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Nuclear

May 1, 2003

United States Nuclear Regulatory Commission Attention: Document Control Desk Washington, D.C. 20555

LaSalle County Station, Units 1 and 2 Facility Operating License Nos. NPF-11 and NPF-18

NRC Docket Nos. 50-373 and 50-374

Subject:

2002 Radioactive Effluent Release Report

Enclosed is the Exelon Generation Company, (EGC), LLC, LaSalle County Station 2002 Annual Radioactive Effluent Release Report. This report is submitted in accordance with Technical Specification 5.6.3, "Radioactive Effluent Release Report."

Should you have any questions concerning this letter, please contact Mr. Glen T. Kaegi, Regulatory Assurance Manager, at (815) 415-2800.

Respectfully,

Susan Landahl Plant Manager

LaSalle County Station

Susan Landal

**Attachment** 

cc: Regional Administrator - NRC Region III

NRC Senior Resident Inspector - LaSalle County Station

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#### Supplemental Information

#### 1. Regulatory Limits

#### a. Gaseous Effluents

- 1) The air dose due to noble gases released in gaseous effluents, from each reactor unit, from the site shall be limited to the following:
  - a) During any calendar quarter: Less than or equal to 5 mrad for gamma radiation and less than or equal to 10 mrad for beta radiation, and
  - b) During any calendar year: Less than or equal to 10 mrad for gamma radiation and less than or equal to 20 mrad for beta radiation.
- 2) The dose to an individual from radioiodines and radioactive materials in particulate form, and radionuclides, other than noble gases, with half-lives greater than eight days in gaseous effluents released, from each reactor unit, from the site shall be limited to the following:
- a) During any calendar quarter: Less than or equal to 7.5 mRems to any organ, and
  - b) During any calendar year: Less than or equal to 15 mRems to any organ.

#### b. Liquid Effluents

- 1) The dose or dose commitment to an individual from radioactive materials in liquid effluents released, from each reactor unit, from the site shall be limited:
  - a) During any calendar quarter: Less than or equal to 1.5 mRem to the total body and to less than or equal to 5 mRem to any organ, and
  - b) During any calendar year: Less than or equal to 3 mRem to the total body and to less than or equal to 10 mRem to any organ.

#### c. Total Dose -

1) The dose or dose commitment to any member of the public, due to releases or radioactivity and radiation, from uranium fuel cycle sources shall be limited to less than or equal to 25 mRem to the body or any organ (except the thyroid, which shall be limited to less than or equal to 75 mRem) over 12 consecutive months.

#### Supplemental Information (continued)

#### Allowable Concentrations –

#### a. Gaseous Effluents

- 1) The dose rate due to radioactive materials released in gaseous effluents from the site shall be limited to the following:
  - a) For noble gases: Less than or equal to 500 mRem/year to the total body and less than or equal to 3000 mRem/year to the skin, and
  - b) For all radioiodines and for all radioactive materials in particulate form, and radionuclides, other than noble gases, with half-lives greater than eight days: Less than or equal to 1500 mRem/year to any organ via the inhalation pathway.

#### b. Liquid Effluents

1) The concentration of radioactive material released from the site shall be limited to ten (10) times the concentrations specified in 10 CFR Part 20, Appendix B, Table II, Column 2 for radionuclides other than dissolved or entrained noble gases. For dissolved or entrained noble gases, the concentration shall be limited to the following:

Nuclide	DWC (μci/ml)
Kr-85m	2.00E-04
Kr-85	5.00E-04
Kr-87	4.00E-05
Kr-88	9.00E-05
Ar-41	7.00E-05
Xe-131m	7.00E-04
Xe-133m	5.00E-04
Xe-133	6.00E-04
Xe-135m	2.00E-04
Xe-135	2.00E-04

#### 3. Average Energy

Not applicable - average energy is no longer used to determine dose to the public.

#### 4. Measurements and Approximations of Total Radioactivity

#### a. Gaseous Effluents

- 1) Containment Vent and Purge System is sampled by grab sample which is analyzed for principal gamma emitters and H-3.
- 2) Main Vent Stack is sampled by grab sample, which is analyzed for principal gamma emitters and H-3.
- Standby Gas Treatment System is sampled by grab sample, which is analyzed for principal gamma emitters.

#### Supplemental Information (continued)

All release types as listed in 1 and 2 above, at the vent stack and as listed in 3 above, at the Standby Gas Treatment System whenever there is flow, are continuously sampled by charcoal cartridge and particulate filter paper, which are analyzed for iodines and principal gamma emitters. Particulate filter papers are composited and analyzed for gross alpha, Sr-89 and Sr-90. Noble gases, gross beta and gamma are continuously monitored by noble gas monitors for the vent stack and the standby gas treatment system.

#### b. Liquid Effluents

Gaseous

- 1) Batch waste release tanks are sampled each batch for principal gamma emitters, I-131, dissolved and entrained noble gases, H-3, gross alpha, Sr-89, Sr-90 and Fe-55.
- 2) Continuous releases are sampled continuously in proportion to the rate of flow of the effluent stream and by grab sample. Samples are analyzed for principal gamma emitters, I-131, dissolved and entrained noble gases, H-3, gross alpha, Sr-89, Sr-90 and Fe-55.

N/A

#### 5. Batch Releases

a.

1)	Number of batch releases:	None
2)	Total time period for batch releases:	N/A
3)	Maximum time period for a batch release:	N/A
4)	Average time period for batch releases:	N/A

Minimum time period for a batch release:

#### b. Liquid

5)

Liquid		
1)	Number of batch releases:	None
2)	Total time period for batch releases: Min.	N/A
3)	Maximum time period for a batch release: Min.	N/A
4)	Average time period for batch releases: Min.	N/A
5)	Minimum time period for a batch release: Min.	N/A
6)	Average stream flow during periods of release of effluent into a flowing stream: gpm	N/A

#### Supplemental Information (continued)

#### 6. Abnormal Releases

a. Gaseous

1) Number of releases: None

2) Total activity released: N/A

b. Liquid

1) Number of releases: None

2) Total activity released: N/A

#### 7. Process Control Program

There were no changes to the Process Control Program during this time period.

8. Effluent Monitoring Instrumentation timeclocks and sample anomalies.

There were no effluent monitoring instrumentation timeclocks exceeded during this time period.

During the reporting period, the Illinois Department of Nuclear Safety Effluent Monitoring Instrumentation was replaced. This activity involved the opening of a Station Vent Stack access hatch, which created a mixed mode release pathway. Dose calculations were performed for the pathway associated with this activity. The dose information for this pathway is included in the Annual Dose Report. Release activity information is included as the "Gaseous Effluent – Mixed Mode" summary under continuous releases.

During the reporting period, there was one case of loss of power and one case of inadequate flow to the Cooling Pond Blowdown Compositor. This compositor samples the Plant's ultimate outfall for liquid release. Composite samples are collected three times a week, with a weekly composite analyzed for gamma isotopic. There were no radioactive liquid releases conducted during the reporting period. Compensatory sampling was initiated for the low flow condition. For the case of loss of power, the compositor was shutdown for a period of two days without compensatory sampling. A review of historical isotopic and trending of future data ensured representative sampling for the composite samples that were obtained. A review of REMP data also ensured no resultant impact to offsite dose as measured in the environment. The loss of power was associated with a planned maintenance activity. The low flow condition was found to be due to a leak in the sample pump tubing. Both cases were identified and incorporated into the Corrective Actions Program.

#### Supplemental Information (continued)

9. Offsite Dose Calculation Manual Revisions.

An entire copy of the ODCM LaSalle Annex is submitted in accordance with Technical Specification 5.5.1 (refer to Appendix A). Following are change summaries for Rev. 4 and Rev. 5.

Rev 4 changes

- Section 10.1.3.1.2 is in error as it states the following: "The high trip setpoint is established at 1.5 times the
  nominal nitrogen-16 (N-16) background dose rate to help ensure that effluents are maintained ALARA."

  It has been corrected to read as follows: "The high trip setpoint is established at 1.5 times the normal full power
  background rate, including nitrogen-16 (N-16) to help ensure that effluents are maintained ALARA."
- 2. Reference change in ODCM section 10.1.3.1.2 from TS 3.11.2.2 to 3.7.6.

Rev 5 changes

- 1. Figure 10-1 entitled "Simplified Gaseous Radwaste Gaseous Effluent Flow Diagram" has been revised to remove the Turbine Building Sandblast Room from the flow path.
- 2. Table 11-1 and Table 12.5-1 have been revised to require an I-131 analysis for Food Products, which are sampled as part of the Radiological Environmental Monitoring Program.
- 3. Table 12.5-1 has been revised to require an I-131 analysis on each composite when the dose calculated for the consumption of water is greater than 1 mrem per year.
- 4. The evaporators, which at one time were used to process waste, have been abandoned in place per EC #331686 and safety screening L01-0427. ODCM Section 10.2.1, Figure 10-2, Figure 10-4, and Bases 12.3.3.C have been revised to remove the reference to the evaporators.
- 5. Table 11-1, Figure 11-3, and Table 12.5-1 has been revised to add a fish monitoring location for the LaSalle Lake.

#### LASALLE COUNTY NUCLEAR POWER STATION EFFLUENT AND WASTE DISPOSAL ANNUAL REPORT (2002) UNITS ONE AND TWO

### DOCKET NUMBERS 50-373 AND 50-374 GASEOUS EFFLUENTS-SUMMATION OF ALL RELEASES

					Estimated
Units	1st Qtr	2nd Qtr	3rd Qtr	4th Qtr	Total Error %

#### A. Fission and Activation Gas Releases

1. Total Release Activity	Ci	1.31E+03	5.96E+03	2.25E+03	3.77E+03	3.50E+01
2. Average Release Rate	uCi/sec	1.68E+02	7.57E+02	2.83E+02	4.74E+02	
3. Percent of Technical Specification Limit	%	*	*	*	*	

#### **B.** Iodine Releases

1. Total I-131 Activity	Ci	2.95E-02	4.42E-02	7.92E-02	1.63E-01	3.50E+01
2. Average Release Rate	uCi/sec	3.80E-03	5.63E-03	9.96E-03	2.05E-02	
3. Percent of Technical Specification Limit	%	*	*	*	*	

#### C. Particulate (> 8 day half-life) Releases

1. Gross Activity	Ci	6.69E-04	2.78E-03	1.53E-02	9.36E-03	3.30E+01
2. Average Release Rate	uCi/sec	8.60E-05	3.54E-04	1.92E-03	1.18E-03	
3. Percent of Technical Specification Limit	%	*	*	*	*	
3. Gross Alpha Activity	Ci	<1.00E-11	<1.00E-11	2.71E-05	1.87E-05	

#### D. Tritium Releases

1. Total Release Activity	Ci	3.84E+01	1.54E+01	2.55E+01	3.50E+01	2.10E+01
2. Average Release Rate	uCi/sec	4.93E+00	1.96E+00	3.21E+00	4.41E+00	
3. Percent of Technical Specification Limit	%	*	*	*	*	

<sup>&</sup>quot;\*" This information is contained in the Radiological Impact on Man section of the report.

<sup>&</sup>quot;<" Indicates activity of sample is less than LLD given in uCi/ml

#### LASALLE COUNTY NUCLEAR POWER STATION EFFLUENT AND WASTE DISPOSAL ANNUAL REPORT (2002) GASEOUS EFFLUENTS-ELEVATED RELEASE

Unit 1 and Unit 2 Continuous Mode

1st Qtr

2nd Qtr

1.01E-03 3.40E+00 6.78E-04

<1.00e-6 <1.00e-6 <1.00e-6 <1.00e-6

Units

Ci

1. Fission and Activation Gas Releases

Ar-41

Kr-85

3<sup>rd</sup> Qtr

4th Qtr

2.38E-02

Kr-85	l Ci	<1.00e-6	<1.00e-6	<1.00e-0	<b>~1.00e-6</b>
Kr-85m	Ci	3.19E+02	6.54E+02	5.39E+02	5.90E+02
Kr-87	Ci	5.08E+01	1.15E+02	9.24E+01	8.65E+01
Kr-88	Ci	4.40E+02	9.94E+02	7.76E+02	7.33E+02
Xe-131m	Ci	<1.00e-6	<1.00e-6	<1.00e-6	<1.00e-6
Xe-133	Ci	4.96E+02	3.00E+03	6.72E+02	1.30E+03
Xe-133m	Ci	<1.00e-6	7.80E+01	3.49E-04	2.00E-03
Xe-135	Ci	2.01E-03	1.01E+03	2.35E+01	7.78E+02
Xe-135m	Ci	<1.00e-6	1.04E+02	2.68E+01	2.84E+02
Xe-138	Ci	<1.00e-6	<1.00e-6	1.19E+02	4.53E+01
TOTAL	Ci	1.31E+03	5.96E+03	2.25E+03	3.82E+03
2. Iodine Releases					
I-131	Ci	2.95E-02	4.42E-02	7.92E-02	1.63E-01
I-132	Ci	7.77E-03	2.11E-02	5.68E-02	1.28E-01
I-133	Ci	3.09E-02	4.83E-02	1.25E-01	2.94E-01
1-134	Ci	<1.00e-11	<1.00e-11	<1.00e-11	<1.00e-11
I-135	Ci	1.97E-02	3.95E-02	9.94E-02	2.51E-01
TOTAL IODINE	Ci	8.79E-02	1.53E-01	3.60E-01	8.36E-01
TOTAL I-131, I-133, I-135	Ci	8.01E-02	1.32E-01	3.04E-01	7.08E-01
101711111111111111111111111111111111111		0.012 02		0.0 .2 0.	
3. Particulate ( > 8 day half-life) Re	leases				
Cr-51	Ci	<1.00e-11	<1.00e-11	<1.00e-11	<1.00e-11
Mn-54	Ci	2.32E-05	1.54E-05	2.40E-05	1.69E-04
Co-57	Ci	<1.00e-11	<1.00e-11	<1.00e-11	<1.00e-11
Fe-55	Ci	<1.00e-11	<1.00e-11	<1.00e-11	<1.00e-11
Co-58	Ci	<1.00e-11	<1.00e-11	<1.00e-11	<1.00e-11
Fe-59	Ci	<1.00e-11	<1.00e-11	<1.00e-11	<1.00e-11
Co-60	Ci	4.46E-04	1.62E-04	1.74E-04	6.19E-04
Zn-65	Ci	<1.00e-11	<1.00e-11	<1.00e-11	<1.00e-11
Sr-89	Ci	1.95E-04		3.27E-03	3.13E-03
Sr-90	Ci	4.05E-07	1.37E-06	3.70E-06	<1.00e-11
Zr-95	Ci	<1.00e-11	<1.00e-11	<1.00e-11	<1.00e-11
Mo-99	Ci	<1.00e-11	<1.00e-11	<1.00e-11	<1.00e-11
Ru-103	Ci	<1.00e-11	<1.00e-11	<1.00e-11	<1.00e-11
Sn-117m	Ci	<1.00e-11	<1.00e-11	<1.00e-11	<1.00e-11
Cs-134	Ci	4.62E-06		5.33E-04	1.20E-04
Cs-137	Ci	<1.00e-11	<1.00e-11	4.24E-04	1.08E-04
Ba\La-140	Ci	<1.00e-11	9.99E-04	5.72E-03	3.89E-03
Ce-141	Ci	<1.00e-11	8.49E-04	5.13E-03	1.32E-03
Ce-144	Ci	<1.00e-11	<1.00e-11	<1.00e-11	<1.00e-11
	Ci	6.69E-04		1.53E-02	9.36E-03
III AI AI PARIKIN AIRS		U.UUL-UT	F110F-00	1100-05	
TOTAL PARTICULATES					
4. Tritium Releases 1. Total Release Activity	Ci	3.84E+01	1.54E+01	2.55E+01	3.50E+01

#### LASALLE COUNTY NUCLEAR POWER STATION EFFLUENT AND WASTE DISPOSAL ANNUAL REPORT (2002) GASEOUS EFFLUENTS-MIXED MODE RELEASE

Unit 1 and Unit 2 Continuous Mode

	Units	1st Qtr	2nd Qtr	3 <sup>rd</sup> Qtr	4 <sup>th</sup> Qtr
. Fission and Activation Gas Releas	es Ci	<1.00e-6	<1.00e-6	<1.00e-6	<1.00e-6
Gr-85	Ci	<1.00e-6	<1.00e-6	<1.00e-6	<1.00e-6
Kr-85m	Ci	<1.00e-6	<1.00e-6	<1.00e-6	1.38E-01
ζr-87	Ci	<1.00e-6	<1.00e-6	<1.00e-6	2.37E-02
ζι-88	Ci	<1.00e-6	<1.00e-6	<1.00e-6	1.58E-01
Ke-131m	Ci	<1.00e-6	<1.00e-6	<1.00e-6	<1.00e-6
Ke-133	Ci	<1.00e-6	<1.00e-6	<1.00e-6	1.50E-01
Ke-133m	Ci	<1.00e-6	<1.00e-6	<1.00e-6	<1.00e-6
Ke-135	Ci	<1.00e-6	<1.00e-6	<1.00e-6	7.70E-05
Ke-135m	Ci	<1.00e-6	<1.00e-6	<1.00e-6	4.08E-02
Ke-138	Ci	<1.00e-6	<1.00e-6	<1.00e-6	<1.00e-6
	Ci	<1.00e-6	<1.00e-6	<1.00e-6	5.11E-01
TOTAL		1.006-0	<u> </u>	<u> </u>	0.112 01
2. Iodine Releases				14.00- 40	0.005.05
-131	Ci	<1.00e-12	<1.00e-12	<1.00e-12	2.36E-05
-132	Ci	<1.00e-11	<1.00e-11	<1.00e-11	2.69E-05
I-133	Ci	<1.00e-10	<1.00e-10	<1.00e-10	4.68E-05
[-134	Ci	<1.00e-11	<1.00e-11	<1.00e-11	<1.00e-11
-135	Ci	<1.00e-11	<1.00e-11	<1.00e-11	5.07E-05
TOTAL IODINE	Ci	<1.00e-11	<1.00e-11	<1.00e-11	1.48E-04
TOTAL I-131, I-133, I-135	Ci	<1.00e-11	<1.00e-11	<1.00e-11	1.21E-04
3. Particulate ( > 8 day half-life) Rel Cr-51	Ci	<1.00e-11	<1.00e-11	<1.00e-11	<1.00e-11
Mn-54		44.00-44	-4 00- 44		
	Ci	<1.00e-11	<1.00e-11	<1.00e-11	2.93E-07
Co-57	Ci	<1.00e-11	<1.00e-11	<1.00e-11 <1.00e-11	2.93E-07 <1.00e-11
Co-57 Fe-55	Ci Ci	<1.00e-11 <1.00e-11	<1.00e-11	<1.00e-11 <1.00e-11 <1.00e-11	2.93E-07 <1.00e-11 <1.00e-11
Co-57 Fe-55 Co-58	Ci Ci	<1.00e-11 <1.00e-11 <1.00e-11	<1.00e-11 <1.00e-11 <1.00e-11	<1.00e-11 <1.00e-11 <1.00e-11 <1.00e-11	2.93E-07 <1.00e-11 <1.00e-11
Co-57 Fe-55 Co-58 Fe-59	Ci Ci Ci Ci	<1.00e-11 <1.00e-11 <1.00e-11 <1.00e-11	<1.00e-11 <1.00e-11 <1.00e-11 <1.00e-11	<1.00e-11 <1.00e-11 <1.00e-11 <1.00e-11 <1.00e-11	2.93E-07 <1.00e-11 <1.00e-11 <1.00e-11
Co-57 Fe-55 Co-58 Fe-59 Co-60	Ci Ci Ci Ci	<1.00e-11 <1.00e-11 <1.00e-11 <1.00e-11 <1.00e-11	<1.00e-11 <1.00e-11 <1.00e-11 <1.00e-11 <1.00e-11	<1.00e-11 <1.00e-11 <1.00e-11 <1.00e-11 <1.00e-11 <1.00e-11	2.93E-07 <1.00e-11 <1.00e-11 <1.00e-11 <1.00e-11 2.93E-07
Co-57 Fe-55 Co-58 Fe-59 Co-60 Zn-65	Ci Ci Ci Ci Ci	<1.00e-11 <1.00e-11 <1.00e-11 <1.00e-11 <1.00e-11	<1.00e-11 <1.00e-11 <1.00e-11 <1.00e-11 <1.00e-11	<1.00e-11 <1.00e-11 <1.00e-11 <1.00e-11 <1.00e-11 <1.00e-11	2.93E-07 <1.00e-11 <1.00e-11 <1.00e-11 <1.00e-11 2.93E-07 <1.00e-11
Co-57 Fe-55 Co-58 Fe-59 Co-60 Zn-65	Ci Ci Ci Ci Ci Ci	<1.00e-11 <1.00e-11 <1.00e-11 <1.00e-11 <1.00e-11 <1.00e-11	<1.00e-11 <1.00e-11 <1.00e-11 <1.00e-11 <1.00e-11 <1.00e-11	<1.00e-11 <1.00e-11 <1.00e-11 <1.00e-11 <1.00e-11 <1.00e-11 <1.00e-11	2.93E-07 <1.00e-11 <1.00e-11 <1.00e-11 <1.00e-11 2.93E-07 <1.00e-11 3.77E-06
Co-57 Fe-55 Co-58 Fe-59 Co-60 Zn-65 Sr-89 Sr-90	Ci Ci Ci Ci Ci Ci	<1.00e-11 <1.00e-11 <1.00e-11 <1.00e-11 <1.00e-11 <1.00e-11 <1.00e-11 <1.00e-11	<1.00e-11 <1.00e-11 <1.00e-11 <1.00e-11 <1.00e-11 <1.00e-11 <1.00e-11	<1.00e-11 <1.00e-11 <1.00e-11 <1.00e-11 <1.00e-11 <1.00e-11 <1.00e-11 <1.00e-11	2.93E-07 <1.00e-11 <1.00e-11 <1.00e-11 <1.00e-11 2.93E-07 <1.00e-11 3.77E-06 2.26E-08
Co-57 Fe-55 Co-58 Fe-59 Co-60 Zn-65 Sr-89 Sr-90 Zr-95	Ci	<1.00e-11 <1.00e-11 <1.00e-11 <1.00e-11 <1.00e-11 <1.00e-11 <1.00e-11 <1.00e-11 <1.00e-11	<1.00e-11 <1.00e-11 <1.00e-11 <1.00e-11 <1.00e-11 <1.00e-11 <1.00e-11 <1.00e-11	<1.00e-11 <1.00e-11 <1.00e-11 <1.00e-11 <1.00e-11 <1.00e-11 <1.00e-11 <1.00e-11 <1.00e-11	2.93E-07 <1.00e-11 <1.00e-11 <1.00e-11 <1.00e-11 <2.93E-07 <1.00e-11 3.77E-06 2.26E-08 <1.00e-11
Co-57 Fe-55 Co-58 Fe-59 Co-60 Zn-65 Sr-89 Sr-90 Zr-95 Mo-99	Ci	<1.00e-11	<1.00e-11 <1.00e-11 <1.00e-11 <1.00e-11 <1.00e-11 <1.00e-11 <1.00e-11 <1.00e-11 <1.00e-11	<1.00e-11	2.93E-07 <1.00e-11 <1.00e-11 <1.00e-11 <1.00e-11 <1.00e-11 2.93E-07 <1.00e-11 3.77E-06 2.26E-08 <1.00e-11
Co-57 Fe-55 Co-58 Fe-59 Co-60 Zn-65 Sr-89 Sr-90 Zr-95 Mo-99 Ru-103	Ci	<1.00e-11	<1.00e-11	<1.00e-11	2.93E-07 <1.00e-11 <1.00e-11 <1.00e-11 <1.00e-11 2.93E-07 <1.00e-11 3.77E-06 2.26E-08 <1.00e-11 <1.00e-11 <1.00e-11
Co-57 Fe-55 Co-58 Fe-59 Co-60 Zn-65 Sr-89 Sr-90 Zr-95 Mo-99 Ru-103 Sn-117m	Ci	<1.00e-11	<1.00e-11	<1.00e-11	2.93E-07 <1.00e-11 <1.00e-11 <1.00e-11 <1.00e-11 2.93E-07 <1.00e-11 3.77E-06 2.26E-08 <1.00e-11 <1.00e-11 <1.00e-11 <1.00e-11
Co-57 Fe-55 Co-58 Fe-59 Co-60 Zn-65 Sr-89 Sr-90 Zr-95 Mo-99 Ru-103 Sn-117m Cs-134	Ci C	<1.00e-11	<1.00e-11	<1.00e-11	2.93E-07 <1.00e-11 <1.00e-11 <1.00e-11 <1.00e-11 2.93E-07 <1.00e-11 3.77E-06 2.26E-08 <1.00e-11 <1.00e-11 <1.00e-11 <1.00e-11 <1.00e-11
Co-57 Fe-55 Co-58 Fe-59 Co-60 Zn-65 Sr-89 Sr-90 Zr-95 Mo-99 Ru-103 Sn-117m Cs-134 Cs-137	Ci C	<1.00e-11	<1.00e-11	<1.00e-11	2.93E-07 <1.00e-11 <1.00e-11 <1.00e-11 <1.00e-11 2.93E-07 <1.00e-11 3.77E-06 2.26E-08 <1.00e-11 <1.00e-11 <1.00e-11 <1.00e-11 <1.00e-11 <1.00e-11
Co-57 Fe-55 Co-58 Fe-59 Co-60 Zn-65 Sr-89 Sr-90 Zr-95 Mo-99 Ru-103 Sn-117m Cs-134 Cs-137 Ba\La-140	Ci C	<1.00e-11	<1.00e-11	<1.00e-11	2.93E-07 <1.00e-11 <1.00e-11 <1.00e-11 <1.00e-11 <2.93E-07 <1.00e-1 3.77E-06 2.26E-08 <1.00e-1 <1.00e-1 <1.00e-1 <1.00e-1 <1.00e-1 <1.00e-1 <1.00e-1
Co-57 Fe-55 Co-58 Fe-59 Co-60 Zn-65 Sr-89 Sr-90 Zr-95 Mo-99 Ru-103 Sn-117m Cs-134 Cs-137 Ba\La-140 Ce-141	Ci C	<1.00e-11	<1.00e-11	<1.00e-11	2.93E-07 <1.00e-11 <1.00e-11 <1.00e-11 <1.00e-11 2.93E-07 <1.00e-11 3.77E-06 2.26E-08 <1.00e-11
Co-57 Fe-55 Co-58 Fe-59 Co-60 Zn-65 Sr-89 Sr-90 Zr-95 Mo-99 Ru-103 Sn-117m Cs-134 Cs-137 Ba\La-140 Ce-141 Ce-144	Ci C	<1.00e-11	<1.00e-11	<1.00e-11	2.93E-07 <1.00e-11 <1.00e-11 <1.00e-11 <1.00e-11 2.93E-07 <1.00e-11 3.77E-06 2.26E-08 <1.00e-11
Co-57 Fe-55 Co-58 Fe-59 Co-60 Zn-65 Sr-89 Sr-90 Zr-95 Mo-99 Ru-103 Sn-117m Cs-134 Cs-137 Ba\La-140 Ce-141 Ce-144	Ci C	<1.00e-11	<1.00e-11	<1.00e-11	2.93E-07 <1.00e-11 <1.00e-11 <1.00e-11 <1.00e-11 2.93E-07 <1.00e-11 3.77E-06 2.26E-08 <1.00e-11
Co-57 Fe-55 Co-58 Fe-59 Co-60 Zn-65 Sr-89 Sr-90 Zr-95 Mo-99 Ru-103 Sn-117m Cs-134 Cs-137 Ba\La-140 Ce-141 Ce-144 TOTAL PARTICULATES	Ci C	<1.00e-11	<1.00e-11	<1.00e-11	2.93E-07 <1.00e-11 <1.00e-11 <1.00e-11 <1.00e-11 2.93E-07 <1.00e-11 3.77E-06 2.26E-08 <1.00e-11
Co-57 Fe-55 Co-58 Fe-59 Co-60 Zn-65 Sr-89 Sr-90 Zr-95 Mo-99 Ru-103 Sn-117m Cs-134 Cs-137 Ba\La-140 Ce-141	Ci C	<1.00e-11	<1.00e-11	<1.00e-11	2.93E-07 <1.00e-11 <1.00e-11 <1.00e-11 <1.00e-11 2.93E-07 <1.00e-11 3.77E-06 2.26E-08 <1.00e-11 <1.00e-11 <1.00e-11 <1.00e-11 <1.00e-11 <1.00e-11 4.56E-06

<sup>&</sup>quot;<" Indicates activity of sample is less than LLD given in uCi/ml

# LASALLE COUNTY NUCLEAR POWER STATION EFFLUENT AND WASTE DISPOSAL ANNUAL REPORT (2002) LIQUID RELEASES UNIT 1 and UNIT 2

#### SUMMATION OF ALL LIQUID RELEASES

					Estimated
Units	1st Qtr	2nd Qtr	3rd Qtr	4th Qtr	Total Error %

#### A. Fission and Activation Products

1. Total Activity Released	Ci	<lld< th=""><th><lld< th=""><th><lld< th=""><th><lld< th=""><th>N/A</th></lld<></th></lld<></th></lld<></th></lld<>	<lld< th=""><th><lld< th=""><th><lld< th=""><th>N/A</th></lld<></th></lld<></th></lld<>	<lld< th=""><th><lld< th=""><th>N/A</th></lld<></th></lld<>	<lld< th=""><th>N/A</th></lld<>	N/A
2. Average Concentration Released	uCi/ml	<lld< td=""><td><lld< td=""><td><lld< td=""><td><lld< td=""><td></td></lld<></td></lld<></td></lld<></td></lld<>	<lld< td=""><td><lld< td=""><td><lld< td=""><td></td></lld<></td></lld<></td></lld<>	<lld< td=""><td><lld< td=""><td></td></lld<></td></lld<>	<lld< td=""><td></td></lld<>	
3. Percent of Applicable Limit	%	*	*	*	*	

#### B. Tritium

1. Total Activity Released	Ci	<lld< th=""><th><lld< th=""><th><lld< th=""><th><lld< th=""><th>N/A</th></lld<></th></lld<></th></lld<></th></lld<>	<lld< th=""><th><lld< th=""><th><lld< th=""><th>N/A</th></lld<></th></lld<></th></lld<>	<lld< th=""><th><lld< th=""><th>N/A</th></lld<></th></lld<>	<lld< th=""><th>N/A</th></lld<>	N/A
2. Average Concentration Released	uCi/ml	<lld< td=""><td><lld< td=""><td><lld< td=""><td><lld< td=""><td></td></lld<></td></lld<></td></lld<></td></lld<>	<lld< td=""><td><lld< td=""><td><lld< td=""><td></td></lld<></td></lld<></td></lld<>	<lld< td=""><td><lld< td=""><td></td></lld<></td></lld<>	<lld< td=""><td></td></lld<>	
3. Percent of Applicable Limit	%	*	*	*	*	

#### C. Dissolved Noble Gases

1. Total Activity Released	Ci	<lld< th=""><th><lld< th=""><th><lld< th=""><th><lld< th=""><th>N/A</th></lld<></th></lld<></th></lld<></th></lld<>	<lld< th=""><th><lld< th=""><th><lld< th=""><th>N/A</th></lld<></th></lld<></th></lld<>	<lld< th=""><th><lld< th=""><th>N/A</th></lld<></th></lld<>	<lld< th=""><th>N/A</th></lld<>	N/A
2. Average Concentration Released	uCi/ml	<lld< td=""><td><lld< td=""><td><lld< td=""><td><lld< td=""><td></td></lld<></td></lld<></td></lld<></td></lld<>	<lld< td=""><td><lld< td=""><td><lld< td=""><td></td></lld<></td></lld<></td></lld<>	<lld< td=""><td><lld< td=""><td></td></lld<></td></lld<>	<lld< td=""><td></td></lld<>	
3. Percent of Applicable Limit	%	*	*	*	*	

#### D. Gross Alpha

1. Total Activity Released (estimate)	Ci	<lld< th=""><th><lld< th=""><th><lld< th=""><th><lld< th=""><th>N/A</th></lld<></th></lld<></th></lld<></th></lld<>	<lld< th=""><th><lld< th=""><th><lld< th=""><th>N/A</th></lld<></th></lld<></th></lld<>	<lld< th=""><th><lld< th=""><th>N/A</th></lld<></th></lld<>	<lld< th=""><th>N/A</th></lld<>	N/A
2. Average Concentration Released	uCi/ml	<lld< td=""><td><lld< td=""><td><lld< td=""><td><lld< td=""><td></td></lld<></td></lld<></td></lld<></td></lld<>	<lld< td=""><td><lld< td=""><td><lld< td=""><td></td></lld<></td></lld<></td></lld<>	<lld< td=""><td><lld< td=""><td></td></lld<></td></lld<>	<lld< td=""><td></td></lld<>	
3. Percent of Applicable Limit	%	*	*	*	*	

E. Volume of Liquid Waste to Discharge	liters	0.00E+00	0.00E+00	0.00E+00	0.00E+00	N/A
F. Volume of Dilution Water	liters	0.00E+00	0.00E+00	0.00E+00	0.00E+00	N/A

<sup>&</sup>quot;\*" This information is contained in the Radiological Impact on Man section of the report.

<sup>&</sup>quot;<" Indicates activity of sample is less than LLD given in uCi/ml

# LASALLE COUNTY NUCLEAR POWER STATION EFFLUENT AND WASTE DISPOSAL ANNUAL REPORT (2002) LIQUID RELEASES UNIT 1 and UNIT 2 BATCH MODE

Nuclides From Batch Releases	Units	1st Qtr	2nd Qtr	3rd Qtr	4th Qtr
H-3	Ci	1	1	<u> </u>	}
Cr-51	Ci				
Mn-54	Ci	<b>†</b>			<u> </u>
Fe-55	Ci				
Co-58	Ci				
Fe-59	Ci				<u> </u>
Co-60	Ci				
Zn-65	Ci		-		
Sr-89	Ci				
Sr-90	Ci				<u> </u>
Nb-95	Ci				
Zr-95	Ci				
Mo-99	Ci				
Tc-99m	Ci				
Ag-110m	Ci				
Sb-122	Ci				
Sb-124	Ci				
I-131	Ci				
Cs-134	Ci				
Cs-137	. Ci	<u> </u>			
Ba\La-140	Ci				
Ce-141	Ci				
Ce-144	Ci				
W-187	Ci				
TOTAL	Ci	None	None	None	None
Xe-131m	Ci				
Xe-133	Ci				
Xe-133m	Ci				
Xe-135	Ci				
Xe-135m	Ci				
TOTAL	Ci	None	None	None	None

<sup>&</sup>quot;<" Indicates activity of sample is less than LLD given in uCi/ml

# LASALLE COUNTY NUCLEAR POWER STATION EFFLUENT AND WASTE DISPOSAL ANNUAL REPORT (2002) LIQUID RELEASES UNIT 1 and UNIT 2 CONTINUOUS MODE

Nuclides From Continuous Releases	Units	1st Qtr	2nd Qtr	3rd Qtr	4th Qtr
	1 0:	L 41 00E 07	41 00E 07	<1.00E.07	<1.00E.07
Gross Alpha	Ci	<1.00E-07		<1.00E-07	<1.00E-07
H-3	Ci	<1.00E-05	<1.00E-05	<1.00E-05	<1.00E-05
Cr-51	Ci	<5.00E-07		<5.00E-07	<5.00E-07
Mn-54	Ci	<5.00E-07	<5.00E-07	<5.00E-07	<5.00E-07
Fe-55	Ci	<1.00E-06	<1.00E-06	<1.00E-06	<1.00E-06
Co-58	Ci	<5.00E-07	<5.00E-07	<5.00E-07	<5.00E-07
Fe-59	Ci	<5.00E-07	<5.00E-07	<5.00E-07	<5.00E-07
Co-60	Ci	<5.00E-07		<5.00E-07	<5.00E-07
Zn-65	Ci	<5.00E-07	<5.00E-07	<5.00E-07	<5.00E-07
Sr-89	Ci	<5.00E-08	<5.00E-08	<5.00E-08	<5.00E-08
Sr-90	Ci	<5.00E-08	<5.00E-08	<5.00E-08	<5.00E-08
Nb-95	Ci	<5.00E-07	<5.00E-07	<5.00E-07	<5.00E-07
Zr-95	Ci	<5.00E-07	<5.00E-07	<5.00E-07	<5.00E-07
Mo-99	Ci	<5.00E-07	<5.00E-07	<5.00E-07	<5.00E-07
Tc-99m	Ci	<5.00E-07	<5.00E-07	<5.00E-07	<5.00E-07
Ag-110m	Ci	<5.00E-07	<5.00E-07	<5.00E-07	<5.00E-07
Sb-122	Ci	<5.00E-07	<5.00E-07	<5.00E-07	<5.00E-07
Sb-124	Ci	<5.00E-07	<5.00E-07	<5.00E-07	<5.00E-07
I-131	Ci	<1.00E-06	<1.00E-06	<1.00E-06	<1.00E-06
Cs-134	Ci	<5.00E-07	<5.00E-07	<5.00E-07	<5.00E-07
Cs-137	Ci	<5.00E-07	<5.00E-07	<5.00E-07	<5.00E-07
Ba\La-140	Ci	<5.00E-07	<5.00E-07	<5.00E-07	<5.00E-07
Ce-141	Ci	<5.00E-07	<5.00E-07	<5.00E-07	<5.00E-07
Ce-144	Ci	<5.00E-07	<5.00E-07	<5.00E-07	<5.00E-07
W-187	Ci	<5.00E-07	<5.00E-07	<5.00E-07	<5.00E-07
TOTAL	Ci	<lld< td=""><td><lld< td=""><td><lld< td=""><td><lld< td=""></lld<></td></lld<></td></lld<></td></lld<>	<lld< td=""><td><lld< td=""><td><lld< td=""></lld<></td></lld<></td></lld<>	<lld< td=""><td><lld< td=""></lld<></td></lld<>	<lld< td=""></lld<>
Xe-131m	Ci	<1.00E-05	<1.00E-05	<1.00E-05	<1.00E-05
Xe-133	Ci	<1.00E-05	<1.00E-05	<1.00E-05	<1.00E-05
Xe-133m	Ci	<1.00E-05	<1.00E-05	<1.00E-05	<1.00E-05
Xe-135	Ci	<1.00E-05	<1.00E-05	<1.00E-05	<1.00E-05
Xe-135m	Ci	<1.00E-05	<1.00E-05	<1.00E-05	<1.00E-05
TOTAL	Ci	<lld< td=""><td><lld< td=""><td><lld< td=""><td><lld< td=""></lld<></td></lld<></td></lld<></td></lld<>	<lld< td=""><td><lld< td=""><td><lld< td=""></lld<></td></lld<></td></lld<>	<lld< td=""><td><lld< td=""></lld<></td></lld<>	<lld< td=""></lld<>

<sup>&</sup>quot;<" Indicates activity of sample is less than LLD given in uCi/ml

SOLID WASTE AND IRRADIATED FUEL SHIPMENTS

#### EFFLUENT AND WASTE DISPOSAL ANNUAL REPORT (2002) SOLID WASTE AND IRRADIATED FUEL SHIPMENTS FIRST QUARTER

LSA

### A. SOLID WASTE SHIPPED OFFSITE FOR BURIAL OR DISPOSAL

1.	Spent resins, filter sludges,
	evaporator bottoms, etc.

2.

a.	Quantity shippe	d cu.m.		0.00E+00
b.	Total activity	Ci		0.00E+00
c.	Major nuclides (	(estimate %)		N/A
d.	Shipment type			N/A
e.	Solidification ag	gent		None
	mpressible waste, ninated equipment,	etc.		
a.	Quantity shippe	d cu.m.		4.40E+02
b.	Total activity	Ci		2.65E+01
c.	Major nuclides	(estimate %)		
		Mn-54 Fe-55 Co-60 Ni-63 Zn-65	1.17E+01 1.37E+01 4.52E+01 2.06E+01 7.13E+00	

Shipment type

d.

#### EFFLUENT AND WASTE DISPOSAL ANNUAL REPORT (2002) SOLID WASTE AND IRRADIATED FUEL SHIPMENTS FIRST QUARTER

3.	Other
----	-------

a.	Quantity shipped cu.m.	0.00E+00
b.	Total activity Ci	0.00E+00
c.	Major nuclides (estimate %)	N/A
d.	Shipment type	N/A

#### 4. Irradiated Components

a.	Quantity shipped cu.m	0.00E+00
b.	Total activity Ci	0.00E+00
c.	Major nuclides (estimate %)	N/A
d.	Number of shipments	0
e.	Mode of Transportation	N/A
f.	Destination	N/A

#### 5. Solid Waste Disposition

	Number of Shipments	Transportation Mode	<u>Destination</u>
	7	Truck	Duratek- Bear Creek, TN
ADTED	7		

TOTAL THIS QUARTER

Estimated total error % for spent resins, filter sludges, evaporator bottoms, etc. (Jan-Dec) 2.50E+01

Estimated total error % for dry compressible waste, contaminated equipment, etc. (Jan-Dec) 2.50E+01

Estimated total error % for irradiated components (Jan-Dec) N/A

#### B. IRRADIATED FUEL SHIPMENTS

None

#### EFFLUENT AND WASTE DISPOSAL ANNUAL REPORT (2002) SOLID WASTE AND IRRADIATED FUEL SHIPMENTS SECOND QUARTER

#### A. SOLID WASTE SHIPPED OFFSITE FOR BURIAL OR DISPOSAL

1. Spent resins, filter sludges, evaporator bottoms, etc.

d.

Shipment type

	-				
	a.	Quantity shipped	cu.m.		4.84E+00
	b.	Total activity	Ci		6.79E+01
	C.	Major nuclides (estin	mate %)		
			Mn-54	5.52E+00	
			Fe-55	7.15E+01	
			Co-60	1.40E+01	
			Zn-65	3.45E+00	
	d.	Shipment type			LSA
	e.	Solidification ag	ent		None
		•			•
2.		compressible waste, aminated equipment,	etc.		
	a.	Quantity shipped	l cu.m.		3.26E+02
	b.	Total activity	Ci		4.09E-01
	c.	Major nuclides (	estimate %)		
			Mn-54	1.17E+01	
			Fe-55	1.37E+01	
			Co-60	4.52E+01	
			Ni-63	2.06E+01	
			Zn-65	7.13E+00	

LSA

#### EFFLUENT AND WASTE DISPOSAL ANNUAL REPORT (2002) SOLID WASTE AND IRRADIATED FUEL SHIPMENTS SECOND QUARTER

a.	Quantity shipped cu.m.	0.00E+00
b.	Total activity Ci	0.00E+00
c.	Major nuclides (estimate %)	N/A
d.	Shipment type	N/A

#### 4. Irradiated Components

a.	Quantity shipped cu.m	0.00E+00
b.	Total activity Ci	0.00E+00
c.	Major nuclides (estimate %)	N/A
d.	Number of shipments	N/A
e.	Mode of Transportation	N/A
f.	Destination	N/A

#### 5. Solid Waste Disposition

	Number of Shipments	I ransportation Mode	Destination
	6	Truck	Duratek-Bear Creek, TN
	1	Truck	Envirocare of Utah
TOTAL THIS QUARTER	7		

Estimated total error % for spent resins, filter sludges, evaporator bottoms, etc. (Jan-Dec) 2.50E+01

Estimated total error % for dry compressible waste, contaminated equipment, etc. (Jan-Dec) 2.50E+01

Estimated total error % for irradiated components (Jan-Dec) N/A

#### B. IRRADIATED FUEL SHIPMENTS

None

#### EFFLUENT AND WASTE DISPOSAL ANNUAL REPORT (2002) SOLID WASTE AND IRRADIATED FUEL SHIPMENTS THIRD QUARTER

LSA

#### A. SOLID WASTE SHIPPED OFFSITE FOR BURIAL OR DISPOSAL

1. Spent resins, filter sludges, evaporator bottoms, etc.

2.

d.

Shipment type

a.	Quantity shipped	cu m		1.99E+01
a.	Quantity simpped	Cu.III.		1,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,
b.	Total activity	Ci		1.02E+02
c.	Major nuclides (es	stimate %)		
		Mn-54 Fe-55 Co-60 Zn-65	5.52E+00 7.15E+01 1.40E+01 3.45E+00	
d.	Shipment type			LSA
f.	Solidification age	nt		N/A
	npressible waste, nated equipment, e	tc.		
a.	Quantity shipped	cu.m.		1.14E+02
b.	Total activity	Ci		2.22E+00
c.	Major nuclides (e	stimate %)		
		Mn-54 Fe-55 Co-60 Ni-63 Zn-65	1.17E+01 1.37E+01 4.52E+01 2.06E+01 7.13E+00	

#### EFFLUENT AND WASTE DISPOSAL ANNUAL REPORT (2002) SOLID WASTE AND IRRADIATED FUEL SHIPMENTS THIRD QUARTER

~	Other
•	Chilei

a.	Quantity shipped cu.m.	0.00E+00
b.	Total activity Ci	0.00E+00
c.	Major nuclides (estimate %)	N/A
d.	Shipment type	N/A
Irradi	iated Components	

#### 4.

a.	Number of shipments	0
b.	Mode of Transportation	N/A
c.	Destination	N/A

#### Solid Waste Disposition 5.

	Number of Shipments	Transportation Mode	<u>Destination</u>
	3	Truck	Duratek-Bear Creek, TN
	4	Truck	Envirocare of Utah
TOTAL THIS QUARTER	7		

Estimated total error % for spent resins, filter sludges, evaporator bottoms, etc. (Jan-Dec) 2.50E+01 Estimated total error % for dry compressible waste, contaminated equipment, etc. (Jan-Dec) 2.50E+01 Estimated total error % for irradiated components (Jan-Dec) N/A

#### IRRADIATED FUEL SHIPMENTS В.

None

#### EFFLUENT AND WASTE DISPOSAL ANNUAL REPORT (2002) SOLID WASTE AND IRRADIATED FUEL SHIPMENTS FOURTH QUARTER

LSA

#### A. SOLID WASTE SHIPPED OFFSITE FOR BURIAL OR DISPOSAL

1. Spent resins, filter sludges, evaporator bottoms, etc.

2.

d.

Shipment type

	a.	Quantity shipped			cu.m.	4.08E+01
	b. c.	Total activity Major nuclides (e	stimate %)		Ci	4.55E+00
			Mn-54 Fe-55 Co-60 Zn-65		5.52E+00 7.15E+01 1.40E+01 3.45E+00	
	d.	Shipment type				LSA
	e.	Solidification age	nt			None
•		npressible waste, nated equipment, e	tc.			
	a.	Quantity shipped	cu.m.			1.09E+02
	b.	Total activity	Ci			2.12E-02
	c.	Major nuclides (e	stimate %)			
			Mn-54 Fe-55 Co-60 Ni-63 Zn-65	1.3° 4.5° 2.0°	7E+01 7E+01 2E+01 6E+01 3E+00	

#### EFFLUENT AND WASTE DISPOSAL ANNUAL REPORT (2002) SOLID WASTE AND IRRADIATED FUEL SHIPMENTS FOURTH QUARTER

3.	Other (	(Oil for	incinera	tion)
----	---------	----------	----------	-------

a.	Quantity shipped cu.m.	0.00E+00
b.	Total activity Ci	0.00E+00
c.	Major nuclides (estimate %)	N/A
d.	Shipment type	N/A

#### 4. Irradiated Components

a.	Number of shipments	0
b.	Mode of Transportation	N/A
c.	Destination	N/A

#### 5. Solid Waste Disposition

	Number of Shipments	Transportation Mode	<u>Destination</u>
	2	Truck	Duratek-Bear Creek, TN
	4	Truck	Envirocare of Utah
TOTAL THIS QUARTER	6		

Estimated total error % for spent resins, filter sludges, evaporator bottoms, etc. (Jan-Dec) 2.50E+01

Estimated total error % for dry compressible waste, contaminated equipment, etc. (Jan-Dec) 2.50E+01

Estimated total error % for other irradiated components (Jan-Dec) N/A

#### B. IRRADIATED FUEL SHIPMENTS

None

# RADIOLOGICAL IMPACT ON MAN MAXIMUM DOSES RESULTING FROM RELEASES AND COMPLIANCE STATUS

#### ACTUAL 2002

#### MAXIMUM DOSES RESULTING FROM AIRBORNE RELEASES PERIOD OF RELEASE - 01/01/02 TO 12/31/02 CALCULATED 04/04/03 INFANT RECEPTOR

(MRAD)       (WSW)       (WSW) <t< th=""><th></th><th></th><th></th><th>•</th><th></th><th></th></t<>				•		
GAMMA AIR       2.00E-02       4.5E-02       (WSW)	TYPE	QUARTER	QUARTER	QUARTER	QUARTER	ANNUAL
INIKOID IIIKOID IIIKOID	(MRAD) BETA AIR (MRAD) IOT. BODY (MREM) SKIN (MREM) ORGAN	(WSW ) 7.25E-04 (ESE ) 1.51E-02 (WSW ) 1.59E-02 (WSW ) 3.89E-03	(WSW ) 2.77E-03 (ESE ) 3.77E-02 (WSW ) 4.01E-02 (WSW ) 6.19E-02	(WSW ) 1.33E-03 (ESE ) 2.86E-02 (WSW ) 3.01E-02 (WSW ) 1.94E-01	(WSW ) 1.92E-03 (ESE ) 2.95E-02 (WSW ) 3.14E-02 (WSW ) 1.38E-01	6.74E-03 (ESE ) 1.11E-01 (WSW ) 1.18E-01 (WSW ) 3.97E-01
	mura To				THYROID	THYROID

THIS IS A REPORT FOR THE CALENDAR YEAR 2002

#### COMPLIANCE STATUS - 10CFR 50 APP. I INFANT RECEPTOR

#### ----- % OF APP I. -----

GAMMA AIR (MRAD) BETA AIR (MRAD) IOT. BODY (MREM) SKIN (MREM) ORGAN (MREM)	QTRLY OBJ 5.0 10.0 2.5 7.5 7.5	1ST QTR JAN-MAR 0.40 0.01 0.61 0.21 0.05	2ND QTR APR-JUN 1.00 0.03 1.51 0.53 0.83	3RD QTR JUL-SEP 0.76 0.01 1.14 0.40 2.58	4TH QTR OCT-DEC 0.78 0.02 1.18 0.42 1.84	YRLY OBJ 10.0 20.0 5.0 15.0	% OF APP. I 1.47 0.03 2.22 0.78 2.65
		THYROID	THYROID	THYROID	THYROID		THYROID

RESULTS BASED UPON:

#### ACTUAL 2002

## MAXIMUM DOSES RESULTING FROM AIRBORNE RELEASES PERIOD OF RELEASE - 01/01/02 TO 12/31/02 CALCULATED 04/04/03 CHILD RECEPTOR

TYPE	1ST QUARTER JAN-MAR	2ND QUARTER APR-JUN	3RD QUARTER JUL-SEP	4TH QUARTER OCT-DEC	ANNUAL
GAMMA AIR (MRAD) BETA AIR (MRAD) TOT. BODY (MREM) SKIN (MREM) ORGAN (MREM)	2.00E-02 (WSW ) 7.25E-04 (ESE ) 1.51E-02 (WSW ) 1.59E-02 (WSW ) 3.25E-03 (NNE )	4.99E-02 (WSW ) 2.77E-03 (ESE ) 3.77E-02 (WSW ) 4.01E-02 (WSW ) 6.56E-02 (ESE )	3.78E-02 (WSW ) 1.33E-03 (ESE ) 2.86E-02 (WSW ) 3.01E-02 (WSW ) 2.00E-01 (ESE )	3.91E-02 (WSW ) 1.92E-03 (ESE ) 2.95E-02 (WSW ) 3.14E-02 (WSW ) 1.41E-01 (ESE )	1.47E-01 (WSW ) 6.74E-03 (ESE ) 1.11E-01 (WSW ) 1.18E-01 (WSW ) 4.10E-01 (ESE )
THIS IS	THYROID A REPORT FOR THE	THYROID CALENDAR YEA	THYROID AR 2002	THYROID	THYROID

#### COMPLIANCE STATUS - 10CFR 50 APP. I CHILD RECEPTOR

#### ----- % OF APP I. -----

GAMMA AIR (MRAD) BETA AIR (MRAD) TOT. BODY (MREM) SKIN (MREM) ORGAN (MREM)	QTRLY OBJ 5.0 10.0 2.5 7.5 7.5	1ST QTR JAN-MAR 0.40 0.01 0.61 0.21 0.04	2ND QTR APR-JUN 1.00 0.03 1.51 0.53 0.87	3RD QTR JUL-SEP 0.76 0.01 1.14 0.40 2.67	4TH QTR OCT-DEC 0.78 0.02 1.18 0.42 1.87	YRLY OBJ 10.0 20.0 5.0 15.0	% OF APP. I 1.47 0.03 2.22 0.78 2.73
		THYROID	THYROID	THYROID	THYROID		THYROID

RESULTS BASED UPON:

#### ACTUAL 2002

MAXIMUM DOSES RESULTING FROM AIRBORNE RELEASES
PERIOD OF RELEASE - 01/01/02 TO 12/31/02 CALCULATED 04/04/03
TEENAGER RECEPTOR

TYPE		1ST QUARTER JAN-MAR	2ND QUARTER APR-JUN	3RD QUARTER JUL-SEP	4TH QUARTER OCT-DEC	ANNUAL
GAMMA AIR (MRAD) BETA AIR (MRAD) TOT. BODY (MREM) SKIN (MREM) ORGAN (MREM)		2.00E-02 (WSW ) 7.25E-04 (ESE ) 1.51E-02 (WSW ) 1.59E-02 (WSW ) 2.41E-03 (NNE )	4.99E-02 (WSW ) 2.77E-03 (ESE ) 3.77E-02 (WSW ) 4.01E-02 (WSW ) 4.00E-02 (NNE )	3.78E-02 (WSW ) 1.33E-03 (ESE ) 2.86E-02 (WSW ) 3.01E-02 (WSW ) 1.22E-01 (NNE )	3.91E-02 (WSW ) 1.92E-03 (ESE ) 2.95E-02 (WSW ) 3.14E-02 (WSW ) 8.54E-02 (NNE )	1.47E-01 (WSW ) 6.74E-03 (ESE ) 1.11E-01 (WSW ) 1.18E-01 (WSW ) 2.49E-01 (NNE )
THIS I	S A REPOR	THYROID I FOR THE	THYROID CALENDAR YEA	THYROID R 2002	THYROID	THYROID

#### COMPLIANCE STATUS - 10CFR 50 APP. I TEENAGER RECEPTOR

#### ----- % OF APP I. -----

GAMMA AIR (MRAD) BETA AIR (MRAD) TOT. BODY (MREM) SKIN (MREM) ORGAN (MREM)	QTRLY OBJ 5.0 10.0 2.5 7.5 7.5	1ST QTR JAN-MAR 0.40 0.01 0.61 0.21 0.03	2ND QTR APR-JUN 1.00 0.03 1.51 0.53 0.53	3RD QTR JUL-SEP 0.76 0.01 1.14 0.40 1.62	4TH QTR OCT-DEC 0.78 0.02 1.18 0.42 1.14	YRLY OBJ 10.0 20.0 5.0 15.0	% OF APP. I 1.47 0.03 2.22 0.78 1.66
		THYROID	THYROID	THYROID	THYROID		THYROID

RESULTS BASED UPON:

#### ACTUAL 2002 MAXIMUM DOSES RESULTING FROM AIRBORNE RELEASES PERIOD OF RELEASE - 01/01/02 TO 12/31/02 CALCULATED 04/04/03

ADULT RECEPTOR

TYPE	1ST QUARTER JAN-MAR	2ND QUARTER APR-JUN	3RD QUARTER JUL-SEP	4TH QUARTER OCT-DEC	ANNUAL
GAMMA AIR (MRAD) BETA AIR (MRAD) TOT. BODY (MREM) SKIN (MREM) ORGAN (MREM)	2.00E-02 (WSW ) 7.25E-04 (ESE ) 1.51E-02 (WSW ) 1.59E-02 (WSW ) 2.66E-03 (NNE )	4.99E-02 (WSW ) 2.77E-03 (ESE ) 3.77E-02 (WSW ) 4.01E-02 (WSW ) 4.13E-02 (NNE )	3.78E-02 (WSW ) 1.33E-03 (ESE ) 2.86E-02 (WSW ) 3.01E-02 (WSW ) 1.26E-01 (NNE )	3.91E-02 (WSW ) 1.92E-03 (ESE ) 2.95E-02 (WSW ) 3.14E-02 (WSW ) 8.88E-02 (NNE )	1.47E-01 (WSW ) 6.74E-03 (ESE ) 1.11E-01 (WSW ) 1.18E-01 (WSW ) 2.59E-01 (NNE )
THIS IS A	THYROID REPORT FOR THE	THYROID	THYROID AR 2002	THYROID	THYROID

#### COMPLIANCE STATUS - 10CFR 50 APP. I ADULT RECEPTOR

----- % OF APP I. -----

GAMMA AIR (MRAD) BETA AIR (MRAD) IOT. BODY (MREM) SKIN (MREM) ORGAN (MREM)	QTRLY OBJ 5.0 10.0 2.5 7.5 7.5	1ST QTR JAN-MAR 0.40 0.01 0.61 0.21 0.04	2ND QTR APR-JUN 1.00 0.03 1.51 0.53 0.55	3RD QTR JUL-SEP 0.76 0.01 1.14 0.40 1.68	4TH QTR OCT-DEC 0.78 0.02 1.18 0.42 1.18	YRLY OBJ 10.0 20.0 5.0 15.0	% OF APP. I 1.47 0.03 2.22 0.78 1.73
		THYROID	THYROID	THYROID	THYROID		THYROID

#### ACTUAL 2002

## MAXIMUM DOSES (MREM) RESULTING FROM AQUATIC EFFLUENTS PERIOD OF RELEASE - 01/01/02 TO 12/31/02 CALCULATED 04/02/03 INFANT RECEPTOR

DOSE TYPE	1ST QUARTER JAN-MAR	2ND QUARTER APR-JUN	3RD QUARTER JUL-SEP	4TH QUARTER OCT-DEC	ANNUAL
TOTAL	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00
BODY INTERNAL ORGAN	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00

THIS IS A REPORT FOR THE CALENDAR YEAR 2002

#### COMPLIANCE STATUS - 10 CFR 50 APP. I

----- % OF APP I. -----

	QTRLY OBJ	1ST QTR JAN-MAR	2ND QTR APR-JUN	3RD QTR JUL-SEP	4TH QTR OCT-DEC	YRLY OBJ	% OF APP. I
TOTAL BODY (MREM)	1.5	0.00	0.00	0.00	0.00	3.0	0.00
CRIT. ORGAN (MREM)	5.0	0.00	0.00	0.00	0.00	10.0	0.00

RESULTS BASED UPON: ODCM ANNEX REVISION 3.0 MAY 2001

ODCM SOFTWARE VERSION 1.1 January 1995

# 2002 ANNUAL REPORT PROJECTED DOSE AT NEAREST COMMUNITY WATER SYSTEM \* PERIOD OF RELEASE - 01/01/02 TO 12/31/02 CALCULATED 04/02/03 INFANT RECEPTOR

3RD 4TH 1ST 2ND QUARTER OUARTER ANNUAL QUARTER OUARTER DOSE TYPE JUL-SEP OCT-DEC APR-JUN JAN-MAR 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 COTAL 3ODY 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 INTERNAL DRGAN

THIS IS A REPORT FOR THE CALENDAR YEAR 2002

#### COMPLIANCE STATUS - 40 CFR 141

TYPE	ANNUAL LIMIT	% OF LIMIT
TOTAL	4.0 MREM	0.000
BODY INTERNAL ORGAN	4.0 MREM	0.000

THIS CALCULATION OF DOSE IS BASED ON TECHNIQUES DESCRIBED IN THE COMMONWEALTH EDISON OFFSITE DOSE CALCULATION MANUAL. THESE TECHNIQUES DIFFER FROM THOSE DESCRIBED IN 40 CFR 141.

