

*rec'd 3/11/99*  
71-9255



**TRANSNUCLEAR WEST**

March 9, 1999  
NUH05-99-521  
RMG-99-012

Mr. Steven Baggett  
Project Manager, Spent Fuel Project Office  
U.S. Nuclear Regulatory Commission  
11555 Rockville Pike  
Rockville, MD 20852

**SUBJECT:** Amendment Application for NUHOMS<sup>®</sup>-MP187 Transportation Package (Docket No. 71-9255)

**REFERENCE:** S. Redeker letter to USNRC dated January 28, 1999, "(Docket No. 72-11) Rancho Seco Independent Spent Fuel Storage Installation Safety Analysis Report Revision 2."

Dear Mr. Baggett:

Transnuclear West Inc. (TN West) herewith submits a revised drawing for the NUHOMS<sup>®</sup>-MP187 package. TN West requests that Certificate 71-9255 be revised to incorporate this drawing change. A detailed description and technical justification for the change are provided in Attachment 1. The revised drawing, provided as Attachment 2, is:

NUH-05-4001, "NUHOMS<sup>®</sup>-MP187 Multi-Purpose Cask Main Assembly," Revision 11.

TN West will revise the NUHOMS<sup>®</sup>-MP187 SAR to include the revised drawings upon receiving NRC approval. TN West requests NRC approval of this Amendment no later than May 1999 in order to meet the Rancho Seco ISFSI fabrication and fuel load schedule given in the reference letter.

This submittal includes the proprietary version of the drawing, copies of which are segregated consistent with previous SAR submittals. The proprietary material may not be used for any purpose other than to support your staff's review of the Certificate of Compliance application. Attachment 4 is an affidavit specifically requesting that you withhold this proprietary information from public disclosure. The non-proprietary version of drawing NUH-05-4001 previously submitted to the NRC is not affected by this change.

9906160084 990309  
PDR ADOCK 07109255  
C PDR

Transnuclear West Inc.  
3930 Civic Center Drive, Suite 280, Fremont, CA 94538  
Phone: 510-795-9800 • Fax: 510-744-6002

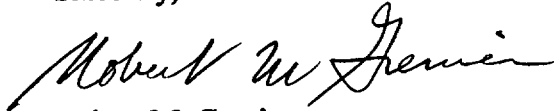
*NT01*  
*1/2*

Mr. Steven Baggett  
U.S. Nuclear Regulatory Commission

NUH05-99-521  
March 9, 1999

Please contact Mr. U. B. Chopra (510-744-6053) or me (510-744-6020) if you require any additional information in support of this submittal.

Sincerely,



Robert M. Grenier  
President and Chief Operating Officer

Attachments:

- 1) Description and Justification for Proposed Changes
- 2) Computer Run Input
- 3) Revised Drawing - Six (6) copies of NUH-05-4001 (proprietary)
- 4) Affidavit Pursuant to 10 CFR 2.790

Docket 71-9255

cc: File NUH005.0003

APPLICATION DATED MARCH 9, 1999  
TRANSNUCLEAR WEST INC.  
DOCKET 71-9255

**Description and Justification for Change**

*Description:* The weld between the MP187 cask inner shell and top forging includes a 1/8 inch thick by 1.0 inch wide backing ring as shown at coordinate C5 on sheet 3 of drawing NUH-05-4001, Revision 10. This backing ring facilitates completion of this containment weld and remains a part of the completed cask. As shown on the revised drawing provided with this application (NUH-05-4001 Revision 11), TN West proposes to increase the size of this ring to 1/4 inch thick by 2.0 inches wide.

*Reason for Change:* The original size of the backing ring was selected to both minimize its impingement on the lead shielding present in the cask and to completely cover the root of the weld. The backing ring design was also consistent with the originally proposed inspection requirements for the weld - multi-layer dye-penetrant examination. However, in the final stages of cask licensing the examination requirements for this weld were revised to require volumetric examination by either radiographic or ultrasonic means. As shown in Figure 1, the edge of the existing backing ring will be visible in the volumetric examination and may appear as an indication or may mask the presence of indications. Revising the width of the ring to remove the edge from the area to be inspected will improve the quality of the volumetric examination.

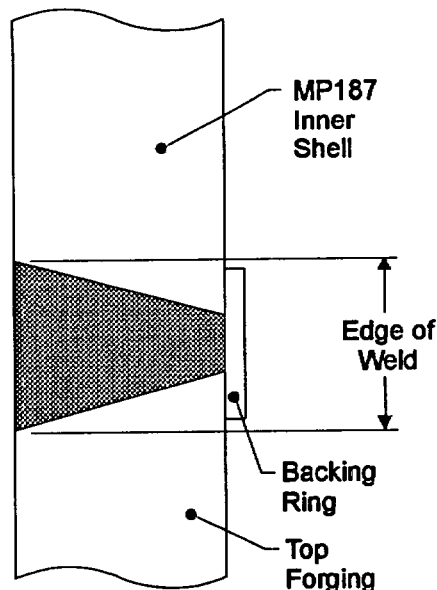


Figure 1, Inner Shell Closure Weld Geometry

Increasing the thickness of the backing ring from 1/8 inches to 1/4 inches will facilitate completion of this containment weld by reducing the potential for melt-through and distortion.

*Justification:* Changing the size of the backing ring has no impact on the structural, thermal, criticality, or containment analyses or on the use of the package. No credit is taken for the ring in the structural or containment analyses. The small size of the ring and its location outside of the active fuel region ensures that the proposed changes will not affect the thermal or criticality analyses. Because the ring displaces a portion of the cask's lead gamma shield, the impact of this change on the shielding analyses presented in Chapter 5 of the SAR is addressed below.

As shown on the drawings provided with this submittal, the inner shell weld and backing ring are 16.0 inches below the top of the cask. Based on the shielding models described in the MP187 SAR, the dose rates at this location assuming that no backing ring is present are 21.5 mrem/hr (surface of package and vehicle outer surface) and 4.91 mrem/hr (2 meters from vehicle outer surface). These results are shown in Table 2 (column labeled "Dose Rate w/o Ring").

The effect of the backing ring on the calculated dose rates is bounded using the "base case" 1-dimensional model described in Section 5.4.1.8.1 of the SAR and provided in Section 5.5.5.1 of the SAR. The neutron and gamma dose rates on the surface of the cask calculated by this model are shown in Table 1 (column labeled "1-D Base"). By modifying the 1-D model to replace either 1/8 inch or 1/4 inch of lead with steel over the entire length of the cask (infinite axial model), TN West bounds the effect of the steel backing ring. Using this model, TN West estimated the change in the package dose rates related to the presence of the existing ring as well as the proposed change. The 1-D results on the surface of the cask are provided in the Table 1 ("1-D for 1/8 in Ring" and "1-D for 1/4 in Ring"). Ratios relative to the base case are calculated for both the 1/8 in ring and the 1/4 in ring as shown in Table 1.

	1-D Base (mrem/hr)	1-D for 1/8 in Ring (mrem/hr)	1-D for 1/4 in Ring (mrem/hr)	Calculated Ratios		Ratios Used Below	
				1/8 in Ring	1/4 in Ring	1/8 in Ring	1/4 in Ring
Neutron	18.32	18.04	17.76	0.985	0.969	1.000	1.000
Gamma	24.24	26.04	27.98	1.074	1.154	1.074	1.154

Table 1, 1-D Shielding Results for Backing Ring

The dose rates on the package and vehicle surfaces (these are identical in the vicinity of the backing ring) and 2 meters from the vehicle surface in the region adjacent to the backing ring are estimated by multiplying the dose rate without the ring by the ratios shown in Table 1. As shown in Table 1, the presence of the ring actually reduces the neutron dose rate on the surface while increasing the gamma dose rate locally. To bound the results the neutron dose rates are not adjusted (refer to column "Ratios Used Below" in Table 1). This is consistent with the fact that the steel ring is a better neutron shield than the lead it displaces and the lead is a better gamma shield than the steel.

The calculated dose rates on the package surface, vehicle outer surface, and 2-meters from the vehicle outer surface are shown in Table 2. The dose rates without the backing ring are taken directly from the MP187 shielding results presented in Chapter 5 of the SAR. The dose rates with the ring are bounded using the ratios from Table 1. The surface dose rates and the 2-meter dose rate increase slightly (less than 4% and 2% respectively), but remain well below the limits at these locations (200 and 10 mrem/hr respectively). The controlling dose rate 2-meters from the vehicle outer surface, 9.94 mrem/hr, is unaffected by this change. Copies of the computer run input are included in Attachment 2.

Based on these results, TN West concludes that the proposed change to the MP187 package will not affect the package's ability to satisfy the requirements of 10CFR71.47 for normal operations. Because the dose rates associated with the hypothetical accident conditions are dominated by postulated gaps in the lead shielding, the presence of the backing ring will not affect compliance with the limits specified in 10CFR71.51.

Location	Dose Rate w/o Ring (mrem/hr)	Dose Rate w/ 1/8 in Ring (mrem/hr)	Dose Rate w/ 1/4 in Ring (mrem/hr)
<i>Package Surface</i>			
Neutron	19.85	19.85	19.85
Gamma	1.69	1.82	1.95
Total	21.54	21.67	21.80
<i>Vehicle Outer Surface</i>			
Neutron	19.85	19.85	19.85
Gamma	1.69	1.82	1.95
Total	21.54	21.67	21.80
<i>2 Meters from Vehicle Outer Surface</i>			
Neutron	3.59	3.59	3.59
Gamma	1.32	1.42	1.52
Total	4.91	5.01	5.11

Table 2, Dose Rates Vicinity of the Closure Weld Backing Strip

APPLICATION DATED MARCH 9, 1999  
 TRANSNUCLEAR WEST INC.  
 DOCKET 71-9255

**Computer Run Input**

ANISN Input for 1/8 Inch Ring

MP187 CASK SHIELDING TRUNNION - FC-COR10.AI  
 ' Section taken through neutron shield, base case  
 ' FC average source term  
 ' Includes 1/8 in backing strip in lead  
 15\$\$

'	ID	ITH	ISCT	ISN	IGE
'	1	0	3	16	2
'	IBL	IBR	IZM	IM	IEVT
'	1	0	16	72	0
'	IGM	IHT	IHS	IHM	MS
'	40	3	4	43	156
'	MCR	MTP	MT	IDFM	IPVT
'	64	0	104	0	0
'	IQM	IPM	IPP	IIM	ID1
'	1	0	0	20	0
'	ID2	ID3	ID4	ICM	IDAT1
'	0	3	1	10	0
'	IDAT2	IFG	IFLU	IFN	IPRT
'	0	0	0	1	1
'	IXTR				
'	0				

'	EV	EVM	EPS	BF	DY
'	0.0	0.0	0.0001	1.420892	360.172
'	DZ	DFM1	XNF	PV	RYF
'	0.0	0.0	0.0	0.0	0.5
'	XLAL	EQL	XNPM	T	
'	0.0002	F0.0		T	

' CROSS SECTION DATA FROM THE CASK-81 LIBRARY

14\*

Cross Section Data from Cask-81 Not Shown

T  
 17\*\*

' Source for 40.0 GWd/MTU Fuel

13R1.57E-01	59R0.00
13R8.93E-01	59R0.00
13R3.48E+00	59R0.00
13R1.38E+01	59R0.00
13R3.25E+01	59R0.00
13R4.40E+01	59R0.00
13R9.33E+01	59R0.00
13R7.49E+01	59R0.00
13R1.76E+01	59R0.00
13R9.56E+01	59R0.00
13R1.64E+02	59R0.00
13R1.40E+02	59R0.00
13R8.87E+01	59R0.00
13R1.01E+01	59R0.00
13R5.11E-02	59R0.00
13R3.71E-03	59R0.00

13R2.44E-04 59R0.00  
 13R3.53E-05 59R0.00  
 13R7.60E-06 59R0.00  
 13R1.19E-06 59R0.00  
 13R2.61E-07 59R0.00  
 13R7.54E-08 59R0.00  
 13R4.42E-01 59R0.00  
 13R2.78E+00 59R0.00  
 13R1.61E+01 59R0.00  
 13R1.84E+01 59R0.00  
 13R9.10E+01 59R0.00  
 13R1.33E+03 59R0.00  
 13R4.89E+03 59R0.00  
 13R3.27E+06 59R0.00  
 13R2.63E+08 59R0.00  
 13R6.18E+08 59R0.00  
 13R1.30E+08 59R0.00  
 13R2.25E+09 59R0.00  
 13R4.09E+09 59R0.00  
 13R1.02E+08 59R0.00  
 13R1.98E+08 59R0.00  
 13R5.12E+08 59R0.00  
 13R9.81E+08 59R0.00  
 13R5.45E+09 59R0.00

