension for ATRIUM-9B Fuel Assemblies at Dresden, Quad Cities, and LaSalle Units", August 2001.
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- 11. NEDE-24011-P-A-14, General Electric Standard Application for Reactor Fuel (GESTAR II) and US Supplement, June 2000.
- 12. NF0300028, Revision 0, "Quad Cities 1 Cycle 18A FRED Form," March 26, 2003.
- 13. NF-MW:02-0413, "Approval of GE Evaluation of Dresden and Quad Cities Pressure Regulator Out of Service Analysis," October 22, 2002.
- 14. NFM-MW:02-0274, "Approval of GE Evaluation of MSIV out of Service for Dresden and Quad Cities", August 2, 2002.
- 15. BNDQ:03-022, Revision 0, "Quad Cities Unit 1 Cycle 18A Composite LHGR Curve Generation for Bundle 2647," May 2003.
- 16. BNDQ:03-024, Revision 0, "Quad Cities Unit 1 Cycle 18A Generation of the Revision 0 Core Operating Limits Report (COLR)," May 2003.

# 1. Average Planar Linear Heat Generation Rate

## **1.1** Technical Specification Reference

Sections 3.2.1 and 3.4.1

## 1.2 Description

Tables 1-1 and 1-2 are used to determine the maximum average planar linear heat generation rate (MAPLHGR) limit for each fuel type. Limits listed in Tables 1-1 and 1-2 are for dual reactor recirculation loop operation (DLO).

For single reactor recirculation loop operation (SLO), the MAPLHGR limits given in Tables 1-1 and 1-2 must be multiplied by a SLO MAPLHGR multiplier. The SLO MAPLHGR multipliers are given in Table 1-3 by fuel type.

Table 1-1: Maximum Average Planar Line FANP (formerly SP	ear Heat Generation Rate (MAPLHGR) for Control (Control Control Co
Applicable to the follov Bundle Type 5, ATRM9-P9DATB348- Bundle Type 7, ATRM9-P9DATB360-	ving fuel bundle types: 11G6.5-SPC100T-9WR-144-T6-2444
Applicable Refere	nce Number(s): 3
Planar Average Exposure (GWD/MT)	MAPLHGR Limit (kW/ft)
0.00	13.52
17.25	13.52
70.00	7.84

	ear Heat Generation Rate (MAPLHGR) for 1999
Applicable to the follow	wing fuel bundle types:
Bundle Type 16, GE14-P10DN/	AB411-14GZ-100T-145-T6-2564
	AB409-15GZ-100T-145-T6-2565
	B194-4G7.0-100T-145-T6-2647
	nce Number(s): 3
Planar Average Exposure (GWD/MT)	MAPLHGR Limit (kW/ft)
0.00	11.68
16.00	11.68
44.09	9.16
55.12	8.09
63.50	6.97
70.00	4.36

Table 1-3: Maximum Average Planar L SLO Multipliers 1	near Heat Generation Rate (MAPLHGR)
Applicable Refere	nce Number(s): 3
Fuel Product Line	SLO MAPLHGR Multiplier
ATRIUM-9B	0.84
GE14	0.77

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# 2. Minimum Critical Power Ratio

# 2.1 Technical Specification Reference

Sections 3.2.2, 3.4.1, and 3.7.7.

## 2.2 Description

The MCPR limit for a specific fuel type/condition is determined by choosing the maximum CPR limit from the pool of applicable limits. The sections below provide the method for determining the applicable MCPR limit in any case. Linear interpolation is to be used to determine values from the following tables for flow/power conditions not specifically listed: 2-3, 2-4, 2-5, and 2-7. Rated core thermal power is 2957 MWth and rated core flow is 98 Mlb/hr.

#### 2.2.1 Manual Flow Control (MFC) MCPR Limits

The operating limit MCPR (OLMCPR) for operation in the manual flow control mode is determined from either Section 2.2.1.1 or 2.2.1.2, whichever is greater at the given power and flow condition.

#### 2.2.1.1 MFC Power-Dependent MCPR (MCPR<sub>P</sub>)

For operation at less than 38.5% of rated core thermal power, the OLMCPR as a function of core thermal power (MCPR<sub>P</sub>) is shown in Table 2-3. For operation at greater than 38.5% of rated core thermal power, the OLMCPR as a function of core thermal power is determined by multiplying the applicable EOOS condition limit as shown in Table 2-1 or 2-2 (see Section 2.2.3) by the applicable MCPR multiplier, K<sub>P</sub>, given in Table 2-3. For operation at exactly 38.5% of rated core thermal power, the OLMCPR as a function of core thermal power is the maximum of either of the two aforementioned methods evaluated at 38.5% of rated core thermal power.

