# Final Status Survey Report for Building Footers 21, 22, 34 and 36 and the 2W Ramp Concrete at the Molycorp Site

Washington, PA



**Revision - 0** Dated 10/09/02

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**Reviews:** 

MACTEC Radiological Engineer

MACTEC Radiological Engineering/H&S Manager

ACTEC Project Manager

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#### 1.0 BACKGROUND INFORMATION

Molycorp, Inc.'s (Molycorp) predecessor, the Molybdenum Corporation of America, was formed from the Electric Reduction Company in Washington, Pennsylvania on June 16, 1920. The facility was purchased to manufacture ferroalloys.

Molybdenum manufacturing began in the 1920s. Processing of this material was idled in 1991. Although primarily manufacturing molybdenum products, the plant also produced ferrocolumbium (FeCb, 1964 to 1971), as well as other ferroalloys, e.g., tungsten.

In February 2002, site decommissioning and demolition was initiated for aboveground structures and buildings. Building final status surveys (FSS) were initiated in mid February, building demolition started in May 2002. Initially, each building or area located in a building was a single survey unit that included the foundation and shell/structure. After completing the FSS for the first set of buildings, it was realized that by combining the foundation and structure into a single survey unit, the completion of the NRC independent verification (IV) survey and release from radiological controls was delayed. In order to facilitate and expedite NRC IV surveys and the release of radiological controls, all subsequent building FSS consisted of independent surveys for the building's foundation and the shell/structure.

During subsequent visits by the NRC, IV surveys were performed of the building's shell and structural materials but not the foundations of the buildings.

Building shells/structures were demolished and the construction debris was removed from site or controlled as radioactive material

#### 2.0 SITE INFORMATION

#### 2.1 SITE DESCRIPTION

The Molycorp, Inc. project site (the site) is located in southwestern Pennsylvania on the outskirts of Washington County approximately 35 miles southwest of Pittsburgh. The site is separated from the populated City's urbanized area by the ramps and structures associated with Interstate 70 (I-70). The region is generally comprised of towns located close to transportation corridors surrounded by agricultural lands and open areas

The current work site consists of approximately 8 acres that is located inside a 20 acre fenced portion of the 59-acre parcel owned by Molycorp that lies entirely within Canton Township at 300 Caldwell Avenue, Washington, Pennsylvania, 15301. The fenced area is situated between 1,010 and 1,045 feet above mean sea level with relatively flat topography.

Molycorp's property has frontage along two dedicated public streets in Canton Township – Caldwell Avenue and Weirich Avenue. The site is transversed by Chartiers Creek that flows south to north through the property. The property is served by the CSX operated railroad via two lines that were formerly owned by the Tylerdale Connecting Railroad Company and the Baltimore and Ohio Railroad.

Adjacent property owners can be classified into three major categories on the current use of the land residential, industrial, and public. The residential property lies to the east of the site on Green Street and to the west along Weirich Avenue. The industrial property is located predominately north of the site and includes property under the ownership of the Findlay Refractories Company and Allegheny Ludlum Corporation. Darrt Development Company owns several scattered parcels located to the south and east of the site. Land under public ownership includes the Canton Township Volunteer Fire Company property, the right-of-way for I-70, and other public streets. The Washington Institute of Technology owns a vacant 38acre parcel adjacent to the southwestern property line

#### 2.2 SITE CONDITIONS AT TIME OF FOUNDATION SURVEY

As part of the past decommissioning activities, building structural materials have been removed and processed, either as clean construction debris or as radiological waste. Clean construction debris has been continually removed from site as building materials and concrete foundations have been cleared from radiological controls by the NRC. Radiological waste has been segregated and stored on-site for final disposal activities. Shipping of radiological waste began in early October, 2002. Radioactive waste shipments will continue through job completion.

#### 2.3 GROUNDS

The Molycorp Washington, PA facility produced a ferrocolumbium alloy from Brazilian ore (pyrochlore) between 1946 and 1970. While the use of pyrochlore was commonplace by that time, this particular ore contained thorium as an accessory metal. The thorium was also in concentrations that required Molycorp to acquire a Source Materials License. This operation resulted in the production of a thorium-bearing slag. A portion of this slag was ball-milled (turned into a granular powder) and used as fill over portions of the site

While significant amounts of this slag have been removed from the site, remaining slag in soil continued to play a significant role in the survey and release of buildings on-site. Building steel walls and concrete floors showed significant readings above "normal" background levels when surveyed by hand-held or portable detectors

Because this elevated background condition exists at the Molycorp site, MACTEC devised instrument detector windows for some of their instruments and used them in areas where thorium slag in soil created a background nuisance during survey activities.

#### 2.4 FOUNDATION CLASSIFICATION

All foundations do not have the same potential for residual contamination and therefore do not require the same level of survey coverage For purposes of establishing the degree of survey effort required, building foundations have been segregated into affected and unaffected foundations.

- Affected foundation: Foundations that have a potential for surface residual contamination from contact with underlying soils
- Unaffected foundation: Foundations not classified as affected.

Foundation Classification <sup>(1)</sup>	Building Number	Radiological Information	
U	1	Concrete floor. Underside of slab identified as contaminated above release limits	
U	2	Concrete floor. Not yet released by NRC. Building foundation is not located on contaminated fill.	
U	2W	Concrete floor. Not yet released by NRC. Building foundation is not located on contaminated fill.	
U	2 Train Bay	Concrete floor. Not yet released by NRC. Building foundation is not located on contaminated fill.	
U	13	Slab final status surveyed and released by NRC.	
U	14	Concrete floor. Not yet released by NRC. Building foundation is not located on contaminated fill.	
U	19	Concrete floor. Not yet released by NRC. Building foundation is not located on contaminated fill.	
U	21	Slab final status surveyed and released by NRC.	
U	22	Concrete floor. Underside of slab identified as contaminated above release limits.	
U	23	Slab final status surveyed and released by NRC.	
U	25	Slab final status surveyed and released by NRC.	
U	26	Concrete floor. Not yet released by NRC. Building foundation is not located on contaminated fill.	
А	28	Concrete floor. Not yet released by NRC. Building foundation is located on contaminated fill.	
U	29	Concrete floor. Underside of slab identified as contaminated above release limits.	
U	31	Concrete floor. Topside of slab identified as contaminated above release limits.	
А	32	Concrete floor. Underside of slab identified as contaminated above release limits.	
A	33	Slab final status surveyed and released by NRC.	
Α	34	Concrete floor. Underside of slab identified as contaminated above release limits.	
А	35	Slab final status surveyed and released by NRC.	

TABLE 1 - CLASSIFICATION OF BUILDING	FOUNDATION
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A	36	Slab final status surveyed and released by NRC.	
U	37	Concrete floor. Underside of slab identified as contaminated above release limits	
A	38	Concrete floor. Not yet released by NRC. Building foundation is located on contaminated fill.	
A	39	Concrete floor. Not yet released by NRC. Building foundation is located on contaminated fill.	
А	42	Slab final status surveyed and released by NRC.	

(1) Building foundation classification is derived from building location, obtained from Molycorp's Material License, Amendment No. 5, SMB-1393.

#### 2.5 SURVEY UNITS

Each building foundation was considered an individual survey unit for final status survey purposes. Determination of compliance with the average unrestricted use limits was evaluated on a survey unit basis. Each survey unit must be shown to meet the average surface contamination and exposure rate limits at a 95% confidence.

#### 3.0 DECOMMISSIONING ACTIVITIES

Decommissioning activities of the buildings on site were performed as a "first step" to release the site for unrestricted future use. The scope of work during this phase includes D and D of all above surface structures.

#### 3.1 **OBJECTIVES**

The objectives for this phase of D and D activities included.

- Removal of equipment and surplus supplies from buildings
- Characterization of hazards associated with the buildings (performance of effective radiological surveys)
- · Remediation or disposal of hazards identified in the characterization process
- Completion of Final Status Survey
- Unrestricted release of buildings
- Demolition of buildings

#### 3.2 **RESULTS OF PREVIOUS SURVEYS**

Numerous radiological studies and surveys have been conducted at the Molycorp Washington, PA site. Since the late 1960s, regulatory requirements and pressure from local agencies have driven surveys and studies of the hazards associated with the production of various ferroalloys. Listed below is a brief history of the previous surveys performed on the Molycorp site:

Applied Health Physics, Inc. was contracted by Molycorp to conduct a series of leaching studies on ferrocolumbium slag during the late 1960s These studies indicated that radioactive materials were fixed and would not leach into the groundwater in excess of prescribed limits. During this period, Molycorp applied unsuccessfully to the Pennsylvania Department of Health's Industrial Wastes Section and AEC for an onsite burial permit. Ferrocolumbium slag cleanup was concentrated in the early to mid-1970s time frame.

In June 1971, an AEC compliance inspection revealed that thorium-bearing slag had been inadvertently buried onsite in violation of the terms and conditions of their license and AEC regulations. The AEC issued a Notice of Violation and requested Molycorp to take remedial action to excavate these materials and dispose of them in accordance with AEC regulations and guidance documents. Applied Health Physics was contracted to perform a thorough radiological survey of the site and to provide health physics and waste disposal services necessary to comply with AEC's request. Survey measurements indicated exposure levels at 1.2 mR/hr in some areas.

In 1972, thoriated material from the site was disposed of at the West Valley, New York, burial site. The disposal was terminated when New York officials decided that the volume of waste was too large and the contamination level insignificant to use up valuable burial area Molycorp performed cleanup operations to segregate and stabilize the remaining thoriated material in a capped pile containing about 27,700 cubic yards of slag on the south property. A 1975 Applied Health Physics, Inc. report indicated the average concentration of thorium-232 in the slag pile was 1,250 pCi/g, with exposures within the 0.2 mR/hr Nuclear Regulatory Commission maximum level allowed at the time (AEC was reorganized as the NRC in 1974). This pile was eventually removed and disposed of.

In 1978, one of two molybdenum-roasting furnaces was shut down as part of a consent decree with the Pennsylvania Department of Environmental Resources (PADER) Air Quality Agency due to exceedances of SO<sub>2</sub> standards. All remaining processes continued until 1991.

Oak Ridge Associated Universities, an NRC contractor, conducted a radiological survey of the site in 1985. The survey identified elevated (twice background or greater) levels of thorium in the dikes that separated the surface impoundments, and indicated the potential of subsurface thoriated slags in the western portion of the site.

RSA, Inc. conducted a subsurface survey for Molycorp in 1990 to characterize the thorium contamination across the western portion of the site (i.e., the impoundment area), and the areas immediately to the north, west, and northwest. Thirty-two holes were drilled on the site and radiation measurements were logged at every six inches of depth from the surface down to bedrock, both above and below water table. Radiation levels were also logged in monitoring wells previously drilled on the site. In addition to the subsurface survey, RSA, Inc. conducted a survey of the radiation exposure rates inside the study area. This survey consisted of approximately 400 measurements of the gamma radiation field at a height of one meter above

ground level Findings reveled that, in general, the subsurface concentrations of thorium were above those in the surface soils in almost every hole drilled. A general pattern was that the underground radiation levels decreased to background at a depth of about ten feet. While a majority of the holes exhibited concentrations of greater than 0.01 percent thorium, in only a few holes did the thorium content exceed an average of 0.05 percent at some point below the surface of the ground.

Foster Wheeler Environmental Corporation conducted a site characterization of the Molycorp Washington, PA site in 1994 and published its report titles "Site Characterization Report for License Termination of the Washington, PA Facility, 1995." This three-volume report was conducted to meet the Site Characterization Plan's objectives

- To determine the extent of the distribution of thoriated residues on the site, in the structures and in the environmental media.
- To determine the rate(s) of migration, if any, of thorium or its daughters through various pathways to man.
- To assess associated non-radiological constituents and determine their affects on the radiological constituents and potential impacts on decommissioning
- To quantify parameters that affect potential human exposure to existing site radiological materials
- To support evaluation of alternative decommissioning actions and detailed planning of a preferred approach for decommissioning, decontamination, and waste disposal.

#### 3.3 DECONTAMINATION PROCEDURES

Building foundations and equipment footings found to contain radioactivity above the release limits were not normally decontaminated. Concrete and foundation materials found to have elevated levels of radioactivity were controlled as radioactive material, are temporarily stored on site, and will ultimately be disposed of as radioactive waste.

#### 4.0 FINAL SURVEY PROCEDURES

The basis of the Molycorp radiological survey design conformed to NUREG/CR 5849, "Manual for Conducting Radiological Surveys in Support of License Termination," RSI's "Decommission Plan for the Washington, PA Facility, Part 1 Revision," and the requirements of Molycorp's "U.S. Nuclear Regulatory Commission Material License, Amendment No. 5, SMB-1393." These references provide adequate information and sampling requirements to ensure a proper survey had been planned and performed. The requirements listed in these references were compiled into a sampling plan (MACTEC's "Concrete Sample and Management Plan") and used as the guidance document for sampling instructions.

#### 4.1 SAMPLING PARAMETERS

Sampling parameters were identified from NUREG/CR 5849, "Manual for Conducting Radiological Surveys in Support of License Termination," RSI's "Decommission Plan for the Washington, PA Facility, Part 1 Revision," and the requirements of Molycorp's "U.S. Nuclear Regulatory Commission Material License, Amendment No. 5, SMB-1393."

Survey results were obtained and used for comparison against the limits for unrestricted release, as defined in the site's NRC License.

Table 2 identifies the release limits of the license.

Radionuclide <sup>(1)</sup>	Average	Maximum	Removable
U-nat, U-235, U-238, and associated decay products	5,000 α	15,000α	1,000α
Transuranics, Ra-226, Ra-228, Th-230,	100	300	20
Th-228, Pa-231, Ac-227, I-125, I-129			
Th-nat, Th-232, Sr-90, Ra-223, Ra-224, U-232, I- 126, I-131, I-133	1,000	3,000	200
Beta-gamma emitters (nuclides with decay modes other than alpha emission or spontaneous fission) except Sr-90 and others noted above	5,000	15,000	1,000

#### TABLE 2 - ACCEPTABLE SURFACE CONTAMINATION LEVELS (DPM/100CM<sup>2</sup>)

(1) Where surface contamination by both alpha and beta-gamma emitting nuclides exist, the limits established for alpha and beta-gamma emitting nuclides should apply independently.

Even though limited quantities of natural uranium has been identified at the Washington, PA site, and is included as a part of the site's NRC License, the more restrictive limits for release (for surface activity) are for the natural thorium radionuclide, which is the significant radionuclide of concern Therefore, the limits for release are due to the natural thorium radionuclide, and the limits are 1,000 dpm/100cm<sup>2</sup> average, 3,000 dpm/100cm<sup>2</sup> maximum and 200 dpm/100cm<sup>2</sup> removable

Because both alpha and beta radiations are a product of the decay of natural thorium (in equilibrium), the limits listed above apply independently to both alpha radiation and beta radiation

Due to the inherent difficulty of properly quantifying the alpha radiation component during the decay of natural thorium when using a hand-held instrument, a ratio of alpha decays to beta decays was identified and beta radiation was used as a surrogate to quantify the alpha activity. This was not the case for determining removable contamination. The Ludlum 2929 was calibrated and set up for the measurement of both alpha and beta radioactivity.

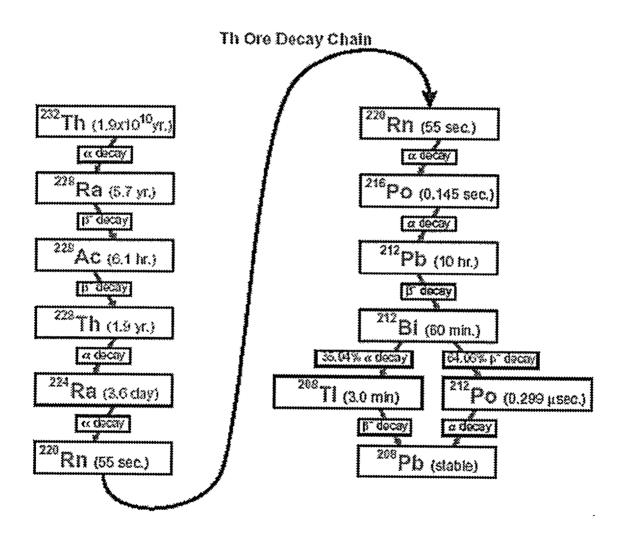
The detectable ratio of alpha to beta is a 2.1 for natural thorium decay. In actuality, the decay of natural thorium produces 6 alphas and 4 betas to reach stable lead. However, one of the betas emitted during the

decay process (from Ra-228) is not detectable (39 keV E-max). The other three betas emitted are detectable and are suitable as a surrogate.

The alpha readings recorded on the various data forms and record sheets were actual instrument readings, obtained from the instrument during the survey, and do not represent this ratio factoring. The use of alpha to beta ratio factoring is incorporated in the data set just prior to statistical analysis and comparison to limit values

Figure 1 is a graphical representation of the decay of natural thorium

FIGURE 1 - NATURAL THORIUM DECAY CHAIN



#### 5.0 SURVEY PROCEDURE

#### 5.1 GENERAL

Approved SOPs and/or field procedures were followed for activities described in this plan.

#### 5.2 SURFACE SCANS

Scanning of surfaces to identify locations of elevated residual surface activity were performed according to Table 3.

Foundation Classification	Survey Location	Surface Scan
All Previously Surveyed Foundation Tops	Top surface of foundation.	5 - 10% cursory beta-gamma scan (at random locations) on top surface of previously surveyed foundations prior to lifting foundation.
Affected Foundations	Underside surface of foundation.	100 % beta-gamma scan of underside of foundation when foundation is lifted.
Unaffected Foundations	Underside surface of foundation.	10 % beta-gamma scan of underside of foundation when foundation is lifted.
Result Requirements		Locations of surface activity exceeding twice background will be marked for further evaluation by direct measurement.

TABLE 3 - SURFACE SCAN SCHEDULE

The instruments that were used for scanning are listed in Table 7. For hand-held instrumentation, the detector was kept as close as possible to the surface and moved across the surface at a slow speed. Scan surveys were performed by moving the detector over the surface area at a maximum speed of 1-2 inches per second and a distance of approximately 1/2 inch for beta. If the count rate increased, the rate of movement of the detector was decreased or stopped. If the increase in count rate was real (approximately twice background and not a random variation in the background count rate), a static 60-second measurement was performed over the area to quantify the activity. Audible indicators (headphones or instrument speaker) were used to identify locations having elevated activity levels. All scanning results were noted on standard survey forms and locations of elevated radiation were identified for later investigation.

Document No.:

#### 5.3 DIRECT SURFACE MEASUREMENTS

Direct measurements were performed according to Table 4.

Foundation Classification	Survey Location	Direct Measurement
All Previously Surveyed Foundations	Top surface of foundation	Measurements will be performed at each location of elevated activity identified by surface scan measurements.
Affected Foundations	Underside surface of foundation.	Measurements will be performed at a minimum of 30 locations for the entire foundation (survey unit) and sufficient additional locations to provide coverage at a minimum of approximately one location per $20 \text{ m}^2$ of the underside surface of the foundation.
Unaffected Foundations	Underside surface of foundation.	Measurements will be performed at a minimum of 30 locations for the entire foundation (survey unit) and sufficient additional locations to provide coverage at a minimum of approximately one location per $50 \text{ m}^2$ of the underside surface of the foundation.
Result Requirements		If measurement indicates residual activity above guideline limits, the affected area is identified and controlled as radioactive material.

Direct surface measurements were performed at the identified locations using the instruments described in Table 7. Direct surface measurements were conducted by integrating counts over a 1-minute period.

Due to the inherent difficulty of properly quantifying the alpha radiation component of the decay of natural thorium when using a hand-held instrument, a derived ratio of alpha decays to beta decays was used. The detectable ratio of alpha to beta is 2:1 for natural thorium decay. In actuality, the decay of natural thorium produces 6 alphas and 4 betas to reach stable lead. However, one of the betas emitted during the decay process (from Ra-228) is not detectable (39 keV E-max). The other three betas emitted are detectable and are suitable as a surrogate. Beta radiation was used as a surrogate to quantify alpha activity when performing direct measurements.