RESULTS BASED UPON: ODC

#### ACTUAL 2002

### MAXIMUM DOSES (MREM) RESULTING FROM AQUATIC EFFLUENTS PERIOD OF RELEASE - 01/01/02 TO 12/31/02 CALCULATED 04/02/03 CHILD RECEPTOR

DOSE TYPE	1ST QUARTER JAN-MAR	2ND QUARTER APR-JUN	3RD QUARTER JUL-SEP	4TH QUARTER OCT-DEC	ANNUAL
TOTAL	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00
BODY INTERNAL ORGAN	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00

THIS IS A REPORT FOR THE CALENDAR YEAR 2002

#### COMPLIANCE STATUS - 10 CFR 50 APP. I

#### ----- % OF APP I. -----

	QTRLY OBJ	1ST QTR JAN-MAR	2ND QTR APR-JUN	3RD QTR JUL-SEP	4TH QTR OCT-DEC	YRLY OBJ	% OF APP. I
TOTAL BODY (MREM	) 1.5	0.00	0.00	0.00	0.00	3.0	0.00
CRIT. ORGAN (MREM	) 5.0	0.00	0.00	0.00	0.00	10.0	0.00

RESULTS BASED UPON:

ODCM ANNEX REVISION 3.0 MAY 2001

ODCM SOFTWARE VERSION 1.1 January 1995 ODCM DATABASE VERSION 1.1 January 1995

#### 2002 ANNUAL REPORT

## PROJECTED DOSE AT NEAREST COMMUNITY WATER SYSTEM \* PERIOD OF RELEASE - 01/01/02 TO 12/31/02 CALCULATED 04/02/03 CHILD RECEPTOR

DOSE TYPE	1ST QUARTER JAN-MAR	2ND QUARTER APR-JUN	3RD QUARTER JUL-SEP	4TH QUARTER OCT-DEC	ANNUAL
TOTAL BODY	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00
INTERNAL ORGAN	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00

THIS IS A REPORT FOR THE CALENDAR YEAR 2002

#### COMPLIANCE STATUS - 40 CFR 141

TYPE	ANNUAL LIMIT	% OF LIMIT
TOTAL	4.0 MREM	0.000
BODY INTERNAL ORGAN	4.0 MREM	0.000

\* THIS CALCULATION OF DOSE IS BASED ON TECHNIQUES DESCRIBED IN THE COMMONWEALTH EDISON OFFSITE DOSE CALCULATION MANUAL. THESE TECHNIQUES DIFFER FROM THOSE DESCRIBED IN 40 CFR 141.

RESULTS BASED UPON:

#### ACTUAL 2002

### MAXIMUM DOSES (MREM) RESULTING FROM AQUATIC EFFLUENTS PERIOD OF RELEASE - 01/01/02 TO 12/31/02 CALCULATED 04/02/03 TEENAGER RECEPTOR

DOSE TYPE	1ST QUARTER JAN-MAR	2ND QUARTER APR-JUN	3RD QUARTER JUL-SEP	4TH QUARTER OCT-DEC	ANNUAL
TOTAL	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00
BODY INTERNAL ORGAN	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00

#### THIS IS A REPORT FOR THE CALENDAR YEAR 2002

#### COMPLIANCE STATUS - 10 CFR 50 APP. I

#### ----- % OF APP I. -----

	QTRLY OBJ	1ST QTR JAN-MAR	2ND QTR APR-JUN	3RD QTR JUL-SEP	4TH QTR OCT-DEC	YRLY OBJ	% OF APP. I
TOTAL BODY (MREM	) 1.5	0.00	0.00	0.00	0.00	3.0	. 0.00
CRIT. ORGAN (MREM	) 5.0	0.00	0.00	0.00	0.00	10.0	0.00

RESULTS BASED UPON:

ODCM ANNEX REVISION 3.0 MAY 2001 ODCM SOFTWARE VERSION 1.1 January 1995

#### 2002 ANNUAL REPORT

#### PROJECTED DOSE AT NEAREST COMMUNITY WATER SYSTEM \* PERIOD OF RELEASE - 01/01/02 TO 12/31/02 CALCULATED 04/02/03 TEENAGER RECEPTOR

DOSE TYPE	1ST QUARTER JAN-MAR	2ND QUARTER APR-JUN	3RD QUARTER JUL-SEP	4TH QUARTER OCT-DEC	ANNUAL
TOTAL BODY	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00
INTERNAL ORGAN	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00

THIS IS A REPORT FOR THE CALENDAR YEAR 2002

#### COMPLIANCE STATUS - 40 CFR 141

TYPE	ANNUAL LIMIT	% OF LIMIT
TOTAL	4.0 MREM	0.000
BODY INTERNAL ORGAN	4.0 MREM	0.000

THIS CALCULATION OF DOSE IS BASED ON TECHNIQUES DESCRIBED IN THE COMMONWEALTH EDISON OFFSITE DOSE CALCULATION MANUAL. THESE TECHNIQUES DIFFER FROM THOSE DESCRIBED IN 40 CFR 141.

RESULTS BASED UPON: ODCM ANNEX REVISION 3.0 MAY 2001 ODCM SOFTWARE VERSION 1.1 January 1995

#### ACTUAL 2002

## MAXIMUM DOSES (MREM) RESULTING FROM AQUATIC EFFLUENTS PERIOD OF RELEASE - 01/01/02 TO 12/31/02 CALCULATED 04/02/03 ADULT RECEPTOR

DOSE TYPE	1ST QUARTER JAN-MAR	2ND QUARTER APR-JUN	3RD QUARTER JUL-SEP	4TH QUARTER OCT-DEC	ANNUAL
COTAL	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00
3ODY [NTERNAL ORGAN	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00

THIS IS A REPORT FOR THE CALENDAR YEAR 2002

#### COMPLIANCE STATUS - 10 CFR 50 APP. I

#### ----- % OF APP I. -----

		QTRLY OBJ	1ST QTR JAN-MAR	2ND QTR APR-JUN	3RD QTR JUL-SEP	4TH QTR OCT-DEC	YRLY OBJ	% OF APP. I
COTAL I	BODY (MREM)	1.5	0.00	0.00	0.00	0.00	3.0	0.00
CRIT. (	ORGAN (MREM)	5.0	0.00	0.00	0.00	0.00	10.0	0.00

RESULTS BASED UPON:

ODCM ANNEX REVISION 3.0 MAY 2001 ODCM SOFTWARE VERSION 1.1 January 1995

#### 2002 ANNUAL REPORT

## PROJECTED DOSE AT NEAREST COMMUNITY WATER SYSTEM \* PERIOD OF RELEASE - 01/01/02 TO 12/31/02 CALCULATED 04/02/03 ADULT RECEPTOR

DOSE TYPE	1ST QUARTER JAN-MAR	2ND QUARTER APR-JUN	3RD QUARTER JUL-SEP	4TH QUARTER OCT-DEC	ANNUAL
TOTAL	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00
BODY INTERNAL ORGAN	0.00E+00	0.00E+00	0.00E+00	0.00E+00	0.00E+00

THIS IS A REPORT FOR THE CALENDAR YEAR 2002

#### COMPLIANCE STATUS - 40 CFR 141

TYPE	ANNUAL LIMIT	% OF LIMIT
TOTAL BODY INTERNAL ORGAN	4.0 MREM	0.000
	4.0 MREM	0.000

\* THIS CALCULATION OF DOSE IS BASED ON TECHNIQUES DESCRIBED IN THE COMMONWEALTH EDISON OFFSITE DOSE CALCULATION MANUAL. THESE TECHNIQUES DIFFER FROM THOSE DESCRIBED IN 40 CFR 141.

RESULTS BASED UPON:

# LASALLE STATION UNIT ONE 10 CFR 20 COMPLIANCE ASSESSMENT PERIOD OF ASSESSMENT 01/01/02 TO 12/31/02

CALCULATED 04/04/03

### 1. 10 CFR 20.1301 (a) (1) Compliance

#### Compliance Summary - 10CFR20

1st 2nd 3rd 4th % of Qtr Qtr Qtr Qtr Limit
TEDE 7.54E-02 1.16E-01 1.25E-01 0.44

RESULTS BASED UPON: ODCM ANNEX REVISION 3.0 MAY 2001

ODCM SOFTWARE VERSION 1.1 January 1995

### 10 CFR 20 COMPLIANCE ASSESSMENT

# PERIOD OF ASSESSMENT 01/01/02 TO 12/31/02 CALCULATED 04/04/03

### 2. 10 CFR 20.1301 (d)/40 CFR 190 Compliance

			Dose (mrem)	Limit (mrem)	% of Limit
Whole (DDE)	Body	Plume Skyshine Ground Total	1.11E-01 3.09E-01 2.05E-03 4.22E-01	<u> 25.0</u> _	1.69
Organ (CDE)	Dose	Thyroid Gonads Breast Lung Marrow Bone Remainder	2.36E-01 1.23E-02 1.22E-02 1.23E-02 1.23E-02 1.23E-02 1.26E-02	75.0 25.0 25.0 25.0 25.0 25.0 25.0	0.32 0.05 0.05 0.05 0.05 0.05 0.05
		CEDE	1.91E-02		
		TEDE	4.41E-01	100.0	0.44

RESULTS BASED UPON: ODCM ANNEX REVISION 3.0 MAY 2001

ODCM SOFTWARE VERSION 1.1 January 1995

### LASALLE STATION UNIT TWO

### 10 CFR 20 COMPLIANCE ASSESSMENT

# PERIOD OF ASSESSMENT 01/01/02 TO 12/31/02 CALCULATED 04/04/03

### 1. 10 CFR 20.1301 (a) (1) Compliance

Total Effective Dose Eqivalent, mrem/yr 3.14E-01

10 CFR 20.1301 (a) (1) limit mrem/yr 100.0

% of limit 0.31

### Compliance Summary - 10CFR20

1st 2nd 3rd 4th % of Qtr Qtr Qtr Qtr Limit
TEDE 8.53E-02 7.18E-02 8.39E-02 7.31E-02 0.31

RESULTS BASED UPON: ODCM ANNEX REVISION 3.0 MAY 2001 ODCM SOFTWARE VERSION 1.1 January 1995 ODCM DATABASE VERSION 1.1 January 1995

### LASALLE STATION UNIT TWO

### 10 CFR 20 COMPLIANCE ASSESSMENT

# PERIOD OF ASSESSMENT 01/01/02 TO 12/31/02 CALCULATED 04/04/03

### 2. 10 CFR 20.1301 (d)/40 CFR 190 Compliance

			Dose (mrem)	Limit (mrem)	% of Limit
Whole Boo (DDE)	ly	Plume Skyshine Ground Total	0.00E+00 3.14E-01 0.00E+00 3.14E-01	25.0	1.26
Organ Dos (CDE)	ee	Thyroid Gonads Breast Lung Marrow Bone Remainder	0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00 0.00E+00	75.0 25.0 25.0 25.0 25.0 25.0 25.0	0.00 0.00 0.00 0.00 0.00 0.00
		CEDE	0.00E+00		
		TEDE	3.14E-01	100.0	0.31

RESULTS BASED UPON: ODCM ANNEX REVISION 3.0 MAY 2001

ODCM SOFTWARE VERSION 1.1 January 1995

ODCM DATABASE VERSION 1.1 January 1995

# EFFLUENT AND WASTE DISPOSAL ANNUAL REPORT (2002)

### METEOROLOGICAL DATA

# MURRAY & TRETTEL, INC.

Wednesday, February 5, 2003

Mr. Mike Wolfe Rad Protection LaSalle Station Exelon Nuclear 2601 N. 21st Road Marseillies, IL 61341

Dear Mr. Wolfe:

Enclosed are copies of the LaSalle Station meteorological site quarterly joint-frequency wind rose tables for 2002. They are being sent pursuant to the Specification for Meteorological Data and Meteorological Monitoring Services & Maintenance (MET1), 3.3.2,3.3.3, METSPECS/18/15 and METSPECS/18/41, Table 2a, format of wind rose table.

At this time, we would like to request the 2002 effluent data for your nuclear plant. The effluent data is required to process the 2002 annual report on the Meteorological Monitoring Program as per Specification No. MET1 3.3.4.

In order to expedite the annual report generation, please forward the 2002 effluent data from your plant to:

Tom Begley Murray & Trettel, Inc 414 W. Frontage Road Northfield, IL 60093

If you have any questions, please contact Tom Begley @ (847) 446-7800 x 175.

Thank you for your assistance.

Sincerely,

Tom Begley

Environmental Meteorologist

/tb

Enclosures

# LaSalle Nuclear Station 33 ft. Wind Speed and Direction

### Number of Observations = 2159 Values are Percent Occurrence

							-	8T317	97AN A	r 1100000										(PF) D1	T. THIS (	TASSES			
SPEED CLASS	¥	MNE	MB	ene	E	ESE	<b>\$</b> E • ₩₩	DIREC SSE	S	SSW.	SW	WSW	¥	MAW	EV	MNW	TOTAL	EU	MU	<b>S</b> Ü	I	SS	MS	ES	TOTAL
KU	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00							
	0.00	0.00		0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00		0.00						
C SU		0.00				0.00				0.00		0.00	0.00	0.00	0.00	0.00	0.00			0.00	0 00				
A N		0.00		0.00	0.00	0.00				0.00	_	0.00	0.00	0.00	0.00	0.00	0.00 0.00				0.00	0.00			
L SS M MS					0.00							0.00		0.00	0.00	0.00	0.00					****	0.00		
ES	0.60	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00				0.00	0.00	0.00							0.00	
																									0.00
							A A0		0.00	A An	B 80	0.00			0.00	n nn	6 60	0.00							
		0.00			0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	6.00	0.00	0.00						
1 80	0.00	0.00			0.00			0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00		*****	0.00					
- N		0.05			0.00			0.00	0.00	0.09	0.14	0.05	0.00	0.00	0.00	0.00	0.42				0.42				
3 <b>8</b> S	0.05	0.05	0.00	0.00	0.00	0.05		0.09		0.05	0.05	0.05	0.00	0.00	0.09	0.00	0.51					0.51			
		0.00			0.00				0.00			0.09	0.09	0.00	0.00	0.00	0.45						0.46		
ES	0.05	0.00	0.00	0.00	0.09	0.00	0.05	0.00	0.00	0.00	0.00	0.00	0.00	0.05	0.00	0.00	0.23							0.23	1.62
																									2.42
KU	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00				•			
	0.00					0.00	0.00		0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.05		0.05						
4 SU	0.00	0.00	0.00			0.00	0.05		0.09	0.05		0.00	0.00		0.00	0.00	0.37			0.37					
- N		0.65				0.09	0.00		0.14		0.19	0.14	0.46 0.19	0.32 0.14	0.46	0.37 0.46	4.40				4.40	4.12			
		0.05 0.00			0.37		0.19		0.37 0.14			0.23 0.37		0.65	0.42	0.19	3.06					7.44	3.06		
					0.00										0.28		2.27							2.27	
_	****	****	****	••••			••••		•••																14.27
													0.00			A An	8 80	8 80							
	0.00							0.00	0.00		0.00	0.00	0.00	0.00	0.00	0.00	0.05	0.09	0.05	• •					
8 SU	0.00				0.00 0.00	0.00	0.00	0.09	0.00			0.19	0.00	0.05	0.00	0.00	0.37		4.03	0.37					
- H	1.71			1.02		0.09	0.09	0.05	0.14		0.32		1.16	0.51	0.93	1.34	10.88				10.88				
1 <b>\$</b> \$	0.42	0.09	0.09	0.09	0.65	0.09	0.46	0,28	0.37	0.56	0.56	0.74	0.65	0.74	0.56	0.69	7.04					7.04			
2 MS	0.00	0.00	0.00	0.00	0.05	0.00	0.09	0.56	0.69	0.56	2.36	2.22	0.79	0.42	0.32	0.00	8.06						<b>8.0</b> 6		
KS	0.00	0.00	0.00	0.00	0.00	0.32	0.32	0.23	0.19	0.37	2.73	1.30	1.39	0.05	0.05	0.00	6.95							6.95	33.44
																									<i>44</i> ,27
E	0.00	0.00	0.05	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.05	0.05							
1 🕅	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.05	0.00	0.00	0.05	0.00	0.00	0.00	0.00	0.09		0.09						
3 SU	0.00	0.00	0.00	0.05	0.00	0.00	0.05	0.00	0.00	0.05	0.32	0.19	0.05	0.19	0.09	0.00	0.97			0.97	15 95				
- I	0.69	0.14	1.20	1.16	0.51	0.19	0.19	0.46	0.65	1.53	0.57	1.07	1.57	7.27	0.75	2.36	15.75 9.26				15.75	9.26			
1 8S	0.09	0.00	0.00	0.09	0.32 0.00	0.00	0.23	0.73	1.45	1.0/	1.55	1.0/	V./1	0.00 0.00	0.20 0.00	0.43						7.40	5.28		
O PLO PE	0.00 0.00	0.00 0.00	0.00	0.00	0.00	0.00	0.23	0.09	0.22	0.23	0.79	0.42	0.05	0.00	0.00	0.00							T.5V	1.90	
به	4.44	7.00	4.00	40		7.00	T 1 = 4	4103	- 145								•								33.30

### January-March, 2002 200Ft-33Ft Delta-T (F)

3.6 - 7.5 mph

7.6 - 12.5 mph

12.6 - 18.5 mph

18.6 - 24.5 mph

> 24.5 mph

																				OWILD:	r vinc /	W ACCU	,		
SPEED								DIREC				eeeeee		eeeeee Lyna	LTM	war.	monts t	1071	MTT	STAB.	m milii (	LASSE: SS	MS	ES	TOTAL
CLASS	K	NNE	KK	ENE	E	ESE	SE	SSE	S	SSW	SW	WSW	. 1	MNW	M	MNW	TOTAL	EU	MU	20	Д	20	M	<b>B</b>	101101
577	A AA	A A0	A AA	A AA	A A6	6 60	0.00	0.00	0.00	0.00	0.00	0.14	0.00	0.00	0.00	0.00	0.14	0.14							
	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.09	0.00	0.00	0.09	0.09	0.14	9.60	0.00	0.42	4122	0.42			•		•	
1 100	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.03	0.00	0.14	0.03	0.05	0.09	0.00	0.00	0.56		V 1	0.56					
9 50	0.00	0.00	0.00	0.00	0.00			0.00	0.79	0.60	0.56	0.14	1.11		0.97	0.60	7.97			0.50	7.97				
- 1	0.23	0.00	0.97	0.32	0.09	0.09	0.00				0.56		0.69	1.25	0.05	0.05	4,21					4.21			
2 SS	0.00	0.00	0.00	0.05	0.00	0.00	0.00	0.05	0.83	0.56		0.14	0.00		0.00	0.00	0.69					****	0.69		
4 MS	0.00	0.00	0.00		0.00	0.00	0.00	0.00	0.09	0.23	0.28				0.00	6.00	0.00						¥.07	0.00	
ES	<b>6.0</b> 0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00							V.VV	13.99
																									13.33
									4 44			6 60	0.00	A AA	0.00	8 88	A AA	0.00							
EU	0.00	0.00	0.00		0.00	0.00	0.00	0.00		0.00			0.00		0.00	0.00		U.UU	A A0						
e m	6.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00		0.00	0.00	0.00	0.00		0.00	0.00	0.00		0.00	A 10					
T SU	0.00	0.00	0.00		0.00	0.00	0.05	0.00	0.05	0.00		0.00	0.05	0.00	0.00	0.05	0.19			0.19	• •				
I	0.00	0.00	0.14		0.00	0.00	0.05	0.09	0.09	0.00		0.05	0.65		0.19	0.19	1.53				1.53				
2 <b>\$</b> S	0,00	0.00	0.00	0.00	0.00	0.00	0.00	0.00		0.23	0.09	0.00	0.46		0.05	0.00	1.62					1.62			
4 NS	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00		0.00		0.00	0.00	-,	0.00	0.00	0.05	•					0.05	A 40	
ES	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00							0.00	
												,													3.38
																						•			
														48 80	e an		488 88		A CO	2 45	40.04	96 99	17 60	11 15	100 00
TOT	5.05	1.90	3.94	3.10	2.87	1.48	2.50	4.03	7.55	8.57	15.15	10.84	10.56	10.05	5.13	0.04	100.00	U.20	V.5U	2,43	40.74	40.77	17.00	11.33	100.00
27.1	På-se	ulan 1	Phal	L!1!																			•		
Willio	nirec	tion 1	ny sta	ollity																					
	ı	MNR	Ek	KNE	R	RSK	<b>S</b> E	SSE	8	SSW	SW	WSW	Ħ	IN	MH	INW	TOTAL	-S1	ABILI	TY CLA	SSES-				
		MINT	D.L.	THE STATE	-	<b>#</b> UU	90	500		90"	•		. **	•						-					
	0.00	0.00	0.14	0.00	0.00	0.00	0.00	0.00	0.00	0.00	6.00	0.14	0.00	0.00	0.00	0.00	0.28	Ext	renely	o Unst	able				
	0.00	0.00				0.00		0.05	0.14	0.00			0.09	0.14	0.00	0.00	0.60		lerate						
	0.00	0.00		••••	0.00	0.00	0.14	0.23	0.28	0.09			0.14	0.32	0.09	0.05			ightly						
	3,61	1.71				0.46	0.37	0.97	1.81	2.64			4.96		3.33				tral		•				
	1.25	0.19				0.42	0.88	1.39	3.57	3.06			2.73		1.30				ghtly	Stabl	e				
		****		0.19		0.09	0.37		1.34		• • • •			1.16					erate						
	0.07	0.00	0.03	0.13	0.03									0.65			11.35		remely						
	U.U3	V.VV	. 0.00	<b>V.</b> 00	V.V3	A.3T	V./2	0.31	V.74	A. 60	3.11	1.70	1.71	V.03	4,32	V.V.	20177	-		, 0000					
¥in/	Niro	ntion 1	hu Win	d Spee	đ																				
BTIN'	DATE(	POTON !	ol um	a phee	•																				
	ĸ	IINE	MR	KNE	E	ESE	SE	<b>S</b> SK	S	SSW	Sil	TSW	K	TAW	IN	MINI	TOTAL	-W	IND SPI	KKD (T	ASSES-				
	-		944		-		-																		
	0.00	0.80	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00		CAI	, M					
				0.00				0.14	0.05	0.19	0.19	0.19	0.00	0.05	0.09	0.00				3.5	moh				
	4.72	4.03	V.V.	J.00	4.47	4,41	4.44	4.25	4.00								14 27		26-						

1.76 0.69 0.32 0.32 0.56 0.56 0.60 0.65 0.88 0.74 1.11 0.93 0.93 1.67 1.44 1.11 14.27

2.13 0.97 1.20 1.11 1.30 0.51 0.97 1.20 1.39 1.81 5.97 5.23 3.98 1.76 1.85 2.04 33.44

0.79 0.14 1.25 1.30 0.83 0.19 0.69 1.71 2.69 4.21 6.21 3.75 2.45 3.33 1.16 2.59 33.30

0.23 0.00 0.97 0.37 0.09 0.09 0.00 0.23 1.95 1.39 1.53 0.69 1.95 2.83 1.02 0.65 13.99

0.00 0.00 0.14 0.00 0.00 0.00 0.09 0.09 0.60 0.23 0.14 0.05 1.16 0.42 0.23 0.23 3.38

LaSalle Muclear Station 375 ft. Wind Speed and Direction

### Number of Observations = 2143 Values are Percent Occurrence

							*****	91 TO 17/10	17017 <i>(</i> 11	10000										STABI	LITY C	LASSES			
SPEED					,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	907			CION CI	CZCCA. NZZ	SW	WSW	¥	KINW	MV	MINW	TOTAL	EU	MU	SU	ľ	<b>8</b> S	KS	ES	TOTAL
CLASS	N	MNK	MR	ENK	K	ESE	SE	SSE	8	DON	ЭĦ	RUR		Artes	<b>#</b> 4	******		-		•	-				
स्रा	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00							
MIT	0.00	0.00	0.00	0.00	••••					0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00		0.00	.*					
C SU	0.00	0.00	0.00	0.00					0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00			0.00					
1 1	0.00	0.00	0.00	0.00					0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.60	0.00				0.00			•	
L SS	0.00	0.00	0.00	0.00			0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00					0.00			
N MS	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00		0.00		0.00	0.00	0.00	0.00	0.00	0.00						0.00	A AA	
ES	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00							0.00	0.00
																									0.00
															A A0	A A0	A A1	A AA							-
EU	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	6.00						
MU	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00		0.00	0.00					
1 SU	0.00	0.00	0.00	0.00		0.00	0.00	0.00		0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00			V.40	0.23				
- K	0.05	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.05	0.00	0.00	0.05	0.09	0.00	0.05	0.14	0.61		•		7.27	0.61			
3 <b>\$</b> \$	0.00	0.05	0.00			0.05	0.00	-	0.00		0.00	0.05	0.00	0.00	0.00	0.00	0.02						0.09		
MS	0.00	0.09			0.00	0.00	0.00	0.00		0.00		0.00	0.00	0.00	0.00	0.05	0.05						••••	0.05	
ES	0.00	0.00	0.00	0.00	0.00	0.00	0.00	Ų.UU	0.00	V.VV	V.UU	0.00	V.00	0.00	V.VV	4.43	7.03								0.98
						•																			
1077	4 40	0.00	A 80	0.00	0.00	0.00	0.00	0.00	0 00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00							
BU Sett	0.00	0.00				0.00	0.00	0.00	0.00		0.00			0.00	0.00	0.00	0.00		0.00	٠					
4 SU	0.00		0.00			0.00	0.00	0.00		0.00			0.00	0.00	0.00	0.00	0.00			0.00					
- W	0.00	0.19				0.09			0.09				0.23	0.09	0.37	0.37	2.43				2.43				
7 SS	0.19	0.14				6.00			0.14				0.05	0.05	0.00	0.00	1.54					1.54			
MS						0.00	0.00		0.00				0.05	0.05	0.00	0.05							0.47		
	****			0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.05	0.05	0.00	0.09	0.05	0.23							0.23	4 67
																									4.67
														A A1	6 66	0.00	0.00	0.00							•
EU	0.00	0.00	0.00	0.00							0.00			0.00				V.VV	0.00						
M	0.00	0.00												0.00		0.00			. 0.00	0.00					
8 SU							• • • • •							0.00	••••					****	5.83				
- 1	0.89	•												0.09		0.14	. '				•	2.80			
1 SS	0.28	0.37	0.19	0.19	0.19	0.03	V.U3	0.U3	0.14	0.13	0.05 A 16				0.14							ar	0.98		
2 10	0.00	0.00	0.0	0.03	0.00	0.00	0.00 00.00	V VU	20.U	0.00	0.13	0.00	0.00	0.05	0.05	0.00	0.14							0.14	
K	0.00	0.00	, u.u	) U.UL	9.00	<b>U.U</b> U	<b>U.U</b> U	0.00	0.03	0.00	0.00	4.40	****	****	*****										9.75
<b>इ</b> ग	. n ba	) n n	1 8 64		0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	)						
1 107	, A.O.	, U.U.	, U.U.	) 0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	)	0.00						
3 51	0.00	0.0	0.14	4 0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	) V.14			0.14					
- 1	1 1 91	0.7	1.1	7 0.6	1 0.33	0.09	0.19	0.23	0.05	C.23	0.28	0.75	1.31	. 0.63	0.98	0.5	10.43	j			10.45				
1 5	0 17	0.2	3 0.0	9 0.14	4 0.19	0.09	0.05	0.09	0.14	0.19	0.28	0.70	0.78	0.19	0.93	0.4	4.6	L .				4.81			
9 10	0 1/	2 0 0	0.0	0.0	0.00	0.00	0.09	0.05	0.00	0.23	0.14	0.37	7 0.28	0.56	0.89	0.19	£ 4.63						2.89	A 45	
E	0.00	0.0	0.0	0.0	0.00	0.00	0.00	0.05	0.09	0.00	0.14	0.09	0.00	0.00	0.05	0.0	0.42	?						0.42	10 71
_																									18.71

### January-March, 2002 375Ft-33Ft Delta-T (F)

12.6 - 18.5 mph 18.6 - 24.5 mph > 24.5 mph

																				Ama Deff to	807 <b>(</b> 81	10000	,		
SPEK								DIREC			ha	98/NET	*******	MIT!	1777	MATE!	TOTAL	<b>I</b> U	MU	STABILI SU	n u	28 28	NS	ES	TOTAL
CLAS	S H	MINE	K	ENE	K	ESE	SE	SSE	8	SSN	SW	NSW	H	WINW	W	IMA	IOTUT	EU.	M	20		90	PL)	<b>E</b> 0	MINI
211	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00			,				
1 10		0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00		0.00						
9 80	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.09	0.00	0.00	0.00	0.00	0.09			0.09					
- 1	1.17		0.56	0.89	0.42	0.05	0.05	0.51	0.56	1.49	1.26	0.75	0.93	2.24	1.21	1.31	13.49			13	.49				
2 SS	0.37			0.00	0.23	0.28	0.00	0.33	0.05	0.61	0.56	0.93	0.42	0.75	0.47	0.23	5.23					5.23			
4 MS		••••		0.00	0.00	0.00	0.05		0.05	0.14	0.33	0.79	1.12	0.98	0.28	0.09	4,15						4.15		
T INS					0.00	0.00	0.00	• • - •		0.00	0.14		0.33	0.09	0.00	0.00	0.89							0.89	
. 60	V.V.	V.00	V.40	0.00	V.V0	4.40	4.00	• • • • •	****	****	****		••••	*****		****									23.85
						•																			
RU	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0 00	0.00	0.00	0.00	0.00	0.00	0.00	0,00	0.00	0.00							
				0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	•	0.00						
G KU				0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.05	0.00	0.00	0.00	0.00	0.05		•	0.05					
TSU	0.00				0.37	0.05	0.14	0.23	1.91	0.75	0.89	0.42	1.59		1.82	0.70	11.71				.71				
2 60					0.28	0.05	0.00	0.37	2.71	3.13	3.03	1.31	2.38	2.85	0.65	0.19	17.08					17.08			
2 88					0.00	0.05	0.00			0.79	4.29	3.03			0.09	0.00	11.34						11.34		
4 103	• • • •			0.00			0.00	0.23	0.33	0.00	0.51			0.23	0.00	0.00	1.87							1.87	
ES	0.0	0.00	0.00	0.00	0.00	0.00	V.V3	V.23	V.33	9.94	4.31	4.41	4.17	V.23	9.40	4.40	-14,								42.04
WY.		3 9 49	2 07	2 60	2 55	1 13	1 07	3 60	7 75	R 26	12 69	10.83	11.62	10.64	9.01	5.27	100.00	0.00	0.00	0.28 44	.14	32.06	19.93	3.59	100.00
101	3.7	4.31	3.31	3.40	2.00	1.43	1.07	3.07	1.13	0.20	28.07	44.03			,,,,	••••									
Wit	d Din	ection	by Sta	hility																					
11 44	~ ~~	*	טן טייי																	* .					
	ı		3 103	ENE	E	ESE	SE	<b>S</b> SE	8	SSW	SW	WSW	¥	MAW	Min	<b>I</b> OW	TOTAL	-83	ABILIT	TY CLASSE	S-				
	-																			٠.					
	0.0	0.0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00			Unstabl					
	0.0	0.0	0.00	0.00	0.00	0.60	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00			y Unstat					
	0.0	0.0	0.14	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.14	0.00	0.00	0.00	0.00	0.28			Unstable	!				
	4.5	7 1.5	3.27	2.19	1.59	0.42	0.47	1.45	2.85	2.75	2.89	2.47	4.62	4.39	5.04	3.64			itral						
	1.2	1 0.7	0.42	0.84	1.03	0.56	0.28	1.03	3.17	4.20	4.06	3.27	3.73	3.92	2.38	1.17	•			Stable					
	0.1	9 0.1	0.14	0.05	0.05		0.28		1.21		4.95		2.75		1.40	0.37				ly Stable	•				
	0.0	0.0	0.00	0.00	0.00	0.00	0.05	0.33	0.51	0.00	0.79	0.75	0.51	0.37	0.19	0.09	3.59	X	remely	Stable					
Wi	nd Dir	ection	by Wir	id Spee	đ			•													••	• •			
											***		••	***	987	2017.7	mont f	47	nan an	700 AT 100	180				
	I	IN		ENE	K	ESE	SE	SSK	8	SSW	Sh	NSW	W	MAN	NA.	WUN	TOTAL	<b>-</b> 7.	ואס אוו	EED CLASS	-64				
					0.86		A AC	6 60		6 64	A AA	0 88	6 60	6 80	A An	<b>n n</b> n	8 80		CAI	. M					
	0.0	U 0.0	V 0.0	0.00	U.U0	U.00	V.00	U.U0	V.UU	U.UU	V.V0	V.UU	V.UV	0.VU	N.VV	V.VV	0.00			3.5 mpl	,				
	0.0	5 0.1	1 0.0	0.14	0.05	U.05	0.00	V.U5	U.U5	U.V5	V.UU	V.U3	V.U3	W.UU	0.U3	V.17	0.98			7.5 mg					
	0.3	3 0.3	7 0.20	0.33	0.19	0.09	0.19	0.37	U.23	U.37	0.23	N.13	V.57	0.55 0.13	9.5/	V.3/	4.67								
	1.1	7 0.9	3 0.4	0.84	0.61	0.23	0.28	0.42	0.42	V.28	V.bl	V.61	CO.V	V.30	1.14	V.30	9.75 18.71			12.5 mpl					

 2.38
 0.93
 1.40
 0.75
 0.51
 0.19
 0.33
 0.42
 0.28
 0.65
 0.84
 1.96
 2.29
 1.40
 2.85
 1.54
 18.71

 1.59
 0.09
 0.56
 0.89
 0.65
 0.33
 0.09
 1.17
 0.70
 2.24
 2.29
 2.80
 2.80
 4.06
 1.96
 1.63
 23.85

 0.47
 0.00
 1.26
 0.14
 0.65
 0.14
 0.19
 1.26
 6.07
 4.67
 8.73
 5.18
 5.41
 4.43
 2.57
 0.89
 42.04

### LaSalle Nuclear Station 33 ft. Wind Speed and Direction

### Number of Observations = 8457 Values are Percent Occurrence

SPER	n							DIREC	יז אווזיי	LASSES								•••		STAB1	LITY (	<b>LASSES</b>	****		
CLAS		INE	ME	ENE	E	ESE	SE	SSE	S	SSW	SW	TISW	W	WNW	MM	MNW	TOTAL	EU	MU	SU	N	<b>S</b> S	MS	ES	TOTAL
EU	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00							
MO	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00		0.00					•	
C SU	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00 0.00			0.00	0.00				
A H	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00		·		٠.٠٠	0.00			
M MS	0.00	• • • • • • • • • • • • • • • • • • • •	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00						0.00		
ES	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00		•					0.00	
																									0.00
-				A 60	8 80	A 00	A AD	0.00	0.00	0.00	6.60	0.00	0.00	0.00	0.00	0.00	0 00	0.00							
ASU Medi	0.00	0.00 0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	8.00	0.00	0.00	0.00	0.00	0.00	0.00	****	0.00						:
1 80			0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00			0.00		,			
- 1	0.09	0.08	0.02	0.05	0.01	0.09	0.01	0.04	0.04	0.05	0.09	0.06	0.04	0.06	0.04	0.02	0.79				0.79				
3 59	0.09	0.08	0.04	0.02	0.04	0.05	0.05	0.07	0.07	0.06	0.05	0.04	0.06	0.01	0.07	0.00	0.74					0.74	A 6/		
MS	0.04		0.04	0.01	0.02	0.02	0.01	0.02	0.05	0.04	0.01 0.05	0.07 0.06	0.11	0.01 0.05	0.02	0.05 0.05	0.54 0.53						0.54	0.53	
E	0.02	2 0.00	0.01	0.00	0.05	U.U2	V.V5	0.02	V.UU	0.01	V.V3	V.V0	V.V3	6.03	V.V.	V.VJ	V.JJ		•					*****	2.61
E	0.0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.01	0.01	0.00	0.00	0.00	0.00	0.00		0.02							
M	0.0	0.06	0.02	0.01	0.00	0.04	0.61	0.04	0.02	0.02	0.04	0.05	0.01	0.01	0.01	0.01	0.37		0.37	1 61					
4 \$1		0.07	0.07	0.08	0.12	0.06	0.05	0.14	0.15	0.15 0.25	0.11	0.13 0.45	0.14	0.13	0.02	0.04 0.63	1.51 7.97			1.51	7.97				
- 1 7 S	1.03 6.73		0.38	0.39 0.15	0.41	0.37 0.34	0.35 0.21	0.34	0.31	0.23	0.48		0.37		0.44	0.40	6.21					6.21			
NS.	0.0				0.41	0.53	0.48	0.33	0.51		0.63	0.44	0.38	0.59	0.34	0.19	5.73						5.73		
E	. ,,,,,	2 0.01		0.01	0.24	0.52	0.43	0.78	0.61	0.82	0.89	0.56	0.38	0.53	0.11	0.04	5.94							5.94	
																									27.75
127	3 0.0	0.00	0 07	0.02	0.03	0.00	0.00	0.00	0.00	0.11	0.04	0.18	0.11	0.00	0.00	0.00	0.52	0.52					**		•
M			0.09	0.20	0.04	0.01	0.61	0.05	0.04	0.19	0.17	0.14	0.14	0.05	0.04	0.00	1.23		1.23						
8 S	0.0	7 0.06	0.14	0.12	0.13	0.08	0.12	0.12	0.11	0.15	0.31	0.33	0.13	0.15	0.07	0.11	2.20			2.20					
- 1	T 1.3				0.78	0.27	0.20	0.19	0.53	0.69	1.03	0.99	1.12		0.99	1.61	13.72				13.72				
1 \$	5 0.4	1 0.11	0.40	0.57					0.69	0.79		0.63			0.51 0.17	0.56 0.01	8.74 5.62					8.74	5.62		
2 N	5 V.U	0.00	0 00	0.00	20.U	0.05 ft ft	0.14 0.14	0.11 6.28	0.37	0.00	1.42	1.08	0.61	0.16			5.03					•	0.02	5.03	•
-	3 4.0	U V.VV	V.UU	V.UU	0.03	0.21	V.13	V.50	0.50	****	-,	2.00	****	••••			••••								37.05
																		• •-							
E	0.0	2 0.00	0.02	0.06	0.00	0.00	0.00	0.01	0.02	0.11	0.08	0.04	0.02	0.02	0.00	0.00	0.41	0.41	A 20						
1 M	U 0.0	0.01	0.04	0.05	0.02	0.00	0.01	0.04	0.04 0.07	0.15	0.14 0.24	0.12 A 10	V.Q9	V.14 0 21	0.00 0.00	V.V4	0.89 1.56		0.89	1.56					
<b>5 8</b>	U V.O	4 U.UU 6 A 11	U.U5	V.Vb	0.Ub	0.V1	0.V3	0.03	0.07	0.78	0.74	0.69	0.91	1.42	0.69	1.51	1.56 11.43				11.43				
1 8	S 0.0	5 0.00	0.09	0.22	0.50	0.07	0.11	0.28	0.91	1.02	1.05	0.58	0.56	0.41	0.17	0.07	6.09					6.09			
8 M	S 0.0	0.00	0.00	0.00	0.00	0.00	0.00	0.15	0.26	0.50	0.99	0.32	0.12	0.00	0.00	0.00	2.34						2.34		
E	S 0.0	0 0.00	0.00	0.00	0.00	0.00	0.06	0.02	0.02	0.11	0.22	0.14	0.01	0.00	0.00	0.00	0.59							0.59	12 22
																			•						23.32

12.6 - 18.5 mph 18.6 - 24.5 mph

> 24.5 mph

LaSalle Buclear Station
33 ft. Wind Speed and Direction

																				Am n	PT 1887 A	<b>* * *</b>			
SPEED							- WIND	DIREC	lion C					20000	477	ender EREE	anoma t	 El7	Mi		M Triti (	iasses Ss	KS	ES	TOTAL
CLASS	N	MNK	MK	KNE	K	ese	SE	SSE	S	SSW	SW	WSW	W	ION	ĦИ	INW	TOTAL	EU	M	SU	R	93	n.	<b>B</b> J	IOTUD
ध्या	A AA	A 80	0.00	0.00	0.00	0.00	0.00	0.00	0.07	8 12	0.02	0.04	0.00	0.00	0.00	0.00	0.25	0.25							
EU 1 MT	0.UU	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.05	0.12	0.02	0.05	0.02	0.06	0.02	0.00	0.34		0.34			7			
TIN	0.00	0.00	0.00	0.00	0.01	0.00	0.00	0.00	0.07	0.08	0.07	0.09	0.02	0:11	0.01	0.00	0.47			0.47					
7 50	• • • •		0.33	0.25	0.01	0.26	0.05	0.06	0.27	0.37	0.22	0.09	0.53	0.57	0.43	0.27	4.04				4.04				
- H	0.11	0.00					0.02	0.02	0.33	0.43	0.34	0.08	0.34	0.56	0.05	0.01	2.26					2.26			
2 SS	0.00	0.00	0.00	0.01	0.01	0.05	0.02	0.02		0.07	0.09	0.01	0.00	0.01	0.00	0.00	0.25					4	0.25		
4 KS	0.00	0.00	0.00	0.00	0.00	0.00		0.00		0.00	0.00	0.00	0.00		0.00	0.00	0.00							0.00	
ES	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	V.VV	0.00	0.00		0.00	4.00	•	,								7.61
991			A AA		A 66	0.00	0.00	0.00	0.00	0.07	0.00	0.00	0.00	0.00	0.00	0.00	0.07	0.07							
EU	0.00	0.00	0.00	0.00	0.00		0.00			0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.01	. ••••	0.01						
G MU	0.00	0.00	0.00	0.00	Q.QU	0.00	0.00	0.00	0.01		0.00	0.00	0.01	0.00		0.01	0.06		****	0.06					
T SU	0.00	0.00	0.00	0.00	0.00	0.00	0.01	0.00	0.01	0.01	0.06	0.01	0.20	0.14	0.08	0.08	0.80				0.80				
	0.00	0.00	0.04	0.00	0.04	0.00	0.01	0.04	0.05			0.02	0.20	0.20		0.00	0.70					0.70			
2 55	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.02	0.14	0.06	0.02		0.00	0.20		0.00	0.01					****	0.01		
4 MS	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00			0.00	0.00		•				0.02	0.00	* * .
ES	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	U.UU	0.00	V.VV							4.00	1.66
																								,	2.00
																				•	•	•	•		
-			4 00	4 44	r 43	9 64	1 65	4 76	7 10	a co	19 56	0 00	8 81	0 27	4 02	E 83	100 00	1 28	2 84	5.81	38.76	24.74	14.50	12.08	100.00
TOT	4.69	3.56	4.72	4.00	5.83	3.57	3.05	4.30	1,19	y.85	12.30	0.00	0.01	0.37	2.74	3.63	100.00	1.50	4.01	7.01	30.70	82112	21.JV	20.00	200.00
Wind	Dim	tion 1	wr Ctal	hility																		,			
MITTE	DITE	CIUII I	ny ora	niircj							•														
	F	MINE	IE	ENR	E	ESE	SE	SSE	8	SSW	SW	WSW	W	MNW	K	DW	TOTAL	-\$	Tabilly	ALD Y	SSES-		-		
	•	, ma			_				-																
	0.02	0.00	0.09	0.08	0.00	0.00	0.00	0.01	0.09	0.41	0.15	0.25	0.13	0.02	0.00	0.00	1.28	<b>E</b> r	tremely	Unst	able				
	0.05	0.11			0.06	0.05	0.04	0.12	0.15	0.48	0.37	0.35	0.27	0.26	0.07	0.05	2.84		derate						
	0.15	0.13			0.32		0.22	0.35	0.41	0.50	0.72	0.73	0.50	0.60	0.20	0.28	5.81	\$1	ightly	Unsta	ble				
	3.02	2.15			2.25	1.24	0.71	0.98	1.70	2.19	2.70	2,29	3.31	3.77	2.66	4.13	38.76	Ne	utral						
	1.28	0.95			2.05	0.72	0.72	0.84	2.45	2.58	2.93	1.66	2.22	2.27	1.25	1.04	24.74	<b>S1</b>	ightly	Stabl	e	•		•	
	0.13		0.06		0.83	0.65	0.64	0.95	1.44	1.81	3.11	1.74	1.28	0.80	0.53	0.25	14.50	No	derate	ly Sta	ble				
	0.05	0.01	0.01	0.01	0.33	0.76	0.72	1.11	0.93	1.71	2.58	1.83	1.10	0.64	0.20	6.08	12.08	Ex	tremely	y Stab	le				
		V.V.	****	• • • • • • • • • • • • • • • • • • • •	*****	••••	••••		••••																
																							٠		
Win	l Dire	ction !	by Win	d Spee	đ																				
			•	•										•											
	I	NNE	M	ENE	E	ESE	SE	SSE	S	SSW	SH	WSW	Ħ	MNW	NW	MAN	TOTAL	-1	IND SP	erd (T	ASSES-				
	-																		<b></b>			•			
	0.00	9.00	0.00	0.00	0.00	0.00	0.00	0,00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00		CA						
	0.20	0.19	0.11	0.08	0.12	0.19	0.12	0.15	0.15	0.15	0.20	0.22	0.30	0.13	0.18	0.12	2.61			3.5					
	1.97	2.09	0.76	0.71	1.68	1.86	1.54	1.86	1.92	2.02	2.70	1.93	1.79	2.28	1.36	1.30	27.75		3.6 -						
	1.84	1.16	1.97	1.67	2.39	0.89	0.99	1.29	2.22	3.37	5.32	4.25	3.49	2.09	1.52	2.28	37.05		7.6 -						
	A 67	ñ 12	1 21	1 20	1 25	A 22	A 31	6 92	1 82	2 76	RA F	2 06	1.98	2.21	0.95	1.75	23.32		12.6 -	18.5	mb				

0.57 0.12 1.51 1.28 1.35 0.33 0.31 0.92 1.83 2.76 3.48 2.06 1.90 2.21 0.95 1.75 23.32

0.11 0.00 0.33 0.26 0.26 0.31 0.07 0.08 0.85 1.18 0.78 0.37 0.92 1.30 0.51 0.28 7.61 0.00 0.00 0.04 0.00 0.04 0.00 0.02 0.06 0.21 0.20 0.08 0.04 0.41 0.35 0.11 0.09 1.66

LaSalle Nuclear Station 375 ft. Wind Speed and Direction

### Number of Observations = 8735 Values are Percent Occurrence

THE REPORT OF THE PARTY OF THE								erene.	n en es	BTAT A	E 3.00D0										CTART	i.tav	(T.)	CCEC			
## 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0	SPEED CLASS	K	NAR	NB	ENE	1	ESE	- WIND SK		TION C			WSW	¥	KNY	M	MAN	TOTAL	EU	M					MS	ES	TOTAL
## 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0					٠																						
C SU 9.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	EU	0.00	0.00	0.00															0.00	A A0							•
N   0.00   0.0	NU A MI	0.00	0.00	0.00																V.UU	0.00						
S   0.00   0.	C SU		0.00 An A																			0.0	0				
No.   Color	L SS		0.00	0.00											0.00	0.00								.00			
No.				0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00			0.00								0.00		
NO   0,00   0,	ES	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00								0.00	A A0
NO   0.00   0.																											<b>U.U</b> U
NO   0.00   0.	867	A 'AA	A A0	0.00	A AA	0.00	A 80	0.00	0.00	0.00	0.00	8 80	0.80	0 00	8 60	6 00	6 00	0.00	0.00								
1 ST 0 .0.0 0 .0	AU Mil	8 60		0.00		• • • •					****							-	••••	0.00							
3 SS 0.62 0.63 0.02 0.05 0.05 0.05 0.02 0.01 0.02 0.01 0.02 0.02 0.02 0.02	1 SU	0.00		0.00										0.00			0.00				0.00						
SE   0.01   0.05   0.00   0	- N	0.03				0.05	0.01			0.02	0.01	0.01	0.06	0.02	0.05	0.01	0.01					0.3					
ES 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.	3 <b>\$</b> S	0.02	0.03	0.02	0.06	0.03	0.02	0.01	0.02	0.02	0.02												0				
8.89  EU 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.	MS						4																		0.15	A A1	
EU 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.	ES	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.01	A.01								0.01	0.80
NO   0.00   0.																											4.07
NO   0.00   0.	<b>e</b> tt	6 60	0.00	0 00	0.00	0.00	0 00	0.00	0.00	0.00	0.60	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00								
4 SU 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0	MI			7					4	0.00	0.00	0.00	0.00	0.00	0.00	0.00		0.00		0.00							
7 SS 0.16 0.09 0.21 0.14 0.09 0.07 0.14 0.08 0.75 0.08 0.16 0.09 0.10 0.08 0.08 0.09 1.81  MS 0.05 0.08 0.06 0.07 0.06 0.07 0.02 0.01 0.05 0.01 0.02 0.03 0.06 0.00 0.01 1.03  ES 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.		0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00				0.00						
NS 0.05 0.08 0.06 0.07 0.06 0.07 0.06 0.07 0.02 0.01 0.05 0.14 0.07 0.15 0.08 0.11 0.01 0.01 1.03  ES 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.	- I	0.44	0.41	0.35	0.38	0.38	0.30	0.26	0.33	0.29	0.30	0.25										5.2		••			
ES 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.	7 \$S																_						1		1 02		
EU 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.	MS																								1.03	0.23	
EU 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.	KS	0.00	0.00	0.00	0.00	0.00	U.UU	0.00	V.V2	Ç.VJ	0.01	V.V4	0.03	V.00	0.00	V.V2	4.01	V.43								4.65	8.36
NU 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.																											
8 SU 0.00 0.00 0.01 0.03 0.01 0.03 0.01 0.00 0.00	EU	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00		0.00								
- W 1.09 1.04 0.65 0.81 0.63 0.37 0.34 0.40 0.58 0.53 0.80 0.98 0.58 0.68 0.88 0.80 11.17  1 \$S\$ 0.38 0.34 0.29 0.41 0.41 0.27 0.18 0.16 0.18 0.21 0.14 0.37 0.29 0.14 0.23 0.16 4.16  2 \$W\$ 0.05 0.05 0.05 0.02 0.09 0.07 0.13 0.11 0.23 0.16 0.18 0.29 0.18 0.16 0.22 0.18 0.14 2.26  E\$\$ 0.01 0.01 0.00 0.00 0.00 0.00 0.00 0.	MU	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00								0.00							
1 SS 0.38 0.34 0.29 0.41 0.41 0.27 0.18 0.16 0.18 0.21 0.14 0.37 0.29 0.14 0.23 0.16 4.16 2 MS 0.05 0.05 0.02 0.09 0.07 0.13 0.11 0.23 0.16 0.18 0.29 0.18 0.16 0.22 0.18 0.14 2.26 ES 0.01 0.01 0.00 0.00 0.00 0.00 0.00 0.0	8 SU	0.00	0.00	0.01	0.03	0.01	0.00	0.00	0.00												0.17	•• •	9				
2 MS 0.05 0.05 0.02 0.09 0.07 0.13 0.11 0.23 0.16 0.18 0.29 0.18 0.16 0.22 0.18 0.14 2.26  EU 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.	- N													••••								11,1		16			
ES 0.01 0.01 0.00 0.00 0.00 0.01 0.02 0.02	1 85	0.38 0.05	0.34 0.05	0.29	0.41	0.41	0.27	0.18 6 11	0.10	0.16	0.21												•		2.26		
EU 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.	Z PAS	8.03 8 ft	0.03 0.01	0.02	0.03	0.00	0.13	0.02	0.02	0.11	0.08	0.10	0.06	0.03	0.02	0.03	0.01	0.54							,	0.54	
1 MU 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0	-	4147	4.41	4.00	0.00	****	****	****	*****	,,,,,,		•••	•		****												18.29
1 MU 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0																	4										
3 SU 0.00 0.00 0.08 0.05 0.00 0.00 0.01 0.00 0.01 0.01 0.01	EU	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00		0.00	A A4							
- N 1.08 0.76 1.64 1.20 0.73 0.22 0.18 0.34 0.38 0.66 1.06 1.01 1.25 1.03 1.17 0.96 13.67  1 SS 0.52 0.47 0.48 0.78 0.46 0.27 0.15 0.16 0.27 0.30 0.47 0.55 0.49 0.47 0.60 0.42 6.86  8 NS 0.14 0.02 0.02 0.08 0.07 0.16 0.18 0.26 0.18 0.31 0.35 0.35 0.26 0.57 0.45 0.19 3.62  ES 0.00 0.00 0.00 0.00 0.00 0.01 0.14 0.29 0.09 0.11 0.15 0.16 0.06 0.02 0.05 0.07 1.14	1 10	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.01	0.01	0.00	0.00	0.00			V.02	A 20						
1 SS 0.52 0.47 0.48 0.78 0.46 0.27 0.15 0.16 0.27 0.30 0.47 0.55 0.49 0.47 0.60 0.42 6.86 6.86  8 NS 0.14 0.02 0.02 0.08 0.07 0.16 0.18 0.26 0.18 0.31 0.35 0.35 0.26 0.57 0.45 0.19 3.62  8 S 0.00 0.00 0.00 0.00 0.00 0.01 0.14 0.29 0.09 0.11 0.15 0.16 0.06 0.02 0.05 0.07 1.14 1.14	3 50	0.00	0.00	0.08	0.05	0.00	0.00	U.00	0.01	V.UU	N.AT	1 NE	1 81	1 25	1 02	1.17	0.46	13.67			V.30		7				
8 MS 0.14 0.02 0.02 0.08 0.07 0.16 0.18 0.26 0.18 0.31 0.35 0.35 0.26 0.57 0.45 0.19 3.62  8 NS 0.00 0.00 0.00 0.00 0.00 0.01 0.14 0.29 0.09 0.11 0.15 0.16 0.06 0.02 0.05 0.07 1.14  1.14	- M	7.UŠ	V. 10	U 18	1.40	0.13 0 16	0.22	0.15	0.16	0.30	0.30	0.47	0.55	0.49	0.47	0.60	0.42	6.86				٠.٠		.86			
RS 0.00 0.00 0.00 0.00 0.01 0.14 0.29 0.09 0.11 0.15 0.16 0.06 0.02 0.05 0.07 1.14	2 103	0.34	0.02	0.02	0.08	0.07	0.16	0.18	0.26	0.18	0.31	0.35	0.35	0.26	0.57	0.45	0.19	3.62	,				-	-	3.62		
25.69	ES	0.00	0.00	0.00	0.00	0.00	0.01	0.14	0.29	0.09	0.11	0.15	0.16	0.06	0.02	0.05	0.07	1.14								1.14	
																											25.69

### January-December, 2002 375Ft-33Ft Delta-T (F)

7.6 - 12.5 mph

12.6 - 18.5 mph 18.6 - 24.5 mph > 24.5 mph

																				Ama na		AT SAIRE			
SPEKD			•••••			**-	- NIND	DIREC	rion C							4-4	E0511				LLITY !	CLASSES		<b>T</b> 0	<b>55001 1</b>
CLASS	K	MNR	<b>I</b> R	KNE	E	ESE	<b>S</b> e	<b>S</b> SE	S	SSW	SW	WSW	¥	WAW	Wif	MINW	TOTAL	EU	W	SU	N	SS	MS	ES	TOTAL
का	A A0	0.60	0.00	0.00	A 80	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00					٠		
1 100	0.00			6.00	0.00	0.00	0.00	0.00	0.01	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.01		0.01						
1 100	0.00	0.00	0.00	0.00		0.00	0.00	0.00	0.05	0.07	0.06	0.02	0.00	0.00	0.00	0.00	0.24		****	0.24					
9 80	0.03	0.00	0.00	0.00			0.10	0.29	0.50	0.93	0.98	0.63	0.81	1.31		0.87	11.00				11.00				
- 1	0.74	0.15	1.03	0.87	0.56	0.17				0.50	0.50	0.49	0.37	0.62	0.57	0.29	5.79				27.44	5.79			
2 5S	Q.27	0.05	0.17	0.15	0.50		0.16	0.24	0.31	0.34	0.65	0.52	0.57		0.23	0.10	3.95					4.17	3.95	•	
4 MS	0.01	0.00	0.00	0.00	0.11	0.23	0.23	0.16		0.25	0.23	0.32			0.00	0.01	1.37						3.73	1.37	
ES	0.03	0.00	0.00	0.00	0.00	0.06	0.09	0.13	0.13	V,23	0.23	U.41	V.17	0.07	V.V	A.AT	1.31							****	22.37
														•											26.41
1717	A AA	0.00	A A0	0.00	0.00	0.00	0.60	0.00	0.60	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00							
	0.00	0.00	0.00		0.00	0.00	0.00	0.00	0.00	0.01	0.02	0.00	0.00	0.00	0.00	0.00	0.03	****	0.03						
G MU	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.01	0.14	0.02	0.01	0.00	0.00	0.01	0.00	0.19		V,43	0.19					
T SU	0.00	0.00	0.00	0.00			0.00	6.11	0.01	0.85	0.58	0.26	0.71	0.65	0.95	0.40	7.01			V.23	7.01				
	0.18	0.00	0.50	0.19	0.42	0.31	••	0.11		2.31	1.97	0.73	1.20	1.11	0.32	0.07	9.54					9.54			
2 8S	0.03	0.00	0.00	0.02	0.16	0.14	0.10		1.17	0.96	1.84		0.79	0.21	0.02	0.00	6.22					,,,,	6.22		
4 MS	0.00	0.00	0.00	0.00	0.02	80.0	0.17	0.38		0.07	0.23	0.41			0.02	0.00					•		V.44	1.41	
ES	0.00	0.00	0.00	0.00	0.00	0.01	0.07	0.11	0.38	V.V/	V.23	V.41	V.V3	0.00	V.VV	V.VV	1.71	•						<b>2,11</b>	24.40
												*	•												85.70
TOT	5 28	1 58	5 54	5 37	4 80	<b>3 10</b>	2.80	3.97	6.75	9.44	11.33	8.82	8.72	8.16	7.24	4.99	100.00	0.00	0.07	0.98	48.49	28.53	17,22	4.71	100.00
	. 3104	4.50	••••	•.•.		0.25	2.00	••••	****	••	•====														
																						•			
Win	Direc	ction 1	by Stal	bility												•									
					_	<b>50</b> 77	87	802	٥	000	<b>0</b> 13	an (Mar		· Mari	W	MINW	TOTAL	_61	TABILIT	v ma	eere_				
	N	MNE	MR	ENR	E	ESE	SE	SSE	9	<b>S</b> 5W	SN	NSW	Ħ	INN	a.	MUN	IVIAL	-01	INDIRE	1 CM	- الحدود				
	6.00	0 00	6 60	0.00	8 80	0 00	0 00	0.00	0.00	0.00	6.00	0.00	0.00	0.00	0.00	0.00	0.00	Ext	remely	Unst	able				
	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.01	0.01	0.02	0.01	0.01	0.00	0.00	0.00			ieratel						
		0.00	•		0.00	0.00	0.00	0.01	0.06	0.26	0.11	0.18	0.09	0.01	0.02	0.00			ightly						
	0.03				2.77		1.00	1 40	2.54	3.27	3.76	3.22	3.84	3.93	4.40	3.37			itral						
	3.56		1.17				8 74	1,23	2.11	3.42		2.24		2.42	1.82	1.06			ightly	Stabl	é			٠	
	1.39		0.10				0.74	1 0/	1.28	1.95				1.61		0.45			ieratel						
	0.25	V.21	0.10	0.44	4 44	00.0	0.78							0.19					remely						
	U.U3	0.01	0.00	U.UU	U.UU	U.U7	V.34	9.37	9.70	V.33	6.13	0.07	4.37	V.13	4.20	¥ 7.84	3.10	(Base)							
Win	d Dire	ction	by Win	d Spee	đ																				
				-5												•									
	H	MNE	MIK.	KNE	E	ESE	SE	<b>S</b> SE	8	SSW	SW	WSW	¥	<b>TINN</b>		MNW	TOTAL	-11.	IND SPI	KD (CL	asses-	•			
								4 50						8 80		A AA	A 8A		<i>(</i> 111	ъ.					
	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	V.U0	0.00	0.00	0.00	V.U)	U.UU	0.00			N .					
	0.07	0.11	0.02	0.09	0.09	0.03	0.03	0.03	0.08	0.05	0.01	0.07	0.06	0.05	0.03	U.Ub	0.89			3.5					
	0.64	0.58	0.62	0.58	0.53	0.44	0.42	0.45	0.53	0.53	V.50	0.55	U.70	0.41	U.45	U.44	8.36 18.29		3.6 - 7.6 -						
	4 69	1 44	A 67	1 35	1 19	. A 70	n 22	n 91	7 M	7 M	1 75	7 68	1 10	1 05	1 ((	1 11	1X ZV		1.B =	14.5	ши				

1.52 1.44 0.97 1.35 1.12 0.78 0.66 0.81 1.04 1.04 1.35 1.60 1.10 1.05 1.33 1.11 18.29

1.73 1.25 2.22 2.11 1.26 0.66 0.65 1.06 0.93 1.40 2.05 2.22 2.13 2.11 2.27 1.65 25.69 1.10 0.19 1.20 1.02 1.19 0.74 0.58 0.81 1.20 2.10 2.75 1.87 1.99 2.50 1.85 1.27 22.37 0.22 0.00 0.50 0.22 0.61 0.54 0.45 0.80 2.98 4.34 4.67 2.51 2.75 2.05 1.31 0.47 24.40