#### 2.2.1.2 MFC Flow-Dependent MCPR (MCPR<sub>F</sub>)

The OLMCPR as a function of flow (MCPR<sub>F</sub>) is determined from either Table 2-4 or Table 2-5 depending on the EOOS condition. The MCPR<sub>F</sub> limit is independent of the flow control mode of the reactor.

#### 2.2.2 Automatic Flow Control (AFC) MCPR Limits

The operating limit MCPR (OLMCPR) in the automatic flow control mode is to be determined from either Section 2.2.2.1 or 2.2.2.2, whichever is greater at the given power and flow condition.

#### 2.2.2.1 AFC Power-Dependent MCPR

For operation at less than 38.5% of rated core thermal power, the OLMCPR as a function of core thermal power (MCPR<sub>P</sub>) is shown in Table 2-7. For operation at greater than 38.5% of rated core thermal power, the OLMCPR as a function of core thermal power is determined by multiplying the applicable EOOS condition limit as shown in Table 2-6 by the applicable MCPR multiplier, K<sub>P</sub>, given in Table 2-7. For operation at exactly 38.5% of rated core thermal power, the OLMCPR as a function of core thermal power, the OLMCPR as a function of core thermal power is the maximum of either of the two aforementioned methods evaluated at 38.5% of rated core thermal power.

#### 2.2.2.2 AFC Flow-Dependent MCPR

The OLMCPR as a function of flow (MCPR<sub>F</sub>) is determined from either Table 2-4 or Table 2-5 depending on the EOOS condition. The MCPR<sub>F</sub> limit is independent of the flow control mode of the reactor.

#### 2.2.3 Option A and Option B

OLMCPR values have been determined based upon two assumed core average scram times – Option A which assumes the Technical Specification 20% insertion core average scram time and Option B which assumes a core average 20% insertion scram time equal to 0.694 seconds.

Option A OLMCPR values may be utilized if the core average 20% insertion scram time is less than or equal to the Technical Specification required time. Reload analyses performed by Global Nuclear Fuel (GNF) for cycle 18A Option A MCPR limits utilized a 20% core average insertion time of 0.900 seconds (References 7 and 8).

Option B OLMCPR values may be utilized if the core average 20% insertion scram time is less than or equal to 0.694 seconds (References 7 and 8).

If the core average scram insertion time does not meet the Option B criteria, but is less than the Option A criteria, the appropriate OLMCPR value may be determined from a linear interpolation between the Option A and Option B limits with standard mathematical rounding to two decimal places. When performing a linear interpolation to determine MCPR limits, ensure that the time used for Option A is 0.900 seconds, which is the 20% insertion time utilized by GNF in the reload analyses. For manual flow control operation, Option A based OLMCPRs are found in Table 2-1 while Option B based OLMCPRs are contained in Table 2-2. For automatic flow control operation only Option A based OLMCPRs are available and are given in Table 2-6 (no adjustment for core average scram time is available for AFC mode).

#### 2.2.4 Recirculation Pump Motor Generator Settings

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Quad Cities Unit 1 Cycle 18A was analyzed with a maximum core flow runout of 110% of rated core flow. Therefore, the recirculation pump motor generator scoop tube mechanical and electrical stops must be set to maintain core flow less than 110% of rated core flow, which is equivalent to 107.8 Mlb/hr (1.10 \* 98.0 Mlb/hr), for all runout events (Reference 12). A maximum core flow runout of 110% of rated core flow is consistent with what was used in the analysis presented in Reference 4.