Alpha readings obtained during the surveying process were recorded on the proper data form(s) and/or record sheet(s) but were not be used to quantify the alpha activity component for direct measurements

Alpha to beta ratio factoring was incorporated in the data set just prior to statistical analysis and comparison to limit values.

#### 5.4 SMEAR SURVEYS

Smear surveys were conducted according to Table 5.

Foundation Classification	Survey Location	Removable Surface Activity
All Previously Surveyed Foundations	Top surface of foundation.	Collected from each location where a direct surface activity measurement is made (alpha and beta analysis).
Affected Foundations	Underside surface of foundation	Collected from each location where a direct surface activity measurement is made (alpha and beta analysis).
Unaffected Foundations	Underside surface of foundation.	Collected from each location where a direct surface activity measurement is made (alpha and beta analysis).

#### TABLE 5 - LOOSE SURFACE MEASUREMENT SCHEDULE Image: Comparison of the second secon

Smear sampling was performed in accordance with applicable procedures Smears were counted for gross alpha and beta with the appropriate instrument described in Table 7.

#### 5.5 EXPOSURE RATE MEASUREMENTS

Exposure rate measurements were performed according to Table 6.

Foundation Classification	Survey Location	Exposure Rate Measurement
NA	Eternal surface of "clean" concrete waste pile.	Gamma exposure rates measured 1 meter perpendicular to the piled concrete surface at 1 measurement per 50 $m^2$ of surface area.

#### TABLE 6 - EXPOSURE RATE MEASUREMENT SCHEDULE

Exposure rate measurements were performed at the identified locations using the instruments described in Table 7. Pile exposure rate measurements were not be taken at locations greater than seven feet above ground level.

#### 5.6 BACKGROUND LEVEL DETERMINATION

Background levels were determined for concrete surfaces by taking a minimum of 10 measurements at locations of similar construction, but without a history of radioactive materials use (off-site locations)

#### 5.7 **DOCUMENTATION**

All survey and sampling efforts were documented by sampling personnel One member of the sampling team was assigned as a document coordinator and was responsible for recording all required information during survey and sampling activities, other than the normal sampling information commonly performed by the individual obtaining the sample. Samples that were sent to an off-site processing facility were transferred from sample collection personnel to the designated counting technician for handling and custody control. This technician was responsible for documentation, sample identification, packaging, and shipping of samples, as required. A standard chain-of-custody record was used to record sample transfers to offsite facilities. Samples were held in the custody of the document coordinator until being shipped to the laboratory.

All survey data was documented on the appropriate radiological survey form, map, and/or data sheet. Information included, but was not limited to:

- Date, time and purpose of the survey
- General and specific location of the survey
- Name and signature of the surveyor
- Instrument model, serial number, and calibration due date
- Survey results for radiological contamination (recorded in dpm/100 cm<sup>2</sup>)

Survey documentation was completed and reviewed in a timely manner. Errors identified during the review process were brought to the Health Physics Technician (HPT) for correction.

#### 6.0 INSTRUMENTATION

#### 6.1 INSTRUMENT OPERATION AND CALIBRATION

All instruments were operated, maintained, and calibrated according to the manufacturer's recommendations and/or the specifications of ANSI N323-1978.

- Survey instruments were calibrated before initial use, at least semi-annually and following maintenance or repair that could affect calibration. Calibration sources were National Institute of Science and Technology (NIST) traceable.
- Meters need not be calibrated for readings above 1,000 mR/hr.
- Daily functional checks were conducted on each instrument to verify that the equipment is functioning properly.
- When not in use, instruments were stored at a central location and protected from harsh environments
- Records of instrument calibration and daily functional checks are maintained for inspection.

• Calibration stickers which include; sources used to calibrate, correction factors or efficiencies for each scale or decade calibrated, the date calibrated and due date, were attached to each instrument.

#### 6.2 MINIMUM DETECTABLE ACTIVITY

The detection sensitivity of a measurement system refers to the statistically determined quantity of radioactive material or radiation that can be measured or detected at a pre-selected confidence level. This sensitivity is a factor of both the instrumentation and the technique or procedure being used. Typically, detection sensitivity has been defined (EPA 1980) as the level above which there is less than a 5% probability that radioactivity will be reported present when it is really absent (Type I error) or reported absent when it is really present (Type II error).

Minimum detectable activity (MDA) is an *a priori* estimate of the minimum activity level which is practically measurable with a specific instrument and sampling and/or measurement technique. The basic equation for determining field instrument MDA (NUREG/CR-5849) is:

FIGURE 1 - BASIC MDA EQUATION

$$MDA = \frac{2.71 + 4.65\sqrt{B_R * t}}{E * \frac{A}{100}}$$

Where:

 $\begin{array}{rcl} B_R & = & background \ count \ rate \\ t & = & background \ count \ time \ (min) \\ E & = & efficiency \\ A & = & area \ of \ probe \end{array}$ 

#### 6.3 INSTRUMENT SELECTION

During the final status survey of building foundations at the Molycorp site, several radiological instruments were used to identify and quantify the radioactivity of building surfaces. The instruments identified in Table 7 are commonly used for measuring surface deposited radioactive levels from thorium series source of radioactivity. These instruments are reliable, readily available, and reasonably easy to use by trained personal. As necessary, instruments were substituted with an equivalent, or better, instrument. Prior to instrument substitution, the site radiological engineer was notified and approved of the substitution.

Instruments	Probe	Radiation	MDA (dpm/100 cm <sup>2</sup> )	Use
Ludlum, Model 2360	43-89	Alpha	67	Static Surveys
Ludlum, Model 2360	43-89	Beta	520	Static Surveys
Ludlum, Model 2350-1	43-68	Alpha	66	Static Surveys
Ludlum, Model 2350-1	43-68	Beta	319	Static Surveys
Ludlum, Model 2929	43-10-1	Alpha	29	Counter Scaler
Ludlum, Model 2929	43-10-1	Beta	182	Counter Scaler
Ludlum, Model 2350-1	43-68	Alpha	105	Scan Surveys
Ludlum, Model 2350-1	43-68	Beta	625	Scan Surveys
Ludlum, Model 239-1F	43-37	Alpha	64	Floor Monitor
Ludlum, Model 239-1F	43-37	Beta	1186	Floor Monitor
Ludlum, Model 19	Internal	Gamma	NA	Exposure Rates

 TABLE 7 - INSTRUMENTATION GUIDE

#### 6.4 INSTRUMENT USE TECHNIQUES

Instruments selected for performing final status surveys were provided by GTS Duratek, Field Engineering and Field Services group, Kingston, TN. Prior to delivery, instrument calibrations and operations were verified by the vendor, and shipped to Washington, PA. Upon arrival, the instruments were inspected and verified operational. Instrument backgrounds were preformed. QC check control limits were established and Chi-squared tests were performed, as necessary.

Prior to daily use, instruments were response checked and compared against their two and three sigma warning and control limit values. For scaler instruments, daily backgrounds were determined and MDCs were calculated in addition to their response checks. After daily use, hand-held instruments were once again source response checked to ensure that the instrument did not fail during the day's work. All instrument "daily checks" data was logged in the appropriate data log record.

Qualified HP technicians were trained on the use of the instruments, and provided access to the instrument's User Manuals. Surveys were performed in accordance with approved radiological survey procedures on site. Survey results were reviewed by the Radiological Engineer for accuracy and completeness.

#### 7.0 SURVEY FINDINGS

Detailed data reports (Survey Findings Report) for each survey unit sampled are provided as an appendix to this report Field data collection forms, survey report forms, instrumentation information (background, QC, MDA, and source response data forms), statistical test results, and comparisons to release limits are all provided as a single package. Each package also contains a summary of the final status survey for that survey unit and includes information on anomalies discovered during the survey process Where significant differences existed between final status survey results and results of previous surveys for the survey unit, explanations are provided

Raw survey data was compiled into survey data tables, where appropriate, and presented with calculational results and comparisons.

#### 7.1 TECHNIQUES FOR REDUCING/EVALUATING DATA

Survey information was obtained from the instrument's meter face used at the time of the survey. This data was recorded on a Radiological Survey Location Indicator data sheet, in the instrument's units For scans and static measurements, the units were in counts per minute (cpm). Smear data was recorded after counting, subtracting background, and converted to units of disintegrations per minute per 100 square centimeters (dpm/100cm<sup>2</sup>) Dose rate measurements were recorded in units of micro-Roentgen per hour (uR/hr) and taken directly from the instruments meter face. Information used in the conversion from cpm to dpm (instrument efficiencies) was recorded on the Radiation Protection Survey Report form. For scans, the highest reading for the given immediate scan area was recorded in cpm.

Where "hot spots" needed to be evaluated, additional readings were taken and the average hot spot activity was calculated in accordance with NUREG/CR-5849, Section 8 5.2 - Elevated Areas of Activity.

#### 7.2 STATISTICAL EVALUATION AND COMPARISON TABLES

The statistical methodology used to provide the true representation of the data in relationship to the applicable limits is found in Sections 2.0 and 8.0 of NUREG/CR-5849. Comparison tables and tests used in the analysis are presented as part of each survey unit's Survey Findings Report package, as an appendix to this report.

#### 8.0 SUMMARY

Final status survey of the building foundations located at the Molycorp Washington, PA site were performed in accordance with the requirements listed in NUREG/CR 5849, "Manual for Conducting Radiological Surveys in Support of License Termination," RSI's "Decommission Plan for the Washington, PA Facility, Part 1 Revision," Molycorp's "U.S. Nuclear Regulatory Commission Material License, Amendment No. 5, SMB-1393," and MACTEC's "Concrete Sample and Management Plan."

According to the findings of the final status surveys performed at the Molycorp Washington, PA site, all release criteria have been met. Results of the final status survey demonstrate that the residual radioactivity is below the unrestricted use criteria and confirm that the building foundations are suitable for unrestricted use.

#### 9.0 **REFERENCES**

- 1) Manual for Conducting Radiological Surveys in Support of License Termination, NUREG/CR-5849, Draft, December 1993.
- Multi-Agency Radiation Survey and Site Investigation Manual (MARSSIM) Revision 1, NUREG-1575, Rev. 1, US Nuclear Regulatory Commission, Office of Nuclear Regulatory Research, Washington, DC, August 2000.
- 3) Specifications and Guidelines for Quality Systems for Environmental Data Collection and Environmental Technology Programs, American National Standard, ANSI/ASQC E4-1994.
- 4) *Quality Assurance for Radiological Monitoring Program Effluent Streams and the Environment*, NRC Regulatory Guide 4.15, 1979.
- 5) *Termination of Operating Licenses for Nuclear Reactors*, Nuclear Regulatory Commission, Regulatory Guide 1.86, 1974.
- 6) Minimum Detectable Concentrations with Typical Radiation Survey Instruments for Various Contaminants and Field Conditions, NUREG/CR-1507, Final, 1997.
- 7) Statistical Methods for Evaluating the Attainment of Cleanup Standards, Pacific Northwest Laboratory, Richland, WA, December 1992.
- 8) Radiation Detection and Measurement, Knoll, 1979.
- 9) Washing, PA Facility, Decommissioning Plan, Part I Revision, June 30, 1999, Radiological Services Inc.
- 10) Radiation Protection Program, Health Physics Procedures, June 1999, Radiological Services Inc.
- 11) Site Characterization Report for License Termination of the Washington, PA Facility, January 1995, Radiological Services Inc
- 12) U.S. Nuclear Regulatory Commission Materials License, Molycorp, Inc, SMB-1393, Docket No. 040-08778, Amendment 5.
- 13) Antech Ltd. Waltz Mill, Project No. 02-0284W, Analytical Survey Results for Composite Tile Sample at Molycorp, Washington, PA, May 13, 2002.

Appendix A

# Building 21 Footer Data Package Molycorp Washington, PA

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October, 2002

#### **Building 21 Footers Data Package**

This data package contains final status survey information for Building 21, Molycorp, Washington, PA site. The building's footers were surveyed in accordance with the Concrete Sampling and Management Plan.

Field data collection forms, survey report forms, statistical test results, and comparisons to release limits are provided.

#### Summary

Results from the final status survey of Building 21 footers provides evidence that all release criteria have been met, demonstrates that residual radioactivity is below the unrestricted use criteria, and confirms that the footers of Building 21 are suitable for unrestricted use and release.

•			•			5	unvey #	RPP-0P-019
•	DD	O-138 Radiation P	rotection St	urvey F	Report		lycorp / Washir	igton, PA
Section 1: Survey Infor	mation	-						
Date 9-17-02			Location 13Ldg	#21	/	1 1	sue Log Numb	1
RWP Number	Purpo	se of Survey /P	Unconditional	Release	Other	Page		<u> </u>
Survey Title:	55 Fc	SUNDATION	slunder	esid	e)	Smear Number	Beta dpm/100cm <sup>2</sup>	Alpha dpm/100cm <sup>2</sup>
			(F00)	ter)		1		
			·	•		2		
			-			4		
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Bkgd Readings 8-	-10 MR/h					25		
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00 = mRem/h gamma	00 C = mRer	n/h gamma contact 0	= Smear Locati	оп	⊽ = A:	r Sample Loo		X- = Rope, dary, or Barrier
00 β = mRem/h beta	00 βC = mRe	em/h beta contact -0	D- = Large Area	a Wipe	= Bu	lk Material Sa	ample	
Section 2: Instrument				Data at		MDA		Other
Instrument Model/SN	Cal Due Date	Probe Model/SN	Cal Due Date <sup>-</sup>	Detecto θ (cpm/			× B*	DKG ~
2929/115563	6-14-03	1/33871	6-14-03		.347	134 12		1.7
2350-1/126140	1-16-03	43-106/12-14-02	12-14-02	.231/.	,172	2   דור	2 307	1. 1.1
			<u> </u>					
Section 3: Review and	i d Approval	l	<u></u>	<b>L</b> ,,,				
Survey Performed By (S			Area Posted ar			Date and T	Time	
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Radiation Safety Officer		& Sign) tere Kowalaly	•			Date and 9-18.	-02/09	245
Steve Kowa S	hi / d	come pouralaly	(			1-7-10	000 00	, , , , , , , , , , , , , , , , , , , ,

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Survey Area	a information	ו:	FSS Fo	Fouters undA	). د م ه ۱۲	•	Bldg	21		- 
	Instrume Model/S			robe del/SN	Cal Due	S	α β;So can ME DA ME		α Static MDA	β Static MDA
Instrument				<u> </u>	<u> </u>	<b> </b>	i			
Data									<u> </u>	
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						1			Data	
	Print Name	;		Signat	ure		1		Date	
Performed							!			
By:		•		<u></u>			1			
			β Static	β		1	3		Sme	ars
Location	·β Scan	α Scan	(unsh)	Static	α Sta	1	ER'	(0	dpm/10	0 cm²)
LUCATION	(cpm)	(cpm)	(cpm)	(sh)	(cpn	n)	(µrem/hr)		α	β
F-21	7/0	NA	719	(cpm) 4/3	NA		12.	-	. 3	- 56
5-21	680		651	360			11		, 3	-13
F.21	740		7/3	310			11	-	,3	35
F-21	790		162	363			10:	_	.3	35
F-21	760		720	407.			12		3	4.3
F-21	600		523	360	<u> </u>				3	/3
E-21	540		519	356					.6	<u>48</u> -17
E-21	620		598	364			12'		,3	-43
F-21	680		650	391			12	T -,	3	-69
<u> -21</u>  -21	790		760	407			11	1 ~,	3	-56
F-21	580		550	399			11.	1 -	3	-4.3
F-21	570	<u> </u>	540				10	1 2		0
1=-21	540-		510	349			11.		,3	-13 26
F-21 F-21	840		280	401			11		,3	56
	960	v.	900	416	<u>                                      </u>		<i>I·O</i>		2.6	95
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Radiological Survey Results - Survey Location Indicator عروسي المحمد المعني المحمد عن المحمد الم محمد المحمد المحم المحمد المحم المحمد المح Survey Area Information. FSS(FOOTERS) Bldg"21 α α β Cal Probe β'Scan Instrument Cal Scan Static Static Model/SN Due Model/SN Due MDA MDA MDA MDA T Instrument . Data 1 i Signature Date Print Name Performed £ By: .β Smears • . ß Static ER α Static <sup>·</sup>B Scan a Scan Static  $(dpm/100 cm^{2})$ Location (unsh) (µrem/hr) (sh) (cpm) (cpm) (cpm) (cpm) α β (cpm) NA 0 -.3 NA 11 490 471 328 Ţ 8.7 l'!-.3 450 416 286 ړ 9' 2.6 35 3 460 427 315 10: -.3 17 4 590 575 34E -13 10 -. 3 5 284. 380 349 -.3 Ð 11: 360 6 348 347 2.6 -17 111 7 630 603 373 101 580 13 8 -.3 353 562 26 -. 3 10 9 480 450 334 4.3 -.3 11 460 NIA NA 442 323 ID , . , . ł i T .

Inst. #2

Page 3 of 3

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#### Results of Surface Scans Molycorp - Building 21 Survey Unit

#### Footer Material

| Location | Beta Scan<br>gross cpm |     |
|----------|------------------------|-----|
| F1       | 490                    | 183 |
| F2       | 450                    | 143 |
| F3       | 460                    | 153 |
| F4       | 590                    | 283 |
| F5       | 380                    | 73  |
| F6       | 360                    | 53  |
| F7       | 630                    | 323 |
| F8       | 580                    | 273 |
| F9       | 480                    | 173 |
| F10      | 460                    | 153 |
| F11      | 760                    | 453 |
| F12      | 680                    | 373 |
| F13      | 740                    | 433 |
| F14      | 790                    | 483 |
| F15      | 760                    | 453 |
| F16      | 600                    | 293 |
| F17      | 540                    | 233 |
| F18      | 620                    | 313 |
| F19      | 540                    | 233 |
| F20      | 680                    | 373 |
| F21      | 790                    | 483 |
| F22      | 580                    | 273 |
| F23      | 570                    | 263 |
| F24      | 540                    | 233 |
| F25      | 840                    | 533 |
| F26      | 960                    | 653 |
| F27      | 620                    | 313 |

All footer material scans performed with Ludlum Model 2350-1 No. 126190 with 43-106 No. 133871

Monitor Info: Scan MDA Beta - 717 dpm/100cm<sup>2</sup> Scan background Beta - 307 cpm Detector Eff. Beta - .231

#### Elevated Results of Surface Scans Molycorp - Building 21 Survey Unit

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#### Footer Material

| Location | Beta Scan |
|----------|-----------|
|          | net cpm   |

F26 653

# Direct Measurements (Total Activity)

Molycorp - Building 21 Survey Unit

#### Footer Material

| Location | Unshield Beta<br>cpm | Shield Beta<br>cpm | Gross Beta<br>cpm | Bkgd<br>cpm | Net<br>cpm | Direct Beta<br>(dpm/100cm²) | Uncertainty<br>95% CL | MDA<br>(dpm/100cm²) | Direct Alpha <sup>(1)</sup><br>(dpm/100cm <sup>2</sup> ) |
|----------|----------------------|--------------------|-------------------|-------------|------------|-----------------------------|-----------------------|---------------------|----------------------------------------------------------|
| F1       | 471                  | 328                | 143               | 144         | -1         | -4                          | 144                   | 253                 | -9                                                       |
| F2       | 416                  | 286                | 130               | 144         | -14        | -61                         | 140                   | 253                 | -121                                                     |
| F3       | 427                  | 315                | 112               | 144         | -32        | -139                        | 136                   | 253                 | -277                                                     |
| F4       | 575                  | 348                | 227               | 144         | 83         | 359                         | 163                   | 253                 | 719                                                      |
| F5       | 349                  | 284                | 65                | 144         | -79        | -342                        | 123                   | 253                 | -684                                                     |
| F6       | 348                  | 347                | 1                 | 144         | -143       | -619                        | 102                   | 253                 | -1238                                                    |
| F7       | 603                  | 373                | 230               | 144         | 86         | 372                         | 164                   | 253                 | 745                                                      |
| F8       | 562                  | 353                | 209               | 144         | 65         | 281                         | 159                   | 253                 | 563                                                      |
| F9       | 450                  | 334                | 116               | 144         | -28        | -121                        | 137                   | 253                 | -242                                                     |
| F10      | 442                  | 323                | 119               | 144         | -25        | -108                        | 138                   | 253                 | -216                                                     |
| F11      | 719                  | 412                | 307               | 144         | 163        | 706                         | 180                   | 253                 | 1411                                                     |
| F12      | 651                  | 360                | 291               | 144         | 147        | 636                         | 177                   | 253                 | 1273                                                     |
| F13      | 713                  | 310                | 403               | 144         | 259        | 1121                        | 198                   | 253                 | 2242                                                     |
| F14      | 762                  | 363                | 399               | 144         | 255        | 1104                        | 198                   | 253                 | 2208                                                     |
| F15      | 720                  | 407                | 313               | 144         | 169        | 732                         | 181                   | 253                 | 1463                                                     |
| F16      | 523                  | 360                | 163               | 144         | 19         | 79                          | 143                   | 244                 | 158                                                      |
| F17      | 519                  | 356                | 163               | 144         | 19         | 79                          | 143                   | 244                 | 158                                                      |
| F18      | 598                  | 366                | 232               | 144         | 88         | 367                         | 158                   | 244                 | 733                                                      |
| F19      | 521                  | 391                | 130               | 144         | -14        | -58                         | 135                   | 244                 | -117                                                     |
| F20      | 650                  | 320                | 330               | 144         | 186        | 775                         | 178                   | 244                 | 1550                                                     |
| F21      | 760                  | 407                | 353               | 144         | 209        | 871                         | 182                   | 244                 | 1742                                                     |
| F22      | 550                  | 399                | 151               | 144         | 7          | 29                          | 140                   | 244                 | 58                                                       |
| F23      | 540                  | 368                | 172               | 144         | 28         | 117                         | 145                   | 244                 | 233                                                      |
| F24      | 510                  | 349                | 161               | 144         | 17         | 71                          | 143                   | 244                 | 142                                                      |
| F25      | 780                  | 401                | 379               | 144         | 235        | 979                         | 187                   | 244                 | 1958                                                     |
| F26      | 900                  | 416                | 484               | 144         | 340        | 1417                        | 205                   | 244                 | 2833                                                     |
| F27      | 580                  | 411                | 169               | 144         | 25         | 104                         | 144                   | 244                 | 208                                                      |

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All footer material direct measurements performed with Ludlum Model 2350-1 No. 126190 with 43-106 No. 133871

Monitor Info: Direct MDA Beta - 253 dpm/100cm<sup>2</sup> Concrete background Beta - 144 cpm Detector Eff. Beta - .231

(1) - A beta to alpha ratio factoring (1:2, beta to alpha) was used to provide a more accurate alpha activity determination.