### LaSalle Muclear Station 33 ft. Wind Speed and Direction

### Number of Observations = 2179 Values are Percent Occurrence

																				fall ha	t Year	M 3 ACDC			
SPKKI		*****							TION CI		663	en para en MON	w	WITE	171	mw	TOTAL	KU	MIT	21 START		CLASSES SS	MS	ES	TOTAL
CLAS	N	MNE	ME	ENE	E	ESE	SE	SSE	. 8	SSN	SH	WSW		KNW	MH	MAR	IOIVR	ĐŲ	PIU	.00				•••	
RU	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00							•
M	0.00	0.00	0.00	0.00	0.00		0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00		0.00						
C SU	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00			0.00	0.00	0.00	0.00	,	0.00	0.00			0.00					
A N	6.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00			0.00	0.00	0.00			0.00	0.00			.*	0.00				
l SS	0.00	0.00	0.00	0.00	0.00	0.00	0.00	-	••••		0.00	0.00	0.00	0.00		0.00	0.00					0.00	0.00		
n ns	0.00		0.00	0.00					0.00		0.00	0.00	0.00	0.00	0.00	0.00	0.00 0.00						V.00	0.00	
ES	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	<b>V.V</b> V	0.00	0.00	0.00	V.UV	V.VV	V.VV	V.VV							••••	0.00
																				•					• • • • • • • • • • • • • • • • • • • •
1711	0.00	0.00	0.00	A AA	0.00	n na	0 00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00							
170 1700	0.00	0.60	0.00	0.00	0.00	0.00	0.00	0.00		0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00		0.00						
1 50	4.00		0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00			0.00					
- 1	0.09		0.05	0.14	0.00	0.14	0.00	0.00	0.05	0.00	0.18	0.09	0.00	0.00	0.09	0.05	0.96				. 0.98				
3 <b>S</b> S	0.05	0.14	0.05	0.05	0.05	0.09	0.00	0.05		0.14		0.05	0.09	0.00	0.09	0.00	1.01					1.01	0.40		
KS	0.00	0.00	0.09	0.00	0.05	0.00	0.00	0.05	0.09	0.05	0.00	0.05	0.00	0.00	0.00	0.09	0.45						0.46	0.05	
ES	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.05	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.05							V.UJ	2.48
																-									••••
				4 40	A 00	A A2	A A0		A AA	8 88	A AA	0.00	0.00	0 00	0.00	0 00	0.00	0.00				•			
	0.00		0.00			0.00	0.00		0.00	0.00	0.00	0.09	0.00	0.00	0.00	0.00	0.09	****	0.09						
PA,	0.00 0.00		0.00	0.00 0.05	0.00	0.00	0.00	0.09	0.00	0.18	0.14	0.09	0.05	0.18	0.00	0.00	0.96			0.96					
- I			0.60	0.55	0.73		0.23	0.46	0.60		0.55	0.41	0.32	0.23	0.55	1.01	8.99				8.99				
_		0.50		0.14			0.18	0.32			0.69	0.23	0.50	0.69	0.50	0.28	5.87					5.87			
		0.05					0.87			0.55			• • • •	0.64		0.18	6.24						6.24		
E	0.00	0.00	0.00	0.00	0.00	0.14	0.28	0.73	0.87	0.96	0.69	0.41	0.09	0.14	0.00	0.00	4.31							4.31	26.48
										•															20.40
				A 00		A A0	A .AA	0.00	8 60	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00							
	0.00		0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.28	0.09	0.09	0.05	0.00	0.09	0.00			0.73						
8 SI	0.00 0.09		0.03	0.05		0.05	0.23	0.28	0.18	0.32	0.46	0.60	0.23	0.18	0.14	0.14	3.35			3.35	•				
- 1	0.60		1.19		0.83	0.41			1.33		1.10	0.92	1.06	1.56	1.38	2.02	15.14				15.1				
1 \$		. 0 05	0.22	0.64	1 28	0.50	0.41	0,23	0.92	0.05	0.87	0.64	0.96	0.32								7. <b>9</b> 9			
2 M	. 0.00	0.00	0.00	0.00	0.37	0.18	0.32	0.92	0.32	0.64	0.83	0.55	0.50	0.14	0.05	0.00	4.82					•	4.82		
E	0.0	0.00	0.00	0.00	0.00	0.05	0.37	0.78	0.50	0.83	0.73	1.10	0.28	0.00	0.00	0.00	4.64							4.64	36.67
																		•							30.07
						A 44	A AA	A AA	A AA	A 93	6 1/	A AA	A AA	0.00	0 00	0.60	0 50	0.50				4			
<u> </u>	0.00	U 0.00	0.00	0.05	0.00	U.UU	V.UU	V.UU	7.U7	V.43	V 53	N.UU	0.00	0.00	0.00	0.05	0.50 1.97	1	1.97						
1 #	J 0.04	U U.US	V.14	.U.U5	כט.ע אור ה	U.UU A AA	0.03	0.03	0.00	0.00	0.32	0.18	0.28	0.46	0.05	0.23	2.39			2.39					-
5 S	; U.U! E A E!	U.U. 5 A 20	9.10	V.V3	v.U3	0.00	U Ud	0.60	0.83	0.60	0.55	0.64	0.46	1.10	0.83	1.47	12.57	r			12.5	7		•	
1 5	0.0	0.00	0.14	0.28	0.73	0.14	0.00	0.23	0.96	1.28	1.10	0.41	0.09	0.14	0.23	0.00	5./4	r				5.74			
8 14	0.0	0.00	0.00	0.00	0.00	0.00	0.00	0.18	0.37	0.87	0.23	0.00	0.05	0.00	0.00	0.00	1./0						1.70		
E	0.0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.05	0.09	0.00	0.00	0.00	0.00	0.00	0.14							0.14	
_				3.33		_																			25.01

# LaSalle Muclear Station 33 ft. Wind Speed and Direction

### April-Jume, 2002 200Ft-33Ft Delta-T (F)

12.6 - 18.5 mph

18.6 - 24.5 mph

> 24.5 mph

									_											(CODE TO T	1 1497 <i>(</i>	T 3 CCDC			
SPEED							***************************************	DIRECT	CION CI				**	ERWI	177	STATES	MORE T	<b>9</b> 11	MIT	STABI SU	A PTII (	lasses Ss	KS	KS	TOTAL
CLASS	N	MNE	NK	ENE	E	ESE	<b>S</b> E	<b>S</b> SE	S	SSW	SW	RSW	N	MAN	Mil	MM	TOTAL	<b>k</b> U	MU	ðŲ		90	FAL)	40	10mm
KU	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.28	0.41	0.09	0.00	0.00	0.00	0.00	0.00	0.78	0.78							
1 MU	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.09	0.41	0.00	0.05	0.00	0.09	0.09	6.00	0.73		0.73						
9 811	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.14	0.14	0.00	0.09	0.05	0.32	0.05	0.00	0.78			0.78					
- N	0.09	0.00	0.28	0.23	0.41	0.55	0.18	0.00	0.18	0.55	0.09	0.05	0.09	0.69	0.41	0.00	3.81				3.81				
2 SS	0.00	0.00	0.00	0.00	0.05	0.00	0.00	0.00	0.14	0.50	0.05	0.05	0.09	0.41	0.14	0.00	1.42					1.42			
4 MS	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00		0.00	0.00						0.00		
ES		0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00		•				• .	0.00	
		****	****	••••																					7.53
EU	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.28	0.00	0.00	0.00	0.00	0.00	0.00		0.28							•
G MU	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.05	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.05		0.05						
T SU	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.05	0.00	0.00	0,00	0.00	0.00	0.00	0.05			0.05	0.00				
E	0.00	0.00	0.00	0.00	0.14	0.00	0.00	0.00	0.00	0.23	0.00	0.00	0.05	0.50	0.05	0.00	0.96				0.96				
2 <b>S</b> S	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.09	0.14	0.23	0.05	0.00	0.50					0.50	A 60		
4 MS	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00						0.00	n .nn	
ES	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00							0.00	1.84
							•		•				_												1.02
***			e 49	9 81	c 22	4 33	2 26	E 07	0 00	 11 <i>4</i> 7	G 87	7 71	6 20	R 40	5.55	5.83	100.00	1.56	3.58	7.53	42.45	22.53	13.22	9.13	100.00
TOT	2.94	2.89	5.87	3.81	6.33	4.31	3.10	3.31	0.77	11.1/	3.01	1.11	V.63	0.10	3,33	3.03			••••	*****	٠.				
•																									
Win	l Direc	tion 1	by Sta	hility																					
11444			<b>5</b> 7 000															_							
	I	ENE	NK	ENE	ŧ	ESE	SE	SSE	8	SSH	SW	NSW	¥	MENW	MA	MAN	TOTAL	-8	TABILI	IY CLA	SSES-				
														0.00	0.00	A 00	1.56	p.	tremel	v Moch:	ahla				
	0.00	0.00				0.00	0.00	0.00	0.37	0.92				0.00	• • • •	0.00 0.05	3.58		derate						
	0.00	0.05	0.18	0.05		0.05	0.05	0.05	0.14	1.01	0.41	0.55	0.28	0.46	0.18 0.23	0.05	3.30 7.53		ightly						
	0.09						0.45	0.64	0.50	0.78	0.78		0.60	1.15	3.30	4.54			utral	<b>U</b> LLO COL	urc.				
	2.20	1.97	4.50				0.83	1.33	2.98		2.48	2.11		1.79	1.51	0.60			ightly	Stahl	s.				
	0.50						0.60	0.83	2.39		2.75	1.47	1.88			••••			derate						
	0.14	0.05	0.09	0.05	0.78	0.64	1.19	1.56	1.24	2.11	1.70	1.10	1.19	0.78					tremel						
	0.00	0.00	0.00	0.00	0.00	0.18	0.64	1.56	1.38	1.54	1.51	1.51	0.51	. 0.14	0.00	0.00	7.13		LI CINCA	7 0000					
									•																
Win	d Dire	atim	hv Vir	nd Snee	νđ																	•			
UTT	a pire	CCTOIL	יות ביי	m ppcc	-14																				
	K	MNE		KNI	K	ESE	SE	SSE	S	SSW	SH	WSW	K	INV	WW	ENW	TOTAL	-1	iind se	KED CI	asses-	•			
	_															<b>.</b>									
	0.00	0.00	0.0	0.00	0.00	0.00	6.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	) `	CA		<b></b>				
*	A 14	n 22	1 8 1	0 15	8 0 09	0.23	0.00	0.14	0.28	0.18	0.23	0.18	0.09	0.00	0.18	V.14	2.40	\$		3.5					
	1 47	15/	0.7	0.70	1.56	1.51	1.65	2.02	2.16	2.29	2.71	1.74	T.01	1.55	1.33	1.4/	40.40			7.5					
	0.73	0.78	1.7	1.33	3 2.52	1.24	1.65	2.48	3.26	2.98	4.08	3.90	3.07	4.20	2.10	4.40	30.0	,		12.5					
	A 50	A 3		. 4 4	1 54	. A 70	0.20	1 22	2 47	3 44	2.62	1.56	1.10	2.07	1.10	1.74	25.01	L	12.6	18.5	MIDIT.				

0.55 0.32 2.85 1.28 1.56 0.78 0.28 1.33 2.43 3.44 2.62 1.56 1.10 2.07 1.10 1.74 25.01

0.09 0.00 0.28 0.23 0.46 0.55 0.18 0.00 0.83 2.02 0.23 0.23 0.23 1.51 0.69 0.00 7.53

### LaSalle Muclear Station 375 ft. Wind Speed and Direction

### Number of Observations = 2178 Values are Percent Occurrence

SPEED							- WIND	DIREC	cion c	ASSES										STABI	LITY (	LASSES			
CLASS	Ĭ	MNE	N.	ENE	R	ESE	SE	SSE	S	SSW	SH	MSW	¥	WNW	W	INN	TOTAL	EU -	MU	SU	I	<b>S</b> S	MS	ES	TOTAL
CIENUT	-	Witn		2014	•		-																		
KU	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00							
M	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00		0.00						
C SU	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00			0.00					
1 1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00				0.00	A AA			
L SS	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00					0.00	A AA		
M MS	0.00	0.00	0.00	0.00	0.00		0.00	0.00		0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00						0.00	0.00	
ES	0.00	0.00	0,00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00						• • •	0.00	8 80
																		•							0.00
																	A AA								
KU	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00			0.00					0.00	A 80					*	•
MU	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00		0.00	6 66					
1 ST	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00			0.00	0.55				•.
- H	0.05	0.05	0.00	0.09	0.09	0.00	0.00	0.00	0.05	0.00	0.00	0.18	0.00	0.05	0.00	0.00					0.55	0.46			•
3 <b>S</b> S	0.00	0.00	0.05	0.05	0.09	0.05	0.00		0.05	0.05	0.00	0.00	0.05	0.00	0.05	0.00	0.46 0.00					V.10	0.00		
KS	0.00	0.00	0.00	0.00	0.00	0.00	0.00		0.00		0.00		0.00	0.00	0.00	0.00							4.40	0.00	
ES	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	<b>U.W</b>								1.01
									A A0	6 60	A 82	A AA	0.00	0.00	0.00	0.00	0.00	0.00							
	0.00		0.00	0.00	0.00		0.00			0.00			0.00	0.00	0.00	0.00		4.40	0.00						
	0.00	8.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00		0.00	0.00	0.00	0.00	0.00	0.00			****	0.00					
4 SU	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00			0.00		0.09	0.00	0.18	0.32				••••	5.51				
- N	0.51		0.51	0.64	0.73		0.23	0.28	0.28		0.37 0.18	_	0.03	0.09	0.14	0.00						2.39			
7 <b>S</b> S	0.18				0.09	0.14			0.28		0.05			0.00		0.00							0.41		
	0.00					0.00 0.00	0.00	0.05	0.00					0.00		0.00								0.14	
ES.	0.00	0.00	0.00	0.00	V.00	<b>V.V</b> U	<b>V.</b> VV	V.V3	0.00	V.VV	4.44	0.00	v.v,	<b>V.V</b>	*.**	••••									8.45
														٠											
IST.	0.00	0.00		0.00	0.00	8 80	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00							
. KU			0.00	0.00	0.00	0.00	0.00					0.00	0.00	0.00	0.00	0.00	0.00		6.00						
8 80			0.00	0.00	6.00	0.00		0.00			0.00	0.00	0.00	0.00	0.00	0.00	0.00			0.00					
. Y	0.64		0.64	0.32				- 44			0.78	1.33	0.46	0.55	1.06	1.33	11.89				11.89				
1 <b>S</b> S	A 55	A 10	0.37	0.46	0.32	0.32	0.37	0.23	0.14	0.18	0.18	0.46	0.18	0.18								4.45			
9 MC	A 60	0.00	N 0.0	0.00	0.00	0.05	0.14	0.32	0.18	0.37	0.28	0.18	0.09	0.14	0.14	0.14	2.02						2.02		
RS	0.00	0.00	0.00	0.00	0.00	0.05	0.00	0.00	0.14	0.18	0.00	0.05	0.05	0.00	0.05	0.00	0.51							0.51	
_	****		• ••••			• • • • • • • • • • • • • • • • • • • •																			18.87
															-										
<b>E</b> TI	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0		0.00							
1 187	0.00	0.00	0.00	0.0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	) 0.80		0.00						
3 50	0.00	0.00	0.00	0.0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0	0.00			0.00					
- 1	0.23	0.32	1.8	1.19	0.60	0.32	0.28	0.73	0.69	0.52	1.15	1.15	1.10	1.97	2.07	1.5	3 15.33				15.93				
1 59	0.28	0.2	0.0	5 0.23	3 0.41	0.28	0.23	0.41	0.37	0.28	0.73	0.64	0.51	. <b>0.6</b> 0	0.28	0.18	5.74					5.74	9 94		
R MS	0.09	0.00	0.00	0.0	0.00	0.14	0.23	0.51	0.18	0.51	0.51	0.46	0.14	0.23	V.14	0.10	3.31						3.31	A 43	
ES	0.0	0.0	0.0	0.0	0.00	0.00	0.05	0.09	0.18	0.23	0.05	0.14	0.00	0.00	0.00	0.0	0.73	٠.						0.73	25.71
																						•			23.11

### April-Jume, 2002 375Ft-33Ft Delta-T (F)

18.6 - 24.5 mph > 24.5 mph

																				ens n	PETRAL	nt a enge			
SPEKD							MIND	DIRECT		LASSES				2871	 tm:	VIII.	WACTI T	277	Mil	eli Piari	m IPIII (	Carcail SS	MS	ES	TOTAL
CLASS	ľ	INK	IK	ENE	K	ese	Se	<b>S</b> SE	S	SSW	SH	WSW	R	MAN	M	MIN	TOTAL	EU	NU	SU	B	90	Pio	<b>B</b> Q	IOTUU
1911	0.00	0.00	A An	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00							
	0.00	0.00	0.00	0.00	0.00	0.00	0.00		0.05		0.00	0.00	0.00	0.00	0.08	0.00	0.05		0.05						
1 100	0.00	0.00	0.00	••••	0.00		0.00	••••	0.18		0.09	0.00	0.00	0.00	0.00	0.00	0.55			0.55					
9 80	0.05	0.00	0.00	0.00					0.92				0.64		1.06	0.83	12.72				12.72				
- N	0.83	0.37	1.79	1.10	0.55	0.45	0.28		0.37	0.63		0.46	0.51		0.51	0.37	6.11					6,11			
2 \$5	0.09	0.00	0.05	0.14	0.64	0.64	0.37		0.37	0.14	-	0.60		0.32	0.18	0.09	3.67					****	3.67		
4 MS	0.00	0.00	0.00	0.00	0.00	0.09	0.18			0.23		0.18	0.14			0.00	0.73					٠.	••••	0.73	-
ES	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.14	V.23	V.UJ	.0.10	A114	0.00	V. UV	0.00	4.13								23.83
-							0 00	n AA	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00							
EU	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	••••	0.09	0.00	0.00	0.00	0.00	0.00	0.14	****	0.14						
G MU	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00			0.05	0.00	0.00	0.00	0.05	0.00	0.64		****	0.64					
T SU	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.05	• • • •		0.18	0.28	1.29	1.10	0.14	8.31				8.31				
	0.14	0.00	0.73	0.23	0.51	0.73	0.28	0.09	0.55					0.41	0.37	0.00	7.25				. 0132	7.25			
2 8\$	0.00	0.00	0.00	0.00	0.09	0.32	0.14	0.09	0.83		1.38	0.73	0.28 0.51		0.00	0.00	4.50						4.50		
4 MS	0.00	0.00	0.00	0.00	0.00	0.05	0.32	0.69	0.92			0.23			0.00	0.00	1.29						1.50	1.29	
<b>B</b> S	0.00	0.00	0.00	0.00	0.00	0.00	0.05	0.09	0.73	0.14	0.00	0.28	0.00	0.00	<b>0.0</b> 0	U.00	1.43	•						4.67	22.13
								•			-														86143
									*																
								- 44		44 84	A 40	4 75	F 80	9 91	7 50	E 80	100 00	8 66	A 10	1 10	E# 01	26 40	12 01	3 40	100 00
TOT	3.63	2.94	6.43	4.64	4.36	3.99	3.81	5.14	9.04	11.94	9.18	6.72	5.68	1.11	1.30	3.00	100.00	U.UU	0.10	1.17	32.31	40.40	17,71	3,40	100.00
																							• .		
Wind	Direc	ction	by Sta	bility													• • •	•	•			·			
	. 1	MNE	MK	ENE	7	ESE	SE	SSE	2	SSW	SW	WSW	¥		IIW	MNA	TOTAL	-S'	PABILIT	i CLA	SSES-				
	B	TILL	2.5	ana	•	<b>200</b>	40	900	0	QU:	ŲH.	NUM	-	******		<b>,</b>									
	0.00	0.00	0.00	0 00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	6.00	0.00	0.00	0.00	Ext	remely	Unst	able				
	0.00	0.00	0.00	0.00	• • • • •	0.00	0.00	0.00	0.05	0.05	0.09	0.00	0.00	0.00	0.00	0.00	0.18		ierately		_				
	0.05	0.00		****			0.00	0.00	0.23	0.73	0.14	0.00	0.00	0.00	0.05	0.00	1.19		ightly i						
	2.39						1 61	2.02	3.90		3.40	3.99	2.57	5.10	5.46	3.95			itral						
	1.10						1 24	1.10	2.02		3.21		1.65	1.84	1.56				ightly :	Stabl	e				
							0.87		1.65		• • • •			0.78	0.46				ieratel						-
	0.09	0.00	0.00	CV.V	0.00	0.05	0.07	1.12	1 10										remely				100		
	<b>U.U</b> U	U.QU	0.00	0.00	<b>0.0</b> 0	Ų.V3	0.43	¥.23	1117	V.70	V.U.	4.01	4120	****	••••	****		,	<i>1</i>						
																	*								
Win	1 Dire	ction	hv Nir	d Spee	đ											•									
11		VV2V**	<b>-</b> 2	m opec	-																				
	X	IN	10	ENE	I	ESE	SE	SSE	8	SSW	SW	NSW	¥	MAW	W	MNW	TOTAL	-1	IND SPE	KD CL	asses-	•			
	-	BUILD				-			•						•										
	8 60	0.00	A A1	0.00	. 6 60	0.00	0 00	0.00	6.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00		CAL	M					
	7.VU	0.00	4.VC	, V.VV	, y.40   ß 14	0.05	8 BA	0.05	0.00	0.05	0.00	0.18	0.05	0.05	0.05	0.00	1.01			3.5	mph	•			
	V.VJ A £A	0.03	V.U.	, V.17	V 62	0.03 14 A	A 27	0.03	0.05	0 27	0.60	0.55	0.37	0.18	0.32	0.32	8.45		3.6						
	7.07	9./0	V.0	. U.03   ∧ 76	, v.03	V.31	1 10	1 15	1 89	1 66	1 24	2.07	0.78	0.R7	1.47	1.56	18.87		7.6 -				•		
	7.13	1.13	1 4 61	. V./(	, V.J3 1 A1	N.DL	1.V0	1.23	1 47	1 63	2 12	2 76	1 74	2.80	2.48	1.70	25.71		12.6 -						
	V.DU	V.01	1.3	) 1.5/   1.5/	. 1.VJ	. V./J	0.10	U 83	2 02	1.84	2.43	2.16	1.88	2.02	1.74	1.29	23.83		18.6 -						

0.96 0.37 1.84 1.24 1.19 1.19 0.63 0.63 2.02 1.84 2.43 2.16 1.88 2.02 1.74 1.29 23.83 0.14 0.00 0.73 0.23 0.60 1.10 0.78 0.96 3.08 6.11 2.48 1.42 1.06 1.79 1.52 0.14 22.13

# LaSalle Muclear Station 33 ft. Wind Speed and Direction

### Number of Observations = 1912 Values are Percent Occurrence

SPEKD							- VIND	DIREC	PTON C	LASSES	****				4					STAB	LITY (	TASSES			
CLASS	H	ENE	MB	ENE	E	ESE	SE	SSE	\$	SSW	SW	NSW	¥	WATE	NW	MNW	TOTAL	EU	MU	SU	X	<b>\$</b> \$	MS	ES	TOTAL
EU	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00							
MU	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00		0.00						
C SU	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00			0.00	0.00				
L SS	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00				V.V	0.00			
H MS	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00						0.00		
ES	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	• .					•	0.00	0.00
																									V.VV
EU	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00			٠. '				
MU	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00		0.00			••			
1 SU	0.00	0.00	0.00	0.00	0.00	0.00 0.16	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00 1.05			0.00	1.05				
3 SS	0.21	0.05	0.05	0.05	0.05	0.05	0.10	0.10	0.10	0.00	0.10	0.00	0.00	0.00	0.00	0.00	0.78				. 4.93	Q.78			
	0.05	0.10	0.00	0.00	0.05	0.00	0.00	0.00	0.10	0.05	0.05	0.05	0.31	0.05	0.05	0.05	0.94						0.94		
ES	0.05	0.00	0.05	0.00	0.10	0.10	0.16	0.05	0.00	0.05	0.10	0.26	0.37	0.16	0.16	0.21	1.83							1.83	4.60
																									1.00
EU	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.05	0.05	0.00	0.00	0.00	0.60	0.00	0.10	0.10							
MU	9.05	0.26	0.10	0.05	0.00	0.16	0.05	0.10	0.10	0.10	0.16	0.10	0.05	0.05	0.00	0.05	1.41		1.41						
4 SU	0.10	0.26	0.31	0.31	0.52	0.21	0.05	0.26	0.52	0.42	0.26 1.15	0.47 0.94	0.52 1.10	0.31	0.05	0.10	4.71			4.71	11:.72				
- N 7 SS	0.94	1.05	0.52	0.47	0.52	0.68	1.20 0.26	0.68	0.47	0.37	0.63	0.47	0.26	0.47	0.37	0.31	7.37				11.72	7.37			
	0.05	0.58	0.05	0.00	1.15	1.26	0.58		1.41	1.10	1.31	0.58	0.21	0.37	0.26	0.16	9.73						9.73		
ES	0.05	0.05	0.00	0.05	0.47	1.52	0.94	1.67	1.05	1.46	1.94	1.62	0.78	0.89	0.10	0.05	12.66							12.66	47.70
																			٠						2/./0
EU	0.00	6.00	0.21	0.10	0.00	0.00	0.00	0.00	0.00	0.37	0.16	0.78	0.47	0.00	0.00	0.00	2.09	2.09				. •			
M	0.00	0.16	0.31	0.89	0.10	0.00	0.05	0.10	0.10	0.42	0.47	0.52	0.58	0.21	0.05	0.00	3.97	•	3.97	2 66		•			
8 SU	0.00	0.05	0.16 1.31	0.47 0.68	0.58	0.05 0.31	0.26	0.10	0.26 0.68	0.21 1.20	0.47 1.36	0.47	0.21 0.78	0.31	0.00	0.05	3.66 11.40			3.66	11.40				
1 <b>S</b> S	0.52	0.16			1.26		0.31		0.78		1.62		0.26	0.26	0.16	0.47	10.93					10.93		÷	
2 MS	0.00	0.00	0.05	0.00	1.10	0.05	0.05	0.16	0.99	0.99	0.26	0.26	0.00	0.00	0.00	0.00	3.92						3.92		
ES	0.00	0.00	0.00	0.00	0.10	0.16	0.00	0.10	0.31	0.21	0.47	0.05	0.05	0.00	0.00	0.00	1.46							1.46	37.45
																							•		37,43
																	1.10	1.10							
1 100	0.00	0.00	0.00	0.16	0.05	0.00	0.00	0.00	0.10	0.26	0.26	0.00	0.10	0.05	0.00	0.05	1.05		1.05						•
3 20	0.00	0.00	0.00	0.05	0.21	0.00	0.00	0.00	0.10 n %	0.26 n c9	0.26	0.16 A 27	0.10 0.10	0.10 A 21	0.00	0.00	1.26 4.71			1.26	4.71				
1 <b>S</b> S	0.10	0.00	v.18 0.16	0.47	0.42	0.00	0.00	0.00	0.10	0.21	0.52	0.10	0.00	6.00	0.00	0.05	1.94				21/4	1.94			
8 MS	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00						0.00		
ES	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00							0.00	18 6#
																									10.04

### LaSalle Nuclear Station 33 ft. Wind Speed and Direction

							RITITO	BIBBA	87031 A	10000										CTA DI	11.19V <i>(</i>	LASSES			
SPEED	N	NONE	ĸ	ENE	 R	ESE	- WIND Se	DIREC	tion c S	Lasses SSW	SN	NSW	ľ	NOVIW	NA.	MAN	TOTAL	EU	MIT	2 <u>1</u>	I .	28 88	MS	KS	TOTAL
CETOO		SULL		81111	•	204	4	402	•				,-												
								A AA	6 60	A AF	A A0	e 66	0.00	A AA	0.00	A 80	0.05	A AE							
		0.00	0.00	0.00	0,00	0.00	0.00	0.00	0.00	0.05 0.05	0.00	0.00	0.00	0.00	0.00	0.00	0.05	V.V3	0.05						
1 MU 9 SU	0.00	0.00	0.00	0.00	0.00		0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00		••••	0.00					
- II	0.00	0.00	0.00	0.00	0.00	•	0.00	0.00	0.00	0.00	0.05	0.00	0.00	0.00	0.00	0.00	0.05			••••	0.05				
2 <b>S</b> S	0.00	0.00	0.00	0.00	0.00	•	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00					0.00			
4 KS	0.00	0.00	0.00	0.00	0.00		0.00	0.00	0.05	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.05						0.05		
ES	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00							0.00	
										-															0.21
												A . AA			0.00	A A0	A AA	A A0							
								0.00			0.00	•	0.00	0.00	0.00	0.00	0.00	U.UV	0.00						
GW		0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00		V.VV	0.00					
T SU	0.00	0.00	0.00	0.00		0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00		0.00	0.00	0.00			••••	0.00				
	0.00	0.00	0.00	0.00		0.00	0.00	0.00	6.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00					0.00			
4 KS	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00		0.00	0.00	0.00	0.00	0.00						0.00		
	0.00	0.00	0.00		0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00							0.00	
											•.														0.00
						٠				•														. ••	
<b>6</b> 00	1 50	4 60	E 95	<i>C</i> 40	9 70	E 90	4 24	E 87	0 11	10 70	12 66	9 10	6 43	5 62	1 72	2 41	180 00	3 35	6.49	9.62	28.92	21.03	14.64	15.95	100.00
101	3.30	1.60	3.13	6.47	0.73	J.40	3.63	J.V/	6.11	13.12	12.00	7.20	0.13	J.V4	2.70	•,72	200.00	7,77	V,	,,,,,					
Wind	Direc	tion b	y Stab	ility						•		•													
Wind			<u>.</u>	-	ĸ	RSR.	<b>S</b> R	SSE	S	SSV	SW	WSW	ij	WNW	Mv	MNW	TOTAL	-\$1	abilit	Y CLAS	SSES-			•	
Wind	Direc	tion b	y Stal	ility ENE	ľ	ESE	SE	SSE	S	SSK	SW	MSW	Ħ.	MINN	<b>M</b> V	MNW									
Wind	N		TE	-	E 0.00		SB 6.00	0.00	0.00	0.63	0.42	0.94	W 0.58	0.10	0.00	0.00	3.35	Ext	remely	Unsta	ble				
Wind	N 0.10 0.05	ENE 0.00 0.42	NR 0.26 0.42	ENE 0.31 1.10	0.00 0.16	0.00 0.16	0.00 0.10	0.00 0.21	0.00 0.31	0.63 0.84	0.42 0.89	0.94 0.63	0.73	0.10 0.31	0.00 0.05	0.00 0.10	3.35 6.49	Ext Mod	remely eratel	Unsta y Unst	able table				
Wind	N 0.10 0.05 0.10	0.00 0.42 0.31	NE 0.26 0.42 0.47	ENE 0.31 1.10 0.84	0.00 0.16 1.31	0.00 0.16 0.26	0.00 0.10 0.31	0.00 0.21 0.37	0.00 0.31 0.89	0.63 0.84 0.89	0.42 0.89 0.99	0.94 0.63 1.10	0.73 0.84	0.10 0.31 0.73	0.00 0.05 0.05	0.00 0.10 0.16	3.35 6.49 9.62	Ext Mod Sli	remely erately ghtly	Unsta y Unst	able table				
Wind	N 0.10 0.05 0.10 2.20	0.00 0.42 0.31 1.67	NE 0.26 0.42 0.47 2.67	ENE 0.31 1.10 0.84 1.88	0.00 0.16 1.31 1.94	0.00 0.16 0.26 1.15	0.00 0.10 0.31 1.52	0.00 0.21 0.37 1.26	0.00 0.31 0.89 1.52	0.63 0.84 0.89 2.25	0.42 0.89 0.99 3.35	0.94 0.63 1.10 2.35	0.73 0.84 2.04	0.10 0.31 0.73 1.67	0.00 0.05 0.05 0.58	0.00 0.10 0.16 0.89	3.35 6.49 9.62 28.92	Ext Mod Sli Neu	remely erately ghtly tral	Unsta V Unst Instal	able table ble				
Wind	N 0.10 0.05 0.10 2.20 0.89	0.00 0.42 0.31 1.67	0.26 0.42 0.47 2.67 1.78	ENE 0.31 1.10 0.84 1.88 2.30	0.00 0.16 1.31 1.94 2.41	0.00 0.16 0.26 1.15 0.63	0.00 0.10 0.31 1.52 0.58	0.00 0.21 0.37 1.26 0.58	0.00 0.31 0.89 1.52 1.46	0.63 0.84 0.89 2.25 2.25	0.42 0.89 0.99 3.35 2.88	0.94 0.63 1.10 2.35 1.26	0.73 0.84 2.04 0.52	0.10 0.31 0.73 1.67 0.73	0.00 0.05 0.05 0.58 0.52	0.00 0.10 0.16 0.89 0.78	3.35 6.49 9.62 28.92 21.03	Ext Mod Sli New Sli	remely erately ghtly tral ghtly	Unsta y Unst Unstal Stable	able table ole				
Wind	N 0.10 0.05 0.10 2.20 0.89 0.10	0.00 0.42 0.31 1.67 1.46 0.68	0.26 0.42 0.47 2.67 1.78 0.10	ENE 0.31 1.10 0.84 1.88 2.30 0.00	0.00 0.16 1.31 1.94 2.41 2.30	0.00 0.16 0.26 1.15 0.63 1.31	0.00 0.10 0.31 1.52 0.58 0.63	0.00 0.21 0.37 1.26 0.58 0.84	0.00 0.31 0.89 1.52 1.46 2.56	0.63 0.84 0.89 2.25 2.25 2.14	0.42 0.89 0.99 3.35 2.88 1.62	0.94 0.63 1.10 2.35 1.26 0.89	0.73 0.84 2.04 0.52 0.52	0.10 0.31 0.73 1.67 0.73 0.42	0.00 0.05 0.05 0.58 0.52 0.31	0.00 0.10 0.15 0.89 0.78 0.21	3.35 6.49 9.62 28.92 21.03 14.64	Ext Mod Sli Neu Sli Mod	remely erately ghtly tral ghtly eratel	Unsta y Unst Unstal Stable y Stal	able table ole				
Wind	N 0.10 0.05 0.10 2.20 0.89 0.10	0.00 0.42 0.31 1.67 1.46 0.68	0.26 0.42 0.47 2.67 1.78 0.10	ENE 0.31 1.10 0.84 1.88 2.30 0.00	0.00 0.16 1.31 1.94 2.41 2.30	0.00 0.16 0.26 1.15 0.63 1.31	0.00 0.10 0.31 1.52 0.58 0.63	0.00 0.21 0.37 1.26 0.58 0.84	0.00 0.31 0.89 1.52 1.46 2.56	0.63 0.84 0.89 2.25 2.25 2.14	0.42 0.89 0.99 3.35 2.88 1.62	0.94 0.63 1.10 2.35 1.26 0.89	0.73 0.84 2.04 0.52 0.52	0.10 0.31 0.73 1.67 0.73 0.42	0.00 0.05 0.05 0.58 0.52 0.31	0.00 0.10 0.15 0.89 0.78 0.21	3.35 6.49 9.62 28.92 21.03	Ext Mod Sli Neu Sli Mod	remely erately ghtly tral ghtly	Unsta y Unst Unstal Stable y Stal	able table ole				
	N 0.10 0.05 0.10 2.20 0.89 0.10 0.10	0.00 0.42 0.31 1.67 1.46 0.68 0.05	0.26 0.42 0.47 2.67 1.78 0.10 0.05	ENE 0.31 1.10 0.84 1.88 2.30 0.00 0.05	0.60 0.16 1.31 1.94 2.41 2.30 0.68	0.00 0.16 0.26 1.15 0.63 1.31	0.00 0.10 0.31 1.52 0.58 0.63	0.00 0.21 0.37 1.26 0.58 0.84	0.00 0.31 0.89 1.52 1.46 2.56	0.63 0.84 0.89 2.25 2.25 2.14	0.42 0.89 0.99 3.35 2.88 1.62	0.94 0.63 1.10 2.35 1.26 0.89	0.73 0.84 2.04 0.52 0.52	0.10 0.31 0.73 1.67 0.73 0.42	0.00 0.05 0.05 0.58 0.52 0.31	0.00 0.10 0.15 0.89 0.78 0.21	3.35 6.49 9.62 28.92 21.03 14.64	Ext Mod Sli Neu Sli Mod	remely erately ghtly tral ghtly eratel	Unsta y Unst Unstal Stable y Stal	able table ole				
	N 0.10 0.05 0.10 2.20 0.89 0.10 0.10	0.00 0.42 0.31 1.67 1.46 0.68 0.05	0.26 0.42 0.47 2.67 1.78 0.10 0.05	ENE 0.31 1.10 0.84 1.88 2.30 0.00	0.60 0.16 1.31 1.94 2.41 2.30 0.68	0.00 0.16 0.26 1.15 0.63 1.31	0.00 0.10 0.31 1.52 0.58 0.63	0.00 0.21 0.37 1.26 0.58 0.84	0.00 0.31 0.89 1.52 1.46 2.56	0.63 0.84 0.89 2.25 2.25 2.14	0.42 0.89 0.99 3.35 2.88 1.62	0.94 0.63 1.10 2.35 1.26 0.89	0.73 0.84 2.04 0.52 0.52	0.10 0.31 0.73 1.67 0.73 0.42	0.00 0.05 0.05 0.58 0.52 0.31	0.00 0.10 0.15 0.89 0.78 0.21	3.35 6.49 9.62 28.92 21.03 14.64	Ext Mod Sli Neu Sli Mod	remely erately ghtly tral ghtly eratel	Unsta y Unst Unstal Stable y Stal	able table ole				
	N 0.10 0.05 0.10 2.20 0.89 0.10 0.10	0.00 0.42 0.31 1.67 1.46 0.68 0.05	0.26 0.42 0.47 2.67 1.78 0.10 0.05	ENE 0.31 1.10 0.84 1.88 2.30 0.00 0.05	0.00 0.16 1.31 1.94 2.41 2.30 0.68	0.00 0.16 0.26 1.15 0.63 1.31	0.00 0.10 0.31 1.52 0.58 0.63 1.10	0.00 0.21 0.37 1.26 0.58 0.84	0.00 0.31 0.89 1.52 1.46 2.56	0.63 0.84 0.89 2.25 2.25 2.14	0.42 0.89 0.99 3.35 2.88 1.62	0.94 0.63 1.10 2.35 1.26 0.89	0.73 0.84 2.04 0.52 0.52	0.10 0.31 0.73 1.67 0.73 0.42	0.00 0.05 0.05 0.58 0.52 0.31	0.00 0.10 0.16 0.89 0.78 0.21 0.26	3.35 6.49 9.62 28.92 21.03 14.64	Ext Mod Sli Med Sli Mod Ext	remely erately ghtly tral ghtly eratel	Unsta y Unstal Unstal Stable y Stal Stabl	able cable ole e ole le				
	N 0.10 0.05 0.10 2.20 0.89 0.10 0.10	0.00 0.42 0.31 1.67 1.46 0.68 0.05	0.26 0.42 0.47 2.67 1.78 0.10 0.05	ENE 0.31 1.10 0.84 1.88 2.30 0.00 0.05	0.60 0.16 1.31 1.94 2.41 2.30 0.68	0.00 0.16 0.26 1.15 0.63 1.31 1.78	0.00 0.10 0.31 1.52 0.58 0.63 1.10	0.00 0.21 0.37 1.26 0.58 0.84 1.83	0.60 0.31 0.89 1.52 1.46 2.56 1.36	0.63 0.84 0.89 2.25 2.25 2.14 1.73	0.42 0.89 0.99 3.35 2.88 1.62 2.51	0.94 0.63 1.10 2.35 1.26 0.89 1.94	0.73 0.84 2.04 0.52 0.52 1.20	0.10 0.31 0.73 1.67 0.73 0.42 1.05	0.00 0.05 0.05 0.58 0.52 0.31 0.26	0.00 0.10 0.16 0.89 0.78 0.21 0.26	3.35 6.49 9.62 28.92 21.03 14.64 15.95	Ext Mod Sli Med Sli Mod Ext	remely erately ghtly itral ghtly erately remely	Unsta y Unstal Unstal Stable Stable Stable	able cable ole e ole le				
	N 0.10 0.05 0.10 2.20 0.89 0.10 0.10 Direct	0.00 0.42 0.31 1.67 1.46 0.68 0.05	0.26 0.42 0.47 2.67 1.78 0.10 0.05	ENE 0.31 1.10 0.84 1.88 2.30 0.00 0.05	0.00 0.16 1.31 1.94 2.41 2.30 0.68	0.00 0.16 0.26 1.15 0.63 1.31 1.78	0.00 0.10 0.31 1.52 0.58 0.63 1.10	0.00 0.21 0.37 1.26 0.58 0.84 1.83	0.00 0.31 0.89 1.52 1.46 2.56 1.36	0.63 0.84 0.89 2.25 2.25 2.14 1.73	0.42 0.89 0.99 3.35 2.88 1.62 2.51	0.94 0.63 1.10 2.35 1.26 0.89 1.94	0.73 0.84 2.04 6.52 0.52 1.20	0.10 0.31 0.73 1.67 0.73 0.42 1.05	0.00 0.05 0.05 0.58 0.52 0.31 0.26	0.00 0.10 0.15 0.89 0.78 0.21 0.26	3.35 6.49 9.62 28.92 21.03 14.64 15.95	Ext Mod Sli New Sli Mod Ext	remely erately tral ghtly lerately remely	Unsta y Unstal Instal Stable y Stal Stabl	able cable cole de de				•
Wind	N 0.10 0.05 0.10 2.20 0.89 0.10 0.10 Direct M 0.00 0.37	0.00 0.42 0.31 1.67 1.46 0.68 0.05	0.26 0.42 0.47 2.67 1.78 0.10 0.05 Wind	ENE 0.31 1.10 0.84 1.88 2.30 0.00 0.05 ENE 0.00 0.10	0.00 0.16 1.31 1.94 2.41 2.30 0.68	0.00 0.16 0.26 1.15 0.63 1.31 1.78	0.00 0.10 0.31 1.52 0.58 0.63 1.10	0.00 0.21 0.37 1.26 0.58 0.84 1.83 SSE 0.00 0.31	0.00 0.31 0.89 1.52 1.46 2.56 1.36	0.63 0.84 0.89 2.25 2.25 2.14 1.73 SSW 0.00 0.10	0.42 0.89 0.99 3.35 2.88 1.62 2.51	0.94 0.63 1.10 2.35 1.26 0.89 1.94 WSW 6.00 0.37	0.73 0.84 2.04 0.52 0.52 1.20 W	0.10 0.31 0.73 1.67 0.73 0.42 1.05	0.00 0.05 0.05 0.58 0.52 0.31 0.26	0.00 0.10 0.15 0.89 0.78 0.21 0.26	3.35 6.49 9.62 28.92 21.03 14.64 15.95	Ext Mod Sli New Sli Mod Ext	remely eratel ghtly tral ghtly eratel remely  ND SPE  C A L	Unstal y Unstal Stable Stable ED CLI M 3.51	able cable cole cole cole cole cole cole cole co				
Wind	N 0.10 0.05 0.10 2.20 0.89 0.10 0.10 Direct N 0.00 0.37 1.41	0.00 0.42 0.31 1.67 1.46 0.68 0.05 ction I	0.26 0.42 0.47 2.67 1.78 0.10 0.05 Wind ME 0.00 0.16 1.41	ENE 0.31 1.10 0.84 1.88 2.30 0.00 0.05 ENE 0.00 0.10 1.26	0.00 0.16 1.31 1.94 2.41 2.30 0.68 1 8	0.00 0.16 0.26 1.15 0.63 1.31 1.78 ESE 0.00 0.31 4.34	0.00 0.10 0.31 1.52 0.58 0.63 1.10 SE 0.00 0.26 3.09	0.00 0.21 0.37 1.26 0.58 0.84 1.83 SSE 0.00 0.31 3.66	0.00 0.31 0.89 1.52 1.46 2.56 1.36 8 0.00 0.26 4.08	0.63 0.84 0.89 2.25 2.14 1.73 SSW 0.00 0.10 3.82	0.42 0.89 0.99 3.35 2.88 1.62 2.51 SW 0.00 6.26 5.49	0.94 0.63 1.10 2.35 1.26 0.89 1.94 WSW 0.00 0.37 4.18	0.73 0.84 2.04 0.52 0.52 1.20 W 6.00 0.73 2.93	0.10 0.31 0.73 1.67 0.73 0.42 1.05	0.00 0.05 0.05 0.58 0.52 0.31 0.26	0.00 0.10 0.16 0.89 0.78 0.21 0.26	3.35 6.49 9.62 28.92 21.03 14.64 15.95 TOTAL 0.00 4.60 47.70	Ext Mod Sli New Sli Mod Ext	remely eratel ghtly eratel ghtly eratel remely C & L	Unstate y Unstate y Unstate Unstate Stable Stable Stable M 3.5 1 7.5 1	able cable cle cle cle cle cle cle cle cle cle c				
Wind	N 0.10 0.05 0.10 2.20 0.89 0.10 0.10 Direct N 0.00 0.37 1.41 1.36	0.00 0.42 0.31 1.67 1.46 0.68 0.05 etion l	0.26 0.42 0.47 2.67 1.78 0.10 0.05 WR 0.00 0.16 1.41 3.19	ENE 0.31 1.10 0.84 1.88 2.30 0.00 0.05 ENE 0.00 0.10 1.26 3.56	0.00 0.16 1.31 1.94 2.41 2.30 0.68 B 0.00 0.26 3.56 4.08	0.00 0.16 0.26 1.15 0.63 1.31 1.78 ESE 0.00 0.31 4.34 0.63	0.00 0.10 0.31 1.52 0.58 0.63 1.10 EE 0.00 0.26 3.09 0.89	0.00 0.21 0.37 1.26 0.58 0.84 1.83 SSE 0.00 0.31 3.66 1.10	0.00 0.31 0.89 1.52 1.46 2.56 1.36 8 0.00 0.26 4.08 3.14	0.63 0.84 0.89 2.25 2.14 1.73 SSW 0.00 0.10 3.82 5.13	0.42 0.89 0.99 3.35 2.88 1.62 2.51 SH 0.00 6.26 5.49 4.81	0.94 0.63 1.10 2.35 1.26 0.89 1.94 WSW 0.00 0.37 4.18 3.77	0.73 0.84 2.04 0.52 0.52 1.20 W 6.00 0.73 2.93 2.35	0.10 0.31 0.73 1.67 0.73 0.42 1.05	0.00 0.05 0.05 0.58 0.52 0.31 0.26 MW 0.00 0.21 1.15 0.42	0.00 0.10 0.16 0.89 0.76 0.21 0.26	3.35 6.49 9.62 28.92 21.03 14.64 15.95 TOTAL 0.00 4.60 47.70 37.45	Ext Mod Sli New Sli Mod Ext	remely eratel ghtly tral ghtly leratel remely RD SPE C A L 3.6 - 7.6 -	Unstate y Unstate y Unstate Unstate Unstate Unstate Unstate y Stable Stable M 3.5 1 7.5 1 12.5 1	able cable cole cole cole cole cole cole cole co				
Wind	N 0.10 0.05 0.10 2.20 0.89 0.10 0.10 Direct N 0.00 0.37 1.41 1.36 0.42	0.00 0.42 0.31 1.67 1.46 0.68 0.05 etion l	0.26 0.42 0.47 2.67 1.78 0.10 0.05 WR 0.00 0.16 1.41 3.19 0.99	ENE 0.31 1.10 0.84 1.88 2.30 0.00 0.05 ENE 0.00 0.10 1.26 3.56 1.57	0.00 0.16 1.31 1.94 2.41 2.30 0.68 B 0.00 0.26 3.56 4.08 0.89	0.00 0.16 0.26 1.15 0.63 1.31 1.78 ESE 0.00 0.31 4.34 0.63 0.00	0.00 0.10 0.31 1.52 0.58 0.63 1.10 SE 0.00 0.26 3.09 0.89 0.00	0.00 0.21 0.37 1.26 0.58 0.84 1.83 SSE 0.60 0.31 3.66 1.10 0.00	0.00 0.31 0.89 1.52 1.46 2.56 1.36 8 0.00 0.26 4.08 3.14 0.58	0.63 0.84 0.89 2.25 2.25 2.14 1.73 SSW 0.00 0.10 3.82 5.13 1.57	0.42 0.89 0.99 3.35 2.88 1.62 2.51 SH 0.00 0.26 5.49 4.81 2.04	0.94 0.63 1.10 2.35 1.26 0.89 1.94 WSW 0.00 0.37 4.18 3.77 0.78	0.73 0.84 2.04 0.52 0.52 1.20 W 6.00 0.73 2.93 2.35 0.42	0.10 0.31 0.73 1.67 0.73 0.42 1.05	0.00 0.05 0.05 0.58 0.52 0.31 0.26 MW 0.00 0.21 1.15 0.42 0.00	0.00 0.10 0.16 0.89 0.78 0.21 0.26 MNW 0.00 0.31 0.94 0.84	3.35 6.49 9.62 28.92 21.03 14.64 15.95 TOTAL 0.00 4.60 47.70 37.45 10.04	Ext Mod Sli New Sli Mod Ext	remely eratel ghtly eratel ghtly eratel remely C & L	Unstate y Unstate y Unstate y Unstate Unstate y Stable Stable Stable M 3.5 m 7.5 m 12.5 m 18.5 m 18.5 m	able cable cle cle cle cle cle cle cle cle cle c				
Wind	N 0.10 0.05 0.10 2.20 0.89 0.10 0.10 Direc	0.00 0.42 0.31 1.67 1.46 0.68 0.05 etion l	0.26 0.42 0.47 2.67 1.78 0.10 0.05 WE 0.00 0.16 1.41 3.19 0.99	ENE 0.31 1.10 0.84 1.88 2.30 0.00 0.05 ENE 0.00 0.10 1.26 3.56 1.57 0.00	0.00 0.16 1.31 1.94 2.41 2.30 0.68 8 0.00 0.26 3.56 4.08 0.89 0.00	0.00 0.16 0.26 1.15 0.63 1.31 1.78 ESE 0.00 0.31 4.34 0.63 0.00 0.00	0.00 0.10 0.31 1.52 0.58 0.63 1.10 8E 0.00 0.26 3.09 0.89 0.00 0.00	0.00 0.21 0.37 1.26 0.58 0.84 1.83 SSE 0.00 0.31 3.66 1.10 0.00 0.00	0.00 0.31 0.89 1.52 1.46 2.56 1.36 8 0.00 0.26 4.08 3.14 0.58 0.05	0.63 0.84 0.89 2.25 2.25 2.14 1.73 SSW 0.00 0.10 3.82 5.13 1.57 0.10	0.42 0.89 0.99 3.35 2.88 1.62 2.51 SW 0.00 0.26 5.49 4.81 2.04 0.05	0.94 0.63 1.10 2.35 1.26 0.89 1.94 WSW 0.00 0.37 4.18 3.77 0.78 0.00	0.73 0.84 2.04 6.52 0.52 1.20 W 6.00 0.73 2.93 2.35 0.42 0.00	0.10 0.31 0.73 1.67 0.73 0.42 1.05	0.00 0.05 0.05 0.58 0.52 0.31 0.26 MW 0.00 0.21 1.15 0.42 0.00 0.00	0.00 0.10 0.16 0.89 0.78 0.21 0.26 MNW 0.00 0.31 0.94 0.84 0.31	3.35 6.49 9.62 28.92 21.03 14.64 15.95 TOTAL 0.00 4.60 47.70 37.45	Ext Mod Sli Neu Sli Mod Ext	remely erately tral ghtly erately erately remely construction of the construction of t	Unstate y Unstate y Unstate y Unstate Unstate y Stable Stable Stable M 3.5 m 7.5 m 12.5 m 18.5 m 18.5 m	able cable cle cle cle cle cle cle cle cle cle c				

LaSalle Nuclear Station
375 ft. Wind Speed and Direction

### Number of Observations = 2208 Values are Percent Occurrence

SPEKI							- WIND	ntrr(	TION C	LASSES								•••		STAB1	LITY (	LASSES		••••	
CLASS		MNE	NE	ENE	E	ESE	SE	SSE	8	SSN	SW	NSN	¥	NNW		MAN	TOTAL	EU	MU	SU	H	SS	MS	ES	TOTAL
RU NU C SU A H I SS N MS	0.00 0.00 0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00 0.00	00.0 00.0 00.0 00.0 00.0	0.00 0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00 0.00 0.00	0.00 00.00 00.00 00.00 00.00	0.00 0.00 0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00 0.00	0.00 00.00 00.00 00.00 00.00	0.00 0.00 0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00 0.00 0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
NU 1 SU - N 3 SS NS ES	0.00 0.00 0.00 0.00 0.00 0.05	0.00 0.00 0.00 0.05 0.00 0.14 0.00	0.00 0.00 0.00 0.00 0.05 0.00	0.00 0.00 0.00 0.05 0.00 0.00	0.00 0.00 0.05 0.05 0.05 0.05	0.00 0.00 0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00 0.05 0.09	0.00 0.00 0.00 0.05 0.00 0.00	0.00 0.00 0.00 0.00 0.00 0.14 0.00	0.00 0.00 0.05 0.00 0.05	0.00 0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00 0.09 0.00	0.00 0.00 0.05 0.00 0.00	0.00 0.00 0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.27 0.18 0.50	0.00	0.60	0.00	0.27	0.18	0.50	0.00	0.95
EU NU 4 SU - H 7 SS NS ES	0.00 0.00 0.00 0.50 0.14 0.14		0.00 0.00 0.00 0.72 0.18 0.14	0.00 0.00 0.68 0.14 0.23	0.00 0.00 0.00 0.59 0.09 0.14 0.00	0.00 0.00 0.00 0.72 0.09 0.14 0.00	0.00 0.00 0.00 0.77 0.05 0.09 0.00	0.00 0.00 0.68 0.09 0.00	0.00 0.00 0.00 0.77 0.18 0.14		0.00 0.00 0.00 0.36 0.14 0.23	0.00 0.00 0.00 0.59 0.09 0.41	0.00 0.00 0.00 1.13 0.18 0.23 0.09	0.00 0.00 0.45 0.18 0.36 0.00	0.00 0.00 0.00 0.36 0.18 0.05	0.00 0.00 0.00 0.27 0.18 0.00	0.00 0.00 0.00 9.92 2.08 2.81	0.00	0.00	0.00	9.92	2.08	2.81	0.32	15.13
2 MS	0.18	0.00 0.00 0.00 1.49 0.18 0.14	0.00 0.00 0.05 0.91 0.14 0.05	0.32	0.00 0.00 0.05 1.36 0.72 0.27	0.00 0.00 0.00 0.82 0.45 0.32	0.00 0.00 0.63 0.23 0.09	0.00 0.00 0.00 0.63 0.23 0.27	0.00 0.00 0.00 0.72 0.41 0.32	0.00 0.18 0.68 0.32 0.14	0.00 0.00 0.09 1.31 0.18 0.45	6.00 6.00 6.05 1.77 0.50 0.41 6.05	0.00 0.00 0.14 1.04 0.27 0.32 0.09	0.00 0.00 0.00 1.22 0.00 0.54 0.00	0.00 0.00 0.00 0.82 0.23 0.23	0.00 0.00 0.00 0.45 0.09 0.05	0.00 0.60 0.68 16.49 5.12 4.08 0.68	0.00	0.00	0.68	16.49	5.12	4.08	0.68	27.04
1 MU 3 SU - H 1 \$S 8 MS	0.00 0.00 0.45 0.41 0.14	0.54	0.00 0.18 1.49 1.13 0.09	0.00 0.18 1.90 2.67 0.32	0.00 0.00 1.22 0.95 0.27	0.00 0.00 0.32 0.50 0.32	0.00 0.00 0.18 0.32 0.27	0.00 0.00 0.14 0.05 0.36	0.00 0.00 0.63 0.50 0.36	0.00 0.00 0.95 0.36 0.14	0.00 0.05 1.31 0.50 0.27	0.05 0.54 0.91 0.59 0.36	0.05 0.23 1.00 0.23 0.27	0.00 0.05 0.27 0.41 0.72	0.00 0.05 0.18 0.63 0.36	0.00 0.00 0.27 0.41 0.05	0.09 1.27 11.82 10.19 4.35	0.00	0.09	1.27	11.82	10.19	4.35	2.26	29.98

### July-September, 2002 375Ft-33Ft Delta-T (F)

3.6 - 7.5 mph

7.6 - 12.5 aph

12.6 - 18.5 mph

18.6 - 24.5 mph

> 24.5 mph

SPEKD							WIND	DIREC	rion C	LASSES					,					STAB	LITY (	iasses	}		
CLASS	H	MNE	<b>K</b> R	ENE	E	ESE	SE	<b>SSE</b>	S	SSW	SW	NSW	W	WINW	IW	MMW	TOTAL	EU	M	SU	N	SS	AS	ES	TOTAL
														A 46		A 00	A A6	A 60							
EU	0.00	0.00	0.00	0.00	0.00	0.00								0.00		0.00		0.00	e es						
1 W	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00			0.00	0.00		0.00	A 33					
9 SU	0.09	0.00	0.00	0.00	0.05	0.00	0.00	0.00		0.05			0.00			0.00	0.32			0.32					
- N	0.36	0.00	1.00	0.82	0.23	0.05	0.05	0.09	0.50	1.22	1.27	0.41	0.18	•••	0.05	0.09	6.61				6.61				
2 <b>S</b> S	0.18	0.14	0.45	0.41									0.14		0.14	0.18	5.30					5.30			
4 MS	0.00	0.00	0.00	0.00	0.45	0.59	0.32	0.09	0.32	0.63	0.91	0.32	0.27	0.23	0.00	0.18	4.30						4.30		
KS	0.14	0.00	0.00	0.00	0.00	0.18	0.14	0.41	0.27	0.45	0.32	0.05	0.09	0.00	0.00	0.05	<b>2.0</b> 8							2.08	
_	****		••••													٠.						. · · · ·			18.61
															•								•		
KI	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.60	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00							
G MU	0.00	0.00	0.00		0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00		0.00						
T SU	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00		0.05	0.00	0.00	0.00	0.00	0.00	0.09			0.09					
	0.05	0.00	0.00		0.05	0.00	0.00	0.00	0.23	0.36	0.36		0.00	0.00	0.00	0.14	1.36				1.36				
	0.05	0.00	0.00	• • • •		• • • •	0.00	0.00			1.18				0.00	0.00	2.94					2.94			
2 5S					•		0.23	0.23	0.41		0.82					0.00	3.31				• .		3.31		
2 NO	0.00	0.00					0.00		0.27			0.05		0.00		0.00	0.59							0.59	
ES	U.UU	0.00	0.00	0.00	0.00	V.V3	V.W	V.V3	V.21	0.03	V.V)	4.03	4.40	V.VU		****									8.29
										•								. •				•			• • • • • • • • • • • • • • • • • • • •
													•												
<b>TOT</b>	A 21	1 25	6 67	10 42	2 52	A 71	Z 03	4.57	7.20	9.87	11.41	8.42	6.07	4.89	3.44	2.40	100.00	0.00	0.09	2.36	46.47	25.82	19.34	5.93	100.00
101	7.41	1.50	4.57	10.45	7,30	3112	1.00	••••	.,																
Win	Direc	tion I	ny Sta	bility																					•
11211		,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	, 000	,																					
	I	INE	ME	ENE	E	ESE	SE	SSE	S	SSW	SW	WSW	¥	MAW	m	MAW	TOTAL	-8	PABILIT	Y CLA	SSES-	•			•
	-	_								•									_						
	6.00	0.00	0.00	0.00	0.00	0.60	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00		tremely						
	0.00		0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.05	0.05	0.00	0.00	0.00	0.09	Mo	deratel	y Uns	table				
	0.09				0.09	0.00	0.00	0.00	0.00	0.27	0.32	0.59	0.36	0.05	0.05	0.00	2.36	<b>\$1</b>	ightly	Unsta	ble				
	2.26					1.90	1.63	1.59	2.85	3.99	4.62	3.76	3.35	2.31	1.40	1.22	46.47	Ne	utral						
	1.18		1.95	-			0.72		1,72				0.91	0.68	1,18	0.86	25.82	<b>S</b> 1	ightly	Stabl	e				
		0.51				1.40					2.67			1.86	-		19.34		deratel					٠.	
	V.30	7.33 20.0	0.41	V.00	0 00	0 22	0 50	1.54	0.95	0.59	0.82	0.45	0.32				5.93						•		
	A.10	ÇV.V	v.V.	, v.vu	****	A . 23	4.37	-15	-1,73		- 1 - 4		-,						-2						
									•																
Vin	d Dire	ction :	by Wir	nd Spee	d																				
	K	MNE	N	ENE	E	ESE	SE	SSE	8	SSW	SW	WSW	¥	MENTA	WW	IEW	TOTAL	-N	ind spi	e ce	asses-				
	A AA	A 80	0.01	) () () ()	0.00	0.00	0 00	ስ <b>ሰ</b> ስ	0 00	0.00	0.00	0.60	0.00	0.00	0.00	0.00	0.00		CAI	. N					
	U.VU	V.VU	U.U.	, V.VL	. 0.00	0.UU A AA	0.00	7.00	0.00 ∩ 1#	U U0	6 40	0 00	0 00	0.05	0.00	0.00	0.95			3.5	moh				
	V.V5	A.12	V.U	y.V3	לט.ט	w.vv	A.73	V.V3	A.14	y.U3	4.40		0.00	4.45	4.00	4.40	15.13		3.6 -						

0.77 0.91 1.04 1.04 0.82 0.95 0.91 0.82 1.27 1.13 0.72 1.09 1.63 1.00 0.59 0.45 15.13

1.54 1.86 1.13 2.94 2.40 1.59 1.00 1.22 1.59 1.36 2.13 2.76 1.86 1.77 1.31 0.59 27.04