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	Table 2-1: Optic				
a been betrefaren and fabries of the second second		ble Reference Nu	mber(s): 3,4	_	nie. In water of the state of
		li se	Cycle Expos	sure Range	
EOOS Combination <sup>[4]</sup>	Fuel Type	<2200 MWD/MT	≥2200 MWD/MT & <eor<sup>[1]-2128 MWD/MT</eor<sup>	≥EOR <sup>1</sup> -2128 MWD/MT & <eor< th=""><th>≥EOR<sup>[1]</sup> (Coastdown)</th></eor<>	≥EOR <sup>[1]</sup> (Coastdown)
	GE14	1.53	1.66	1.66	1.66
Base Case	ATRIUM-9B	1.50	1.66	1.66	1.66
	GE14	1.54	1.67	1.67	1.67
Base Case SLO	ATRIUM-9B	1.51	1.67	1.67	1.67
FWHOOS/FFWTR	GE14	1.55	1.66	1.66	1.66
	ATRIUM-9B	1.52	1.66	···· <b>1.</b> 66	1.66
FWHOOS/FFWTR SLO	GE14	1.56	1.67	1.67	1.67
FWHUUS/FFWIR SLU	ATRIUM-9B	1.53	1.67	1,67	1.67
TBPOOS <sup>[2]</sup>	GE14	1.72	1.72	1.72	1.74 <sup>[3]</sup>
IBP005	ATRIUM-9B	1.68	1.68	1.68	1.70 <sup>[3]</sup>
TBPOOS SLO <sup>[2]</sup>	GE14	1.73	1.73	1.73	1.75 <sup>[3]</sup>
182003 310	ATRIUM-9B	1.69	1.69	1.69	1.71 <sup>[3]</sup>
TCV Slow Closure	GE14	1.61	1.66	1.66	1.66
	ATRIUM-9B	1.55	1.66	1.66	1.66
TCV Slow Closure SLO	GE14	1.62	1.67	1.67	1.67
TOV SIOW CIUSUIE SLU	ATRIUM-9B	1.56	1.67	1.67	1.67
PLUOOS	GE14	1.64	1.66	1.66	1.66
PLUUUS	ATRIUM-9B	1.58	1.66	1.66	1.66
PLUOOS SLO	GE14	1.65	1.67	1.67	1.67
FL0003 3L0	ATRIUM-9B	1.59	1.67	1.67	1.67
TCV Stuck Closed	GE14	1.55	1.66 <sup>·</sup>	1.66	1.66
	ATRIUM-9B	1.52	1.66	1.66	1.66
TCV Stuck Closed SLO	· GE14	1.56	1.67	1.67	1.67
TOV SLUCK Closed SLU	ATRIUM-9B	1.53	1.67	1.67	1.67

Notes for Table 2-1:

1. 2. EOR refers to the end of rated power operation - the all-rods-out condition at 100% rated power and 100% rated flow.

TBPOOS cases include a +0.03 OLMCPR penalty for operation below analysis basis dome pressure per page 24 of Reference 4.

TBPOOS cases which cover operation in coast down conditions include a +0.02 OLMCPR penalty per page 22 of 3. Reference 4.

All EOOS combinations presented here, except for the BASE CASE and BASE CASE SLO, account for both normal 4. feedwater temperature operation and operation with FFWTR/FHOOS.

All EOOS combinations except TBPOOS/TBPOOS SLO have their Option A OLMCPRs set by the RWE event for cycle 5. exposures ≥2200 MWD/MT.

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	able 2-2: Optic					
<u>Terraiten i mani kanan dalam mbaki kanan dala ni sundern</u>		ble Reference Nu		an 798 and a substance of the second	and a set of a party of the party of the	
PROFILE OF			Cycle Expos	sure Range <sup>(3)</sup>	di ang kang kang kang kang kang kang kang	
EOOS Combination <sup>[2]</sup>	Fuel Type	<2200 MWD/MT	≥2200 MWD/MT & <eor<sup>(!]-2128 MWD/MT</eor<sup>	MWD/MT&	≥EOR <sup>t‼</sup> (Coastdown)	
	GE14	1.44	1.66	1.66	1.66	
Base Case	ATRIUM-9B	1.44	1.66	1.66	1.66	
	GE14	1.45	1.67	1.67	1.67	
Base Case SLO	ATRIUM-9B	UM-9B 1.45 1.67 1.67		1.67		
	GE14	1.44	1.66	1.66	1.66	
FWHOOS/FFWTR	ATRIUM-9B	1.44	1.66	1.66	1.66	
FWHOOS/FFWTR SLO	GE14	1.45	1.67	1.67	1.67	
FVVHUUS/FFVVIR SLU	ATRIUM-9B	1.45	1.67	1.67	1.67	
TBPOOS <sup>[2]</sup>	GE14	1.55	1.66	1.66	1.66	
100000	ATRIUM-9B	1.51	1.66	1.66	1.66	
TBPOOS SLO <sup>[2]</sup>	GE14	1.56	1.67	1.67	1.67	
IBF0033L0	ATRIUM-9B	1.52	1.67	<u> </u>	1.67	
TCV Slow Closure	GE14	1.44	1.66	1.66	1.66	
TCV Slow Closure	ATRIUM-9B	1.44	1.66	1.66	1.66	
TCV Slow Closure SLO	GE14	1.45	1.67	1,67	1.67	
	ATRIUM-9B	1.45	1.67	1.67 1.67		
PLUOOS	GE14	1.47	1.66	1.66	1.66	
FL0003	ATRIUM-9B	. 1.44	1.66	1.66	1.66	
PLUOOS SLO	GE14	1.48	1.67	1.67	1.67	
	ATRIUM-9B	1.45	1.67	1.67	1.67	
TCV Stuck Closed	GE14	1.44	1.66	1.66	1.66	
	ATRIUM-9B	1.44	1.66	1.66	1.66	
TCV Stuck Closed SLO	GE14	1.45	1.67	1.67	1.67	
	ATRIUM-9B	1.45	1.67	1.67	1.67	

Notes for Table 2-2:
 EOR refers to the end of rated power operation – the all-rods-out condition at 100% rated power and 100% rated flow.
 All EOOS combinations presented here, except for the BASE CASE and BASE CASE SLO, account for both normal feedwater temperature operation and operation with FFWTR/FHOOS.
 All EOOS combinations have their Option B OLMCPRs set by the RWE event for cycle exposures ≥2200 MWD/MT.

