

Calculation of impedance functions of the Storage Pads (V<sub>s</sub> for 67 ft)  
Using the method in SC-21, PFS Ex. MM

Storage Pad per SC-21	Assumptions	Storage Pads V <sub>s</sub> for 67 ft
67 ft x 30 ft.	Length (L) x Width (B)	67 ft x 30 ft.
450,000 ksf for 3000 psi concrete	E - Youngs modulus of mat	450,000 ksf for 3000 psi concrete
3 ft.	t - thickness of mat	3 ft.
(.100 ksf/32.17)(750 fps) <sup>2</sup> = 1749 ksf	μ = ρ V <sub>s</sub> <sup>2</sup>	(.100 ksf/32.17)(1081 fps) <sup>2</sup> = 3632 ksf
sqrt((67 ft x 30 ft)/4) = 22.4 ft.	a = sqrt((L x B)/4)	sqrt((67 ft x 30 ft)/4) = 22.4 ft
0.1 ksf	unit weight of soil	0.1 ksf

$$\delta = (Et^3)/(\mu a^3(1-\nu^2)) = \text{relative stiffness}$$

Storage Pad - SC-21

$$\frac{(450,000 \text{ ksf})(3 \text{ ft})^3}{(1749 \text{ ksf})(22.4 \text{ ft})^3(1 - 0.40^2)}$$

$$\delta = 0.735$$

Storage Pad V<sub>s</sub> for 67 ft

$$\frac{(450,000 \text{ ksf})(3 \text{ ft})^3}{(3,632 \text{ ksf})(22.4 \text{ ft})^3(1 - 0.40^2)}$$

$$\delta = 0.353$$

$$a_0 = \Omega a/V_s = \text{dimensionless parameter}$$

a<sub>0</sub> = 0.19 to 0.94 for frequencies  
between 1Hz - 5 Hz

$$a_0 = 0.65 \text{ for frequency of } 5 \text{ Hz} \\ \frac{(5 \text{ cycles/sec})(2\pi \text{ radians/cycle})(129.6 \text{ ft})}{1081 \text{ ft/sec}}$$

\*

Soil shear wave velocity using the average velocity over the depth of 67 ft

V<sub>s</sub> = weighted average of Best Estimate Properties from G(PO17)-2, ICEC, p.8

$$V_{sav} = (5/67)(1497) + (5/67)(415) + 2/67(622) + (6/67)(779) + (8/67)(760) + (9/67)(818) + (15/67)(956) + (17/67)(1716) = 1081 \text{ fps.}$$



# CALCULATION SHEET

ORIGINATOR                      DATE 4/3/01 CALC. NO. G(PO17)-2 REV. NO. 3  
 PROJECT Private Fuel Storage Facility CHECKED OH DATE 4/3/01  
 SUBJECT Storage Pad Analysis and Design JOB NO. 1101-000  
 SHEET 8

**Table 1**  
**Dynamic Soil Properties for SASSI Model**  
 (Source: Reference 5)  
**Upper-Bound Properties**

SHAKE Layers	Depth Top (ft)	Depth Bottom (ft)	Wave Velocity			Damping Ratio		Poisson's Ratio
			Density (pcf)	Vs (fps)	Vp (fps)	Shear (%)	Compression (%)	
1-2	0	5	100	2120	3380	0.91	0.91	0.176
3-4	5	10	80	557	1385	3.48	3.48	0.403
5	10	12	80	807	1543	2.69	2.69	0.312
6-7	12	18	100	983	1803	1.82	1.82	0.289
8-9	18	26	94	973	1764	2.31	2.31	0.281
10-12	26	35	115	1053	2042	5.07	5.07	0.319
13-15	35	50	115	1488	2949	4.04	4.04	0.329
16-23	50	90	120	2481	4808	1.21	1.21	0.318
24-26	90	125	135	4101	7104	4.28	4.28	0.250
27-35	125	300	145	4101	7104	4.28	4.28	0.250
36-39	300	500	145	5657	9798	3.10	3.10	0.250
40-41	500	700	145	6398	11155	2.53	2.53	0.255
	700		170	6398	11155	2.16	1.00	0.255

**Best Estimate Properties**

SHAKE Layers	Depth Top (ft)	Depth Bottom (ft)	Wave Velocity			Damping Ratio		Poisson's Ratio
			Density (pcf)	Vs (fps)	Vp (fps)	Shear (%)	Compression (%)	
1-2	0	5	100	1497	2390	0.94	0.94	0.177
3-4	5	10	80	415	1131	4.78	4.78	0.422
5	10	12	80	622	1260	3.60	3.60	0.339
6-7	12	18	100	779	1472	2.29	2.29	0.306
8-9	18	26	94	760	1440	3.01	3.01	0.307
10-12	26	35	115	818	1667	6.21	6.21	0.341
13-15	35	50	115	956	2085	6.13	6.13	0.367
16-23	50	90	120	1716	3400	1.74	1.74	0.329
24-26	90	125	135	2900	5023	4.32	4.32	0.250
27-35	125	300	145	2900	5023	4.32	4.32	0.250
36-39	300	500	145	3450	5975.5	3.67	3.67	0.250
40-41	500	700	145	3950	6841.5	3.33	3.33	0.250
	700		170	6398	11155	1.76	1.00	0.255

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CLEAR REGULATORY COMMISSION

Docket No. \_\_\_\_\_ Official Exh. No. 172  
In the matter of PFS  
Staff \_\_\_\_\_ IDENTIFIED ✓  
Applicant \_\_\_\_\_ RECEIVED ✓  
Intervenor ✓ REJECTED \_\_\_\_\_  
Other \_\_\_\_\_ WITHDRAWN \_\_\_\_\_  
DATE 4/24/02 Witness \_\_\_\_\_  
Clerk pal