0.77 0.14 1.45 1.22 1.54 0.95 0.59 0.72 1.54 2.90 3.62 1.18 0.68 0.63 0.18 0.50 18.61

0.09 0.00 0.00 0.09 0.23 0.09 0.23 0.32 1.09 2.90 2.49 0.63 0.00 0.00 0.00 0.14 8.29

1.00 1.18 2.90 5,07 2.45 1.13 1.18 1.45 1.59 1.49 2.45 2.76 1.81 1.45 1,36 0.72 29.98

# LaSalle Nuclear Station 33 ft. Wind Speed and Direction

### Number of Observations = 2207 Values are Percent Occurrence

KKD KKD	ter .	2070	<b>#</b> 17	E1111	•	2011		DIREC	_			100		STATES.		mit.	TOTAL	KU		SU	10	SS	MC	20	TOTA
ASS		ENE	·IE	ENE	K	ESE	SE	SSE	S	SSW	SR	NSN	₩	MNW	WN	INW	IVIAL	EU	MU	ĐŲ	×	. 80	FLS	20	1011
EU	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00							
U	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00		0.00	0.00	0.00	0.00	0.00		0.00				-		
SU	0.00	0.00	0.00					0.00	0.00	0.00	0.00		0.00		0.00		0.00			0.00					
I	0.00	0.00	0.00							0.00	0.00	0.60	0.00	0.00	0.00	0.00	0.00				0.00	0.60			
		0.00			0.00			0.00		0.00		0.00	0.00	0.00	0.00	0.00	0.00					<b>U.</b> 00	0.00		
		0.00													0.00	0.00	0.00			·			0.00	0.00	
	4.40		0.00	V.VV	V.VV	V.VV	V.VV	V.VV	****	****	****	****	****	****	****	****	••••	•••						••••	0
DIT	6:80	0.00	A 00	A AA	A AA	A A0	A AA	0.00	A AA	6 60	A 00	0.00	a an	6.80	0.00	A AA	0.00	0.00	٠.			•			
		0.00			0.00					0.00	0.00	0.00		0.00		0.00	0.00		0.00						
_	0.00		0.00				0.00			0.00			0.00	0.00	0.00	0.00	0.00		••••	0.00				•	
		0.14										0.05	0.09	0.18	0.05	0.00	0.77		•		0.77				
SS	0.05	0.00	0.05	0.00	0.05	0.00	0.09	0.05	0.05	0.05	0.00	0.05	0.14	0.05	0.09	0.00	0.68					0.68		•	
		0.00					0.00				0.00		0.05	0.00	0.05	0.05	0.36						0.36		
S	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.09	0.00	0.05	0.00	0.05	0.00	0.18							0.18	٠.
					•						٠			<i>:</i>	•										1
Ü	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00							
MU	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.05	0.00	0.05		0.05						
SU	0.09	0.00	0.00	0.00	0.00		0.00		0.05		0.00		0.05		0.05		0.41			0.41					
	1.36	1.36			0.27			0.09						0.82			7.20		•		7.20	7.57			
		1.36		0.14		0.27	0.23 0.27			0.36					0.59 0.41		7.57 4.40					1.31	4.40		
		0.18													• • • •		5.30						3.30	5.30	
~	4.40	V.V	4.00	0.00	A 120	V.J0	V.111	•.,,	V113	7100	7.00	··	*	V.05	****	****			٠					••••	24
				A 40			A A0		A AA	A A0	A AA	A A0	A AA	A AA	A AA	7A A		A A0							
III	0.14	0.00	0.00	0.00	0.00	0.00	0.00	0.00		0.09	0.00		0.00		0.00	0.00	0.09	V.V3	0.50				٠.		
_	0.18	0.09	0.05	0.00	0.00	0.23	0.00	0.00	0.00	0.09	0.32		0.09			0.23	1.59		V.00	1.59					
	2.08	1.68	1.59		0.77	0.27	0.09	0.05	0.00			1.27	1.45		1.36	2.58	17.08				17.08				
S	0.68	0.14	0.23	0.23	0.86	0.18	0.23	0.14	0.68	0.95	0.95	0.45	0.86	1.18	0.77		9.24				:	9.24			
S	0.00	0.00	0.00	0.00	0.14	0.14	0.09	0.09	0.32	0.50	1.95	0.50	1.31	0.14	0.27	0.05	5.48					•	5.48		
<b>S</b>	0.00	0.00	0.00	0.00	0.09	0.32	0.05	0.00	0.18	1.63	1.63	1.72	0.68	0.18	0.14	0.00	6.62							6.62	46
													٠.												40
U	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.05	0.00	0.05	0.00	0.00	0.00	0.00	0.00	0.00	0.09	0.09							
U	0.06	0.00	0.00	0.00	0.00	0.00	0.00	0.09	0.00	0.05	0.00	0.09	0.05	0.14	0.00	0.05	0.45		0.45						
		0.00																-	•	1.59					
																	11.92				11.92	<i>(</i>			
5	U.00	0.00	0.09	0.09	0.68	0.14	0.18	0.09	1.00	0.82	1.13	V.68	1.31	0.55	V.14	0.00	6.93					6.93	2.13		
io PC	0.00	0.00	0.00	0.00	0.00	0.00	U.UU	CU,U	0.43 0.00	V.32	V VV V	V.21	0.30 AA A	0.00	0.00	0.UU	2.13 0.27						2.13	0.27	
N	v.VV	v.00	V.VV	V.VU	V.VV	V.UV	V.VV	V. VV	V.UV	A.11	V.VU	A . T.2	V.VV	V.VV	v.vv	4.00	V.6/							V.D.	23

LaSalle Euclear Station
33 ft. Wind Speed and Direction

<b>CONTR</b>							STEED	ntope	TION C	1 10000										STAR	II.TTY (	CLASSES			
SPEED	ĸ	NNE	NR	ENE	 1	ESŔ	- Wind Se	SSE	8 1104 F	rssea WZ <b>2</b>	SW	VSW	K	MA	W	MAN	TOTAL	KU	MU	SU		SS	· MS	ES	TOTAL
	-	-			-			-	•		_														
					4 80	A 44	A AA	A AA	A AA	A AA	A AA	0.00	0.00	0.00	0.00	0.00	0.00	0.00				-			
	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.05	0.00	0.00	0.00	0.00	0.14	4.00	0.14	•-		•			
1 MU 9 SU	0.00	0.00	0.00	0.00	0.05	0.00	0.00	0.00	0.00	0.18	0.14	0.14	0.00	0.00	0.00	0.00	0.50		****	0.50					
- N	0.00	0.00	0.05	0.41	0.41	0.36	0.00	0.05	0.09	0.27	0.18	0.18	0.86	0.23	0.27	0.45	3.90				3.90				
2 SS	0.00	0.00	0.00	0.00	0.00	0.18	0.09	0.05	0.32	0.59	0.72	0.14	0.54	0.50	0.00	0.00	3.13					3.13			
4 NS	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.09	0.05	0.09	0.00	0.00	0.00	0.00	0.00	0.23						0.23		
ES	0.00	.0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00							0.00	
															•										7. <b>8</b> 8
											'n 66	A AA	A AA		0.00	8.80	. 4.40	A A0	•						
	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00						
G MU	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00		V.4V	0.00					
T SU N	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.05	0.00	0.00	0.18	0.00	0.09	0.00	0.09	0.14	0.63				0.63				
2 SS	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.09	0.09	0.00	0.00	0.00	0.18	0.23	0.00	0.00	0.59					0.59			
4 MS	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00						0.00		
KS	0.00	0.00		0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00							0.00	
														•											1.22
														•			·		*						
			• • •								12 (1	7 04	11 (1	0 (1	C 16	0 02	100 00	A 10	1 12	# AG	<b>41 50</b>	20 14	13 60	12 27	100.00
TUT	7.07	4.94	3.44	2.90	5.66	3.40	1.86	2.49	4.20	\$.11	12.60	1.04	11.04	7.61	6.10	5.02	100.00	A.10	1.13	1.00	41.30	40.11	14.00	14,31	100.00
			. •																				-		
Wind	Direc	ction 1	y Stal	ility																					
	-		_		_	202	ATI	AAR		Office	m			ents	367.2	Maria	enverat.		P3 DTT.79	ev eta	eere.				
	K	INE	MB	ENE	I	ESE	<b>S</b> e	<b>S</b> SE	8	SSW	SW	nsn	¥	MNW	M		TOTAL	-S	[ABILIT	TY CLA	SSES-				
			ME 0.00		0.00 E	ESE 0.00	<b>S</b> E 0.00	\$SE 0.05	S 0.00	SSW 0.14		NSW 0.00	W 0.00	WWW 0.00	W 0.00	MANN 0.00	TOTAL 0.18		PABILIT Eremely		٠.				
	0.00 0.14	0.00	ME 0.00		0.00 0.00	ESE 0.00 0.00			0.00 0.05				0.00 0.05					Ext		<b>U</b> nst	able				
	0.00	0.00 0.00	0.00	ENB 0.00	0.00 0.00 0.05	0.00	0.00	0.05		0.14	0.00	0.00 0.14 0.41	0.05 0.45		0.00 0.05 0.41	0.00	0.18 1.13 4.08	Ext Mod Sli	remely leratel	Unst Ly Uns	able table				
	0.00 0.14	0.00 0.00 0.09	0.00 0.00 0.05	ENB 0.00 0.00	0.00 0.00 0.05 2.81	0.00	0.00	0.05 0.18	0.05 0.05 0.50	0.14 0.14 0.27 1.27	0.00 0.23 0.63 2.81	0.00 0.14 0.41 2.49	0.05 0.45 4.12	0.00 0.14 0.23 4.62	0.00 0.05 0.41 3.17	0.00 0.05 0.54 5.80	0.18 1.13 4.08 41.50	Ext Mod S1: Her	tremely derated ightly utral	Unst y Uns Unsta	able table ble				
	0.00 0.14 0.41 3.94 2.40	0.00 0.00 0.09 3.17 1.50	0.00 0.00 0.05 2.76 0.63	ENE 0.00 0.00 0.05 2.36 0.45	2.81 1.90	0.00 0.00 0.27 1.04 0.77	0.00 0.00 0.00 0.23 0.82	0.05 0.18 0.18 0.41 0.54	0.05 0.05 0.50 2.27	0.14 0.14 0.27 1.27 2.76	0.00 0.23 0.63 2.81 2.99	0.00 0.14 0.41 2.49 1.63	0.05 0.45 4.12 3.53	0.00 0.14 0.23 4.62 3.04	0.00 0.05 0.41 3.17 1.59	0.00 0.05 0.54 5.80 1.31	0.18 1.13 4.08 41.50 28.14	Ext Mod Sli Her Sl:	tremely derated ightly utral ightly	Unst y Uns Unsta Stabl	able table ble				
	0.00 0.14 0.41 3.94 2.40 0.18	0.00 0.00 0.09 3.17 1.50 0.18	0.00 0.00 0.05 2.76 0.63	ENE 0.00 0.00 0.05 2.36 0.45 0.05	2.81 1.90 0.32	0.00 0.00 0.27 1.04 0.77 0.63	0.00 0.00 0.00 0.23 0.82 0.36	0.05 0.18 0.18 0.41 0.54 0.36	0.05 0.05 0.50 2.27 0.77	0.14 0.14 0.27 1.27 2.76 1.13	0.00 0.23 0.63 2.81 2.99 3.35	0.00 0.14 0.41 2.49 1.63 1.18	0.05 0.45 4.12 3.53 2.22	0.00 0.14 0.23 4.62 3.04 0.82	0.00 0.05 0.41 3.17 1.59 0.72	0.00 0.05 0.54 5.80 1.31 0.32	0.18 1.13 4.08 41.50 28.14 12.60	Ext Nox Sl: Her Sl: Nox	tremely derated ightly utral ightly derated	Unst y Uns Unsta Stahl y Sta	able table ble e ble				
	0.00 0.14 0.41 3.94 2.40 0.18	0.00 0.00 0.09 3.17 1.50 0.18	0.00 0.00 0.05 2.76 0.63	ENE 0.00 0.00 0.05 2.36 0.45 0.05	2.81 1.90 0.32	0.00 0.00 0.27 1.04 0.77 0.63	0.00 0.00 0.00 0.23 0.82 0.36	0.05 0.18 0.18 0.41 0.54 0.36	0.05 0.05 0.50 2.27 0.77	0.14 0.14 0.27 1.27 2.76 1.13	0.00 0.23 0.63 2.81 2.99	0.00 0.14 0.41 2.49 1.63 1.18	0.05 0.45 4.12 3.53 2.22	0.00 0.14 0.23 4.62 3.04 0.82	0.00 0.05 0.41 3.17 1.59 0.72	0.00 0.05 0.54 5.80 1.31 0.32	0.18 1.13 4.08 41.50 28.14	Ext Nox Sl: Her Sl: Nox	tremely derated ightly utral ightly	Unst y Uns Unsta Stahl y Sta	able table ble e ble				
	0.00 0.14 0.41 3.94 2.40 0.18	0.00 0.00 0.09 3.17 1.50 0.18	0.00 0.00 0.05 2.76 0.63	ENE 0.00 0.00 0.05 2.36 0.45 0.05	2.81 1.90 0.32	0.00 0.00 0.27 1.04 0.77 0.63	0.00 0.00 0.00 0.23 0.82 0.36	0.05 0.18 0.18 0.41 0.54 0.36	0.05 0.05 0.50 2.27 0.77	0.14 0.14 0.27 1.27 2.76 1.13	0.00 0.23 0.63 2.81 2.99 3.35	0.00 0.14 0.41 2.49 1.63 1.18	0.05 0.45 4.12 3.53 2.22	0.00 0.14 0.23 4.62 3.04 0.82	0.00 0.05 0.41 3.17 1.59 0.72	0.00 0.05 0.54 5.80 1.31 0.32	0.18 1.13 4.08 41.50 28.14 12.60	Ext Nox Sl: Her Sl: Nox	tremely derated ightly utral ightly derated	Unst y Uns Unsta Stahl y Sta	able table ble e ble				
Wind	0.00 0.14 0.41 3.94 2.40 0.18 0.00	0.00 0.00 0.09 3.17 1.50 0.18	0.00 0.00 0.05 2.76 0.63 0.00	ENE 0.00 0.00 0.05 2.36 0.45 0.05	2.81 1.90 0.32 0.59	0.00 0.00 0.27 1.04 0.77 0.63	0.00 0.00 0.00 0.23 0.82 0.36	0.05 0.18 0.18 0.41 0.54 0.36	0.05 0.05 0.50 2.27 0.77	0.14 0.14 0.27 1.27 2.76 1.13	0.00 0.23 0.63 2.81 2.99 3.35	0.00 0.14 0.41 2.49 1.63 1.18	0.05 0.45 4.12 3.53 2.22	0.00 0.14 0.23 4.62 3.04 0.82	0.00 0.05 0.41 3.17 1.59 0.72	0.00 0.05 0.54 5.80 1.31 0.32	0.18 1.13 4.08 41.50 28.14 12.60	Ext Nox Sl: Her Sl: Nox	tremely derated ightly utral ightly derated	Unst y Uns Unsta Stahl y Sta	able table ble e ble				
Wind	0.00 0.14 0.41 3.94 2.40 0.18 0.00	0.00 0.00 0.09 3.17 1.50 0.18 0.00	0.00 0.05 2.76 0.63 0.00 0.00	ENE 0.00 0.05 2.36 0.45 0.05 0.00	2.81 1.90 0.32 0.59	0.00 0.00 0.27 1.04 0.77 0.63 0.68	0.00 0.00 0.00 0.23 0.82 0.36 0.45	0.05 0.18 0.18 0.41 0.54 0.36	0.05 0.05 0.50 2.27 0.77 0.63	0.14 0.14 0.27 1.27 2.76 1.13 2.40	0.00 0.23 0.63 2.81 2.99 3.35 2.58	0.00 0.14 0.41 2.49 1.63 1.18 1.99	0.05 0.45 4.12 3.53 2.22 1.27	0.00 0.14 0.23 4.62 3.04 0.82 0.77	0.00 0.05 0.41 3.17 1.59 0.72 0.23	0.00 0.05 0.54 5.80 1.31 0.32	0.18 1.13 4.08 41.50 28.14 12.60 12.37	Ext Moo S1: Mer S1: Moo Ext	remely leratel ightly utral ightly leratel iremely	Unst y Uns Unsta Stabl y Stab	able table ble e ble				
Wind	0.00 0.14 0.41 3.94 2.40 0.18 0.00	0.00 0.00 0.09 3.17 1.50 0.18 0.00	0.00 0.05 2.76 0.63 0.00 0.00	ENE 0.00 0.05 2.36 0.45 0.05 0.00	2.81 1.90 0.32 0.59	0.00 0.00 0.27 1.04 0.77 0.63	0.00 0.00 0.00 0.23 0.82 0.36 0.45	0.05 0.18 0.18 0.41 0.54 0.36	0.05 0.05 0.50 2.27 0.77 0.63	0.14 0.14 0.27 1.27 2.76 1.13	0.00 0.23 0.63 2.81 2.99 3.35 2.58	0.00 0.14 0.41 2.49 1.63 1.18 1.99	0.05 0.45 4.12 3.53 2.22	0.00 0.14 0.23 4.62 3.04 0.82	0.00 0.05 0.41 3.17 1.59 0.72 0.23	0.00 0.05 0.54 5.80 1.31 0.32	0.18 1.13 4.08 41.50 28.14 12.60	Ext Moo S1: Mer S1: Moo Ext	remely leratel ightly utral ightly leratel iremely	Unst y Uns Unsta Stabl y Stab	able table ble e ble				
Wind	0.00 0.14 0.41 3.94 2.40 0.18 0.00	0.00 0.00 0.09 3.17 1.50 0.18 0.00	0.00 0.05 2.76 0.63 0.00 0.00	ENE 0.00 0.05 2.36 0.45 0.05 0.00	2.81 1.90 0.32 0.59	0.00 0.00 0.27 1.04 0.77 0.63 0.68	0.00 0.00 0.00 0.23 0.82 0.36 0.45	0.05 0.18 0.18 0.41 0.54 0.36 0.77	0.05 0.05 0.50 2.27 0.77 0.63	0.14 0.14 0.27 1.27 2.76 1.13 2.40	0.00 0.23 0.63 2.81 2.99 3.35 2.58	0.00 0.14 0.41 2.49 1.63 1.18 1.99	0.05 0.45 4.12 3.53 2.22 1.27	0.00 0.14 0.23 4.62 3.04 0.82 0.77	0.00 0.05 0.41 3.17 1.59 0.72 0.23	0.00 0.05 0.54 5.80 1.31 0.32 0.00	0.18 1.13 4.08 41.50 28.14 12.60 12.37	Ext Moo S1: Mer S1: Moo Ext	tremely leratel ightly itral ightly leratel tremely	Unst Ly Unsta Stabl Ly Stab ( Stab	able table ble e ble				
Wind	0.00 0.14 0.41 3.94 2.40 0.18 0.00	0.00 0.09 0.09 3.17 1.50 0.18 0.00	0.00 0.05 2.76 0.63 0.00 0.00	ENE 0.00 0.05 2.36 0.45 0.05 0.00	2.81 1.90 0.32 0.59	0.00 0.00 0.27 1.04 0.77 0.63 0.68	0.00 0.00 0.00 0.23 0.82 0.36 0.45	0.05 0.18 0.18 0.41 0.54 0.36 0.77	0.05 0.05 0.50 2.27 0.77 0.63	0.14 0.14 0.27 1.27 2.76 1.13 2.40	0.00 0.23 0.63 2.81 2.99 3.35 2.58	0.00 0.14 0.41 2.49 1.63 1.18 1.99	0.05 0.45 4.12 3.53 2.22 1.27	0.00 0.14 0.23 4.62 3.04 0.82 0.77	0.00 0.05 0.41 3.17 1.59 0.72 0.23	0.00 0.05 0.54 5.80 1.31 0.32 0.00	0.18 1.13 4.08 41.50 28.14 12.60 12.37	Ext Moo S1: Mer S1: Moo Ext	tremely leratel ightly itral ightly itral ightly itrael ightly ieratel iremely	y Unsta y Unsta Unsta Stabl y Stab y Stab	able table ble e ble le				
Wind	0.00 0.14 0.41 3.94 2.40 0.18 0.00	0.00 0.09 3.17 1.50 0.18 0.00	0.00 0.05 2.76 0.63 0.00 0.00	0.00 0.05 2.36 0.45 0.05 0.05 0.00	2.81 1.90 0.32 0.59	0.00 0.00 0.27 1.04 0.77 0.63 0.68	0.00 0.00 0.00 0.23 0.82 0.36 0.45	0.05 0.18 0.18 0.41 0.54 0.36 0.77	0.05 0.05 0.50 2.27 0.77 0.63	0.14 0.14 0.27 1.27 2.76 1.13 2.40 SSW 0.00 0.14	0.00 0.23 0.63 2.81 2.99 3.35 2.58	0.00 0.14 0.41 2.49 1.63 1.18 1.99	0.05 0.45 4.12 3.53 2.22 1.27	0.00 0.14 0.23 4.62 3.04 0.82 0.77	0.00 0.05 0.41 3.17 1.59 0.72 0.23	0.00 0.05 0.54 5.80 1.31 0.32 0.00	0.18 1.13 4.08 41.50 28.14 12.60 12.37	Ext Mox S1: Her S1: Mox Ext	tremely leratel ightly itral ightly itral ightly itrael ightly ieratel iremely	y Unsta y Unsta Stabl ly Stab y Stab	able table ble e ble le ASSES-				
Wind	0.00 0.14 0.41 3.94 2.40 0.18 0.00 1 Direc W 0.00 0.18 3.22 3.08	0.00 0.09 3.17 1.50 0.18 0.00 ction l	0.00 0.05 2.76 0.63 0.00 0.00 WE 0.00 0.05 0.59	ENE 0.00 0.05 2.36 0.45 0.05 0.00 1 Speed ENE 0.00 0.05 0.54	2.81 1.90 0.32 0.59	0.00 0.00 0.27 1.04 0.77 0.63 0.68 ESR 0.00 0.09 1.31 1.13	0.00 0.00 0.00 0.23 0.82 0.36 0.45	0.05 0.18 0.18 0.41 0.54 0.36 0.77 SSE 0.00 0.05 1.31 0.36	0.05 0.05 0.50 2.27 0.77 0.63 8 0.00 0.05 0.82 1.22	0.14 0.14 0.27 1.27 2.76 1.13 2.40 SSW 0.00 0.14 1.45 3.76	0.00 0.23 0.63 2.81 2.99 3.35 2.58 SW 0.00 0.14 1.81 6.34	0.00 0.14 0.41 2.49 1.63 1.18 1.99 WSW 0.00 0.18 1.13 4.03	0.05 0.45 4.12 3.53 2.22 1.27 W 0.00 0.32 1.81 4.40	0.00 0.14 0.23 4.62 3.04 0.82 0.77 WNW 0.00 0.23 2.63 3.04	0.00 0.05 0.41 3.17 1.59 0.72 0.23	0.00 0.05 0.54 5.80 1.31 0.32 0.00	0.18 1.13 4.08 41.50 28.14 12.60 12.37 TOTAL 0.00 1.99 24.92 40.60	Ext Nox Sli Hee Sl: Mox Ext	iremely leratel lightly litral lightly leratel liremely  C A 1  < 3.6 - 7.6 -	y Unsta y Unsta Stabl y Stab y Stab M 3.5 7.5:	able table ble e ble ASSES- mph mph mph				
Wind	0.00 0.14 0.41 3.94 2.40 0.18 0.00 Direc W 0.00 0.18 3.22 3.08	0.00 0.00 0.09 3.17 1.50 0.18 0.00 ction l	0.00 0.05 2.76 0.63 0.00 0.00 by Wind	ENE 0.00 0.05 2.36 0.45 0.05 0.00 1 Speed ENE 0.00 0.05 0.54 0.91 1.00	2.81 1.90 0.32 0.59 1 1 8 0.00 0.05 1.27 1.86 2.04	0.00 0.00 0.27 1.04 0.77 0.63 0.68 ESE 0.00 0.09 1.31 1.13 0.32	0.00 0.00 0.00 0.23 0.82 0.36 0.45	0.05 0.18 0.18 0.41 0.54 0.36 0.77 SSE 0.00 0.05 1.31 0.36 0.54	0.05 0.05 0.50 2.27 0.77 0.63 8 0.00 0.05 0.82 1.22 1.50	0.14 0.14 0.27 1.27 2.76 1.13 2.40 SSW 0.00 0.14 1.45 3.76 1.68	0.00 0.23 0.63 2.81 2.99 3.35 2.58 SW 0.00 0.14 1.81 6.34 2.90	0.00 0.14 0.41 2.49 1.63 1.18 1.99 WSW 0.00 0.18 1.13 4.03 1.99	0.05 0.45 4.12 3.53 2.22 1.27 W 0.00 0.32 1.81 4.40 3.44	0.00 0.14 0.23 4.62 3.04 0.82 0.77 WNW 0.00 0.23 2.63 3.04 2.76	0.00 0.05 0.41 3.17 1.59 0.72 0.23 MW 0.00 0.23 1.50 2.67 1.40	0.00 0.05 0.54 5.80 1.31 0.32 0.00 NNW	0.18 1.13 4.08 41.50 28.14 12.60 12.37 TOTAL 0.00 1.99 24.92 40.60 23.38	Ext Nox Sl: Her Sl: Nox Ext	iremely leratel lightly litral lightly leratel remely  C A 1  < 3.6 - 7.6 - 12.6 -	y Unsta y Unsta Stabl y Stab y Stab 3.5 7.5 12.5 18.5	able table ble e ble le ASSES- mph mph mph mph				
Wind	0.00 0.14 0.41 3.94 2.40 0.18 0.00 0.18 3.22 3.08 0.50 0.09	0.00 0.09 3.17 1.50 0.18 0.00 ction 1 MNE 0.00 0.14 2.90 1.90 0.00	0.00 0.05 2.76 0.63 0.00 0.00 Wind WE 0.00 0.05 0.59 1.86 0.91	ENE 0.00 0.05 2.36 0.45 0.05 0.00 1 Speed ENE 0.00 0.05 0.54 0.91 1.00	2.81 1.90 0.32 0.59 1 0.00 0.05 1.27 1.86 2.04 0.45	0.00 0.00 0.27 1.04 0.77 0.63 0.68 ESE 0.00 0.09 1.31 1.13 0.32	0.00 0.00 0.00 0.23 0.82 0.36 0.45	0.05 0.18 0.18 0.41 0.54 0.36 0.77 SSE 0.00 0.05 1.31 0.36 0.54 0.09	0.05 0.05 0.50 2.27 0.77 0.63 8 0.00 0.05 0.82 1.22 1.50 0.50	0.14 0.14 0.27 1.27 2.76 1.13 2.40 SSW 0.00 0.14 1.45 3.76 1.68 1.09	0.00 0.23 0.63 2.81 2.99 3.35 2.58 8W 0.00 0.14 1.81 6.34 2.90 1.22	0.00 0.14 0.41 2.49 1.63 1.18 1.99 0.00 0.18 1.13 4.03 1.99 0.50	0.05 0.45 4.12 3.53 2.22 1.27 W 0.00 0.32 1.81 4.40 3.44 1.40	0.00 0.14 0.23 4.62 3.04 0.82 0.77 WINH 0.00 0.23 2.63 3.04 2.76 0.72	0.00 0.05 0.41 3.17 1.59 0.72 0.23 MW 0.00 0.23 1.50 2.67 1.40 0.27	0.00 0.05 0.54 5.60 1.31 0.32 0.00 NNW 0.05 1.63 3.58 2.17 0.45	0.18 1.13 4.08 41.50 28.14 12.60 12.37 TOTAL 0.00 1.99 24.92 40.60 23.38 7.88	Ext Mood Sl: Hen Sl: Mood Ext	tremely leratel ightly itral ightly itral ightly itral ightly ieratel iremely  C A 1  < 3.6 - 7.6 - 12.6 - 18.6 -	y Unsta y Unsta Unsta Stabl y Stab y Stab 3.5 7.5 12.5 18.5 24.5	able table ble e ble ASSES-				
Wind	0.00 0.14 0.41 3.94 2.40 0.18 0.00 0.18 3.22 3.08 0.50 0.09	0.00 0.09 3.17 1.50 0.18 0.00 ction 1 MNE 0.00 0.14 2.90 1.90 0.00	0.00 0.05 2.76 0.63 0.00 0.00 Wind WE 0.00 0.05 0.59 1.86 0.91	ENE 0.00 0.05 2.36 0.45 0.05 0.00 1 Speed ENE 0.00 0.05 0.54 0.91 1.00	2.81 1.90 0.32 0.59 1 0.00 0.05 1.27 1.86 2.04 0.45	0.00 0.00 0.27 1.04 0.77 0.63 0.68 ESE 0.00 0.09 1.31 1.13 0.32	0.00 0.00 0.00 0.23 0.82 0.36 0.45	0.05 0.18 0.18 0.41 0.54 0.36 0.77 SSE 0.00 0.05 1.31 0.36 0.54 0.09	0.05 0.05 0.50 2.27 0.77 0.63 8 0.00 0.05 0.82 1.22 1.50 0.50	0.14 0.14 0.27 1.27 2.76 1.13 2.40 SSW 0.00 0.14 1.45 3.76 1.68 1.09	0.00 0.23 0.63 2.81 2.99 3.35 2.58 8W 0.00 0.14 1.81 6.34 2.90 1.22	0.00 0.14 0.41 2.49 1.63 1.18 1.99 0.00 0.18 1.13 4.03 1.99 0.50	0.05 0.45 4.12 3.53 2.22 1.27 W 0.00 0.32 1.81 4.40 3.44 1.40	0.00 0.14 0.23 4.62 3.04 0.82 0.77 WINH 0.00 0.23 2.63 3.04 2.76 0.72	0.00 0.05 0.41 3.17 1.59 0.72 0.23 MW 0.00 0.23 1.50 2.67 1.40 0.27	0.00 0.05 0.54 5.60 1.31 0.32 0.00 NNW 0.05 1.63 3.58 2.17 0.45	0.18 1.13 4.08 41.50 28.14 12.60 12.37 TOTAL 0.00 1.99 24.92 40.60 23.38	Ext Mood Sl: Hen Sl: Mood Ext	tremely leratel ightly itral ightly itral ightly itral ightly ieratel iremely  C A 1  < 3.6 - 7.6 - 12.6 - 18.6 -	y Unsta y Unsta Stabl y Stab y Stab 3.5 7.5 12.5 18.5	able table ble e ble ASSES-				

LaSalle Muclear Station 375 ft. Wind Speed and Direction

### Number of Observations = 2206 Values are Percent Occurrence

<b>OPCULE</b>							WTW.	DIREC	TOUT (	.10070								•••	400000	STARI	LITY (	IASSES			
SPEKE		MINE	KE	ENE	E	ESE	SE SE	SSE	8	SSW W28	SN	WSW	¥	NNW	NN	MAN	TOTAL	EU	M	SU	K	SS	MS	ES	TOTAL
							4					•							•						
EU	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00						0.00							
MU	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00		0.00	0.00	•	•			
C SU	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00 0.00			0.00	0.00				
7.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00				0.00	0.00			
N NG T 90	0.00	0.00	0.00	0.00	0.00		0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00						0.00		
RS	0.00	0.00		0.00					0.00		0.00	0.00		0.00	0.00	0.00	0.00						•	0.00	
,,,,,	****	****	****		••••	****	• • • • • • • • • • • • • • • • • • • •		•••																0.00
																					•		•		
EU	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00		0.00	0.00	0.00	0.00	0.00			0.00		:			٠		
	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00		0.00	0.00	•				
1 50	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.05	0.00 0.36			0.00	0.36				
- N	0.05	0.00	0.00	0.00	0.05	0.05	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00		0.27		•		4.30	0.27			
3 8S	0.09	0.09	0.00	6.05 0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00		0.00			0.00					••••	0.00		
		****			0.00				0.00			0.00		0.00	0.00		0.00							0.00	
20	4.44	0.00	4.40	4.44	•.••	****	****	••••	****	••••															0.63
EU	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	•	0.00		0.00			0.00							
M	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00		0.00		0.00	A AA					
4 SU	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00		0.00			0.00	3.22				
- I	0.59	0.27	0.14	0.14	0.14	0.09	0.00	0.14	0.00	0.09	0.14	0.18 0.05		0.23	0.41		3.22 1.22				3.44	1.22			•
7 <b>S</b> S	0.14	0.00	0.14		0.09	0.05	0.23	0.05	0.00		0.23	0.05		0.05	0.00		0.41					-100	0.41		
	0.05	0.00	0.00	0.00		0.14		****		0.05	0.09			0.00			0.23						•••	0.23	
<b>50</b>	<b>0.0</b> 0	0.00	V.VU	0.00	V.VV	V.VV	0.00	0.00	V.00			****	••••	****	••••	••••	**								5.08
																						.**			
EU	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00							
MU	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00		0.00	0.00		0.00	0.00		0.00		0.00						
8 SU	0.00		0.00	0.00	0.00	0.00	0.00	0.00	0.00		0.00			0.00	0.00	0.00	0.00			0.00	10 24				
- I	1.90				0.50	0.41	0.14	0.14	0.00		0.77				1.00 0.18	1.09 0.32	10.34 4.22				10.34	4.22			
1 55	0.27	0.63	0,45	0.23	0.41	0.23	CU.U	V.14	CU.U	0.14	0.03	0.27	0.30 0.32	0.27		0.32						1100	1.90		
4 FQ	0.00	CV.V	0.00	0.00	0.00	0.14	0.05	0.10	0.03	0.69	0.32	0.14	0.00	0.05	0.00		0.82							0.82	
20	V.VD	V.VV	0.00	V.V0	V.V	V.VV	0.03	0.00	4.23	V143	7.0-	****	****	-,,-	*****										17.27
EU	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00							
1 MU	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00		0.00						
3 SU	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.05	0.00	0.05	0.00	0.00	0.00	0.00	0.00	0.00	0.09			0.09	16 14				
• I	1.72	1.41	1.99	1.09	0.77	0.14	0.09	0.27	0.14	0.54	1.50	1.16	1.59	1.22	1.45	1.31	16.41				16.41	6.62			
1 55	1.04	0.82	0.63	0.05	0.27	0.23	0.00	0.09	V.05	U.35	U.36	V.21	0.34 0.36	V.00	V.34	U.03	6.62 3.90					U.U.	3.90		
ZM 8	0.18	U,05	U.00	U.00	0.00 0.00	0.18 A AF	0,14 0.00	0 00	0 00 0.10	U.30	0.50 0.00	0.23 A AQ	V.JO 0 18	0.77	0.71	0.27	1.13						J.JU	1.13	
5.0	v.vv	V.00	v.UU	V.UV	v.00	v.VJ	U.V.	V.VJ	V. VV	V.10	¥.VJ	4.43	7.10	- (4)	7.40	****									28.15

### October-December, 2002 375Ft-33Ft Delta-T (F)

12.6 - 18.5 mh 18.6 - 24.5 mph > 24.5 mph

																				-		AT 1 0 0 0 0			
SPEED	*							DIRECT	CION CI	ASSES						••••	MARTIN T		LETT		ILITY	CLASSES SS		D0	TOTAL
CLASS	n	MNE	NE	ENE	K	ese	SE	SSE	8	SSW	SW	WSW	W	WAW	MA	MINW	TOTAL	EU	MU	SU		99	MS	ES	IOIAL
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4 30	0.45	0.05	0.18	0.05	0.32					0.45		0.36	0.59			0.05	3.67					*****	3.67		
4 MS	0.00	0.00	0.00	0.00						0.32	0.41		0.14			0.00	1.77							1.77	
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4 115	0.00	0.00	0.00	0.00	0.00	0.18	0.14	0.18	0.18	0.09	0.32	0.95	0.05	0.09	0.00	0.00	1.90						• • • • • • • • • • • • • • • • • • • •	1.90	
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# EFFLUENT AND WASTE DISPOSAL ANNUAL REPORT (2002)

# APPENDIX A OFFSITE DOSE CALCULATION MANUAL

# APPENDIX L OFFSITE DOSE CALCULATION MANUAL (ODCM) LASALLE ANNEX

**Revision 5** 

## RADIOACTIVE EFFLUENT TREATMENT AND MONITORING

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## RADIOACTIVE EFFLUENT TREATMENT AND MONITORING

### 10.1 AJRBORNE RELEASES

### 10.1.1 System Description

A simplified gaseous radwaste and gaseous effluent flow diagram are provided in Figure 10-1.

The airborne release point for radioactive effluents is the ventilation stack which is classified as a stack in accordance with the definitions in Section 4.1.4 and the results in Table A-1 of Appendix  $\Delta$ 

In addition, the standby gas treatment system effluent is released through a separate stack inside the ventilation stack. This release point has the same location and classification as the ventilation stack.

Exfiltration to the environment from the Turbine Building has been identified at times of positive pressure in the Turbine Building. Within 20 hours of the turbine building being at positive pressure continuous air sampling shall be in place in the south Turbine Building trackway to monitor releases through this pathway. The releases through the trackway door and other potential release paths contain insignificant levels of contamination when compared to the Station Vent Stack which has a 1,000,000 cfm typical stack flow compared to the Trackway flow rate of 40,000 scfm and conservatively estimated as a total of 80,000 scfm to account for pathways other than the trackway. In addition, typical releases from LaSalle Station have not exceeded 0.02% of the 10CFR50 Appendix I dose limits. Any identified release via this pathway is a ground level release and should be considered in dose calculations. See Figure 10-1 for further information.

Waste oil burning to fuel a heat recovery system is planned to begin in the Fall of 1998. Sampling and analyses of each batch of oil is required to be performed in accordance with ODCM Table 12.4.1-1. The effluent will be verified to be within the instantaneous release limits prior to each batch (assuming 100% of the activity in the waste oil is released in the gaseous effluent). The oil burning unit is located in an onsite building within the protected area. The effluent is released out the top of the building, is a ground level release, and will be quantified and considered in dose calculations.

Airborne releases to the environment may result if a fire occurs in a contaminated material warehouse. In the event of a fire in a contaminated material warehouse this pathway would be considered a ground level release and should be quantified and considered in dose calculations.

### 10.1.1.1 Condenser Offgas Treatment System

The condenser offgas treatment system is designed and installed to reduce radioactive gaseous effluents by collecting non-condensable off-gases from the condenser and providing for holdup to reduce the total radioactivity by radiodecay prior to release to the environment. The daughter products are retained by charcoal and HEPA filters. The system is described in Section 11.3.2.1 of the LaSalle UFSAR.

### 10.1.1.2 Ventilation Exhaust Treatment System

Ventilation exhaust treatment systems are designed and installed to reduce gaseous radioiodine or radioactive material in particulate form in selected effluent streams by passing ventilation or vent exhaust gases through charcoal adsorbers and/or HEPA filters prior to release to the environment. Such a system is not considered to have any effect on noble gas effluents. The ventilation exhaust treatment systems are shown in Figure 10-1.

Engineered safety features atmospheric cleanup systems are not considered to be ventilation exhaust treatment system components.

#### 10.1.2 Radiation Monitors

### 10.1.2.1 Station Vent Stack Effluent Monitor

Monitor OPLD5J (Wide Range Noble Gas Monitor) continuously monitors the final effluent from the station vent stack.

The monitor system has isokinetic sampling, gaseous grab sampling, iodine and particulate sampling, tritium sampling, and postaccident sampling capability.

In normal operation the low-range noble gas channel is on line and active. The mid-range channel replaces the low-range channel at a concentration of 0.01  $\mu$ Ci/cc png\* and the high-range channel replaces the mid-range channel at a concentration of 10  $\mu$ Ci/cc png.

The low-range and mid/high-range lodine and particulate samplers operate in a similar manner. In normal operation the low-range samplers are on line. At a concentration of 0.001  $\mu$ Cl/cc png the mid/high-range samplers are brought on line, and at a concentration of 0.1  $\mu$ Cl/cc png the low-range sample pump is turned off.

No automatic isolation or control functions are performed by this monitor. Pertinent information on this monitor is provided in the LaSalle UFSAR Section 11.5.2.2.1.

#### 10.1.2.2 Standby Gas Treatment System Effluent Monitor

Monitor OPLD2J (Wide Range Noble Gas Monitor) continuously monitors the final effluent from the standby gas treatment system (SGTS) stack.

The SGTS stack monitor has isokinetic sampling, gaseous grab sampling, particulate and lodine sampling, and post accident sampling capability.

In normal operation the low range noble gas channel is on line and active. The mid-range channel replaces the low-range channel at a concentration of 0.01  $\mu$ Cl/cc png and the high-range channel replaces the mid-range channel at a concentration of 10  $\mu$ Cl/cc png.

<sup>\*</sup> To facilitate use of the wide range gas monitors on the Station Vent Stack and Standby Gas Treatment System Stack in post-accident dose assessment, the output of each is expressed in units of pseudo noble gas (png) activity. Pseudo noble gas is a fictitious radionuclide defined to have emission characteristics representative of a post-accident noble gas mix. Upon decay, a pseudo noble gas nuclide emits one gamma ray with energy 0.8 MeV and one beta particle with endpoint energy 1.68 MeV and average energy 0.56 MeV.

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The low-range and mid/high-range iodine and particulate samples operate in a similar manner. In normal operation, the low-range samples are on-line. At a concentration of 0.001  $\mu$ Ci/cc png the mid/high-range samplers are brought on-line, and at a concentration of 0.1  $\mu$ Ci/cc png the low-range sample pump is turned off.

No automatic isolation or control functions are performed by this monitor.

Pertinent Information on this monitor is provided in the LaSalle UFSAR Section 11.5.2.2.2.

### 10.1.2.3 Reactor Building Ventilation Monitors

Monitors 1(2)D18-NOO9 continuously monitor the effluent from the Unit 1(2) reactor building. On high alarm, the monitors automatically initiate the following actions:

- A. Shutdown and isolation of the reactor building vent system
- B. Startup of the standby gas treatment system
- C. Isolation of primary containment purge and vent lines

Pertinent Information on these monitors is provided in LaSalle UFSAR Section 11.5.2.1.1.

### 10.1.2.4 Condenser Air Ejector Monitors

Monitors 1(2)D18-N002/N012 (pre-treatment) and 1(2)D18-N903A/B (post-treatment) continuously monitor gross gamma activity downstream of the steam jet air ejector and prior to release to the main stack.

On "high-high" alarm monitor 1(2)D18-N903A/B automatically initiates closure of valve 1(2)N62-F057 thus terminating the release.

Pertinent information on these monitors is found in LaSalle UFSAR Sections 11.5.2.1.2 and 11.5.2.1.3.

#### 10.1.2.5 Turbine Building Trackway

In order to quantify any identified releases via the Turbine Building trackway, at times of positive pressure in the Turbine Building, airborne sampling should be continuously collected using an air sampler located within the trackway. The air sampler collecting shall begin within 20 hours of the turbine building being at positive pressure, and then continuously for as long as the turbine building remains at positive pressure. The samples collected should be counted on a weekly basis. Air sampling to identify noble gas, iodine and particulate monitoring (either as a grab sample or continuous sampling) is designed to ensure evaluation of releases emanating from the Turbine Building.

The curie content of any contaminated material warehouse is maintained current by site administrative procedures. If a fire were to occur, the actual curie content of the warehouse would be used in determining the ground level release.

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10.1.3 Alarm and Trip Setpoints
10.1.3.1 Setpoint Calculations
10.1.3.1.1 Reactor Building Vent Effluent Monitor

The setpoint for the reactor building vent effluent monitor is established at 10 mR/hr.

10.1.3.1.2 Condenser Air Ejector Monitors

**Pre-Treatment Monitor** 

The high trip setpoint is established at 1.5 times the normal full power background rate, including nitrogen-16 (N-16) to help ensure that effluents are maintained ALARA.

The high-high trip setpoint is established at  $\leq$  100  $\mu$ Cl/sec per MW-th  $\equiv$  3.4E+05  $\mu$ Cl/sec per Technical Specification 3.7.6.

**Post-Treatment Monitor** 

The off-gas isolation setpoint is conservatively set at or below one-half the release limit calculated using the more conservative value obtained from equations 10-3 and 10-4 below.

The off gas isolation setpoint is converted into the monitor units of counts per second (cps) as follows:

(10-2)

 $P \le Q_{SVS} \times E \times [R_{png} / R_{OG}] + F_{OG}$ 

P Off-gas Post-treatment Monitor Isolation Setpoint

[cps]

The off-gas post-treatment monitor setpoint which initiates isolation of flow of off-gas to the station vent stack.

Q<sub>SVS</sub> Actual Station Vent Stack High Alarm Setpoint

[uCl/sec of png]

The actual high alarm setpoint of the Station Vent Stack wide range gas monitor in units of  $\mu$ Ci/sec of png (pseudo noble gas). This is determined by using Equations 10-3 and 10-4 and then converting the result to units of  $\mu$ Ci/sec of png.

E Efficiency of the Off-Gas Post Treatment Monitor

[cps/(µCi/sec of off gas mix)]

R<sub>prog</sub> Response of the Station Vent Stack WRGM to Pseudo Noble Gas

[cpm per µCi/cc of pseudo noble gas]

Ros Response of the Station Vent Stack WRGM to Off Gas

[cpm per µCi/cc of off gas]

Fog Maximum Off-Gas Flow Rate

[cc/sec]

10.1.3.1.3 Station Vent Stack Effluent Monitor

The high alarm setpoint for the station vent stack effluent monitor is conservatively set at or below one-half the calculated release limit calculated using the more conservative value obtained from equations 10-3 and 10-4 below. These equations yield the release limit in units of  $\mu$ Ci/sec of the mix specified in Section 10.1.3.3. For consistency with the monitor readout,

this calculated release limit is converted to units of  $\mu\text{Cl/sec}$  of pseudo noble gas before being entered into the monitor data base.

### 10.1.3.1.4 Standby Gas Treatment Stack Monitor

The high alarm setpoint for the standby gas treatment system effluent monitor is conservatively set at or below one-half the release limit calculated using the more conservative value obtained from equations 10-3 and 10-4 below. These equations yield the release limit in units of  $\mu$ Cl/sec of the mix specified in Section 10.1.3.3. For consistency with the monitor readout, this calculated release limit is converted to units of  $\mu$ Cl/sec of pseudo noble gas before being entered into the monitor data base.

### 10.1.3.2 Release Limits

Alarm and trip setpoints of gaseous effluent monitors are established to ensure that the release rate limits of RETS are not exceeded. The release limit  $Q_{\alpha}$  is found by solving Equations 10-3 and 10-4.

$$(1.11) Q_{ts} \sum \{f_i \, \overline{S}_i\} \le 500 \text{ mrem/yr}$$

 $Q_{E} \sum \{\overline{L_{i}} f_{i}(X/Q)_{i} \exp(-\lambda_{i} R/3600 U_{i}) + (1.11)(f_{i})S_{i}\} < 3000 \text{ mrem } / \text{yr}$ 

The summations are over noble gas radionuclides i.

fi Fractional Radionuclide Composition:

The release rate of noble gas radionuclide i divided by the total release rate of all noble gas radionuclides.

Q<sub>ts</sub> Total Allowed Release Rate, Stack Release

[uCi/sec of ODCM mix]

(10-3)

The total allowed release rate of all noble gas radionuclides released as stack releases in units of  $\mu$ Ci/sec of the mix specified in section 10.1.3.3.

† exp (-λ<sub>1</sub>R/3600 U<sub>s</sub>) is conservatively set equal to 1.0 for purposes of determining setpoints.

The remaining parameters in Equation 10-3 have the same definitions as in Equation A-8 of Appendix A. The remaining parameters in Equation 10-4 have the same definition as in Equation A-9 of Appendix A.

Equation 10-3 is based on Equation A-8 of Appendix A and the RETS restriction on whole body dose rate (500 mrem/yr) due to noble gases released in gaseous effluents (see Section A.1.3.1 of Appendix A). Equation 10-4 is based on Equation A-9 of Appendix A and the RETS restriction on skin dose rate (3000 mrem/yr) due to noble gases released in gaseous effluents (see Section A.1.3.2 of Appendix A).

The more conservative solution from Equations 10-3 and 10-4 is used as the limiting noble gas release rate.

Calibration methods and surveillance frequency for the monitors will be conducted as specified in the RETS.

### 10.1.3.3 Release Mixture

In the determination of alarm and trip set points, the radioactivity mixture in the exhaust air is assumed to have the radionuclide composition in Table 10-1.

#### 10.1.3.4 Conversion Factors

The conversion factors used to establish gaseous effluent monitor setpoints are obtained as follows.

Station vent stack effluent monitor.

Calibrations compare the response of station detectors to that of a reference detector using NIST traceable sources. Conversion factors for the station detectors are obtained from the response to noble gas or solid sources.

Condenser air ejector monitor.

**Pretreatment Monitor** 

The value is determined using noble gas radionuclides identified in a representative sample, and the offgas release rate and monitor response at the time the sample is taken.

Post-treatment Monitor

The value is determined using noble gas radionuclides identified in a representative sample, and the offgas concentration and monitor response at the time the sample is taken.

Standby gas treatment system monitor.

Calibrations compare the response of station detectors to that of a reference detector using NIST traceable sources. Conversion factors for the station detectors are obtained from the response to noble gas or solid sources.

#### 10.1.3.5 HVAC Flow Rates

The main stack flow rate is obtained from either the process computer or Monitor RM-23.

The SGTS flow rate is obtained from either the process computer or chart recorders in the main control room.

10.1.4 Allocation of Effluents from Common Release Points

Radioactive gaseous effluents released from the main chimney are comprised of contributions from both units. Under normal operating conditions, it is difficult to allocate the radioactivity between units due to fuel performance, in-plant leakage, power history, and other variables. Consequently, no allocation is normally made between the units. Instead, the entire release is treated as a single source.

10.1.5 Dose Projections

Because the gaseous releases are continuous, the doses are routinely calculated in accordance with the RETS.

10.2 LIQUID RELEASES

10.2.1 System Description

A simplified liquid radwaste and liquid effluent flow diagram are provided in Figures 10-2 and 10-3.

The liquid radwaste treatment system is designed and installed to reduce radioactive liquid effluents by collecting the liquids, providing for retention or holdup, and providing for treatment by filter or demineralizer for the purpose of reducing the total radioactivity prior to release to the environment. The system is described in Section 11.2.2 of the LaSalle UFSAR.

#### 10.2.1.1 Radwaste Discharge Tanks

There are two discharge tanks (1(2)WF05T, 25,000 gallons each) which receive water for discharge to the Illinois River via the cooling lake blowdown.

#### 10.2.1.2 Cooling Pond Blowdown

Cooling Pond Blowdown is the liquid discharge line to the Illinois River. The Cooling Pond Blowdown has a flow monitoring device as well as a compositor to meet the sampling requirements of ODCM Table 12.3.1-2.

#### 10.2.2 Radiation Monitors

#### 10.2.2.1 Liquid Radwaste Effluent Monitor

Monitor 0D18-K907 monitors all releases from the release tanks. On hi-hi alarm the monitor automatically initiates closure of valves 0WL067 and trips the radwaste discharge pump to terminate the release.

Pertinent information on the monitor and associated control devices is provided in LaSalle UFSAR Section 11.5.2.3.3.

#### 10.2.2.2 Service Water Effluent Monitors

Monitors 1/(2)D18-K912 continuously monitor the service water effluent. On high alarm service water discharge may be terminated manually. No control device is initiated by these monitors.

Pertinent information on these monitors is provided in LaSalle UFSAR 11.5.2.3.2.

#### 10.2.2.3 RHR Heat Exchanger Cooling Water Effluent Monitors

Instrument channels 1/(2)D18-N906/8 continuously monitor the RHR heat exchanger cooling water effluent. On high alarm the operating loop may be terminated manually and the redundant loop brought on line. No control device is initiated by these monitors.

Pertinent information on these monitors is provided in LaSalle UFSAR Section 11.5.2.3.4.

#### 10.2.3 Alarm and Trip Setpoints

#### 10.2.3.1 Setpoint Calculations

Alarm and trip setpoints of liquid effluent monitors at the principal release points are established to ensure that the limits of RETS are not exceeded in the unrestricted area.

#### 10.2.3.1.1 Liquid Radwaste Effluent Monitor

The monitor setpoint is found by solving equation 10-5 for the total isotopic activity.

$$P \leq K \times [\Sigma C_i^T / \Sigma (C_i^T / 10 \times DWC_i)] \times [(F^d + F_{max}^f)/F_{max}^f]$$

(10-5)

	P	Release Setpoint	[cpm]
	K	[Σ (K <sub>i</sub> x C <sub>i</sub> x W <sub>i</sub> )/ Σ C <sup>T</sup> <sub>i</sub> ] [cpm/□Ci/ml]	[cpm/µCl/ml]
	K <sub>t</sub>	Counting efficiency for radionuclide i	[cpm/µCi/ml]
	Wı	Weighting Factor	
	$C_i^T$	Concentration of radionuclide i in the release tank.	[µCi/ml]
	$F_{ m max}'$	Maximum Release Tank Discharge Flow Rate The maximum flow rate is 45 gpm.	[gpm]
	DWC	Derived Water Concentration of radionuclide i	[μCl/ml]
		The concentration of radionuclide I given in Appendix B, Tal 10CFR20.1001-2402.	ble 2, Column 2 to
	10	Multiplier associated with the limits specified in 12.3.1.A.	••
	$\cdot F^d$	Dilution Flow	[gpm]
10.2.3.1.2	Service Wa	ater Effluent Monitors	
	The monito	or setpoint is established at two times the background count rate	te (not to exceed 10000
10.2.3.1.3	RHR Heat	Exchanger Cooling Water Monitors	
	The monito	or setpoint is established at two times the background count ra	te (not to exceed 10000

cpm).

10.2.3.2 Discharge Flow Rates

10.2.3.2.1 Release Tank Discharge Flow Rate

Prior to each batch release, a grab sample is obtained.

The results of the analysis of the sample determine the discharge rate of each batch as follows:

$$F_{max}^{r} = 0.1 \times [F^{d}/\Sigma (C_{i}/10 \times DWC_{i})]$$

(10-6)

The summation is over radionuclides i.

0.1 Reduction factor for conservatism.

Frmax Maximum Permitted Discharge Flow Rate

[gpm]

The maximum permitted flow rate from the radwaste discharge tank.

F<sup>d</sup> Dilution Flow

[gpm]

C<sub>i</sub> Concentration of Radionuclide i in the Release Tank

[µCl/mL]

The concentration of radioactivity in the radwaste discharge tank based on measurements of a sample drawn from the tank.

DWC<sub>I</sub> Maximum Permissible Concentration of Radionuclide I

[µCi/ml]

The concentration of radionuclide i given in Appendix B, Table 2, Column 2 to 10CFR20.1001-2402.

10 Multiplier associated with the limits specified in 12.3.1.A.

MF Multiplication Factor

 $F_{max}^{r} < 0.5; MF = 3$ 

 $0.5 < F_{max}^{r} < 5$ ; MF = 5

 $5 < F_{max}^r$ ; MF = 7.5

10.2.3.2.2 Recommended Release Tank Flow Rate.

 $F'_{rec} = F' \max X MF$ 

(10-7)

Frec recommended discharge flow rate

(gpm)

F'max maximum permitted discharge flow rate

(gpm)

MF multiplication factor.

10.2.3.3 Release Limits

Release limits are determined from RETS. Calculated maximum permissible discharge rates are divided by 10 for conservatism and to ensure that release concentrations are well below applicable derived water concentrations (DWC).

10.2.3.4 Release Mixture

For the liquid radwaste effluent monitor the release mixture used for the setpoint determination is the radionuclide mix identified in the grab sample isotopic analysis plus four additional radionuclides. The additional radionuclides are H-3, Fe-59, Sr-89, and Sr-90. The quantities to be added are obtained from the most current analysis for these four radionuclides.

For all other liquid effluent monitors no release mixture is used because the setpoint is established at "two times background."

10.2.3.5 Conversion Factors

The readout for the liquid radwaste effluent monitor is in CPM. The calibration constant is based on the detector sensitivity to Cs-137/Ba-137 and an energy response curve.

10.2.3.6 Liquid Dilution Flow Rates

A conservative maximum blowdown flowrate of 20,000 gpm is used for all radwaste discharge calculations unless actual blowdown flow is determined to be less.

10.2.4 Allocation of Effluents from Common Release Points

Liquid releases from the Station will be allocated one half to Unit 1 and one half to Unit 2. Other potential pathways (i.e., RHR) are allocated to their respective unit.

10.2.5 Projected Doses for Releases

Doses are not calculated prior to release. Dose contributions from liquid effluents are determined in accordance with the RETS and station procedures.

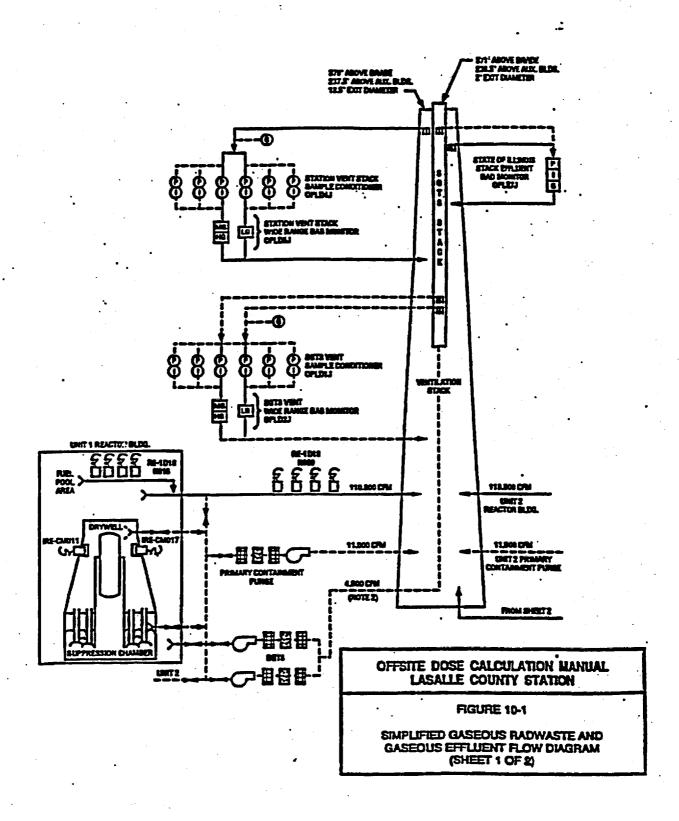
10.3 SOLIDIFICATION OF WASTE/PROCESS CONTROL PROGRAM

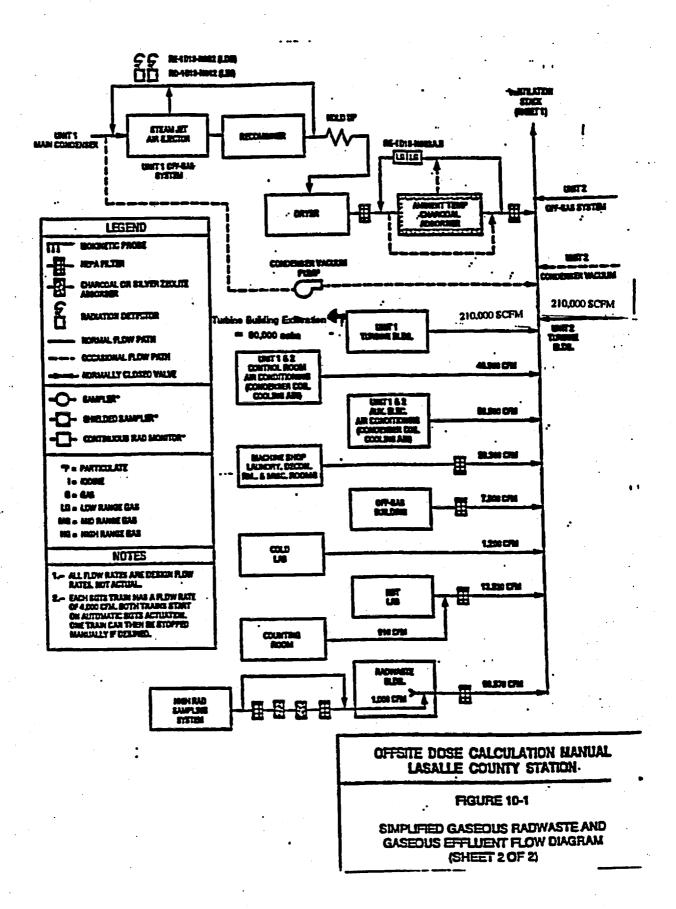
The process control program (PCP) contains the sampling, analysis, and formulation determination by which solidification of radioactive wastes from liquid systems is ensured.

