

Attachment Two

SAFETY ANALYSIS REPORT

For

MODEL CNS 1-13C TYPE B SHIPPING PACKAGING

REVISION 2

JULY 1999

Submitted by:

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Columbia, S.C. 29210**

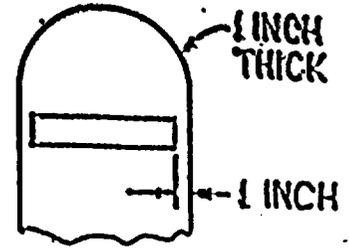
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2.5.1 Lifting Devices (continued)

d. Tension In Lug

$$\sigma_t = \frac{P}{A} \quad \sigma_t = \frac{(38,925) \text{ lbs.}}{(2) \times (1) \text{ in.} \times (1) \text{ in.}} = 19,460 \text{ psi}$$

$$\text{Safety Factor} = \frac{\sigma_y}{\sigma_t} = \frac{(30,000) \text{ psi}}{(19,460) \text{ psi}} = 1.54$$



e. Vertical Welding on Lug

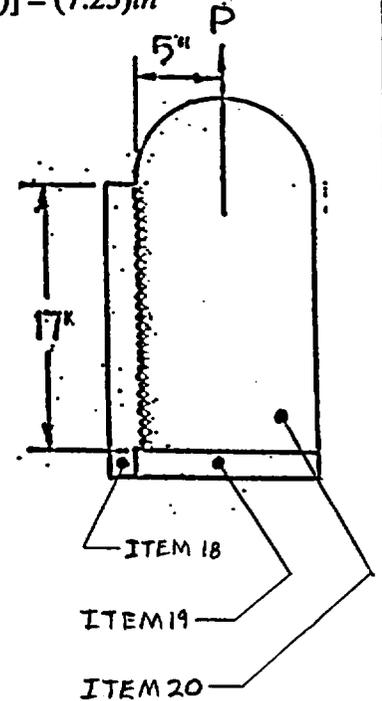
Assuming 3/8 in. fillet welds on each side, except 1/8 in. weld for 2 1/8 in. length in area of each bolt hole. Also, this analysis neglects the bottom plate.

$$A_w = [(2) \times (12) \text{ in.} \times (3/8) \text{ in.} \times (.707)] + [(2) \times (5) \text{ in.} \times (1/8) \text{ in.} \times (.707)] = (7.25) \text{ in.}^2$$

(i) Shear Stress (σ_s)

$$\sigma_s = \frac{P}{A_w} \quad \sigma_s = \frac{(38,925) \text{ lbs.}}{(7.25) \text{ in.}^2} = (5,369) \text{ psi}$$

$$\text{Safety Factor} = \frac{\sigma_{ys}}{\sigma_s} = \frac{(17,320) \text{ psi}}{(5,371) \text{ psi}} = 3.22$$



2.5.1 Lifting Devices (continued)

f. Bending Stress (σ_b) $\sigma_b = \frac{M \times c}{I} \quad M = P \times L$

$$I = 2 \left[\frac{b \times h^3}{12} \right] \text{ (Two sides)}$$

Locating the Neutral Axis $N.A. = \frac{\sum AY}{\sum A}$

Throat of 3/8" weld = 3/8" X .707 = .265 in.
Throat of 1/8" weld = 1/8" X .707 = .0884 in.

$$N.A. = \frac{.265 \times [(4.1875 \times 2.09) + (1.375 \times 7) + (7.1875 \times 13.40)] + .0884 [(2.125 \times 5.25) + (2.125 \times 8.75)]}{2(.0884 \times 2.125) + (.265 \times 4.1875) + (.265 \times 1.375) + (.265 \times 7.1875)}$$

$$N.A. = 8.8$$

Calculations for the five weld segments follow:

$$I_{x-x} = 2 \times \left[\frac{1}{12} \times .265 \times (4.1875)^3 + .265 \times 4.1875 \times (6.706)^2 \right] = (103.05)in.^4$$

$$I_{x-x} = 2 \times \left[\frac{1}{12} \times .088 \times (2.125)^3 + .088 \times 2.125 \times (3.55)^2 \right] = (4.854)in.^4$$

$$I_{x-x} = 2 \times \left[\frac{1}{12} \times .265 \times (1.375)^3 + .265 \times 1.375 \times (1.8)^2 \right] = (2.476)in.^4$$

$$I_{x-x} = 2 \times \left[\frac{1}{12} \times .088 \times (2.125)^3 + .088 \times 2.125 \times (.05)^2 \right] = (.14)in.^4$$

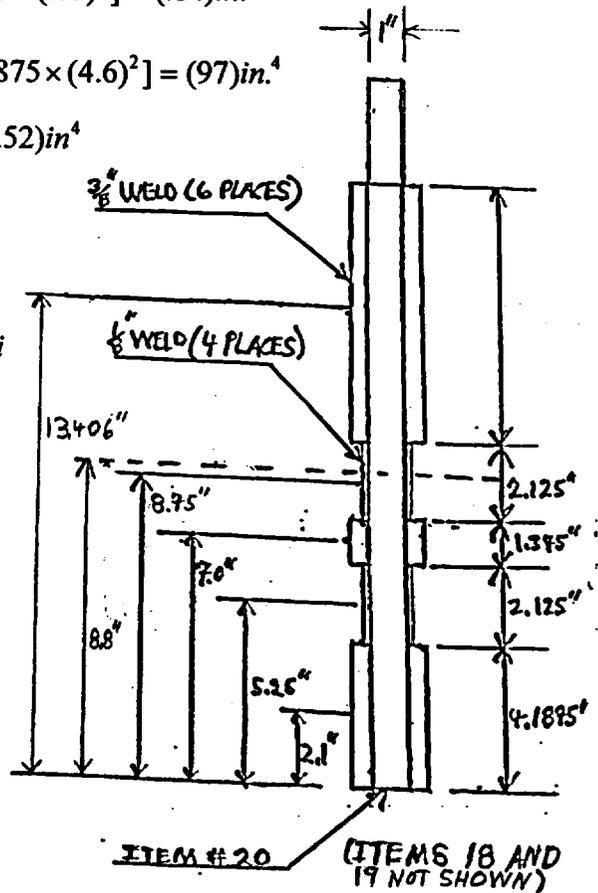
$$I_{x-x} = 2 \times \left[\frac{1}{12} \times .265 \times (7.1875)^3 + .265 \times 7.1875 \times (4.6)^2 \right] = (97)in.^4$$