T  
 3\*\* 13R1.0 F0.0  
 T

1\*\*  
 ' U235 FISSION SPECTRUM  
 1.984E-04 1.064E-03 4.013E-03 1.559E-02 3.676E-02  
 5.035E-02 1.093E-01 9.024E-02 2.149E-02 1.190E-01  
 2.138E-01 1.928E-01 1.298E-01 1.549E-02 7.893E-05  
 5.740E-06 3.775E-07 5.453E-08 1.176E-08 1.832E-09  
 4.039E-10 1.166E-10 F0.0

4\*\*  
 ' FINE MESH  
 0.00 0.65 1.94 4.52 9.69  
 21.59 35.56 40.20 50.54 60.87  
 66.04 68.62 69.92 70.56 71.85  
 74.44 76.20 79.93 82.47 83.74  
 84.53 85.32 85.73 86.36 87.63  
 88.87 89.54 89.87 90.20 90.54  
 90.87 91.54 92.12 92.71 93.20  
 94.35 95.69 96.36 97.16 97.69  
 98.36 98.69 99.06 99.38 99.70  
 100.97 101.60 102.24 104.22 105.44  
 106.05 106.35 106.68 106.96 107.32  
 107.95 108.48 109.09 109.86 110.40  
 111.01 111.62 112.23 112.83 113.44  
 114.05 114.65 115.36 116.06 116.67  
 117.00 117.47 117.74

5\*\* F1.0

6\*\*  
 ' S16 CYLINDRICAL ANGULAR QUADRATURE WEIGHTS  
 .0000000 .0135762 .0135762 .0000000 .0155634  
 .0155634 .0155634 .0155634 .0000000 .0158598  
 .0158598 .0158598 .0158598 .0158598 .0158598  
 .0000000 .0155786 .0155786 .0155786 .0155786  
 .0155786 .0155786 .0155786 .0155786 .0000000

.0149596	.0149596	.0149596	.0149596	.0149596
.0149596	.0149596	.0149596	.0149596	.0149596
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.0140964	.0140964	.0140964	.0140964	.0140964
.0140964	.0140964	.0140964	.0000000	.0130431
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.0130431	.0130431	.0130431	.0130431	.0130431
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.0118407	.0118407	.0118407	.0118407	.0118407
.0118407	.0118407	.0118407	.0118407	.0118407

7\*\*

' S16 CYLINDRICAL ANGULAR QUADRATURE COSINES									
-.1452095	-.1026786	.1026786	-.3282956	-.3033056					
-.1256333	.1256333	.3033056	-.5006822	-.4836218					
-.3540357	-.1295861	.1295861	.3540357	.4836218					
-.6552589	-.6426682	-.5448278	-.3640423	-.1278347					
.1278347	.3640423	.5448278	.6426682	-.7862754					
-.7765950	-.7005765	-.5559806	-.3569615	-.1230006					
.1230006	.3569615	.5559806	.7005765	.7765950					
-.8889435	-.8813385	-.8212767	-.7052463	-.5411545					
-.3401840	-.1160304	.1160304	.3401840	.5411545					
.7052463	.8212767	.8813385	-.9595308	-.9534975					
-.9056852	-.8124580	-.6784908	-.5105012	-.3169129					
-.1074334	.1074334	.3169129	.5105012	.6784908					
.8124580	.9056852	.9534975	-.9954761	-.9906826					
-.9526112	-.8779315	-.7695134	-.6315233	-.4692642					
-.2889715	-.0975737	.0975737	.2889715	.4692642					
.6315233	.7695134	.8779315	.9526112	.9906826					

8\$\$	13R1	6R2	2R3	2R4	3R5	12R6	4R7	1R8	2R9
	1R10	1R11	3R12	8R13	12R14	1R15	1R16		
9\$\$	69	81	85	81	85	89	89	89	85
	85	85	85	93	93	85	81		

' FX91	1	2	3	4
' H	5	6	7	8
' B	9	10	11	12
' C	13	14	15	16
' N	17	18	19	20
' O	21	22	23	24
' AL	25	26	27	28
' SI	29	30	31	32
' CA	33	34	35	36
' CR	37	38	39	40
' FE	41	42	43	44
' NI	45	46	47	48
' ZR	49	50	51	52
' PB	53	54	55	56
' U235	57	58	59	60
' U238	61	62	63	64
' FLUXDOSIUM	65	66	67	68
' DRY FUEL	69	70	71	72
' FC TOP DRY	73	74	75	76
' BOTTOM	77	78	79	80
' AIR	81	82	83	84
' SS304	85	86	87	88
' LEAD	89	90	91	92
' BISCO NS3	93	94	95	96
' HONEYCOMB	97	98	99	100



' FOAM 101 102 103 104

10\$\$

' FLUXDOSIUM  
65 66 67 68  
' DRY FUEL  
69 70 71 72  
69 70 71 72  
69 70 71 72  
69 70 71 72  
69 70 71 72  
69 70 71 72  
69 70 71 72  
69 70 71 72  
69 70 71 72  
' FC TOP DRY  
73 74 75 76  
73 74 75 76  
73 74 75 76  
73 74 75 76  
' BOTTOM  
77 78 79 80  
77 78 79 80  
77 78 79 80  
' AIR  
81 82 83 84  
81 82 83 84  
' SS304  
85 86 87 88  
85 86 87 88  
85 86 87 88  
' LEAD  
89 90 91 92  
' BISCO NS3  
93 94 95 96  
93 94 95 96  
93 94 95 96  
93 94 95 96  
93 94 95 96  
93 94 95 96  
93 94 95 96  
93 94 95 96  
93 94 95 96  
' HONEYCOMB  
97 98 99 100  
' FOAM  
101 102 103 104  
101 102 103 104  
101 102 103 104  
101 102 103 104

11\$\$

' FLUXDOSIUM  
1 2 3 4  
' DRY FUEL  
9 10 11 12  
13 14 15 16  
21 22 23 24  
25 26 27 28  
37 38 39 40

41 42 43 44  
45 46 47 48  
49 50 51 52  
57 58 59 60  
61 62 63 64  
' FC TOP DRY  
37 38 39 40  
41 42 43 44  
45 46 47 48  
49 50 51 52  
' BOTTOM  
37 38 39 40  
41 42 43 44  
45 46 47 48  
' AIR  
17 18 19 20  
21 22 23 24  
' SS304  
37 38 39 40  
41 42 43 44  
45 46 47 48  
' LEAD  
53 54 55 56  
' BISCO NS3 -  
5 6 7 8  
9 10 11 12  
13 14 15 16  
21 22 23 24  
25 26 27 28  
29 30 31 32  
33 34 35 36  
37 38 39 40  
41 42 43 44  
45 46 47 48  
' HONEYCOMB  
25 26 27 28  
' FOAM  
5 6 7 8  
13 14 15 16  
17 18 19 20  
21 22 23 24  
12\*\*  
' FLUXDOSIUM  
4R1.000E0  
' DRY FUEL  
4R8.137E-4  
4R2.033E-4  
4R9.994E-3  
4R8.656E-4  
4R8.658E-4  
4R2.923E-3  
4R4.648E-4  
4R3.255E-3  
4R4.301E-5  
4R4.953E-3  
' FC TOP DRY  
4R1.344E-3  
4R4.552E-3  
4R7.138E-4  
4R1.869E-3

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' BOTTOM
  4R2.244E-3
  4R7.345E-3
  4R1.379E-3
' AIR
  4R3.587E-5
  4R9.534E-6
' SS304
  4R1.728E-2
  4R6.073E-2
  4R7.447E-3
' LEAD
  4R3.296E-2
' BISCO NS3 2 W/O B4C
  4R4.180E-2
  4R7.131E-4
  4R7.871E-3
  4R3.442E-2
  4R8.528E-3
  4R1.155E-3
  4R1.351E-3
  4R6.104E-4
  4R2.242E-3
  4R2.631E-4
' HONEYCOMB
  4R6.435E-3
' FOAM
  4R9.378E-3
  4R6.746E-3
  4R7.713E-4
  4R2.026E-3
19$$ F3
22$$ F-1
23$$ 1 2 3
      T      T

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ANISN Input for 1/4 Inch Ring

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MP187 CASK SHIELDING TRUNNION - FC-COR10.AI
' Section taken through neutron shield, base case
' FC average source term
' Includes 1/4 in backing strip in lead

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15$$$
'   ID      ITH      ISCT      ISN      IGE
'   1        0        3        16        2
'   IBL     IBR     IZM     IM     IEVT
'   1        0        16     72        0
'   IGM     IHT     IHS     IHM     MS
'   40       3        4        43     156
'   MCR     MTP     MT      IDFM    IPVT
'   64       0       104      0        0
'   IQM     IPM     IPP     IIM     ID1
'   1        0        0       20        0
'   ID2     ID3     ID4     ICM     IDAT1
'   0        3        1       10        0
'   IDAT2   IFG     IFLU    IFN     IPRT
'   0        0        0        1        1
'   IXTR
'   0

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16**
'   EV      EVM      EPS      BF      DY
   0.0      0.0      0.0001  1.420892  360.172
'   DZ      DFM1     XNF      PV      RYF
   0.0      0.0      0.0      0.0      0.5
'   XLAL     EQL      XNPM      T
   0.0002   F0.0      T
'   CROSS SECTION DATA FROM THE CASK-81 LIBRARY