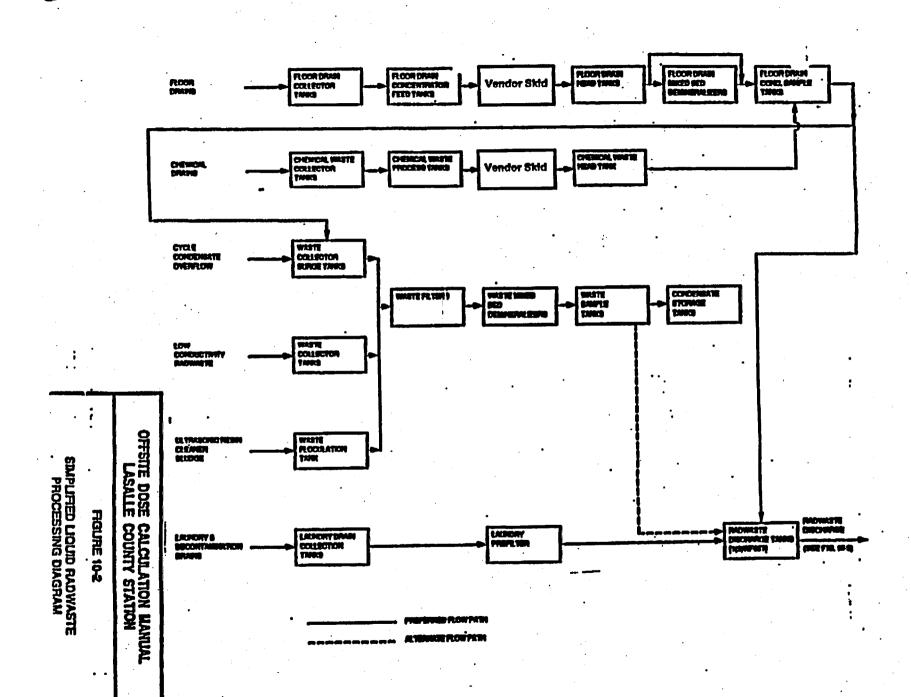
Figure 10-4 is a simplified diagram of solid radwaste processing.

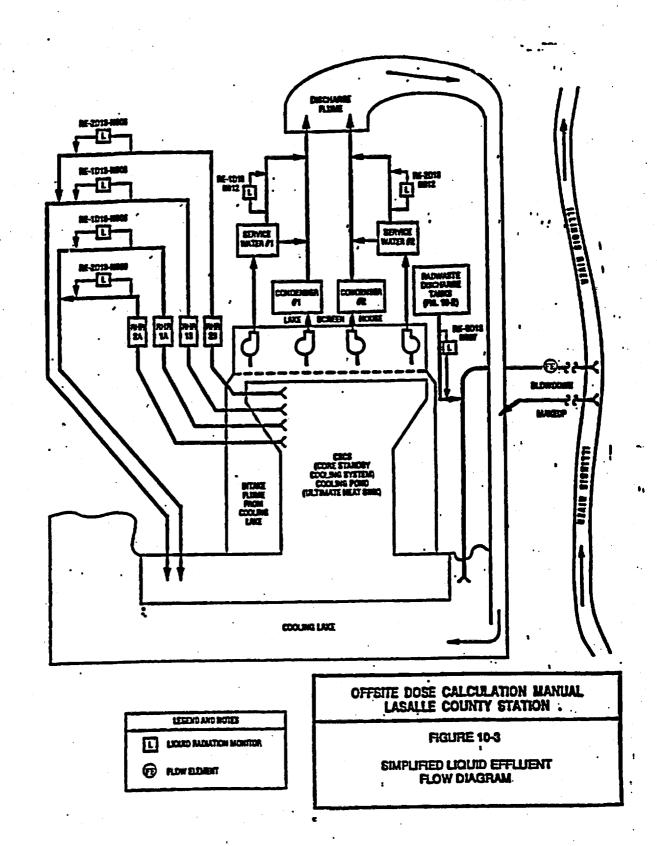
TABLE 10-1
Assumed Composition of the LaSalle Station Noble Gas Effluent

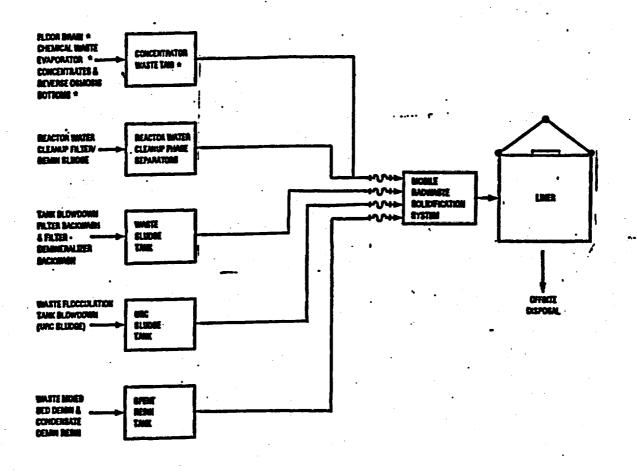
<u>Isotope</u>	Percent of Total Annual Release
Kr-83m	4.5E-3
Kr-85m	8.0E-3
Kr-85	2.6E-5
Kr-87	2.6E-2
Kr-88	2.6E-2
Kr-89	1.7E-1
Kr-90	3.7E-1
Xe-131m	2.0E-5
Xe-133m	3.8E-4
Xe-133	1.1E-2
Xe-135m	3.4E-2
Xe-135	2.9E-2
Xe-137	2.0E-1
Xe-138	1.2E-1

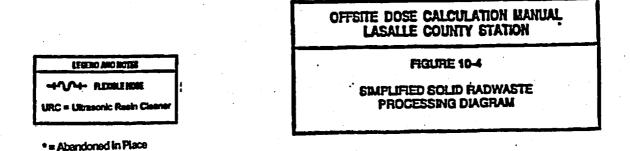












#### **CHAPTER 11**

#### LaSalle Annex Index

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11-11

#### LASALLE

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Sample Locations

**CHAPTER** 

# CHAPTER 11 RADIOLOGICAL ENVIRONMENTAL MONITORING PROGRAM

The Radiological Environmental Monitoring Program for the environs around LaSalle Station is given in Table 11-1.

Figures 11-1 through 11-3 show sampling and monitoring locations.





Exposure Pathway and/or Sample	Sample or Monitoring Loca	tion	Sampling or Collection Frequency	Type and Frequency of Analysis
1. Airborne  Radioiodine and a. Particulates	Indicators-Near Field L-01, Nearsite No. 1, 1.5 mi NNW L-03, Onsite No. 3, 1.0 mi ENE L-05, Onsite No. 5, 0.3 mi ESE L-06, Nearsite No. 6, 0.4 mi WSW	(2.4 km R) (1.6 km D) (0.5 km F) (0.6 km M)	Continuous sampler operation with particulate sample collection weekly, or more frequently if required by dust loading, and radiolodine canister collection biweekly.	I-131 analysis biweekly on near field and control samples <sup>1</sup> .  Particulate Sampler:  Gross beta analysis following weekly filter change <sup>2</sup> and gamma isotopic analysis <sup>3</sup> quarterly on composite filters by location on near field and control samples. <sup>1</sup>
b.	L-04, Rte 170, 3.2 mi E L-07, Seneca, 5.2 mi NNE L-08, Marseilles, 6.0 mi NNW L-11, Ransom, 6.0 mi S	(5.1 km E) (8.4 km B) (9.7 km R) (9.7 km J)		





Table 11-1 (Cont'd)

Badlalastast Paulusaus			las Bussians
Radiological Environme	iliai v	AOIIILOI.	illy rivyiaili

Exposure Pathway and/or Sample	Sample or Monitoring Location		Sampling or Collection Frequency	Type and Frequency of Analysis
2. <u>Direct Radiation</u>	a. <u>Indicators</u> -Inner Ring	(0.0.1 A)	Quarterly	Gamma dose on each TLD
	L-101-1, 0.5 mi N	(0.8 km A)		quarterly.
	L-101-2, 0.5 mi N	(0.8 km A)		
ŧ.	L-102-1, 0.6 mi NNE L-102-2, 0.6 mi NNE	(1.0 km B) (1.0 km B)	•	
	L-103-1, 0.7 mi NE	(1.0 km C)		
	L-103-1, 0.7 mi NE	(1.1 km C)		
	· •			
•	L-104-1, 0.8 mi ENE L-104-2, 0.8 mi ENE	(1.3 km D) (1.3 km D)		
	L-105-1, 0.7 ml E	(1.5 km E)	•	
	L-105-1, 0.7 m E L-105-2, 0.7 m E	. (1.1 km E)		
	L-106-1, 1.4 ml ESE	(2.2 km F)		
, '	L-106-2, 1.4 ml ESE	(2.2 km F)		
	L-107-1, 0.8 ml SE	(1.3 km G)		
	L-107-2, 0.8 mi SE	(1.3 km G)		
	L-108-1, 0.5 mi SSE	(0.8 km H)		
	L-108-2, 0.5 ml SSE	(0.8 km H)		
	L-109-1, 0.6 ml S	(1.0 km J)		
	L-109-2, 0.6 ml S	(1.0 km J)		
	L-110-1, 0.6 mi SSW	(1.0 km K)		•
	L-110-2, 0.6 ml SSW	(1.0 km K)		
	L-111b-1, 0.8 mi SW	(1.3 km L)		
•	L-111b-2, 0.8 ml SW	(1.3 km L)	• •	•
	L-112-1, 0.9 ml WSW	(1.4 km M)		
	L-112-2, 0.9 ml WSW	(1.4 km M)		
	L-113a-1, 0.8 ml W	(1.3 km N)		
	L-113a-2, 0.8 mi W	(1.3 km N)		
İ	L-114-1, 0.9 mi WNW	(1.4 km P)		
1	L-114-2, 0.9 ml WNW	(1.4 km P)		
	L-115-1, 0.7 mi NW	(1.1 km Q)		
İ	L-115-2, 0.7 ml NW	(1.1 km Q)		
	L-116-1, 0.6 mi NNW	(1.0 km R)		
	L-116-2, 0.6 mi NNW	(1.0 km R)		





Table 11-1 (Cont'd)

Exposure Pathway and/or Sample	Sample or Monito	oring Location	Sampling of <u>Collection Freq</u>	Type and Frequency of Analysis
2. Direct Radiation	b. Indicators-Outer Ring			
(Cont'd)	L-201-3, 4.0 mi N	(6.4 km A)		
(	L-201-4, 4.0 mi N	(6.4 km A)		
	L-202-3, 3.6 mi NNE	(5.8 km B)		
,	L-202-4, 3.6 mi NNE	(5.8 km B)	•	
	L-203-1, 4.0 mi NE	(6.4 km C)		
	L-203-2, 4.0 mi NE	(6.4 km C)		
	L-204-1, 3.2 mi ENE	(5.2 km D)		
	L-204-2, 3.2 mi ENE	(5.2 km D)	· ·	
	L-205-1, 3.2 mi ESE	(5.2 km F)		
	L-205-2, 3.2 ml ESE	(5.2 km F)		
	L-205-3, 5.1 mi E	(8.2 km E)		
	L-205-4, 5.1 mi E	(8.2 km E)		
	L-206-1, 4.3 mi SE	(6.9 km G)		
	L-206-2, 4.3 mi SE	(6.9 km G)		·
	L-207-1, 4.5 mi SSE	(7.2 km H)		
	L-207-2, 4.5 mi SSE	(7.2 km H)		
	L-208-1, 4.5 mi S	(7.2 km J)		
	L-208-2, 4.5 mi S	(7.2 km J)		
	L-209-1, 4.0 mi SSW	(6.4 km K)		
	L-209-2, 4.0 mi SSW	(6.4 km K)		
	L-210-1, 3.3 mi SW	(5.3 km L)		
	L-210-2, 3.3 ml SW	(5.3 km L)		
	L-211-1, 4.5 mi WSW	(7.2 km M)		
	L-211-2, 4.5 mi WSW	(7.2 km M)		
	L-212-1, 4.0 ml WSW	(6.4 km M)		
	L-212-2, 4.0 mi WSW	(6.4 km M)		
	L-213-3, 4.9 ml W	(7.9 km N)		
	L-213-4, 4.9 mi W	(7.9 km N)		
	L-214-3; 5.1 mi WNW	(8.2 km P)		
	L-214-4, 5.1 mi WNW	(8.2 km P)		÷
	L-215-3, 5.0 mi NW	(8.0 km Q)		,
	L-215-4, 5.0 ml NW	(8.0 km Q)	÷	
	L-216-3, 5.0 mi NNW	(8.0 km R)		•
	L-216-4, 5.0 mi NNW	(8.0 km R)		•





	Exposure Pathway and/or Sample		Sample or Monitoring Location	Sampling or Collection Frequency	Type and Frequency of Analysis
2.	Direct Radiation (Cont'd)	C.	<u>Other</u>		
			<u>Indicators</u>		
			One at each of the airborne location given in part 1.a and 1.b.		
		d.	Controls		
			One at each airborne control location given in part 1.c.		





E	Exposure Pathway and/or Sample		Sample or Monitoring Location		Sampling or Collection Frequency	Type and Frequency of Analysis
3.	<u>W</u> a	terborne				
	a	Ground/Well	a.	Indicators L-27, LSCS Onsite Well at Station L-28, Marseilles Well, 7.0 ml NW (11.3 km Q)	Quarterly	Gamma isotopic <sup>3</sup> and tritium analysis quarterly.
	b.	<b>Drinking Water</b>	•. •	There is no drinking water pathway within 6.2 mi (10 km) downstream of station.		
	C.	Surface Water	a.	Indicator L-40, Illinois River downstream, 5.2 mi NNW (8.4 km R)	Weekly grab sample	Gross beta and gamma isotopic analysis on monthly composite; tritium analysis on quarterly composite.
	d.	Control	<b>a.</b>	Control L-21, Illinois River at Seneca, 4.0 mi NE (6.4 km C)	Weekly grab sample	Gross beta and gamma isotopic analysis on monthly composite; tritium analysis on quarterly composite.
	e.	Sediments	a.	Indicators	Semiannually	Gamma isotopic analysis <sup>3</sup> semiannually.
				L-40, Illinois River downstream, 5.2 mi NNW (8.4 km R) L-41, Illinois River downstream 4.6 mi NNW (7.4 km A)		• •



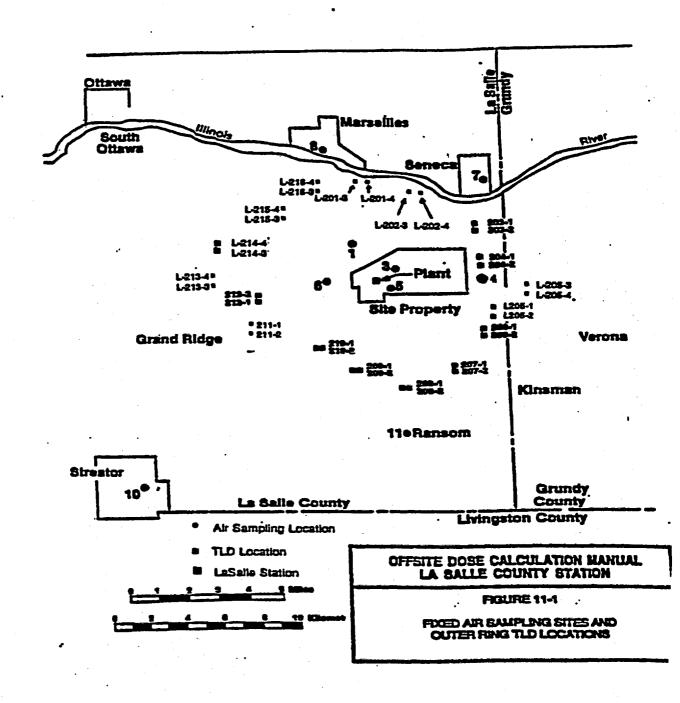


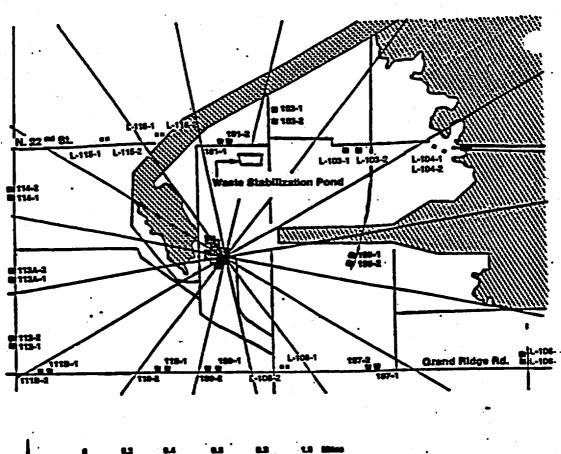
-		sure Pathway d/or Sample		Sample or Monitoring Location		Sampling or Collection Frequency	Type and Frequency of Analysis
4.	Inc	restion					
	a.	Milk	a.	<u>Indicators</u>		Biweekly: May through October; monthly:	Gamma isotopic <sup>3</sup> and I-131 analysis <sup>4</sup> biweekly May
				At the time of this revision, there are no de within 6.2 miles which consistently produc	lairi <del>es</del>	November through April	through October, monthly November through April.
			b.	<u>Controls</u>			
l				L-42, Biros Dairy, 14.2 ml E (22.9 km E)			
	b.	<u>Fish</u>	a.	Indicator			
			L-35, Marseilles Pool of Illinois River, 6.5 ml NW		km Q)	Two times annually	Gamma isotopic analysis <sup>3</sup> on edible portions of each
				L-34, LaSalle Lake 2 ml E (3.2 kg	km E)		
		•	b.	Control			
				L-36, Illinois River upstream of discharge, 4.3 mi NNE (6.9 l	km B)	•	
	C.	Food Products	a.	Indicators			
				Two samples from each of the four major within 6.2 miles of the station, if available		Annually	Gamma isotopic analysis <sup>3</sup> and I-131 analysis each
	on availability and therefor		Sample locations for food products may on availability and therefore are not requidentified here but shall be taken. <u>Controls</u>			sample.	
				Two samples within 9.3 to 18.6 miles of t	the station,		•

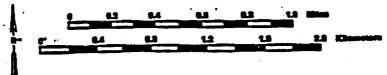




- Far field samples are analyzed when near field results are inconsistent with previous measurements and radioactivity is confirmed as having its origin in airborne effluents released from the station, or at the discretion of the Radiation Protection Director.
- Airborne particulate sample filters shall be analyzed for gross beta radioactivity 24 hours or more after sampling to allow for radon and thoron daughter decay. If gross beta activity in air particulate samples is greater than 10 times the yearly mean of control samples, gamma isotopic analysis shall be performed on the individual samples.
- Gamma isotopic analysis means the identification and quantification of gamma emitting radionuclides that may be attributable to the effluents from the station.
- I-131 analysis means the analytical separation and counting procedure are specific for this radionuclide.

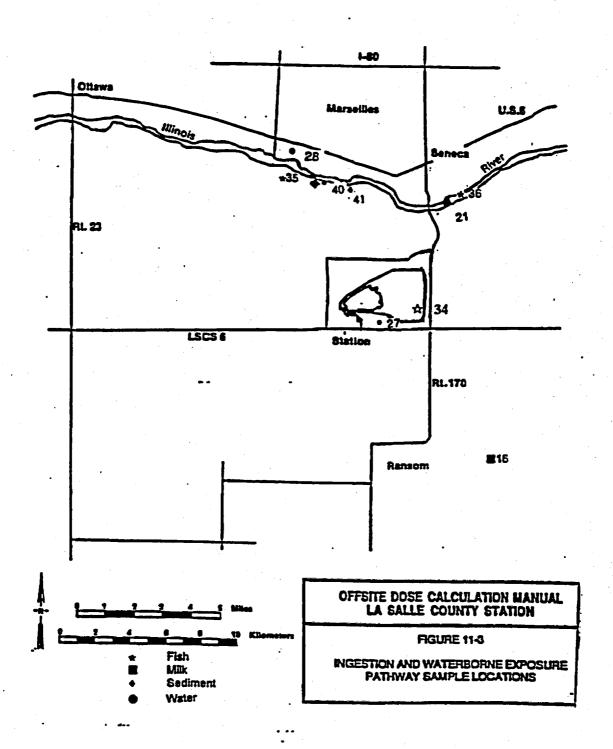






TLD Location

OFFESTIE DOSE CALCULATION MANUAL
LA SALLE COUNTY STATION
FIGURE 11-2
PANER RING TLD LOCATIONS



# LASALLE ANNEX INDEX CHAPTER 12

. Revision 5

#### **SPECIAL NOTE**

The transfer of the Radiological Effluent Technical Specifications (RETS) to the ODCM has been approved by the Nuclear Regulatory Commission in Amendments 85/69.

#### **CHAPTER 12**

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#### NOTE

The requirements of TSR 3.0.b apply to Chapter 12.

#### 12.0 RADIOLOGICAL EFFLUENT TECHNICAL STANDARDS

Chapter 12 of the LaSalle Station ODCM is a compilation of the various regulatory requirements, surveillances and bases, commitments and/or components of the radiological effluent and environmental monitoring programs for LaSalle Station. To assist in the understanding of the relationship between effluent regulations, ODCM equations, RETS (Chapter 12 section) and related Technical Specification requirements, Table 12.0-1 is a matrix which relates these various components. The Radiological Environmental Monitoring Program fundamental requirements are contained within this chapter, with LaSalle specific information in Chapter 11 and a supplemental matrix in Table 12.0-2.

TABLE 12.0-1
EFFLUENT COMPLIANCE MATRIX

Regulation	Dose to be compared to limit	ODCM	RETS	Technical
Regulation	Dose to be compared to infin	Equation	1.2.0	Specification
10CFR50 Appendix I	gamma air dose and beta air dose due to airborne radioactivity in effluent plume.	A-1 A-2	12.4.2	5.5.4.h
	whole body and skin dose due to airborne radioactivity in effluent plume are reported only if certain gamma and beta air dose criteria are exceeded.	A-6 A-7	N/A	N/A
	CDE for all organs and all four age groups due to lodines and particulates in effluent plume. All pathways are considered.	A-13	12.4.3	5.5.4.I
	CDE for all organs and all four age groups due to radioactivity in liquid effluents.	A-29	12.3.2	5.5.4.d
10CFR20	1. TEDE, totaling all deep dose equivalent components (direct, ground and plume shine) and committed effective dose equivalents (all pathways, both airborne and liquid-borne). CDE aluation is made for adult only g FGR 11 database.	A-38	12.4.9	5.5.4.c
40CFR190 (now by reference, also part of	Whole body dose (DDE) due to direct dose, ground and plume shine from all sources at a station.	A-35	12.4.7	5.5.4.J
10CFR20)	Organ doses (CDE) to an adult due to all pathways.	A-13		
Technical Specifications	"Instantaneous" whole body (DDE), thyroid (CDE) and skin (SDE), dose rates to an adult due to radioactivity in airborne effluents.	A-8 A-9 A-28	12.4.1	5.5.4.g
	For the thyroid dose, only inhalation is considered.			5.5.4.b
	"Instantaneous" concentration limits for liquid effluents.	A-32	12.3.1	
Technical Specifications	Radioactive Effluent Release Report	NA	12.6.2	5.6.3

Table 12.0-2

#### **REMP Compliance Matrix**

Regulation	Component	RETS	Technical Specification
10CFR50 Appendix I Section IV.B.2	Implement environmental monitoring program.	12.5.1	N/A
10CFR50 Appendix I Section IV.B.3	Land Use Census	12.5.2	N/A
10CFR50 Appendix I Section IV.B.2	Interlaboratory Comparison Program	12.5.3	N/A
10CFR50 Appendix I Section IV B.2 and Technical Specifications	Annual Radiological Environmental Operating Report	12.6.1	5.6.2

#### 12.1 **DEFINITIONS**

- 12.1.1 <u>ACTION</u> ACTION shall be that part of a requirement which prescribes remedial measures required under designated conditions.
- 12.1.2 CHANNEL CALIBRATION A CHANNEL CALIBRATION shall be the adjustment, as necessary, of the channel output such that it responds with the necessary range and accuracy to known values of the parameter which the channel monitors. The CHANNEL CALIBRATION shall encompass the entire channel, including the required sensor, alarm, display, and trip functions, and shall include the CHANNEL FUNCTIONAL TEST. Calibration of instrument channels with resistance temperature detector (RTD) or thermocouple sensors may consist of an inplace qualitative assessment of sensor behavior and normal calibration of the remaining adjustable devices in the channel. The CHANNEL CALIBRATION may be performed by any series of sequential, overlapping or total channel steps so that the entire channel is calibrated.
- 12.1.3 <u>CHANNEL CHECK</u> A CHANNEL CHECK shall be the qualitative assessment, by observation, of channel behavior during operation. This determination shall include, where possible, comparison of the channel indication and status to other indications or status derived from independent instrument channels measuring the same parameter.
- 12.1.4 CHANNEL FUNCTIONAL TEST A CHANNEL FUNCTIONAL TEST shall be the injection of a simulated signal into the channel as close to the sensor as practical to verify OPERABILITY including required alarm, interlock, display, and trip functions, and channel failure trips. The CHANNEL FUNCTIONAL TEST may be performed by any series of sequential, overlapping, or total channel steps so that the entire channel is tested.
- 12.1.5 <u>DOSE EQUIVALENT I-131</u> DOSE EQUIVALENT I-131 shall be that concentration of I-131, (microcuries/gram), that alone would produce the same thyroid dose as the quantity and isotopic mixture of I-131, I-132, I-133, I-134, and I-135 actually present. The thyroid dose conversion factors used for this calculation shall be those listed in Table III of TID-14844, AEC 1962, "Calculation of Distance Factors for Power and Test Reactor Sites;" Table E.7 of Regulatory Guide 1.109, Rev. 1, NRC, 1977; or ICRP 30, Supplement to Part 1, pages 192-212, Table titled, "Committed Dose Equivalent in Target Organs or Tissues per Intake of Unit Activity."
- 12.1.6 <u>FREQUENCY</u> Table 12.1-1 provides the definitions of various frequencies for which surveillances, sampling, etc. are performed unless defined otherwise. The provisions of Technical Specifications SR 3.0.2 and SR 3.0.3 are applicable to the frequencies except that they do not apply to the frequencies associated with the Radiological Environmental Monitoring Program (Section 12.5).
- 12.1.7 GASEOUS RADWASTE TREATMENT SYSTEM A GASEOUS RADWASTE TREATMENT SYSTEM shall be any system designed and installed to reduce radioactive gaseous effluents by collecting primary coolant system offgases from the primary system and providing for delay or holdup for the purpose of reducing total radioactivity prior to release to the environment.
- 12.1.8 <u>MEMBER(S) OF THE PUBLIC</u> means an individual except when that individual is receiving an occupational dose.
- 12.1.9 <u>MODE</u> A MODE shall correspond to any one of the inclusive combination of mode switch position, average reactor coolant temperature, and reactor pressure vessel head closure bolt tensioning specified in Table 12.1-2 with fuel in the reactor vessel.

- 12.1.10 OCCUPATIONAL DOSE means the dose received by an individual in the course of employment in which the individual's assigned duties involve exposure to radiation and/or to radioactive material from licensed and unlicensed sources of radiation, whether in the possession of the licensee or other person. Occupational dose does not include dose from background radiation as a patient from medical practices, from voluntary participation in medical research programs, or as a member of the public.
- 12.1.11 OPERABLE OPERABILITY A system, subsystem, division, component, or device shall be OPERABLE or have OPERABILITY when it is capable of performing its specified function(s), and when all necessary attendant instrumentation, controls, normal or emergency electrical power, cooling and seal water, lubrication, and other auxiliary equipment that are required for the system, subsystem, division, component or device to perform its function(s) are also capable of performing their related support function(s).
- 12.1.12 PROCESS CONTROL PROGRAM The PROCESS CONTROL PROGRAM (PCP) shall contain the current formulas, sampling, analyses, test, and determinations to be made to ensure that processing and packaging of solid radioactive wastes based on demonstrated processing of actual or simulated wet solid wastes shall be accomplished in such a way as to assure compliance with 10 CFR Parts 20, 61, and 71, State regulations, burial ground requirements, and other requirements governing the disposal of solid radioactive waste.
- 12.1.13 <u>PURGE PURGING</u> PURGE or PURGING shall be the controlled process of discharging air or gas from a confinement to maintain temperature, pressure, humidity, concentration or other operating condition, in such a manner that replacement air or gas is required to purify the confinement.
- 12.1.14 <u>RATED THERMAL POWER (RTP)</u> RTP shall be a total reactor core heat transfer rate to the reactor coolant of 3489 Mwt.
- 12.1.15 <u>SITE BOUNDARY</u> The SITE BOUNDARY shall be that line beyond which the land is neither owned, nor leased, nor otherwise controlled by the licensee.
- 12.1.16 <u>SOLIDIFICATION</u> SOLIDIFICATION shall be the conversion of radioactive wastes from liquid systems to a homogeneous (uniformly distributed), monolithic, immobilized solid with definite volume and shape, bounded by a stable surface of distinct outline on all sides (free-standing).
- 12.1.17 <u>SOURCE CHECK</u> A SOURCE CHECK shall be the qualitative assessment of channel response when the channel sensor is exposed to a radioactive source.
- 12.1.18 THERMAL POWER THERMAL POWER shall be the total reactor core heat transfer rate to the reactor coolant.
- 12.1.19 <u>UNRESTRICTED AREA BOUNDARY</u> means an area, access to which is neither limited nor controlled by the licensee.
- 12.1.20 <u>VENTILATION EXHAUST TREATMENT SYSTEM</u> A VENTILATION EXHAUST TREATMENT SYSTEM shall be any system designed and installed to reduce gaseous radiolodine or radioactive material in particulate form in effluents by passing ventilation or vent exhaust gases through charcoal adsorbers and/or HEPA filters for the purpose of removing lodines or particulates from the gaseous exhaust system prior to the release to the environment (such a system is not considered to have any effect on noble gas effluents). Engineered Safety Feature (ESF) atmospheric cleanup systems are not considered to be VENTILATION EXHAUST TREATMENT SYSTEM components.

- 12.1.21 <u>VENTING</u> VENTING shall be the controlled process of discharging air or gas from a confinement to maintain temperature, pressure, humidity, concentration or other operating condition, in such a manner that replacement air or gas is not provided or required during VENTING. Vent, used in system names, does not imply a VENTING process.
- 12.1.22 Definitions Peculiar to Estimating Dose to Members of the Public Using the ODCM Computer Program.
  - a. ACTUAL ACTUAL refers to using known release data to project the dose to members of the public for the previous time period. This data is stored in the database and used to demonstrate compliance with the reporting requirements of Chapter 12.6.
  - b. PROJECTED PROJECTED refers to using known release data from the previous time period or estimated release data to forecast a future dose to members of the public. This data is not incorporated into the database.

#### **TABLE 12.1-1**

#### **FREQUENCY NOTATION**

NOTATION	FREQUENCY
S - Shiftly	At least once per 12 hours.
D - Daily	At least once per 24 hours.
W - Weekly	At least once per 7 days.
M - Monthly	At least once per 31 days.
Q - Quarterly	At least once per 92 days.
SA - Semiannually	At least once per 184 days.
A - Annually	At least once per 366 days.
E - Sesquiannually	At least once per 18 months.
B - Refueling cycle	At least once per 24 months.
S/U - Startup	Prior to each reactor startup.
P - Prior	Prior to each radioactive release.
N.A.	Not applicable.

#### Table 12.1-2 (Page 1 of 1)

#### **MODES**

MODE	TITLE	REACTOR MODE SWITCH POSITION	AVERAGE REACTOR COOLANT TEMPERATURE (°F)
1	Power Operation	RUN	N/A
2	Startup	Refuef <sup>(a)</sup> or Startup/Hot Standby	N/A
.3	Hot Shutdown <sup>(a)</sup>	Shutdown	> 200
4	Cold Shutdown <sup>(a)</sup>	Shutdown	≤ 200
5	Refueling <sup>(b)</sup>	Shutdown or Refuel	NA NA

- (a) All reactor vessel head closure bolts fully tensioned.
- (b) One or more reactor vessel head closure bolts less than fully tensioned.

#### 12.2 <u>INSTRUMENTATION</u>

#### 12.2.1 Radioactive Liquid Effluent Monitoring Instrumentation

#### **Operability Requirements**

12.2.1.A The re

The radioactive liquid effluent monitoring instrumentation channels shown in Table 12.2.1-1 shall be OPERABLE with their alarm/trip setpoints set to ensure that the limits of Section 12.3.1.A are not exceeded. The alarm trip setpoints of these channels shall be determined in accordance with the ODCM Chapter 10.

Applicability:

At all times, when flow is present in the system.

#### Action:

- a. With a radioactive liquid effluent monitoring instrumentation channel alarm/trip setpoint less conservative than required, immediately suspend the release of radioactive liquid effluents monitored by the affected channel or declare the channel inoperable.
- b. With less than the minimum number of radioactive liquid effluent monitoring instrumentation channels OPERABLE, take the ACTION shown in Table 12.2.1-1. Restore the inoperable instrumentation to OPERABLE status within the time specified in the ACTION or, explain in the next Radioactive Effluent Release Report why this inoperability was not corrected within the time specified.

#### Surveillance Requirements

12.2.1.B

Each radioactive liquid effluent monitoring instrumentation channel shall be demonstrated OPERABLE by performance of the CHANNEL CHECK, SOURCE CHECK, CHANNEL FUNCTIONAL TEST and CHANNEL CALIBRATION operations at the frequencies shown in Table 12.2.1-2.

#### Bases

12.2.1.C

The radioactive liquid effluent monitoring instrumentation is provided to monitor and control, as applicable, the releases of radioactive materials in liquid effluents during actual or potential releases of liquid effluents. The alarm/trip setpoints for these instruments shall be calculated in accordance with the procedures in the ODCM to ensure that the alarm/trip will occur prior to exceeding the limits of RETS. The OPERABILITY and use of this instrumentation is consistent with the requirements of General Design Criteria 60, 63, and 64 of Appendix A to 10 CFR Part 50.

#### **TABLE 12.2.1-1**

#### RADIOACTIVE LIQUID EFFLUENT MONITORING INSTRUMENTATION

		INSTRUMENT	MINIMUM CHANNELS OPERABLE	ACTION	
1.		MA SCINTILLATION MONITOR PROVIDING ALARM AUTOMATIC TERMINATION OF RELEASE			
	a.	Liquid Radwaste Effluent Line	1		100
2.	GAM! NOT	MA SCINTILLATION MONITORS PROVIDING ALARM PROVIDING AUTOMATIC TERMINATION OF RELEA	BUT SE	•	
• .	a. b. c. d. e. f.	Service Water System Effluent Line (Unit 1) Service Water System Effluent Line (Unit 2) RHR Service Water (Line A) Effluent Line (Unit 1) RHR Service Water (Line A) Effluent Line (Unit 2) RHR Service Water (Line B) Effluent Line (Unit 1) RHR Service Water (Line B) Effluent Line (Unit 2)	1 1 1 1 1		101 101 101 101 101 101
3.	FLOV	V RATE MEASUREMENT DEVICES			
	a. b.	Liquid Radwaste Effluent Line Cooling Pond Blowdown Pipe*	1 1		102 102

<sup>\*</sup> Same as River Discharge Blowdown Pipe.

#### RADIOACTIVE LIQUID EFFLUENT MONITORING INSTRUMENTATION

#### TABLE 12.2.1-1 (Continued)

#### TABLE NOTATION

#### ACTION 100

With the number of OPERABLE channels less than required by the Minimum Channels OPERABLE requirement, effluent releases may continue for up to 14 days provided that prior to initiating a release:

- a. At least two independent samples are analyzed in accordance with Section 12.3.1.B.1, and
- b. At least two technically qualified members of the Facility Staff independently verify the release rate calculations and discharge line valving;

Otherwise, suspend release of radioactive effluents via this pathway.

#### **ACTION 101**

With the number of channels OPERABLE less than required by the Minimum Channels OPERABLE requirement, effluent releases via this pathway may continue for up to 30 days provided that, at least once per 8 hours, grab samples are collected and analyzed for principal gamma emitters and I-131 at a lower limit of detection as specified in Table 12.3.1-2. If effluent releases continue via this pathway beyond 30 days, continue to collect and analyze samples, then explain in the next Radioactive Effluent Release Report why this inoperability was not corrected within the time specified.

#### ACTION 102

With the number of channels OPERABLE less than required by the Minimum Channels OPERABLE requirement, actual radioactive releases in progress via this pathway may continue provided the flow rate is estimated at least once per 4 hours. Pump curves for Instrument 3a, or for known valve positions for Instrument 3b, may be used to estimate flow. Actual releases of radioactive effluent will not be initiated without an OPERABLE channel.





TABLE 12.2.1-2

RADIOACTIVE LIQUID EFFLUENT MONITORING INSTRUMENTATION SURVEILLANCE REQUIREMENTS

<u>INS</u>	TRUMENT	CHANNEL CHECK	SOURCE CHECK	CHANNEL FUNCTIONAL _TEST	CHANNEL CALIBRATION
1.	GAMMA SCINTILLATION MONITOR PROVIDING ALARM AND AUTOMATIC TERMINATION OF RELEASE	•			
	a. Liquid Radwaste Effluents Line	D	P	Q(1)	B(3)
2.	GAMMA SCINTILLATION MONITORS PROVIDING ALARM BUT NOT PROVIDING AUTOMATIC TERMINATION OF RELEASE			•	
	<ul> <li>a. Service Water System Effluent Line (Unit 1)</li> <li>b. Service Water System Effluent Line (Unit 2)</li> <li>c. RHR Service Water (Line A) Effluent Line (Unit 1)</li> <li>d. RHR Service Water (Line A) Effluent Line (Unit 2)</li> <li>e. RHR Service Water (Line B) Effluent Line (Unit 1)</li> <li>f. RHR Service Water (Line B) Effluent Line (Unit 2)</li> </ul>	D D D D	M M M M M	Q(2) Q(2) Q(2) Q(2) Q(2) Q(2)	B(3) B(3) B(3) B(3) B(3)
3.	FLOW RATE MEASUREMENT DEVICES				
	a. Liquid Radwaste Effluent Line     b. Cooling Pond Blowdown Pipe	D(4) D(4)	N.A. N.A.	P Q	B E

## RADIOACTIVE LIQUID EFFLUENT MONITORING INSTRUMENTATION

## TABLE 12.2.1-2 (Continued)

### TABLE NOTATION

- (1) The CHANNEL FUNCTIONAL TEST shall also demonstrate that automatic isolation of this pathway and control alarm annunciation occurs if any of the following conditions exist:
  - 1. Instrument indicates measured levels above the alarm/trip setpoint.
  - 2. Loss of power.
  - 3. Instrument alarms on downscale failure.
  - 4. Instrument controls not set in Operate or High Voltage mode.
- (2) The CHANNEL FUNCTIONAL TEST shall also demonstrate that control room alarm annunciation occurs if any of the following conditions exist:
  - 1. Instrument indicates measured levels above the alarm setpoint.
  - 2. Loss of power.
  - 3. Instrument alarms on downscale failure.
  - 4. Instrument controls not set in Operate or High Voltage mode.
- (3) The initial CHANNEL CALIBRATION shall be performed using one or more of the reference radioactive standards certified by the National Institute of Standards and Technology (NIST) or using standards that have been obtained from suppliers that participate in measurement assurance activities with NIST. These standards shall permit calibrating the system over its intended range of energy and measurement range. For subsequent CHANNEL CALIBRATION, the initial reference radioactive standards or radioactive sources that have been related to the initial calibration shall be used.
- (4) CHANNEL CHECK shall consist of verifying indication of flow during periods of release. CHANNEL CHECK shall be made at least once per 24 hours on days in which continuous, periodic, or batch releases are made.

## 12.2 <u>INSTRUMENTATION</u>

12.2.2 Radioactive Gaseous Effluent Monitoring Instrumentation

**Operability Requirements** 

12.2.2.A The radioactive gaseous effluent monitoring instrumentation channels shown in Table 12.2.2-1 shall be OPERABLE with their alarm/trip setpoints set to ensure that the limits of Section 12.4.1.A are not exceeded. The alarm/trip setpoints of these channels shall be determined in accordance with the ODCM.

Applicability: As shown in Table 12.2.2-1.

### Action:

- a. With a radioactive gaseous effluent monitoring instrumentation channel alarm/trip setpoint less conservative than required, immediately suspend the release of radioactive gaseous effluents monitored by the affected channel or declare the channel inoperable.
- b. With less than the minimum number of radioactive gaseous effluent monitoring instrumentation channels OPERABLE, take the ACTION shown in Table 12.2.2-1.

## Surveillance Requirements

12.2.2.B Each radioactive gaseous effluent monitoring instrumentation channel shall be demonstrated OPERABLE by performance of the CHANNEL CHECK, SOURCE CHECK, CHANNEL FUNCTIONAL TEST and CHANNEL CALIBRATION operations at the frequencies shown in Table 12.2.2-2.

## Bases

The radioactive gaseous effluent monitoring instrumentation is provided to monitor and control, as applicable, the releases of radioactive materials in gaseous effluents during actual or potential releases of gaseous effluents. The alarm/trip setpoints for these instruments shall be calculated in accordance with the procedures in the ODCM to ensure that the alarm/trip will occur prior to exceeding the limits of RETS.



## TABLE 12.2.2-1 RADIOACTIVE GASEOUS EFFLUENT MONITORING INSTRUMENTATION

	MINIMUM CHANNELS OPERABLE	APPLICABILITY	ACTION
INSTRUMENT'	OFENABLE	MI E(ONDIANIA	· · · · · · · · · · · · · · · · · · ·
1. MAIN CONDENSER OFFGAS TREATMENT SYSTEM EFFLUENT MONITORING SYSTEM a. Noble Gas Activity Monitor - Providing Alarm and Automatic Termination of Release (1(2) D18-N903A, K901A, K601A, R601) and/or (1(2) D18-N903B, K901B, K601B, R601)	2	**	110
2. MAIN STACK MONITORING SYSTEM a. Noble Gas Activity Monitor (0D18-N514, R517, R518 Low Range	1	•	110
WRGM) or (0D18-N515, R517, R518 Mid Range WRGM)	1	•	111
b. Iodine Sampler (Grab Sampler) c. Particulate Sampler (Grab Sampler)	1	•	111
<ul> <li>c. Particulate Sampler (Glab Sampler)</li> <li>d. Effluent System Flow Rate Monitor (0FT-VR019, 0FY-VR019 and 19A, 0FR-VR019, 0D18-K510, 0D18-R518)</li> <li>e. Sampler Flow Rate Monitor (Low: 0D18-N527, 0D18-N528, 0D18-R518; Mid/Hi: 0D18-N530, 0D18-N531, 0D18-R518)</li> </ul>	1 1	* *	112 112
<ol> <li>CONDENSER AIR EJECTOR RADIOACTIVITY MONITOR         <ul> <li>(Prior to Input to Holdup System)</li> <li>a. Noble Gas Activity Monitor (1(2) D18-N002, K613, R604)</li> <li>(1(2) D18-N012, K600, R605)</li> </ul> </li> </ol>	1	#	113
<ol> <li>SBGTS MONITORING SYSTEM</li> <li>Noble Gas Activity Monitor (0D18-N511, R515, R516 Low Range WRGM)</li> <li>or (0D18-N512, R515, R516 Mid Range WRGM)</li> </ol>	1	##	110
b. Iodine Sampler (Grab Sampler)	1	##	111
c. Particulate Sampler (Grab Sampler)	.1	##	111
d. Effluent System Flow Rate Monitor (1(2)FT-VG009, 1(2)FY-VG009, 1(2)FR-VG009)	1	## .	112
e. Sampler Flow Rate Monitor (Low: 0D18-N521, 0D18-N522, 0D18-R516; Mid/Hi: 0D18-N524, 0D18-N525, 0D18-R516)	1	## •	112
Equipment Part Number (EPN) numbers or monitor types are provided in parentheses "()"	•	•	***

## RADIOACTIVE GASEOUS EFFLUENT MONITORING INSTRUMENTATION TABLE 12.2.2-1 (Continued) TABLE NOTATION

- At all times.
- During effluent releases via this pathway.
- # During operation of the main condenser air ejector.
- ## During operation of the SBGTS.
- ACTION 110 a. For the Main Condenser Offgas Treatment System Effluent Monitoring System:

With only one channel OPERABLE, place the inoperable channel in a tripped condition within 1 hour.

With no channel OPERABLE, effluent releases via this pathway may continue for up to 30 days provided grab samples are taken at least once per 8 hours and these samples are analyzed for noble gas gamma emitters within 24 hours. (See NOTE below.)

b. For the Low/Mid Range of the Main Stack Monitoring System or SBGTS Monitoring System:

With the number of channels OPERABLE less than required by the Minimum Channels OPERABLE requirement, effluent releases via this pathway may continue for up to 30 days provided grab samples are taken at least once per 8 hours and these samples are analyzed for noble gas gamma emitters within 24 hours at a lower limit of detection as specified in Table 12.4.1-1. (See NOTE below.)

- ACTION 111 With the number of channels OPERABLE less than required by the Minimum Channels OPERABLE requirement, effluent releases via this pathway may continue for up to 30 days provided that within 4 hours after the channel has been declared inoperable, samples are continuously collected with auxiliary sampling equipment as required in Table 12.4.1-1. (See NOTE below.)
- ACTION 112 With the number of channels OPERABLE less than required by the Minimum Channels OPERABLE requirement, effluent releases via this pathway may continue for up to 30 days provided the flow rate is estimated at least once per 4 hours. (See NOTE below.)
- ACTION 113 With the number of channels OPERABLE less than required by the Minimum Channels OPERABLE requirement, the output from the charcoal adsorber vessels may be released to the environment for up to 72 hours provided:
  - a. The offgas treatment system is not bypassed, and
  - b. The offgas treatment delay system noble gas activity effluent downstream monitor is OPERABLE;

Otherwise, be in at least Mode 2 with the main steam isolation valves closed within 12 hours.

NOTE: For Actions 110 through 112 above, effluent releases may continue beyond the 30 days as long as the applicable sampling requirements are met. Explain in the next Radioactive Effluent Release Report why the inoperability was not corrected within the time specified.

TABLE 12.2.2-2			ATION SURVE	ILLANCE REQUIREME	NTS OPERATIONAL
TABLE 12.2.2-2  RADIOACTIVE GASEOUS EFFLUEN  INSTRUMENT	CHANNEL CHECK	SOURCE CHECK	FUNCTIONAL	CHANNEL CALIBRATION	CONDITIONS FOR WHICH SURVEIL- LANCE REQUIRED
MAIN CONDENSER OFFGAS TREATMENT SYSTE     EFFLUENT MONITORING SYSTEM	EM				
a. Noble Gas Activity Monitor - Providing Alarm and Automatic Termination of Release	D	D	Q(1)	B(3)	••
2. MAIN STACK MONITORING SYSTEM  a. Noble Gas Activity Monitor  b. lodine Sampler  c. Particulate Sampler  d. Effluent System Flow Rate Monitor  Computer Flow Rate Monitor	D W W D	M N.A. N.A. N.A. N.A.	Q(4) N.A. N.A. Q Q	B(3) N.A. B B	•
3. CONDENSER AIR EJECTOR RADIOACTIVITY M	ONITOR D	M	Q(2)	B(3)	#
a. Noble Gas Activity Monitor  a. Noble Gas Activity Monitor  b. Iodine Sampler  c. Particulate Sampler  d. Effluent System Flow Rate Monitor  e. Sampler Flow Rate Monitor	W W D D	M N.A N.A. N.A N.A	N.A.	B(3) N.A. ## B B	## ## ## ##

## RADIOACTIVE GASEOUS EFFLUENT MONITORING INSTRUMENTATION SURVEILLANCE REQUIREMENTS

## TABLE 12.2.2-2 (Continued)

## TABLE NOTATION

•	At all	times.
**	Durin	g effluent releases via this pathway.
#	Durin	g operation of the main condenser air ejector.
##	Durin	g operation of the SBGTS.
(1)	The (	CHANNEL FUNCTIONAL TEST shall also demonstrate the automatic isolation capability of eathway for the following conditions:
•	1.	Upscale.
	2.	Inoperative.
	3.	Downscale.
(2)	The (	CHANNEL FUNCTIONAL TEST for the log scale monitor shall also demonstrate that control alarm annunciation occurs for the following conditions:
	1.	Upscale.
	2.	Inoperative.
	3.	Downscale.
(3)	radio using assu inten the in	initial CHANNEL CALIBRATION shall be performed using one or more of the reference pactive standards certified by the National Institute of Standards and Technology (NIST) or g standards that have been obtained from suppliers that participate in measurement trance activities with NIST. These standards shall permit calibrating the system over its uded range of energy and measurement range. For subsequent CHANNEL CALIBRATION initial reference radioactive standards or radioactive sources that have been related to the I calibration shall be used.

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## RADIOACTIVE GASEOUS EFFLUENT MONITORING INSTRUMENTATION SURVEILLANCE REQUIREMENTS

## TABLE 12.2.2-2 (Continued)

## **TABLE NOTATION**

- (4) The CHANNEL FUNCTIONAL TEST shall also demonstrate that control room alarm annunciation occurs if any of the following conditions exists:
  - 1. Instrument indicates measured levels above the alarm setpoint.
  - 2. Loss of Counts

## 12.3 LIQUID EFFLUENTS

### 12.3.1 Concentration

**Operability Requirements** 

The concentration of radioactive material released from the site shall be limited to ten (10) times the concentration value in Appendix B, Table 2, Column 2 to 10CFR20.1001-20.2402 for radionuclides other than dissolved or entrained noble gases. For dissolved or entrained noble gases, the concentration shall be limited to the concentrations specified in Table 12.3.1-1.

<u>Applicability:</u> At all times. Action:

With the concentration of radioactive material released from the site exceeding the above limits, immediately restore the concentration to within the above limits.

Surveillance Requirements

- 12.3.1.B.1 The radioactivity content of each batch of radioactive liquid waste shall be determined prior to release by sampling and analysis in accordance with Table 12.3.1-2. The results of pre-release analyses shall be used with the calculational methods in the ODCM to assure that the concentration at the point of release is maintained within the limits of Section 12.3.1.A.
- Post-release analyses of samples composited from batch releases shall be performed in accordance with Table 12.3.1-2. The results of the previous post-release analyses shall be used with the calculational methods in the ODCM to assure that the concentrations at the point of release were maintained within the limits of Section 12.3.1.A.
- 12.3.1.B.3 The radioactivity concentration of liquids discharged from continuous release points shall be determined by collection and analysis of samples in accordance with Table 12.3.1-2. The results of the analyses shall be used with the calculational methods in the ODCM to assure that the concentrations at the point of release are maintained within the limits of Section 12.3.1.A.
- 12.3.1.B.4 Identify outside temporary liquid holdup tanks within the site and restrict the quantity of radioactive material contained in specified tanks to provide assurance that in the event of an uncontrolled release of the tanks contents, the resulting concentrations would be less than the limits of Section 12.3.1.A. Refer to LaSalle Technical Specification 5.5.9.b.

Bases

This requirement is provided to ensure that the concentration of radioactive materials released in liquid waste effluents from the site will be less than ten (10) times the concentration levels specified in Appendix B, Table 2, Column 2 to 10CFR20.1001-2402. This limitation provides additional assurance that the levels of radioactive materials in bodies of water outside the site will result in exposure within (1) the Section II.A design objectives of Appendix I, 10 CFR 50, to an individual, and (2) the limits of 10 CFR 20.1301 to the population. In addition, this limit is associated with 40 CFR 141 which states concentration limits at the nearest downstream potable water supply.

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## **TABLE 12.3.1-1**

# ALLOWABLE CONCENTRATION (AC) OF DISSOLVED OR ENTRAINED NOBLE GASES RELEASED FROM THE SITE TO UNRESTRICTED AREAS IN LIQUID WASTE

NUCLIDE	AC(µCi/m!)*
Kr 85 m	2E-4
85	5E-4
87	4E-5
<b>88</b>	9E-5
Ar 41	7E-5
Xe 131 m	7E-4
133 m	5E-4
133	6E-4
135 m	2E-4
135	. 2E-4

Computed from Equation 20 of ICRP Publication 2 (1959), adjusted for Infinite cloud submersion In water, and R = 0.01 rem/week, p<sub>w</sub> = 1.0 gm/cm<sup>3</sup>, and P<sub>w</sub>/P<sub>t</sub> = 1.0.

## **TABLE 12.3.1-2**

RADIOACTIVE LIQUID WASTE SAMPLING AND ANALYSIS PROGRAM

RADIOACTIVE LIQUID WASTE SAMPLING AND ANALYSIS PROGRAM					
LIQUID RELEASE TYPE	SAMPLING FREQUENCY	MINIMUM ANALYSIS FREQUENCY	TYPE OF ACTIVITY ANALYSIS	LOWER LIMIT OF DETECTION (LLD) (µCI/ml) <sup>8</sup>	
A. Batch Waste Release Tanks <sup>4</sup>	P Each Batch	P Each Batch	Principal Gamma Emitters <sup>1</sup>	5x10 <sup>-7</sup>	
	÷		I-131	1x10 <sup>-6</sup>	
	P One Batch/M	M	Dissolved and Entrained Gases (Gamma Emitters)	1x10 <sup>-5</sup>	
	P Each Batch	M Composite <sup>b</sup>	н-3	1x10 <sup>-6</sup>	
			Gross Alpha	1x10 <sup>-7</sup>	
	P Each Batch	Q Composite <sup>b</sup>	Sr-89, Sr-90	5x10 <sup>-6</sup>	
			Fe-55	1x10 <sup>-6</sup>	
B. Continuous Releases	Continuous <sup>c</sup>	W Composite <sup>c</sup>	Principal Gamma Emitters	5x10 <sup>-7</sup>	
Cooling Pond Blowdown			I-131	1x10 <sup>-6</sup>	
	M Grab Sample	М	Dissolved and Entrained Gases (Gamma Emitters)	1x10 <sup>-5</sup>	
	Continuous <sup>c</sup>	M Composite <sup>c</sup>	Н-3	1x10 <sup>-5</sup>	
			Gross Alpha	1x10 <sup>-7</sup>	
	Continuous	Q Composite <sup>c</sup>	Sr-89, Sr-90	5x10 <sup>-8</sup>	
			Fe-55	1x10 <sup>-6</sup>	

## RADIOACTIVE LIQUID WASTE SAMPLING AND ANALYSIS PROGRAM

## TABLE 12.3.1-2 (Continued)

## TABLE NOTATION

a. The LLD is the smallest concentration of radioactive material in a sample that will be detected with 95% probability with 5% probability of falsely concluding that a blank observation represents a "real" signal.

For a particular measurement system (which may include radiochemical separation):

4.66 s<sub>b</sub>

LLD = E.V. 2.22x10<sup>6</sup>. Y. exp (-λΔt)

Where:

- LLD is the "a priori" lower limit of detection as defined above (as microcurie per unit mass or volume),
- s<sub>b</sub> is the standard deviation of the background counting rate or of the counting rate of a blank sample as appropriate (as counts per minute),
- E is the counting efficiency (as counts per transformation),
- V is the sample size (in units of mass or volume),

2.22x10<sup>6</sup> is the number of transformations per minute per microcurie,

- Y is the fractional radiochemical yield (when applicable),
- λ is the radioactive decay constant for the particular radionuclide and for composite samples, and
- At Is the elapsed time between midpoint of sample collection and time of counting (for plant effluents, not environmental samples). For batch samples taken and analyzed prior to release, Δt is taken to be zero.

The value of  $s_b$  used in the calculation of the LLD for a detection system shall be based on the actual observed variance of the background counting rate or of the counting rate of the blank samples (as appropriate) rather than on an unverified theoretically predicted variance. Typical values of E, V, Y, and  $\Delta t$  shall be used in the calculation.

## Alternate LLD Methodology

An alternate methodology for LLD determination follows and is similar to the above LLD equation:

(2.71 + 4.65√B)• Decay LLD = \_\_\_\_\_\_ E q b Y t (2.22 x 10<sup>6</sup>)

## TABLE 12.3.1-2 (Continued) RADIOACTIVE LIQUID WASTE SAMPLING AND ANALYSIS PROGRAM TABLE NOTATIONS

Where:

B = background sum (counts)

E = counting efficiency

q = sample quantity (mass or volume)

b = abundance (if applicable)

Y= fractional radiochemical yield or collection efficiency (if applicable)

t= count time (minutes)

2.22 x 10<sup>6</sup> = number of disintegrations per minute per microCurie

 $2.71 + 4.65\sqrt{B} = k^2 + (2k\sqrt{2}\sqrt{B})$ , and k = 1.645

(k=value of the t statistic from the single-tailed t distribution at a significance level of 0.95 and infinite degrees of freedom. This means that the LLD result represents a 95% detection probability with a 5% probability of falsely concluding that the nuclide is present when it is not or that the nuclide is not present when it is.)

Decay =  $e^{\lambda \Delta t} [\lambda RT/(1-e^{-\lambda RT})][\lambda T_d/(1-e^{-\lambda Td})]$  if applicable

 $\lambda$  = radioactive decay constant (units consistent with  $\Delta t$ , RT and  $T_d$ )

 $\Delta t$  = "delta t", or the elapsed time between sample collection or the midpoint of sample collection and the time the count is started, depending on the type of sample (units consistent with  $\lambda$ )

RT = elapsed real time, or the duration of the sample count (units consistent with  $\lambda$ )

 $T_d$  = sample deposition time, or the duration of analyte collection onto the sample media (units consistent with  $\lambda$ )

The LLD may alternately be determined using installed radioanalytical software, if available. In addition to determining the correct number of channels over which to total the background sum, utilizing the software's ability to perform decay corrections (i.e. during sample collection, from sample collection to start of analysis, and during counting), this alternate method will result in a more accurate determination of the LLD.

It should be recognized that the LLD is defined as a before the fact limit representing the capability of a measurement system and not as an after the fact limit for a particular measurement.

## RADIOACTIVE LIQUID WASTE SAMPLING AND ANALYSIS PROGRAM

## TABLE 12.3.1-2 (Continued)

## TABLE NOTATION

- b. A composite sample is one in which the quantity of liquid sampled is proportional to the quantity of liquid waste discharged and in which the method of sample employed results in a specimen which is representative of the liquids released.
- c. To be representative of the quantities and concentrations of radioactive materials in liquid effluents, samples shall be collected in proportion to the rate of flow of the effluent stream. Prior to analyses, all samples taken for the composite shall be thoroughly mixed in order for the composite sample to be representative of the effluent release.
- d. A batch release is the discharge of liquid waste of a discrete volume. Prior to sampling for analyses, each batch shall be isolated, and then thoroughly mixed to assure representative sampling.
- e. A continuous release is the discharge of liquid wastes of a nondiscrete volume; e.g., from a volume of system that has an input flow during the continuous release.
- f. The principal gamma emitters for which the LLD specification applies exclusively are the following radionuclides: Mn-54, Fe-59, Co-58, Co-60, Zn-65, Mo-99, Cs-134, Cs-137, Ce-141, and Ce-144. This list does not mean that only these nuclides are to be detected and reported. Other peaks which are measurable and identifiable, at the 95% confidence level, together with the above nuclides, shall also be identified and reported.

## 12.3 LIQUID EFFLUENTS

12.3.2 Dose

**Operability Requirements** 

12.3.2.A The dose or dose commitment to an individual from radioactive materials in liquid effluents released, from each reactor unit, from the site shall be limited:

- a. During any calendar quarter to less than or equal to 1.5 mrem to the total body and to less than or equal to 5 mrem to any organ, and
- b. During any calendar year to less than or equal to 3 mrem to the total body and to less than or equal to 10 mrem to any organ.

APPLICABILITY:

At all times.

### **ACTION:**

a. With the calculated dose from the release of radioactive materials in liquid effluents exceeding any of the above limits, prepare and submit to the Commission, pursuant to 10CFR50, Appendix I, Section IV.A, a report which identifies the cause(s) for exceeding the limit(s) and defines the corrective actions to be taken to reduce the releases of radioactive materials in liquid effluents during the remainder of the current calendar quarter and during the subsequent three calendar quarters, so that the cumulative dose or dose commitment to an individual from these releases is within 3 mrem to the total body and 10 mrem to any organ. The Report shall also include the radiological impact on finished drinking water supplies at the nearest downstream drinking water source. The Report is due to the NRC within 30 days from the end of the quarter in which the release occurred.

Surveillance Requirements

12.3.2.B <u>Dose Calculations</u>- Cumulative dose contributions from liquid effluents shall be determined in accordance with the ODCM at least once per 31 days, when liquid discharges are performed.

Bases

This requirement is provided to implement the requirements of Sections II.A, III.A 12.3.2.C and IV.A of Appendix I, 10 CFR Part 50. The Limiting Condition for Operation implements to guides set forth in Section II.A of Appendix I. The ACTION statements provide the required operating flexibility and at the same time implement the guides set forth in Section IV.A of Appendix I to assure that the releases of radioactive material in liquid effluents will be kept "as low as Is reasonably achievable." Also, for fresh water sites with drinking water supplies which can be potentially affected by plant operations, there is reasonable assurance that the operation of the facility will not result in radionuclide concentrations in the finished drinking water that are in excess of the requirements of 40 CFR 141. The dose calculations in the ODCM implement the requirements in Section III.A of Appendix I that conformance with the guides of Appendix I be shown by calculational procedures based on models and data, such that the actual exposure of an Individual through appropriate pathways is unlikely to be substantially underestimated. The equations specified in the ODCM for calculating the doses due to the actual release rates of radioactive materials in liquid effluents are consistent with the methodology provided in Regulatory Guide 1.109, "Calculation of Annual Doses to Man from Routine Releases of Reactor Effluents for the

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Purpose of Evaluating Compliance with 10 CFR Part 50, Appendix I," Revision 1, October 1977 and Regulatory Guide 1.113, "Estimating Aquatic Dispersion of Effluents from Accidental and Routine Reactor Releases for the Purpose of Implementing Appendix I," April 1977.