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The second second second second second		App		eference		and a second		1.0.00 MA		
EOOS	Core Flow			Co	THE SHOP STORY DR	and state of the second	er (% Rát	ed) (		
Combination	(% Rated)	0.,	25	38.5	38.5	45	60 🖓	70	70 💥	≥10
國國國際國際		Operati	ng Limit	MCPR <sup>III</sup>		perating	Limit M	CPR Mult	iplier, K <sub>P</sub>	1.50
Base Case	≤60	3.16	2.58	2.27	1.32	1.28	1.15	N/A	N/A	1.00
Dase Case	>60	3.77	2.99	2.56	1.52	1.20	1.15			1.00
Base Case SLO	≤60	3.17	2.59	2.28	1.32	1.28	1.15	N/A	N/A	1.00
	>60	3.78	3.00	2.57	1.32	1.20	1.15	N/A	NWA -	1.0
FWHOOS/FFWTR	<sup>∶</sup> ≤60	<b>3.16</b> ∙	2.58	2.27	1 22	1.28	1.15	N/A	N/A	4.00
	:⇒60	. 3.77	2.99	2.56	1.32	1.20	1.13			1.00
FWHOOS/FFWTR	≤60	3.17	2.59	2.28	1 22	1.70	4.4 5	N/A	N/A	
SLO :	>60	3.78	3.00	2.57	1.32	1.28	1,15		- WA	1.00
TBPOOS	≤60	5.55	3.77	2.82	1.37	1.37 1.28	1.15	N/A	N/A	4.00
	>60	6.79	4.62	3.45		1.20	1.15		WA	1.00
TBPOOS SLO	≤60	5.56	3.78	2.83	1.37	1.28	1.15	Ñ/A	N/A	1.00
	>60	6.80	4.63	3.46		1.20	1.15		10/A	1.00
TCV Slow Closure	≤60	5.55	3.77	2.82	1.64	-N/A	1.45	1.26	1.11	1.00
	>60	6.79	4.62	3.45	1,04		1.45	1.20		1.0
TCV Slow Closure	≤60	5.56	3.78	2.83	1.64	N/A	1.45	1.26	1.11	1.00
SLO	>60	6.80	4.63	3.46	1.04		1.40	1.20		· 1.00
PLUOOS	≤60	5.55	3.77	2.82	1.64	N/A	1.45	1.26	1.11	1.00
. 20000	>60	6.79	4.62	3.45			1.70	1.20	1.11	1.00
PLUOOS SLO	≤60	5.56	3.78	2.83	1.64	N/A	1.45	1.26	1.11	1.00
. 20000 020	>60	6.80	4.63	3.46			1	1.20	1.17	1.00
CV Stuck Closed	≤60	3.16	2.58	2.27	1.32	1.28	1.15	N/A	N/A	1.00
	>60	3.77	2.99	2.56		1.20				1.00
CV Stuck Closed	_≤60	3.17	2.59	2.28	1.32	1.28	1.15	N/A	N/A	4.00
SLO <sub>.</sub>	· >60	3.78	3.00	2.57	1.52 1.28				1.00	

Values are to be linearly interpolated between listed core thermal power values.

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Table 2-4: Flow Depender	it OLMCPR (MCPR <sub>F</sub> ) for All Fuel Types
and All Operating Conc	ditions Except TCV Stuck Closed <sup>[1,2]</sup>
Applicable Re	eference Number(s): 10, 3, 4
General Core Flow (% Rated)	
110.0	1.22
100.0	1.22
0.0	1.86

Notes for Table 2-4:

This table is not applicable to TCV Stuck Closed operating conditions. 1.

2. This table is applicable to both Manual Flow Control and Automatic Flow Control operation.

Values are to be linearly interpolated between listed core flow values. З.

Table 2-5: Flow Dependent OLM and TCV Stuck Closed	MCPR (MCPR <sub>F</sub> ) for All Fuel Types Operating Conditions <sup>(1/2)</sup>
	e Number(s): 10, 3, 4
Core Flow (% Rated)	
110.0	1.27
108.9	1.27
0.0	1.97

Notes for Table 2-5:

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- 1.
- This table is applicable to TCV Stuck Closed operating conditions only. This table is applicable to both Manual Flow Control and Automatic Flow Control operation. 2. 3.