#### Elevated Direct Measurements (Total Activity) Molycorp - Building 21 Survey Unit

#### Footer Material

| Location | Direct Beta<br>(dpm/100cm <sup>2</sup> ) | Direct Alpha<br>(dpm/100cm <sup>2</sup> ) |
|----------|------------------------------------------|-------------------------------------------|
| F11      |                                          | 1411                                      |
| F12      |                                          | 1273                                      |
| F13      | 1121                                     | 2242                                      |
| F14      | 1104                                     | 2208                                      |
| F15      |                                          | 1463                                      |
| F20      |                                          | 1550                                      |
| F21      |                                          | 1742                                      |
| F25      |                                          | 1958                                      |
| F26      | 1417                                     | 2833                                      |

All concrete with elevated direct measurement readings was identified, marked and segregated from clean concrete Concrete with elevated readings (above release limits) will be controlled until shipped off-site as radiological waste or additional surveys will be performed and the 1 square meter average determined.

### Removable Surface Activity Measurements Molycorp - Building 21 Survey Unit

#### **Footer Material**

| Location | Removable Beta<br>(dpm/100cm <sup>2</sup> ) | Uncertainty<br>95% CL | MDA | Removable Alpha<br>(dpm/100cm <sup>2</sup> ) | Uncertainty<br>95% CL | MDA |
|----------|---------------------------------------------|-----------------------|-----|----------------------------------------------|-----------------------|-----|
| F1       | 0                                           | 9.4                   | 134 | -0.3                                         | 1.8                   | 12  |
| F2       | 8.7                                         | 15.2                  | 134 | -0.3                                         | 1.8                   | 12  |
| F3       | 35                                          | 25.9                  | 134 | 2.6                                          | 5.4                   | 12  |
| F4       | 17                                          | 19.2                  | 134 | -0.3                                         | 1.8                   | 12  |
| F5       | -13                                         | 17.4                  | 134 | -0.3                                         | 1.8                   | 12  |
| F6       | · 0                                         | 9.4                   | 134 | -0.3                                         | 1.8                   | 12  |
| F7       | -17                                         | 19.2                  | 134 | 2.6                                          | 5.4                   | 12  |
| F8       | 13                                          | 17.4                  | 134 | -0.3                                         | 1.8                   | 12  |
| F9       | 26                                          | 22.8                  | 134 | -0.3                                         | 1.8                   | 12  |
| F10      | 4.3                                         | 12.6                  | 134 | -0.3                                         | 1.8                   | 12  |
| F11      | -56                                         | 31.9                  | 134 | -0.3                                         | 1.8                   | 12  |
| F12      | -13                                         | 17.4                  | 134 | -0.3                                         | 1.8                   | 12  |
| F13      | 35                                          | 25.9                  | 134 | -0.3                                         | 1.8                   | 12  |
| F14      | 35                                          | 25.9                  | 134 | -0.3                                         | 1.8                   | 12  |
| F15      | 43                                          | 28.3                  | 134 | -0 3                                         | 1.8                   | 12  |
| F16      | 13                                          | 17.4                  | 134 | -0.3                                         | 1.8                   | 12  |
| F17      | 48                                          | 29.8                  | 134 | 2.6                                          | 5.4                   | 12  |
| F18      | -17                                         | 19.2                  | 134 | -0.3                                         | 1.8                   | 12  |
| F19      | -43                                         | 28.3                  | 134 | -0.3                                         | 1.8                   | 12  |
| F20      | -69                                         | 35.1                  | 134 | -0.3                                         | 1.8                   | 12  |
| F21      | -56                                         | 31.9                  | 134 | -0.3                                         | 1.8                   | 12  |
| F22      | -4.3                                        | 12.6                  | 134 | -0.3                                         | 1.8                   | 12  |
| F23      | 0                                           | 9.4                   | 134 | 5.5                                          | 7.8                   | 12  |
| F24      | -13                                         | 17.4                  | 134 | -0.3                                         | 1.8                   | 12  |
| F25      | 26                                          | 22.8                  | 134 | -0.3                                         | 1.8                   | 12  |
| F26      | 56                                          | 31.9                  | 134 | -0.3                                         | 1.8                   | 12  |
| F27      | 95                                          | 40.8                  | 134 | 2.6                                          | 5.4                   | 12  |

# Ludlum 2929 No. 115563 with 43-10 No. 127216 Info:

|                  | Beta  | Alpha |
|------------------|-------|-------|
| Background (cpm) | 73    | 0.1   |
| Bkgd ct. time    | 60    | 60    |
| Sample ct. time  | 1     | 1     |
| Efficiency       | 0.231 | 0.347 |
| MDA              | 134   | 12.0  |

### Elevated Removable Surface Activity Measurements Molycorp - Building 21 Survey Unit

**Footer Material** 

No elevated removable surface activity was reported above limits.

#### Exposure Rate Measurements Molycorp - Building 21 Survey Unit

#### Footer Material

| Location | Exposure Rate<br>(uR/hr) | Net Exp Rate<br>(uR/hr) |
|----------|--------------------------|-------------------------|
| F1       | 11                       | 2                       |
| F2       | 11                       | 2                       |
| F3       | 9                        | 0                       |
| F4       | 10                       | 1                       |
| F5       | 10                       | 1                       |
| F6       | 11                       | 2                       |
| F7       | 11                       | 2                       |
| F8       | 10                       | 1                       |
| F9       | 10                       | 1                       |
| F10      | 11                       | 2                       |
| F11      | 12                       | 2<br>3<br>2             |
| F12      | 11                       |                         |
| F13      | 11                       | 2                       |
| F14      | 10                       | 1                       |
| F15      | 12                       | 3<br>2                  |
| F16      | 11                       |                         |
| F17      | 11                       | 2                       |
| F18      | 12                       | 3                       |
| F19      | 11                       | 2                       |
| F20      | 12                       | 2<br>3<br>2             |
| F21      | 11                       | 2                       |
| F22      | 11                       | 2                       |
| F23      | 10                       | 1                       |
| F24      | 11                       | 2                       |
| F25      | 11                       | 2                       |
| F26      | 10                       | 1                       |
| F27      | 11                       | 2                       |

Background dose rate: 8-10 uR/hr with Model 19, No. 22526

# Summary of Building Surface Direct Reading (Total Activity) Results Molycorp - Building 21 Survey Unit

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#### Footer Material

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|         | В                 | leta       |                           | Alpha   |         |            |                         |  |
|---------|-------------------|------------|---------------------------|---------|---------|------------|-------------------------|--|
| n<br>18 | $\overline{x}$ 23 | s<br>250.6 | μ <sub>α</sub><br>125.0   | n<br>18 | x<br>45 | s<br>501.3 | μ <sub>α</sub><br>250.0 |  |
|         | $t_{1-\alpha}$    | 1.734      |                           |         |         |            |                         |  |
|         |                   | Guid       | elines/Cond<br>Satisfied? | itions  |         |            |                         |  |

Beta Alpha Yes Yes

### Summary of Exposure Rate Measurements Molycorp - Building 21 Survey Unit

#### Footer Material

| n  | $\frac{1}{x}$ | S   | $\mu_{\alpha}$ |
|----|---------------|-----|----------------|
| 27 | 1.8           | 0.7 | 2.1            |

t<sub>1-α</sub> 1.703

Guidelines/Conditions Satisfied?

Yes

Appendix B

# Building 22 Footer Data Package Molycorp Washington, PA

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October, 2002

### **Building 22 Footers Data Package**

This data package contains final status survey information for Building 22, Molycorp, Washington, PA site. The building's footers were surveyed in accordance with the Concrete Sampling and Management Plan.

Field data collection forms, survey report forms, statistical test results, and comparisons to release limits are provided.

### Summary

Results from the final status survey of Building 22 footers provides evidence that all release criteria have been met, demonstrates that residual radioactivity is below the unrestricted use criteria, and confirms that the footers of Building 22 are suitable for unrestricted use and release.

### RPP-0P-019

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|                                                | DD                | O-138 Radiat                     | ion Protecti  | on Survey Re      | port   Site Mo           | lycorp / Washington P                         |
|------------------------------------------------|-------------------|----------------------------------|---------------|-------------------|--------------------------|-----------------------------------------------|
| Section 1: Survey Inform                       | ation             |                                  |               |                   |                          |                                               |
| Date                                           | Time              | 117.                             | Location      | 1 22              | Survey I                 | ssue Log Number                               |
| 9-23-02                                        |                   | 1630                             | BL            | lz 22             |                          | 02-1035                                       |
| RWP Number                                     |                   | ise of Surveγ<br>/P □ Routine Su | rvey 🗆 Uncond | tional Release 🗇  |                          |                                               |
| Survey Title.                                  | =5 S              | Bldg                             | 22 (For       | NDATION           | Smear<br>Number          | Beta Alp<br>dpm/100cm <sup>2</sup> dpm/1      |
|                                                |                   | Ũ                                | 5             | etco3 "           |                          |                                               |
|                                                |                   |                                  |               |                   |                          |                                               |
|                                                |                   |                                  |               |                   | 3                        | <u> </u>                                      |
|                                                | 1 11.11           | te 57747 10                      | 1. The        |                   | 1                        |                                               |
|                                                | •                 |                                  | - 7 /4/       | w ow              | 6                        |                                               |
|                                                | Cox               | lerete                           |               |                   | 7                        |                                               |
|                                                |                   |                                  | BKG           | MOA               | 8                        | · · · ·                                       |
|                                                |                   | -                                | 1411          | MOA<br>253        | 9                        | 1                                             |
|                                                | INST #            | 1/                               | 117           |                   | . 10                     |                                               |
| -                                              |                   | 1                                | <b>C</b> 1    | 0                 | 1 1 1                    | 1                                             |
|                                                |                   |                                  | 8             | 92                | 12                       | 1                                             |
|                                                |                   |                                  |               |                   | 13                       |                                               |
|                                                |                   |                                  |               |                   | 14                       |                                               |
|                                                |                   |                                  |               |                   | 15                       |                                               |
| I) Data Point<br>R.м.A. for                    | - #/              | was Mi                           | arked i       | removed to        | 0 16                     |                                               |
| I) DAIN TOTICI                                 | ,                 | , et -                           | ,             |                   | 17                       | <u>    \                                 </u> |
| R.M.A. For                                     | rAd w             | ASTE                             |               |                   | 1 19                     |                                               |
| :                                              |                   |                                  |               |                   | 20                       | 1 1                                           |
|                                                |                   |                                  |               |                   | 21                       |                                               |
|                                                |                   | _                                |               |                   | 22                       | · · · ·                                       |
|                                                |                   |                                  |               |                   | 23                       | :                                             |
|                                                | 10 <sup>4</sup> - | 2526 000                         | 1-29-03       |                   | 24                       |                                               |
| Meder                                          | _ 17 _ 2          | 2320                             |               |                   | 25                       |                                               |
| Bkqd Readings 8-1                              | OHRIA             | υ                                |               |                   | 26                       | 1                                             |
| Legend                                         |                   |                                  |               |                   |                          |                                               |
| 00 = mRem/h gamma (                            | 00 C = mRen       | n/h gamma conta                  |               |                   | 7 = Air Sample Loc       | Boundary or                                   |
| $00 \beta = mRem/h beta$                       | 00 βC = mRe       | m/h beta contact                 | = Larg        | e Area Wipe       | = Bulk Material Sa       | ample                                         |
| Section 2: Instrument L                        |                   |                                  |               |                   |                          | Other                                         |
| Instrument Model/SN                            | Cal Due<br>Date   | Probe Model/                     | SN Cal D      |                   |                          | Other                                         |
| 2350-11126190                                  |                   | 43-106 /13                       |               |                   | 172' 776 5               | 360 /                                         |
|                                                | ,.14-03           |                                  |               | 03 .23/1.3        |                          |                                               |
|                                                | Δ/                |                                  |               |                   | 1                        | 1                                             |
|                                                |                   | A                                |               |                   |                          | A                                             |
|                                                |                   |                                  |               |                   |                          |                                               |
|                                                | Approval          | L.,                              | i             |                   | ,,,,,,,,,_               | ·····                                         |
| Section 3: Review and                          |                   | <u> </u>                         | Area Pos      | ted and/or Barric |                          | /                                             |
| Section 3: Review and Survey Performed By (Sig | in) /             |                                  |               |                   |                          | 1                                             |
| Survey Performed By (Sig                       | - / /             |                                  | 🗇 Yes 🎜       | Not Req           | uired 9-23-              | 02/1630                                       |
|                                                | with !            | Sign)                            | TYes 2        | Not Req           | Ured 9-23-<br>Date and 1 | 02/1630<br>ime<br>02/0800                     |

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| Survey Area        | a Informatio                 | n:<br>2555                                   | RL         | da t                  | <sup>4</sup> 32 (            | four           | dAi       |            | )                                       |                  |                    | rvey tog-            |                    |                       |
|--------------------|------------------------------|----------------------------------------------|------------|-----------------------|------------------------------|----------------|-----------|------------|-----------------------------------------|------------------|--------------------|----------------------|--------------------|-----------------------|
|                    | Instrum<br>Model/            | ent                                          | Cal<br>Due | Cal Prob              |                              | I Probe        |           | Cal<br>Due | s                                       | α<br>ican<br>1DA | β¦Sc:<br>MD        | ,                    | α<br>Static<br>MDA | β ··<br>Static<br>MDA |
| Instrument<br>Data |                              |                                              |            |                       |                              |                |           |            | <br> <br> <br> <br> <br> <br> <br> <br> |                  |                    |                      |                    |                       |
| Performed          | Print Name                   | e!                                           | <u> </u>   |                       | Signat                       | ure            | <u> </u>  |            | 1                                       | 1_               | Date               | 3                    |                    |                       |
| Ву:                |                              |                                              |            |                       |                              |                |           |            | •                                       | -                |                    |                      |                    |                       |
| Location           | <sup>·</sup> β Scan<br>(cpm) | α Scar<br>(cpm)                              | n (u       | Static<br>nsh)<br>pm) | β<br>Static<br>(sh)<br>(cpm) | α Stat<br>(cpm |           | E<br>(µrer | R'<br>n/hr)                             | •                | Sme<br>dpm/10<br>a | ears<br>)0 cm²)<br>β |                    |                       |
|                    | 980                          | NA                                           | 19         | 04                    | 604                          | NIA            | 4         | 1          | 2                                       | -,               | 95                 | 35                   |                    |                       |
| 2                  | 960                          |                                              |            | 37                    | 672                          |                |           |            | 2                                       |                  | 95                 | 30                   |                    |                       |
| 3                  | 1050                         |                                              | 9          | 76                    | 741                          | <u> </u>       |           |            | 0                                       |                  | 95                 | 129                  |                    |                       |
| <u> </u>           | 740                          |                                              |            | 06                    | 454                          | /              | 1         |            | 0:                                      |                  | 95                 | -69                  |                    |                       |
| 5                  | 650                          | <u> </u>                                     |            | 514                   | 482                          |                | <u>  </u> |            | $\frac{2}{2}$                           |                  | 95                 | 61                   |                    |                       |
| 6                  | 630                          | <u>                                     </u> |            | 96                    | 495                          |                |           | r 2<br>1 E | 3:                                      |                  | 9                  | 8.7                  |                    |                       |
| 7                  | 790                          |                                              |            | 164                   | 567                          | /              |           |            | 7'                                      |                  | 95<br>95           | /3                   |                    |                       |
| <u> </u>           | 760                          |                                              |            | 25<br>97              | 498                          | {              | • • •     | E          |                                         |                  | 95                 | -43                  |                    |                       |
| 10                 | 720                          |                                              |            | ,60                   |                              | {              |           |            | 7                                       |                  | 95                 | 0                    |                    |                       |
| 11                 | 650                          |                                              | l          | 24                    |                              |                |           | 6          | 7                                       |                  | 9                  | 8.7                  |                    |                       |
| 12                 | 690                          | <u> /</u>                                    |            | 640                   | 502                          |                |           | 9          | ? •                                     | ·                | 95                 | - 48<br>13<br>0      |                    |                       |
| /3                 | 630                          |                                              |            | ,09                   | 197                          |                |           | 11         |                                         | -,               | 951                | 13                   |                    |                       |
| 14                 | 640                          |                                              |            | 24                    | 481                          | l              |           | 1          | 0.                                      | -,               | 95                 | 0                    |                    |                       |
| 15                 | 660                          | NA                                           |            | 37                    | 506                          | - SI           | 4         | 9          | ?                                       | -                | ,95                | 13                   |                    |                       |
|                    |                              |                                              |            |                       |                              |                |           |            |                                         |                  |                    |                      |                    |                       |
|                    |                              |                                              |            |                       |                              |                |           |            |                                         |                  |                    |                      |                    |                       |
|                    |                              | <br>                                         |            |                       |                              |                |           |            | <u>.</u>                                |                  | ł                  |                      |                    |                       |
|                    |                              | ļ                                            |            |                       |                              |                |           |            |                                         |                  |                    |                      |                    |                       |
|                    |                              |                                              |            |                       |                              |                |           |            |                                         |                  |                    |                      |                    |                       |
| <u> </u>           |                              |                                              |            |                       |                              |                |           |            |                                         |                  |                    |                      |                    |                       |
|                    |                              |                                              |            |                       | · · · · ·                    |                |           | <br> -     |                                         |                  |                    |                      |                    |                       |
|                    |                              | <u> </u>                                     |            |                       |                              |                |           |            |                                         | •                | ·                  |                      |                    |                       |
| <b></b>            |                              |                                              |            |                       |                              |                |           |            | 1                                       |                  |                    |                      |                    |                       |
|                    |                              | <u> </u>                                     |            |                       |                              |                |           |            | .                                       |                  |                    |                      |                    |                       |
| <u></u>            |                              |                                              |            |                       |                              |                |           |            | :                                       |                  |                    |                      |                    |                       |

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### Results of Surface Scans Molycorp - Building 22 Survey Unit

#### **Footer Material**

| Location | Beta Scan<br>gross cpm |     |
|----------|------------------------|-----|
| F1       | 980                    | 620 |
| F2       | 960                    | 600 |
| F3       | 1050                   | 690 |
| F4       | 740                    | 380 |
| F5       | 650                    | 290 |
| F6       | 630                    | 270 |
| F7       | 790                    | 430 |
| F8       | 760                    | 400 |
| F9       | 720                    | 360 |
| F10      | 690                    | 330 |
| F11      | 650                    | 290 |
| F12      | 690                    | 330 |
| F13      | 630                    | 270 |
| F14      | 640                    | 280 |
| F15      | 660                    | 300 |

All footer scans performed with Ludlum Model 2350-1 No. 126190 with 43-106 No. 133871

Scan MDA Beta - 776 dpm/100cm<sup>2</sup> Scan background Beta - 360 cpm Detector Eff. Beta - .231

### Elevated Results of Surface Scans Molycorp - Building 22 Survey Unit

Footer Material

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No elevated scan results were reported.