This requirement applies to the release of radioactive materials in liquid effluents from each reactor at the site. For units with shared radwaste treatment systems, the liquid effluents from the shared are proportioned among the units sharing that system.

## 12.3 LIQUID EFFLUENTS

## 12.3.3 Liquid Waste Treatment System

Operability Requirements

The liquid radwaste treatment system shall be OPERABLE. The appropriate portions of the system shall be used to reduce the radioactive materials in liquid wastes prior to their discharge when the projected doses due to the liquid effluent from each reactor unit, from the site, when averaged over 31 days, would exceed 0.06 mrem to the total body or 0.2 mrem to any organ.

Applicability: At all times.

## Action:

- a. With the liquid radwaste treatment system inoperable for more than 31 days or with radioactive liquid waste being discharged without treatment and in excess of the above limits, prepare and submit to the Commission within 30 days a Special Report which includes the following Information:
  - 1. Identification of the inoperable equipment or subsystems and the reason for inoperability.
  - 2. Action(s) taken to restore the inoperable equipment to OPERABLE status, and
  - 3. Summary description of action(s) taken to prevent a recurrence.

Surveillance Requirements

- 12.3.3.B.1 Doses due to liquid releases shall be projected at least once per 31 days when releases are to be performed, in accordance with the methods in the ODCM.
- The liquid radwaste treatment system shall be demonstrated OPERABLE by operating the liquid radwaste treatment system equipment for at least 30 minutes at least once per 92 days unless the liquid radwaste system has been utilized to process radioactive liquid effluents during the previous 92 days.

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**Bases** 

The OPERABILITY of the liquid radwaste treatment system ensures that this 12.3.3.C system will be available for use whenever liquid effluents require treatment prior to release to the environment. The requirement that the appropriate portions of this system be used when specified provides assurance that the releases of radioactive materials in liquid effluents will be kept "as low as is reasonably achievable." A system bypass allows connection to portable waste treatment equipment. This enables the efficient processing of liquid radwaste through the use of state-of-theart radwaste processing technology. The portable radwaste treatment system may be used in lieu of various portions of the liquid radwaste treatment system when a portable waste treatment is not used, Surveillance Requirement 12.3.3.B.2 may be extended to 180 days. This specification implements the requirements of 10 CFR Part 50.36a. General Design Criterion 50 of Appendix A to 10 CFR Part 50 and the design objective given in Section II.0 of Appendix I to 10 CFR Part 50. The specified limits governing the use of appropriate portions of the liquid radwaste treatment system were specified as a suitable fraction of the dose design objectives set forth In Section II.A of Appendix I, 10 CFR Part 50, for liquid effluents.

## 12.4 GASEOUS EFFLUENTS

## 12.4.1 Dose Rate

### **Operability Requirements**

- The dose rate due to radioactive materials released in gaseous effluents from the site to areas at and beyond the SITE BOUNDARY, shall be limited to the following:
  - a. For noble gases: Less than or equal to a dose rate of 500 mrem/yr to the total body and less than or equal to a dose rate of 3000 mrem/yr to the skin, and
  - b. For iodine-131, for iodine-133, for tritium, and for all radionuclides in particulate form with half lives greater than 8 days: Less than or equal to a dose rate of 1500 mrems/yr to any organ via the inhalation pathway.

Applicability: At all times.

## Action:

With the dose rate(s) exceeding the above limits, immediately decrease the release rate to within the above limit(s).

## Surveillance Requirements

- 12.4.1.B.1 The dose rate due to noble gases in gaseous effluents shall be determined to be within the above limits in accordance with the methodology and parameters of the ODCM by obtaining representative samples and performing analyses in accordance with the sampling and analysis program specified in Table 12.4.1-1.
- The dose rate due to lodine-131, lodine-133, tritium, and all radionuclides in particulate form with half lives greater than eight days, in accordance with the methodology and parameters of the ODCM by obtaining representative samples and performing analyses in accordance with the sampling and analysis program specified in Table 12.4.1-1.

## **Bases**

This specification is provided to ensure that the dose at any time at the site 12.4.1.C boundary from gaseous effluents from all units on the site will be within the annual dose limits of RETS for unrestricted areas. These limits provide reasonable assurance that radioactive material discharged in gaseous effluents will not result in the exposure of an individual in an unrestricted area, either within or outside the site boundary exceeding the limits specified in 10CFR20.1301. For individuals who may at times be within the site boundary, the occupancy of the individual will be sufficiently low to compensate for any increase in the atmospheric diffusion factor above that for the site boundary. The specified release rate limits restrict, at all times, the corresponding gamma and beta dose rates above background to an individual at or beyond the site boundary to less than or equal to a dose rate of 500 mrem/year to the total body or to less than or equal to a dose rate of 3000 mrem/year to the skin. These release rate limits also restrict, at all times, the corresponding thyroid dose rate above background via the inhalation pathway to less than or equal to a dose rate of 1500 mrem/year.

This specification applies to the release of radioactive effluents in gaseous effluents from all reactors at the site. For units within shared radwaste treatment systems, the gaseous effluents from the shared system are proportioned among the units sharing that system.

## TABLE 12.4.1-1 RADIOACTIVE GASEOUS WASTE SAMPLING AND ANALYSIS PROGRAM

GASEOUS RELEASE TYPE	SAMPLING FREQUENCY	MINIMUM ANALYSIS FREQUENCY	TYPE OF ACTIVITY ANALYSIS	LOWER LIMIT OF DETECTION (LLD) (µCi/mi) <sup>6</sup>
A. Containment Vent and Purge System <sup>h</sup>	P Each Purge <sup>b</sup> Grab Sample	P Each Purge <sup>b</sup>	Principal Gamma Emitters <sup>9</sup>	1x10 <sup>-1</sup> 
			Н-3	1x10 <sup>-6</sup>
B. Main Vent Stack	M <sup>b</sup> Grab Sample	Wp	Principal Gamma Emitters <sup>g</sup>	1x10 <sup>-4</sup>
	W <sup>b,s</sup> Grab Sample	M <sub>p'e</sub>	H-3	1x10 <sup>6</sup>
C. Standby Gas Treatment System	D <sup>c</sup> Grab Sample	De	Principal Gamma Emitters <sup>0</sup>	1x10 <sup>-1</sup>
D. Main Vent Stack And Standby Gas Treatment System <sup>c</sup>	Continuous <sup>1</sup>	W <sup>d</sup> Charcoal Sample	I-131	1x10 <sup>-12</sup>
			I-133	1x10 <sup>-10</sup>
	Continuous	W <sup>d</sup> Particulate Sample	Principal Gamma Emitters <sup>©</sup> (I- 131, Others)	1x10 <sup>-11</sup>
	Continuous <sup>f</sup>	M Composite Particulate Sample	Gross Alpha	1x10 <sup>-11</sup>
	Continuous <sup>f</sup>	Q Composite Particulate Sample	Sr-89,Sr-90	1x10 <sup>-11</sup>
	Continuous <sup>f</sup>	Noble Gas Monitor	Noble Gases Gross Beta or Gamma	1x10 <sup>-6</sup>

## TABLE 12.4.1-1 (Continued)

GASEOUS RELEASE TYPE	SAMPLING FREQUENCY	MINIMUM ANALYSIS FREQUENCY	TYPE OF ACTIVITY ANALYSIS	LOWER LIMIT OF DETECTION (LLD) (µCi/ml) <sup>4</sup>
E. Oil Burner	P Each Batch Grab Sample	P Each Batch	Principle Gamma Emitters	5x10 <sup>-7</sup>
			Dissolved and Entrained Gases (Gamma Emitters)	1x10 <sup>-6</sup>
		ļ ·	I-131	1x10 <sup>-6</sup>
	P Each Batch Grab Sample	M Composite	н-з	1×10 <sup>-5</sup>
	Grab Sample	:	Gross Alpha	1x10 <sup>-7</sup>
		Q Composite	Sr-89, Sr-90	5x10 <sup>-8</sup>
			Fe-55	1x10 <sup>-6</sup>

## TABLE 12.4.1-1 (Continued)

## RADIOACTIVE GASEOUS WASTE SAMPLING AND ANALYSIS PROGRAM

## TABLE NOTATION

a. The LLD is the smallest concentration of radioactive material in a sample that will be detected with 95% probability with 5% probability of falsely concluding that a blank observation represents a "real" signal.

For a particular measurement system (which may include radiochemical separation):

4.66 s<sub>b</sub>

LLD = E.V. 2.22x10<sup>6</sup>. Y. exp (-
$$\lambda$$
Δt)

Where:

- LLD is the "a priori" lower limit of detection as defined above (as microcurie per unit mass or volume),
- s<sub>b</sub> is the standard deviation of the background counting rate or of the counting rate of a blank sample as appropriate (as counts per minute),
- E is the counting efficiency (as counts per transformation),
- V is the sample size (in units of mass or volume),
- 2.22x10<sup>6</sup> is the number of transformations per minute per microcurie,
- Y is the fractional radiochemical yield (when applicable),
- λ is the radioactive decay constant for the particular radionuclide, and
- At is the elapsed time between midpoint of sample collection and time of counting (for plant effluents, not environmental samples).

The value of  $s_b$  used in the calculation of the LLD for a detection system shall be based on the actual observed variance of the background counting rate or of the counting rate of the blank samples (as appropriate) rather than on an unverified theoretically predicted variance. Typical values of E, V, Y, and  $\Delta t$  shall be used in the calculation.

### Alternate LLD Methodology

An alternate methodology for LLD determination follows and is similar to the above LLD equation:

## TABLE 12.4.1-1 (Continued) RADIOACTIVE GASEOUS WASTE SAMPLING AND ANALYSIS PROGRAM TABLE NOTATION

Where:

B = background sum (counts)

E = counting efficiency

q = sample quantity (mass or volume)

b = abundance (if applicable)

Y= fractional radiochemical yield or collection efficiency (if applicable)

t= count time (minutes)

2.22 x 10<sup>6</sup> = number of disintegrations per minute per microCurie

 $2.71 + 4.65\sqrt{B} = k^2 + (2k\sqrt{2}\sqrt{B})$ , and k = 1.645

(k=value of the t statistic from the single-tailed t distribution at a significance level of 0.95 and infinite degrees of freedom. This means that the LLD result represents a 95% detection probability with a 5% probability of falsely concluding that the nuclide is present when it is not or that the nuclide is not present when it is.)

Decay =  $e^{\lambda \Delta^t} [\lambda RT/(1-e^{-\lambda RT})][\lambda T_d/(1-e^{-\lambda Td})]$  if applicable

 $\lambda$  = radioactive decay constant (units consistent with  $\Delta t$ , RT and  $T_d$ )

 $\Delta t$  = "delta t", or the elapsed time between sample collection or the midpoint of sample collection and the time the count is started, depending on the type of sample (units consistent with  $\lambda$ )

RT = elapsed real time, or the duration of the sample count (units consistent with  $\lambda$ )

 $T_d$  = sample deposition time, or the duration of analyte collection onto the sample media (units consistent with  $\lambda$ )

The LLD may alternately be determined using installed radioanalytical software, if available. In addition to determining the correct number of channels over which to total the background sum, utilizing the software's ability to perform decay corrections (i.e. during sample collection, from sample collection to start of analysis, and during counting), this alternate method will result in a more accurate determination of the LLD.

It should be recognized that the LLD is defined as a before the fact limit representing the capability of a measurement system and not as an after the fact limit for a particular measurement.

b. Sampling and analyses shall also be performed following shutdown, startup, or a thermal power change exceeding 20 percent of rated thermal power in 1 hour unless (1) analysis shows that the dose equivalent I-131 concentration in the primary coolant has not increased more than a factor of 5, and (2) the noble gas activity monitor shows that effluent activity has not increased by more than a factor of 3.

## TABLE 12.4.1-1 (Continued) RADIOACTIVE GASEOUS WASTE SAMPLING AND ANALYSIS PROGRAM TABLE NOTATION

- c. Whenever there is flow through the SBGTS. (If SBGT is run more than 10 minutes in a 24 hour period then it must be run a minimum of 5 hours. The 5 hour run is required to meet the sample requirements for lodine and particulates.) When SBGT equipment is started and shutdown, ensure noble gas lodine and particulate samples are taken.
- d. Samples shall be changed at least once per 7 days and the analyses completed within 48 hours after removal from the sampler. Sampling shall also be performed within 24 hours following each shutdown, startup, or thermal power level change exceeding 20% of rated thermal power in one hour. This requirement does not apply if 1) analysis shows that the dose equivalent I-131 concentration in the primary coolant has not increased by more than a factor of 5, and 2) the noble gas activity monitor shows that effluent activity has not increased by more than a factor of 3. When samples collected for 24 hours are analyzed, the corresponding LLDs may be increased by a factor of 10.
- e. Tritium grab samples shall be taken at least once per 7 days from the plant vent to determine tritium releases in the ventilation exhaust from the spent fuel pool area whenever spent fuel is in the spent fuel pool. If there is no spent fuel in the fuel pool, sampling and analysis of tritium grab samples shall be performed at least monthly.
- f. The ratio of the sample flow rate to the sampled stream flow rate shall be known for the time period covered by each dose or dose rate calculation made in accordance with Sections 12.4.1.A, 12.4.2.A and 12.4.3.A.
- g. The principal gamma emitters for which the LLD specification applies include the following radionuclides: Kr-87, Kr-88, Xe-133, Xe-133m, Xe-135, and Xe-138 for gaseous emissions and Mn-54, Fe-59, Co-58, Co-60, Zn-65, Mo-99, Cs-134, Cs-137, Ce-141 and Ce-144 for particulate emissions. This list does not mean that only these nuclides are to be detected and reported. Other peaks which are measurable and identifiable, at the 95% confidence level, together with the above nuclides, shall also be identified and reported.
- h. The drywell tritium and noble gas sample results are valid for 30 hours from sample time if 1) the drywell radioactivity monitors have not indicated an increase in airborne or gaseous radioactivity, and 2) the drywell equipment and floor drain sump pumps run times have not indicated an increase in leakage in the drywell since the sample was taken, and 3) conditions are such that activity can be calculated for the radionuclide concentration at the time of the release.

If there is any reason to suspect that gaseous radioactivity levels have changed in the drywell that would compromise the calculated, or estimated, radionuclide concentrations at the time of the release, since the last sample (30 hours), a new sample and analyses should be requested prior to starting a drywell purge to meet the intent of providing current analyses to reflect actual activity released to the environment. If a known steady state leakage condition exists in the drywell it is possible to calculate a safe and accurate release package. Final release quantification will be based on calculated radionuclide concentrations at the time of the actual release.

If the drywell is <u>purged</u> in accordance with the ODCM definition, both noble gas and tritium analyses must be completed before the purge begins. If the drywell is simply <u>vented</u> in accordance with the ODCM definition, no sample is required before venting.

## 12.4 GASEOUS EFFLUENTS 12.4.2 Dose - Noble Gases

Operability Requirements

12.4.2.A The air dose due to noble gases released in gaseous effluents, from each reactor unit, from the site shall be limited to the following:

- a. During any calendar quarter: Less than or equal to 5 mrad for gamma radiation and less than or equal to 10 mrad for beta radiation, and
- b. During any calendar year: Less than or equal to 10 mrad for gamma radiation and less than or equal to 20 mrad for beta radiation.

## Applicability: At all times.

Action:

a. With the calculated air dose from radioactive noble gases in gaseous effluents exceeding any of the above limits, prepare and submit to the Commission, pursuant to 10CFR50, Appendix I, Section IV.A, a report which identifies the cause(s) for exceeding the limit(s) and defines the corrective actions to be taken to reduce the releases and the proposed corrective actions to be taken to assure that subsequent releases will be in compliance with the above limits. This report is due to the NRC within 30 days from the end of the quarter in which the release occurred.

Surveillance Requirements

12.4.2.B

<u>Dose Calculations</u> - Cumulative dose contributions for the current calendar quarter and current calendar year shall be determined in accordance with the ODCM at least once per 31 days.

**Bases** 

12.4.2.C

This specification is provided to implement the requirements of Sections II.B, III.A and IV.A of Appendix I, 10 CFR Part 50. The Operability Requirements are the guides set forth in Section II.B of Appendix I. The ACTION statements provide the required operating flexibility and at the same time implement the guides set forth In Section IV.A of Appendix I to assure that the releases of radioactive material in gaseous effluents will be kept "as low as is reasonably achievable." The Surveillance Requirements implement the requirements in Section III.A of Appendix I that conformance with the guides of Appendix I be shown by calculational procedures based on models and data such that the actual exposure of an individual through appropriate pathways is unlikely to be substantially underestimated. The dose calculations established in the ODCM for calculating the doses due to the actual release rates of radioactive noble gases in gaseous effluents are consistent with the methodology provided in Regulatory Gulde 1.109, "Calculation of Annual Doses to Man from Routine Releases of Reactor Effluents for the Purpose of Evaluating Compliance with 10 CFR Part 50, Appendix I, "Revision 1, October 1977 and Regulatory Guide 1.111, "Methods for Estimating Atmospheric Transport and Dispersion of Gaseous Effluents in Routine Releases from Light-Water Cooled Reactors," Revision I, July 1977. The ODCM equations provided for determining the air doses at the site boundary are based upon the historical average atmospheric conditions.

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## 12.4 GASEOUS EFFLUENTS

12.4.3 Dose - Iodine-131, Iodine-133, Tritium, and Radionuclides in Particulate Form

Operability Requirements

- 12.4.3.A The dose to a MEMBER OF THE PUBLIC from lodine-131, lodine-133, tritium, and all radionuclides in particulate form with half-lives greater than 8 days in gaseous effluents released, from each reactor unit, to areas at and beyond the SITE BOUNDARY shall be limited to the following:
  - a. During any calendar quarter: Less than or equal to 7.5 mrems to any organ and,
  - b. During any calendar year: Less than or equal to 15 mrems to any organ.

Applicability: At all times.

## Action:

a. With the calculated dose from the release of iodine-131, iodine-133, tritium, and radionuclides in particulate form with half lives greater than 8 days, in gaseous effluents exceeding any of the above limits, prepare and submit to the Commission, pursuant to 10CFR50, Appendix I, Section IV.A, a report that Identifies the cause(s) for exceeding the limit and defines the corrective actions that have been taken to reduce the releases and the proposed correction actions to be taken to assure that subsequent releases will be in compliance with the above limits. This report is due to the NRC within 30 days from the end of the quarter in which the released occurred.

Surveillance Requirements

12.4.3.B Cumulative dose contributions for the current calendar quarter and current calendar year for iodine-131, iodine-133, tritium, and radionuclides in particulate form with half lives greater than 8 days shall be determined in accordance with the methodology and parameters in the ODCM at least once per 31 days.

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**Bases** 

12.4.3.C

The specification is provided to implement the requirements of Sections II.C, III.A and IV.A of Appendix I, 10 CFR Part 50. The Operability Requirements are the guides set forth In Section II.C of Appendix I. The ACTION statements provide the required operating flexibility and at the same time implement the guides set forth In Section IV.A of Appendix I to assure that the releases of radioactive materials in gaseous effluents will be kept "as low as is reasonably achievable." The ODCM calculational methods specified in the Surveillance Requirements implement the requirements in Section III.A of Appendix I that conformance with the guides of Appendix I be shown by calculational procedures based on models and data, such that the actual exposure of an individual through appropriate pathways is unlikely to be substantially underestimated. The ODCM calculational methods for calculating the doses due to the actual release rates of the subject materials are consistent with the methodology provided in Regulatory Guide 1.109, "Calculation of Annual Doses to Man from Routine Releases of Reactor Effluents for the Purpose of Evaluating Compliance with 10 CFR Part 50, Appendix I, "Revision 1, October 1977 and Regulatory Guide 1.111, "Methods for Estimating Atmospheric Transport and Dispersion of Gaseous Effluents in Routine Releases from Light-Water-Cooled Reactors," Revision 1, July 1977. These equations also provide for determining the actual doses based upon the historical average atmospheric conditions. The release rate specifications for radiolodines, radioactive materials in particulate form and radionuclides other than noble gases are dependent on the existing radionuclide pathways to man, in the unrestricted area. The pathways which were examined in the development of these calculations were: 1) individual inhalation of airborne radionuclides, 2) deposition of radionuclides onto green leafy vegetation with subsequent consumption by man, 3) deposition onto grassy areas where milk animals and meat producing animals graze with consumption of the milk and meat by man, and 4) deposition on the ground with subsequent exposure of man.

#### **GASEOUS EFFLUENTS** 12.4

Gaseous Radwaste Treatment System 12.4.4

Operability Requirements

The GASEOUS RADWASTE (OFF-GAS) TREATMENT SYSTEM shall be in 12.4.4.A operation.

> Whenever the main condenser air ejector system is in operation. Applicability:

### Action:

- With the GASEOUS RADWASTE (OFF-GAS) TREATMENT SYSTEM a. inoperable for more than 7 days, prepare and submit to the Commission within 30 days, a Special Report which includes the following information:
  - Identification of the inoperable equipment or subsystems and the 1. reason for inoperability.
  - Action(s) taken to restore the inoperable equipment to 2. OPERABLE status, and
  - Summary description of action(s) taken to prevent a recurrence. 3.

Surveillance Requirements

The GASEOUS RADWASTE TREATMENT SYSTEM shall be verified to be in 12.4.4.B operation at least once per 7 days.

**Bases** 

The OPERABILITY of the GASEOUS RADWASTE TREATMENT SYSTEM and 12.4.4.C the VENTILATION EXHAUST TREATMENT SYSTEM ensures that the system will be available for use whenever gaseous effluents require treatment prior to release to the environment. The requirement that the appropriate portions of these systems be used, when specified, provides reasonable assurance that the releases of radioactive materials in gaseous effluents will be kept "as low as is reasonably achievable". This specification implements the requirements of 10 CFR Part 50.36a, General Design Criterion 60 of Appendix A to 10 CFR Part 50, and the design objectives given in Section II,0 of Appendix I to 10 CFR Part 50. The specified limits governing the use of appropriate portions of the systems were specified as a sultable fraction of the dose design objectives set forth in Sections II.B and II.C of Appendix I, 10 CFR Part 50, for gaseous effluents.

#### 12.4 **GASEOUS EFFLUENTS**

12.4.5.A

#### **Ventilation Exhaust Treatment System** 12.4.5

Operability Requirements

The appropriate portions of the VENTILATION EXHAUST TREATMENT SYSTEM shall be OPERABLE and be used to reduce radioactive materials in gaseous waste prior to their discharge when the projected doses due to gaseous effluent releases from each reactor unit, from the site, when averaged over 31 days, would exceed 0.3 mrem to any organ.

At all times. Applicability:

Action:

With the VENTILATION EXHAUST TREATMENT SYSTEM inoperable for more than 31 days, and with gaseous waste being discharged without treatment and in excess of the above limits, prepare and submit to the Commission within 30 days, a Special Report which includes the following information:

- Identification of the Inoperable equipment or subsystems and the reason 1. for inoperability.
- Action(s) taken to restore the inoperable equipment to OPERABLE 2. status, and
- Summary description of action(s) taken to prevent a recurrence. 3.

Surveillance Requirements

- Doses due to gaseous releases from the site shall be projected at least once per 12.4.5.B.1 31 days in accordance with the ODCM.
- The VENTILATION EXHAUST TREATMENT SYSTEM shall be demonstrated 12.4.5.B.2 OPERABLE by operating the VENTILATION EXHAUST TREATMENT SYSTEM equipment for at least 30 minutes, at least once per 92 days unless the appropriate system has been utilized to process radioactive gaseous effluents during the previous 92 days.

Bases

The OPERABILITY of the GASEOUS RADWASTE TREATMENT SYSTEM and 12.4.5.C the VENTILATION EXHAUST TREATMENT SYSTEM ensures that the system will be available for use whenever gaseous effluents require treatment prior to release to the environment. The requirement that the appropriate portions of these systems be used, when specified, provides reasonable assurance that the releases of radioactive materials in gaseous effluents will be kept "as low as is reasonably achievable\*. This specification implements the requirements of 10 CFR Part 50.36a, General Design Criterion 60 of Appendix A to 10 CFR Part 50, and the design objectives given in Section II,0 of Appendix I to 10 CFR Part 50. The specified limits governing the use of appropriate portions of the systems were specified as a suitable fraction of the dose design objectives set forth in Sections II.B and II.C of Appendix I, 10 CFR Part 50, for gaseous effluents.

## 12.4 GASEOUS EFFLUENTS

## 12.4.6 Venting or Purging

Operability Requirements

12.4.6.A VENTING or PURGING of the containment drywell shall be through the Primary Containment Vent and Purge System or the Standby Gas Treatment System.

Applicability: Whenever the drywell is vented or purged.

### Action:

a. With the requirements of the above specification not satisfied, suspend all VENTING and PURGING of the drywell.

## Surveillance Requirements

- 12.4.6.B.1 The containment drywell shall be determined to be aligned for VENTING or PURGING through the Primary Containment Vent and Purge System or the Standby Gas Treatment System within 4 hours prior to start of and at least once per 12 hours during VENTING or PURGING of the drywell.
- 12.4.6.B.2 Prior to use of the Purge System through the Standby Gas Treatment System in MODE 1, 2 or 3 assure that:
  - a. Both Standby Gas Treatment System trains are OPERABLE, and
  - b. Only one of the Standby Gas Treatment System trains is used for PURGING.

## **Bases**

12.4.6.C This specification provides reasonable assurance that releases from drywell purging operations will not exceed the annual dose limits of 10CFR20 for unrestricted areas.

## 12.4 GASEOUS EFFLUENTS

## 12.4.7 Total Dose

**Operability Requirements** 

The dose or dose commitment to any member of the public, due to releases of radioactivity and radiation, from uranium fuel cycle sources shall be limited to less than or equal to 25 mrem to the total body or any organ (except the thyroid, which shall be limited to less or equal to 75 mrem) over 12 consecutive months.

Applicability: At all times.

## Action:

With the calculated doses from the release of radioactive materials in liquid or gaseous effluents exceeding twice the limits of Sections 12.3.2.A.a, 12.3.2.A.b, 12.4.2.A.a. 12.4.2.A.b. 12.4.3.A.a or 12.4.3.A.b, prepare and submit a Special Report to the Director, Nuclear Reactor Regulation, U.S. Nuclear Regulatory Commission, Washington, D.C. 20555, within 30 days, which defines the corrective action to be taken to reduce subsequent releases to prevent recurrence of exceeding the limits of Section 12.4.7.A. This Special Report shall include an analysis which estimates the radiation exposure (dose) to a member of the public from uranium fuel cycle sources (including all effluents pathways and direct radiation) for a 12 consecutive month period that includes the release(s) covered by this report. If the estimated dose(s) exceeds the limits of Section 12.4.7.A. and if the release condition resulting in violation of 40 CFR 190 has not already been corrected, the Special Report shall include a request for a variance In accordance with the provisions of 40 CFR 190 and including the specified information of 40 CFR 190.11. Submittal of the report is considered a timely request, and a variance is granted until staff action on the request is complete. The variance only relates to the limits of 40 CFR 190, and does not apply in any way to the requirements for dose limitation of 10 CFR Part 20, as addressed in other sections of this technical specification.

## Surveillance Requirements

12.4.7.B <u>Dose Calculations</u> - Cumulative dose contributions from direct radiation and liquid and gaseous effluents shall be determined in accordance with Sections 12.3.2.B, 12.4.2.B and 12.4.3.B, and in accordance with the ODCM.

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**Bases** 

12.4.7.C

This specification is provided to meet the dose limitations of 40 CFR 190. The specification requires the preparation and submittal of a Special Report whenever the calculated doses from plant radioactive effluents exceed twice the design objective doses of Appendix I. For sites containing up to 4 reactors, it is highly unlikely that the resultant dose to a member of the public will exceed the dose limits of 40 CFR 190 if the individual reactors remain within the reporting requirement level. The Special Report will describe a course of action which should result in the limitation of dose to a member of the public for 12 consecutive months to within the 40 CFR 190 limits. For the purpose of the Special Report, it may be assumed that the dose commitment to the member of the public from other uranium fuel cycle sources is negligible, with the exception that dose contributions from other nuclear fuel cycle facilities at the same site or within a radius of 5 miles must be considered. If the dose to any member of the public is estimated to exceed the requirements of 40 CFR 190, the Special Report with a request for a variance (provided the release conditions resulting in violation of 40 CFR 190 have not already been corrected), in accordance with the provisions of 40 CFR 190.11, is considered to be a timely request and fulfills the requirements of 40 CFR 190 until NRC staff action is completed. An individual is not considered a member of the public during any period in which he/she is engaged in carrying out any operation which is part of the nuclear fuel cycle.

## 12.4 GASEOUS EFFLUENTS

### 12.4.8 Main Condenser

**Operability Requirements** 

12.4.8.A The release rate of the sum of the activities from the noble gases measured prior to the holdup line shall be limited to less than or equal to 3.4 x 10<sup>5</sup> microcuries/second after decay of 30 minutes.

Applicability:

MODE 1. MODES 2 and 3 with any main steam line not isolated

and steam jet air ejectors (SJAE) not in operation.

## Action:

With the release rate of the sum of the activities from the noble gases prior to the holdup line exceeding  $3.4 \times 10^5$  microcuries/second after decay of 30 minutes, restore the release rate to within its limit within 72 hours or either isolate all main steam lines or isolate the SJAEs in the next 12 hours, or be in MODE 3 in the next 12 hours and MODE 4 in the next 24 hours.

Surveillance Requirements

- 12.4.8.B.1 The radioactivity rate of noble gases prior to the holdup line shall be continuously monitored in accordance with the ODCM and Table 12.2.2-2.
- 12.4.8.B.2

  \*The release rate of the sum of the activities from noble gases prior to the holdup line shall be determined to be within the limits of specification 12.4.8.A at the following frequencies by performing an isotopic analysis of a representative sample of gases taken prior to the holdup line.
  - At least once per 31 days.
  - b. Within 4 hours following an increase, as indicated by the off gas pretreatment Noble Gas Activity Monitor, of greater than 50%, after factoring out increases due to changes in THERMAL POWER level, in the nominal steady state fission gas release from the primary coolant.
- \* Not required to be performed until 31 days after any main steam line not isolated and SJAE not in operation.

**Bases** 

12.4.8.C In accordance with surveillance requirements contained within ODCM Chapter 12 Item number 12.4.8.B.1 and 2, this specification provides reasonable assurance that the releases from the main condenser will not exceed the requirements of the LaSalle Technical Specifications 3.7.6. In addition, a sample is required within 4 hours if the increase is not due to thermal power changes. If the cause is known and not fuel related and less than 1 hour in duration, then no sample is required. [This is based on interpretation letter from W. R. Huntington to Operating Engineers, Shift Engineers and F.R. Lawless, dated May 24, 1984.]

## 12.4.9 Dose Limits for Members of the Public

Operability Requirements

The licensee shall conduct operations such that the TEDE to individual MEMBERS OF THE PUBLIC does not exceed 100 mrem in a year. In addition, the dose in any unrestricted area from external sources does not exceed 2 mrem in any one hour. The Effluents Program shall implement monitoring, sampling, and analysis of radioactive liquid and gaseous effluents in accordance with 10CFR20.1302 and with the methodology and parameters in the ODCM.

Applicability: At all times.

## Action:

- 1. If the calculated dose from the release or exposure of radiation meets or exceeds the 100 mrem/year limit for the MEMBER OF THE PUBLIC, prepare and submit a report to the Commission in accordance with 10CFR20.2203.
- If the dose in any unrestricted area from external sources of radiation meets or exceeds the 2 mrem in any one hour limit for the MEMBER OF THE PUBLIC, prepare and submit a report to the Commission in accordance with 10CFR20,2203.

Surveillance Requirements

12.4.9.B Calculate the TEDE to individual MEMBERS OF THE PUBLIC annually to determine compliance with the 100 mrem/year limit in accordance with the ODCM. In addition, evaluate and/or determine if direct radiation exposures exceed 2 mrem in any hour in unrestricted areas.

**Bases** 

This section applies to direct exposure of radioactive materials as well as radioactive materials released in gaseous and liquid effluents. 10CFR20.1301 sets forth the 100 mrem/year dose limit to members of the public; 2 mrem in any one hour limit in the unrestricted area; and reiterates that the licensee is also required to meet the 40CFR190 standards. 10CFR20.1302 provides options to determine compliance to 10CFR20.1301. Compliance to the above operability requirement is based on 10CFR20, 40CFR190 and LaSalle Station Technical Specification 5.5.4.g.

## 12.5 RADIOLOGICAL ENVIRONMENTAL MONITORING PROGRAM

12.5.1 Monitoring Program

**Operability Requirements** 

12.5.1.A The Radiological Environmental Monitoring Program shall be conducted as specified in Table 12.5-1.

Applicability: At all times.

### Action:

With the Radiological Environmental Monitoring Program not being conducted as specified in Table 12.5-1, prepare and submit to the Commission, in the Annual Radiological Environmental Operating Report required by Technical Specification 5.6.2, a description of the reasons for not conducting the program as required and the plans for preventing a recurrence.

Deviations are permitted from the required sampling schedule if specimens are unobtainable due to hazardous conditions, seasonal unavailability, malfunction of sampling equipment, if a person/business who participates in this program goes out of business or no longer can provide sample, or contractor omission which is corrected as soon as discovered. If the equipment malfunctions, corrective actions shall be completed as soon as practical. If a person/business supplying samples goes out of business, a replacement supplier shall be found as soon as possible. All deviations from the sampling schedule shall be described in the Annual Radiological Environmental Operating Report.

2. With the level of radioactivity as the result of plant effluents in an environmental sampling medium at a specified location exceeding the reporting levels of Table 12.5-2 when averaged over any calendar quarter, prepare and submit to the Commission within 30 days, a Special Report that identifies the cause(s) for exceeding the limit(s) and defines the corrective actions to be taken to reduce radioactive effluents so that the potential annual dose\* to a MEMBER OF THE PUBLIC is less than the calendar year limits of Section 12.3.2, 12.4.2, or 12.4.3. When more than one of the radionuclides in Table 12.5.2 are detected in the sampling medium, this report shall be submitted if:

<u>concentration (1)</u> + <u>concentration (2)</u> ≥ 1.0 reporting level (1) reporting level (2)

When radionuclides other than those in Table 12.5-2 are detected and are the result of plant effluents, this report shall be submitted if the potential annual dose\* to A MEMBER OF THE PUBLIC from all radionuclides is equal to or greater than the calendar year limits of Section 12.3.2, 12.4.2, or 12.4.3. This report is not required if the measured level of radioactivity was not the result of plant effluents; however, in such an event, the condition shall be reported and described in the Annual Radiological Environmental Operating Report required by Section 12.6.1.

<sup>\*</sup>The methodology and parameters used to estimate the potential annual dose to a MEMBER OF THE PUBLIC shall be indicated in this report.

## 12.5 RADIOLOGICAL ENVIRONMENTAL MONITORING PROGRAM (Continued)

3. If the sample type or sampling location(s) as required by Table 12.5-1 become(s) permanently unavailable, identify suitable alternative sampling media for the pathway of interest and/or specific sampling locations for obtaining replacement samples and add them to the Radiological Environmental Monitoring Program as soon as practicable. The specific locations from which samples were unavailable may then be deleted from the monitoring program.

Prepare and submit controlled version of the ODCM within 180 days including a revised figure(s) and table reflecting the new location(s) with supporting information identifying the cause of the unavailability of samples and justifying the selection of new location(s) for obtaining samples.

## Surveillance Requirements

12.5.1.B The radiological environmental monitoring program samples shall be collected pursuant to Table 12.5-1 from the specific locations given in the table and figure(s) in the ODCM, and shall be analyzed pursuant to the requirements of Table 12.5-1 and the detection capabilities required by Table 12.5-3.

#### Bases

The Radiological Environmental Monitoring Program required by this section provides representative measurements of radiation and of radioactive materials in those exposure pathways and for those radionuclides that lead to the highest potential radiation exposures of MEMBERS OF THE PUBLIC resulting from the station operation. This monitoring program implements Section IV.B.2 of Appendix I to 10 CFR Part 50 and thereby supplements the radiological effluent monitoring program by verifying that the measurable concentrations of radioactive materials and levels of radiation are not higher than expected on the basis of the effluent measurements and the modeling of the environmental exposure pathways. Guidance for this monitoring program is provided by the Radiological Assessment Branch Technical Position on Environmental Monitoring. The initially specified monitoring program will be effective for at least the first 3 years of commercial operation. Following this period, program changes may be initiated based on operational experience.

The required detection capabilities for environmental sample analyses are tabulated in terms of the lower limits of detection (LLDs). The LLDs required by Table 12.5-3 are considered optimum for routine environmental measurements in industrial laboratories. It should be recognized that the LLD is defined as a before the fact limit representing the capability of a measurement system and not as an after the fact limit for a particular measurement.

Detailed discussion of the LLD, and other detection limits, can be found in HASL Procedures Manual, <u>HASL-300</u> (revised annually), Currie, LA., "Limits for Qualitative Detection and Quantitative Determination - Application to Radiochemistry," <u>Anal. Chem. 40</u>, 586-93 (1968), and Hartwell, J.K., "Detection Limits for Radioanalytical Counting Techniques," Atlantic Richfield Hanford Company Report <u>ARH-SA-215</u> (June 1975).

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12.5 RADIOLOGICAL ENVIRONMENTAL MONITORING PROGRAM (Continued)

Interpretations	

12.5.1.D Table 12.5-1 requires "one sample of each community drinking water supply downstream of the plant within 10 kilometers." Drinking water supply is defined as water taken from rivers, lakes, or reservoirs (not well water) which is used for drinking.

## TABLE 12.5-1 RADIOLOGICAL ENVIRONMENTAL MONITORING PROGRAM

EXPOSURE PATHWAY AND/OR SAMPLE	NUMBER OF REPRESENTATIVE SAMPLES AND SAMPLE LOCATIONS <sup>(1)</sup>	SAMPLING AND COLLECTION FREQUENCY	TYPE AND FREQUENCY OF ANALYSIS		
Airborne Radiolodine and Particulates	Samples from a total of eight locations:  a. Indicator- Near Field  Four samples from locations within 4 km (2.5 mi) in different sectors.  b. Indicator- Far Field  Three additional locations within 4 to 10 km (2.5 to 6.2 mi) in different sectors.  c. Control  One sample from a control location within 10 to 30 km (6.2 to 18.6 mi).	Continuous sampler operation with particulate sample collection weekly (or more frequently if required due to dust loading) and radiolodine canister collection biweekly.	Radioiodine Canister: I-131 analysis biweekly on near field and control samples. (2)  Particulate Sampler: Gross beta analysis following weekly filter change (3) and gamma isotopic analysis (4) quarterly on composite filters by location on near field and control (2) samples.		





TABLE 12.5-1 (Continued)
RADIOLOGICAL ENVIRONMENTAL MONITORING PROGRAM

EXPOSURE PATHWAY AND/OR SAMPLE	NUMBER OF REPRESENTATIVE SAMPLES AND SAMPLE LOCATIONS <sup>(1)</sup>	SAMPLING AND COLLECTION FREQUENCY	TYPE AND FREQUENCY OF ANALYSIS
2. Direct Radiation <sup>(5)</sup>	Forty routine monitoring stations either with a thermoluminescent dosimeter (TLD) or with one instrument for measuring dose rate continuously, placed as follows:	Quarterly	Gamma dose on each TLD quarterly.
	a. Indicator-Inner Ring (100 Series TLD)		
	One in each meteorological sector, in the general area of the SITE BOUNDARY (within 0.1 to 2.0 ml; 0.2 to 3.2 km)		
	b. Indicator- Outer Ring (200 Series TLD) One in each meteorological sector, within 4.8 to 10 km (3 to 6.2 mi); and		
	c. Other One at each Airborne location given in part 1.a. and 1.b. The balance of the TLDs to be placed at special interest locations beyond the Restricted Area where either a MEMBER OF THE PUBLIC or Commonwealth Edison employees have routine access. (300 Series TLD)		





### TABLE 12.5-1 (Continued)

### RADIOLOGICAL ENVIRONMENTAL MONITORING PROGRAM

E	XPOSURE PATHWAY AND/OR SAMPLE	NUMBER OF REPRESENTA SAMPLES AND SAMPLE LOCA		TYPE AND FREQUENCY OF ANALYSIS
2.	Direct Radiation <sup>(5)</sup> (Cont'd)	Control One at each Airborne control given in part 1.c	location Quarterly	Gamma dose on each TLD quarterly.
3.	Waterborne a. Ground/Well	Indicator  Samples from two sources of to be affected. (6)	Quarterly nly if likely	Gamma isotopic <sup>(4)</sup> and tritium analysis quarterly.
	b. Drinking <sup>(7)</sup>	Indicator  One Sample from each components of the Components of the Station discharge.  Indicator  One Sample from each components of the Components of the	ruid be arge within	Gross beta and gamma isotopic analyses <sup>(4)</sup> on monthly composite; tritium analysis on quarterly Composite. I-131 analysis on each composite when the dose calculated for the consumption of water is greater than 1 mrem per year.
	c. Surface Water <sup>(7)</sup>	if no community water supply Water) exists within 10 km do of discharge then surface wa sampling shall be performed.	ownstream ter	Gross beta and gamma isotopic analyses <sup>(4)</sup> on monthly composite; tritium analysis on quarterly composite.
		Indicator One sample downstream		



## TABLE 12.5-1 (Continued) RADIOLOGICAL ENVIRONMENTAL MONITORING PROGRAM

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EXPOSURE PA AND/ OR SA		NUMBER OF REPRESENTATIVE SAMPLES AND SAMPLE LOCATIONS(1)	SAMPLING AND COLLECTION FREQUENCY	TYPE AND FREQUENCY OF ANALYSIS
d. Control Sar	mple <sup>(7)</sup> a	One surface sample upstream discharge.	Weekly grab samples.	Gross beta and gamma isotopic analyses <sup>(4)</sup> on monthly composite; tritium analysis on quarterly composite.
e. Sediment	8	At least one sample from downstream <sup>(7)</sup> area within 10 km (6.2 mi).	Semiannually.	Gamma isotopic analysis <sup>(4)</sup> semiannually.
4. Ingestion a. Milk <sup>(6)</sup>		Samples from milking animals from a maximum of three locations within 10 km (6.2 ml) distance.  Control  One sample from milking animals at a control location within 10 to 30 km (6.2 to 18.6 ml).	Biweekly <sup>(9)</sup> when animals are on pasture (May through October), monthly at other times (November through April).	Gamma isotopic <sup>(4)</sup> and 1-131 <sup>(10)</sup> analysis on each sample.

TABLE 12.5-1 (Continued)
RADIOLOGICAL ENVIRONMENTAL MONITORING PROGRAM

E	XPOSURE PATHWAY		NUMBER OF REPRESENTATIVE	SAMPLING AND	TYPE AND FREQUENCY OF ANALYSIS
	AND/OR SAMPLE	SA	MPLES AND SAMPLE LOCATIONS <sup>(1)</sup>	COLLECTION FREQUENCY	ANALISIS
b.	Fish	a.	Indicator	Two times annually.	Gamma isotopic analysis <sup>(4)</sup> on edible portions
			Representative samples of commercially and recreationally important species in discharge area.		
			Representative samples from the LaSalle Lake.		
		b.	Control Representative samples of commercially and recreationally important species in control locations upstream of discharge.	•	Gamma isotopic <sup>(4)</sup> and I-131
c.	Food Products	a.	Indicator	Annually	Analysis on each Sample.
			Two representative samples from the principal food pathways grown in each of four major quadrants within 10 km (6.2 mi), if available:		Campio
			At least one root vegetable sample(11)		
			At least one broad leaf vegetable (or vegetation) <sup>(11)</sup>		
	•	b.	Control		
			Two representative samples similar to indicator samples grown within 15 to 30 km (9.3 to 18.6 ml), if available.		-

# TABLE 12.5-1 (Continued) RADIOLOGICAL ENVIRONMENTAL MONITORING PROGRAM TABLE NOTATIONS

- (1) Specific parameters of distance and direction from the centerline of the midpoint of the two units and additional description where pertinent shall be provided for each and every sample location in Table 12.5-1, except for vegetation. For vegetation, due to location variability year to year, the parameters of distance and direction shall be provided in the Annual Environmental Operating Report.
- (2) Far field samples are analyzed when the respective near field sample results are inconsistent with previous measurements and radioactivity is confirmed as having its origin in airborne effluents from the station, or at the discretion of the Radiation Support Director.
- (3) Airborne particulate sample filters shall be analyzed for gross beta radioactivity 24 hours or more after sampling to allow for radon and thoron daughter decay. If gross beta activity in air particulate samples is greater than 10 times the yearly mean of control samples, gamma isotopic analysis shall be performed on the individual samples.
- (4) Gamma isotopic analysis means the identification and quantification of gamma emitting radionuclides that may be attributable to the effluents from the station.
- One or more instruments, such as a pressurized ion chamber, for measuring and recording dose rate continuously may be used in place of, or in addition to, integrating dosimeters. Film badges shall not be used as dosimeters for measuring direct radiation. The 40 locations is not an absolute number. The number of direct radiation monitoring stations may be reduced according to geographical limitations; e.g., If a station is adjacent to a lake, some sectors may be over water thereby reducing the number of dosimeters which could be placed at the indicated distances. The frequency of analysis or readout for TLD systems will depend upon the characteristics of the specific system used and should be selected to obtain optimum dose information with minimal fading.
- (6) Groundwater samples shall be taken when this source is tapped for drinking or irrigation purposes in areas where the hydraulic gradient or recharge properties are suitable for contamination.
- (7) The "downstream" sample shall be taken in an area beyond but near the mixing zone. The "upstream sample" shall be taken at a distance beyond significant influence of the discharge. Upstream samples in an estuary must be taken far enough upstream to be beyond the station influence.
- (8) If milking animals are not found in the designated indicator locations, or if the owners decline to participate in the REMP, all milk sampling may be discontinued.
- (9) Biweekly refers to every two weeks.
- (10) I-131 analysis means the analytical separation and counting procedure are specific for this radionuclide.
- (11) One sample shall consist of a volume/weight of sample large enough to fill contractor specified container.

**TABLE 12.5-2** 

## REPORTING LEVELS FOR RADIOACTIVITY CONCENTRATIONS IN ENVIRONMENTAL SAMPLES REPORTING LEVELS

	WATER	AIRBORNE PARTICULATE	FISH	MILK	FOOD PRODUCTS
ANALYSIS	(pCi/l)	OR GASES (pCi/m3)	(pCi/kg, wet)	(pCi/l) (pCi/kg, wet)	
H-3 20,000 <sup>(1)</sup>					•
Mn-54	1,000		30,000		•
Fe-59	400		10,000	-	
Co-58	1,000		30,000	•	
Co-60	300		10,000		
Zn-65	300		20,000	•	
Zr-Nb-95	400				
I-131	2 <sup>(2)</sup>	0.9		3	100
Cs-134	30	10	1,000	60	1,000
Cs-137	50	20	2,000	<b>70</b> .	2,000
Ba-La-140	200			300	

<sup>(1)</sup> For drinking water samples. This is 40 CFR Part 141 value. If no drinking water pathway exists, a value of 30,000 pCI/I may be used.

<sup>(2)</sup> If no drinking water pathway exists, a value of 20 pCi/l may be used.



TABLE 12.5-3

DETECTION CAPABILITIES FOR ENVIRONMENTAL SAMPLE ANALYSIS

LOWER LIMIT OF DETECTION (LLD)<sup>(2)(3)</sup>

ANALYSIS	WATER (pCi/l)	AIRBORNE PARTICULATE OR GASES (pCl/m³)	FISH (pCl/kg, wet)	MILK (pCI/I)	FOOD PRODUCTS (pCi/kg, wet)	SEDIMENT (pCI/kg, dry)
Gross Beta	4	0.01	1000			
н-3	2,000 <sup>(7)</sup>					
Mn-54	15		130			
Fe-59	30		260		•	
Co-58,60	15		130			
Zn-65	30		260			
Zr-Nb-95	15					
I-131 <sup>(0)</sup>	1/15 <sup>(4)</sup>	0.07	100	0.5/5 <sup>(5)</sup>	60	
Cs-134	15	0.01	100	15	60	150
Cs-137	18	0.01	100	18	80	. 180
Ba-La-140	15			15		

# TABLE 12.5-3 (Continued) DETECTION CAPABILITIES FOR ENVIRONMENTAL SAMPLE ANALYSIS TABLE NOTATIONS

- (1) The nuclides on this list are not the only nuclides intended to be considered. Other peaks that are identifiable, together with those of the above nuclides, shall also be analyzed and reported in the Annual Radiological Environmental Operating Report.
- (2) Required detection capabilities for thermoluminescent dosimeters used for environmental measurements shall be in accordance with the recommendations of Regulatory Guide 4.13.
- (3) The Lower Limit of Detection (LLD) is defined, for purposes of these specifications, as the smallest concentration of radioactive material in a sample that will yield a net count, above system background, that will be detected with 95% probability with only 5% probability of falsely concluding that a blank observation represents a "real" signal.

For a particular measurement system, which may include radiochemical separation, the LLD is defined as follows:

LLD = 
$$\frac{4.66 \text{ Sb} + 3/\text{tb}}{(\text{E) (V) (2.22) (Y) (exp (-  $\lambda\Delta t$ ))}}$$

LLD  $\frac{4.66 \text{ Sb}}{(\text{E) (V) (2.22) (Y) (exp (- $\lambda\Delta t$ ))}}$ 

Where: 4.66 Sb >> 3/tb

- LLD = the "a priori" Minimum Detectable Concentration (picoCuries per unit mass or volume),
- sb = the standard deviation of the background counting rate or of the counting rate of a blank sample, as appropriate (counts per minute),

E = the counting efficiency(counts per disintegration),

V = the sample size (units of mass or volume),

2.22 = the number of disintegrations per minute per picoCurie,

Y = the fractional radiochemical yield, when applicable,

the radioactive decay constant for the particular radionuclide
 (sec-1),

# TABLE 12.5-3 (Continued) DETECTION CAPABILITI ES FOR ENVIRONMENTAL SAMPLE ANALYSIS TABLE NOTATIONS

tb = counting time of the background or blank (minutes), and

 $\Delta t$  = the elapsed time between sample collection, or end of the sample collection period, and the time of counting (sec).

Typical values of E, V, Y, and  $\Delta t$  should be used in the calculation.

It should be recognized that the LLD is defined as a before the fact limit representing the capability of a measurement system and not as an after the fact limit for a particular measurement.

Analyses shall be performed in such a manner that the stated LLDs will be achieved under routine conditions. Occasionally, background fluctuations, unavoidable small sample sizes, the presence of interfering nuclides, or other uncontrollable circumstances may render these LLDs unachievable. In such cases, the contributing factors shall be identified and described in the Annual Radiological Environmental Operating Report.

- 14) If no drinking water pathway exists, the value of 15 pCi/l may be used.
- (5) A value of 0.5 pCi/l shall be used when the animals are on pasture (May through October) and a value of 5 pCi/l shall be used at all other times (November through April).
- (6) This LLD applies only when the analytical separation and counting procedure are specific for this radionuclide.
- (7) This LLD is the minimum allowable, however, vendors performing environmental sample analyses off-site will be required to meet an LLD of 200 pCi/l.

### 12.5.2 Land Use Census

Operability Requirements
--------------------------

12.5.2.A. A Land Use Census shall be conducted and shall identify within a distance of 10 km (6.2 miles) the location in each of the 16 meteorological sectors\* of the nearest milk animal, the nearest residence\*\*, and an enumeration of livestock. For dose calculation, a garden will be assumed at the nearest residence.

Applicability: At all times.

#### Action:

With a Land Use Census identifying a location(s) that yields a calculated dose or dose commitment, via the same exposure pathway 20% greater than at a location from which samples are currently being obtained in accordance with Section 12.5.1, add the new location(s) within 30 days to the Radiological Environmenta! Monitoring Program given in Chapter 11. The sampling location(s), excluding the control location, having the lowest calculated dose or dose commitment(s), via the same exposure pathway, may be deleted from this monitoring program after October 31 of the year in which this Land Use Census was conducted. Submit in the next Annual Radiological Environmental Operating Report documentation for a change in the ODCM Including a revised figure(s) and table(s) for the ODCM reflecting the new location(s) with information supporting the change in sampling locations.

\*This requirement may be reduced according to geographical limitations; e.g. at a lake site where some sector's will be over water.

\*\*The nearest industrial facility shall also be documented if closer than the nearest residence.

### Surveillance Requirements

12.5.2.B The Land Use Census shall be conducted during the growing season, between June 1 and October 1, at least once per 12 months using that information that will provide the best results, such as by a door-to-door survey, aerial survey, or by consulting local agriculture authorities. The results of the Land Use Census shall be included in the Annual Radiological Environmental Operating Report.

### <u>Bases</u>

12.5.2.C This specification is provided to ensure that changes in the use of areas at and beyond the SITE BOUNDARY are identified and that modifications to the Radiological Environmental Monitoring Program given in the ODCM are made if required by the results of this census. This census satisfies the requirements of Section IV.B.3 of Appendix I to 10 CFR Part 50. An annual garden census will not be required since the licensee will assume that there is a garden at the nearest residence in each sector for dose calculations.

12.5.3		International Comparison Program
Operabil	ity R	equirements
12.5.3.A		Analyses shall be performed on radioactive materials supplied as part of an Interlaboratory Comparison Program that correspond to samples required by Table 12.5-1.
		Applicability: At all times.
		Action:
	1.	With analyses not being performed as required above, report the corrective actions taken to prevent a recurrence to the Commission in the Annual Radiological Environmental Operating Report.
Surveilla	nce	Requirements
12.5.3.B	ļ	A summary of the results obtained as part of the above required Interlaboratory Comparisor Program shall be included in the Annual Radiological Environmental Operating Report.
Bases		
12.5.3.C	<b>;</b>	The requirement for participation in an Interlaboratory Comparison Program is provided to ensure that independent checks on the precision and accuracy of the measurements of radioactive material in environmental samples matrices are performed as part of the quality assurance program for environmental monitoring in order to demonstrate that the results are valid for the purposes of Section IV.B.2 of Appendix I to 10 CFR Part 50.

### 12.6 REPORTING REQUIREMENTS

### 12.6.1 Annual Radiological Environmental Operating Report\*

Routine Annual Radiological Environmental Operating Report covering the operation of the Units during the previous calendar year shall be submitted by May 15 of each year. The report shall include summaries, interpretations, and an analysis of trends of the results of the radiological environmental monitoring program for the report period. The material provided shall be consistent with the objectives outlined in the Offsite Dose Calculation Manual, and in 10CFR50, Appendix I, Sections IV.B.2, IV.B.3, and IV.c. It should include, as found appropriate, a comparison of preoperational studies with operational controls or with previous environmental surveillance reports, and an assessment of the observed impacts of the plant operation on the environment.

The Annual Radiological Environmental Operating Report shall include the results of all radiological environmental samples and of all environmental radiation measurements taken during the period pursuant to the locations specified in the tables and figures in Chapter 11 of the ODCM, as well as summarized and tabulated results of these analyses and measurements in the format of the table in the Radiological Assessment Branch Technical Position, Revision 1, November 1979. In the event that some individual results are not available for inclusion with the report, the report shall be submitted noting and explaining the reasons for the missing results. The missing data shall be submitted as soon as possible in a supplementary report.

The reports shall also include the following: a summary description of the Radiological Environmental Monitoring Program; legible maps covering all sampling locations keyed to a table giving distances and directions from the midpoint between the two units; reasons for not conducting the Radiological Environmental Monitoring Program as required by Section 12.5.1, and discussion of all deviations from the sampling schedule of Table 12.5-1; a Table of Missed Samples and a Table of Sample Anomalies for all deviations from the sampling schedule of Table 11.1-1; discussion of environmental sample measurements that exceed the reporting levels of Table 12.5-2 but are not the result of plant effluents; discussion of all analyses in which the LLD required by Table 12.5-3 was not achievable; results of the Land Use Census required by Section 12.5.2; and the results of licensee participation in an Interlaboratory Comparison Program and the corrective actions being taken if the specified program is not being performed as required by Section 12.5.3.

The Annual Radiological Environmental Operating Report shall also include an annual summary of hourly meteorological data collected over the previous year. This annual summary may be either in the form of an hour-by-hour listing on magnetic tape of wind speed, wind direction, atmospheric stability, and precipitation (if measured), or in the form of joint frequency distributions of wind speed, wind direction, and atmospheric stability. In lieu of submission with the Annual Radiological Environmental Operating Report, the licensee has the option of retaining the summary of required meteorological data on site in a file that shall be provided to the NRC upon request.

\*A single submittal may be made for a multiple unit station. The submittal should combine sections common to all units at the station.

### 12.6.1 Annual Radiological Environmental Operating Report (Continued)

The Annual Radiological Environmental Operating Report shall also include an assessment of the radiation doses due to the radioactive liquid and gaseous effluents released from the unit or station during the previous calendar year. This report shall also include an assessment of radiation doses to the most likely exposed MEMBER OF THE PUBLIC from reactor releases and other nearby uranium fuel cycle sources, including doses from primary effluent pathways and direct radiation, for the previous calendar year. The assessment of radiation doses shall be performed in accordance with the methodology and parameters in the ODCM and in compliance with 10CFR20 and 40 CFR 190, "Environmental Radiation Protection Standards for Nuclear Power Operation."

### 12.6.2 Radioactive Effluent Release Report4

- a. The radioactive effluent release reports covering the operation of the unit during the previous calendar year of operation shall be submitted in accordance with 10CFR50.36a prior to May 1 of each year. The report shall include a summary of the quantities of radioactive liquid and gaseous effluent and solid waste released from the unit. The material provided shall be consistent with the objectives outlined in the ODCM and the PROCESS CONTROL PROGRAM and in conformance with 10CFR50.36a and 10CFR50, Appendix I, Section IV.B.1.
- b. The radioactive effluent release reports shall include a summary of the quantities of radioactive liquid and gaseous effluents and solid waste released from the unit as outlined in Regulatory Guide 1.21, "Measuring, Evaluating and Reporting Radioactivity in Solid Wastes and Releases of Radioactive Materials in Liquid and Gaseous Effluents from Light-Water-Cooled Nuclear Power Plants," Revision 1, June 1974, with data summarized on a quarterly basis following the format of Appendix B thereof.
- c. The radioactive effluent release report shall include the following information for each type of solid waste shipped offsite during the report period:
  - 1. Container volume,
  - 2. Total curie quantity (specify whether determined by measurement or estimate),
  - 3. Principal radionuclides (specify whether determined by measurement or estimate),
  - 4. Type of waste (e.g., spent resin, compacted dry waste, evaporator bottoms),
  - 5. Type of container (e.g., LSA, Type A, Type B, Large Quantity), and
  - 6. Solidification agent (e.g., cement, urea formaldehyde).

The radioactive effluent release reports shall include unplanned releases from the site to unrestricted areas of radioactive materials in gaseous and liquid effluents on a quarterly basis.

The radioactive effluent release reports shall include any changes to the PROCESS CONTROL PROGRAM (PCP) made during the reporting period.

The radioactive effluent release reports shall include a description of licensee initiated major changes to the radioactive waste treatment systems (liquid, gaseous and solid), as described in Section 12.6.3.)

<sup>4</sup>A single submittal may be made for a multiple unit station. The submittal should combine those sections that are common to all units at the station; however, for units with separate radwaste systems, the submittal shall specify the releases of radioactive material from each unit.

### 12.6 REPORTING REQUIREMENTS

### 12.6.3 Offsite Dose Calculation Manual (ODCM)\*

- 12.6.3.1The ODCM shall contain the methodology and parameters used in the calculation of offsite doses resulting from radioactive gaseous and liquid effluents, in the calculation of gaseous and liquid effluent monitoring alarm and trip setpoints, and in the conduct of the radiological environmental monitoring program; and
- The ODCM shall also contain the radioactive effluent controls and radiological environmental monitoring activities, and descriptions of the information that should be included in the Annual Radiological Environmental Operating, and Radioactive Effluent Release Reports required by Technical Specifications 5.6.2 and 5.6.3.
- 12.6.3.3 Licensee-Initiated changes to the ODCM:
  - Shall be documented and records of reviews performed shall be retained as required by the Quality Assurance (QA) Manual. This documentation shall contain:
    - Sufficient information to support the change(s) together with the appropriate analyses or evaluations justifying the change(s); and
    - 2. A determination that the change(s) maintain the level of radioactive effluent control required by 10 CFR 20.1302, 40 CFR Part 190, 10 CFR 50.36a, and 10 CFR Part 50, Appendix I, and not adversely impact the accuracy or reliability of effluent, dose, or setpoint calculations.
      - a. Shall become effective after approval of the Plant Manager.
      - b. Shall be submitted to the NRC in the form of a complete, legible copy of the entire ODCM as a part of or concurrent with the Radioactive Effluent Release Report for the period of the report in which any change to the ODCM was made. Each change shall be identified by markings in the margin of the affected pages, clearly indicating the area of the page that was changed, and shall indicate the date (i.e., month and year) the change was implemented.