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Values are to be linearly interpolated between listed core flow values.

		Applicable Referen	nce Number(s): 3,4		
<b>EXAMPLE EXAMP</b>		<b>JERIORI</b> AND A STREET	Cycle Expo	sure Range 🖅	Nicken (Constant)
EOOS Combination <sup>[2,3]</sup>	Fuel Type	<2200 MWD/MT	≥2200 MWD/MT & <eor<sup>11-2128 MWD/MT</eor<sup>	≥EOR <sup>[1]</sup> -2128 ≦ MWD/MT & <eor< th=""><th>≥EOR<sup>[1]</sup> (Coastdown)</th></eor<>	≥EOR <sup>[1]</sup> (Coastdown)
	GE14	1.73	1.86	1.86	1.86
Base Case	ATRIUM-9B	1.70	1.86	1,86	1.86

Operation in Automatic Flow Control mode with TCV Slow Closure, TCV Stuck Closed, or PLUOOS is not an allowed condition.

3 Operation in Automatic Flow Control mode with an MSIVOOS or a pressure regulator OOS is not an allowed condition.

		Applica	able Refere	nce Number(	s): <u>4, 3</u>			
	Core	Core Thermal Power (% Rated)						
EOOS Combination <sup>[1,3]</sup>	Flow	0.44	25	38.5	38.5	-1¥45 1	60	≥100
	(% Rated)	Opera	ting Limit I	ИСРВ	Operati	ng Limit M(	CPR Multip	ier, K <sub>P</sub> l <sup>2</sup>
Base Case	≤60	3.16	2.58	2.27	1.32	1.28	1 45	1.00
	>60	3.77	2.99	2.56	1.52	1.20	1.15	1.00
otes for Table 2-7:	<u>,                                     </u>						s is not an allo	L

# 3. Linear Heat Generation Rate

# 3.1 Technical Specification Reference

Section 3.2.3.

## 3.2 Description

The linear heat generation rate (LHGR) limit is the product of the LHGR limit from Tables 3-1, 3-2, 3-3 or 3-4 (depending of the fuel type) and the minimum of either the power dependent LHGR multiplication factor, LHGRFAC<sub>P</sub>, the flow dependent LHGR multiplication factor, LHGRFAC<sub>F</sub> or the single loop operation (SLO) multiplication factor. The applicable LHGRFAC<sub>P</sub> limit is to be determined from Table 3-5 or Table 3-8 depending on the flow control mode in use. The applicable LHGRFAC<sub>F</sub> limit is to be determined from Table 3-5 or Table 3-8 depending on the flow control mode in use. The applicable LHGRFAC<sub>F</sub> limit is to be determined from Table 3-6 or 3-7, depending on the EOOS status. The SLO multiplication factor can be found in Table 3-9.

GE14-P10DNAB411-14GZ-1	00T-145-T6-2564 (Type 16)
Nodal Exposure (GWD/MT)	
0.00	13.40
12.50	13.40
15.20	13.05
24.00	11.95
47.00	9.10
56.25	8.00
62.85	5.00

1. Values are to be linearly interpolated between listed nodal exposure values.

	Z-100T-145-T6-2565 (Type 17)
Nodal Exposure (GWD/MT)	
0.00	13.40
12.50	13.40
15.00	13.05
18.70	12.60
27.50	11.50
56.00	8.00
62.50	5.00

GE14-P10DNAB194-4G7:0-100T-145-T6-2647 (Type 1) Applicable Reference Number(s): 15				
Nodal Exposure (GWD/MT)	LHGR Limit (kW/ft) <sup>[1]</sup>			
0.00	13.40			
11.02	13.40			
13.22	12.91			
16.53	12.91			
55.11	8.20			
60.62	5.62			
61.71	5.00			

1. Values are to be linearly interpolated between listed nodal exposure values.

Table 3-4: LHGR Limits for ATRM9-P9DATB348-11G6.5-SPC100T-9V	Bundle Types VR-144-T6-2444 (Type 5) and
ATRM9-P9DATB360-11G6.5-SPC100T-	9WR-144-T6-2445 (Type 7)
Applicable Reference Nun	nber(s): 9
Nodal Exposure (GWD/MT)	LHGR Limit (kW/ft)
0.00	14.40
15.00	14.40
64.30	7.90
Notes for Table 3-4: 1. Values are to be linearly interpolated between listed nodal exposure	values