### Direct Measurements (Total Activity) Molycorp - Building 22 Survey Unit

### Footer Material

| Location | Unshield Beta<br>cpm | Shield Beta<br>cpm | Gross Beta<br>cpm | Bkgd<br>cpm | Net<br>cpm | Direct Beta<br>(dpm/100cm <sup>2</sup> ) | Uncertainty<br>95% CL | MDA<br>(dpm/100cm <sup>2</sup> ) | Direct Alpha <sup>(1)</sup><br>(dpm/100cm <sup>2</sup> ) |
|----------|----------------------|--------------------|-------------------|-------------|------------|------------------------------------------|-----------------------|----------------------------------|----------------------------------------------------------|
| F1       | 904                  | 604                | 300               | 144         | 156        | 675                                      | 179                   | 253                              | 1351                                                     |
| F2       | 837                  | 672                | 165               | 144         | 21         | 91                                       | 149                   | 253                              | 182                                                      |
| F3       | 976                  | 741                | 235               | 144         | 91         | 394                                      | 165                   | 253                              | 788                                                      |
| F4       | 706                  | 454                | 252               | 144         | 108        | 468                                      | 169                   | 253                              | 935                                                      |
| F5       | 614                  | 482                | 132               | 144         | -12        | -52                                      | 141                   | 253                              | -104                                                     |
| F6       | 596                  | 495                | 101               | 144         | -43        | -186                                     | 133                   | 253                              | -372                                                     |
| F7       | 764                  | 567                | 197               | 144         | 53         | 229                                      | 157                   | 253                              | 459                                                      |
| F8       | 725                  | 549                | 176               | 144         | 32         | 139                                      | 152                   | 253                              | 277                                                      |
| F9       | 697                  | 498                | 199               | 144         | 55         | 238                                      | 157                   | 253                              | 476                                                      |
| F10      | 660                  | 546                | 114               | 144         | -30        | -130                                     | 136                   | 253                              | -260                                                     |
| F11      | 624                  | 481                | 143               | 144         | -1         | -4                                       | 144                   | 253                              | -9                                                       |
| F12      | 640                  | 502                | 138               | 144         | -6         | -26                                      | 142                   | 253                              | -52                                                      |
| F13      | 609                  | 497                | 112               | 144         | -32        | -139                                     | 136                   | 253                              | -277                                                     |
| F14      | 624                  | 481                | 143               | 144         | -1         | -4                                       | 144                   | 253                              | -9                                                       |
| F15      | 637                  | 506                | 131               | 144         | -13        | -56                                      | 141                   | 253                              | -113                                                     |

All footer direct measurements performed with Ludlum Model 2350-1 No. 126190 with 43-106No. 133871

Direct MDA Beta - 253 dpm/100cm<sup>2</sup> Concrete background Beta - 144 cpm Detector Eff. Beta - .231

(1) - A beta to alpha ratio factoring (1:2, beta to alpha) was used to provide a more accurate alpha activity determination.

### Elevated Direct Measurements (Total Activity) Molycorp - Building 22 Survey Unit

Footer Material

Location Direct Alpha (dpm/100cm<sup>2</sup>)

F1 1351

Concrete pieces with elevated readings have been segregated from clean concrete and moved to a designated RMA. Radiologically clean concrete has been left in the footprint of the building, awaiting release authorization.

### Removable Surface Activity Measurements Molycorp - Building 22 Survey Unit

### Footer Material

| Location | Removable Beta<br>(dpm/100cm <sup>2</sup> ) | Uncertainty<br>95% CL | MDA | Removable Alpha<br>(dpm/100cm <sup>2</sup> ) | Uncertainty<br>95% CL | MDA |
|----------|---------------------------------------------|-----------------------|-----|----------------------------------------------|-----------------------|-----|
| F1       | 35                                          | 25.9                  | 134 | -0.95                                        | 3.3                   | 14  |
| F2       | 30                                          | 24.2                  | 134 | -0.95                                        | 3.3                   | 14  |
| F3       | 129                                         | 47.2                  | 134 | -0 95                                        | 3.3                   | 14  |
| F4       | -69                                         | 35.1                  | 134 | -0.95                                        | 3.3                   | 14  |
| F5       | 61                                          | 33.2                  | 134 | <b>-0</b> .95                                | 3.3                   | 14  |
| F6       | 8.7                                         | 15.2                  | 134 | 1.9                                          | 4.6                   | 14  |
| F7       | -2.9                                        | 11.6                  | 134 | -0.95                                        | 3.3                   | 14  |
| F8       | 13                                          | 17.4                  | 134 | -0 95                                        | 3.3                   | 14  |
| F9       | -43                                         | 28.3                  | 134 | -0.95                                        | 3.3                   | 14  |
| F10      | 0                                           | 9.3                   | 134 | -0.95                                        | 3.3                   | 14  |
| F11      | 8.7                                         | 15.2                  | 134 | 1.9                                          | 4.6                   | 14  |
| F12      | -48                                         | 29.7                  | 134 | -0.95                                        | 3.3                   | 14  |
| F13      | 13                                          | 17.4                  | 134 | -0.95                                        | 3.3                   | 14  |
| F14      | 0                                           | 9.3                   | 134 | -0.95                                        | 3.3                   | 14  |
| F15      | 13                                          | 17.4                  | 134 | -0.95                                        | 3.3                   | 14  |

### Ludlum 2929 No. 115563 with 43-10 No. 127216 Info:

|                  | Beta  | Alpha |
|------------------|-------|-------|
| Background (cpm) | 72    | 0.33  |
| Bkgd ct. time    | 60    | 60    |
| Sample ct. time  | 1     | 1     |
| Efficiency       | 0.231 | 0.347 |
| MDA              | 134   | 14.0  |
|                  |       |       |

### Elevated Removable Surface Activity Measurements Molycorp - Building 22 Survey Unit

**Footer Material** 

No elevated removable surface activity was reported above limits.

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### Exposure Rate Measurements Molycorp - Building 22 Survey Unit

Footer Material

| Location | Exposure Rate<br>(uR/hr) | Net Exp Rate<br>(uR/hr) |
|----------|--------------------------|-------------------------|
| F1       | 12                       | 3                       |
| F2       | 12                       | 3                       |
| F3       | 20                       | 10                      |
| F4       | 10                       | 1                       |
| F5       | 10                       | 1                       |
| F6       | 8                        | -1                      |
| F7       | 8                        | -1                      |
| F8       | 7                        | -2                      |
| F9       | 8                        | -1                      |
| F10      | 9                        | 0                       |
| F11      | 9                        | 0                       |
| F12      | 9                        | 0                       |
| F13      | 10                       | 1                       |
| F14      | 10                       | 1                       |
| F15      | 9                        | 0                       |

Background dose rate: 8-10 uR/hr with Model 19, No. 22526

### Summary of Building Surface Direct Reading (Total Activity) Results Molycorp - Building 22 Survey Unit

Footer Material

|    | В              | eta   |              |    |                | Alpha |              |
|----|----------------|-------|--------------|----|----------------|-------|--------------|
| n  | $\bar{x}$      | s     | $\mu_{lpha}$ | n  | $\overline{x}$ | S     | $\mu_{lpha}$ |
| 14 | 69             | 200.4 | 162.9        | 14 | 137            | 400.7 | 325.9        |
|    | $t_{1-\alpha}$ | 1.761 |              |    |                |       |              |
|    |                |       |              |    |                |       |              |

Guidelines/Conditions Satisfied?

| Beta | Alpha |
|------|-------|
| Yes  | Yes   |

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### Summary of Exposure Rate Measurements Molycorp - Building 22 Survey Unit

### Footer Material

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| n  | $\frac{1}{x}$ | S   | $\mu_{\alpha}$ |
|----|---------------|-----|----------------|
| 15 | 1.0           | 2.9 | 2.3            |

t<sub>1-α</sub> 1.753

### Guidelines/Conditions Satisfied?

Yes

Appendix C

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# Building 34 Footer Data Package Molycorp Washington, PA

October, 2002

### **Building 34 Footers Data Package**

This data package contains final status survey information for Building 34, Molycorp, Washington, PA site. The building's footers were surveyed in accordance with the Concrete Sampling and Management Plan.

Field data collection forms, survey report forms, statistical test results, and comparisons to release limits are provided.

### Summary

Results from the final status survey of Building 34 footers provides evidence that all release criteria have been met, demonstrates that residual radioactivity is below the unrestricted use criteria, and confirms that the footers of Building 34 are suitable for unrestricted use and release.

### RPP-OP-019

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|            | •                                                                                                                                     |                |            |                            |                                 |
|------------|---------------------------------------------------------------------------------------------------------------------------------------|----------------|------------|----------------------------|---------------------------------|
| •          | DDO-138 Radiation Protection Survey Report                                                                                            | Site M         | Aolycorp / | Washing                    | ton PA                          |
|            | Section 1: Survey Information                                                                                                         |                |            |                            |                                 |
|            | Date C 10 Time 1700 Location 1 24                                                                                                     | Survey         | Issue Lo   | g Number                   | ~                               |
|            | RWP Number A A Purpose of Survey                                                                                                      |                | 72-        |                            |                                 |
|            | RWP Number WA Durpose of Survey Dunconditional Release D Other                                                                        | Pag            | je         | _ of3                      | i                               |
|            | Survey Title: FSS FOUNDATIONS (FOOTERS) 34                                                                                            | Smear<br>Numbe |            | ata<br>00cm <sup>2</sup> d | Alpha<br>dpm/100cm <sup>2</sup> |
| <b>.</b> " | 1) F19, F22, F23, F27, F30 All SENT to R.M.A.                                                                                         | 2              |            |                            |                                 |
|            | For RAD WASTE. FI. FJ FJ FR FIR. FIL TO PUA.                                                                                          | 3              | $\wedge$   |                            |                                 |
|            | For RAD WASTE. FI, FD, FT, FR, FID, FII, TO RMA.<br>For shipment.                                                                     | 4              |            |                            |                                 |
|            | 1 Minute STATICS TAKEN on                                                                                                             | 5              |            |                            |                                 |
|            | Releast                                                                                                                               | 6              |            | $\downarrow \downarrow$    |                                 |
|            | Concrete                                                                                                                              |                |            | -                          |                                 |
|            |                                                                                                                                       | 8 -            |            |                            | ,                               |
|            | INST#1 144 253                                                                                                                        | 10             |            |                            |                                 |
|            | INST#1 144 253                                                                                                                        | 11             |            | - <b> </b>                 |                                 |
|            |                                                                                                                                       | 12             | -          |                            |                                 |
|            | 8 92                                                                                                                                  | 13             |            |                            |                                 |
|            | - 16                                                                                                                                  | 14             |            |                            |                                 |
|            |                                                                                                                                       | 15             |            |                            |                                 |
|            | BKC                                                                                                                                   | 16             |            | <u> _</u>                  |                                 |
|            | INST # 2 < B 81                                                                                                                       | 17             |            | 1-14                       |                                 |
|            | . 144 244                                                                                                                             | ! 18<br>  19   | - A        |                            |                                 |
|            | INST 2                                                                                                                                | 1 20           |            | +                          |                                 |
|            | 8 81                                                                                                                                  | 21             |            | +                          |                                 |
|            | 0 5                                                                                                                                   | 22             | 1          |                            |                                 |
|            |                                                                                                                                       | 23             |            |                            |                                 |
|            | Duc                                                                                                                                   | 24             |            | <u> </u>                   | ·<br>/                          |
|            | Model 19 \$22526 1.29.03                                                                                                              | 25             |            |                            | <u> </u>                        |
|            | Bkgd Readings 10-12 Mr/hr                                                                                                             | 26             |            |                            |                                 |
|            | Legend<br>$00 = m\text{Rem/h}$ gamma $00 \text{ C} = m\text{Rem/h}$ gamma contact $D = \text{Smear Location}$ $\nabla = \text{Air S}$ | comple t       | ocation    |                            | = Rope.                         |
|            |                                                                                                                                       | Material S     |            |                            | ry, or Barrier                  |
|            | 00 β = mRem/h beta 00 βC = mRem/h beta contact $-D$ = Large Area Wipe = Bulk i<br>Section 2: Instrument Used                          |                | <u> </u>   |                            |                                 |
|            | Instrument Model/SN   Cal Due   Probe Model/SN Cal Due   Detector Eff                                                                 | MDA            | i          | 0                          | ther                            |
|            | Date Date B(cpm/dom)                                                                                                                  |                |            |                            | ska a                           |
| ا * الانتر | 2350-1 (126190 1-16-03 43-106 13387112-14-02 1231/. 1729                                                                              |                |            | . 26.                      | 6.6                             |
| Inst # 2   | 2350-1 129414 8-2-03 43-106 128914 2.2.03 ,240 ,145 7                                                                                 |                |            | 78                         | 4.4                             |
|            | 2929/115563 644-03 43-108 127216 6-14-03 231 347 1                                                                                    | 34   (         | (3         | 73                         | .22                             |
|            |                                                                                                                                       |                |            |                            |                                 |
|            |                                                                                                                                       |                |            |                            |                                 |
|            | Section 3: Review and Approval                                                                                                        | Date and       | 1 Time     |                            |                                 |
|            |                                                                                                                                       | 9-18           |            | 1,7.                       | 00                              |
|            |                                                                                                                                       | Date and       |            | <u> </u>                   |                                 |
|            |                                                                                                                                       | 9-23           |            | 100                        | 0                               |
|            | Dive powajsill / sure to march                                                                                                        |                | 1          |                            |                                 |

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Radiological Survey Results - Survey Location Indicator Survey 02 - 1020 Bldg 34 (Footers) Survey Area Information: FSS FOUNDATIONS β α. α β Scan Probe Cal Cal Instrument Static Static Scan Model/SN MDA Due Due Model/SN MDA MDA MDA . Instrument Data • Date Signature Print Name Performed By: ß Smears **B** Static ER a Static Static  $(dpm/100 cm^{2})$ a Scan β Scan (unsh) Location (cpm) (urem/hr) (sh) (cpm) (cpm) α β (cpm) (cpm) -17 -,6 4 960 NA 460 10201 F-1 A 5.1 26 2: 890 420 F-2 940 \* -26 -,6 12 509 311 F-3 560 -22 2.2 13 291 507 F-4 500 -22 12 2.2 533 423 F-5 590 69 4 16.7 F-6. 323 211 380 -26 2.2 803 5 460 1.7 860 2.2 -35 12 915 478 F-18 F-9 980 \* -4.3 -,6 12 649 498 710 -65 -.6 K K K 15 440 790 F-10 820 -56 5.1 13 893 541 F.11 940 13 2.2 12 667 452 F-12 700 -,6 17 11 574 443 F-13 620 8.7 3 2,2 724 475 F-14 780-4.3 4 -.6 1A 502 1=-15 NA 722 760 . Ť . . .

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INSt. #1

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Sunves to2-1020

Radiological Survey Results - Survey Location Indicator

| Survey Area        | Information         | "Fs           | SF         | Found                   | a tion              | , B-          | LZZ      | #34 (                                | Foo         | ten,)               |                    |
|--------------------|---------------------|---------------|------------|-------------------------|---------------------|---------------|----------|--------------------------------------|-------------|---------------------|--------------------|
|                    | Instrume<br>Model/S | ent           | Cal<br>Due | P                       | robe<br>del/SN      | Cal<br>Due    | s        | $\alpha^{\dagger}$ $\beta^{\dagger}$ | Scan<br>IDA | 5                   | β<br>Static<br>MDA |
| Instrument<br>Data |                     |               |            |                         |                     |               |          |                                      |             |                     |                    |
|                    | ·                   |               |            |                         |                     |               |          |                                      |             | ·                   |                    |
|                    | Print Name          |               |            |                         | Signati             | Jre           |          |                                      |             | Date                | <u> </u>           |
| Performed          |                     |               |            |                         |                     |               |          | :                                    |             |                     |                    |
| By:                |                     |               |            |                         |                     |               |          |                                      | _<br>       |                     |                    |
| Location           | β Scan<br>(cpm)     | α Sca<br>(cpm | an   '(i   | Static<br>unsh)<br>cpm) | β<br>Static<br>(sh) | α Sta<br>(cpr |          | ER<br>(µrem/r                        | ır)         | Sme<br>(dpm/10<br>α |                    |
| FIL                | 575                 | ٨Þ            |            | 57                      | (cpm)  <br>397      | 14            | <u>~</u> | 14.                                  |             | -,6                 | 4,3                |
| F17                | 370                 |               | :          | 158<br>402              | 279                 |               |          | 10                                   |             | 2.2                 | <u>13</u><br>-17   |
| F18<br>F19         | 920                 |               |            | 874                     | 416                 |               |          | 14                                   |             | -, 6<br>-, 6        | 13<br>-4,3         |
| F2D<br>F21         | 510                 |               |            | 491<br>478              | 377.                |               |          | 15                                   |             | 6                   | 26                 |
| F22<br>F23         | 895                 |               |            | 872<br>664              | 369                 |               |          | 13                                   |             | 6<br>5.1            | 17<br>-48          |
| F24<br>F25         | 459                 |               |            | 407_                    | 313                 |               |          | 14                                   |             | 2.2                 | 8.7<br>22          |
| F 26<br>F 27       | 509<br>850          |               |            | <u>485</u><br>814       | 400                 |               |          | 12                                   |             | -,6                 | 26                 |
| F 28<br>F 29       | 570                 |               |            | <u>557</u><br>453       | 453                 |               |          | 12                                   |             | ~.6<br>6            | 22                 |
| F 30               | 1360                | V             |            | 345                     | 597                 | I I           |          | 15                                   |             | 2,2                 | 22                 |
|                    |                     |               |            |                         |                     |               |          |                                      |             |                     |                    |
|                    |                     |               |            |                         |                     |               |          |                                      |             |                     |                    |
|                    |                     |               |            |                         |                     |               |          |                                      |             |                     |                    |
|                    |                     |               |            |                         |                     | <u> </u>      |          |                                      |             | •                   |                    |
|                    |                     |               |            |                         |                     |               |          |                                      |             |                     |                    |
|                    |                     |               |            |                         |                     |               |          | · · ·                                |             |                     |                    |

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### Results of Surface Scans Molycorp - Building 34 Survey Unit