<sup>\*</sup>The OFFSITE DOSE CALCULATION MANUAL (ODCM) is common to LaSalle Unit 1 and LaSalle Unit 2.

### 12.6 REPORTING REQUIREMENTS

### 12.6.4 Major Changes to Radioactive Waste Treatment Systems

- 12.6.4.1 License initiated major changes to the radioactive waste treatment systems (liquid and gaseous):
  - a. Shall be reported to the Commission in the Radioactive Effluent Release Report for the period in which the evaluation was reviewed by the Onsite Review and Investigative Function. The discussion of each change shall contain:
    - 1. A summary of the evaluation that led to the determination that the change could be made in accordance with 10 CFR 50.59;
    - 2. Sufficient detailed information to totally support the reason for the change without benefit or additional or supplemental information;
    - A detailed description of the equipment, components and processes involved and the interfaces with other plant systems;
    - 4. An evaluation of the change which shows the predicted releases of radioactive materials in liquid and gaseous effluents waste that differ from those previously predicted in the license application and amendments thereto;
    - 5. An evaluation of the change which shows the expected maximum exposures to individual in the unrestricted area and to the general population that differ from those previously estimated in the license application and amendments thereto:
    - 6. A comparison of the predicted releases of radioactive materials, in liquid and gaseous effluents, to the actual releases for the period to when the changes are to be made;
    - 7. An estimate of the exposure to plant operating personnel as a result of the change; and
    - 8. Documentation of the fact that the change was reviewed and found acceptable by the Onsite Review and Investigative Function.
  - b. Shall become effective upon review and acceptance by the Onsite Review and Investigative Function.

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# APPENDIX F STATION-SPECIFIC DATA FOR LASALLE UNITS 1 AND 2

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# APPENDIX F STATION-SPECIFIC DATA FOR LASALLE UNITS 1 AND 2

### F.1 INTRODUCTION

This appendix contains data relevant to the LaSale site. Included is a figure showing the unrestricted area boundary, restricted area boundary, and values of parameters used in offsite dose assessment.

### F2 REFERENCES

- Sargent & Lundy, Analysis and Technology Division, LaSalle Calculation No. ATD-0164, Revisions 0, 1, 2 and 3.
- Sargent & Lundy, Nuclear Safeguards and Licensing Division, LaSalle Calculation No. ATD-0139, "N-16 Skyshine Ground Level Doses from LaSalle Turbine System & Piping, Revision C.
- S. Vertication of Environmental Parameter used for Commonwealth Edison Company's Offsite Dose Calculations, "NUS Corporation, 1988.

## Table F-1 Aquatic Environment Dose Parameters

### General Information®

The station Equid discharge flows into the Minois River then into the Mississippi River.

Recreation includes one or more of the following: boating, waterskling, swimming, and sport fishing.

Two downstream dams are on the Winols River, Marselles and Starved Rock. This information is based on Section 2.4.1.1 and Figures 2.4-2 and 2.4-6 of the LaSalle Environmental Report.

### Water and Fish Ingestion Parameters

Parameter*		Yakın
VM", VM' F", cis F', cis t', hr' t", hr'	•	1.0 1.85E4 1.31E4 24.0 97.0

### Umits on Radioactivity in Unprotected Outdoor Tanks\*

Outside Temporary Tank ≤ 10 Cf

This is based on information in LaSale Environmental Report, Figure 3.3-1 and Section 2.1.4.2.1.

<sup>\*</sup> The parameters are defined in Sections A.2.1 of Appendix A.

<sup>&</sup>quot; if (hr) = 24 hr (all stations) for the fish ingestion pathway

<sup>&</sup>quot; (" (hr) = 97 hr (distance to nearest public potable water Intake, Peoria, is 97 miles; flow rate of 1 mph is assumed.)

<sup>\*</sup> See Section A.2.4 of Appendix A.

Tritium and dissolved or entrained nable pases are excluded from this limit.

### Table F-2

### Station Characteristics

STATION: LaSale											
LOCATION: 6 miles south of Man	LOCATION: 6 miles south of Marseilles, Minols - LaSalle County										
CHARACTERISTICS OF ELEVAT	ED RELEASE POINT	•									
1) Release Height =112.8_m² 2) Extt Speed . =14.7_ms²*	1) Release Height =112.8_m²										
CHARACTERISTICS OF VENT S	TACK RELEASE POINT: Not Ap	plicable (NA)									
1) Release Height =m 3) Exit Speed =ms <sup>4</sup>	· 2) Dia	meter =m									
CHARACTERISTICS OF GROUN	D LEVEL RELEASE										
1) Release Height = 0 m 2) Building Factor (D) = <u>56.4</u>	_m°										
METEOROLOGICAL DATA											
A_400_ft Tower is Located_72	SE of elevated releas	se point									
Tower Data Used in Calculations											
· Release Point	·Wind Speed and Direction	Differential Temperature									
Elevated	375 ft	375-83 ft									

Elevated

<sup>(</sup>NA) (NA) Vent 200-33 ft Ground 33 ft

<sup>\*</sup>Used in calculating the meteorological and dose factors in Tables F-5, F-6, and F-7. See Sections B.3 through B.6 of Appendix B.

Table F-3 Critical Ranges

<u>Direction</u>	Unrestricted Area Boundary*	Restricted Area Boundary (m)	Nearest Resident	Nearest Dairy Farm Within 5 Miles*
·	• •	4000	6300	None
N ·	1036	1036	2800 -	· None
NNE	1978 .	1378	3400	None.
NE .	2408	1609	5300	None
EN'E	4450	1079	8300	•
		-	5200	None
· E	1996	833	2300	None
ESE	1485	845	2700	None
CE.	. 969	969	2900	None .
ESE	638	698	2800	
•		620	2400	None
8	629		1100	None
SSW .	835	835	1600	None
Wa	628	628	2400	None .
WSW	533	533	2400	•
		.204	1300	· None .
W	524	524	1400	None
· WNW	643	643	2900	None
NW	762	782	2700	7400
NNW	. 890	690	2100	

Used in calculating the meteorological dose factors in Tables F-5 and F-7. See Sections B.3 through B.6 of Appendix B.

<sup>1994</sup> annual survey by Teledyne Isotopes Midwest Laboratories. The distances are rounded to the nearest conservative 100 meters.

c 1994 annual milk animal census, by Teledyne Isotopes Midwest Laboratories. Used in Calculating the D/Q values in table F.6. The distances are rounded to the nearest conservative 100 meters. A default value of 8000 meters is used when there are no dairies within 5 miles.

Table F-4
Average Wind Speeds

Downwind		Averan	Average Wind Speed (m/sec)*				
Direction		Elevated	<u>Vent</u>	Ground Lavel			
N	• • • •	8.7	7.7	4.9			
NNE		10.1	0.8	<b>5.1</b>			
NE		9.2	7.4	4.9			
ENE	•	0.9	72	4.8			
Ė	•	9.5	7.8	5.2			
ESE	• •	9.7	8.4	. 5.9			
SE.		8.1	. 7A	5.9			
· ESE		7.4	6.7	5.0			
		6.7	6.3	4.8			
wea		5.6	8.7	2.9			
·sw		5.5	4.1	8:1			
wsw		6.9	5.4	9.6			
W		7.6	6.5	4.5			
WNW		7.5	6.3	4.3			
		7.5		3.9			
NNW	•	8.8	6.7	4.3			

<sup>\*</sup>Based on LaSalle site meteorological data, January 1978 through December 1987. Calculated Reference 1 of Section F.2, using formulas in Section B.1.3 of Appendix B.

Table F-5

X/Q and D/Q Maxima at or Beyond the Unrestricted Area Soundary

Downstad		leveredrese				Hived Hede(Vent) Release			Greend Lovel Ruleaca		
Piraction		( <del>************************************</del>	Radius (meters)	(1/ <del>m,5</del> ) b/d		(ees/E <sub>202</sub> )	(1/ <del>4**2</del> )	Redium (meters)	(200/E/03)	(1\ <del>-,.5</del> )	
₩ ,	5633.	6.1232-09	1036.	7.2036-10	6000.	6.207E-07	8.3116-10	1036.	1.5242-06	1.0102-01	
MAG	1378.	7.045E-09	1370.	9.831E-10	5633.		7.657E-10		9.7378-07		
WE	4400.	5,5372-09	2408.	4.245E-10			4.6366-10		3.907E-07		
ENE	5200.	5,0862-09	4450.	2.021E-10			2.0246-10	4470.	1,4762-07		
€ .	5200.	5.8652-09	1976.	5.4152-10			6.376E-10	1996.	4.0702-07		
ESE	5200.		1500.	0.8762-10			1.2278-09		7.2238-07		
88	5633.	7-1168-09	1500.	7.5056-10			1.707E-09		1.137E-06		
812	5200.	4.717E-09		7.1762-10			2.1246-09				
8	5633.	3.9106-09		4.1362-10			1,3032-09		1.174E-06		
23V	6000.	5.2672-09		3.7771-10			9.9998-18		1.1122-06		
84	6000.	4.767E-09		8.545E-10					7.9406-07		
<b>VTV</b>	6000	6.0652-09		6.527E-10			2.154E-09		1.8642-06		
v	6437.						\$.0775-09		2.1016-06		
		3.3342-09		4.811E-10			1.6276-07		2,6306-06		
PART	7242.	3.916E-09		3.1771-19			9.0712-10	643.	2.4272-06	1,5000-00	
186	7242.	3.766E-09		3.1122-10	5633.	4.1272-07	6.460E-19	762.	1.7842-06		
	4437.	4.2402-09	1500.	3.8062-19	4437.	4-0952-09	5.5742-10		1_4092-04		

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Note:

Based on Reference 2 of Section F.2 and the formulas in Sections B.3 and B.4 of Appendix B.

Used for beta sir, beta skin, and inhalation dose pathways. See sections A.1.2, A.1.3 and A.1.4.2 of Appendix A.

Used for produce and leafy vegetable pathways. See A.1.4 of Appendix A.



Table F-5a

## X/Q and D/Q Maxima at or Beyond the Restricted Area Boundary

Downwind						Mixed Mode(Vent) Release			nd Level Rel	e250 F
Direction		X/Q (sec/m**3)	Radius (meters)	D/Q (1/m**2)	Redfus (meters)	X/Q (sec/m**3)	D/Q (1/m**2)	Radius (meters)	X/Q (sec/m**3)	D/Q (1/m**2)
H	5633.	6.123E-09	1036.	7.203E-10	6000.	6.289E-09	8.311E-10	1036.	1.524E-06	1-019E-08
WHE	1378.	7.045E-09	1378.	9.831E-10	5633.		9.659E-10	1378.	9.737E-07	
NE	4400.	5.535E-09		6.556E-10		6.052E-09	7.953E-10	1609.	7.003E-07	
ENE	5200.	5.0865-09	1079.	6.376E-10	1079.		9.861E-10	1079.	1.1285-06	
E	5200.	5.865E-09	1500.	6.659E-10	1055.	7.712E-09	1.160E-09	1055.		8.779E-09
ESE	5200.	8.000E-09	1500.	8.8968-10	1055.	9.981E-09	1.546E-09	1055.		1.021E-08
SE	5633.	7.1168-09	1500.	7.505E-10	969.	1.087E-08	1.709E-09	969.	1.137E-06	1.1235-08
SSE	5200.	6.717E-09	698.	7.210E-10	698.		2.4038-09	698.		1.428E-08
S	5633.	5.910E-09	1500.	6.136E-10	820.	8.455E-09	1.312E-09	820.		1.0582-08
22/	6000.	5.269E-09	835.	5.793E-10	835.	7.322E-09	9.999E-10	835.	7.940E-07	5.359E-09
SV	6000.	6.767E-09	628.	8.545E-10	628.	2.224E-08	2.154E-09	628.	1.864E-06	1.407E-08
NSM	6000.	6.065E-09	533.	6.527E-10	540.	2.105E-08	2.079E-09	533.	2.101E-06	1-9705-08
¥	6437.	5.354E-09		4.811E-10			1.629E-09	524.	2.830E-06	
WW	7242.	3.916E-09	1500.	3.175E-10		5.963E-09	9.071E-10		2.429E-06	
MA	7242.	3.766E-09		3.118E-10			6.660E-10			1.055E-08
MAN	6437.	4.240E-09		3.806E-10			5.574E-10	890.		8.840E-09



### Table F-6

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### D/Q at the Nearest Milk Cow and Meat Animal Locations within 5 miles

Channeled Heatest Hilk Com D/Q(1/m==2)					Nearest Heat Animal D/Q(1/m**2)				
Direction		Elevated	Mixed	Ground	Redius	Elevated	Mixed	Ground	
	(meters)	Release	Release	Heleese	(wetata)	Kelease	Release	Release	
N	8000.	9.711E-11	1.006E-10	2.915E-10	6400.	1.3878-10	1.436E-10	4.3526-10	
NNE	8000.			3.2776-10	3100.			1.7602-09	
PHE -	8000.			2.851E-10				5.403E-10	
ENR	8000.	8.559E-11	8.420E-11	2.381E-10	5000.			5.5198-10	
E	8000.	1.056E-10	9.772E-11	2.587E-10	6000.			2.587E-10	
ESE	8000.			3.010E-10				3.0102-10	
SE	8000.	1.242E-10	1.3228-10	2.881E-10	7600.			3.160g-10	
SSE	8000.	1.174F.10	1.2788-10	2.152E-10	7600.				
S	8000.	0 447E 11	0.0050.10	2.1526-10	7600.			2.360E-10	
SSM				2.065E-10		9.447E-31	9.895E-11	2.065E-10	
	8000.			1.077E-10		8.647E-11	9.097E-11	1.077E-10	
SW	8000.			1.7932-10		1.0962-10	1.210E-10	1.79JE-10	
wsw	8000.	1.017E-10	1.0832-10	1.940E-10	8000.			1.940E-10	
M	8000.	8.494E-11	1.094E-10	2.354E-10	4800.			5.866E-10	
WW	8000.	5.834E-11	6.886E-11	1.994E-10	5200.			4.312E-10	
NH	8000.			1.0205-10				2.7302-10	
\$4544	7400.			2.269E-10	7600.			2.163E-10	

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Note: Based on Reference 2 of Section F.2 and the formulas in Section B.4 of Appendix B.







Maximum Offsite Finite Plume Gamma Dose Factors Based on 1 cm Depth at the Unrestricted Area Boundary for Kr-83m

Downlind Unrestricted Elevated(Stack) Release Direction Area Bound Redius S SBAR					Hode(Vent) Release	Ground Level Release		
<i>- - - - - - - - - -</i>	(meters)		\$ SBAR : (mred/yr)/(uCl/sec)	Redfus (meters)	V VEAR (mrad/yr)/(uC1/sec)	Radius (meters)	GEAR (mrad/yr)/(uC1/se/)	
M	1036.	1036.	4.787E-07 3.609E-07	1036.	5.281E-07 3.982E-07	1036.	1.7852-04 1.3462-04	
MME	1378.	1378.	8.751E-07 6.599E-07	1378.	6.905E-07 5.206E-07	1378.	1.139E-04 8.586E-03	
WE	2408.	2408.	6.471E-07 4.879E-07	2408.	6.697E-07 5.049E-07	2408.	4.355E-05 3.284E-05	
ene	4450.	4450.	5.700E-07 4.298E-07	4450.	5.653E-07 4.262E-07	4450.	1.4668-05 1.1058-05	
E	1996.	1996.	4.687E-07 3.534E-07	1996.	7.559E-07 5.700E-07	1996.	5.4912-05 4.1402-05	
ESE	1465.	1465.	5.252E-07 3.960E-07	1465.	1.002E-06 7.559E-07	1465.	6.270E-05 6.236E-05	
SE	969.	969.	3.545E-07 2.673E-07	969.	1.267E-06 9.554E-07	969.	1.333E-04 1.005E-04	
SSE	838.	838.	3.051E-07 2.301E-07		1.512E-06 1.140E-06	838.	1.323E-04 9.978E-05	
S	829.	829.	2.840E-07 2.141E-07		1.0406-06 7.8426-07	829.	1.330E-04 1.003E-04	
SSN	835.	835.	3.185E-07 2.401E-07		1-0716-06 8-0766-07	835.	9.3268-05 7.0328-05	
SW	628.	628.	3.177E-07 2.395E-07		2.826E-06 2.131E-06	628.	2.305E-04 1.738E-04	
NZA	533.	533.	2.617E-07 1.973E-07	533.	2.674E-06 2.017E-06	533.	2.568E-04 1.936E-04	
	524.	524.	2.327E-07 1.754E-07		1.658E-06 1.250E-06	524.	3.352E-04 2.527E-04	
unu	643.	643.	1.714E-07 1.29ZE-07		7.235E-07 5.455E-07	643.	2.728E-04 2.057E-04	
KV	762.	762.	1.7448-07 1.3158-07		4.3916-07 3.3116-07	762.	2.219E-04 1.673E-04	
MAN	890.	890.	2.397E-07 1.807E-07		3.334E-07 2.514E-07	890.	1.823E-04 1.374E-04	

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Note: Based on Reference 1 of Section F.2 and the formulas in Sections B.5 and B.6 of Appendix B.

### Table F-7 (Continued)

Maximum Offsite Finite Plume Gamma Dose Factors Based on 1 cm Depth at the Unrestricted Area Boundary for Kr-85m

Downlad t	heasteleta	4 Flavet	ed(Stack) Release	Hixed !	Mode(Vent) Release'	Ground Level Release		
	Area Bound		S SBAR	Redius	A ABYS.	Redfus	G GBAR F	
. Discrition	(meters)	(meters)	(mrad/yr)/(uCi/sec)	(meters)	(mrad/AL)\(nc \zec)	(meters)	(mrad/yr)/(uCi/sec)	
	1036.	1036.	5.747E-05 5.560E-05	1036.	6.602E-05 6.388E-05	1036.	9.660E-04 9.252E-04	
KME	1378.	1378.	5.0632-05 4.8962-05		5.514E-05 5.334E-05	1378.	6.7762-04 6.4962-04	
ME	2408.	2408.	2,592E-05 2,506E-05		2.727E-05 2.636E-05	2408.	2.969E-04 2.849E-04	
ENE	4450.	4450.	1.3516-05 1.3046-05		1.3326-05 1.2866-05	4450.	1.156E-04 1.111E-04	
Enc	1996.	1996.	2.7058-05 2.6168-05		2.863E-05 2.767E-05	1996.	3.557E-04 3.412E-04	
<del>-</del>	1465.	1465.	4.351E-05 4.209E-05	• –	4.6248-05 4.4708-05	1465.	5.201E-04 4.989E-04	
ESE	•	969.	5.596E-05 5.415E-05		6.610E-05 6.391E-05	969.	7.793E-04 7.470E-04	
SE	969.		5.518E-05 5.339E-05		6.630E-05 6.410E-05		7.683E-04 7.364E-04	
SSE	838.	<b>638.</b>			5.3306-05 5.1546-05	829.	7.986E-04 7.657E-04	
\$	829.	829.	4.712E-05 4.560E-05		5.351E-05 5.174E-05	835.	5.684E-04 5.450E-04	
SSW	<b>835.</b>	835.	4.4228-05 4.2798-05	835.			1.2856-03 1.2316-03	
SV	628.	628.	7.2818-05 7.0468-05		9.952E-05 9.618E-05		1.3896-03 1.3316-03	
NZM	533.	533.	7.757E-05 7.507E-05		9.714E-05 9.388E-05		1.687E-03 1.614E-03	
u	524.	524.	7.6016-05 7.3566-05		9.705E-05 9.385E-05	524.		
WH	643.	643.	5.2862-05 5.1162-05		6.615E-05 6.399E-05	643.	1.3272-03 1.2702-03	
8119	762.	762.	4.6682-05 4.5182-05	762.	5.688E-05 5.503E-05		1.094E-03 1.047E-03	
MAN	890.	890.	4.683E-05 4.532E-05	890.	5.142E-05 4.976E-05	890.	9.28ZE-04 8.885E-04	

### Table F-7 (Continued)

### Maximum Offsite Finite Plume Gamma Dose Factors Based on 1 cm Depth at the Unrestricted Area Boundary for Kr-85

										•7	
Downsind t	Inrestricted	Elevate	ed(Stack) Re	ele <del>sso</del>	Mfxed (	Hode(Vent)	Reterre	Grous	nd Level A	reteasi	l
Direction	Area Bound	Redius	\$	SEAR	Redfus	٧	VBAR	Radius	G	GÉAR	Ĩ
	(metèrs) Jši	(meters)	(mrad/yr)/	(uCi/sec)	(meters)	(mrad/yr)/	(rrc1\zec)	(meters)	(mred/yr)	/(uCi/sec)	
	1036.	1036.	8.547E-07	8.265E-07	1036.	9.889E-07	9.563E-07	1036.	1.056E-0	75 1.021E-05	
NNE	1378.	1378.	7.309E-07	7.058E-07	1378.	8.077E-07	7.811E-07	1378.	7.4742-0	36 7.227E-06	
NE	2408.	2408.	3.651E-07	3.530E-07	2408.	3.909E-07	3.780E-07	2408.	3.363E-0	06 3.252E-06	
ENE	4450.	4450.	1.885E-07	1.823E-07	4450.	1.8562-07	1.7956-07	4450.	1.377E-0	06 1.332E-06	
E	1996.	1996.	3.912E-07	3.782E-07	1996.	4.096E-07	3.961E-07	1996.	4.008E-0	06 3.876E-06	
ESE	1465.	1465.	6.359E-07	6.149E-07	1465.	6.632E-01	6.413E-07	1465.	5.7836-0	06 5.593E-06	
SE	969.	969.	8.386E-07	8.110E-07	969.	9.583E-07	9.267E-07	969.	8.555E-0	06 8.273E-06	
35E	838.	838.	8.350E-07	8.075E-07	838.	9.612E-07	9.294E-07	838.	8.432E-0	06 B.154E-06	•
S	829.	829.	7.2628-07	7.023E-07	829.	8.067E-01	7.801E-07	829.	8.7412-0	06 <b>0.4</b> 53E-06	
SSW	835.	835.	6.857E-07	6.630E-07	835.	8.402E-07	8.124E-07	835.	6.270E-0	06 6.063E-06	
514	628.	628.	1.142E-06	1.104E-06	6281	1.4946-06	1.444E-06			05 1.355E-05	
NZM	533.	533.	1.211E-06	1.171E-06	533.	1.4338-06	1.3862-06	533.	1.510E-	05 1.460E-05	
W	524.	524.	1.172E-06	1.134E-06	524.	1.443E-06	1.395E-06	524.		05 1.763E-05	
LINU	643.	643.	8.185E-07	7.915E-07	643L	1.000E-0	9.670E-07	643.	1.436E-	05 1.389E-05	
KI	762.	762.	7.192E-07	6.954E-07	762.	8.694E-07	8.407E-07	762.	1.188E-	DS 1.148E-05	
MALT	890.	890.	7.128E-07	6.893E-07	890.	7.849E-01	7.590E-07	890.	1.011E-	DS 9.778E-06	Ė



### Table F-7 (Continued)

## Maximum Offsite Finite Plume Gamma Dose Factors Based on 1 cm Depth at the Unrestricted Area Boundary for Kr-87

Downwind Unrestricted Elevated(Stack) Release Direction Area Bound Radius S SBAR					Hode(Vent) Release	Ground Level Release		
Direction	(meters)		(mrad/yr)/(uCl/sec)	Redfus (meters)	V VEAR (mrad/yr)/(uCi/sec)	Redius (meters)	G GBAR† (mrad/yr)/(uCi/sec)	
	1036.	1036.	3.226E-04 3.135E-04	1036.	3.758E-04 3.652E-04	1036.	2.879E-03 2.795E-03	
NNE .	1378.	1378.	2.672E-04 2.597E-04	1378.	3.005E-04 2.920E-04	1378.	2.0198-03 1.9608-03	
NE NE	2408.	2408.	1.283E-04 1.246E-04	2408.	1.359E-04 1.320E-04	2408.	8.605E-04 8.355E-04	
ENE	4450.	4450.	5.904E-05 5.737E-05	4450.	5.859E-05 5.69ZE-05	4450.	3.133E-04 3.042E-04	
E	1996.	1996.	1.412E-04 1.372E-04	1996.	1.458E-04 1.417E-04	1996.	1.030E-03 9.998E-04	
ESE	1465.	1465.	2.351E-04 2.284E-04	1465.	2.426E-04 2.357E-04	1465.	1.545E-03 1.500E-03	
SE	969.	969.	3.211E-04 3.120E-04	969.	3.612E-04 3.510E-04	969.	2.355E-03 2.287E-03	
SSE	838.	838.	3.254E-04 3.162E-04		3.655E-04 3.552E-04	838.	2.3298-03 2.2628-03	
S	829.	829.	2.850E-04 2.770E-04		3.0816-04 2.9946-04	829.	2.431E-03 2.361E-03	
SSM	835.	835.	2.742E-04 2.665E-04	835.	3.400E-04 3.305E-04	835.	1.706E-03 1.657E-03	
SV	628.	628.	4.614E-04 4.484E-04	628.	5.936E-04 5.769E-04	628.	3.903E-03 3.790E-03	
NZN	533.	533.	4.880E-04 4.743E-04	533.	5.683E-04 5.523E-04	533.	4.251E-03 4.128E-03	
U	524.	524.	4.675E-04 4.543E-04	524.	5.708E-04 5.547E-04	524.	5.136E-03 4.986E-03	
UNU	643.	643.	3.224E-04 3.133E-04	643.	3.914E-04 3.804E-04	643.	4.001E-03 3.884E-03	
WW	762.	762.	2.8236-04 2.7436-04	762.	3.397E-04 3.301E-04	762.	3.2768-03 3.1808-03	
RINA	890.	890.	2.747E-04 2.669E-04	890.	3.0318-04 2.9458-04	890.	2.763E-03 2.683E-03	

### Table F-7 (Continued)

## Maximum Offsite Finite Plume Gamma Dose Factors Based on 1 cm Depth at the Unrestricted Area Boundary for Kr-88

Downrind Unrestricted Elevated(Stack) Release Direction Area Bound Radius S SBRR			Mixed Mode(Vent) Release Redius V VBAR		Ground Level Release		
	(meters)	(meters)	(mrad/yr)/(uCi/sec)	(meters)	(mrad/yr)/(uCi/sec)	(meters)	(mrad/yr)/(uCi/sec)
Ж	1036.	1036.	8.602E-04 8.374E-04	1036.	1.003E-03 9.769E-04	1036.	6.988E-03 6.787E-03
NNE	1378.	1378.	7.111E-04 6.922E-04		7.989E-04 7.777E-04	1378.	4.940E-03 4.798E-03
HE	2408.	2408.	3.435E-04 3.344E-04	2408.	3.6942-04 3.5962-04		2.1826-03 2.1206-03
ENE	4450.	4450.	1.648E-04 1.604E-04	4450.	1.646E-04 1.60ZE-04	4450.	8.502E-04 8.263E-04
E	1996.	1996.	3.781E-04 3.680E-04		3.928E-04 3.824E-04		2.599E-03 2.525E-03
ESE	1465.	1465.	6.235E-04 6.070E-04		6.445E-04 6.273E-04		3.816E-03 3.707E-03
SE	969.	969.	8.537E-04 8.311E-04		9.571E-04 9.317E-04	969.	5.712E-03 5.549E-03
\$3E	838.	838.	8.671E-04 8.442E-04		9.702E-04 9.445E-04	838.	5.645E-03 5.483E-03
\$	829.	829.	7.696E-04 7.492E-04		8.417E-04 B.194E-04	829.	5.862E-03 5.695E-03
22M	835.	835.	7.427E-04 7.231E-04	835.	9.375E-04 9.127E-04	835.	4.167E-03 4.048E-03
SW	628.	628.	1.246E-03 1.213E-03	628.	1.601E-03 1.559E-03	628.	9.396E-03 9.126E-03
nzn	533.	533.	1.3146-03 1.2796-03		1.525E-03 1.485E-03		1.017E-02 9.882E-03
W	524.	524.	1.2496-03 1.2166-03	524.	1.520E-03 1.480E-03	524.	1.225E-02 1.190E-02
LARM	643.	643.	8.669E-04 8.440E-04		1.045E-03 1.017E-03		9.595E-03 9.317E-03
m	762.	762.	7.580E-04 7.379E-04		9.125E-04 8.884E-04	762.	7.895E-03 7.666E-03
MMA	890.	890.	7.369E-04 7.174E-04		8.161E-04 7.945E-04	890.	6.693E-03 6.500E-03

Table F-7 (Continued)

## Maximum Offsite Finite Plume Gamma Dose Factors Based on 1 cm Depth at the Unrestricted Area Boundary for Kr-89

Downwind Unrestricted Elevated(Stack) Release Direction Area Bound Radius \$ 5282				Mixed Hode(Vent) Release		Ground Level Release	
Pirection	(meters)		S SBAR (mrsd/yr)/(uCi/sec)	Radius (meters)	W YBAR (mrad/yr)/(uCl/sec)	Radius (meters)	G GBAR # (mrad/yr)/(uCi/sed)
M	1036.	1036.	3.9048-04 3.7948-04	1036.	4.258E-04 4.139E-04	1036.	2.051E-03 1.992E-03
MXE	1378.	1378.	2.820E-04 2.741E-04	1378.	2.988E-04 2.904E-04	1378.	1.151E-03 1.118E-03
NE	2408.	2408.	8.306E-05 8.072E-05	2408.	7.403E-05 7.195E-05	2408.	2.060E-04 2.001E-04
ENE	4450.	4450.	1.570E-05 1.526E-05	4450.	1.1536-05 1.1216-05	4450.	1.701E-05 1.653E-05
E	1996.	1996.	1.052E-04 1.023E-04	1996.	9.299E-05 9.037E-05	1996.	3.031E-04 2.944E-04
ESE	1465.	1465.	2.365E-04 2.299E-04	1465.	2.240E-04 2.177E-04	1465.	7.762E-04 7.540E-04
SE	969.	969.	3.891E-04 3.782E-04	969.	4.188E-04 4.070E-04	969.	1.846E-03 1.793E-03
SSE	838.	838.	4.108E-04 3.993E-04	838.	4.365E-04 4.243E-04	838.	1.831E-03 1.778E-03
S	829.	829.	3.408E-04 3.312E-04	829.	3.253E-04 3.162E-04	829.	2.034E-03 1.976E-03
SSW	835.	835.	2.921E-04 2.839E-04	835.	2.779E-04 2.702E-04		1.021E-03 9.916E-04
SW	628.	628.	5.830E-04 5.667E-04	628.	6.600E-04 6.415E-04	628.	3.274E-03 3.180E-03
usu	533.	533.	6.913E-04 6.720E-04	533.	7.525E-04 7.314E-04		4-592E-03 4-460E-03
W	524.	524.	6.961E-04 6.766E-04	524.	8.259E-04 8.028E-04		5.967E-03 5.796E-03
unu	643.	643.	4.295E-04 4.174E-04	643.	5.147E-04 5.003E-04		3.746E-03 3.638E-03
Mrs	762.	762.	3.500E-04 3.402E-04		4.035E-04 3.922E-04		2.561E-03 2.488E-03
811118	890.	890.	3.301E-04 3.208E-04		3.4156-04 3.3196-04		1.966E-03 1.909E-03

### Table F-7 (Continued)

## Maximum Offsite Finite Plume Gamma Dose Factors Based on 1 cm Depth at the Unrestricted Area Boundary for Kr-90

Downwind Unrestricted Elevated(Stack) Release Direction Area Bound Redius S SBAR			Mixed Mode(Vent) Release Redius V VEAR		Ground Level Release Redfue G GBAR 1		
	(meters)	,,	(mred/yr)/(uCl/sec)		(mrad/yr)/(uCi/sec)		(mred/yr)/(uCl/sec)
H	1036.	1036.	6.7852-05 6.5862-05	1036.	5.199E-05 5.047E-05	1036.	8.2038-05 7:9548-05
NNE	1378.	1378.	3.195E-05 3.102E-05	1378.	2.161E-05 2.098E-05	1378.	2.265E-05 2.196E-05
NE	2408.	2408.	2.160E-06 2.097E-06	2408.	9.136E-07 8.86EE-07	2408.	5.870E-07 5:693E-07
ENE	4450.	4450.	1.109E-07 1.076E-07	4450.	3.907E-08 3.792E-08	4450.	1.814E-08 1:759E-08
E	1996.	1996.	4.713E-06 4.575E-06		2.562E-06 2.486E-06		2.865E-06 2.779E-06
ESE	1465.	1465.	2.134E-05 2.072E-05	1465.	1.551E-05 1.506E-05	1465.	2.503E-05 2.427E-05
SE	969.	969.	5.843E-05 5.673E-05	969	5.324E-05 5.168E-05	969.	1.365E-04 1.324E-04
SSE	838.	838.	6.863E-05 6.663E-05	838.	6.174E-05 5.993E-05	838.	1.227E-04 1.190E-04
S	829.	829.	5.057E-05 4.909E-05	829.	3.745E-05 3.635E-05	829.	1.055E-04 1.023E-04
SSW	835.	835.	3.062E-05 2.972E-05	835.	1.274E-05 1.237E-05	835.	1.835E-05 1.779E-05
SW	628.	628.	9.754E-05 9.470E-05	628.	6.538E-05 6.347E-05	628.	1.410E-04 1.368E-04
usu	533.	533.	1.892E-04 1.836E-04	533.	1.525E-04 1.480E-04	533.	4.8612-04 4.7132-04
W	524.	524.	2.165E-04 2.101E-04	524.	2.185E-04 2.121E-04	524.	8.427E-04 8.170E-04
MW	643.	643.	1.018E-04 9.883E-05	643.	1.008E-04 9.787E-05	643.	3.141E-04 3.045E-04
3678	762.	762.	6.634E-05 6.440E-05	762.	5.8158-05 5.6458-03	762.	1.306E-04 1.267E-04
MARI	890.	890.	5.725E-05 5.558E-05	890.	4.336E-05 4.209E-05	890.	8.619E-05 8.551E-05



### Table F-7 (Continued)

## Maximum Offsite Finite Plume Gamma Dose Factors Based on 1 cm Depth at the Unrestricted Area Boundary for Xe-131m

Downwind Unrestricted Elevated(Stack) Release			Mixed (	Hode(Vent) Release	Ground Level Release		
Direction	Area Bound	***	S SPAR	Redius	V VBAR	Redfus	
	(meters)	(meters)	(mred/yr)/(uC\$/sec)	(meters)	(mrad/yr)/(uCi/sec)	(meters)	(mrad/yr)/(uCi/sec
Ħ	1036.	1036.	1.6062-06 1.4732-06	1036.	1.827E-06 1.679E-06	1036.	1.645E-04 1.283E-04
NNE	1378.	1378.	1.778E-06 1.572E-06	1378.	1.726E-06 1.553E-06	1378.	1.072E-04 8.384E-05
WE	2408.	2408.	1.086E-06 9.376E-07		1.136E-06 9.826E-07	2408.	4.347E-05 3.412E-05
ENE	4450.	4450.	7.931E-07 6.617E-07	4450.	7.858E-07 6.550E-07	4450.	1.623E-05 1.279E-05
E	1996.	1996.	9.572E-07 8.457E-07	1996.	1.230E-06 1.058E-06	1996.	5.428E-05 4.253E-05
ESE	1465.	1465.	1.347E-06 1.215E-06	1465.	1.789E-06 1.560E-06	1465.	7.935E-05 6.215E-05
SE	969.	969.	1.472E-06 1.365E-06	969.	2.406E-06 2.115E-06	969.	1.240E-04 9.696E-05
SSE	838.	838.	1.415E-06 1.318E-06		2.598E-06 2.260E-06	838.	1.228E-04 9.597E-05
5	829.	829.	1.231E-06 1.144E-06		1.966E-06 1.727E-06	829.	1.232E-04 9.639E-05
SSM	835.	835.	1.196E-06 1.103E-06	835.	2.003E-06 1.755E-06		8.798E-05 6.885E-05
SW	628.	628.	1.802E-06 1.691E-06		4.345E-06 3.728E-06		2.109E-04 1.646E-04
NZM	533.	533.	1.859E-06 1.755E-06		4-161E-06 3-577E-06		2.324E-04 1.813E-04
V	524.	524.	1.800E-06 1.703E-06		3.359E-06 2.972E-06		3.000E-04 2.335E-04
WW	643.	643.	1.2632-06 1.1942-06		1.9765-06 1.7915-06		2.446E-04 1.902E-04
KV	762.	762.	1.135E-06 1.069E-06		1.561E-06 1.437E-06		2.005E-04 1.560E-04
MASS	890.	890.	1.191E-06 1.112E-06		1.363E-06 1.263E-06		1.664E-04 1.295E-04

# Maximum Offsite Finite Plume Gamma Dose Factors Based on 1 cm Depth at the Unrestricted Area Boundary for Xe-133m

			ed(Stack) Release	****	Hode(Vent) Release		nd Level Release
Direction	Area Bound (meters)		S SBAR (mrad/yr)/(uCi/sec)	Redius (meters)	v VBAR (mred/yr)/(uCi/sec)	Radius (meters)	GEAR (mred/yr)/(uCl/sec)
N	1036.	1036.	8.557E-06 8.199E-06	1036.	9.814E-06 9.407E-06	1036.	2.822E-04 2.410E-04
MME	1378.	1378.	7.917E-06 7.509E-06	1378.	8.400E-06 8.009E-06	1378.	1.901E-04 1.633E-04
ME	2408.	2408.	4.246E-06 3.993E-06		4.482E-06 4.217E-06	2408.	8.0322-05 6.9502-05
ENE	4450.	4450.	2.488E-06 2.298E-06		2.450E-06 2.262E-06	4450.	3.108E-05 2.706E-05
E	1996.	1996.	4.247E-06 4.028E-06	1996.	4.721E-06 4.433E-06	1996.	9.835E-05 8.482E-05
ESE	1465.	1465.	6.614E-06 6.309E-06		7.393E-06 6.978E-06	1465.	1.4326-04 1.2346-04
SE	969.	969.	8.229E-06 7.903E-06		1.039E-05 9.834E-06	•	2.189E-04 1.879E-04
SSE	838.	838.	8.0702-06 7.7582-06		1.060E-05 9.998E-06		2.163E-04 1.856E-04
\$	829.	829.	6.932E-06 6.660E-06		8.449E-06 7.995E-06	829.	2.2018-04 1.8938-04
SSV	835.	835.	6.541E-06 6.276E-06		8.500E-06 8.036E-06	835.	1.574E-04 1.354E-04
SV	628.	628.	1.0596-05 1.0206-05		1.637E-05 1.535E-05	628.	3.6685-04 3.1405-04
usu	533.	533.	1.1212-05 1.0812-05		1.588E-05 1.490E-05	533.	4.005E-04 3.423E-04
u	524.	524.	1.096E-05 1.056E-05		1.504E-05 1.427E-05	524.	5.039E-04 4.287E-04
LINU	643.	643.	7.6482-06 7.3742-06		9.956E-06 9.510E-06		4.055E-04 3.441E-04
MA	762.	762.	6.7748-06 6.5268-06		8.435E-06 8.088E-06		3.334E-04 2.831E-04
NKA	890.	890.	6.855E-06 6.594E-06		7.5888-06 7.2868-06		2.794E-04 2.377E-04



### Table F-7 (Continued)

# Maximum Offsite Finite Plume Gamma Dose Factors Based on 1 cm Depth at the Unrestricted Area Boundary for Xe-133

			ed(Stock) Release		Node(Vent) Release	Ground Level Release		
Directio	n Area Bound		S STAR	Redius		Redius	G GBAR	
	(meters)	(meters)	(mred/yr)/(uCi/sec)	(meters)	(mred/yr)/(uC1/sec)	(metela)	(mred/yr)/(uCi/sec)	
ĸ	1036.	1036.	7.010E-06 6.757E-06	1036.	7.933E-06 7.649E-06	1036.	3.136E-04 2.785E-04	
	1378.	137B.	6.939E-06 6.629E-06		7.149E-06 6.860E-06	1378.	2.132E-04 1.903E-04	
ME	2							
NE	2408.	2408.	3.969E-06 3.767E-06		4.106E-06 3.897E-06		9.0948-05 8.1648-05	
ENE	4450.	4450.	2.442E-06 2.286E-06	4450.	2.384E-06 2.229E-06	4450.	3.540E-05 3.193E-05	
E	1996.	1996.	3.841E-06 3.671E-06	1996.	4.3108-06 4.0838-06	1996.	1.109E-04 9.929E-05	
ESE	1465.	1465.	5.762E-06 5.534E-06	5	6.599E-06 6.277E-06	1465.	1.612E-04 1.443E-04	
SE	969.	969.	6.641E-06 6.416E-06	•	8.978E-06 8.558E-06	969.	2.450E-04 2.185E-04	
SSE	838.	638.	6.364E-06 6.153E-06	838.	9.231E-06 8.769E-06	838.	2.418E-04 2.156E-04	
\$	829.	829.	5.333E+06 5.152E-06	829.	6.962E-06 6.627E-06	829.	2.476E-04 2.212E-04	
SSW	835.	835.	4.969E-06 4.793E-06	835.	6.598E-06 6.266E-06	835.	1.770E-04 1.582E-04	
SW	628.	628.	7.7982-06 7.5492-06		1.362E-05 1.285E-05	628.	4.090E-04 3.640E-04	
USW	533.	533.	8.245E-06 7.992E-06	533.	1.3262-05 1.2522-05	533.	4.447E-04 3.951E-04	
U	524.	524.	8.166E-06 7.919E-06	2	1.2208-05 1.1648-05		5.551E-04 4.911E-04	
WIN	643.	643.	5.715E-06 5.541E-06		7.885E-06 7.574E-06		4.444E-04 3.922E-04	
M	762.	762.	5.117E-06 4.958E-06		6.538E-06 6.303E-06		3.661E-04 3.233E-04	
					5.911E-06 5.708E-06		3.080E-04 2.725E-04	
HHU	690.	890.	5.340E-06 5.165E-06	OYU.	3.4116.00 3.1006.00	270.	3.000E-04 E.1E3E-04	



### Table F-7 (Continued)

### Maximum Offsite Finite Plume Gamma Dose Factors Based on 1 cm Depth at the Unrestricted Area Boundary for Xe-135m

Downwind I	mestricte	d Elevate	ed(Stack) Release	Mixed !	Mode(Yent) Release	Ground Level Release		
Direction	Area Bound	Redfus	s spar	Redius		Redius G GBAR		
	(meters)	(meters)	(mred/yr)/(uCi/sec)	(meters)	(mred/yr)/(uCi/sec)	(meters) (mrsd/yr)/(uCi/sdb)		
. N	1036.	1036.	1.3965-04 1.3495-04	1036.	1.598E-04 1.545E-04	1036. 1.531E-03 1.475E-03	j	
MIE	.1378.	1378.	1.151E-04 1.113E-04		1.274E-04 1.232E-04	1378. 1.019E-03 9.821E-04	6	
WE	2408.	2408.	5.077E-05 4.907E-0		5.129E-05 4.958E-05		5	
ENE	4450.	4450.	1.9198-05 1.8548-0		1.778E-05 1.718E-05	4450.: 8.758E-05 8.445E-05	j	
E	1996.	1996.	5.672E-05 5.483E-0		5.675E-05 5.486E-05		,	
ESE	1465.	1465.	1.005E-04 9.716E-0		1.0246-04 9.9026-05			
SE	969	969.	1.3898-04 1.3438-04		1.5758-04 1.5228-04			
					1.591E-04 1.538E-04	· · · · · · · · · · · · · · · · · · ·		
SSE	838.	838.	1.402E-04 1.356E-0					
S	829.	829.	1.183E-04 1.144E-0	<b>6 829.</b>	1.235E-04 1.194E-04			
SSU	835.	835.	1.104E-04 1.068E-0	6 835.	1.260E-04 1.218E-04	835. 8.762E-04 8.444E-04	ì	
SW	628.	628.	1.904E-04 1.841E-0	628.	2.444E-04 2.363E-04	628. 2.173E-03 2.094E-03	ı	
NSM	533.	533.	2.0638-04 1.9958-0		2.427E-04 2.345E-04	533. 2.479E-03 2.388E-03	,	
W	524.	524.	2.033E-04 1.966E-0		2.511E-04 2.427E-04		ı	
URU	643.	643.	1.3636-04 1.3186-0		1.687E-04 1.631E-04		ı	
*			·		1.423E-04 1.376E-04			
W	762.	762.					_	
MMM	890.	890.	1.161E-04 1.122E-0	<b>6 890.</b>	1.259E-04 1.217E-04	890. 1.48ZE-03 1.427E-03	,	



### Table F-7 (Continued)

Maximum Offsite Finite Plume Gamma Dose Factors Based on 1 cm Depth at the Unrestricted Area Boundary for Xe-135

Downwind Unrestricted Elevated(Stack) Release Direction Area Bound Radius S SBAR					Mode(Vent) Release V VBAR	Ground Level Release Redius G CEAR		
J11331131	(meters)		(mred/yr)/(uCl/sec)	Redius (neters)	(mred/yr)/(uCi/sec)		(mrad/yr)/(uCl/sec)	
	1036.	1036.	8.165E-05 7.902E-05	1036.	9.3876-05 9.0856-05	1036.	1.302E-03 1.257E-03	
MME	1378.	1378.	7.171E-05 6.940E-05	1378.	7.8212-05 7.5692-05	1378.	9.178E-04 8.866E-04	
NE	2408.	2408.	3.669E-05 3.550E-05		3.8762-05 3.7512-05	2408.	4.075E-04 3.937E-04	
ENE	4450.	4450.	1.928E-05 1.866E-05	4450.	1.899E-05 1.837E-05	4450.	1.625E-04 1.570E-04	
E	1996.	1996.	3.838E-05 3.714E-05		4.056E-05 3.925E-05		4.869E-04 4.704E-04	
ESE	1465.	1465.	6.171E-05 5.972E-05		6-539E-05 6-328E-05	1465.	7.073E-04 6.833E-04	
SE	969.	969.	7.953E-05 7.697E-05		9.346E-05 9.044E-05	969.	1.052E-03 1.017E-03	
SSE	838.	838.	7.845E-05 7.593E-05		9.367E-05 9.064E-05		1.037E-03 1.002E-03	
S	829.	829.	6.719E-05 6.503E-05		7.587E-05 7.342E-05		1.078E-03 1.041E-03	
55N	835.	835.	6.306E-05 6.103E-03		7.636E-05 7.389E-05		7.699E-04 7.438E-04	
511	628.	628.	1.039E-04 1.006E-04		1.409E-04 1.363E-04		1.729E-03 1.670E-03	
NZM	533.	533.	1.106E-04 1.071E-04		1.372E-04 1.328E-04		1.864E-03 1.801E-03	
W	524.	524.	1.082E-04 1.048E-04		1.374E-04 1.329E-04		2.256E-03 2.179E-03	
WW	643.	643.	7.5386-05 7.2966-05	,	9.395E-05 9.092E-05		1.775E-03 1.713E-03	
KN	762.	762.	6.654E-05 6.440E-05		8.098E-05 7.838E-05		1.466E-03 1.415E-03	
1001	890.	890.	6.671E-05 6.456E-05		7.327E-05 7.092E-05	1 7 7 7	1.247E-03 1.204E-03	

### Table F-7 (Continued)

Maximum Offsite Finite Plume Gamma Dose Factors Based on 1 cm Depth at the Unrestricted Area Boundary for Xe-137

			ed(Stack) Release		Hode(Vent) Release	Ground Level Release		
Direction	Area Bound		s sbar	Redius	A ABYE	Redius G GBAR ,		
	(meters)	(meters)	(mrad/yr)/(uCl/sec)	(meters)	(mred/yr)/(uCi/sec)	(meters) (mrad/yr)/(uCi/sec)		
	1036.	1036.	4.780E-05 4.627E-05	1036.	5.2426-05 5.0746-05	1036. 3.409E-04 3.298E-04		
NNE	1378.	1378.	3.585E-05 3.471E-05	1378.	3.814E-05 3.692E-05	1378. 1.975E-04 1.911E-04		
ME	2408.	2408.	1.153E-05 1.116E-05	2408.	1.052E-05 1.018E-05	2408. 3.979E-05 3.850E-05		
ENE	4450.	4450.	2.5128-06 2.4328-06	4450.	1.933E-06 1.871E-06	4450. 3.949E-06 3.821E-06		
E	1996.	1996.	1.420E-05 1.374E-05	1996.	1.2856-05 1.2446-05	1996. 5.599E-05 5.418E-05		
ESE	1465.	1465.	3.033E-05 2.936E-05	1465.	2.918E-05 2.825E-05	1465. 1.327E-04 1.284E-04		
SE	969.	969.	4.743E-05 4.591E-05	969.	5.188E-05 5.023E-05	969. : 2.989E-04 2.892E-04		
SSE	838.	838.	4.926E-05 4.769E-05	838.	5.357E-05 5.186E-05	838. 2.970E-04 2.874E-04		
S	829.	829.	4.072E-05 3.942E-05		3.9756-05 3.8496-05			
รรษ	835.	835.	3.5218-05 3.4088-05		3.424E-05 3.315E-05			
511	628.	628.	6.779E-05 6.563E-05	628.	7.9386-05 7.6856-05	TETT ITLET IN ATTICE IN		
nzn 22	533.	533.	7.919E-05 7.667E-05		8.829E-05 8.548E-05			
					9.608E-05 9.30ZE-05			
W	524.	524.	7.9908-05 7.7368-05		**			
unu	643.	643.	5.023E-05 4.863E-05		6.090E-05 5.896E-05			
873	762.	762.	4.160E-05 4.028E-05	762.	4.841E-05 4.687E-05			
\$1713	890.	890.	3.985E-05 3.858E-05	890.	4.152E-05 4.020E-05	890. 3.279E-04 3.172E-04		

Table F-7 (Continued)

### Maximum Offsite Finite Plume Gamma Dose Factors Based on 1 cm Depth at the Unrestricted Area Boundary for Xe-138

	inrestricted Area Bound		ed(Stack) Release S SEAR	Mixed   Redius	Mode(Vent) Release V VEAR	Ground Level Returne Redfus G GBAR		
Direction			(mrad/yr)/(uCl/sec)		(mrad/yr)/(uCl/sec)		(mrad/yr)/(upl/sec)	
	1036.	1036.	3.9262-04 3.8162-04	1036.	4.5236-04 4.3966-04	1036.	3.178E-03.3.084E-03	
MME	1378.	1378.	3.160E-04 3.071E-04	1378.	3.536E-04 3.437E-04	1378.	2.117E-03: Z.055E-03	
NE	2408.	2408.	1.356E-04 1.318E-04	2408.	1.379E-04 1.340E-04	2408.	7.244E-04:7.032E-04	
ENE	4450.	4450.	4.939E-05 4.799E-05	4450.	4.572E-05 4.443E-05	4450.	1.769E-04:3,718E-04	
E	1996.	1996.	1.540E-04 1.497E-04	1996.	1.535E-04 1.492E-04	1996.	8.921E-04 8.659E-04	
ESE	1465.	1465.	2.766E-04 2.689E-04	1465.	2.804E-04 2.725E-04		1.532E-03'1.487E-03	
SE	969.	969.	3.9386-04 3.8286-04	969.	4.408E-04 4.285E-04		2.641E-03 2.564E-03	
SSE	838.	838.	4.037E-04 3.924E-04		4.484E-04 4.358E-04		2.628E-03 2.551E-03	
352	829.	829.	3.457E-04 3.360E-04		3.560E-04 3.460E-04	829.	2.809E-03 2.727E-03	
ssv	835.	835.	3.277E-04 3.186E-04		3.8325-04 3.7246-04		1.8286-03 1.7746-03	
SV	628.	628.	5.698E-04 5.538E-04		7.209E-04 7.007E-04	628.	4.546E-03 4.412E-03	
USU	533.	533.	6.144E-04 5.973E-04		7.121E-04 6.921E-04		5.2062-03 5.0532-03	
ű	524.	524.	5.976E-04 5.809E-04	524.	7.318E-04 7.113E-04	524.	6.383E-03 6.195E-03	
WW	643.	643.	3.986E-04 3.875E-04	643.	4.887E-04 4.750E-04	643.	4.757E-03 4.616E-03	
NV.	762.	762.	3.457E-04 3.360E-04		4.1316-04 4.0166-04	762.	3.746E-03 3.635E-03	
WWW	890.	890.	3.330E-04 3.236E-04		3.626E-04 3.525E-04		3.069E-03 2.978E-03	

Table F-7 (Continued)

### Maximum Offsite Finite Plume Gamma Dose Factors Based on 1 cm Depth at the Unrestricted Area Boundary for Ar-41

Downwind Unrestricted Elevated(Steck) Release Direction Area Bound Radius S SBAR					Mode(Vent) Relesse V VEAR	Ground Level Release Redius G GBAR F		
	(meters)	(meters)	(mrad/yr)/(uCl/sec):	Redius (meters)	(mrad/yr)/(uCl/sec)	(meters)	(mrsd/yr)/(uCi/sec)	
<b>#</b> :-	1036.	1036.	4.746E-04 4.594E-04		5.528E-04 5.351E-04	1036.	4.557E-03 4.411E-03	
MME.	1378.	1378.	3.954E-04 3.828E-04		4.439E-04 4.297E-06		3.203E-03 3.101E-03	
NE.	2408.	2408.	1.925E-04 1.863E-04	2408.	2.045E-04 1.980E-04	2408.	1.387E-03 1.343E-03	
ENE	4450.	4450.	9.141E-05 8.846E-05	4450.	9.0616-05 8.7726-05	4450.	5.219E-04 5.052E-04	
E	1996.	1996.	2.110E-04 2.043E-04	1996.	2.180E-04 2.110E-04	1996.	1.658E-03 1.605E-03	
ESE	1465.	1465.	3.480E-04 3.368E-04	1465.	3.593E-04 3.478E-04	1465.	2.459E-03 2.381E-03	
SE	969.	969.	4.711E-04 4.560E-04		5.320E-04 5.149E-04	969.	3.715E-03 3.597E-03	
SSE	838.	838.	4.761E-04 4.608E-04		5.378E-04 5.206E-04		3.6718-03 3.5548-03	
33E \$	829.	829.	4.168E-04 4.035E-04		4.533E-04 4.388E-04		3.823E-03 3.701E-03	
-	835.	835.	3.9948-04 3.8668-04		4.930E-04 4.772E-04		2.700E-03 2.614E-03	
SSV		628.	6.711E-04 6.496E-04		8.5918-04 8.3168-04		6.139E-03 5.943E-03	
SV	628.		7.089E-04 6.862E-04		8.229E-04 7.966E-04		6.667E-03 6.453E-03	
hzn	533.	533.			8.291E-04 8.026E-04		8.057E-03 7.799E-03	
W	524.	524.	6.80ZE-04 6.584E-04					
unu	643.	643.	4.708E-04 4.558E-04	643.	5.716E-04 5.533E-04		6.300E-03 6.099E-03	
KV	762.	762.	4.123E-04 3.991E-04	762.	4.970E-04 4.811E-04	762.	5.1732-03 5.0082-03	
MMA	890.	890.	4.025E-04 3.896E-04	670.	4.447E-04 4.305E-04	890.	4.3742-03 4.2342-03	





Table F-7a

### Maximum Offsite Finite Plume Gamma Dose Factors Based on 1 cm Depth at the Restricted Area Boundary for Kr-83m

Downwind	mind Restricted Elevated(Stack) Release				Rode(Vent) Release	Ground Level Release		
Direction	Area Bound	Redius	S SBAR	Redius	Y VBAR	Redius	G GBAR	
	(meters)	(Beters)	(mrad/yr)/(uCi/xec)	(meters)	(mrad/yr)/(uCi/sec)	(merels)	(mrad/yr)/(uCi/sec)	
H	1036.	1036.	4.787E-07 3.609E-07	1036.	5.281E-07 3.982E-07	1036.	1.785E-04 1.346E-04	
MME	1378.	1378.	8.751E-07 6.599E-07	1378.	6.905E-07 5.206E-07	1378.	1.139E-04 8.586E-05	
KE	1609.	1609.	6.873E-07 5.182E-07	1609.	7.291E-07 5.497E-07	1609.	8.106E-05 6.112E-05	
ENE	1079.	1079.	4.160E-07 3.137E-07	1079.	8.010E-07 6.039E-07	1079.	1.322E-04 9.967E-05	
£	1055.	1055.	3.476E-07 2.621E-07	1055.	9.1818-07 6.9238-07	1055.	1.483E-04 1.118E-04	
ESE	1055.	1055.	4.371E-07 3.296E-07		1.175E-06 8.856E-07		1.3946-04 1.0516-04	
SÉ.	969.	969.	3.545E-07 2.673E-07	969.	1.267E-06 9.554E-07	969.	1.333E-04 1.005E-04	
SSE	698.	698.	2.415E-07 1.821E-07		1.646E-06 1.241E-06		1.773E-04 1.337E-04	
S	820.	820.	2.803E-07 2.114E-07		1.047E-06 7.895E-07		1.354E-04 1.021E-04	
SSU	835.	835.	3.165E-07 2.401E-07		1.071E-06 8.076E-07	835.	9.3266-05 7.0326-05	
SW	628.	628.	3.177E-07 2.395E-07		2.826E-06 2.131E-06	628.	2.305E-04 1.738E-04	
USV	533.	533.	2.617E-07 1.973E-07	533.	2.6748-06 2.0178-06	533.	2.568E-04 1.936E-04	
W	524.	524.	2.327E-07 1.754E-07	524.	1.658E-06 1.250E-06		3.352E-04 2.527E-04	
<b>LINU</b>	643.	643.	1.714E-07 1.29ZE-07	643.	7.235E-07 5.455E-07		2.728E-04 2.057E-04	
m	762.	762.	1.744E-07 1.315E-07	762.	4.3912-07 3.3112-07		2.219E-04 1.673E-04	
PETER	890.	890.	2.397E-07 1.807E-07	890.	3.334E-07 2.514E-07	890.	1.823E-04 1.374E-04	

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$$F_R = F_{Rb} \left[ \frac{R_o}{R} \right] = xp1.5$$

This analysis indicates that the change in range would increase the dose factor error by approximately 40%. Since this difference is well within the expected error of the current factors, no further adjustment in the above factors is considered necessary.

te: Based on Reference 1 of Section F.2 and the formulas in Sections B.5 and B.6 of Appendix B.

The restricted area boundary (RAB) was redefined in sectors E and ESE to 833 and 848 from 1055 and 1055 meters, respectively. As a result of this change of range, the dose factors were re-evaluated using the following equation. Here, F<sub>n</sub> is the resulting dose factor at the new range (i.e. 833). F<sub>n</sub>, is the value provided in the above ODCM tables (i.e. S, SBAR, V, VBAR, G, GBAR). R<sub>o</sub> is the former RAB distance (i.e. 1055), and R is the RAB distance (i.e. 833).