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14\*

Cross Section Data from Cask-81 Not Shown

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17\*\*

' Source for 40.0 Gwd/MTU Fuel

```

13R1.57E-01   59R0.00
13R8.93E-01   59R0.00
13R3.48E+00   59R0.00
13R1.38E+01   59R0.00
13R3.25E+01   59R0.00
13R4.40E+01   59R0.00
13R9.33E+01   59R0.00
13R7.49E+01   59R0.00
13R1.76E+01   59R0.00
13R9.56E+01   59R0.00
13R1.64E+02   59R0.00
13R1.40E+02   59R0.00
13R8.87E+01   59R0.00
13R1.01E+01   59R0.00
13R5.11E-02   59R0.00
13R3.71E-03   59R0.00
13R2.44E-04   59R0.00
13R3.53E-05   59R0.00
13R7.60E-06   59R0.00
13R1.19E-06   59R0.00
13R2.61E-07   59R0.00
13R7.54E-08   59R0.00
13R4.42E-01   59R0.00
13R2.78E+00   59R0.00
13R1.61E+01   59R0.00
13R1.84E+01   59R0.00
13R9.10E+01   59R0.00
13R1.33E+03   59R0.00
13R4.89E+03   59R0.00
13R3.27E+06   59R0.00
13R2.63E+08   59R0.00
13R6.18E+08   59R0.00
13R1.30E+08   59R0.00
13R2.25E+09   59R0.00
13R4.09E+09   59R0.00
13R1.02E+08   59R0.00
13R1.98E+08   59R0.00
13R5.12E+08   59R0.00
13R9.81E+08   59R0.00
13R5.45E+09   59R0.00

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3\*\* 13R1.0 F0.0

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1\*\*

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'   U235 FISSION SPECTRUM
   1.984E-04  1.064E-03  4.013E-03  1.559E-02  3.676E-02

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5.035E-02	1.093E-01	9.024E-02	2.149E-02	1.190E-01
2.138E-01	1.928E-01	1.298E-01	1.549E-02	7.893E-05
5.740E-06	3.775E-07	5.453E-08	1.176E-08	1.832E-09
4.039E-10	1.166E-10	F0.0		

4\*\*

' FINE MESH

0.00	0.65	1.94	4.52	9.69
21.59	35.56	40.20	50.54	60.87
66.04	68.62	69.92	70.56	71.85
74.44	76.20	79.93	82.47	83.74
84.53	85.32	85.73	86.36	87.63
88.87	89.54	89.87	90.20	90.54
90.87	91.54	92.12	92.71	93.20
94.35	95.69	96.36	97.16	97.69
98.36	98.69	99.06	99.38	99.70
100.97	101.60	102.24	104.22	105.44
106.05	106.35	106.68	106.96	107.32
107.95	108.48	109.09	109.86	110.40
111.01	111.62	112.23	112.83	113.44
114.05	114.65	115.36	116.06	116.67
117.00	117.47	117.74		

5\*\* F1.0

6\*\*

' S16 CYLINDRICAL ANGULAR QUADRATURE WEIGHTS

.0000000	.0135762	.0135762	.0000000	.0155634
.0155634	.0155634	.0155634	.0000000	.0158598
.0158598	.0158598	.0158598	.0158598	.0158598
.0000000	.0155786	.0155786	.0155786	.0155786
.0155786	.0155786	.0155786	.0155786	.0000000
.0149596	.0149596	.0149596	.0149596	.0149596
.0149596	.0149596	.0149596	.0149596	.0149596
.0000000	.0140964	.0140964	.0140964	.0140964
.0140964	.0140964	.0140964	.0140964	.0140964
.0140964	.0140964	.0140964	.0000000	.0130431
.0130431	.0130431	.0130431	.0130431	.0130431
.0130431	.0130431	.0130431	.0130431	.0130431
.0130431	.0130431	.0130431	.0000000	.0118407
.0118407	.0118407	.0118407	.0118407	.0118407
.0118407	.0118407	.0118407	.0118407	.0118407
.0118407	.0118407	.0118407	.0118407	.0118407

7\*\*

' S16 CYLINDRICAL ANGULAR QUADRATURE COSINES

-.1452095	-.1026786	.1026786	-.3282956	-.3033056
-.1256333	.1256333	.3033056	-.5006822	-.4836218
-.3540357	-.1295861	.1295861	.3540357	.4836218
-.6552589	-.6426682	-.5448278	-.3640423	-.1278347
.1278347	.3640423	.5448278	.6426682	-.7862754
-.7765950	-.7005765	-.5559806	-.3569615	-.1230006
.1230006	.3569615	.5559806	.7005765	.7765950
-.8889435	-.8813385	-.8212767	-.7052463	-.5411545
-.3401840	-.1160304	.1160304	.3401840	.5411545
.7052463	.8212767	.8813385	-.9595308	-.9534975
-.9056852	-.8124580	-.6784908	-.5105012	-.3169129
-.1074334	.1074334	.3169129	.5105012	.6784908
.8124580	.9056852	.9534975	-.9954761	-.9906826
-.9526112	-.8779315	-.7695134	-.6315233	-.4692642
-.2889715	-.0975737	.0975737	.2889715	.4692642
.6315233	.7695134	.8779315	.9526112	.9906826

8\$\$	13R1	6R2	2R3	2R4	3R5	12R6	4R7	2R8	1R9
	1R10	1R11	3R12	8R13	12R14	1R15	1R16		
9\$\$	69	81	85	81	85	89	89	85	85
	85	85	85	93	93	85	81		
'	FX91	1	2	3	4				
'	H	5	6	7	8				
'	B	9	10	11	12				
'	C	13	14	15	16				
'	N	17	18	19	20				
'	O	21	22	23	24				
'	AL	25	26	27	28				
'	SI	29	30	31	32				
'	CA	33	34	35	36				
'	CR	37	38	39	40				
'	FE	41	42	43	44				
'	NI	45	46	47	48				
'	ZR	49	50	51	52				
'	PB	53	54	55	56				
'	U235	57	58	59	60				
'	U238	61	62	63	64				
'	FLUXDOSIUM	65	66	67	68				
'	DRY FUEL	69	70	71	72				
'	FC TOP DRY	73	74	75	76				
'	BOTTOM	77	78	79	80				
'	AIR	81	82	83	84				
'	SS304	85	86	87	88				
'	LEAD	89	90	91	92				
'	BISCO NS3	93	94	95	96				
'	HONEYCOMB	97	98	99	100				
'	FOAM	101	102	103	104				
10\$\$									
'	FLUXDOSIUM								
	65	66	67	68					
'	DRY FUEL								
	69	70	71	72					
	69	70	71	72					
	69	70	71	72					
	69	70	71	72					
	69	70	71	72					
	69	70	71	72					
	69	70	71	72					
	69	70	71	72					
	69	70	71	72					
'	FC TOP DRY								
	73	74	75	76					
	73	74	75	76					
	73	74	75	76					
	73	74	75	76					
'	BOTTOM								
	77	78	79	80					
	77	78	79	80					
	77	78	79	80					
'	AIR								
	81	82	83	84					
	81	82	83	84					
'	SS304								
	85	86	87	88					
	85	86	87	88					

85 86 87 88  
' LEAD  
89 90 91 92  
' BISCO NS3  
93 94 95 96  
93 94 95 96  
93 94 95 96  
93 94 95 96  
93 94 95 96  
93 94 95 96  
93 94 95 96  
93 94 95 96  
' HONEYCOMB  
97 98 99 100  
' FOAM  
101 102 103 104  
101 102 103 104  
101 102 103 104  
