

UNITED STATES
NUCLEAR REGULATORY COMMISSION
OFFICE OF INSPECTION AND ENFORCEMENT
WASHINGTON, D.C. 20555

February 16, 1979

IE Information Notice No. 79-04

DEGRADATION OF ENGINEERED SAFETY FEATURES

Summary

On September 16, 1978, an unusual sequence of events occurred at Arkansas Nuclear One, Units 1 and 2. The events involved the electrical power sources and culminated in the spurious activation and degraded operation of Unit 2 Engineered Safety Features (ESF). Analysis of the course of the incident has identified three safety concerns in the electrical distribution system operation and design.

- (1) The offsite power supply for ANO Unit 1 Engineered Safety Feature loads was deficient in that degraded voltage could have resulted in the unavailability of ESF equipment, if it were to be needed.
- (2) The design of the ANO site electrical system that provides offsite power to Units 1 and 2 did not fully meet the Commission's Regulations, 10 CFR 50, Appendix A, General Design Criterion 17, because in certain circumstances a loss of one of the two offsite power circuits would also result in a loss of the other such circuit.
- (3) Deficiencies existed in the operation of the Unit 2 inverters that convert DC to AC power for the uninterruptable 120 volt vital AC buses.

Description of Circumstances

Initially Unit 1 was operating at 100 percent power; Unit 2 was in hot standby performing hot functional testing in preparation for initial criticality and power operation¹ Unit 1 auxiliary electrical loads were being supplied from the Unit 1 main generator via the unit auxiliary transformer. Unit 2 auxiliary electrical loads were being fed from the offsite grid through Startup Transformer No. 3. The normal operating status was interrupted by the failure of the Unit 1 Loop "A" Main Steam Line Isolation Valve (MSIV) air operator solenoid causing the MSIV to close as designed. The Unit 1 Reactor Protection System sensed conditions requiring reactor shutdown and tripped the reactor. The

¹ The Unit 2 Operating License did not permit criticality of power operation at the time of the incident.

Unit 1 turbine-generator tripped concurrently. Because the Unit 1 generator could no longer supply power for the Unit 1 auxiliary loads, these loads were automatically transferred to Startup Transformer No. 1 to supply this power from offsite. The sequence of events should have ended at this point.

The power to Startup Transformer No. 3, which was feeding Unit 2, and to Startup Transformer No. 1, now feeding Unit 1, normally passes through a single piece of equipment, the Bus Tie Auto-Transformer. (Figure 1 shows a simplified block diagram of the principal electrical equipment involved.) The Auto-Transformer has the capacity to provide power for both units, but due to an error, the protective relays were still adjusted for the operation of Unit 1 only. As a result, when both units concurrently drew power from the Auto-Transformer these protection relays tripped and cut off power to Startup Transformer Nos. 1 and 3.

Startup Transformer No. 2, also shown in Figure 1, thus became the only source of offsite power for both Units 1 and 2. The onsite switching equipment automatically transferred the full auxiliary loads for both units to this transformer. However, this transformer is not designed to carry full auxiliary loads for both units. For this reason, Startup Transformer No. 2 became overloaded and the voltage dropped on the station distribution system for offsite power. At this time and during most of the incident, operating personnel at both units were unaware of the degraded voltage⁽²⁾ condition due to the overloaded Startup Transformer No. 2.⁽³⁾

2 Two other events involving degraded voltage for ESF equipment occurred at Millstone Unit 2 in July 1976. These events were reported as an abnormal occurrence (No. 76-9) in NUREG-0900-5, Report to Congress on Abnormal Occurrences, July-September 1976.

3 It was subsequently determined that the following combinations of Unit 1 and Unit 2 operation would lead to the loss of the Bus Tie Auto-Transformer and the subsequent overloading of Startup Transformer No. 2:

1. Both Units in either the startup or shutdown mode, or
2. Trip of one unit while the other is in either the startup or shutdown mode, or
3. Simultaneous trip of both units.

At Unit 2, eight seconds after the switch to Startup Transformer No. 2, the relays (4) which operate to protect Engineered Safety Feature (ESF) equipment from low (degraded) voltage disconnected and therefore deenergized both Unit 2 ESF buses as designed. At the same time, the Unit 2 Core Protection Calculator (CPC) instrumentation registered trips which indicated a loss of AC power to the circuits (5) that supply at least two instrument channels.