### **Footer Material**

| Location | Beta Scan<br>gross cpm | Beta Scan<br>net cpm | Instrument<br># |
|----------|------------------------|----------------------|-----------------|
| F1       | 1020                   | 514                  | 1               |
| F2       | 940                    | 434                  | 1               |
| F3       | 560                    | 54                   | 1               |
| F4       | 580                    | 74                   | 1               |
| F5       | 590                    | 84                   | 1               |
| F6       | 380                    | -126                 | 1               |
| F7       | 860                    | 354                  | 1               |
| F8       | 980                    | 474                  | 1               |
| F9       | 710                    | 204                  | 1               |
| F10      | 820                    | 314                  | 1               |
| F11      | 940                    | 434                  | 1               |
| F12      | 700                    | 194                  | 1               |
| F13      | 620                    | 114                  | 1               |
| F14      | 780                    | 274                  | 1               |
| F15      | 760                    | 254                  | 1               |
| F16      | 575                    | 197                  | 2               |
| F17      | 370                    | -8                   | 2               |
| F18      | 431                    | 53                   | 2               |
| F19      | 920                    | 542                  | 2<br>2          |
| F20      | 510                    | 132                  | 2               |
| F21      | 515                    | 137                  | 2               |
| F22      | 895                    | 517                  | 2               |
| F23      | 695                    | 317                  | 2               |
| F24      | 459                    | 81                   | 2               |
| F25      | 480                    | 102                  | 2               |
| F26      | 509                    | 131                  | 2               |
| F27      | 850                    | 472                  | 2               |
| F28      | 570                    | 192                  | 2<br>2<br>2     |
| F29      | 475                    | 97                   | 2               |
| F30      | 1360                   | 982                  | 2               |

All footer scans performed with either: #1 - Ludlum Model 2350-1 No. 126190 with 43-106 No. 133871

Scan MDA Beta - 920 dpm/100cm<sup>2</sup> Scan background Beta - 506 cpm Detector Eff. Beta - .231

or

# 2 - Ludlum Model 2350-1 No. 129414 with 43-106 No. 128914

Scan MDA Beta - 765 dpm/100cm<sup>2</sup> Scan background Beta - 378 cpm Detector Eff. Beta - .240

### Elevated Results of Surface Scans Molycorp - Building 34 Survey Unit

### Footer Material

| Location | Beta Scan |
|----------|-----------|
|          | net cpm   |

F30 982

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### Direct Measurements (Total Activity)

Molycorp - Building 34 Survey Unit

### Footer Material

| Location | Unshield Beta | Shield Beta | Gross Beta | Bkgd | Net  | Direct Beta               | Uncertainty | MDA                       | Direct Alpha <sup>(1)</sup> | Instrument       |
|----------|---------------|-------------|------------|------|------|---------------------------|-------------|---------------------------|-----------------------------|------------------|
|          | cpm           | cpm         | cpm        | cpm  | cpm  | (dpm/100cm <sup>2</sup> ) | 95% CL      | (dpm/100cm <sup>2</sup> ) | (dpm/100cm <sup>2</sup> )   | #                |
| F1       | 960           | 460         | 500        | 144  | 356  | 1541                      | 215         | 253                       | 3082                        | 1                |
| F2       | 890           | 420         | 470        | 144  | 326  | 1411                      | 210         | 253                       | 2823                        | 1                |
| F3       | 509           | 311         | 198        | 144  | 54   | 234                       | 157         | 253                       | 468                         | 1                |
| F4       | 507           | 291         | 216        | 144  | 72   | 312                       | 161         | 253                       | 623                         | 1                |
| F5       | 533           | 423         | 110        | 144  | -34  | -147                      | 135         | 253                       | -294                        | 1                |
| F6       | 323           | 211         | 112        | 144  | -32  | -139                      | 136         | 253                       | -277                        | 1                |
| F7       | 803           | 460         | 343        | 144  | 199  | 861                       | 187         | 253                       | 1723                        | 1                |
| F8       | 915           | 478         | 437        | 144  | 293  | 1268                      | 205         | 253                       | 2537                        | 1                |
| F9       | 649           | 498         | 151        | 144  | 7    | 30                        | 146         | 253                       | 61                          | 1                |
| F10      | 790           | 440         | 350        | 144  | 206  | 892                       | 189         | 253                       | 1784                        | 1                |
| F11      | 893           | 541         | 352        | 144  | 208  | 900                       | 189         | 253                       | 1801                        | 1                |
| F12      | 667           | 452         | 215        | 144  | 71   | 307                       | 161         | 253                       | 615                         | 1                |
| F13      | 574           | 443         | 131        | 144  | -13  | -56                       | 141         | 253                       | -113                        | 1                |
| F14      | 724           | 475         | 249        | 144  | 105  | 455                       | 168         | 253                       | 909                         | 1                |
| F15      | 722           | 502         | 220        | 144  | 76   | 329                       | 162         | 253                       | 658                         | 1                |
| F16      | 557           | 397         | 160        | 144  | 16   | 67                        | 142         | 244                       | 133                         | 2                |
| F17      | 358           | 279         | 79         | 144  | -65  | -271                      | 122         | 244                       | -542                        | 2                |
| F18      | 402           | 300         | 102        | 144  | -42  | -175                      | 128         | 244                       | -350                        | 2                |
| F19      | 874           | 416         | 458        | 144  | 314  | 1308                      | 200         | 244                       | 2617                        | 2                |
| F20      | 491           | 377         | 114        | 144  | -30  | -125                      | 131         | 244                       | -250                        | 2<br>2           |
| F21      | 478           | 346         | 132        | 144  | -12  | -50                       | 136         | 244                       | -100                        |                  |
| F22      | 872           | 369         | 503        | 144  | 359  | 1496                      | 208         | 244                       | 2992                        | 2<br>2<br>2<br>2 |
| F23      | 664           | 358         | 306        | 144  | 162  | 675                       | 173         | 244                       | 1350                        | 2                |
| F24      | 407           | 313         | 94         | 144  | -50  | -208                      | 126         | 244                       | -417                        | 2                |
| F25      | 467           | 384         | 83         | 144  | -61  | -254                      | 123         | 244                       | -508                        | 2                |
| F26      | 485           | 400         | 85         | 144  | -59  | -246                      | 124         | 244                       | -492                        |                  |
| F27      | 814           | 460         | 354        | 144  | 210  | 875                       | 182         | 244                       | 1750                        | 2<br>2<br>2<br>2 |
| F28      | 557           | 453         | 104        | 144  | -40  | -167                      | 129         | 244                       | -333                        | 2                |
| F29      | 453           | 346         | 107        | 144  | -37  | -154                      | 129         | 244                       | -308                        | 2                |
| F30      | 1345          | 597         | 748        | 144  | 604  | 2517                      | 244         | 244                       | 5033                        | 2                |
|          |               |             |            |      | ~~ . |                           |             |                           | 0000                        | <b>4</b>         |

All footer direct measurements performed with either: #1 - Ludlum Model 2350-1 No. 126190 with 43-106No. 133871

Direct MDA Beta - 253 dpm/100cm<sup>2</sup> Concrete background Beta - 144 cpm Detector Eff. Beta - .231

or

# 2 - Ludium Model 2350-1 No. 129414 with 43-106 No. 128914

Direct MDA Beta - 244 dpm/100cm<sup>2</sup> Concrete background Beta - 144 cpm Detector Eff. Beta - .240

(1) - A beta to alpha ratio factoring (1:2, beta to alpha) was used to provide a more accurate alpha activity determination.

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### Elevated Direct Measurements (Total Activity) Molycorp - Building 34 Survey Unit

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### Footer Material

| Location | Direct Beta<br>(dpm/100cm <sup>2</sup> ) | Direct Alpha<br>(dpm/100cm <sup>2</sup> ) |
|----------|------------------------------------------|-------------------------------------------|
| F1       | 1541                                     | 3082                                      |
| F2       | 1411                                     | 2823                                      |
| F7       |                                          | 1723                                      |
| F8       | 1268                                     | 2537                                      |
| F10      |                                          | 1784                                      |
| F11      |                                          | 1801                                      |
| F19      | 1308                                     | 2617                                      |
| F22      | 1496                                     | 2992                                      |
| F23      |                                          | 1350                                      |
| F27      |                                          | 1750                                      |
| F30      | 2517                                     | 5033                                      |

Concrete pieces with elevated readings have been segregated from clean concrete and moved to a designated RMA. Radiologically clean concrete has been left in the footprint of the building, awaiting release authorization.

## Removable Surface Activity Measurements Molycorp - Building 34 Survey Unit

### Footer Material

| Location | Removable Beta<br>(dpm/100cm <sup>2</sup> ) | Uncertainty<br>95% CL | MDA | Removable Alpha<br>(dpm/100cm <sup>2</sup> ) | Uncertainty<br>95% CL | MDA |
|----------|---------------------------------------------|-----------------------|-----|----------------------------------------------|-----------------------|-----|
| F1       | -17                                         | 19.2                  | 134 | -0.6                                         | 2.6                   | 13  |
| F2       | 26                                          | 22.8                  | 134 | 5.1                                          | 7.5                   | 13  |
| F3       | -26                                         | 22.8                  | 134 | -0.6                                         | 2.6                   | 13  |
| F4       | -22                                         | 21.3                  | 134 | 2.2                                          | 4.9                   | 13  |
| F5       | -22                                         | 21.3                  | 134 | 2.2                                          | 4.9                   | 13  |
| F6       | 69                                          | 35.1                  | 134 | 16.7                                         | 13.6                  | 13  |
| F7       | -26                                         | 22.8                  | 134 | 2.2                                          | 4.9                   | 13  |
| F8       | -35                                         | 25.9                  | 134 | 2.2                                          | 4.9                   | 13  |
| F9       | -4.3                                        | 12.6                  | 134 | -0.6                                         | 2.6                   | 13  |
| F10      | -65                                         | 34.2                  | 134 | -0.6                                         | 2.6                   | 13  |
| F11      | -56                                         | 31.9                  | 134 | 5.1                                          | 7.5                   | 13  |
| F12      | 13                                          | 17.4                  | 134 | 2.2                                          | 4.9                   | 13  |
| F13      | 17                                          | 19.2                  | 134 | -0.6                                         | 2.6                   | 13  |
| F14      | 8.7                                         | 15.2                  | 134 | 2.2                                          | 4.9                   | 13  |
| F15      | 4.3                                         | 12.6                  | 134 | -0.6                                         | 2.6                   | 13  |
| F16      | 4.3                                         | 12.6                  | 134 | -0.6                                         | 2.6                   | 13  |
| F17      | 13                                          | 17.4                  | 134 | 2.2                                          | 4.9                   | 13  |
| F18      | -17                                         | 19.2                  | 134 | -0.6                                         | 2.6                   | 13  |
| F19      | 13                                          | 17.4                  | 134 | -0.6                                         | 2.6                   | 13  |
| F20      | -4.3                                        | 12.6                  | 134 | -0.6                                         | 2.6                   | 13  |
| F21      | 26                                          | 22.8                  | 134 | -0.6                                         | 2.6                   | 13  |
| F22      | -39                                         | 27.1                  | 134 | 2.2                                          | 4.9                   | 13  |
| F23      | 17                                          | 19.2                  | 134 | -0.6                                         | 2.6                   | 13  |
| F24      | -48                                         | 29.8                  | 134 | 5.1                                          | 7.5                   | 13  |
| F25      | 8.7                                         | 15.2                  | 134 | 2.2                                          | 4.9                   | 13  |
| F26      | 22                                          | 21.3                  | 134 | -0.6                                         | 2.6                   | 13  |
| F27      | 26                                          | 22.8                  | 134 | -0.6                                         | 2.6                   | 13  |
| F28      | 30                                          | 24.2                  | 134 | -0.6                                         | 2.6                   | 13  |
| F29      | 22                                          | 21.3                  | 134 | -0.6                                         | 2.6                   | 13  |
| F30      | 22                                          | 21.3                  | 134 | 2.2                                          | 4.9                   | 13  |

### Ludlum 2929 No. 115563 with 43-10 No. 127216 Info:

|                  | Beta  | Alpha |
|------------------|-------|-------|
| Background (cpm) | 73    | 0.22  |
| Bkgd ct. time    | 60    | 60    |
| Sample ct. time  | 1     | 1     |
| Efficiency       | 0.231 | 0.347 |
| MDA              | 134   | 13.0  |

### Elevated Removable Surface Activity Measurements Molycorp - Building 34 Survey Unit

Footer Material

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No elevated removable surface activity was reported above limits.

### Exposure Rate Measurements Molycorp - Building 34 Survey Unit

Footer Material

| Location | Exposure Rate<br>(uR/hr) | Net Exp Rate<br>(uR/hr) |
|----------|--------------------------|-------------------------|
| F1       | 14                       | 3                       |
| F2       | 12                       | 1                       |
| F3       | 12                       | 1                       |
| F4       | 13                       | 2                       |
| F5       | 12                       | 1                       |
| F6       | 14                       | 3                       |
| F7       | 15                       | 4                       |
| F8       | 12                       | 1                       |
| F9       | 12                       | 1                       |
| F10      | 15                       | 4                       |
| F11      | 13                       | 2                       |
| F12      | 12                       | 1                       |
| F13      | 11                       | 0                       |
| F14      | 13                       | 2                       |
| F15      | 14                       | 3                       |
| F16      | 14                       | 3                       |
| F17      | 10                       | -1                      |
| F18      | 13                       | 2                       |
| F19      | 14                       | 3                       |
| F20      | 12                       | 1                       |
| F21      | 15                       | 4                       |
| F22      | 14                       | 3                       |
| F23      | 13                       | 2                       |
| F24      | 15                       | 4                       |
| F25      | 14                       | 3                       |
| F26      | 12                       | 1                       |
| F27      | 14                       | 3                       |
| F28      | 12                       | 1                       |
| F29      | 13                       | 2                       |
| F30      | 15                       | 4                       |

Background dose rate: 10-12 uR/hr with Model 19, No. 22526

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### Summary of Building Surface Direct Reading (Total Activity) Results Molycorp - Building 34 Survey Unit

### Footer Material

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|    | E              | Beta  |                |    |           | Alpha |                |
|----|----------------|-------|----------------|----|-----------|-------|----------------|
| n  | $\bar{x}$      | S     | $\mu_{\alpha}$ | n  | $\bar{x}$ | S     | $\mu_{\alpha}$ |
| 19 | -14            | 229.6 | 77.5           | 19 | -27       | 459.2 | 154.9          |
|    | $t_{1-\alpha}$ | 1.729 |                |    |           |       |                |

### Guidelines/Conditions Satisfied?

| Beta | Alpha |
|------|-------|
| Yes  | Yes   |

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### Summary of Exposure Rate Measurements Molycorp - Building 34 Survey Unit

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### Footer Material

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- 21 S.

| n  | x   | S   | $\mu_{\alpha}$ |
|----|-----|-----|----------------|
| 30 | 2.1 | 1.3 | 2 5            |
|    |     |     |                |

t<sub>1-α</sub> 1.697

Guidelines/Conditions Satisfied?

Yes

Appendix D

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# Building 36 Footer Data Package Molycorp Washington, PA

October, 2002

### **Building 36 Footers Data Package**

This data package contains final status survey information for Building 36, Molycorp, Washington, PA site. The building's footers were surveyed in accordance with the Concrete Sampling and Management Plan.

Field data collection forms, survey report forms, statistical test results, and comparisons to release limits are provided.

### Summary

Results from the final status survey of Building 36 footers provides evidence that all release criteria have been met, demonstrates that residual radioactivity is below the unrestricted use criteria, and confirms that the footers of Building 36 are suitable for unrestricted use and release.

#### RPP-OP-019

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|                               | DDO-         | -138 Radiation  | Protection Su                   | urvey Report        | Site Mo         | ycorp / Washin                 | gton, PA                        |
|-------------------------------|--------------|-----------------|---------------------------------|---------------------|-----------------|--------------------------------|---------------------------------|
| Section 1: Survey Information | <br>on       | <u></u>         |                                 |                     |                 |                                |                                 |
| Date 9-16-02                  | Time         | 600             | Location<br>Bldg3               | 6 (Foundation       | Survey Is       | sue Log Numb<br>)ス - 100       | er<br>(                         |
| RWP Number/A                  | Purpose      | of Survey:      |                                 |                     | Page            | of                             | 2_                              |
| Survey Title: FSS F           |              |                 |                                 |                     | Smear<br>Number | Beta<br>dpm/100cm <sup>2</sup> | Alpha<br>dpm/100cm <sup>2</sup> |
|                               |              |                 |                                 |                     | 1               | <u> </u>                       |                                 |
|                               |              |                 |                                 |                     | 2               |                                |                                 |
|                               |              |                 |                                 |                     | 3               | <u></u>                        |                                 |
|                               |              |                 |                                 |                     | 4               | ├                              |                                 |
|                               | -            | •               |                                 |                     | 6               |                                |                                 |
| //                            | MINUT        | STATIC          | 5 TAKana                        | n                   | 7               |                                |                                 |
|                               | Formal       | a Smirice       |                                 |                     | 8               |                                |                                 |
|                               | 1 Ulina      |                 |                                 |                     | 9               |                                |                                 |
|                               |              | 13 K            | 6 12                            | (0/+                | 10              |                                |                                 |
|                               |              | B- 14           | <u>6 M</u><br><u>14</u> 2.<br>9 | 53                  | 11              |                                |                                 |
|                               |              |                 | -                               |                     | 12              | <u>├</u>                       |                                 |
|                               |              | ~/ <i>&amp;</i> | , <u> </u>                      | · つ                 | 13              | <u> </u>                       |                                 |
|                               |              |                 | 7                               | 6                   | · 15            |                                | Λ                               |
|                               |              |                 |                                 |                     | 16              |                                | /]                              |
|                               |              |                 |                                 |                     | 17              |                                | 77                              |
|                               |              |                 |                                 |                     | 18              |                                |                                 |
|                               |              |                 |                                 |                     | 19              |                                |                                 |
|                               |              |                 |                                 |                     | 20              |                                |                                 |
|                               |              |                 |                                 |                     | 21              | ┼                              |                                 |
|                               |              |                 |                                 |                     | 22              | <u> </u>                       | ┪─────                          |
| , H                           |              |                 |                                 |                     | 23              |                                |                                 |
| Model 19 #2                   | 2526         | 1-29-03         |                                 |                     | 25              |                                |                                 |
| Bkgd Readings: 8-10           | <i>nalhr</i> |                 |                                 |                     | 26              |                                |                                 |
| Legend <sup>.</sup>           |              |                 |                                 | $\nabla = \Delta r$ | Sample Lo       | cation -X-X-X                  | (- = Rope,                      |
| 5                             |              | 5               |                                 |                     | Material S      | Boun                           | dary, or Barrier                |
| p                             |              | vh beta contact |                                 |                     |                 |                                |                                 |
| Section 2: Instrument Use     | al Due       | Probe Model/SN  | Cal Due                         | Detector Eff        | MDA             |                                | Other                           |
|                               | Date:        |                 | Date <sup>.</sup>               | B (cpm/dpm)         | <u>B</u> -      | × B- 1                         | BKG ~                           |
| 2929 115563 6-                | 14-03 4      | 43-10 (12721)   | <u> </u>                        | ,231,747            | 134 - 1         |                                | .17                             |
| 2350-1/126150 1-1             | 16-03 4      | 13-106/13387    | 1 12-14-02                      | 231 342             | 132 6           |                                | 1.4                             |
|                               |              | N               |                                 |                     |                 | N                              |                                 |
|                               | -            | A               | <u> </u>                        |                     |                 | <u> </u>                       |                                 |
|                               |              | A               |                                 |                     | <u></u>         |                                |                                 |
| Section 3: Review and Ap      |              | <u></u>         |                                 | - dies Desmonte d   | Date and        |                                |                                 |
| Survey Performed By (Sign)    | ./           |                 |                                 | nd/or Barricaded    | 9.16            |                                | б                               |
| Radiation Safety Officer (Pri | ull          | Sign)           |                                 |                     | Date and        |                                | -                               |
|                               |              | we Kourlo       | ()                              |                     | 0               |                                | 45                              |
| Steve Kowalski                | 1-04         | we murile       | <u> </u>                        |                     | ┙╾┹╼┹╼          |                                |                                 |