101 102 103 104  
11\$\$  
' FLUXDOSIUM  
1 2 3 4  
' DRY FUEL  
9 10 11 12  
13 14 15 16  
21 22 23 24  
25 26 27 28  
37 38 39 40  
41 42 43 44  
45 46 47 48  
49 50 51 52  
57 58 59 60  
61 62 63 64  
' FC TOP DRY  
37 38 39 40  
41 42 43 44  
45 46 47 48  
49 50 51 52  
' BOTTOM  
37 38 39 40  
41 42 43 44  
45 46 47 48  
' AIR  
17 18 19 20  
21 22 23 24  
' SS304  
37 38 39 40  
41 42 43 44  
45 46 47 48  
' LEAD  
53 54 55 56  
' BISCO NS3 -  
5 6 7 8  
9 10 11 12  
13 14 15 16  
21 22 23 24  
25 26 27 28  
29 30 31 32

' 33 34 35 36  
 37 38 39 40  
 41 42 43 44  
 45 46 47 48  
 ' HONEYCOMB  
 25 26 27 28  
 ' FOAM  
 5 6 7 8  
 13 14 15 16  
 17 18 19 20  
 21 22 23 24  
 12\*\*  
 ' FLUXDOSIUM  
 4R1.000E0  
 ' DRY FUEL  
 4R8.137E-4  
 4R2.033E-4  
 4R9.994E-3  
 4R8.656E-4  
 4R8.658E-4  
 4R2.923E-3  
 4R4.648E-4  
 4R3.255E-3  
 4R4.301E-5  
 4R4.953E-3  
 ' FC TOP DRY  
 4R1.344E-3  
 4R4.552E-3  
 4R7.138E-4  
 4R1.869E-3  
 ' BOTTOM  
 4R2.244E-3  
 4R7.345E-3  
 4R1.379E-3  
 ' AIR  
 4R3.587E-5  
 4R9.534E-6  
 ' SS304  
 4R1.728E-2  
 4R6.073E-2  
 4R7.447E-3  
 ' LEAD  
 4R3.296E-2  
 ' BISCO NS3 2 W/O B4C  
 4R4.180E-2  
 4R7.131E-4  
 4R7.871E-3  
 4R3.442E-2  
 4R8.528E-3  
 4R1.155E-3  
 4R1.351E-3  
 4R6.104E-4  
 4R2.242E-3  
 4R2.631E-4  
 ' HONEYCOMB  
 4R6.435E-3  
 ' FOAM  
 4R9.378E-3  
 4R6.746E-3  
 4R7.713E-4



4R2.026E-3  
19\$\$ F3  
22\$\$ F-1  
23\$\$ 1 2 3  
T T

**AFFIDAVIT PURSUANT  
TO 10 CFR 2.790**

Transnuclear West Inc.            )  
State of California                )     SS.  
County of Alameda                )

I, Robert M. Grenier, depose and say that I am President and Chief Operating Officer of Transnuclear West Inc., duly authorized to make this affidavit, and have reviewed or caused to have reviewed the information which is identified as proprietary and referenced in the paragraph immediately below. I am submitting this affidavit in conformance with the provisions of 10 CFR 2.790 of the Commission's regulations for withholding this information.

The information for which proprietary treatment is sought is contained in the following document:

The drawings included in Attachment 3 of this submittal and identified as proprietary.  
NUH-05-4001, Revision 11

This section of the document has been appropriately designated as proprietary.

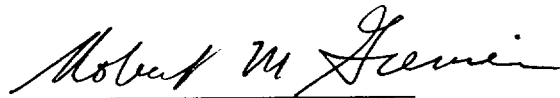
I have personal knowledge of the criteria and procedures utilized by Transnuclear West Inc. in designating information as a trade secret, privileged or as confidential commercial or financial information.

Pursuant to the provisions of paragraph (b) (4) of Section 2.790 of the Commission's regulations, the following is furnished for consideration by the Commission in determining whether the information sought to be withheld from public disclosure, included in the above referenced document, should be withheld.

- 1) The information sought to be withheld from public disclosure are licensing drawings and calculations of a concrete modular storage and transportation system, which is owned and has been held in confidence by Transnuclear West Inc.
- 2) The information is of a type customarily held in confidence by Transnuclear West Inc. and not customarily disclosed to the public. Transnuclear West Inc. has a rational basis for determining the types of information customarily held in confidence by it.
- 3) The information is being transmitted to the Commission in confidence under the provisions of 10 CFR 2.790 with the understanding that it is to be received in confidence by the Commission.
- 4) The information, to the best of my knowledge and belief, is not available in public sources, and any disclosure to third parties has been made pursuant to regulatory provisions or proprietary agreements which provide for maintenance of the information in confidence.
- 5) Public disclosure of the information is likely to cause substantial harm to the competitive position of Transnuclear West Inc. because:
  - a) A similar product is manufactured and sold by competitors of Transnuclear West Inc.

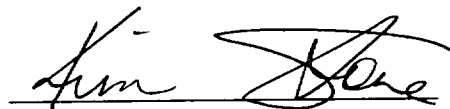
- b) Development of this information by Transnuclear West Inc. required thousands of man-hours and hundreds of thousands of dollars. To the best of my knowledge and belief, a competitor would have to undergo similar expense in generating equivalent information.
- c) In order to acquire such information, a competitor would also require considerable time and inconvenience related to the development of a design and analysis of a dry spent fuel storage system.
- d) The information required significant effort and expense to obtain the licensing approvals necessary for application of the information. Avoidance of this expense would decrease a competitor's cost in applying the information and marketing the product to which the information is applicable.