The loss of power on two 120 volt vital AC instrument buses caused, as designed, an actuation of all Unit 2 Engineered Safety Features. Thus, when the two Unit 2 emergency diesel generators started and provided power to the previously deenergized ESF buses, the Engineered Safety Features equipment began to operate. However, due to inverter failures, premature actuation of the Recirculation Actuation System (RAS) occurred. This actuation momentarily opened a flow path directly between the Refueling Water Tank (RWT) and the containment sump. ESF operation and premature RAS operation combined to transfer approximately 60,000 gallons of borated refueling water to the containment sump in about 90 seconds.

- 4 These relays are the second level of undervoltage protection required as a result of the NRC staff review of the 1976 Millstone 2 degraded voltage event. Corrective design changes (i.e., undervoltage relays and load sequencing to offsite power) had been implemented on Unit 2 for degraded voltage protection. These design changes had not been implemented on Unit 1 at the time of the event.
- 5 Each one of the four CPC instrumentation circuits receives power from a vital AC bus which in turn receives power from a battery through an inverter that converts DC power to AC power. Each inverter normally provides power through a circuit with access to both an ESF bus and the station batteries. Each inverter also has an automatic switch that can cut off this normal supply circuit and shift the loads to an alternate supply circuit, which includes just the ESF bus. (See insert on Figure 1.) With both Unit 2 ESF buses momentarily deenergized the only source of instrument power was from the station batteries through the normal switch position. However, although the exact cause is unknown, all four inverter automatic switches were found in the alternate position. Three of four inverters had improper settings on time delay relays and one inverter had the undervoltage trip setting too high, which may have in part been the cause. IE Circular No. 79-02, Failure of 120 Volt Vital AC Power Supplies, dated January 16, 1979, provided details of the inverter problems and recommended items to be reviewed to avoid similar problems.

The normal design sequence calls for the RAS to automatically change the valve lineup when signals from the level instruments on the Refueling Water Tank (RWT) indicate that the tank is nearly empty, which is expected to occur approximately 30 minutes after the LOCA. During this incident, the RAS acted immediately in response to the failure of the inverters and made the change in lineup while the RWT was nearly full. The loss of power from the inverters caused a false low water level indication in the RWT. This false indication provided the signals for the automatic actuation of the RAS.

Had the Emergency Core Cooling System and/or the Containment Spray System been needed in the event of a design basis loss of coolant accident, it would not have performed as designed because of the premature RAS valve actuation. ESF degradation on Unit 2 did not involve a threat to the health and safety of the public because Unit 2 was pre-operational and had no radioactive fission product inventory in the core. However, there was no assurance that the inverter deficiencies which caused the premature operation of the RAS valves would have been corrected prior to Unit 2 power operation.

In the event of a LOCA with a fission product inventory, if the RAS were to initiate at the beginning of the accident, as it did in this incident, the low pressure and high pressure coolant injection subsystems (LPCI and HPCI) of Emergency Core Cooling (ECC) and the Containment Spray System might not function properly. Actuation of RAS causes isolation of the water in the RWT, which is the source of short term cooling water for Emergency Core Cooling and Containment Spray. The premature actuation of RAS also causes these pump suction lines to be connected to the containment sump when there may not be sufficient water available.

Initially, the sequence of events on September 16 did not indicate any problem with the electrical distribution system of Unit 1. However, subsequent analysis indicated that in the event of a LOCA at Unit 1 during which Startup Transformer No. 1 received both the auxiliary electrical loads and starting loads of the Engineered Safety Features a voltage reduction would result. The safety loads might not initially transfer to the Unit 1 diesel generators but could remain on the startup transformer with reduced (degraded) voltage. Although there is margin in the sizing of emergency equipment and the conditions of operation of such equipment, this situation could cause fuses to blow in Engineered Safety Feature circuits which could result in disabling the safety equipment.

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Cause or Causes The immediate causes of the unusual event at Arkansas Nuclear One were: (1) loss of the Bus Tie Auto-Transformer which resulted in degraded power operation through Startup Transformer No. 2, and (2) multiple Unit 2 inverter failures.