Radiological Survey Results - Survey Location Indicator

SURVEY 02-1001

|           |                     |                 |                   | und ATI           | Cal           | (   | 100        | β¦Sca         | α          | β                 |
|-----------|---------------------|-----------------|-------------------|-------------------|---------------|-----|------------|---------------|------------|-------------------|
|           | Instrume<br>Model/S | _               |                   | del/SN            | Due           |     | an  <br>DA | MDA           |            | Static<br>MDA     |
| nstrument |                     |                 |                   |                   |               |     |            | 1             |            |                   |
| Data      |                     |                 | •                 |                   |               |     |            | <u> </u>      |            |                   |
|           |                     |                 |                   |                   | 1             |     |            |               | •          |                   |
|           |                     |                 |                   |                   |               |     |            |               |            |                   |
|           | Print Name          | l,,             | <u>l</u>          | Signati           | ure           | ·   |            |               | Dat        | e                 |
| Performed |                     |                 |                   |                   |               |     |            | 1             |            |                   |
| By:       |                     |                 | <u></u>           |                   |               |     |            |               |            |                   |
|           |                     |                 |                   |                   |               |     |            | <del></del> _ |            |                   |
|           |                     | . 5000          | β Static          | β<br>Static       | α Sta         | tic | E          | ז'  <br>צ'    |            | ears $(0, -2)$    |
| _ocation  | ·β Scan<br>(cpm)    | α Scan<br>(cpm) | (unsh)            | (sh)              | (cpr          |     | (µгеп      |               | • •        | $00 \text{ cm}^2$ |
|           | (0,0,0,0)           | (               | (cpm)             | (cpm)             |               |     |            | 1             | α          | β                 |
| 1         | 470                 | 12              | 449               | 415               | 6             |     |            | <u>&gt;</u> : | -,5        | -39               |
| 2         | 480                 | 10              | 464               | 353               | 4             |     | 7          |               | -,5<br>-,5 | 69                |
| 3         | 460                 | 8               | 446               | 365               | 2             | -+  | 9          |               | 2.4        | 22                |
| <u> </u>  | 540                 | 19              | 712<br>458        | 332<br>369        | 2             |     | 10         | i             | 5          | 13                |
| <u>s</u>  | 480                 | 9               | 445               | 360               | 5             |     | 11         |               | 5          | -56               |
| 7         | 420                 | 6               | 409               | 325               | 2             |     | 10         |               | 2.4        | - 30              |
| 8         | 510                 | 5               | 487               | 354               | 3             | ,   | 10         | 21            | 7.9        | - 39              |
| 9         | 4.30                | 6               | 397               | 331               | $\frac{7}{3}$ |     |            |               | 5          | 91                |
| 10        | 460                 | 5               | 431               | <u>357</u><br>321 | 7             |     |            |               | 5          | 1 - 8.7           |
| <br>      | 480                 |                 | <u>458</u><br>451 | 350               | 8             | i   |            | 7             | 15         | - 4.3             |
| 13        | 440                 | 6               | 424               | 331               | 4             |     |            |               | 2.4        | 43                |
| 14        | 420                 | 8               | 441               | 347               | 9             |     | 10         |               | 5          | 35                |
| 15        | 450                 | 4               | 437-              |                   | 5             |     | 10         |               | 2,4        | -17               |
| 16        | 400                 | 7               | 383               | 1                 | 4             |     | 9          | <u>2</u>      | 5          | 13                |
| 17<br>18  | 410                 | 6               | 371               | 326               |               |     |            | 0.            | -,5        | 22                |
| 19        | 480                 | . 9             | 427               | 318               | 6             |     | 1          | 0             | 2.4        | 48                |
| 20        | 480                 | 8               | 440               | 1                 | 5             |     | ./.        | /             | -15        | 4,3               |
| 21        | 500                 | 6               | 468               | 358               | 1.            |     | 10         |               | 2.4        | 39                |
| 22        | 490                 | 9               | 459               | 344               | 4             |     | - 10       |               | -,5        | 4.3               |
| 23        | 390                 | 13              | 375               |                   | 9             |     | . 10       |               | 5          | 65                |
| 24        | 410                 | 11              | 385               |                   | 3             |     | 10         |               | 2.4        | -2:               |
| 25        | 660                 |                 | 500               | 350               | 2             |     | 1          | /:            | -,5        | 8.7               |
| 27        | 540<br>560          | 6               | 527               |                   |               | /   | 11         | ' i           | 5          | 43                |

Page 2 of 2

### Results of Surface Scans Molycorp - Building 36 Survey Unit

### Footer Material

| Location | Beta Scan<br>gross cpm | Beta Scan<br>net cpm |  |  |
|----------|------------------------|----------------------|--|--|
| F1       | 470                    | 150                  |  |  |
| F2       | 480                    | 160                  |  |  |
| F3       | 460                    | 140                  |  |  |
| F4       | 540                    | 220                  |  |  |
| F5       | 480                    | 160                  |  |  |
| F6       | 460                    | 140                  |  |  |
| F7       | 420                    | 100                  |  |  |
| F8       | 510                    | 190                  |  |  |
| F9       | 430                    | 110                  |  |  |
| F10      | 460                    | 140                  |  |  |
| F11      | 480                    | 160                  |  |  |
| F12      | 470                    | 150                  |  |  |
| F13      | 440                    | 120                  |  |  |
| F14      | 420                    | 100                  |  |  |
| F15      | 450                    | 130                  |  |  |
| F16      | 400                    | 80                   |  |  |
| F17      | 410                    | 90                   |  |  |
| F18      | 480                    | 160                  |  |  |
| F19      | 460                    | 140                  |  |  |
| F20      | 480                    | 160                  |  |  |
| F21      | 500                    | 180                  |  |  |
| F22      | 490                    | 170                  |  |  |
| F23      | 390                    | 70                   |  |  |
| F24      | 410                    | 90                   |  |  |
| F25      | 660                    | 340                  |  |  |
| F26      | 540                    | 220                  |  |  |
| F27      | 560                    | 240                  |  |  |

All footer scans performed with Ludlum Model 2350-1 No. 126190 with 43-106 No. 133871

Monitor Info: Scan MDA Beta - 732 dpm/100cm<sup>2</sup> Scan background Beta - 320 cpm Detector Eff. Beta - .231

### Elevated Results of Surface Scans Molycorp - Building 36 Survey Unit

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Footer Material

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No elevated scan results were reported.

### Direct Measurements (Total Activity)

Molycorp - Building 36 Survey Unit

### Footer Material

| Location | Unshield Beta<br>cpm | Shield Beta<br>cpm | Gross Beta<br>cpm | Bkgd<br>cpm | Net<br>cpm | Direct Beta<br>(dpm/100cm <sup>2</sup> ) | Uncertainty<br>95% CL | MDA<br>(dpm/100cm <sup>2</sup> ) | Direct Alpha <sup>(1)</sup><br>(dpm/100cm <sup>2</sup> ) |
|----------|----------------------|--------------------|-------------------|-------------|------------|------------------------------------------|-----------------------|----------------------------------|----------------------------------------------------------|
| F1       | 449                  | 415                | 34                | 144         | -110       | -476                                     | 113                   | 253                              | -952                                                     |
| F2       | 464                  | 353                | 111               | 144         | -33        | -143                                     | 135                   | 253                              | -286                                                     |
| F3       | 446                  | 365                | 81                | 144         | -63        | -273                                     | 127                   | 253                              | -545                                                     |
| F4       | 492                  | 332                | 160               | 144         | 16         | 69                                       | 148                   | 253                              | 139                                                      |
| F5       | 458                  | 369                | 89                | 144         | -55        | -238                                     | 130                   | 253                              | -476                                                     |
| F6       | 445                  | 360                | 85                | 144         | -59        | -255                                     | 128                   | 253                              | -511                                                     |
| F7       | 409                  | 325                | 84                | 144         | -60        | -260                                     | 128                   | 253                              | -519                                                     |
| F8       | 487                  | 354                | 133               | 144         | -11        | -48                                      | 141                   | 253                              | -95                                                      |
| F9       | 397                  | 331                | 66                | 144         | -78        | -338                                     | 123                   | 253                              | -675                                                     |
| F10      | 431                  | 357                | 74                | 144         | -70        | -303                                     | 125                   | 253                              | -606                                                     |
| F11      | 458                  | 321                | 137               | 144         | -7         | -30                                      | 142                   | 253                              | -61                                                      |
| F12      | 451                  | 350                | 101               | 144         | -43        | -186                                     | 133                   | 253                              | -372                                                     |
| F13      | 424                  | 331                | 93                | 144         | -51        | -221                                     | 131                   | 253                              | -442                                                     |
| F14      | 441                  | 347                | 94                | 144         | -50        | -216                                     | 131                   | 253                              | -433                                                     |
| F15      | 437                  | 321                | 116               | 144         | -28        | -121                                     | 137                   | 253                              | -242                                                     |
| F16      | 383                  | 300                | 83                | 144         | -61        | -264                                     | 128                   | 253                              | -528                                                     |
| F17      | 371                  | 326                | 45                | 144         | -99        | -429                                     | 117                   | 253                              | -857                                                     |
| F18      | 447                  | 294                | 153               | 144         | 9          | 39                                       | 146                   | 253                              | 78                                                       |
| F19      | 427                  | 318                | 109               | 144         | -35        | -152                                     | 135                   | 253                              | -303                                                     |
| F20      | 440                  | 353                | 87                | 144         | -57        | -247                                     | 129                   | 253                              | -494                                                     |
| F21      | 468                  | 358                | 110               | 144         | -34        | -147                                     | 135                   | 253                              | -294                                                     |
| F22      | 459                  | 344                | 115               | 144         | -29        | -126                                     | 137                   | 253                              | -251                                                     |
| F23      | 375                  | 300                | 75                | 144         | -69        | -299                                     | 126                   | 253                              | -597                                                     |
| F24      | 385                  | 307                | 78                | 144         | -66        | -286                                     | 126                   | 253                              | -571                                                     |
| F25      | 604                  | 358                | 246               | 144         | 102        | 442                                      | 168                   | 253                              | 883                                                      |
| F26      | 500                  | 362                | 138               | 144         | -6         | -26                                      | 142                   | 253                              | -52                                                      |
| F27      | 527                  | 375                | 152               | 144         | 8          | 35                                       | 146                   | 253                              | 69                                                       |

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All footer direct measurements performed with Ludlum Model 2350-1 No. 126190 with 43-106No. 133871

Monitor Info: Direct MDA Beta - 253 dpm/100cm<sup>2</sup> Concrete background Beta - 144 cpm Detector Eff. Beta - .231

(1) - A beta to alpha ratio factoring (1:2, beta to alpha) was used to provide a more accurate alpha activity determination.

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#### Elevated Direct Measurements (Total Activity) Molycorp - Building 36 Survey Unit

Footer Material

No elevated direct measurements were reported.

#### Removable Surface Activity Measurements Molycorp - Building 36 Survey Unit

#### Footer Material

| Location | Removable Beta<br>(dpm/100cm <sup>2</sup> ) | Uncertainty<br>95% CL | MDA | Removable Alpha<br>(dpm/100cm <sup>2</sup> ) | Uncertainty<br>95% CL | MDA |
|----------|---------------------------------------------|-----------------------|-----|----------------------------------------------|-----------------------|-----|
|          |                                             |                       |     |                                              |                       |     |
| F1       | 0                                           | 9.2                   | 134 | -0.5                                         | 2.4                   | 12  |
| F2       | -39                                         | 27.1                  | 134 | -0.5                                         | 2.4                   | 12  |
| F3       | 69                                          | 35.1                  | 134 | -0.5                                         | 2.4                   | 12  |
| F4       | 22                                          | 21.2                  | 134 | 2.4                                          | 5.2                   | 12  |
| F5       | 13                                          | 17.4                  | 134 | -0.5                                         | 2.4                   | 12  |
| F6       | -56                                         | 31.9                  | 134 | -0.5                                         | 2.4                   | 12  |
| F7       | -30                                         | 24.2                  | 134 | 2.4                                          | 5.2                   | 12  |
| F8       | -39                                         | 27.1                  | 134 | 7.9                                          | 9.4                   | 12  |
| F9       | 39                                          | 27.1                  | 134 | -0.5                                         | 2.4                   | 12  |
| F10      | 91                                          | 40.0                  | 134 | -0.5                                         | 2.4                   | 12  |
| F11      | -8.7                                        | 15.2                  | 134 | -0.5                                         | 2.4                   | 12  |
| F12      | -4.3                                        | 12.5                  | 134 | -0.5                                         | 2.4                   | 12  |
| F13      | 43                                          | 28.3                  | 134 | 2.4                                          | 5.2                   | 12  |
| F14      | 35                                          | 25.8                  | 134 | -0.5                                         | 2.4                   | 12  |
| F15      | 17                                          | 19.2                  | 134 | -0.5                                         | 2.4                   | 12  |
| F16      | -17                                         | 19.2                  | 134 | 2.4                                          | 5.2                   | 12  |
| F17      | 13                                          | 17.4                  | 134 | -0.5                                         | 2.4                   | 12  |
| F18      | 22                                          | 21.2                  | 134 | -0.5                                         | 2.4                   | 12  |
| F19      | 48                                          | 29.7                  | 134 | 2.4                                          | 5.2                   | 12  |
| F20      | 4.3                                         | 12.5                  | 134 | -0.5                                         | 2.4                   | 12  |
| F21      | 39                                          | 27.1                  | 134 | 2.4                                          | 5.2                   | 12  |
| F22      | 56                                          | 31.9                  | 134 | -0.5                                         | 2.4                   | 12  |
| F23      | 4.3                                         | 12.5                  | 134 | -0.5                                         | 2.4                   | 12  |
| F24      | 65                                          | 34.1                  | 134 | -0.5                                         | 2.4                   | 12  |
| F25      | -22                                         | 21.2                  | 134 | 2.4                                          | 5.2                   | 12  |
| F26      | 8.7                                         | 15.2                  | 134 | -0.5                                         | 2.4                   | 12  |
| F27      | 43                                          | 28.3                  | 134 | -0.5                                         | 2.4                   | 12  |

## Ludlum 2929 No. 115563 with 43-10 No. 127216 Info:

|                  | Beta  | Alpha |
|------------------|-------|-------|
| Background (cpm) | 71    | 0.17  |
| Bkgd ct. time    | 60    | 60    |
| Sample ct. time  | 1     | 1     |
| Efficiency       | 0.231 | 0.347 |
| MDA              | 134   | 12.0  |

#### Elevated Removable Surface Activity Measurements Molycorp - Building 36 Survey Unit

#### **Footer Material**

No elevated removable surface activity was reported above limits.

#### Exposure Rate Measurements Molycorp - Building 36 Survey Unit

Footer Material

| Location | Exposure Rate<br>(uR/hr) | Net Exp Rate<br>(uR/hr) |
|----------|--------------------------|-------------------------|
| F1       | 10                       | 1                       |
| F2       | 9                        | 0                       |
| F3       | 8                        | -1                      |
| F4       | 9                        | 0                       |
| F5       | 10                       | 1                       |
| F6       | 11                       | 2                       |
| F7       | 10                       | 1                       |
| F8       | 10                       | 1                       |
| F9       | 9                        | 0                       |
| F10      | 8                        | -1                      |
| F11      | 8                        | -1                      |
| F12      | 9                        | 0                       |
| F13      | 9                        | 0                       |
| F14      | 10                       | 1                       |
| F15      | 10                       | 1                       |
| F16      | 10                       | 1                       |
| F17      | 9                        | 0                       |
| F18      | 10                       | 1                       |
| F19      | 10                       | 1                       |
| F20      | 11                       | 2                       |
| F21      | 10                       | 1                       |
| F22      | 11                       | 2                       |
| F23      | 10                       | 1                       |
| F24      | 9                        | 0                       |
| F25      | 10                       | 1                       |
| F26      | 11                       | 2                       |
| F27      | 11                       | 2                       |

Background dose rate: 8-10 uR/hr with Model 19, No. 22526

#### Summary of Building Surface Direct Reading (Total Activity) Results Molycorp - Building 36 Survey Unit

#### Footer Material

|    | В                | eta   |              |    |           | Alpha |              |
|----|------------------|-------|--------------|----|-----------|-------|--------------|
| n  | $\bar{x}$        | s     | $\mu_{lpha}$ | n  | $\bar{x}$ | S     | $\mu_{lpha}$ |
| 27 | -167             | 182.3 | -106.8       | 27 | -333      | 364.7 | -213.7       |
|    | t <sub>1-α</sub> | 1.703 |              |    |           |       |              |
|    |                  |       |              |    |           |       |              |

Guidelines/Conditions Satisfied?

> Beta Alpha Yes Yes

#### Summary of Exposure Rate Measurements Molycorp - Building 36 Survey Unit

#### Footer Material

| n  | $\frac{1}{x}$ | s   | $\mu_{lpha}$ |
|----|---------------|-----|--------------|
| 27 | 0.7           | 0.9 | 1.0          |

t<sub>1-α</sub> 1.703

Guidelines/Conditions Satisfied?

Yes

Appendix E

## 2W Concrete Ramp Data Package

Molycorp Washington, PA

October, 2002

#### 2W Concrete Ramp Footers Data Package

This data package contains final status survey information for the 2W Concrete Ramp, Molycorp, Washington, PA site. The 2W Concrete Ramp was surveyed in accordance with the Concrete Sampling and Management Plan.

Field data collection forms, survey report forms, statistical test results, and comparisons to release limits are provided.