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The state of the second se	a the second state of Press	Appli	cable Refe	erence Nur					
		Core Thermal Power (% Rated)							
EOOS Combination	Core Flow (% Rated)		25	38.5	38.5	70	70		ં≓≥100
	NET: MR	1.545416	analisi	建设部门	IGRFAC	Multiplier	[1,2] 		<b>Fishers</b>
Base Case	All	0.50	0.56	0.59	0.68	N/A	N/A	0.86	1.00
Base Case SLO	All	0.50	0.56	0.59	0.68	N/A	N/A	0.86	1.00
FWHOOS/FFWTR	All	0.50	0.56	0.59	0.68	N/A .	N/A	0.86	1.00
FWHOOS/FFWTR SLO	All	0.50	0.56	0.59	0.68	N/A	N/A .	0.86	1.00
TBPOOS	≤60	0.22	0.39	0.48	0.54	 N/A	N/A	N/A	4.00
	>60	0.33	0.39	0.42	0.54	N/A	N/A	N/A	1.00
	≤60	0.22	0.39	0.48	0.54	N/A	N/A	N/A	1.00
TBPOOS SLO	>60	0.33	0.39	0.42		N/A			
TCV Slow Closure	≤60	0.22	0.39	0.48	0.54	0.73	0.78	N/A	1.00
TCV Slow Closule	>60	0.33	0.39	. 0.42	0.04	54 0.73	0.78		1.00
TCV Slow Closure	≤60	0.22	0:39	0.48	0.54	0.54 0.73	0.78 N/A	AI/A	1.00
SLO	>60	0.33	0.39	0.42	0.54	0.75		. N/A	1.00
PLUOOS	≤60	0.22	0.39	0.48	0.54	0.54 0.73	0.78 N/A	4.00	
F20003	>60	0.33	0.39	0.42	0.54	0.75	0.70		1.00
PLUOOS SLO	≤60	0.22	0.39	0.48	0.54	0.73	0.78	N/A	1.00
	>60	0.33	0.39	0.42		0.15	0.70		1.00
TCV Stuck Closed	All	0.50	0.56	0.59	0.68	N/A	N/A	0.86	1.00
TCV Stuck Closed SLO	All	0.50	0.56	0.59	0.68	N/Ă	N/A	0.86	1.00

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Notes for Table 3-5:
Values are to be linearly interpolated between listed core power values.
The LHGR multiplier for any core power/flow condition is the limiting of the LHGRFAC<sub>P</sub>, LHGRFAC<sub>P</sub>, and SLO Multiplier (if applicable).

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Applicable Reference Number(s): 4, 3					
Core Flow (% Rated)					
0.0	0.28				
30.0	0.55				
40.0	0.64				
50.0	0.77				
80.0	1.00				
≥100.0	1.00				

This table is not applicable to TCV Stuck Closed operating conditions. 1.

2. This table is applicable to both Manual Flow Control and Automatic Flow Control operation.

Values are to be linearly interpolated between listed core flow values.

3. 4. The LHGR multiplier for any core power/flow condition is the limiting of the LHGRFAC<sub>P</sub>, LHGRFAC<sub>P</sub>, and SLO Multiplier (if applicable).

Table 3-7: LHGRFAC <sub>F</sub> Multipliers for TCV Stuck Closed Conditions <sup>[1,3]</sup>						
Applicable Reference Number(s): 4						
Core Flow (% Rated)						
0.0	0.14					
30.0	0.41					
40.0	0.50					
50.0	0.63					
80.0	0.86					
98.3	1.00					
≥100.0	1.00					
Notes for Table 3-7:						

This table is applicable to TCV Stuck Closed operating conditions only. 1

Values are to be linearly interpolated between listed core flow values. 2.

З. This table is applicable to both Manual Flow Control and Automatic Flow Control operation.

4. The LHGR multiplier for any core power/flow condition is the limiting of the LHGRFACr, LHGRFACr, and SLO Multiplier (if applicable)

Table 3-8: LHGRFACP Multipliers for Automatic Flow Control						
Applicable Reference Number(s): 4						
Core Thermal Power (% Rated)						
0.0	0.00					
50.0	0.50					
≥100.0	1.00					
Nator for Table 2.9						

Notes for Table 3-8:

Values are to be linearly interpolated between listed core flow values. 1.

The LHGR multiplier for any core power/flow condition is the limiting of the LHGRFACP, LHGRFACF, and SLO Multiplier (if 2. applicable).

Applicable Refere	or All Fuel Types
Fuel Product Line Market	
ATRIUM-9B	0.84
GE14	0.77

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# 4. Control Rod Withdrawal Block Instrumentation

# 4.1 Technical Specification Reference

Table 3.3.2.1-1

## 4.2 Description

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The rod block monitor upscale instrumentation setpoints are determined from the relationships shown below (Reference 6).