- e) The information consists of description of the design and analysis of a dry spent fuel storage and transportation system, the application of which provides a competitive economic advantage. The availability of such information to competitors would enable them to modify their product to better compete with Transnuclear West Inc., take marketing or other actions to improve their product's position or impair the position of Transnuclear West's product, and avoid developing similar data and analyses in support of their processes, methods or apparatus.
- f) In pricing Transnuclear West's products and services, significant research, development, engineering, analytical, licensing, quality assurance and other costs and expenses must be included. The ability of Transnuclear West's competitors to utilize such information without similar expenditure of resources may enable them to sell at prices reflecting significantly lower costs.

Further the deponent sayeth not.



Robert M. Grenier  
President and Chief Operating Officer  
Transnuclear West Inc.

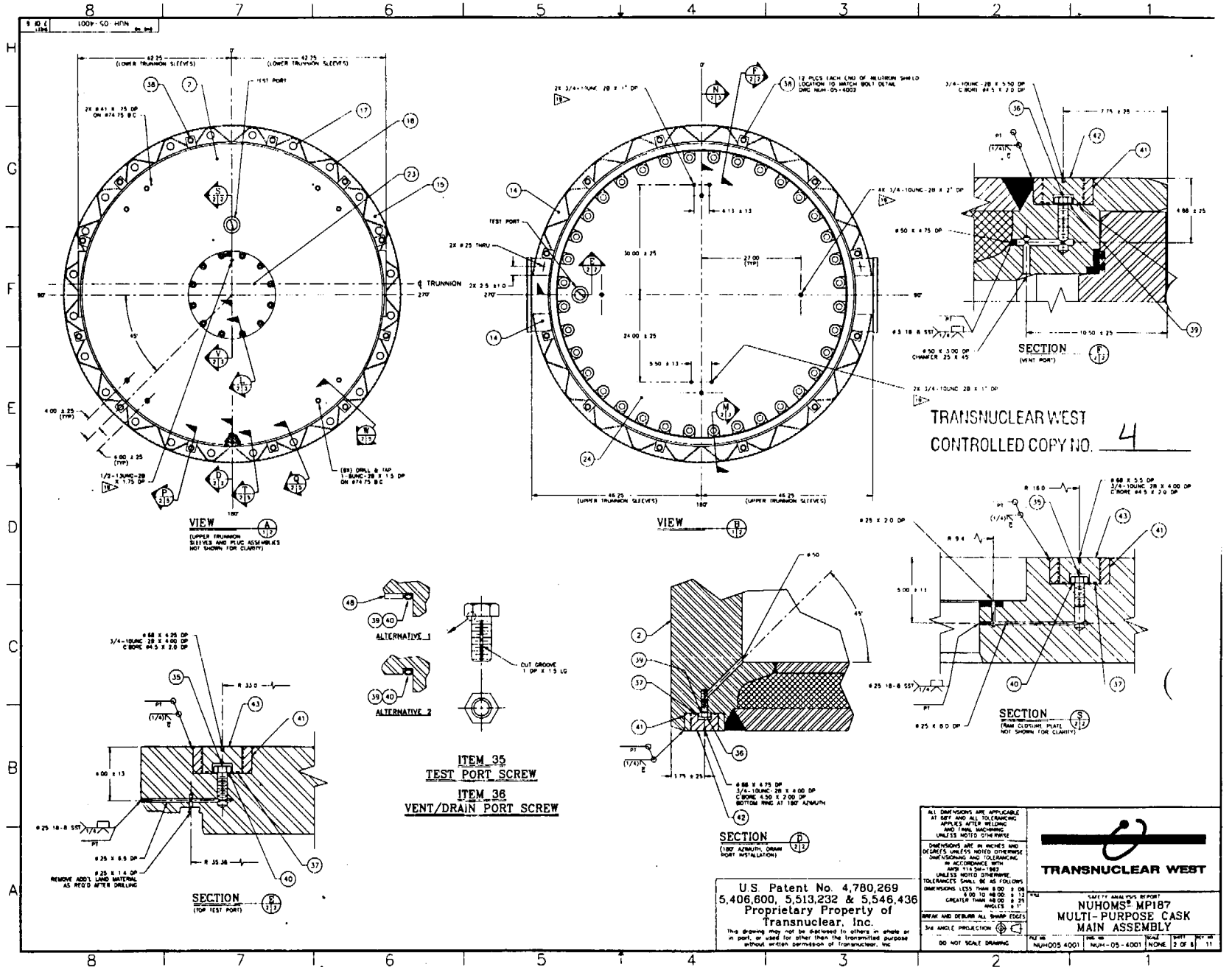
Subscribed and sworn to me before this 9<sup>th</sup> day of March, 1999, by Robert M. Grenier.



Notary Public







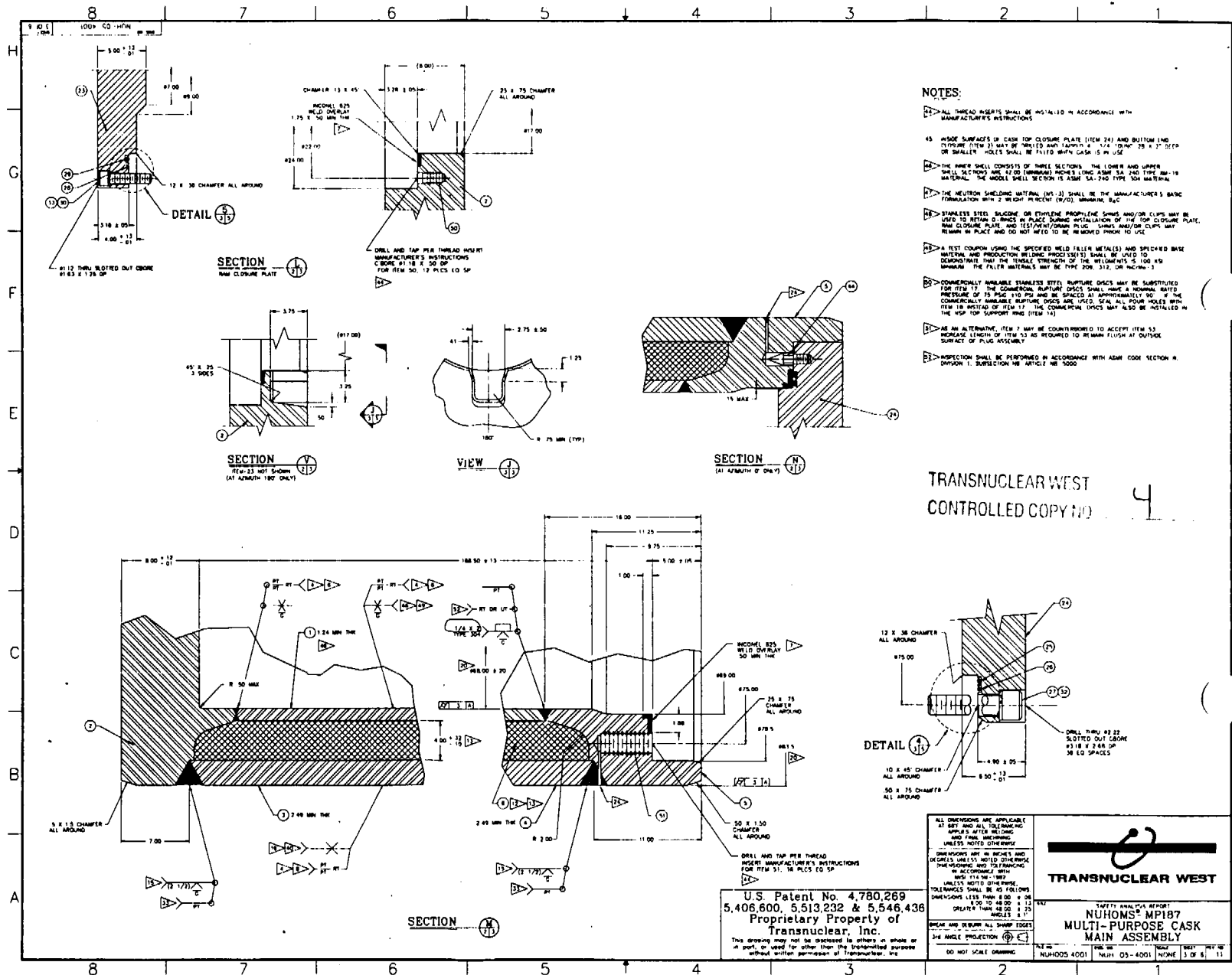
U.S. Patent No. 4,780,269  
 5,406,600, 5,513,232 & 5,546,436  
 Proprietary Property of  
 Transnuclear, Inc.  
 This drawing may not be disclosed to others in whole or in part, or used for other than the transmitted purpose without written permission of Transnuclear, Inc.

ALL DIMENSIONS ARE APPLICABLE AT SPT AND ALL TOLERANCING APPLIES AFTER WELDING AND TAPING, MACHINING UNLESS NOTED OTHERWISE.  
 DIMENSIONS ARE IN INCHES AND DECIMALS UNLESS NOTED OTHERWISE. DIMENSIONS AND TOLERANCING IN ACCORDANCE WITH ASME Y14.5M-1987.  
 UNLESS NOTED OTHERWISE, DIMENSIONS LESS THAN 8.00 ± .04 ARE TO 48.00 ± .25 GREATER THAN 48.00 ± .25 ARE TO .01.  
 SWAG AND DEBURR ALL SWAG EDGES.  
 SEE ANGLE PROJECTION.  
 DO NOT SCALE DRAWING.

**TRANSNUCLEAR WEST**

SAFETY ANALYSIS REPORT  
 NUHOMS<sup>®</sup> MP187  
 MULTI-PURPOSE CASK  
 MAIN ASSEMBLY

DATE: 12/84  
 SCALE: NONE  
 SHEET NO.: 2 OF 3  
 DRAWING NO.: NUH-005 4001  
 REV: NUH-05-4001



- NOTES:**
- 1. ALL THREAD INSERTS SHALL BE INSTALLED IN ACCORDANCE WITH MANUFACTURER'S INSTRUCTIONS.
  - 2. WIDE SURFACES OF CASE FOR CLOSURE PLATE (ITEM 24) AND BOTTOM END CLOSURE (ITEM 25) MUST BE FINISHED AND SHOWN AS 1/4" TO 1/2" x 1/2" OR SMALLER HOLES SHALL BE FILLED WITHIN CASE IS IN USE.
  - 3. THE INNER SHELL CONSISTS OF THREE SECTIONS. THE LOWER AND UPPER SHELL SECTIONS ARE 42.00 (MINIMUM) INCHES LONG AS SHOWN SA. 100 TYPE 304-18 MATERIAL. THE MIDDLE SHELL SECTION IS AS SHOWN SA. 240 TYPE 304 MATERIAL.
  - 4. THE NEUTRON SHIELDING MATERIAL (NS-3) SHALL BE THE MANUFACTURER'S BASIC FORMULATION WITH 2 WEIGHT PERCENT (W/O) BURNABLE BAC.
  - 5. STAINLESS STEEL SADDLE OR ETHYLENE PROPYLENE SHIMS AND/OR CLIPS MAY BE USED TO RETAIN 31 PILES IN PLACE DURING INSTALLATION OF THE TOP CLOSURE PLATE. MAIN CLOSURE PLATE AND TEST/RT/DORM PLUG SHIMS AND/OR CLIPS MAY REMAIN IN PLACE AND DO NOT NEED TO BE REMOVED PRIOR TO USE.
  - 6. A TEST COUPON USING THE SPECIFIED WELD FILLER METAL(S) AND SPECIFIED BASE METAL AND PRODUCTION BELOW PRODUCTION SHALL BE USED TO DEMONSTRATE THAT THE TENSILE STRENGTH OF THE WELDS IS 5,000 KSI MINIMUM. THE FILLER METALS MAY BE TYPE 305, 315, OR INCONEL-3.
  - 7. COMMERCIALLY AVAILABLE STAINLESS STEEL RIPTURE DISCS MAY BE SUBSTITUTED FOR ITEM 17. THE COMMERCIAL RIPTURE DISCS SHALL HAVE A NOMINAL RATED PRESSURE OF 75 PSIG AND BE SPACED AT APPROXIMATELY 90°. IF THE COMMERCIALLY AVAILABLE RIPTURE DISCS ARE USED, SEAL ALL FOUR HOLES WITH ITEM 18 INSTEAD OF ITEM 17. THE COMMERCIAL DISCS MAY ALSO BE INSTALLED IN THE TOP SUPPORT RING (ITEM 13).
  - 8. AS AN ALTERNATE, ITEM 7 MAY BE CONSIDERED TO ACCEPT ITEM 53 INCREASE LENGTH OF ITEM 13 AS REQUIRED TO REMAIN FLUSH AT OUTSIDE SURFACE OF PLUG ASSEMBLY.
  - 9. INSPECTION SHALL BE PERFORMED IN ACCORDANCE WITH ASME CODE SECTION 8 DIVISION 1. INSPECTION REFERENCE ARTICLE NS-1000.

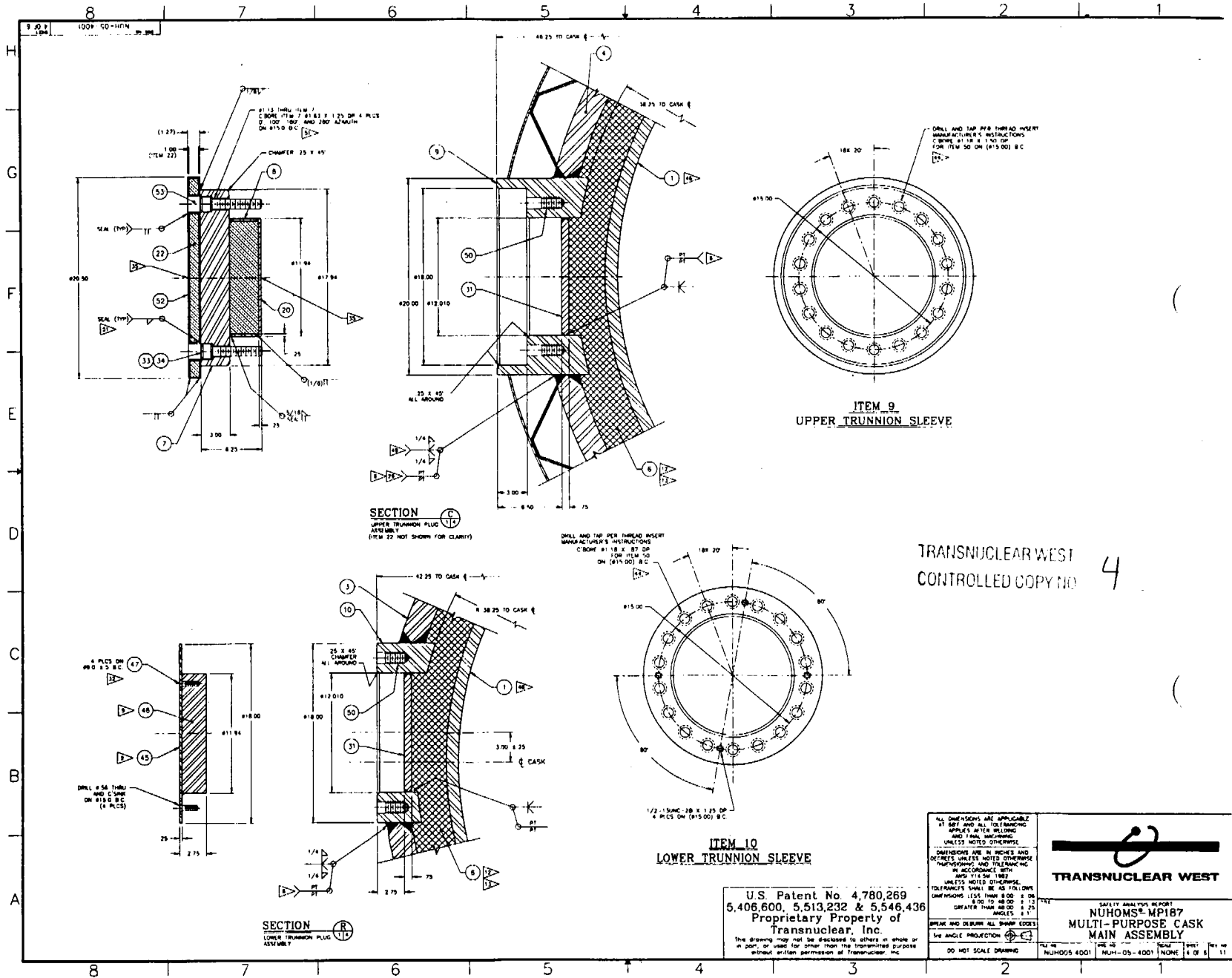
TRANSNUCLEAR WEST  
CONTROLLED COPY NO. 4

ALL DIMENSIONS ARE APPLICABLE AT 25° AND ALL DIMENSIONS APPLIES AFTER WELDING AND FINISH MECHANISM UNLESS NOTED OTHERWISE  
DIMENSIONS ARE IN INCHES AND DECIMALS UNLESS NOTED OTHERWISE THE FOLLOWING ARE TO BE ACCORDANCE WITH UNLESS NOTED OTHERWISE  
DIMENSIONS SHALL BE AS FOLLOWS  
DIMENSIONS LESS THAN 8.00 ± .015  
DIMENSIONS 8.00 TO 48.00 ± .12  
DIMENSIONS GREATER THAN 48.00 ± .25  
DIMENSIONS 1.00 ± .015  
DIMENSIONS 1.00 ± .015  
DIMENSIONS 1.00 ± .015  
DIMENSIONS 1.00 ± .015  
DO NOT SCALE DRAWING

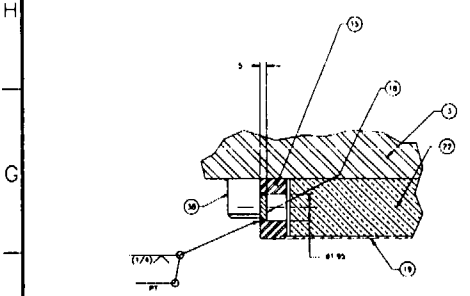


U.S. Patent No. 4,780,269  
5,406,600, 5,513,232 & 5,546,436  
Proprietary Property of  
Transnuclear, Inc.  
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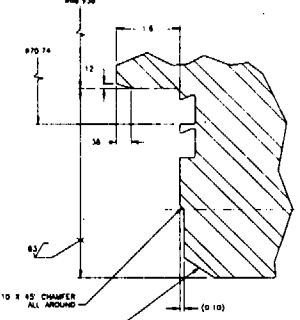
SAFETY ANALYSIS REPORT  
NUHOMS<sup>®</sup> MP187  
MULTI-PURPOSE CASK  
MAIN ASSEMBLY  
REV. 05-4001  
DATE 05-4001  
PAGE 3 OF 11



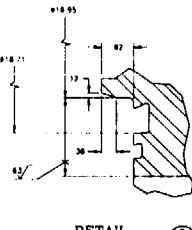
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1009-CO-NH



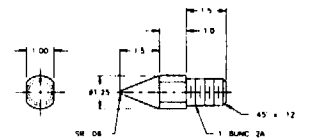
SECTION  
BOTTOM END VIEW  
(TYPICAL 17 PLCS)



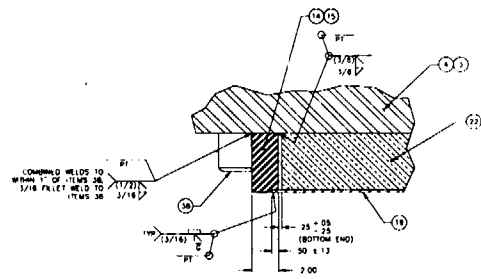
DETAIL  
TOP CLOSURE PLATE SEAL



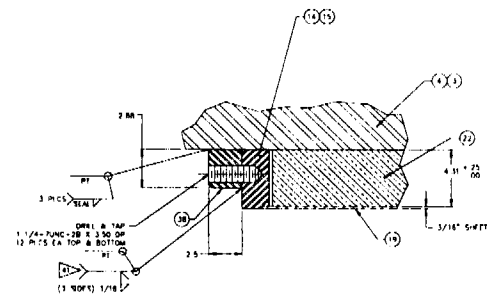
DETAIL  
NEW CLOSURE PLATE SEAL