#### Summary

Results from the final status survey of the 2W Concrete Ramp provides evidence that all release criteria have been met, demonstrates that residual radioactivity is below the unrestricted use criteria, and confirms that the concrete from the 2W Concrete Ramp is suitable for unrestricted use and release.

| _                                                                                                                                       |                                         |                     |                 |                 |                 |                                | RPP-OP-019                         |
|-----------------------------------------------------------------------------------------------------------------------------------------|-----------------------------------------|---------------------|-----------------|-----------------|-----------------|--------------------------------|------------------------------------|
|                                                                                                                                         |                                         | -138 Radiation P    | rotection Su    | rvey Report     | Site Mo         | ycorp / Wash                   | ngton, PA                          |
| Section 1: Survey Inform                                                                                                                |                                         |                     |                 |                 |                 |                                |                                    |
| Date                                                                                                                                    | Time                                    |                     | ocation.        | 0               |                 | sue Log Num                    |                                    |
| 9-11-02                                                                                                                                 |                                         |                     | W2+             | ACIDTLAN        |                 | <u>-0979</u>                   |                                    |
| RWP Number                                                                                                                              | Purpos                                  | e of Survey. FSS    | Unconditional F | lelease 🗙 Other | Page            | of                             | <u></u>                            |
|                                                                                                                                         | 22                                      |                     |                 |                 | Smear<br>Number | Beta<br>dpm/100cm <sup>2</sup> | Alpha<br>dpm/100cm <sup>2</sup>    |
| Survey Title: Acid                                                                                                                      | tank                                    | Concrete 7          | Kamp peni       | ra wa           | 1               |                                |                                    |
|                                                                                                                                         |                                         |                     |                 |                 | 2               |                                |                                    |
|                                                                                                                                         | •                                       |                     |                 |                 | 3               |                                |                                    |
|                                                                                                                                         |                                         |                     |                 |                 | 4               |                                |                                    |
|                                                                                                                                         |                                         |                     |                 |                 | 5               |                                | 1/                                 |
|                                                                                                                                         |                                         |                     |                 |                 | 6               |                                | ļ_/                                |
| 1                                                                                                                                       | mute                                    | - Statics           | taken           |                 | 7               |                                | _ <i>\/</i>                        |
|                                                                                                                                         |                                         | • -                 | · - •           |                 | 8               |                                |                                    |
| درى                                                                                                                                     | 0020                                    | rete                |                 |                 | 9               | <u> </u>                       |                                    |
|                                                                                                                                         |                                         |                     |                 |                 | 10              |                                |                                    |
|                                                                                                                                         |                                         | BKg<br>144          | MDA             |                 | 12              |                                | 1                                  |
| (                                                                                                                                       | 2                                       |                     |                 |                 | 13              |                                | /                                  |
|                                                                                                                                         | Y-                                      | 144                 | 244             |                 | 14              |                                |                                    |
|                                                                                                                                         | L                                       | ର                   |                 |                 | 15              |                                |                                    |
|                                                                                                                                         | d                                       | 8                   | 91              |                 | 16              |                                | <u></u>                            |
|                                                                                                                                         |                                         |                     |                 |                 | 17              |                                | <u>\</u>                           |
|                                                                                                                                         |                                         |                     |                 |                 | 18              |                                |                                    |
|                                                                                                                                         |                                         |                     | •               |                 | 19              | · · ·                          |                                    |
|                                                                                                                                         |                                         |                     |                 |                 | 20              |                                |                                    |
|                                                                                                                                         |                                         |                     |                 | -               | 21              | ++                             |                                    |
| •                                                                                                                                       |                                         |                     |                 |                 | 22              | ++                             |                                    |
|                                                                                                                                         |                                         | ,                   |                 |                 | 24              |                                |                                    |
| Mod                                                                                                                                     | el 19/2                                 | 2526/1-29-0         | 3               |                 | 25              |                                |                                    |
| -                                                                                                                                       | -10 MRI                                 |                     |                 |                 | 26              |                                |                                    |
| Legend                                                                                                                                  |                                         |                     |                 |                 |                 |                                |                                    |
| 00 = mRem/h gamma                                                                                                                       | 00 C = mRen                             | n/h gamma contact ① | = Smear Locati  |                 | Sample Lo       | Bor                            | (-X- = Rope,<br>indary, or Barrier |
| 00 $β$ = mRem/h beta                                                                                                                    | 00 βC = mRe                             | em/h beta contact - | O- = Large Are: | a Wipe 📑 = Bul  | k Material S    | Sample                         |                                    |
| Section 2: Instrument                                                                                                                   | Used                                    |                     |                 | ·               |                 |                                | 01505                              |
| Instrument Model/SN                                                                                                                     | Cal Due                                 | Probe Model/SN      | Cal Due<br>Date | Detector Eff ·  | V- MDA          | d B-                           | Other<br>BKG L                     |
|                                                                                                                                         | Date.                                   | 43.10/127216        | 6-14-03         | .231/.347       | 134/            | 12 73                          | / ,18                              |
| 2929/115563                                                                                                                             | 6-14-03                                 |                     | 2-02.03         |                 |                 | 8 229                          | 1_2                                |
| 2750/129414                                                                                                                             | 2-02-03                                 | 43.106/128914       |                 |                 |                 | N                              | $\sim$                             |
|                                                                                                                                         | ~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~ |                     |                 | ,               |                 | A                              |                                    |
|                                                                                                                                         |                                         | <u> </u>            |                 |                 |                 |                                |                                    |
| Section 3: Review an                                                                                                                    | d Approval                              | l                   | <u>_</u>        |                 |                 |                                |                                    |
| Section 3: Review and Approval           Survey Performed By (Sign)             Area Posted and/or Barricaded             Date and Time |                                         |                     |                 |                 |                 |                                |                                    |
| ane-Autr                                                                                                                                |                                         |                     | C Yes No        | Vot Required    | 911.            |                                | 0                                  |
| Radiation Safety Office                                                                                                                 | r (Print Name                           | & Sign)             | `               |                 | Date and        | 1                              | 230                                |
| Steve Kowals                                                                                                                            | Ki / S                                  | the Kowals          | L               |                 | 9-16            | -02/1                          | 230                                |
|                                                                                                                                         |                                         |                     | -               |                 |                 | /                              |                                    |

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Sunded # 02-0979

## Radiological Survey Results - Survey Location Indicator

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| Survey Area Information: |            |          |          |                           |               |            |   |                  |            |   |                    |                              |
|--------------------------|------------|----------|----------|---------------------------|---------------|------------|---|------------------|------------|---|--------------------|------------------------------|
| Instrument               |            |          |          | Cal Probe<br>Due Mòdel/SN |               | Cal<br>Due |   | α<br>ican<br>1DA | β Sc<br>MD |   | α<br>Static<br>MDA | β<br>Static<br>MDA           |
| Data                     |            |          |          |                           |               | -          |   |                  | 1          |   |                    |                              |
|                          |            |          |          |                           |               |            |   |                  | 1          |   |                    |                              |
|                          |            |          |          |                           |               |            |   |                  | i          |   | •                  |                              |
|                          |            |          |          |                           |               |            |   |                  | 1          |   |                    |                              |
| Performed                | Print Name | e<br>    |          |                           | Signat        | ure        |   |                  |            |   | Dat                | e                            |
| By:                      |            |          |          |                           |               |            |   |                  | i          |   |                    |                              |
|                          |            |          |          |                           |               |            |   |                  |            |   |                    |                              |
| Location                 | β Scan     | a Scan   |          | Static<br>nsh)            | β<br>Static   | α Stat     |   |                  | R.         |   | Sme<br>(dpm/1)     | ears<br>10 cm <sup>2</sup> ) |
| Ramp                     | (cpm)      | (cpm)    | (c       | pm)                       | (sh)<br>(cpm) | (cpm       | ) | (µrer            | 10111)     |   | α .                | β                            |
| 1                        | 312        | 7        | 1 2      | 98                        | 268           | 5          |   |                  | 71         | - | ,5                 | - 4.3                        |
| 2                        | 383        | 10       |          | 67                        | 317           | 7          |   |                  | 71         |   | ,5                 | -22                          |
| 3                        | 425        | 9        |          | 09                        | 127.          | 7          |   |                  | Pi         |   | .5                 | - 65                         |
| 4                        | 392        | 8        | 1        | 57                        | 273           | 6          |   |                  | 81         |   | .5                 | -30                          |
| 5                        | 382        | 5        |          | 61                        | 279.          | 2          |   |                  | 7          |   | .5                 | -13                          |
| 6                        | 370        | 6        |          | 46                        | 254           | 3          |   |                  | PI         |   | ,5                 | 4.3                          |
| 7                        | 385        | 10       |          | 58                        | 282           | 7          |   |                  | <u> </u>   |   | .5                 | 8.7                          |
| <u>8</u> .               | 352        | 6        | 3        | 16                        | 238           | 4          |   | (                | 2          |   | .4                 | 17                           |
| 9                        | 360        |          |          | 18                        | 255           |            |   |                  | <u> </u>   | _ | ,5                 | 8.7                          |
| 10                       | 370        | 8        |          | 59                        | 292           |            |   |                  | 5          |   | .4                 | - 4.3                        |
|                          | 410        |          |          | 93                        | 296           | 8          |   |                  | 8          |   | ,5                 | 13                           |
| 12                       | 360        | 10       | <u> </u> | 47                        | 279           | 7          |   | (                | 5          |   | 5                  | 4.3                          |
|                          |            |          | ļ        |                           |               |            |   |                  |            |   |                    |                              |
|                          |            |          | }        |                           |               |            |   |                  |            |   |                    |                              |
| TAUK                     | 400        | 3        | <u> </u> | 0.0                       | 200           |            |   |                  | ·          |   | 5                  | 13                           |
|                          | 400        | 2        |          | <u>88</u>                 | 299           | l          |   |                  |            |   | ,5                 | 4.3                          |
| <u> </u>                 | 390        | - 3      |          | <u>70</u><br>ገና           | 273<br>310    | <u> </u>   |   |                  |            |   | .4                 | -22                          |
| <u>&gt;</u><br>4         | 390        | 7        |          | 76                        | 282           | <u> </u>   |   | (                | <u>,</u>   |   | .5                 | -17                          |
| 5                        | 385        | 6        |          | $\frac{10}{12}$           | 252           | <u> </u>   |   |                  | 5          |   | ,5                 | 32                           |
| <u>5</u>                 | 370        | 5        |          | 1 <u>-</u><br>46          | 305           | <u>-</u>   |   |                  | 5.         |   | .5                 | -8.7                         |
|                          |            | <u>_</u> | <u> </u> |                           |               |            |   |                  | , ·        |   |                    |                              |
|                          |            |          |          |                           |               |            |   | :                | 1          |   |                    |                              |
| <u></u>                  | 1          |          | 1        |                           |               |            |   |                  | 1          |   |                    |                              |
|                          | 1          |          | 1        |                           |               |            |   |                  | 1          |   |                    |                              |
|                          |            |          |          |                           |               |            |   |                  |            |   |                    |                              |
|                          |            |          | [        |                           |               |            |   | _                | 1          |   |                    |                              |

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#### Results of Surface Scans Molycorp - Building 2W Ramp Survey Unit

#### **Concrete Material**

| Location                                 | Beta Scan                                     | Beta Scan                                     |
|------------------------------------------|-----------------------------------------------|-----------------------------------------------|
|                                          | gross cpm                                     | net cpm                                       |
| F1                                       | 312                                           | 83                                            |
| F2                                       | 383                                           | 154                                           |
| F3                                       | 425                                           | 196                                           |
| F4                                       | 392                                           | 163                                           |
| F5                                       | 382                                           | 153                                           |
| F6                                       | 370                                           | 141                                           |
| F7                                       | 385                                           | 156                                           |
| F8                                       | 352                                           | 123                                           |
| F9                                       | 360                                           | 131                                           |
| F10                                      | 370                                           | 141                                           |
| F11                                      | 410                                           | 181                                           |
| F12                                      | 360                                           | 131                                           |
| F5<br>F6<br>F7<br>F8<br>F9<br>F10<br>F11 | 382<br>370<br>385<br>352<br>360<br>370<br>410 | 153<br>141<br>156<br>123<br>131<br>141<br>181 |

All concrete scans performed with Ludium Model 2350-1 No. 129414 with 43-106 No. 128914

Scan MDA Beta - 595 dpm/100cm<sup>2</sup> Scan background Beta - 229 cpm Detector Eff. Beta - .240

#### Elevated Results of Surface Scans Molycorp - Building 2W Ramp Survey Unit

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**Concrete Material** 

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No elevated scan results were reported.

### Direct Measurements (Total Activity)

Molycorp - Building 2W Ramp Survey Unit

#### **Concrete Material**

| Location | Unshield Beta<br>cpm | Shield Beta<br>cpm | Gross Beta<br>cpm | Bkgd<br>cpm | Net<br>cpm | Direct Beta<br>(dpm/100cm <sup>2</sup> ) | Uncertainty<br>95% CL | MDA<br>(dpm/100cm <sup>2</sup> ) | Direct Alpha <sup>(1)</sup><br>(dpm/100cm <sup>2</sup> ) |
|----------|----------------------|--------------------|-------------------|-------------|------------|------------------------------------------|-----------------------|----------------------------------|----------------------------------------------------------|
| F1       | 298                  | 268                | 30                | 144         | -114       | -475                                     | 108                   | 244                              | -950                                                     |
| F2       | 362                  | 317                | 45                | 144         | -99        | -413                                     | 112                   | 244                              | -825                                                     |
| F3       | 409                  | 327                | 82                | 144         | -62        | -258                                     | 123                   | 244                              | -517                                                     |
| F4       | 357                  | 273                | 84                | 144         | -60        | -250                                     | 123                   | 244                              | -500                                                     |
| F5       | 361                  | 279                | 82                | 144         | -62        | -258                                     | 123                   | 244                              | -517                                                     |
| F6       | 346                  | 254                | 92                | 144         | -52        | -217                                     | 125                   | 244                              | -433                                                     |
| F7       | 358                  | 282                | 76                | 144         | -68        | -283                                     | 121                   | 244                              | -567                                                     |
| F8       | 316                  | 238                | 78                | 144         | -66        | -275                                     | 122                   | 244                              | -550                                                     |
| F9       | 318                  | 255                | 63                | 144         | -81        | -338                                     | 117                   | 244                              | -675                                                     |
| F10      | 359                  | 292                | 67                | 144         | -77        | -321                                     | 119                   | 244                              | -642                                                     |
| F11      | 393                  | 296                | 97                | 144         | -47        | -196                                     | 127                   | 244                              | -392                                                     |
| F12      | 347                  | 279                | 68                | 144         | -76        | -317                                     | 119                   | 244                              | -633                                                     |

All concreter direct measurements performed with Ludlum Model 2350-1 No. 129414 with 43-106 No. 128914

Direct MDA Beta - 244 dpm/100cm<sup>2</sup> Concrete background Beta - 144 cpm Detector Eff. Beta - .240

(1) - A beta to alpha ratio factoring (1:2, beta to alpha) was used to provide a more accurate alpha activity determination.

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#### Elevated Direct Measurements (Total Activity) Molycorp - Building 2W Ramp Survey Unit

**Concrete Material** 

No elevated direct measurements were reported.

#### Removable Surface Activity Measurements Molycorp - Building 2W Ramp Survey Unit

#### **Concrete Material**

| Location | Removable Beta<br>(dpm/100cm <sup>2</sup> ) | Uncertainty<br>95% CL | MDA | Removable Alpha<br>(dpm/100cm <sup>2</sup> ) | Uncertainty<br>95% CL | MDA |
|----------|---------------------------------------------|-----------------------|-----|----------------------------------------------|-----------------------|-----|
| F1       | -4.3                                        | 12.6                  | 134 | -0.5                                         | 2.4                   | 12  |
| F2       | -22                                         | 21.3                  | 134 | -0.5                                         | 2.4                   | 12  |
| F3       | -65                                         | 34.2                  | 134 | -0.5                                         | 2.4                   | 12  |
| F4       | -30                                         | 24.2                  | 134 | -0.5                                         | 2.4                   | 12  |
| F5       | -13                                         | 17.4                  | 134 | -0.5                                         | 2.4                   | 12  |
| F6       | 4.3                                         | 12.6                  | 134 | -0.5                                         | 2.4                   | 12  |
| F7       | 8.7                                         | 15.2                  | 134 | -0.5                                         | 2.4                   | 12  |
| F8       | 17                                          | 19.2                  | 134 | 2.4                                          | 5.2                   | 12  |
| F9       | -8.7                                        | 15.2                  | 134 | -0.5                                         | 2.4                   | 12  |
| F10      | -4.3                                        | 12.6                  | 134 | 2.4                                          | 5.2                   | 12  |
| F11      | 13                                          | 17.4                  | 134 | -0.5                                         | 2.4                   | 12  |
| F12      | 4.3                                         | 12.6                  | 134 | -0.5                                         | 2.4                   | 12  |

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## Ludlum 2929 No. 115563 with 43-10 No. 127216 Info:

|                  | Beta  | Alpha |
|------------------|-------|-------|
| Background (cpm) | 73    | 0.18  |
| Bkgd ct. time    | 60    | 60    |
| Sample ct. time  | 1     | 1     |
| Efficiency       | 0.231 | 0.347 |
| MDA              | 134   | 12.0  |

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#### Elevated Removable Surface Activity Measurements Molycorp - Building 2W Ramp Survey Unit

#### **Concrete Material**

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No elevated removable surface activity was reported above limits.

#### Exposure Rate Measurements Molycorp - Building 2W Ramp Survey Unit

#### **Concrete Material**

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| Location | Exposure Rate<br>(uR/hr) | Net Exp Rate<br>(uR/hr) |
|----------|--------------------------|-------------------------|
| F1       | 7                        | -2                      |
| F2       | 8                        | -1                      |
| F3       | 8                        | -1                      |
| F4       | 8                        | -1                      |
| F5       | 7                        | -2                      |
| F6       | 8                        | -1                      |
| F7       | 8                        | -1                      |
| F8       | 9                        | 0                       |
| F9       | 8                        | -1                      |
| F10      | 8                        | -1                      |
| F11      | 8                        | -1                      |
| F12      | 8                        | -1                      |

Background dose rate: 8-10 uR/hr with Model 19, No. 22526

## Summary of Building Surface Direct Reading (Total Activity) Results Molycorp - Building 2W Ramp Survey Unit

#### **Concrete Material**

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|         | E                | Beta      |                          | Alpha   |  |            |                          |  |  |  |  |
|---------|------------------|-----------|--------------------------|---------|--|------------|--------------------------|--|--|--|--|
| n<br>12 |                  | s<br>79.8 | μ <sub>α</sub><br>-258.9 | n<br>12 |  | s<br>159.6 | μ <sub>α</sub><br>-517.9 |  |  |  |  |
|         | t <sub>1-α</sub> | 1.782     |                          |         |  |            |                          |  |  |  |  |
|         |                  | Guid      | lelines/Cond             | itions  |  |            |                          |  |  |  |  |

Satisfied?

| Beta | Alpha |
|------|-------|
| Yes  | Yes   |

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#### Summary of Exposure Rate Measurements Molycorp - Building 2W Ramp Survey Unit

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#### **Concrete Material**

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| n  | $\frac{1}{x}$ | S   | $\mu_{\alpha}$ |
|----|---------------|-----|----------------|
| 12 | -1.1          | 0.5 | -0.8           |

t<sub>1-α</sub> 1.782

#### Guidelines/Conditions Satisfied?

Yes

Appendix F

## **Instrumentation Data**

Molycorp Washington, PA

#### Instrumentation Data

This data package contains instrumentation information (background, QC, and source response data forms) for the instruments used during the final status survey of building foundations.

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# EFF . 231 Daily Instrumentation Operational Check Sheet

| Instrument   | 23                                                     | 50-1                | 412619                    | 10          | F                     | Probe:              | 43-106           | <sup>H.</sup> /33 | 871      |               |
|--------------|--------------------------------------------------------|---------------------|---------------------------|-------------|-----------------------|---------------------|------------------|-------------------|----------|---------------|
| Cal Due:     |                                                        | 1-16-               | 03                        |             | (                     | Cal Due:            | 12               | -14-02            | <b>.</b> | <u></u>       |
| Source       | ID: Te 9                                               | · 2 ·               | lean Source<br>Count Rate |             |                       | lean +2 σ<br>Value: | 4780             | ] Mean<br>V       |          | 196           |
| Radiat<br>Ty | lion<br>pe:                                            | 3- 8                | igma Value                | : 7/        | N                     | lean +3 σ<br>Value: | 4851             | Mean<br>V         | alue: Υ  | 425           |
| ,            | - • • • <u>-</u> · · · · · · · · · · · · · · · · · · · | Background          |                           |             |                       | Source              | Çheck            |                   | Res      | ults          |
| Date         | Time                                                   | Count<br>Time (min) | Gross<br>Counts           | BKGD<br>CPM | Count .<br>Time (min) | Gross<br>Counts     | W/I 2 σ<br>Value | W/I 3 σ<br>Value  | LLD      | SAT/<br>UNSAT |
| 9-17-02      | 0615                                                   | 5                   | 1653                      | 331         | l                     | 4490                | L .              |                   | 69       | Sat           |
| 9-17-02      | 1650                                                   | <u> </u>            | $\sim$                    | )           |                       | 4773                | /                |                   |          | Sat           |
| 9-18-02      | 0710                                                   | 5                   | 1647                      | 329         | l                     | 4748                |                  | ·                 | 69       | sat           |
| 9-18-2       | 1705                                                   |                     |                           |             | 1                     | 4612                | <u></u>          | •                 |          | st            |
| 9-19-02      | 0635                                                   | 5                   | 1677                      | 335         |                       | 4501                |                  |                   | . 69     | Set           |
| 9.19.02      | 1620                                                   |                     |                           |             | ll'                   | 4421                |                  | ~                 |          | dart          |
| 4-23.02      | 0800                                                   | 5                   | 1588                      | 318         | <u> </u>              | 4427                |                  | <u> </u>          | 67       | Lut           |
| 4.23.02      | 1650                                                   | <u> </u>            |                           |             | <u> </u>              | 4571                | <u> </u>         | <u>~</u>          |          | Sut           |
| 4.24-02      | 0640                                                   | 5                   | 1713                      | 343         | 1                     | 4498                |                  |                   | 69.7     | Sat           |
| 4.24.02      | 1645                                                   |                     |                           |             | <u> </u>              | 4622                | ~                | <u> </u>          |          | Sat           |
| 9.25-02      | 0655                                                   | 5                   | 1591                      | 318         |                       | 4498                | <u> </u>         | ~                 | 67.2     | Sat           |
| 9.25.00      | 1705                                                   |                     |                           |             | 1                     | 4676                | <u> </u>         | ~                 |          | Sut           |
| 9-26-02      | 0620                                                   | 5                   | 1406                      | 281         | (                     | 4520                |                  |                   | 63       | Sat           |
| 9-30-02      | 0645                                                   | 5                   | 1520                      | 304         |                       | 4544                |                  | <u> </u>          | 65.8     | Sait          |
| 4.70.02      | 1710                                                   |                     |                           | <u> </u>    | 1                     | 4651                |                  |                   |          | Sat           |
| 10-1-02      | 06-10                                                  | 5                   | 1604                      | 321         | 1                     | 4556                |                  |                   | 67,5     | sit           |