#### Maximum Offsite Finite Piume Gamma Dose Factors Based on 1 cm Depth at the Restricted Area Boundary for Kr-85m

Downstad	Restricted	Elevat	ed(Stack) Release	Mixed (	Mode(Vent) Release	Grou	nd Level Release	
Direction	Area Bound	Redius	S SEAR	Redius	V VBAR	Redfus	G GBAR (mred/yr)/(uC1/sec)	•
	(meters)	(matern)	(mrad/yr)/(uCi/sec)	(matern)	(mrad/yr)/(uCi/sec)	(metal.s)	(man) ALAL (mr. () sach	1
×	1036.	1036.	5.747E;05 5.560E-05	1036.	6.602E-05 6.388E-05	1036.	9.6606-04 9.2526-04	ſ
MME	1378.	1378.	5.063E-05 4.896E-05		5.514E-05 5.334E-05	1378.	6.776E-04 6.496E-04	
ME	1609.	1609.	3.6328-05 3.5128-05		3.847E-05 3.720E-05		5.003E-04 4.798E-04	
ENE	1079.	1079.	4.315E-05 4.174E-05	· · · · · · · · · · · · · · · · · · ·		1079.	7.345E-04 7.037E-04	•
E	1055.	1055.	4.5726-05 4.4246-0	1055.	5.053E-05 4.886E-05	1055.	8.134E-04 7.792E-04	,
ESE	1055.	t055.	5.730E-05 5.544E-05		6.298E-05 6.090E-05	1055.	8.020E-04 7.687E-04	,
SE	969.	969.	5.596E-05 5.415E-05	969.	6.610E-05 6.391E-05	969.	7.793E-04 7.470E-04	,
SSE	698.	698.	6.471E-05 6.263E-05		7.905E-05 7.643E-05	698.	9.815E-04 9.404E-04	,
\$	820.	820.	4.756E-05 4.603E-0		5.386E-05 5.208E-05	820.	8.103E-04 7.769E-04	,
SSW	835.	835.	4.422E-05 4.279E-05	835.	5.351E-05 5.174E-05	835.	5.684E-04 5.450E-04	,
SV	628.	628.	7.281E-05 7.046E-05		9.952E-05 9.618E-05	628.	1.285E-03 1.231E-03	
USU	533.	533.	7.757E-05 7.507E-0		9.7146-05 9.3886-05	533.	1.3896-03 1.3316-03	,
¥	524.	524.	7.601E-03 7.356E-0		9.705E-05 9.385E-05	524.	1.687E-03 1.614E-03	J
ww	643.	643.	5.286E-05 5.116E-0		6.615E-05 6.399E-05	643.	1.327E-03 1.270E-03	,
· KIN	762.	762.	4.668E-05 4.518E-0		5.688E-05 5.503E-05		1.094E-03 1.047E-03	ı
eney.	890.	890.	4.683E-05 4.532E-0		5.142E-03 4.976E-03	890.	9.2828-04 8.8858-04	,

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The restricted area boundary (RAB) was redefined in sectors E and ESE to 833 and 848 from 1055 and 1055 meters, respectively. As a result of this change of range, the dose factors were re-evaluated using the following equation. Here,  $F_R$  is the resulting dose factor at the new range (i.e. 833).  $F_{Re}$  is the value provided in the above ODCM tables (i.e. S, SBAR, V, VBAR, G, GBAR).  $F_R$  is the former RAB distance (i.e. 1055) and  $F_R$  is the RAB distance (i.e. 833).

$$F_R = F_R \left[ \frac{R_p}{R} \right] \exp 1.5$$

#### Maximum Offsite Finite Plume Gamma Dose Factors Based on 1 cm Depth at the Restricted Area Boundary for Kr-85

Downlind Restricted Elevated(Stack) Release			Mixed Mode(Vent) Release			Ground Level Release				
Direction	Area Sound (meters)	Radius (meters)	S (mred/yr)/(uC		Redius (meters)	V (mred/yr)/	VBAR (uCi/sec)	Redius (meters)	Q (mrad/yr)/	GBAR (uC1/sec)
. #	1036.	1036.	8.547E-07 8.2	265E+07.	1036	9.889E-07	9.5636-07	1036.	1.056E-05	1.021E-05
MME	1378.	1378.	7.309E-07 7.0	068E-07	1378.	8.077E-07	7.811E-07	1378.	7.4742-06	7.227E-06
NE	1609.	1609.	5.225E-07 5.	052E-07	1609.	5.615E-07	5.430E-07	1609.	5.559E-06	5.375E-06
ENE	1079.	1079.	6.463E-07 6.		1079.	6.707E-07	6.486E-07	1079.	8.057E-06	7.791E-06 ·
E	1055.	1055.	6.819E-07 6.		1055.	7.385E-07	7.142E-07	1055.	8.923E-06	8.628E-06
ESE	1055.	1055.	8.484E-07 8.		1055.		8.808E-07	1055.	8.805E-06	8.517E-06
SE	969.	969.	8.386E-07 8.		969.		9.267E-07	969.	8.555E-06	8.273E-06
SSE	678.	698.	9.869E-07 9.		698.	, ,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	1.115E-06	698.	1.072E-05	1.036E-05
S	820.	820.	7.333E-07 7.		820.		7.885E-07		8.866E-06	
SSN	835.	835.	6.857E-07 6.		835.		8.124E-07			6-063E-06
. SV	628.	628.	1.142E-06 1.		628.		1.444E-06			1.355E-05
USU	533.	533.	1.211E-06 1.		533.	••••	1.3862-06		**	1.460E-05
N2M			1.1728-06 1.		533. 524.		1.3958-06			1.763E-05
	524.	524.	8.185E-07 7.		643.		9.670E-07			1.389E-05
WW	643.	643.					1.4			1.148E-05
MM	762.	762.	7.192E-07 6.		762.		8.407E-07		177	
30774	890.	890.	7.1282-07 6.	9A7E-01	890.	7.849E-07	7.590E-07	890.	1.0115-03	9.778E-06

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The restricted area boundary (RAB) was redefined in sectors E and ESE to 833 and 848 from 1055 and 1055 meters, respectively. As a result of this change of range, the dose factors were re-evaluated using the following equation. Here,  $F_R$  is the resulting dose factor at the new range (i.e. 633).  $F_{Re}$  is the value provided in the above ODCM tables (i.e. S, SBAR, V, VBAR, G, GBAR).  $F_R$  is the former RAB distance (i.e. 1055) and  $F_R$  is the RAB distance (i.e. 833).

$$F_R = F_{R_0} \left( \frac{R_0}{R} \right) \exp 1.5$$

### Maximum Offsite Finite Plume Gamma Dose Factors Based on 1 cm Depth at the Restricted Area Boundary for Kr-87

	Restricted		ed(Steck) Release		Hode(Vent) Release		nd Level Release
Direction	Area Bound (meters)		\$ SBAR (mrad/yr)/(uCi/sec)	Redius (meters)	W VBAR (mrad/yr)/(uC1/sec)	Redius (meters)	G GEAR (mred/yr)/(uCl/sec)
'n	1036.	1036.	3.226E-04 3.135E-04	1036.	3.758E-04 3.652E-04	1036.	2.879E-03 2.795E-03
MIE	1378.	1378.	2.67ZE-04 2.597E-04	1378.	3.005E-04 2.920E-04	1378.	2.019E-03 1.960E-P3
HE	1609.	1609.	1.908E-04 1.853E-04		2.038E-04 1.981E-04	1609.	1.480E-03 1.437E-D3
ENE	1079.	1079.	2.430E-04 2.361E-04		2.534E-04 2.462E-04	1079.	2.1926-03 2.1296-03
E	1055.	1055.	2.601E-04 2.528E-04	1055.	2.785E-04 2.706E-04	1055.	2.423E-03 2.353E-03
ESE	1055.	1055.	3.217E-04 3.125E-04		3.412E-04 3.315E-04	1055.	2.407E-03 2.337E-03
SE	969.	969.	3.211E-04 3.120E-04		3.612E-04 3.510E-04	969.	2.355E-03 2.287E-03
SSE	698.	698.	3.885E-04 3.776E-04		4.423E-04 4.298E-04		2.985E-03 2.898E-03
S	820.	820.	2.881E-04 2.800E-04		3.117E-04 3.029E-04	820.	2.467E-03 2.396E-03
85W	835.	835.	2.742E-04 2.665E-04		3.400E-04 3.305E-04		1.706E-03 1.657E-03
SV	628.	628.	4.614E-04 4.484E-04		5.936E-04 5.769E-04		3.903E-03 3.790E-03
usu	533.	533.	4.880E-04 4.743E-04		5.683E-04 5.523E-04		4.251E-03 4.128E-03
¥	524.	524.	4.675E-04 4.543E-04		5.708E-04 5.547E-04		5-136E-03 4-986E-03
URV .	643.	643.	3.224E-04 3.133E-04		3.914E-04 3.804E-04		4.0012-03 3.8842-03
MA	762.	762.	2.823E-04 2.743E-04		3.397E-04 3.301E-04		3.2762-03 3.1802-03
Willia William	890.	890.	2.747E-04 2.669E-04		3.0312-04 2.9452-04		2.763E-03 2.683E-03

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The restricted area boundary (RAB) was redefined in sectors E and ESE to 833 and 848 from 1055 and 1055 meters, respectively. As a result of this change of range, the dose factors were re-evaluated using the following equation. Here,  $F_R$  is the resulting dose factor at the new range (i.e. 833).  $F_{Re}$  is the value provided in the above ODCM tables (i.e. S, SBAR, V, VBAR, G, GBAR).  $R_e$  is the former RAB distance (i.e. 1055) and R is the RAB distance (i.e. 833).

$$F_R = F_{R_0} \left[ \frac{R_0}{R} \right] = xp1.5$$

### Maximum Offsite Finite Plume Gamma Dose Factors Based on 1 cm Depth at the Restricted Area Boundary for Kr-88

Downlind Disection	Restricted Area Bound		ed(Stack) Release S SBAR	Mixed (	Mode(Vent) Release V VBAR	Grou Radius	nd Level Release G GBAR
- 11 cot(w)	(meters)		(mred/yr)/(uCi/sec)		(mrad/yr)/(uCi/sec)		(mrad/yr)/(uCl/sec)
Ħ	1036.	1036.	8.60ZE-04 8.374E-04	1036.	1.003E-03 9.769E-04	1036.	6.988E-03 6.787E-03
MME	1378.	1378.	7.111E-04 6.922E-04	1378.	7.989E-04 7.777E-04	1378.	-4.940E-03 4.798E-03
NE	1609.	1609.	5.087E-04 4.932E-04		5.485E-04 5.340E-04	1609.	£ 3.656E-03 3.552E-03
ENE	1079.	1079.	6.528E-04 6.355E-04		6.769E-04 6.589E-04	1079.	5.337E-03 5.184E-03
E	1055.	1055.	6.915E-04 6.732E-04		7.419E-04 7.222E-04	1055.	-5.907E-03 5.737E-03
ESE	1055.	1055.	8.514E-04 8.288E-04	•	9.030E-04 8.790E-04	1055.	: 5.857E-03 5.689E-03
SE	969.	969.	8.537E-04 8.311E-04		9.571E-04 9.317E-04	969.	5.712E-03 5.549E-03
SSE	698.	698.	1.034E-03 1.007E-03		1.1726-03 1.1416-03		17-193E-03 6-986E-03
S	820.	820.	7.7778-04 7.5718-04		8.513E-04 8.287E-04	820.	5.947E-03 5.777E-03
ssn	835.	835.	7.427E-04 7.231E-04		9.375E-04 9.127E-04		4.167E-03 4.048E-03
SV	628.	628.	1.246E-03 1.213E-03		1.601E-03 1.559E-03		9.396E-03 9.126E-03
nzn	533.	533.	1.314E-03 1.279E-03		1.525E-03 1.485E-03		1.017E-02 9.882E-03
• • •			******************		***************************************		******
u	524.	524.	1.249E-03 1.216E-03		1.520E-03 1.480E-03		1.225E-02 1.190E-02
Mu	643.	643.	8.669E-04 8.440E-04		1.045E-03 1.017E-03		9.595E-03 9.317E-03
(47)	762.	762.	7.580E-04 7.379E+04	762.	9.125E-04 8.884E-04	762.	7.895E-03 7.666E-03
RITTLE	890.	890.	7.369E-04 7.174E-04	870.	8.161E-04 7.945E-04	890.	6.693E-03 6.500E-03

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The restricted area boundary (RAB) was redefined in sectors E and ESE to 833 and 848 from 1055 and 1055 meters, respectively. As a result of this change of range, the dose factors were re-evaluated using the following equation. Here, F<sub>R</sub> is the resulting dose factor at the new range (i.e. 833). F<sub>R</sub> is the value provided in the above ODCM tables (i.e. S, SBAR, V, VBAR, G, GBAR). R, is the former RAB distance (i.e. 1055) and R is the RAB distance (i.e. 833).

$$F_R = F_R \left(\frac{R_p}{R}\right) = \infty 1.5$$



#### Table F-7a (Continued)

#### Maximum Offsite Finite Plume Gamma Dose Factors Based on 1 cm Depth at the Restricted Area Boundary for Kr-89

	Restricted Area Bound (meters)	Redius	ed(Steck) Release S SBAR (mred/yr)/(uG1/sec)	Redfus	Mode(Vent) Release V YBAR (mrad/yr)/(uCl/sec)	Ground Level Release Radius G GBAR (meters) (mrad/yr)/(uCl/sqb	<b>)</b>
. 16	1036.	1036.	3.904E-04 3.794E-04	1036.	4.258E-04 4.139E-04	1036. 2.051E-03 1.992E-	03
NNE	1378.	1378.	2.820E-04 2.741E-04	1378.	2.988E-04 2.904E-04		03
KE	1609.	1609.	1.750E-04 1.701E-04	1609.	1.654E-04 1.607E-04		
EXE .	1079.	1079.	2.703E-04 2.628E-04	1079.	2.619E-04 2.545E-04	1079. 1.450E-03 1.409E-	
E	1055.	1055.	3.041E-04 2.956E-04	1055.	2.972E-04 2.888E-04	1055. 1.5698-03 1.5248-	
ESE	1055.	1055.	3.931E-04 3.821E-04	1055.	3.909E-04 3.800E-04	1055. 1.682E-03 1.633E-	
SE	969.	969.	3.891E-04 3.782E-04	969.	4.188E-04 4.070E-04	*	
SSE	698.	698.	5.333E-04 5.184E-04	698.	5.7978-04 5.6348-04	177 7 77227 77 17117	-
33E \$	820.	820.	3.464E-04 3.367E-04	820.	3.3128-04 3.2198-04		
_			2.9218-04 2.8398-04		2.779E-04 2.702E-04		
SSM	835.	835.		835.			
211	628.	628.	5.830E-04 5.667E-04	628.	6.600E-04 6.415E-04		-
nzn	533.	533.	6.913E-04 6.720E-04	533.	7.5258-04 7.3148-04	533. 4.592E-03 4.460E-	03
W	· 524.	524.	6.961E-04 6.766E-04	524.	8.259E-04 8.028E-04	524. 5.967E-03 5.796E-	03
MIN	643.	643.	4.295E-04 4.174E-04	643.	5.147E-04 5.003E-04	643. 3.746E-03 3.638E-	03
1719	762.	762.	3.500E-04 3.402E-04	762.	4.035E-04 3.922E-04		
- MAN	890.	890.	3.301E-04 3.208E-04	890.	3.4152-04 3.3192-04		

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The restricted area boundary (RAB) was redefined in sectors E and ESE to 833 and 848 from 1055 and 1055 meters, respectively. As a result of this change of range, the dose factors were re-evaluated using the following equation. Here, F<sub>R</sub> is the resulting dose factor at the new range (i.e. 833). F<sub>Re</sub> is the value provided in the above ODCM tables (i.e. S, SBAR, V, VBAR, G, GBAR). R<sub>e</sub> is the former RAB distance (i.e. 1055) and R is the RAB distance (i.e. 833).

$$F_R = F_{Ro} \left( \frac{R_o}{R} \right) \exp 1.5$$

## Maximum Offsite Finite Plume Gamma Dose Factors Based on 1 cm Depth at the Restricted Area Boundary for Kr-90

Downlind Restricted Elevated(Stack) Release					Node(Vent) Release	Ground Level Release			
Direction	Area Bound (meters)		S SBAR	Redius	Y YEAR	Radius	G GBAR		
•	(mereta)	(mercis)	(mred/yr)/(uCi/sec)	(matala)	(mred/yr)/(uCi/sec)	(marela)	(mrad/yr)/(uCi/sec)		
. 10	1036.	1036.	6.785E-05 6.586E-05	1036.	5.199E-05 5.047E-05	1036.	8.2038-05 7.9548-05		
NYE	1378.	1378.	3.1956-05 3.1026-05	1378.	2.161E-05 2.098E-05	1378.	2.265E-05 2.196E-05		
ME	1609.	1609.	1.240E-05 1.203E-05		6.949E-06 6.745E-06	1609.	7.357E-06 7.134E-06		
ENE	1079.	1079.	3.718E-05 3.610E-05	1079.	2.538E-05 2.464E-05	1079.	4.577E-05 4.438E+05		
E	1055.	1055.	4.582E-05 4.448E-05		3.257E-05 3.162E-05	1055.	6.817E-05 6.610E-05		
ESE	1055.	1055.	6.315E-05 6.130E-05		5.071E-05 4.922E-05	1055.	1.0788-04 1.0468-04		
SE	969.	969.	5.843E-05 5.673E-05		5.324E-05 5.168E-05	989.	1.365E-04 1.324E-04		
SSE	698.	698.	1.170E-04 1.136E-04		1.103E-04 1.070E-04	698.	2.578E-04 2.500E-04		
\$	820.	820.	5.233E-05 5.081E-05		3.888E-05 3.775E-05	820.	1.108E-04 1.075E-04		
SSU	835.	835.	3.062E-05 2.972E-05		1.2746-05 1.2376-05	835.	1.8358-05 1.7798-05		
SW	628.	628.	9.754E-05 9.470E-05		6.538E-05 6.347E-05	628.	1.410E-04 1.368E-04		
MZM	533.	533.	1.892E-04 1.836E-04		1.525E-04 1.480E-04	533.	4-861E-04 4-713E-04		
V	524.	524.	2.165E-04 2.101E-04		2.185E-04 2.121E-04	524.	8.427E-04 8.170E-04		
MIN	643.	643.	1.018E-04 9.883E-05		1.0086-04 9.7876-05	643.	3.141E-04 3.045E-04		
MA	762.	762.	6.634E-05 6.440E-05		5.815E-05 5.645E-05	762.	1.306E-04 1.267E-04		
STATES.	890.	890.	5.725E-05 5.558E-05		4.336E-05 4.209E-05	890.	8.819E-05 8.551E-05		

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The restricted area boundary (RAB) was redefined in sectors E and ESE to 833 and 848 from 1055 and 1055 meters, respectively. As a result of this change of range, the dose factors were re-evaluated using the following equation. Here, F<sub>R</sub> is the resulting dose factor at the new range (i.e. 833). F<sub>Re</sub> is the value provided in the above ODCM tables (i.e. S, SBAR, V, VBAR, G, GBAR). R<sub>e</sub> is the former RAB distance (i.e. 1055) and R is the RAB distance (i.e. 833).

$$F_R = F_R \left(\frac{R_s}{R}\right) \exp 1.5$$

#### Table F-7a (Continued)

# Maximum Offsite Finite Plume Gamma Dose Factors Based on 1 cm Depth at the Restricted Area Boundary for Xe-131m

			ed(Stack) Release	Mixed	Mode(Vent) Release	Grou	nd Level Release
Direction	Area Bound (meters)	Redius (meters)	S SPAR (mrad/yr)/(uCi/sec)	Redius (meters)	W VBAR (mrad/yr)/(uCi/sec)	Radius (meters)	G GBAR (mrad/yr)/(uCl/sec)
N	1036.	1036.	1.606E-06 1.473E-06	1036.	1.827E-06 1.679E-06	1036.	1.645E-04 1.283E-04
MME	1378.	1378.	1.778E-06 1.572E-06	1378.	1.726E-06 1.553E-06	1378.	1.0726-04 8.3846-05
ME	1609.	1609.	1.327E-06 1.167E-06		1.409E-06 1.239E-06	1609.	7.747E-05 6.064E-05
ENE	1079.	1079.	1.254E-06 1.143E-06		1.612E-06 1.423E-06	1079.	1.225E-04 9.563E-05
£	1055.	1055.	1.249E-06 1.150E-06	1055.	1.806E-06 1.592E-06	1055.	1.376E-04 1.073E-04
ESE	1055.	1055.	1.566E-06 1.442E-06	1055.	2.270E-06 1.998E-06	1055.	1.298E-04 1.014E-04
SE	969.	969.	1.472E-06 1.365E-06	969.	2.406E-06 2.115E-06	969.	1.240E-04 9.696E-05
SSE	698.	698.	1.566E-06 1.476E-06		2.969E-06 2.597E-06		1.624E-04 1.267E-04
\$	820.	820.	1.238E-06 1.151E-06	820.	1.983E-06 1.742E-06		1.2536-04 9.6026-05
SSV	835.	835.	1.1968-06 1.1038-06	835.	2.0036-06 1.7556-06		8.798E-05 6.885E-05
SV	628.	628.	1.802E-06 1.691E-06	628.	4.3458-06 3.7288-06		2.109E-04 1.646E-04
NSN	533.	533.	1.859E-06 1.755E-06	533.	4.161E-06 3.577E-06	533.	2.324E-04 1.813E-04
Ü	524.	524.	1.800E-06 1.703E-06	524.	3.359E-06 2.972E-06	524.	3.000E-04 2.335E-04
WW	643.	643.	1.2638-06 1.1948-06		1.9768-06 1.7918-06		
1672	762.	762.	1.135E-06 1.069E-06		1.561E-06 1.437E-06	643. 743	2.446E-04 1.90ZE-04
MAT	890.	890.	1.191E-06 1.112E-06		1.363E-06 1.263E-06		2.005E-04 1.560E-04 1.664E-04 1.295E-04

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The restricted area boundary (RAB) was redefined in sectors E and ESE to 833 and 848 from 1055 and 1055 meters, respectively. As a result of this change of range, the dose factors were re-evaluated using the following equation. Here, F<sub>R</sub> is the resulting dose factor at the new range (i.e. 833). F<sub>Re</sub> is the value provided in the above ODCM tables (i.e. S, SBAR, V, VBAR, G, GBAR). R<sub>e</sub> is the former RAB distance (i.e. 1055) and R is the RAB distance (i.e. 833).

$$F_R = F_{R_0} \left(\frac{R_0}{R}\right) \exp 1.5$$

#### Table F-7a (Continued)

Maximum Offsite Finite Plume Gamma Dose Factors Based on 1 cm Depth at the Restricted Area Boundary for Xe-133m

Downwind	Restricted	Elevate	ed(Stack) Release	Mixed (	Node(Vent) Release		nd Level Release
Direction	Area Bound (meters)	Radius (meters)	S SBAR (mrad/yr)/(uCi/sec)	Redius (meters)	V VBAR (mrad/yr)/(uCi/sec)	Radius (meters)	G GBAR (mrad/yr)/(uG1/sec)
	1036.	1036.	8.557E-06 8.199E-06	1036.	9.814E-06 9.407E-06	1036.	2.822E-04 2.410E-04
MRE	1378.	1378.	7.917E-06 7.509E-06		8.400E-06 8.009E-06	1378.	1.901E-04 1.633E-04
NE	1609.	1609.	5.7292-06 5.4232-06	1609.	6.093E-06 5.768E-06	1609.	1.389E-04 1.195E-04 ·
ENE	1079.	1079.	6.486E-06 6.205E-06	1079.	7.141E-06 6.771E-06	1079.	2.1212-04 1.8152-04
E	1055.	1055.	6.770E-06 6.492E-06	1055.	7.917E-06 7.501E-06		2.368E-04 2.024E-04
ESE	1055.	1055.	8.481E-06 B.132E-06		9.879E-06 9.355E-06		2.2762-04 1.9512-04
SE	969.	969.	8.229E-06 7.903E-06		1.039E-05 9.834E-06	<del>9</del> 69.	2.189E-04 1.879E-04
SSE	698.	698.	9.363E-06 9.021E-06		1.250E-05 1.181E-05	698.	2.815E-04 2.409E-04
53E	820.	820.	6.991E-06 6.718E-06		8.532E-06 8.075E-06		2.236E-04 1.923E-04
_		835.	6.5418-06 6.2768-06		8.500E-06 8.036E-06		1.574E-04 1.354E-04
SSM	835.		1.0592-05 1.0202-05		1.637E-05 1.535E-05		3.668E-04 3.140E-04
5 <b>W</b>	628.	628.			1.588E-05 1.490E-05		4.005E-04 3.423E-04
usv	533.	533.	1.121E-05 1.081E-05				5.039E-04 4.287E-04
u	524.	. 524.	1.096E-05 1.056E-05		1.504E-05 1.427E-05		4.055E-04 3.441E-04
unu	643.	643.	7.648E-06 7.374E-06		9.956E-06 9.510E-06	643.	
MA	762.	762.	6.774E-06 6.526E-06	762.	8.435E-06 8.088E-06		3.334E-04 2.831E-04
RHIL	890.	890.	6.855E-06 6.594E-06	890.	· 7.588E-06 7.286E-06	890.	2.794E-04 2.377E-04

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The restricted area boundary (RAB) was redefined in sectors E and ESE to 833 and 848 from 1055 and 1055 meters, respectively. As a result of this change of range, the dose factors were re-evaluated using the following equation. Here,  $F_R$  is the resulting dose factor at the new range (i.e. 833).  $F_{Re}$  is the value provided in the above ODCM tables (i.e. S, SBAR, V, VBAR, G, GBAR).  $F_R$  is the former RAB distance (i.e. 1055) and R is the RAB distance (i.e. 833).

$$F_R = F_{R_0} \left[ \frac{R_0}{R} \right] = xp1.5$$

Maximum Offsite Finite Plume Gamma Dose Factors Based on 1 cm Depth at the Restricted Area Boundary for Xe-133

ind	Restricted	Flovet	ed(Stack) Release	Mixed I	Mode(Vent) Release	Grou	nd Level Release
	Area Sound	Redius	\$ 58AR (mred/yr)/(uCl/sec)	Redius	Y VBAR (mrad/yr)/(ucl/sep)	Redius (meters)	G GBAR (mrad/yr)/(uCi/sec)
ME NAS SE SE SE SE SE SE SE SE SE SE SE SE SE	1036. 1378. 1609. 1079. 1055. 1055. 969. 698. 820. 835. 628. 533. 524.	1036. 1378. 1609. 1079. 1055. 1055. 969. 698. 820. 835. 628. 533. 524.	7.010E-06 6.737E-06 6.939E-06 6.629E-06 5.088E-06 4.853E-06 5.306E-06 5.106E-06 5.535E-06 5.340E-06 7.016E-06 6.769E-06 6.641E-06 6.416E-06 7.217E-06 6.994E-06 5.369E-06 5.188E-06 4.769E-06 7.549E-06 7.798E-06 7.99ZE-06 8.245E-06 7.99ZE-06 8.166E-06 7.919E-06	1036. 1378. 1609. 1079. 1055. 1055. 969. 698. 820. 835. 628. 533.	7.933E-06 7.649E-06 7.149E-06 6.860E-06 5.323E-06 5.076E-06 6.045E-06 5.769E-06 6.764E-06 6.452E-06 8.566E-06 8.169E-06 8.978E-06 8.556E-06 1.073E-05 1.021E-03 7.024E-06 6.687E-06 6.598E-05 1.285E-03 1.326E-05 1.285E-03	1378. 1609. 1079. 1055. 1055. 969. 698. 820. 8 835. 6 628. 5 533.	3.136E-04 2.785E-04 2.132E-04 1.903E-04 1.562E-04 1.397E-04 2.362E-04 2.101E-04 2.632E-04 2.336E-04 2.543E-04 2.266E-04 2.450E-04 2.185E-04 3.132E-04 2.785E-04 1.770E-04 1.502E-04 4.090E-04 3.640E-04 4.447E-04 3.951E-04 5.551E-04 4.911E-04
MAT MA	762. 890.	762. 890.	5.117E-06 4.956E-06 5.340E-06 5.165E-06	762.	6.538E-06 6.303E-06 5.911E-06 5.708E-0		3.661E-04 3.233E-04 3.080E-04 2.725E-04

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The restricted area boundary (RAB) was redefined in sectors E and ESE to 833 and 848 from 1055 and 1055 meters, respectively. As a result of this change of range, the dose factors were re-evaluated using the following equation. Here, F<sub>R</sub> is the resulting dose factor at the new range (i.e. 833). F<sub>Re</sub> is the value provided in the above ODCM tables (i.e. S, SBAR, V, VBAR, G, GBAR). R<sub>e</sub> is the former RAB distance (i.e. 1055) and R is the RAB distance (i.e. 833).

$$F_R = F_{Ro} \left( \frac{R_o}{R} \right) \exp 1.5$$

### Maximum Offsite Finite Plume Gamma Dose Factors Based on 1 cm Depth at the Restricted Area Boundary for Xe-135m

	Restricted Area Bound (meters)		Mixed Mode(Vent) Release Redius V VBAR (meters) (mrad/yr)/(uCi/sec)	Ground Level Release Redius G GBAR (meters) (mred/yr)/(uCi/sec)
H HE HE EXE SSE SSU SSU SSU SSU SSU SSU SSU SSU SS	1036. 1378. 1609. 1079. 1055. 1055. 969. 698. 820. 835. 628. 533. 524. 643. 762.	1036. 1.396E-04 1.349E-04 1.13E-04 1.113E-04 1.113E-05 1.15E-04 1.113E-06 1.079. 1.024E-06 9.890E-07 1055. 1.121E-04 1.084E-07 1055. 1.411E-04 1.365E-07 1.3	1378. 1.274E-04 1.232E-04 1609. 8.260E-05 7.985E-05 1079. 1.064E-04 1.028E-04 1055. 1.183E-04 1.44E-04 1055. 1.490E-04 1.441E-04 1.522E-04 1.522E-04 1.525E-04 1.522E-04 1.525E-04 1.209E-04 1.251E-04 1.209E-04 1.251E-04 1.218E-04 1.251E-04 1.236E-04 1.251E-04 1.236E-04 1.251E-04 1.236E-04 1.251E-04 1.2363E-04 1.251E-04 1.376E-04 1.423E-04 1.376E-04	1378. 1.019E-03 9.821E-04 1609. 7.033E-04 6.778E-04 1079. 1.147E-03 1.105E-03 1055. 1.253E-03 1.207E-03 1055. 1.256E-03 1.211E-03 969. 1.262E-03 1.216E-03 698. 1.667E-03 1.606E-03 820. 1.363E-03 1.314E-03 835. 8.762E-04 8.444E-04 628. 2.173E-03 2.094E-03 533. 2.479E-03 2.388E-03 524. 3.050E-03 2.937E-03 643. 2.286E-03 2.201E-03 762. 1.806E-03 1.739E-03

LASALLE SITE METEOROLOGICAL DATA 1/78 - 12/87

The restricted area boundary (RAB) was redefined in sectors E and ESE to 833 and 848 from 1055 and 1055 meters, respectively. As a result of this change of range, the dose factors were re-evaluated using the following equation. Here, F<sub>R</sub> is the resulting dose factor at the new range (i.e. 833). F<sub>Re</sub> is the value provided in the above ODCM tables (i.e. S, SBAR, V, VBAR, G, GBAR). R<sub>e</sub> is the former RAB distance (i.e. 1055) and R is the RAB distance (i.e. 833).

$$F_R = F_{Ro} \left[ \frac{R_o}{R} \right] \exp 1.5$$

#### Maximum Offsite Finite Plume Gamma Dose Factors Based on 1 cm Depth at the Restricted Area Boundary for Xe-135

Downwind	Restricted	Elevate	rd(Stack) Release		Hode(Vent) Release	Release Ground Level Release				
Direction	Area Bound		s SBAR	Redius	Y YBAR	Redius	•			
j	(meters)	(meters)	(mrad/yr)/(uG1/sec)	(meters)	(mrad/yr)/(uCi/sec)	(meters)	(mred/yr)/(uC1/sec),			
			•							
• 🙀	1036.	1036.	8.165E-05 7.902E-05	1036.	9.387E-05 9.085E-05	1036.	1.302E-03 1.257E-03			
MME	1378.	1378.	7.1712-05 6.9402-05	1378.	7.821E-05 7.569E-05	1378.	9.178E-04 8.866E-04			
NE	1609.	1609.	5.140E-05 4.974E-05	1609.	5.463E-05 5.286E-05	1609.	5.801E-04 6.570E-04			
ENE	1079.	1079.	6.139E-05 5.942E-05		6.476E-05 6.267E-05	1079.	9.912E-04 9.573E-04			
Ē	1055.	1055.	6.493E-05 6.284E-05		7.155E-05 6.924E-05	1055.	1.097E-03 1.060E-03			
_	1055.	1055.	8.130E-05 7.869E-05		8.905E-05 8.617E-05	1055.	.1.083E-03 1.046E-03			
ESE							1.052E-03 1.017E-03			
SE	969.	969.	7.953E-05 7.697E-05		9.346E-05 9.044E-05	969.	******			
SSE	698.	698.	9.205E-05 8.910E-05	698.	1.117E-04 1.081E-04		1.321E-03 1.276E-03			
\$	820.	820.	6.782E-05 6.564E-05	820.	7.666E-05 7.419E-05	820.	1.093E-03 1.056E-03			
SSW	835.	835.	6.306E-05 6.103E-05		7.636E-05 7.389E-05	835.	:7.699E-04 7.438E-04			
SW	628.	628.	1.039E-04 1.006E-04		1.409E-04 1.363E-04	628.	1.729E-03 1.670E-03			
นรม	533.	533.	1.106E-04 1.071E-04		1.372E-04 1.328E-04		1.8646-03 1.8016-03			
u u	524.	524.	1.082E-04 1.046E-04		1.374E-04 1.329E-04		2.256E-03 2.179E-03			
							1.775E-03 1.713E-03			
MM	643.	643.	7.538E-05 7.296E-05		9.395E-05 9.092E-05					
m	762.	762.	6.654E-05 6.440E-05		8.098E-05 7.838E-05		1.466E-03 1.415E-03			
MMA	890.	890.	6.671E-05 6.456E-05	890.	7.327E-05 7.092E-05	890.	1.247E-03 1.204E-03			

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The restricted area boundary (RAB) was redefined in sectors E and ESE to 833 and 848 from 1055 and 1055 meters, respectively. As a result of this change of range, the dose factors were re-evaluated using the following equation. Here, F<sub>n</sub> is the resulting dose factor at the new range (i.e. 833). F<sub>n</sub> is the value provided in the above ODCM tables (i.e. S, SBAR, V, VBAR, G, GBAR). R<sub>n</sub> is the former RAB distance (i.e. 1055) and R is the RAB distance (i.e. 833).

$$F_R \sim F_{R_0} \left[ \frac{R_0}{R} \right] \exp 1.5$$

Maximum Offsite Finite Plume Gamma Dose Factors Based on 1 cm Depth at the Restricted Area Boundary for Xe-137

-	Restricted Area Bound (meters)	Redfus	ed(Stock) Rolesso S SHAR (mrad/yr)/(uGf/sec)	Redius	Hode(Yent) Release Y YBAR (mrad/yr)/(uCi/sec)	Radius	nd Level Release  G GBAR (mrad/yr)/(uCi/sec)
	1036.	1036.	4.780E-05 4.627E-05	1036.	5.24ZE-05 5.074E-05	1036.	3.409E-04 3.298E-04
. NAE	1378.	1378.	3.5858-05 3.4718-05	1378.	3.814E-05 3.692E-05		1.975E-04 1.911E-04 '
NE	1609.	1609.	2.282E-05 2.209E-05	1609.	2.185E-05 2.115E-05		1.166E-04 1.128E-04
	1079.	1079.	3.3428-05 3.2368-05	1079.	3.282E-05 3.177E-05		2.437E-04 2.358E-04.
ENE	1055.	1055.	3.7412-05 3.6222-05	1055.	3.716E-05 3.597E-05		2.625E-04 2.540E-04
E	1055.	1055.	4.8278-05 4.6738-05	1055.	4.871E-05 4.715E-05		2.765E-04 2.676E-04
ESE	969.	969.	4.7436-05 4.5916-05		5.188E-05 5.023E-05		2.989E-04 2.892E-04
SZE.	698.	698.	6.2736-05 6.0736-05		6.983E-05 6.760E-05		4.329E-04 4.189E-04
	820.	820.	4.133E-05 4.002E-05		4.042E-05 3.913E-05		3.373E-04 3.264E-04
\$			3.521E-05 3.408E-05		3.424E-05 3.315E-05		1.748E-04 1.691E-04
SSN	835.	835.	6.779E-05 6.563E-05		7.938E-05 7.685E-05		5.333E-04 5.161E-04
SV	628.	628.	7.9198-05 7.6678-05		8.829E-05 8.548E-05		7.164E-04 6.932E-04
nzn	533.	533.	7.9908-05 7.7368-05		9.608E-03 9.302E-05		9.223E-04 8.924E-04
W	524.	524. 643.	5.0238-05 4.8638-05		6.090E-05 5.896E-05		6.002E-04 5.808E-04
unu un	643. 762.	762.	4.160E-05 4.028E-05	2 :	4.841E-05 4.687E-05		4.228E-04 4.090E-04
67874 17874	890.	870.	3.985E-05 3.858E-05		4.152E-05 4.020E-05		3.279E-04 3.172E-04

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The restricted area boundary (RAB) was redefined in sectors E and ESE to 833 and 848 from 1055 and 1055 meters, respectively. As a result of this change of range, the dose factors were re-evaluated using the following equation. Here, F<sub>R</sub> is the resulting dose factor at the new range (i.e. 833). F<sub>Re</sub> is the value provided in the above ODCM tables (i.e. S, SBAR, V, VBAR, G, GBAR). R<sub>e</sub> is the former RAB distance (i.e. 1055) and R is the RAB distance (i.e. 833).

$$F_R = F_{Ro} \left( \frac{R_o}{R} \right) \exp 1.5$$

#### Maximum Offsite Finite Plume Gamma Dose Factors Based on 1 cm Depth at the Restricted Area Boundary for Xe-138

	Restricted	_	ed(Stock) Release		Mode(Vent) Release	Ground Level Release Radius G GBAR			
Direction	Area Bound (meters)		s SBAR (mrad/yr)/(uCi/sec)	Redius (meters)	<pre>v VBAR (mrad/yr)/(uCi/sec)</pre>	Radius (meters)	(mred/yr)/(uC1/sec)		
	1036.	1036.	3.9262-04 3.8162-04	1036.	4.523E-04 4.396E-04	1036.	3.178E-03 3.084E-03		
MRE	1378.	1378.	3.160E-04 3.071E-04	1378.	3.536E-04 3.437E-04	1378.	2.117E-03 2.055E-03		
NE	1609.	1609.	2.198E-04 2.136E-04	1609.	2.272E-04 2.208E-04	1609.	1.457E-03 1.414E-03		
EKE	1079.	1079.	2.887E-04 2.806E-04	1079.	2.996E-04 2.91ZE-04	1079.	2.383E-03 2.313E-03		
E	1055.	1055.	3.167E-04 3.079E-04	1055.	3.323E-04 3.230E-04	1055.	2.600E-03 2.524E-03		
ESE	1055.	1055.	3.961E-04 3.850E-04		4.149E-04 4.032E-04	1055.	2.618E-03 2.541E-03		
SE SE	969.	969.	3.938E-04 3.828E-04		4.408E-04 4.285E-04		2.641E-03 2.564E-03		
			4.9116-04 4.7736-04		5.540E-04 5.384E-04		3.494E-03 3.391E-03		
SSE	678.	698.			3.606E-04 3.505E-04		2.857E-03 2.773E-03		
\$	820.	820.	3.498E-04 3.400E-04				1.8282-03 1.7742-03		
ssu	835.	835.	3.277E-04 3.186E-04		3.832E-04 3.724E-04				
SU	628.	628.	5.698E-04 5.538E-04	628.	7.209E-04 7.007E-04		4.546E-03 4.412E-03		
MSM	533.	533.	6.144E-04 5.973E-04	533.	7.121E-04 6.921E-04		5.206E-03 5.053E-03		
U	524.	524.	5.976E-04 5.809E-04	524.	7.316E-04 7.113E-04	524.	6.383E-03 6.195E-03		
MIN	643.	643.	3.986E-04 3.875E-04		4.887E-04 4.750E-04	643.	4.757E-03 4.616E-03		
MA MA	762.	762.	3.457E-04 3.360E-04		4.131E-04 4.016E-04		3.746E-03 3.635E-03		
MAT	890.	890.	3.3306-04 3.2366-04		3.626E-04 3.525E-04	890.	3.069E-03 2.978E-03		

LASALLE SITE METEOROLOGICAL DATA 1/78 - 12/87

The restricted area boundary (RAB) was redefined in sectors E and ESE to 833 and 848 from 1055 and 1055 meters, respectively. As a result of this change of range, the dose factors were re-evaluated using the following equation. Here,  $F_n$  is the resulting dose factor at the new range (i.e. 833).  $F_{ne}$  is the value provided in the above ODCM tables (i.e. S, SBAR, V, VBAR, G, GBAR).  $P_n$  is the former RAB distance (i.e. 1055) and  $P_n$  is the RAB distance (i.e. 833).

$$F_R \sim F_{R_0} \left(\frac{R_0}{R}\right) \exp 1.5$$

# Maximum Offsite Finite Plume Gamma Dose Factors Based on 1 cm Depth at the Restricted Area Boundary for Ar-41

	Restricted Area Sound (meters)	Redius	ed(Stock) Release S SBAR (mrad/yr)/(uCi/sec)	Redius	Hode(Vent) Release V YBAR (mrmd/yr)/(uCi/sec)	Radius	nd Level Release G GBAR (mrad/yr)/(uCl/sec)
MANN MANN MANN MANN MANN MANN MANN MANN	1036. 1378. 1609. 1079. 1055. 1055. 969. 698. 820. 835. 628. 533. 524. 643. 762.	1036. 1378. 1609. 1079. 1055. 1055. 969. 698. 835. 628. 533. 524. 643. 762.	4.746E-04 4.594E-04 3.954E-04 3.828E-04 2.825E-04 2.734E-04 3.582E-04 3.466E-04 4.725E-04 4.574E-04 4.711E-04 4.560E-04 5.672E-04 5.490E-04 4.212E-04 4.077E-04 3.994E-04 3.866E-04 6.711E-04 6.496E-04 7.089E-04 6.862E-04 4.708E-04 4.558E-04 4.708E-04 3.991E-04 4.025E-04 3.896E-04	1079- 1055- 1055- 969- 698- 820- 835- 628- 533- 524- 643- 762-	5.716E-04 5.533E-0 4.970E-04 4.811E-0	1378. 1609. 1079. 1055. 1055. 1055. 1055. 1055. 1059.	4.557E-03 4.411E[03 3.203E-03 3.101E-03 2.558E-03 2.283E-03 3.472E-03 3.361E-03 3.841E-03 3.718E-03 3.807E-03 3.685E-03 3.715E-03 3.597E-03 4.695E-03 4.545E-03 3.879E-03 2.614E-03 6.139E-03 5.943E-03 6.667E-03 6.453E-03 6.057E-03 7.799E-03 6.300E-03 6.099E-03 5.173E-03 4.234E-03

LASALLE SITE METEOROLOGICAL DATA 1/78 - 12/87

The restricted area boundary (RAB) was redefined in sectors E and ESE to 833 and 848 from 1055 and 1055 meters, respectively. As a result of this change of range, the dose factors were re-evaluated using the following equation. Here,  $F_R$  is the resulting dose factor at the new range (i.e. 833).  $F_{Re}$  is the value provided in the above ODCM tables (i.e. S, SBAR, V, VBAR, G, GBAR). R, is the former RAB distance (i.e. 1055) and R is the RAB distance (i.e. 833).

$$F_R = F_{Ro} \left( \frac{R_o}{R} \right) \exp 1.5$$

# Table F-8 Parameters for Calculations of N-16 Skyshine Radiation From LaSalle

Location Number k	Activity	Occupancy Hours OH <sub>x</sub> *	Occupancy Factor OF <sub>t</sub>	Shielding Factor SF <sub>t</sub>	Distance R <sub>k</sub> (m)
1	Living at home (nearest resident)	8360	0.95	0.7	1100
2	Fishing	400	0.05	1.0	2100
3	Living at the National Guard Facility	2500		0.7	2400

M<sub>h</sub> = 5 K = 2.28E-05 mrem/(MWe-hr)

These parameters are used to obtain an initial estimate of skyshine dose to the maximally exposed member of the public using Equation A-34 in Appendix A. If desired, more realistic parameters could be used in place of these to refine the estimate. For example, one could determine whether the nearest resident really fishes the specified number of hours at the specified location.

a The amount of time in a year that a maximally exposed fisherman would spend fishing near the site is estimated as 12 hours per week for 8 months per year. This yields an estimate of:

[12 hours/week] [(8 months/yr)/(12 months/yr)]  $\times$  [52 weeks/yr] = 416 hours/yr

The remaining time is assumed to be spent at the nearest residence.

- b Distance to nearest residence (See Table F-3).
- c The  $OF_k$  is the quotient of the number of hours a location is occupied and the number of hours in a year. Thus  $OH_k/8760$  hours =  $OF_k$  rounded to the 0.01 digit.

In determining the maximally exposed individual, the following possibilities were considered: the nearest resident, fishermen, and persons at the National Guard facility north of the site. The annual exposure time and location of a maximally exposed fisherman were estimated on the basis of discussion with a member of the station staff. The nearest resident was found to have the greatest exposure to skyshine. For details, see Reference 2 of Section F.2.



### Elevated Level Joint Frequency Distribution Table Summary

#### 375 Foot Elevation Data

Summe	ry Tab	le of P	ercent .	by Dire	ation #	nd Cles	•								:		
Cless	N	MME	NE	ENE	E	ESE	SE	352	\$	ZZA	ZA	ASA	`₩	WNW	M	ISM	Total
A B C D E F	.024 .149 .300 2.100 1.018 .320	.032 .175 .262 2.634 .913 .182	.067 .227 .351 3.282 1.162 .248	.057 .149 .255 3.192 1.431 .260	.062 .080 .138 2.780 1.823 .469	.040 .047 .069 1.945 1.495 .707	.030 .056 .104 1.767 1.460 .905	.060 .070 .130 2.053 1.752 .995 .507	2.867	463 .579 .2.875 2.978 1.735	2.124 1.561 .550	.460	1.875 1.012 .309	.064 .192 .420 4.533 2.065 1.099	.063 f. 163 .329 3.922 1.670 .894 .217	.024 .163 .332 3.681 1.196 .553	.942 2.843 4.805 46.851 27.061 .13.438 4.358
Total	•	4.237	6.359	5.356	5.394	4.385	4.601	5.567	8.474	9.457	7.487	6.093	6.688	8.615	7.248	6.073	100,000

### Summary Table of Percent by Direction and Speed

\$peed	H	MME	NE	ENE		ESE	SE	SSE	\$	\$\$W	SW	WSW	W	MM	M	INIM	Total
.45 1.05 2.05 2.05 4.05 5.05 6.05 10.05 13.05 18.00	.018 .016 .162 .381 .808 .489 .577 1.297 .912 .482 .120 .002	.017 .033 .260 .479 .647 .598 .599 .918 .421 .055 .000	.015 .030 .278 .551 .785 .792 .861 1.353 .487 .183 .026	.231	.008 .021 .147 .369 .494 .451 .508 1:207 .998 .328 .011	.010 .023 .149 .287 .428 .403 .419 .972 .751 .692 .240 .011	.013 .032 .159 .311 .437 .420 .479 .989 .736 .749 .283 .013	.459	-	.010 .017 .168 .317 .455 .489 .584 1.500 1.552 2.440 1.215 .109	.000 .017 .155 .272 .428 .492 .523 1.371 1.326 1.822 1.043 .038	.013 .028 .135 .302 .400 .472 .487 1.164 1.086 1.338 .581 .085	.000 .021 .147 .321 .387 .493 .856 1.207 1.240 1.432 .746 .137	.000 .024 .115 .217 .482 .540 .598 1.622 1.671 1.962 1.137 .147	.001 .034 .136 .302 .487 .642 .668 1.659 1.428 .404 .019	.000 .027 .160 .311 .455 .632 .656 1.623 1.270 .800 .222 .018	.137 .402 2.721 5.699 7.798 8.213 9.150 20.637 17.188 16.286 9.183 708

NOTE: Wind directions in tables are presented in "wind from" and not "wind to" direction.

## Supplemental Table A -Continued

## Elevated Level Joint Frequency Distribution Table Summary

### 375 Foot Elevation Data

## Summary Table of Percent by Speed and Glass

Class Speed	A	8	C	D	• E	•	
.45 1.05 2.05 3.05 4.05 5.05 6.05 8.05 10.05 13.05 18.00	.000 .001 .017 .046 .102 .108 .225 .141 .134	.000 .004 .041 .169 .249 .335 .341 .701 .429 .404	.000 .004 .109 .290 .499 .547 .565 1.116 .785 .258	.052 .176 1.540 3.269 4.364 4.159 4.663 10.191 7.441 6.977 3.424 .398	.058 .153 .658 1.193 1.629 1.945 2.320 6.190 4.924 5.670 3.126	.023 .060 .307 .547 .788 .916 .986 2.460 2.591 3.206 1.511	.004 .005 .050 .096 .166 .210 .268 .755 .675 .615

# Mid Elevation Joint Frequency Distribution Table Summaries

Summa	ery Tabi	le of P	ercent (	by Dire	ction s	nd Class	200	Foot Ele	vation D	ata		: *			<b>.</b>	NAM	Total
Class	N	NNE	NE	ENE		ESE	SE	SSE	,· \$	SSM	24	AZA	. 🕊	WW.	i MM		10000
A BC D E F	.381 .313 .531 2.274 .777 .233	.248 .249 .420 2.315 .734	.801 .377 .566 2.517 1.088	.790 .343 .434 2.248 1.105 .205	.531 .290 .390 2.669 1.486 .433	.256 .175 .289 1.715 1.323 .809	.142 .110 .321 1.677 1.243 .802 .835	.119 .104 .282 1.775 1.436 .801	.231 .207 .370 2.781 2.678 1.210	.357 .288 .498 2.045 2.910 1.363 1.239	.441 .327 .479 2.098 1.697 1.183 .927	.370 .292 .470 1.839 1.176 .862 .689	.453 .350 .508 2.140 1.228 .854 .740	.683 .498 .573 3.069 1.712 1.017 .776	.579 .530 .710 2.641 1.429 1.648 .562	.678 .612 .785 2.408 1.015 .446	7.030 5.062 7.634 37.410 23.034 11.419 8.411
G Total	.085 4.575	.060	.021	. 5. 138		•		5.413	8.722	9.721	7.219	5.698	6.268	8.297	7.498	6.094	100.000

Summary Table of Percent by Direction and Speed .

Speed	N	NNE	NE	ENE	E	ESE	SE	SSE	S	SSM	SW	MZM		WHW	MA	HW	Total
.45 1.05 2.05 3.05 4.05 6.05 6.05 8.05 10.05 13.05 13.05	.043 .046 .219 .442 .536 .681 .729 1.088 .472 .202 .111 .007	.003 .072 .575 1.132 .970 .584 .383 .339 .108 .015 .001	.000 .083 .500 1.140 1.375 1.041 .670 .578 .153 .029 .001 .000	.020 .042 .323 .691 .729 .800 .802 1.004 .475 .214 .034 .004	.015 .033 .233 .497 .617 .639 .777 1.657 .801 .809 .177 .001	.003 .025 .197 .350 .528 .533 .728 1.351 .691 .348 .087 .000	.005 .040 .202 .399 .545 .635 .708 1.333 .690 .296 .076	.009 .034 .201 .363 .532 .558 .681 1.426 1.015 .476 .113 .005	.005 .037 .232 .366 .599 .621 .843 2.234 2.122 1.342 .310 .010	.000 .021 .193 .344 .583 .610 .867 2.473 2.439 1.778 .383 .009	.008 .028 .201 .339 .557 .579 .698 1.707 1.012 .154 .014	.000 .038 .189 .353 .486 .560 .687 1.494 1.106 .626 .159 .030	.000 .031 .183 .413 .461 .590 .695 1.604 1.108 .790 .300 .074	.000 .026 .151 .374 .553 .686 .933 1.586 1.414 .683 .074	.000 .034 .153 .366 .630 .737, .940 1.903 1.315 1.096 .312 .013	.000 .046 .163 .374 .616 .720 .916 1.559 .910 .580 .203 .004	.113 .612 3.915 7.946 10.319 10.893 11.959 23.790 16.693 10.728 3.086 .247

NOTE:

Wind directions in tables are presented in "wind from" and not "wind to" direction.



# Supplemental Table B - Continued

# Mid Elevation Joint Frequency Distribution Table Summaries

## 200 Foot Elevation Data

# Summery Table of Percent by Speed and Class

	• •						_
Class.	A		C.	P	. E	F	Q
		<u> </u>	٠, ,				
Speed:		ĭ	•		•		
		:			-007	.021	.009
.45	.000	.000	.001	.046	.037		
		.004	.022	.219	. 175	. 116	.083
1.05	.013	• :			.732	.437	.207
2.05	. 172	. 130	.291	1.946			.378
	.600	.453	.809	3.533	1.631	.642	•
3.05	•	• •	•	4.134	2.329	-930	.591
4.05	.776	.688	.970			1.150	.690
6.05	.828	.588	.966	3.915	2.455	* * *	-
	<u> </u>	. 633	.021	4.389	2.742	1.461	1.079
6.05	.835			8.019	6,377	3.357	2.616
8.05	1.542	1.208	1.671				2.160
10.05	1.030	.780	-979	5.271	4.164	2.319	
		• • • • • • • • • • • • • • • • • • • •	.784	4.155	2.854	.935	.697
13.05	.874	.558				.048	.020
18.00	.331	. 207	1231	1.621	630		
			1018	: 162	.020	.005	.001
49.00	.029	.012	///	.,	••	-	

## Supplemental Table C

# Ground Level Joint Frequency Distribution Table Summary

### 33 Foot Elevation Data

Summe	ery Teb	le of P	ercent (	by Dire	ation a	nd Cless	ı								HV	NAM	Total
Cless	N	ME	NE.	ENE	E	ESE	SE	<b>325</b>	\$	22A	· SW	WSW		कारक .	, fra	,	, = 0 = 1
A B C D E F G	.411 .314 .380 3.149 1.131 .166	.318 .150 .233 1.449 .661 .087	.689 .278 .330 2.178 1.168 .177	.887 .310 .328 2.604 1.021 .160	.594 .276 .262 2.687 1.758 .646	.308 .177 .270 1.735 1.434 .840	.133 .108 .189 1.677 1.303 .780 .673	.135 .071 .172 1.540 1.561 .617	1.259 1.183	2.673 2.795 1.280 1.050	.998	.447 .222 .343 1.925 1.480 1.039	.532 .293 .380 2.243 1.557 1.048 .925	.405 .405 .507 3.240 1.945 .867	1.692 .609 .214	.904 .501 .501 2.509 .917 .378 .093	7.982 4.288 5.628 37.051 24.947 11.499 8.627
Total	5.570	2.906	4:836	5.235	6.349	5.379	4.932	5.319	7.862	8.829	7.690	6.422	6.979	8.118	7.771	5,803	100.000

### Summery Table of Percent by Direction and Speed

															•	• .
Speed	. N	ME	ne en	E . E	ESE .	SE	SSE	\$	55 <b>W</b>	SW	WSW	<b>W</b>	MNM	, W	WW	Totel
.45 1.05 2.05 3.05 4.05 5.05 6.05 8.05 10.05 12.05 12.05	.000 .052 .378 1.124 1.328 1.129 .667 .628 .145 .114 .008	.004 .048 .609 1.183 .621 .247 .091 .102 .002 .000	.000 .00 .073 .04 .813 .51 1.802 1.26 1.122 1.23 .617 1.10 .297 .59 .106 .42 .006 .04 .000 .00	6 .056 7 .424 8 1.191 0 1.420 8 1.189 7 .879 2 .817 2 .303 2 .067 2 .000	.000 .058 .601 1.270 1.116 .694 .551 .767 .227 .093 .004	.000 .092 .686 1.276 1.058 .642 .509 .480 .172 .056 .002	.002 .073 .582 1.222 1.079 .738 .866 .642 .289 .094 .012	.006 .081 .532 1.149 1.731 1.276 1.047 1.262 .561 .202 .015	.002 .075 .441 1.156 1.719 1.509 1.434 1.636 .888 .288 .012 .000	.002 .079 .457 1.112 1.648 1.305 1.112 1.291 .532 .119 .031	.004 .087 .466 1.031 1.550 1.129 .808 .827 .358 .121 .046	.002 .102 .613 1.095 1.274 1.029 .894 1.072 .480 .254 .145	.000 .093 .626 1.079 1.023 1.104 .914 1.478 .942 .634 .212 .012	.002 .086 .497 .931 1.000 1.014 .966 1.644 .933 .569 .154 .002	.002 .056 .488 1.043 .896 .777 .813 1.014 .457 .220 .029 .000	.029 1.088 8.731 18.832 19.813 15.808 12.163 14.189 6.038 2.797 .671 .048
Total	8.570	2.906	4.836 ' 8:23	8 6.249	6.379	4,932	5.319	7.862	8.829	7.690	<b>4.422</b>					

NOTE: Wind directions in tables are presented in "wind from" and not "wind to" direction.

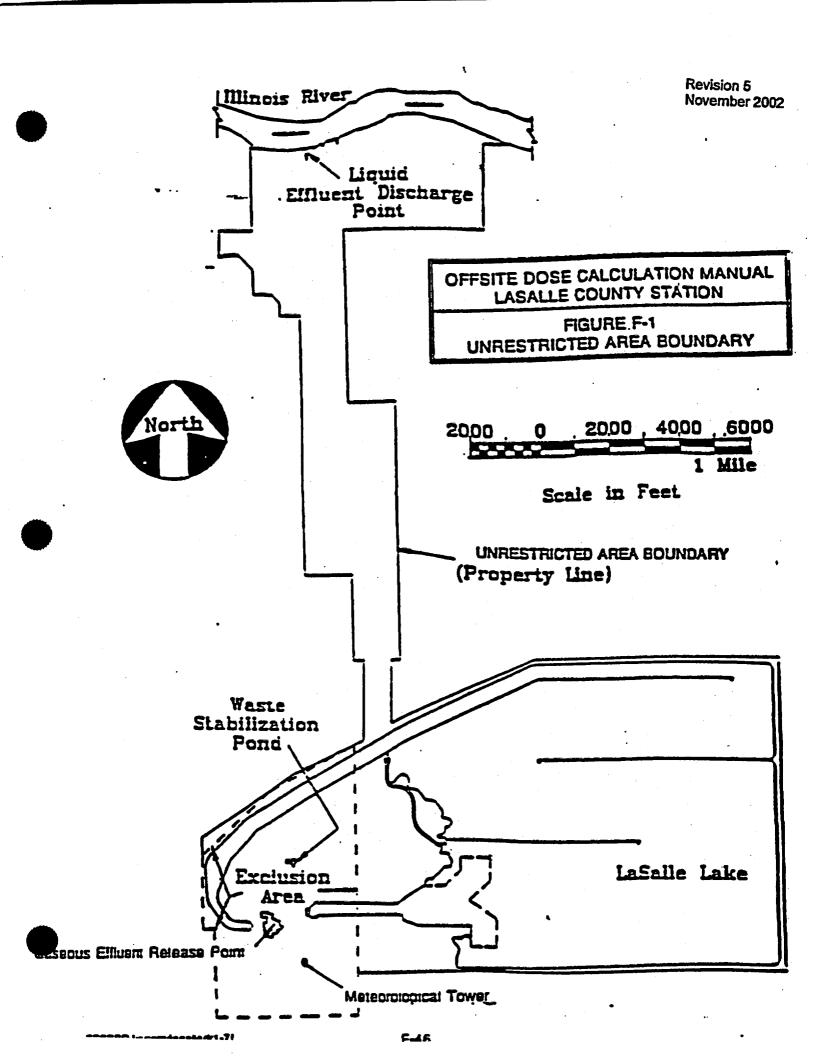
## Supplemental Table C - Continued

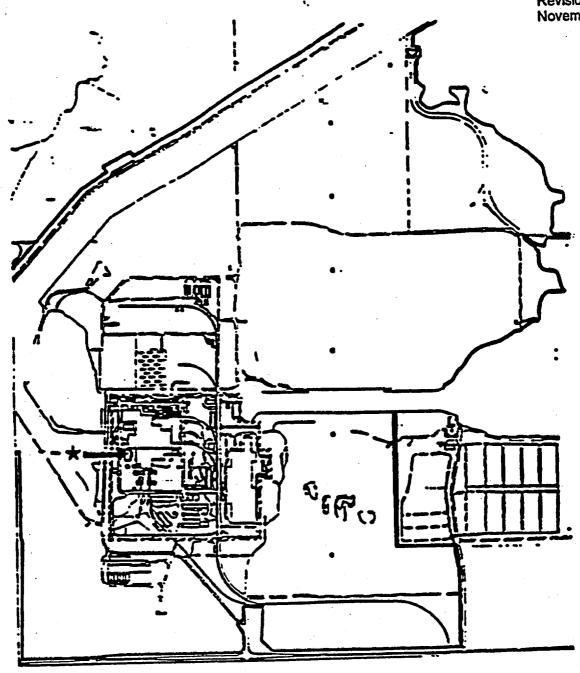
# Ground Level Joint Frequency Distribution Table Summary

#### 33 Foot Elevation Data

# Summery Table of Percent by Speed and Class

Cless . Speed	<b>A</b>	B	C	D	E	F	•
.45 1.05 2.05 3.05 4.05 5.05 6.05 8.05 10.05 13.05 18.00	.000 .021 .326 .998 1.247 1.203 1.201 1.629 .775 .426 .112	.000 .008 .202 .578 .686 .646 .570 .900 .422 .212 .012	.004 .012 .272 .798 .862 .852 .804 1.208 .618 .4245 .000	.002 .197 2.282 5.133 6.435 6.115 5.472 6.605 2.955 1.469 .382 .006	.008 .355 2.334 5.350 4.793 3.880 3.049 3.334 1.334 .438 .069	.010 .299 1.784 3.267 3.084 1.773 .817 .463 .031 .004	.006 .195 1.652 2.808 2.725 1.037 .251 .050 .002 .002

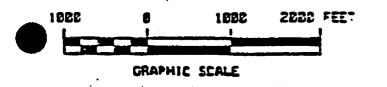




intenm Radwaste Storage Facunty

Restricted Area Boundary

Raowaste Storage Area (When Operational, this area may include 48-packs, DAW, and other types of storage)





OFFSITE DOSE CALCULATION MANUAL LA SALLE COUNTY STATION

FIGURE F-2
RESTRICTED AREA BOUNDARY

E-47