Table 4-1: Rod Block Monitor Upscale Instrumentation Setpoints <sup>(3)</sup>						
Applicable Reference Number(s): 6						
Rod Block Monitor	Allowable Value <sup>[1,2]</sup>					
Upscale Trip Function						
Two Recirculation Loop Operation	0.65 W <sub>d</sub> + 56.1%					
Single Recirculation Loop Operation	0.65 W <sub>d</sub> + 51.4%					
Notes for Table 4-1:	e la companya de la c					
1. Wd - percent of recirculation loop drive flow required to proc						
<ol><li>The setpoint may be lower or higher and still comply with the</li></ol>	e rod withdrawal event (RWE) licensing analysis because the					
RWE is analyzed for unblocked conditions.						
<ol> <li>The allowable value is clamped with a maximum value not to of 100%.</li> </ol>	o exceed the allowable value for a recirculation loop drive flow					

#### **Allowed Modes of Operation** 5.

#### 5.1 **Technical Specification Reference**

Bases Sections 3.2.2, 3.2.3, and 3.7.7

#### Description 5.2

The Allowed Modes of Operation with combinations of Equipment Out-of-Service are as described below:

	ble 5-1: Allowe icable Reference Nu		eration	
ine man bis bis a Campain orthogonal research the month because the		Operatin		<b>MARK TRANSPORT</b>
EOOS Combinations <sup>[1,2,3]</sup>	Standard	CALIFIC FIELD		Coastdown <sup>[4]</sup>
Base Case	Yes	Yes	Yes	Yes
Base Case SLO	Yes	Yes	Yes	Yes
FWHOOS/FFWTR	Yes	Yes	Yes	Yes
FWHOOS/FFWTR SLO	Yes	Yes	Yes	Yes
TBPOOS	Yes	Yes	Yes	Yes
TBPOOS SLO	Yes	Yes	Yes	Yes
TCV Slow Closure <sup>[6]</sup>	Yes	Yes	∴Yes	Yes
TCV Slow Closure <sup>[6]</sup> SLO	Yes	Yes	Yes	Yes
PLUOOS <sup>[7]</sup>	Yes	Yes	Yes	Yes
PLUOOS SLO	Yes	Yes	Yes	Yes
TCV Stuck Closed	Yes	Yes	Yes	Yes
TCV Stuck Closed SLO	Yes	Yes	Yes	Yes
Notes for Table 5-1:		·	*-,_,	

1. Each OOS Option may be combined with up to 18 TIP channels OOS (provided the requirements for utilizing SUBTIP methodology are met) with all TIPS available at startup from a refuel outage and up to 50% of the LPRMs OOS with an LPRM calibration frequency of 2500 Effective Full Power Hours (EFPH) (2000 EFPH +25%). For operation under all EOOS limit sets a 120°F reduction in feedwater temperature throughout the cycle was analyzed (Final Feedwater Temperature Reduction was analyzed for the entire cycle).

A single MSIV may be taken OOS (shut) under any and all OOS Options except Automatic Flow Control, so long as core thermal power is maintained ≤75% of 2957 MWth (References 14 and 3).

All OOS Options support 1 Turbine Bypass Valve OOS, if the OPL-3 assumed opening profile for the Turbine Bypass 3. system is met. If the OPL-3 (References 7 and 8) opening profile is not met, or if more than one Turbine Bypass Valve is OOS, utilize the TBPOOS condition.

Coastdown operation is defined as any cycle exposure beyond the full power, all rods out condition with plant power slowly lowering to a lesser value while core flow is held constant (Reference 11 Section 4.3.1.2.8). Up to a 15% overpower is analyzed per Reference 4.

Increased Core Flow (ICF) is supported to 108% of rated core flow.

For operation with a pressure regulator out-of-service (PROOS), the TCV Slow Closure limits should be applied (Reference 6. 13) and the operational notes from Reference 13 reviewed. PROOS in conjunction with TCV Slow Closure is not an analyzed out-of-service combination.

7. If the Base Case limit set is being used and the PLU is taken OOS for a surveillance and the reactor is maintained at ≥80% rated core thermal power and ≥80% of rated core flow during the PLUOOS period, an administrative limit on FDLRX/MFLPD and MFLCPR can be used instead of the PLUOOS thermal limit set. The FDLRX/MFLPD administrative limit to be used is 0.98 for all scram speeds. The MFLCPR administrative limit is 0.93 for Option A scram times, 0.97 for Option B scram times, and 0.97 for scram times less than or equal to 0.731 seconds but greater than the Option B time. (Reference 16).