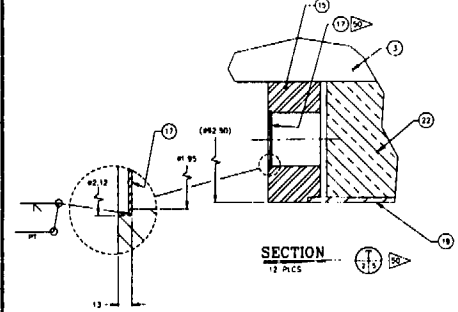
ITEM 44  
TAPERED PIN



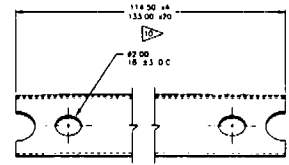
SECTION  
(TYPICAL FOR TOP AND BOTTOM  
NEUTRON SHIELD RING EXCEPT  
AS NOTED. ROTATED FOR CLARITY)



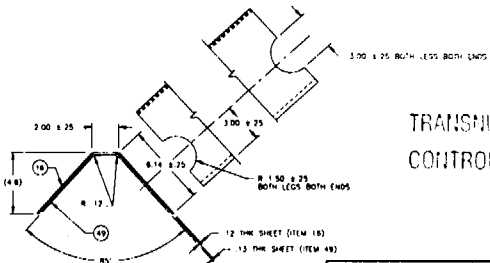
SECTION  
(TYPICAL FOR TOP AND BOTTOM  
NEUTRON SHIELD RING)



SECTION  
12 PLCS



NSP SUPPORT ANGLE ASSEMBLY  
(TYPICAL)



TRANSNUCLEAR WEST  
CONTROLLED COPY NO 4



U.S. Patent No. 4,780,289  
5,408,800, 5,513,232 & 5,546,436  
Proprietary Property of  
Transnuclear, Inc.

The drawing may not be disclosed to others in whole or in part, or used for other than the transmitted purpose without written permission of Transnuclear, Inc.

ALL DIMENSIONS ARE APPLICABLE AT SET AND ALL TO FRAMING UNLESS NOTED OTHERWISE  
DIMENSIONS ARE IN INCHES AND DECIMALS UNLESS NOTED OTHERWISE  
UNLESS NOTED OTHERWISE, DIMENSIONS SHALL BE AS FOLLOWS:  
DIMENSIONS LESS THAN 8.00 ± .06  
8.00 TO 48.00 ± .12  
GREATER THAN 48.00 ± .25  
ANGLES ± .1°  
BREAK AND DEBURR ALL SHARP EDGES  
SEE ANGLE PROJECTION  
DO NOT SCALE DRAWING

SAFETY ANALYSIS REPORT  
NUHOMS-4 MP187  
MULTI-PURPOSE CASK  
MAIN ASSEMBLY

REV SHEET  
14 NUN-05-4001 NONE 15 OF 11

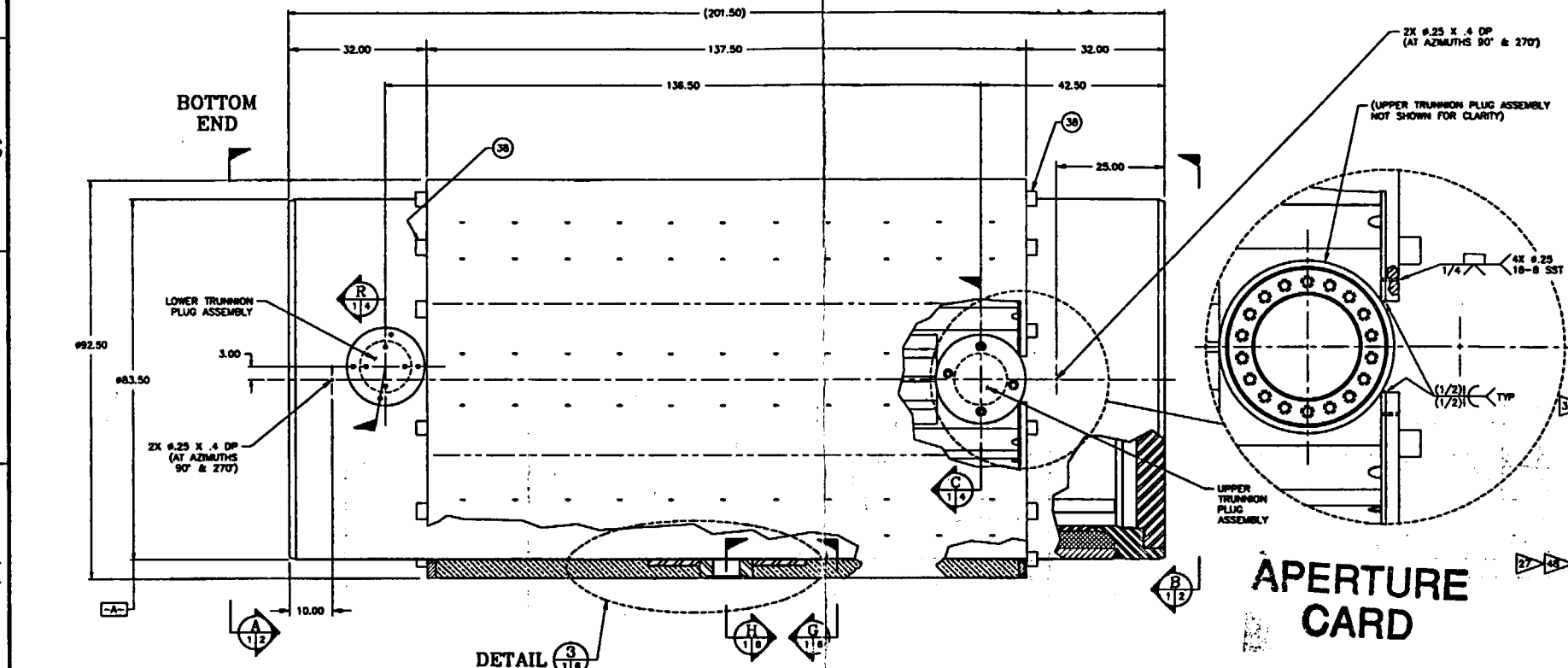




REV	DESCRIPTION	DRW...	ORIGINATED:	VERIFIED:	APPROVED:	LICENSING:
11	AMENDMENT APPLICATION	CML	03/09/99	2/1/99	2/1/99	3/9/99

TRANSNUCLEAR WEST  
CONTROLLED COPY NO. **4**

9906160084-01



ITEM NO.	QTY	PART OR IDENTIFYING NO.	NOMENCLATURE OR DESCRIPTION	MATERIAL SPECIFICATION
53	8		TUBE, LD. SIZED TO FIT ITEMS 33 & 34 (M 1/2" SCHED 40 OR SIMILAR)	STAINLESS STEEL
52	A/R		10 GA SHEET	ASTM A240 TYPE 304
51	36		SCREW THREAD INSERT 2-12UN-2B X 5.50 LG X (2.27) OD	STAINLESS STEEL
50	84		SCREW THREAD INSERT 1-BUNC-2B X 2.00 LG X (1.18) OD	STAINLESS STEEL
49	24		NSP SUPPORT ANGLE, INNER	ALUMINUM
48	2		SPACER WASHER	STAINLESS STEEL
47	16		SCREW, FLAT HD CAP SCREW 1/2-13UNC-2A X 1.0 LG	ASTM A320 GR L43
46	2		LOWER TRUNNION PLUG SHIELDING BLOCK	ASTM A240 TYPE 304
45	2		LOWER TRUNNION PLUG COVER PLATE	ASTM A564 OR 630
44	1		TAPERED PIN	ASTM A193 GR B7
43	2		TEST PORT, PLUG	ASME SA-479 TYPE 304
42	2		VENT/DRAIN PORT, PLUG	ASME SA-479 TYPE 304
41	4		TEST/VENT/DRAIN PORT, THREADED INSERT	ASME SA-479 TYPE 304
40	2		TEST PORT SEAL	METALLIC OR ELASTOMERIC
39	2		VENT/DRAIN PORT SEAL	METALLIC
38	24		IMPACT LIMITER ATTACHMENT BLOCK	ASTM A240 OR A479 TYPE 304
37	4		O-RING (2.0 ID) VENT/DRAIN/TEST PLUG	ELASTOMERIC OR METALLIC
36	2		VENT/DRAIN PORT SCREW, CAP HEX HD 3/4-10UNC-2A X 1 3/4 LG	ASTM A320 GR L43
35	2		TEST PORT SCREW, CAP HEX HD 3/4-10UNC-2A X 1 3/4 LG	ASTM A320 GR L43
34	8		SCREW, CAP HD SOC, 1-BUNC-2A 5.0 LG	ASTM A320 GR L43
33	12		HARDENED WASHER, 1.5 OD X 1.77 THK MAX	ASTM F436
32	36		HARDENED WASHER, 3.0 OD X .28 THK MAX	ASTM F436
31	4		FILLER PLATE	ASTM A240 TYPE 304
30	12		SCREW, CAP HD SOC, 1-BUNC-2A 4.5 LG	ASTM A320 GR L43
29	1		O-RING (17.5 ID); RAM CLOSURE PLATE CROSS-SECTION .425"	METALLIC
28	1		O-RING (19.4 ID); RAM CLOSURE PLATE CROSS-SECTION .248"	METALLIC OR ELASTOMERIC
27	36		SCREW, CAP HD SOC, 2-12UN-2A X 1.18 LG	ASTM A320 GR L43
26	1		O-RING (71.4 ID); TOP CLOSURE PLATE CROSS-SECTION .425"	METALLIC
25	1		O-RING (69.6 ID); TOP CLOSURE PLATE CROSS-SECTION .425"	METALLIC
24	1		TOP CLOSURE PLATE	ASTM A240 TY. 304
23	1		RAM CLOSURE PLATE	ASTM A240 TY. 304-19
22	A/R		CASTABLE NEUTRON SHIELDING MATERIAL	NS-3
21	2		RAILS, .120 THK X 4.0 WIDE	
20	2		UPPER TRUNNION PLUG BOTTOM PLATE	ASTM A240, TY. 304
19	A/R		NEUTRON SHIELD SHELL	ASTM A240 TYPE 304
18	12		PLUGS	ASTM A240, TY. 304
17	12		RUPTURE PLUG, .036 (20 GA) THK	ASTM A240, TY. 304
16	24		NSP SUPPORT ANGLE, OUTER	ASTM A240 TYPE 304
15	1		NSP BOTTOM SUPPORT RING, PLATE	ASTM A240 OR A479 TYPE 304
14	2		NSP TOP SUPPORT RING, PLATE	ASTM A240 OR A479 TYPE 304
13	2		TIE BAR	ASTM A240 TYPE 304-19
12	2		BEARING BLOCK	ASTM A240 TYPE 304-19
11	1		PAD PLATE	ASTM A240 TYPE 304-19
10	2		LOWER TRUNNION SLEEVE	ASTM A182 TYPE F304-19
9	2		UPPER TRUNNION SLEEVE	ASTM A182 TYPE F304-19
8	2		UPPER TRUNNION PLUG SIDE PLATE	ASTM A240, TY. 304
7	2		UPPER TRUNNION PLUG COVER PLATE	ASTM A240, TY. 304
6	A/R		GAMMA SHIELD	ASTM B29 LEAD
5	1		TOP FLANGE, MACHINED RING FORGING	ASTM A182, GRADE F304, F304H OR F304H
4	1		TOP STRUCTURAL SHELL, ROLLED PLATE	ASTM A240 TYPE 304-19
3	1		BOTTOM STRUCTURAL SHELL, ROLLED PLATE	ASTM A240 TYPE 304
2	1		BOTTOM END CLOSURE, MACHINED FORGING	ASTM A182, GRADE F304, F304H OR F304H
1	1		INNER SHELL, ROLLED PLATE	ASTM A240, TYPE 304 AND TYPE 304-19

**NOTES:**

- ALL WELDING SHALL BE PERFORMED IN ACCORDANCE WITH NB-4300 AND SECTION IX. WELDING PROCEDURES SHALL BE QUALIFIED IN ACCORDANCE WITH NB-4330 AND SECTION IX OF THE ASME CODE. WELDS SHOWN TO BE SMOOTH OR FLUSH SHALL HAVE A MAXIMUM REINFORCEMENT OF .03 INCHES AND HAVE A SMOOTH TRANSITION TO THE BASE MATERIAL SURFACE. FINISHED THICKNESS OF ALL GROUNDED OR MACHINED AREAS SHALL BE VERIFIED BY MECHANICAL OR ULTRASONIC MEASUREMENT.
- ALTERNATIVE WELD JOINT PREPARATIONS (U, V, OR J GROOVES) MAY BE USED PROVIDED ALL ASME CODE CRITERIA ARE MET. THE SPECIFIED MINIMUM EFFECTIVE THROAT MUST BE MAINTAINED.