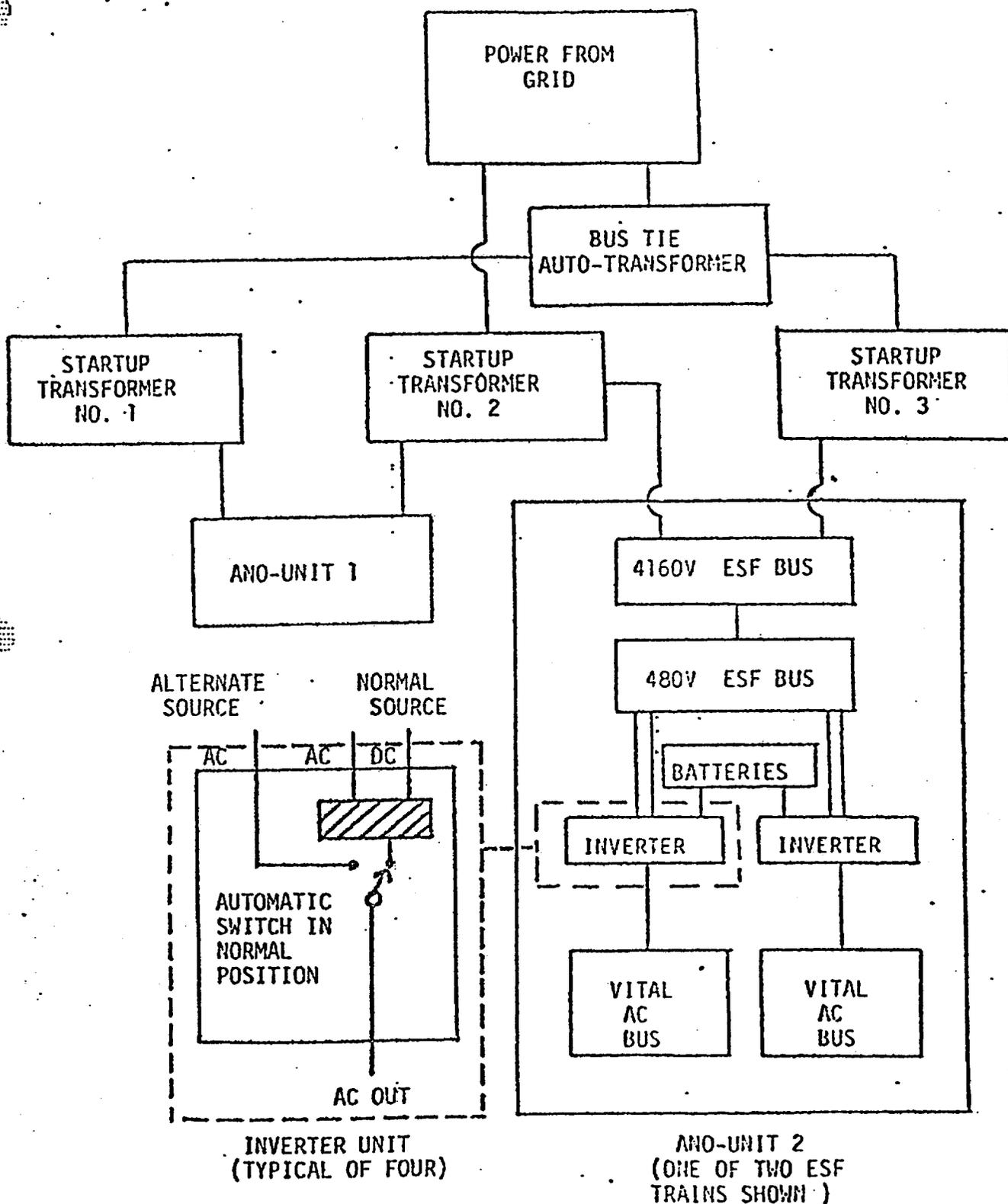
The loss of the Bus Tie Auto-Transformer was caused by inappropriate setpoints for its protective relays. The Bus Tie Auto-Transformer loss had not been adequately reviewed prior to this event in that the overloading of the shared Startup Transformer No. 2 had not been identified during the design and review process.

The primary cause of the failure of the inverters to perform as a reliable power supply was the lack of adequate preoperational test procedures, inadequate knowledge of inverter operation and lack of maintenance control (maintenance has been performed on the inverters several times prior to this event).

This Information Notice provides details of a significant occurrence that is still under review by the NRC staff. After completion of the staff review, this Information Notice will be followed with specific actions to be taken by licensees.

No written response is required. If you desire additional information regarding this matter, contact the Director of the appropriate NRC Regional Office.

Attachment:
Figure 1, Simplified
Block Diagram, Electrical
Distribution



SIMPLIFIED BLOCK DIAGRAM - ELECTRIC DISTRIBUTION

FIGURE 1

Attachment

IE Information Notice No. 79-04
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LISTING OF IE INFORMATION NOTICES
ISSUED IN 1979

Information Notice No.	Subject	Date Issued	Issued To
79-01	Bergen-Paterson Hydraulic Shock and Sway Arrestor	2/2/79	All power reactor facilities with an OL or a CP
79-02	Attempted Extortion - Low Enriched Uranium	2/2/79	All Fuel Facilities
79-03	Limitorque Valve Geared Limit Switch Lubricant	2/9/79	All power reactor facilities with an OL or a CP