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# 6. Methodology References

The analytical methods used to determine the core operating limits shall be those previously reviewed and approved by the NRC (Technical Specification Section 5.6.5), specifically those described in the following documents:

- 1. ANF-1125 (P)(A) and Supplements 1 and 2, "Critical Power Correlation ANFB," April 1990.
- 2. ANF-524 (P)(A) Revision 2 and Supplements 1 and 2, "ANF Critical Power Methodology for Boiling Water Reactors," November 1990.
- 3. XN-NF-79-71 (P)(A) Revision 2 and Supplements 1, 2 & 3, "Exxon Nuclear Plant Transient Methodology for Boiling Water Reactors," March 1986.
- 4. XN-NF-80-19 (P)(A) Volume 1 Supplements 1 and 2, "Exxon Nuclear Methodology for Boiling Water Reactors Neutronic Methods for Design and Analysis," March 1993.
- 5. XN-NF-80-19 (P)(A) Volume 1 Supplement 3, Supplement 3 Appendix F, and Supplement 4, "Exxon Nuclear Methodology for Boiling Water Reactors," November 1990.
- 6. XN-NF-80-19 (P)(A) Volumes 2, 2A, 2B and 2C, "Exxon Nuclear Methodology for Boiling Water Reactors: EXEM BWR ECCS Evaluation Model," September 1982.
- 7. XN-NF-80-19 (P)(A) Volume 3 Revision 2, "Exxon Nuclear Methodology for Boiling Water Reactors, THERMEX: Thermal Limits Methodology Summary Description," January 1987.
- 8. XN-NF-80-19 (P)(A) Volume 4 Revision 1, "Exxon Nuclear Methodology for Boiling Water Reactors: Application of the ENC Methodology to BWR Reloads," June 1986.
- 9. XN-NF-85-67 (P)(A) Revision 1, "Generic Mechanical Design for Exxon Nuclear Jet Pump BWR Reload Fuel," September 1986.
- 10. ANF-913 (P)(A) Volume 1 Revision 1, and Volume 1 Supplements 2, 3, 4, "COTRANSA2: A Computer Program for Boiling Water Reactor Transients Analysis," August 1990.
- 11. XN-NF-82-06- (P)(A) Revision 1 and Supplements 2, 4 and 5, "Qualification of Exxon Nuclear Fuel for Extended Burnup," October 1986.
- 12. XN-NF-82-06- (P)(A) Supplement 1 Revision 2, "Qualification of Exxon Nuclear Fuel for Extended Burnup Supplement 1 Extended Burnup Qualification of ENC 9x9 BWR Fuel," May 1988.
- ANF-89-14(P)(A) Revision 1 and Supplements 1 & 2, "Advanced Nuclear Fuels Corporation Generic Mechanical Design for Advanced Nuclear Fuels Corporation 9X9 – IX and 9x9 – 9X BWR Reload Fuel," October 1991.
- 14. ANF-89-98 (P)(A), "Generic Mechanical Design Criteria for BWR Fuel Designs," Revision 1 and Revision 1 Supplement 1, May 1995.
- 15. ANF-91-048 (P)(A), "Advanced Nuclear Fuels Corporation Methodology for Boiling Water Reactors EXEM BWR ECCS Evaluation Model," January 1993.

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- 16. Commonwealth Edison Company Topical Report NFSR-0091, "Benchmark of CASMO/ MICROBURN BWR Nuclear Design Methods," Revision 0 and Supplements on Neutronic Licensing Analysis (Supplement 1) and La Salle County Unit 2 benchmarking (Supplement 2), December 1991, March 1992, and May 1992, respectively.
- 17. EMF-85-74 (P) Revision 0 and Supplement 1(P)(A) and Supplement 2(P)(A), "RODEX2A (BWR) Fuel Rod Thermal-Mechanical Evaluation Model," February 1998.
- 18. NEDE-24011-P-A-14 Revision 14, "General Electric Standard Application for Reactor Fuel (GESTAR)," June 2000.
- 19. NEDC-32981P Revision 0, "GEXL96 Correlation for ATRIUM-9B Fuel", September 2000.
- 20. ANF-1125(P)(A), Supplement 1 Appendix E, "ANFB Critical Power Correlation Determination of ATRIUM-9B Additive Constant uncertainties," September 1998.
- 21. ANF-91-048(P)(A), Supplements 1 and 2, "BWR Jet Pump Model Revision for RELAX," October 1997.
- 22. Commonwealth Edison Topical Report NFSR-0085, Revision 0, "Benchmark of BWR Nuclear Design Methods," November 1990.
- 23. Commonwealth Edison Topical Report NFSR-0085, Supplement 1 Revision 0, "Benchmark of BWR Nuclear Design Methods Quad Cities Gamma Scan Comparisons," April 1991.
- 24. Commonwealth Edison Topical Report NFSR-0085, Supplement 2 Revision 0, "Benchmark of BWR Nuclear Design Methods Neutronic Licensing Analyses," April 1991.