- ALL WELDS SHALL BE LIQUID PENETRANT INSPECTED ON FINAL PASS IN ACCORDANCE WITH ASME CODE, SECTION III, DIVISION I, SUBSECTION NB, ARTICLE NB-5000 AND SECTION V, ARTICLE B.
- RADIOGRAPHIC INSPECTION SHALL BE PERFORMED IN ACCORDANCE WITH ASME CODE SECTION III, DIVISION I, SUBSECTION NB, ARTICLE NB-5000 AND SECTION V, ARTICLE 2. RADIOGRAPHIC INSPECTION SHALL BE PERFORMED ON THE FOLLOWING:
  - ALL LONGITUDINAL SEAM WELDS OF CASK INNER AND STRUCTURAL SHELLS.
  - ALL CIRCUMFERENTIAL SEAM WELDS OF CASK INNER AND STRUCTURAL SHELLS, EXCEPT END WELDS OF SHELL TO TOP & BOTTOM FORGINGS.
- ALL WELDS SHALL BE VISUALLY EXAMINED IN ACCORDANCE WITH NB 4424 OF ASME CODE. VISUAL WELD INSPECTORS SHALL BE QUALIFIED PER ASME CODE.
- INDICATED WELDS SHALL BE LIQUID PENETRANT INSPECTED ON ROOT AND FINAL PASSES IN ACCORDANCE WITH ASME CODE, SECTION III, DIVISION I, SUBSECTION NB, ARTICLE NB-5000, AND SECTION V, ARTICLE B.
- WELD OVERLAY SHALL BE MADE USING ERNIMON-3 OR ERNIMON-3 ELECTRODE MEETING SFA 5.14 OR SFA 5.11, RESPECTIVELY.
- CADMIUM PLATED.
- OPTIONAL CADMIUM, CHROME OR NICKEL PLATE SURFACE TO A THICKNESS OF .0005 MM/.001 MAX.
- CUT NSP SUPPORT ANGLE ASSEMBLIES TO CLEAR SHEAR KEY AS REQUIRED. TRIM NSP SUPPORT ANGLE ASSEMBLIES ADJACENT TO UPPER TRUNNION SLEEVES.
- LEAD TO BE CAST IN PLACE, CONFORMING TO ASTM B29.
- LEAD SHIELDING INTEGRITY SHALL BE DETERMINED BY GAMMA SCAN, AFTER COOL DOWN TO AMBIENT TEMPERATURE. ACCEPTANCE CRITERIA PER SECTION 8.0 OF SAR.
- NEUTRON SHIELD SUPPORT ANGLES (ITEMS 16 & 40) MAY BE FORMED AND INSTALLED AS SEPARATE PIECES. NO CONTROL OF CONTACT AREA IS REQUIRED. ALTERNATIVELY, MATERIALS MAY BE BONDED OR RIVETED TOGETHER AND PLACED AS A SINGLE ITEM.
- FINAL STRUCTURAL SHELL TO FORGING WELD SHALL BE MADE AFTER LEAD POUR AND COOL DOWN. PREVENT LEAD INGRESS TO WELD DURING WELDING USING METHODS SUCH AS: CLOSE TOLERANCE JOINTS, SHIM STOCK, OR OTHER PROVEN MEANS. PRIOR TO WELDING, CLEAN AREA TO DEMONSTRATE THERE IS NO RESIDUAL LEAD CONTAMINATION.
- LOCATION OF FULL PENETRATION LONGITUDINAL AND CIRCUMFERENTIAL SEAM WELDS IN INNER SHELL (ITEM 1), BOTTOM STRUCTURAL SHELL (ITEM 3), AND TOP STRUCTURAL SHELL (ITEM 4) MAY BE MADE AT FABRICATOR'S OPTION. LENGTH OF ITEM 4 MAY BE INCREASED TO ELIMINATE AN ADDITIONAL CIRCUMFERENTIAL WELD IN ITEM 3. ITEM 4 SHALL BE NOT LESS THAN 58.88 INCHES LONG.
- DESIGN PRESSURE IS 50 psig. CASK CONTAINMENT BOUNDARIES SHALL BE SUBJECT TO AN INTERNAL TEST PRESSURE EQUAL TO A MINIMUM OF 150% OF THE DESIGN PRESSURE PER 10 CFR 71.85(b).
- CASK CONTAINMENT BOUNDARIES SHALL BE HELIUM LEAK TESTED TO DEMONSTRATE A LEAKAGE RATE NOT TO EXCEED 1 X 10<sup>-7</sup> STANDARD CUBIC CENTIMETERS PER SECOND, IN ACCORDANCE WITH ANSI N14.3.
- INDICATED HOLES ARE PROVIDED FOR THE INSTALLATION OF A LIFT HANDLING FIXTURE FOR LIFTING AND HANDLING OF THE CASK. EACH LOCATION SHALL BE STENCILED OR OTHERWISE LABELED WITH THE FOLLOWING WARNING: "LIFT ONLY".
- CASK INNER AND STRUCTURAL SHELLS SHALL COMPLY WITH THE TOLERANCE REQUIREMENTS OF ASME CODE, SECTION III, DIVISION I, SUBSECTION NC, ARTICLE NC-4220.
- ALL SHELL JOINTS SHALL BE MADE IN ACCORDANCE WITH ASME CODE, SECTION III, DIVISION I, SUBSECTION NB, ARTICLE NB-4230.
- ANY ADDITIONAL WELDS REQUIRED TO JOIN SHELL MATERIALS SHALL BE FULL PENETRATION WELDS INSPECTED PER NOTES 3, 4 & 5.
- NOMINAL LEAD THICKNESS IS 4.0.
- OPTIONAL: WATER RELIEF HOLES SHALL BE PROVIDED AT EACH PIN AND BOLT HOLE (37 PLCS). HOLES SHALL BE .625 AND SHALL BE DRILLED TO MEET BOTTOM OF HOLE AS SHOWN. RELIEF HOLES SHALL BE TAPPED 5/8-18UNC-2B X .50 DP.
- RAILS MAY BE FABRICATED FROM SHORTER MATERIAL. FULL PENETRATION BUTT WELDS WITH SURFACE GROUND FLUSH SHALL BE PROVIDED TO FORM A CONTINUOUS RAIL. RAILS SHALL BE FORMED TO PROVIDE AT LEAST 50% SURFACE CONTACT WITH INNER SHELL (ITEM 1). MAXIMUM GAP SHALL NOT EXCEED .02. SLIDING SURFACE OF RAILS SHALL HAVE A 64 INCH RMS FINISH AND SHALL BE COATED WITH E/M CORPORATION PERMALUK RN OR EQUIVALENT DRY FILM LUBRICANT.
- STITCH WELD MAY BE CONTINUOUS TO AVOID CRACK TRAPS OR CHALK BETWEEN STITCH WELDS AND AT BOTTOM END OF RAIL (ITEM 21)
- SEAL MATERIAL METALLIC HELICOLEX HM SERIES WITH ALUMINUM JACKET INCOEL LINER AND INCOEL SPRING.
- ELASTOMERIC SEALS FOR CASK SECONDARY SEALS SHALL HAVE A CROSS-SECTIONAL DIAMETER OF .275 (ITEM 28).
- UPPER CASK TRUNNION SLEEVE TO SHELL WELDS SHALL BE LEAD TESTED TO 150% THE MAXIMUM DESIGN LOAD PRIOR TO JOINING INNER AND STRUCTURAL SHELLS.
- ALL EXPOSED WELDS MAY BE GROUND SMOOTH TO ENHANCE CASK DECONTAMINATION.
- RAIL MATERIAL: NITRONIC 80, SHEET, COLD REDUCED, ASTM A240, GRADE UNS S21800, RC 29-35, OR EQUIVALENT.
- MATERIAL FOR ITEM 45 MAY BE 18-8 STAINLESS STEEL OR ASTM A564 OR 630; ITEM 46 MAY BE 18-8 SST OR ASTM A240 TYPE 304.
- INDICATED WELD SHALL BE LIQUID PENETRANT INSPECTED ON ROOT PASS, FINAL PASS, AND EACH LAYER OF WELD DEPOSITION, IN ACCORDANCE WITH ASME CODE, SECTION III, DIVISION I, SUBSECTION NB, ARTICLE NB-5000, AND SECTION V ARTICLE 6. RADIOGRAPHIC OR ULTRASONIC EXAMINATION MAY BE SUBSTITUTED FOR SPECIFIED PT PROVIDED ALL ASME CODE CRITERIA ARE MET.
- ADDITIONAL NEUTRON SHIELD FOUR HOLES MAY BE ADDED TO ITEMS 14 & 15 AND CLOSED PER SECTION 00 WITHOUT ITEM 38.