$$I = 103.05 + 4.854 + 2.476 + .14 + 97 = (207.52)in.^4$$

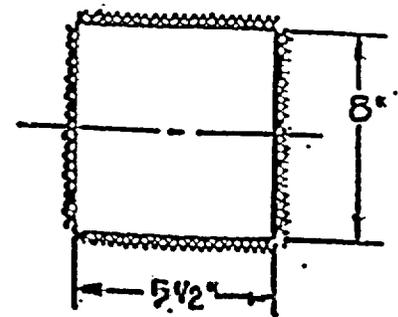
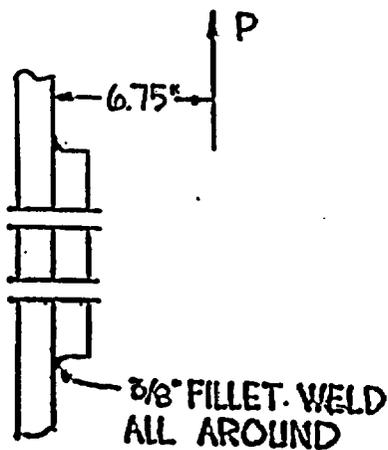
L = 5 in.
c = 8.8 in.

$$\sigma_b = \frac{(38,925)lbs. \times (5)in. \times (8.8)in.}{(207.52)in.^4} = 8,253 psi$$

$$\text{Safety Factor} = \frac{(30,000) psi}{(8,253) psi} = 3.64$$



(2) Welding on Cask Reinforcing Plate.



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"CNS 1-13C SHIPPING CASK"
SHEET 1 OF 3**

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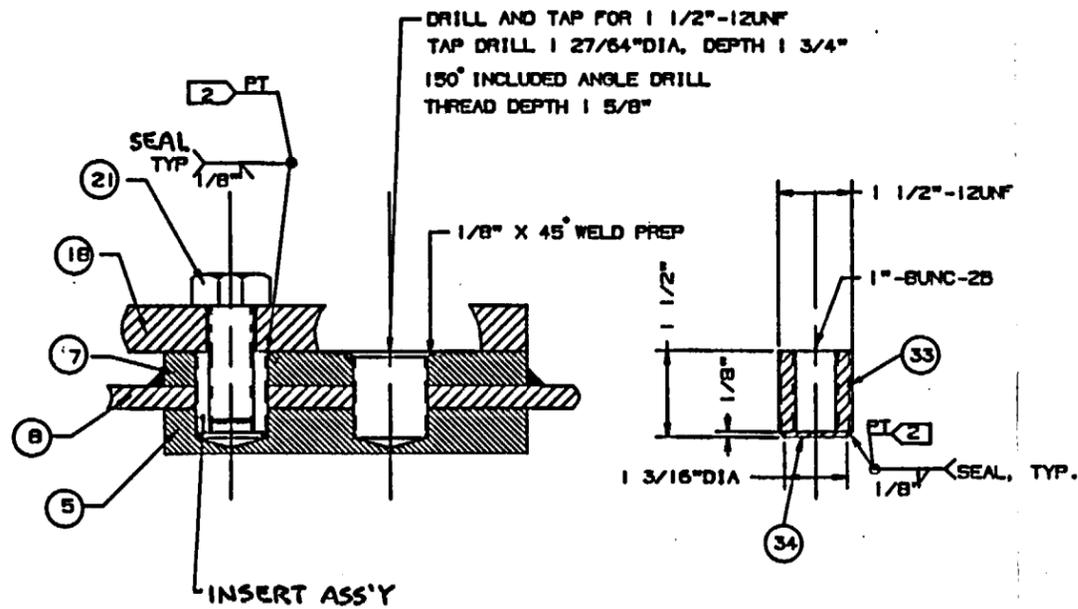
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- NOTES:
- 1) FOR GENERAL NOTES AND BILL OF MATERIALS SEE SHEET 1 OF 3
 - 2) WELDS SHALL BE LIQUID PENETRANT (PT) INSPECTED IN ACCORDANCE WITH ASME CODE SECTION III, DIV 1, SUBSECTION NB, ARTICLE NB-5000 AND SECTION V, ARTICLE 6

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DIMENSIONS ARE IN INCHES UNLESS NOTED DO NOT SCALE PRINT TOLERANCES (UNLESS NOTED) HOLE DIA. & LOC. ± 1/32 DEC. X ± .1 DEC. XX ± .01 DEC. XXX ± .005 ANGLES ± 1° FRACTIONS ± 1/8 DOES NOT APPLY TO REFERENCE DIMENSIONS	PROJECT No. 25889	FSCM NUMBER 54643	CHEM-NUCLEAR SYSTEMS, INC.		
	FILE I.D. 0014030		CNSI 1-13C SHIPPING CASK		
	DRAWN BY R. FERREN	11/24/92			
	CHECKED BY [Signature]	11/24/92			
	ENGINEER [Signature]	11/24/92	SIZE E	DRAWING NUMBER C-110-E-0005	REV. 6
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