- FABRICATOR MAY ELECT TO USE FOUR HOLES IN FACE TO PLACE NSL WELD PLUG AFTER NSL HAS SET AT LEAST 48 HOURS. PROVIDE 1/2" VENT HOLE IN CENTER OF PLATE AS PERMANENT VENT.
- FOR ON-SITE FUEL TRANSFER OPERATIONS PERFORMED UNDER 10CFR72 REQUIREMENTS, O-RINGS ARE NOT REQUIRED TO BE INSTALLED. FOR ON-SITE FUEL STORAGE MODE PER 10CFR72 REQUIREMENTS, ALL O-RINGS SHALL BE METALLIC. FOR PART 71 TRANSPORTATION, METALLIC SEALS SHALL BE USED FOR ALL PRIMARY CONTAINMENT SEALS. EITHER METALLIC OR ELASTOMERIC MATERIAL MAY BE USED FOR SECONDARY SEALS AS DESCRIBED IN THE PARTS LIST.
- BACKING BAR MAY BE FORMED BY MACHINING A RECESS IN ITEMS 12 & 13 NOT TO EXCEED .50" WIDE.
- A ONE SIDED FULL PENETRATION BEVEL WELD WITH 3/8" MAX ROOT GAP PLUS 1/2" FILLET MAY BE SUBSTITUTED FOR DOUBLE BEVEL WELD.
- ASME SA-182, TYPE F304-19 FORGINGS MAY BE SUBSTITUTED FOR SPECIFIED PLATE MATERIAL.
- LONGITUDINAL WELD IN TOP STRUCTURAL SHELL MAY BE MADE WITH ELECTRODE COMPATIBLE WITH TYPE 304 MATERIALS PROVIDED IT IS LOCATED AT 90° ±15° FROM UPPER TRUNNION SLEEVE CENTERLINE.
- IMPACT LIMITER ATTACHMENT BLOCKS (ITEM 30) SHALL BE JOINED TO NSP SUPPORT RINGS (ITEMS 14 AND 15) WITH FULL PENETRATION WELDS. ALTERNATIVELY, THE ATTACHMENT BLOCKS AND SUPPORT RINGS MAY BE MACHINED FROM PLATE OR BAR.
- SILVER PLATED STAINLESS STEEL TUBULAR O-RING CROSS-SECTION .0062 INCH PRECOMPRESSED TO .0052 INCH, PRIOR TO PLATING.
- SUPPORT RINGS, ITEM 14 AND 15, MAY BE FABRICATED FROM SEGMENTS JOINED BY FULL PENETRATION WELDS, WITH SURFACE PT EXAMINATION.

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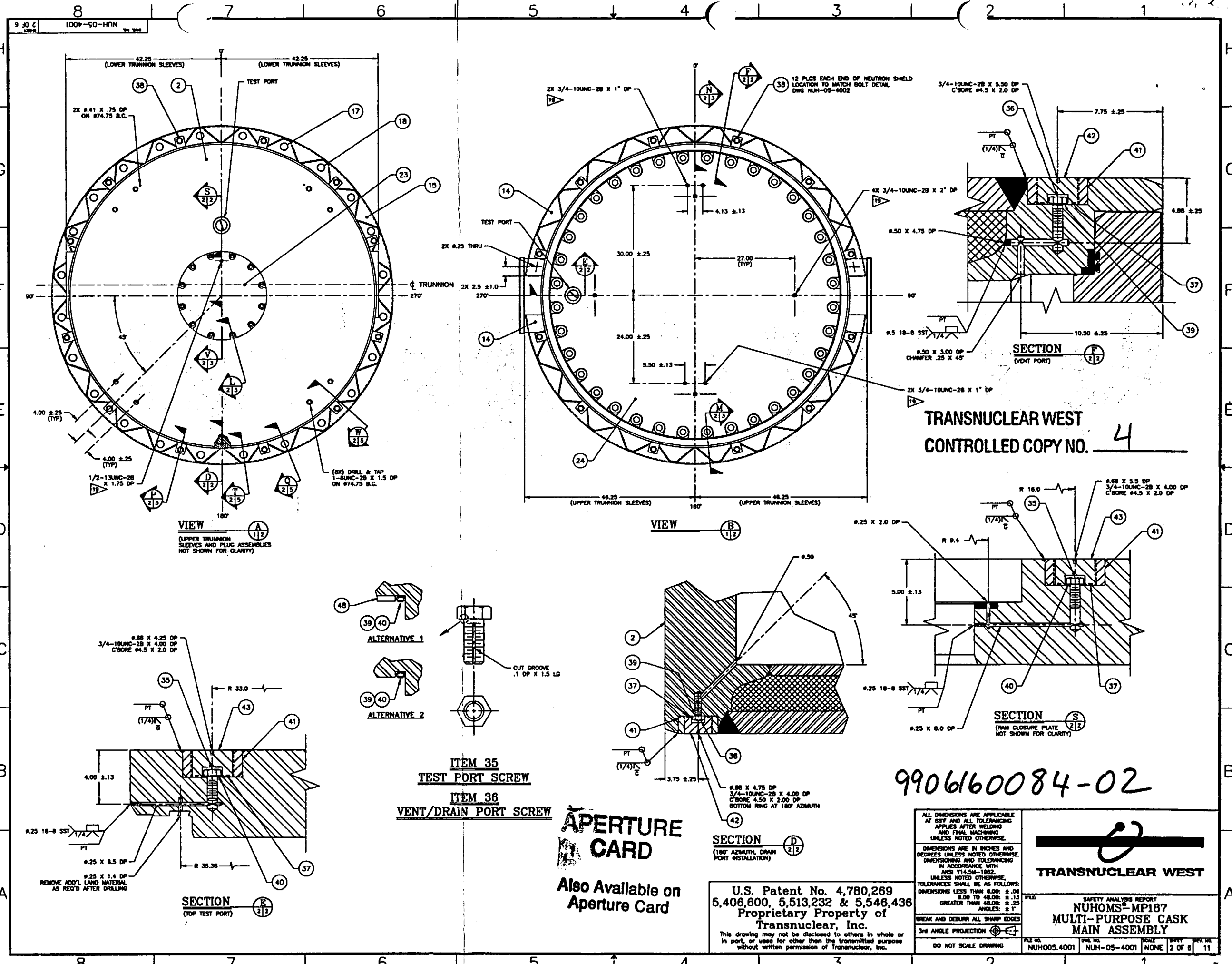
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5,406,600, 5,513,232 & 5,546,436  
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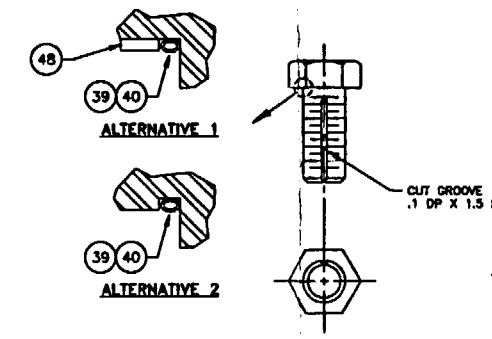
SAFETY ANALYSIS REPORT  
**NUHOMS-187**  
MULTI-PURPOSE CASK  
MAIN ASSEMBLY

REVISIONS: 1 OF 8



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ITEM 35  
TEST PORT SCREW

ITEM 36  
VENT/DRAIN PORT SCREW

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SECTION  
(180° AZIMUTH, DRAIN  
PORT INSTALLATION)

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AND FINAL MACHINING  
UNLESS NOTED OTHERWISE.

DIMENSIONS ARE IN INCHES AND  
DEGREES UNLESS NOTED OTHERWISE.  
DIMENSIONING AND TOLERANCING  
IN ACCORDANCE WITH  
ANSI Y14.5M-1982.

UNLESS NOTED OTHERWISE,  
TOLERANCES SHALL BE AS FOLLOWS:  
DIMENSIONS LESS THAN 8.00: ± .08  
8.00 TO 48.00: ± .13  
GREATER THAN 48.00: ± .25  
ANGLES: ± 1°

BREAK AND DEBURR ALL SHARP EDGES

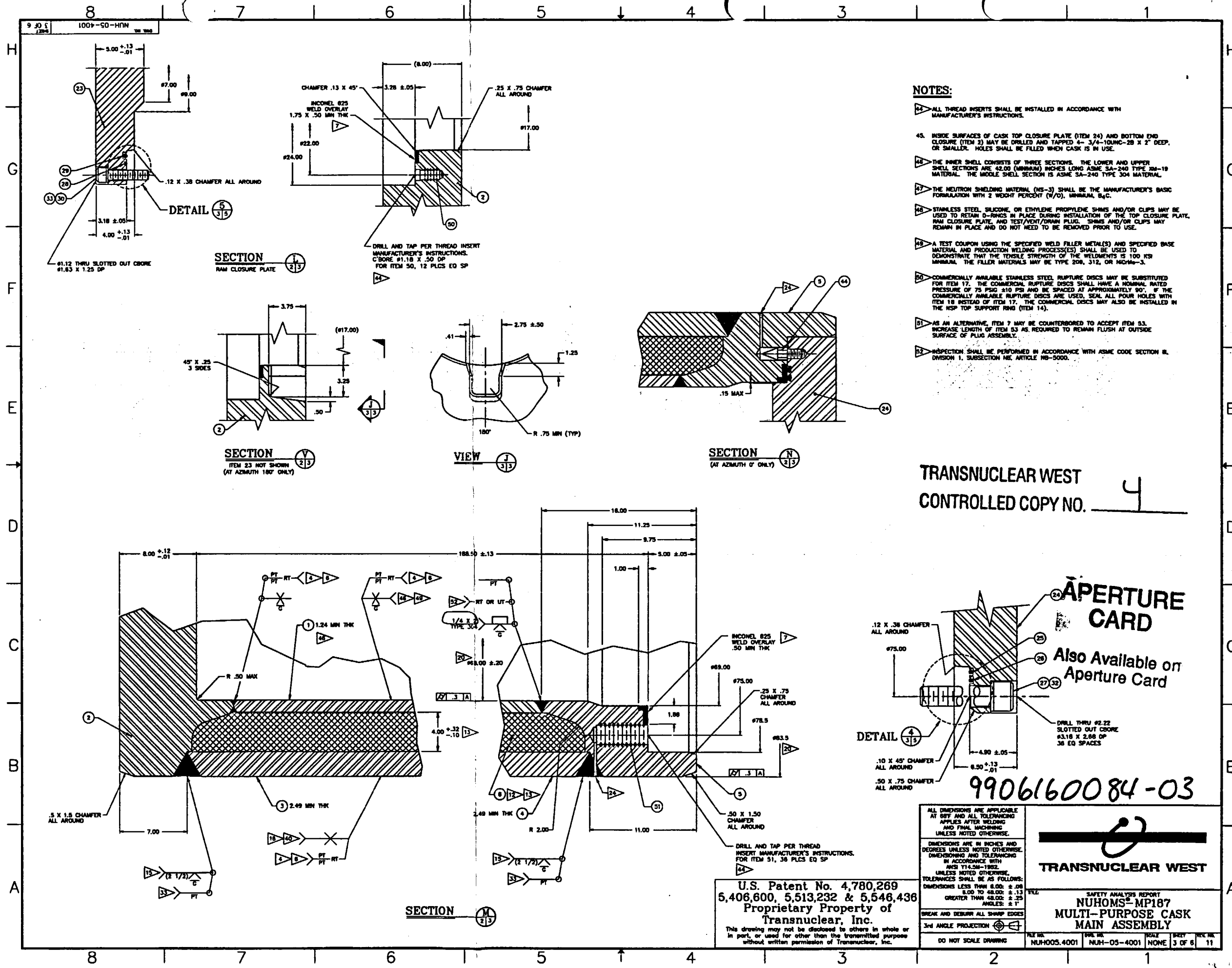
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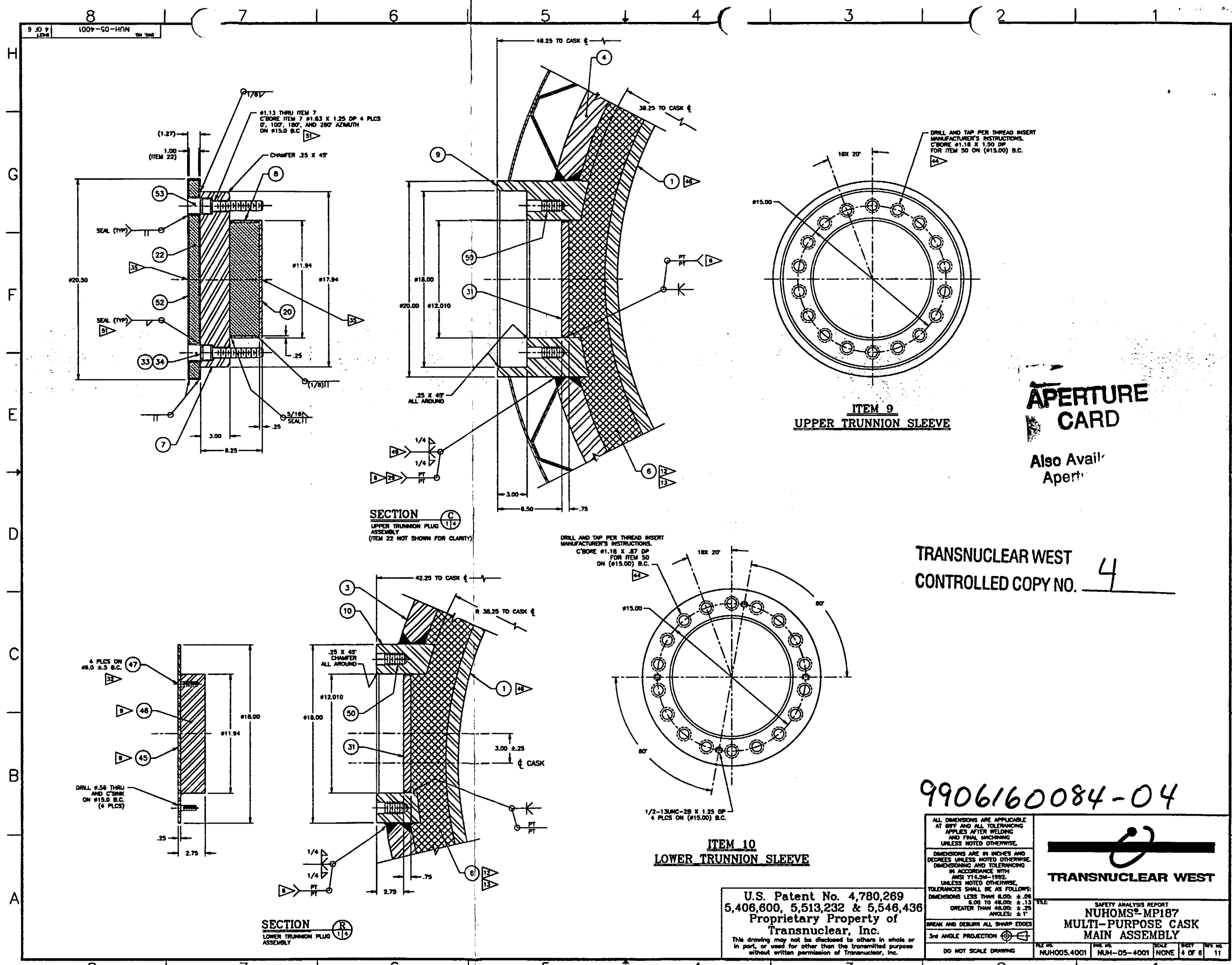
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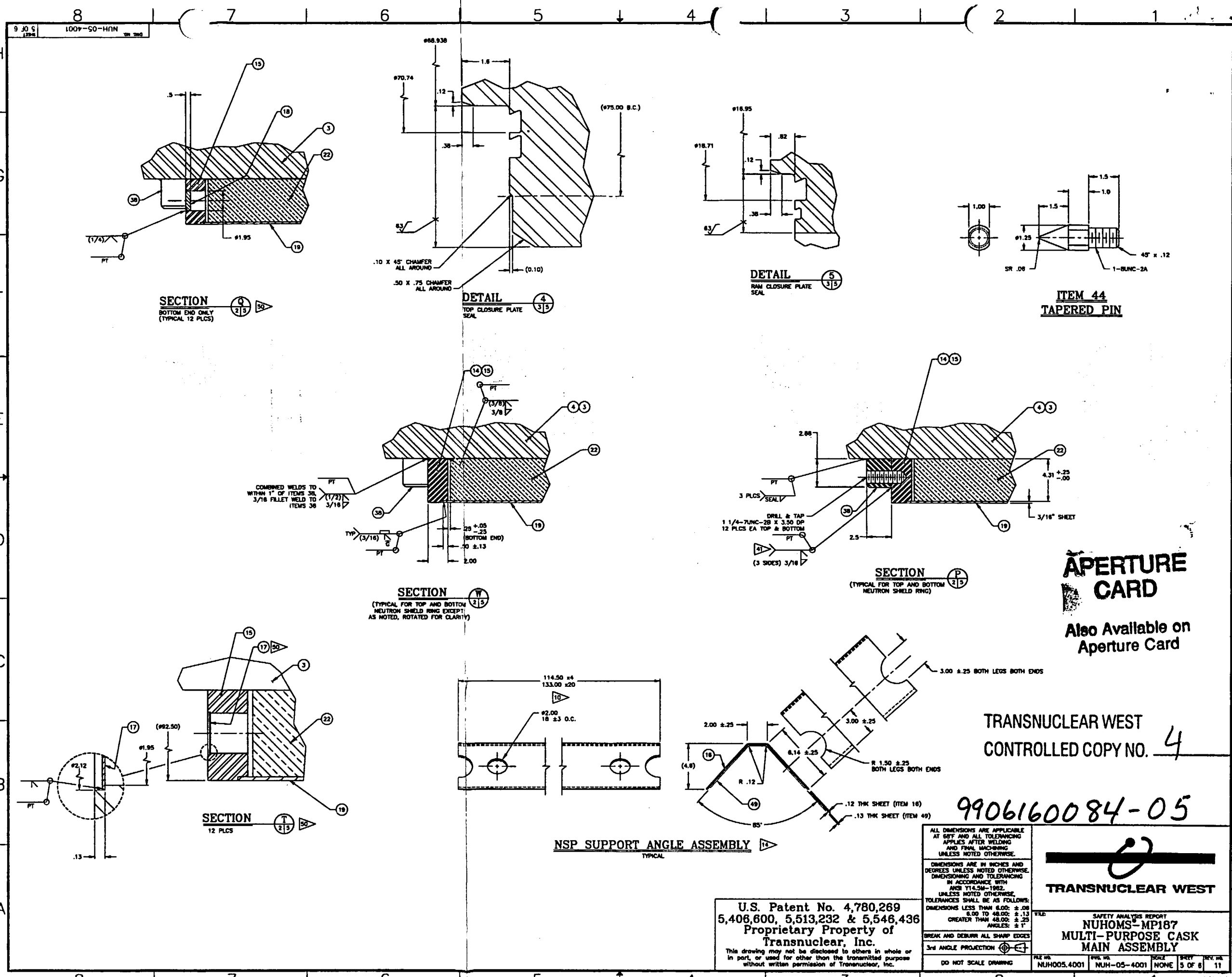


- NOTES:**
- 44 ALL THREAD INSERTS SHALL BE INSTALLED IN ACCORDANCE WITH MANUFACTURER'S INSTRUCTIONS.
  - 45 INSIDE SURFACES OF CASK TOP CLOSURE PLATE (ITEM 24) AND BOTTOM END CLOSURE (ITEM 2) MAY BE DRILLED AND TAPPED 4- 3/4-10UNC-2B X 2" DEEP, OR SMALLER. HOLES SHALL BE FILLED WHEN CASK IS IN USE.
  - 46 THE INNER SHELL CONSISTS OF THREE SECTIONS. THE LOWER AND UPPER SHELL SECTIONS ARE 42.00 (MINIMUM) INCHES LONG ASME SA-240 TYPE 304-19 MATERIAL. THE MIDDLE SHELL SECTION IS ASME SA-240 TYPE 304 MATERIAL.
  - 47 THE NEUTRON SHIELDING MATERIAL (NS-3) SHALL BE THE MANUFACTURER'S BASIC FORMULATION WITH 2 WEIGHT PERCENT (W/O) MINIMUM B<sub>4</sub>C.
  - 48 STAINLESS STEEL, SILICONE, OR ETHYLENE PROPYLENE SHIMS AND/OR CLIPS MAY BE USED TO RETAIN O-RINGS IN PLACE DURING INSTALLATION OF THE TOP CLOSURE PLATE, RAM CLOSURE PLATE, AND TEST/VENT/DRAIN PLUG. SHIMS AND/OR CLIPS MAY REMAIN IN PLACE AND DO NOT NEED TO BE REMOVED PRIOR TO USE.
  - 49 A TEST COUPON USING THE SPECIFIED WELD FILLER METAL(S) AND SPECIFIED BASE MATERIAL AND PRODUCTION WELDING PROCESS(ES) SHALL BE USED TO DEMONSTRATE THAT THE TENSILE STRENGTH OF THE WELDMENTS IS 100 KSI MINIMUM. THE FILLER MATERIALS MAY BE TYPE 208, 312, OR NCM-3.
  - 50 COMMERCIALY AVAILABLE STAINLESS STEEL RUPTURE DISCS MAY BE SUBSTITUTED FOR ITEM 17. THE COMMERCIAL RUPTURE DISCS SHALL HAVE A NOMINAL RATED PRESSURE OF 75 PSIG ±10 PSIG AND BE SPACED AT APPROXIMATELY 90°. IF THE COMMERCIALY AVAILABLE RUPTURE DISCS ARE USED, SEAL ALL FOUR HOLES WITH ITEM 18 INSTEAD OF ITEM 17. THE COMMERCIAL DISCS MAY ALSO BE INSTALLED IN THE NSP TOP SUPPORT RING (ITEM 14).
  - 51 AS AN ALTERNATIVE, ITEM 7 MAY BE CONTIGUOUS TO ACCEPT ITEM 53. INCREASE LENGTH OF ITEM 53 AS REQUIRED TO REMAIN FLUSH AT OUTSIDE SURFACE OF PLUG ASSEMBLY.
  - 52 INSPECTION SHALL BE PERFORMED IN ACCORDANCE WITH ASME CODE SECTION II, DIVISION 1, SUBSECTION NB, ARTICLE NB-5000.

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**SECTION Q**  
BOTTOM END ONLY  
(TYPICAL 12 PLCS)

**DETAIL 4**  
TOP CLOSURE PLATE SEAL

**DETAIL 5**  
RAM CLOSURE PLATE SEAL

**ITEM 44**  
**TAPERED PIN**

**SECTION W**  
(TYPICAL FOR TOP AND BOTTOM NEUTRON SHIELD RING EXCEPT AS NOTED, ROTATED FOR CLARITY)

**SECTION P**  
(TYPICAL FOR TOP AND BOTTOM NEUTRON SHIELD RING)

**SECTION T**  
12 PLCS

**NSP SUPPORT ANGLE ASSEMBLY**  
TYPICAL

**APERTURE CARD**

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