# EFF = , 17 Daily Instrumentation Operational Check Sheet

| Instrument   | 23         | 50-1                | #1261.                    | 90          | I                   | Probe:               | 43-10            | 6 <sup>H</sup> (33 | 871                |               |
|--------------|------------|---------------------|---------------------------|-------------|---------------------|----------------------|------------------|--------------------|--------------------|---------------|
| Cal Due: _   |            | l-16-               | 03                        |             | (                   | Cal Due:             | 12               | -14-02             | <u> </u>           |               |
| Source       | 1D: 11/23  | <i>H</i> . 1        | lean Source<br>Count Rate |             |                     | flean +2 σ<br>Value: | 718              |                    | n -2 σ<br>/alue: 6 | 02            |
| Radial<br>Ty | ion<br>pe: | × "                 | Sigma Value               | : 29        | )<br>)              | /lean +3 σ<br>Value: | 747              |                    | n -3 σ<br>/alue:   | 573           |
|              |            | Background          |                           |             |                     | Source               | Check            |                    | Res                | ults          |
| Date         | Time       | Count<br>Time (min) | Gross<br>Counts           | BKGD<br>CPM | Count<br>Time (min) | Gross<br>Counts      | W/I 2 σ<br>Value | W/I 3 σ<br>Value   | LLD                | SAT/<br>UNSAT |
| 9-17.02      | 0620       | 5                   | 27                        | 5           |                     | 695                  | /                |                    |                    | Set           |
| 9-17.02      | 1655       | ~                   | ~                         |             | 1                   | 672                  | ~                | ~                  |                    | Sat           |
| 9-18.02      | 0645       | 5                   | 16                        | 3.2         | 1                   | 645                  | _                | ·                  | . 9                | Sat           |
| 9-18-02      | 1705       | <u> </u>            |                           |             | 1                   | 691                  | ~                | L                  |                    | Sat           |
| 9.19.02      | 0625       | .5                  | 12                        | 2.4         | l                   | 686                  |                  |                    | 9                  | Sat           |
| 919.02       | 1830       |                     |                           |             | l1`                 | 682                  | ~                | ~                  |                    | Sut           |
| 4.23.02      | 0810       | 5                   | 1 4                       | 2.8         | ll                  | 671                  | -                |                    | 9                  | Sat           |
| 9.23.02      | 1650       |                     |                           |             | (                   | 664                  | · ~              | ;                  |                    | Scut          |
| 9-24-02      | 0640       | <u> </u>            | 17                        | 3.4         | l(                  | 665                  |                  |                    | 9.6                | Sat           |
| 9.24.02      | 1645       |                     |                           |             | k                   | 704                  | <u> </u>         |                    |                    | sut           |
| 9-25-02      | 0655       | 5                   | - 15                      | 5           | L                   | 644                  | <u>~</u>         |                    | 11-                | Sat           |
| 9.25.00      | 1705       |                     |                           |             | ll                  | 647                  | 2                |                    |                    | Sat           |
| 9-26-02      | 0640       | 5                   | 9                         | 1,8         | <u> </u>            | 671                  | /                |                    | 7.8                | Salt          |
| 9.30.02      | 0645       | 5                   | 14                        | 2.8         | /                   | 697                  |                  | 1                  | 9                  | Sat           |
| 9.20.02      | 1710       |                     |                           |             | ļ(                  | 673                  | <u> </u>         |                    |                    | sut           |
| 10-1-02      | 0640       | 5                   | 31                        | 4.2         | <u> </u>            | <i>Lele 5</i>        | _                |                    | -                  | Sist          |

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Daily Instrumentation Operational Check Sheet EFF=,231

| Instrument   | 2350          | -1 412              | 6190                      |             | F                   | Probe: <u> </u>      | 3-106            | # 133 d          | 871               |               |
|--------------|---------------|---------------------|---------------------------|-------------|---------------------|----------------------|------------------|------------------|-------------------|---------------|
| Cal Due: _   | 1-1           | 16-03               |                           |             | (                   | Cal Due:             | 12-              | 14-02            |                   |               |
| Source       | ID:'<br>Te 99 | A                   | lean Source<br>Count Rate | 1 .         |                     | flean +2 σ<br>Value: | 4780             | Mean<br>V        | alue: 4           | 496           |
| Radiai<br>Ty | ion<br>pe: B  | - S                 | ligma Value               | : 7/        | N                   | lean +3 σ<br>Value:  | 4851             | Mear<br>V        | n -3 σ<br>alue: 4 | 425           |
|              |               | Background          |                           |             |                     | Source               | Check            |                  | Res               | ults          |
| Date         | Time          | Count<br>Time (min) | Gross<br>Counts           | BKGD<br>CPM | Count<br>Time (min) | Gross<br>Counts      | W/I 2 σ<br>Value | W/I 3 σ<br>Value | LLD               | SAT/<br>UNSAT |
| 8-14-02      | 1640          |                     | ~                         |             | 1                   | 4731                 |                  | ~                |                   | SAT           |
| 8-15-02      | 0670          | 5                   | 1562                      | 312         | 1                   | 4544                 |                  |                  | 67                | Sat           |
| 8.15.02      | 1640          | ~                   |                           |             | 1                   | 4620                 |                  | -                |                   | Sat           |
| 8-19-02      | 0615          | 5                   | 1526                      | 305         | /                   | 4588                 |                  |                  | 66                | Sat           |
| 8-19.02      | 1440          |                     |                           | ~           | /                   | 4467                 |                  | <u>~</u>         |                   | Sat           |
| 8.20.02      |               | 5                   | 1507                      | 301         | <u> </u>            | 4520                 |                  | ~                | 65                | Set           |
| 8-20-02      | 1640          | ·                   | -                         | -           | /                   | 4629                 |                  |                  | •••••             | Sat           |
| 8-21-02      | .060.5        | 5                   | 1556                      | 311         | 1                   | 4507                 |                  |                  | 68                | Sat           |
| 9.9.02       | 0705          | 5                   | 1528                      | 306         | /                   | 4557                 | · ·              |                  | 66                | Sat           |
| 9-9-02       | 1630          |                     | <u> </u>                  |             | <u> </u>            | 4662                 |                  |                  |                   | Sat           |
| 9-10-02      | 0710          | 5                   | 2020                      | 418         | <i> </i>            | 4534                 | -                |                  | 11                | sit           |
| 9-11-02      | 0620          | .5                  | 1934                      | 387         | <u> </u>            | 4654                 |                  | <u> </u>         | 14                | Sat           |
| 9-12-02      | 0640          | 5                   | 1689                      | 338         | /                   | 4627                 |                  | -                | 69                | Sat           |
| 9-12.02      | 1625          |                     | •                         |             | l                   | 4786                 |                  | · · ·            |                   | Jut           |
| 9-16-02      | 7620          | . 5                 | . 1645                    | 329         |                     | 4761                 |                  |                  | 69                | Sat           |
| 4-16-02      | 1.530         |                     |                           |             | l                   | 4776                 |                  |                  | <b></b>           | Sat           |

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## Daily Instrumentation Operational Check Sheet

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|--------------|------------|---------------------|---------------------------|-----------------|---------------------|---------------------|------------------|-------------------|--------------------|---------------|
| Instrument:  |            |                     | 26190                     |                 | F                   | Probe:              | 13-106           | <sup>#</sup> /338 | 7/                 |               |
| Cal Due:     |            | 1-16-03             | >                         |                 | (                   | Cal Due:            | 12-14            | 4-07              | <u></u>            | ,             |
| Source       |            |                     | lean Source<br>Count Rate |                 |                     | lean +2 σ<br>Value: | 718              | Mean<br>V         | alue: 6            | 02            |
| Radiat<br>Ty | ion<br>pe: | × S                 | Sigma Value               | 29              | N                   | lean +3 σ<br>Value: | 747              | Mear<br>V         | n -3 σ<br>Jalue: 5 | 73            |
|              |            | Background          |                           |                 |                     | Source              | Check            |                   | Res                | ults          |
| Date         | Time       | Count<br>Time (min) | Gross<br>Counts           | BKGD<br>CPM     | Count<br>Time (min) | Gross<br>Counts     | W/I 2 σ<br>Value | W/I 3 ơ<br>Value  | LLD                | SAT/<br>UNSAT |
| 8.14.02      | 1650 .     |                     |                           | , <del></del> - | 1                   | 681                 | -                | _                 |                    | Sot           |
| 8-15-02      | 0635       | 5                   | 12                        | 2.4             |                     | 703                 |                  |                   | 9                  | Sat           |
| 8-15-02      | 16 -10     |                     | -                         |                 |                     | 620                 | 5                | /                 |                    | Sat           |
| 8-19.02      | 0630       | 5                   | 13                        | Z.6             | <u> </u>            | 679                 |                  |                   | 9                  | 5 at          |
| 8-19.02      | 1640       | ~                   | —                         | ~               | 1                   | 678                 | <u> </u>         |                   |                    | Sat           |
| 8-20-06      | 0630       | 5                   | 7                         | 1.4             |                     | 642                 |                  | -                 | 7 & MB             |               |
| 8.20-02      | 1645       |                     | ·                         |                 |                     | 655                 |                  |                   |                    | Sat           |
| 8-21-02      | 0670       | 5                   | 8                         | 1.6             | (                   | 617                 |                  |                   | · 8                | Sat           |
| 9.9.02       | 0705       | 5                   | 8                         | 1.6             | (                   | 658                 |                  | -                 | 8                  | Sat           |
| 9-9-02       | 1630       |                     |                           |                 |                     | 697                 |                  |                   | <u></u>            | Sut           |
| 9-10-02      |            | 5                   | 22                        | 4.4             |                     | 682                 |                  |                   |                    | Sout          |
| 9-11-02      | 0655       | .5                  | 20                        | <u> </u>        |                     | 690                 |                  |                   | 10.                | Set           |
| 9-12-02      | 0645       |                     | 18                        | 3,6             | !                   | 680                 |                  |                   | . 10               | <u>Sat</u>    |
| 9-12.02      | 1625       | 5                   | 9                         | 1.8             | l                   | 677                 |                  |                   | 8                  | 3 Jt<br>Sait  |
| 9-16-02      | 0675       |                     |                           |                 | <u> </u>            | 655                 |                  |                   | 0                  | Sat           |
|              |            | L                   | l                         | L               |                     | <u> </u>            | Lanza            |                   | l                  |               |

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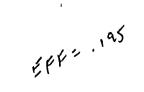
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Daily Instrumentation Operational Check Sheet

|              |             |                     | •                         |                                       |                     |                      |                  | Ħ                |                   |               |
|--------------|-------------|---------------------|---------------------------|---------------------------------------|---------------------|----------------------|------------------|------------------|-------------------|---------------|
| Instrument   | :           | 50-1 U              | 12941                     | 4                                     | F                   | Probe: <u>4</u>      | 3-106            | 128              | 914               |               |
| Cal Due: _   |             | 8-2-                | 03                        |                                       | (                   | Cal Due: 2-2-03      |                  |                  |                   |               |
| Source       | ID: Te9     | <b>^</b>            | lean Source<br>Count Rate | 1 11 .                                | ¥3 N                | lean +2 σ<br>Vaiue:  | 4791             |                  | a-2 σ<br>/alue: 4 | 495           |
| Radial<br>Ty | lion<br>pe: | B- s                | Sigma Value               | 74                                    | / N                 | flean +3 σ<br>Value: | 4864             |                  | n -3 σ<br>/alue:/ | 1421          |
|              |             | Background          |                           | · · · · · · · · · · · · · · · · · · · |                     | Source               | Check            | ,                | Res               | ults          |
| Date         | Time        | Count<br>Time (min) | Gross<br>Counts           | BKGD<br>CPM                           | Count<br>Time (min) | Gross<br>Counts      | W/I 2 σ<br>Value | W/I 3 σ<br>Value | LLD               | SAT/<br>UNSAT |
| 9-18-02      |             | 50                  |                           |                                       | 1                   | 4732                 | Ľ                |                  |                   | Sat           |
| 9-19-02      | 0655        | 5                   | 1625                      | 325                                   | 1                   | 4513                 |                  | -                | 68                | Sat           |
| 9.19.02      | 1635        |                     |                           |                                       |                     | <u>4574</u>          | <u> </u>         | <u> </u>         |                   | Sut           |
| 9-23-02      | 0645        | 5                   | 1332                      | 266                                   | l(                  | 4422                 |                  |                  | 62                | Sat           |
| 9.23.02      | 1655        |                     |                           | •                                     | l                   | 4552                 | ~                | <u> </u>         |                   | Sat           |
| 9-24-02      | 0640        | 5                   | 1487                      | 297                                   | <u> </u>            | 4496                 |                  | -                | 65                | Sat           |
| 9-24.02      | 1650        |                     |                           | ~~~                                   | l                   | 4569                 |                  |                  |                   | Sat           |
| 9-25-02      | 0655        | 5                   | 1512                      | 302                                   | <u> </u>            | 4502                 |                  |                  | 6516              | Sat           |
| 9.25.02      | 1700        |                     | 14444                     | 200                                   | <u> </u>            | 4530<br>4502         | ~                |                  |                   | Sat           |
| 9-26-02      | 0635        | 5                   | 1441                      | 288<br>241                            |                     | 4524                 |                  |                  | 64<br>58.9        | Sat<br>5 4    |
| 9.3002       | 1700        |                     |                           | -                                     |                     | 4435                 | 5                |                  | 70.1              | Sat<br>out    |
| 10-1-02      | 0640        | 5                   | 1362                      | 272                                   |                     | 4510                 |                  |                  | 62.4              | Set-          |
| 10.1.00      | 1645        |                     |                           |                                       | 1                   | 4552                 | -                | <u> </u>         | <u> </u>          | Sut           |
| 10-2-02      | 0625        | 5                   | 1251                      | 250                                   | 1                   | 4498                 |                  | ······           | 60                | Sat           |
| 10-2-02      | 1630        |                     |                           |                                       |                     | 4490                 | ~                | $\checkmark$     |                   | Sir           |



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## **Daily Instrumentation Operational Check Sheet**

| Instrument                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                    | - 2350  | )-1 ±1    | 29414      |          | F        | Probe:                                                                                                           | 43-10               | 6 H1     | 28914              | /    |
|---------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|---------|-----------|------------|----------|----------|------------------------------------------------------------------------------------------------------------------|---------------------|----------|--------------------|------|
| $9.19.02$ $0645$ $5$ $1Y$ $2.8$ $1$ $7\lambda9$ $  9$ $5at$ $9.19.02$ $1635$ $   1$ $735$ $  8at$ $9.23.02$ $0650$ $5$ $10$ $2$ $1$ $684$ $  8$ $5at$ $9.23.02$ $0650$ $5$ $10$ $2$ $1$ $684$ $  8$ $5at$ $9.23.02$ $1655$ $   1$ $705$ $  8.3$ $5at$ $9.24.02$ $0640$ $5$ $11$ $2.22$ $/$ $728$ $  8.3$ $5at$ $9.24.02$ $0640$ $5$ $11$ $2.22$ $/$ $728$ $  8.3$ $5at$ $9.24.02$ $0640$ $5$ $11$ $2.22$ $/$ $728$ $  8.3$ $5at$ $9.25.02$ $0700$ $5$ $17$ $3.4'$ $/$ $685$ $   8.3$ $5at$ $9.25.02$ $1700$ $   1$ $695$ $  8.3$ $5at$ $9.26.02$ $0650$ $5$ $12$ $2.4''$ $1$ $764'$ $ 8.3$ $5at$ $9.26.02$ $5$ $12$ $2.4''$ $1$ $733$ $  8.6$ $5at$ $9.26.02$ $5$ $10$ $2$ $1$ $721$ $  8.0$ $5at$ $10.102$   |         |           |            |          |          |                                                                                                                  |                     |          |                    |      |
| Source                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                        | ID: Th? | 30 3937 N |            |          | ,9 N     |                                                                                                                  | 799                 | 1        | n -2 σ<br>/alue: 6 | 79   |
|                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                               |         | s<br>,    | igma Value | : 30     | 5 N      |                                                                                                                  | 829                 |          | 1 /                | ,49  |
| Source ID: $8 - 2 - 0^{-5}$ Cal Due: $2 - 2 - 0^{-5}$ Source ID: $\frac{1}{1+230} \frac{1}{9}$ Mean Source       739       Mean $+ 2 \sigma$ Mean $- 2 \sigma$ Value: $739$ Mean $+ 2 \sigma$ Value: $679$ Radiation       Sigma Value: $30$ Mean $+ 3 \sigma$ Value: $679$ Background       Source Check       Results         Date       Time (min)       Count       Gross       BKGD       Count       Gross       W/l $2 \sigma$ W/l $3 \sigma$ Value: $679$ Date       Time (min)       Counts       Source Check       Results         Date       Count       Gross       BKGD        W/l $2 \sigma$ W/l $3 \sigma$ UNSAT         Time (min)       Counts       Suft 7 $717$ $717$ $717$ <td>ults</td> |         |           | ults       |          |          |                                                                                                                  |                     |          |                    |      |
| Date                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          | Time    |           |            |          | 1 1      |                                                                                                                  | 1                   |          | LLD                |      |
| 9-18-02                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       | 1700    |           |            | ·        | 1        | 717                                                                                                              | 5                   | ~        |                    | Jut  |
|                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                               |         | 5         | 14         | 2.8      | 1        | 729                                                                                                              |                     | 1        | 9                  |      |
| 9.19.02                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       | 1635    |           |            |          |          |                                                                                                                  | $\dot{\mathcal{C}}$ |          |                    | Sat  |
| 9-23-02                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       | 0650    | 5         | 10         | à        | Ĩ        | 684                                                                                                              | Ú                   |          | · 8                |      |
| 2.23.02                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       | 1655    |           |            |          | 1        | 105                                                                                                              | ~                   |          |                    | Sat  |
| 9-24-02                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       | 0640    | 5         | 11         | 2,2      | 1        | 728                                                                                                              | _                   |          | 8,3                | Sat  |
| 9-24.02                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       | 1650    |           |            |          |          | 709                                                                                                              | ~                   |          |                    | Sut  |
| 9-25-02                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       | 0700    | 5         | 17         | 3.4      |          | 681                                                                                                              |                     |          | 9,6                | Sat  |
| 9.25.02                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       |         |           |            |          | 1        |                                                                                                                  | <u> </u>            |          |                    | Sert |
| 9-26-02                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       | 0655    |           | 11         |          | <u> </u> |                                                                                                                  |                     |          |                    | Sat  |
| 9-30-02                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       | 0650    |           | 12         | 2.4      | <u> </u> | and the second |                     |          | 8.6                |      |
| 9.7000                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                        | 1700    |           |            | <u> </u> | ll       |                                                                                                                  |                     | <u> </u> |                    |      |
|                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                               |         | 5         | 10         | 2        | ιι       |                                                                                                                  |                     |          | 8.0                |      |
|                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                               |         | -         | ·          |          | /        |                                                                                                                  |                     | <u> </u> | I                  |      |
|                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                               |         | 5         | 10         | 2        | <u> </u> |                                                                                                                  |                     |          |                    |      |
| 10.2-02                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       | 1670    |           |            | l        | 1        | 704                                                                                                              | ~                   |          |                    | Sat  |

## Daily Instrumentation Operational Check Sheet

| E            |               | 40                  |                           |             | •                   |                     |                  |                  |                               |               |
|--------------|---------------|---------------------|---------------------------|-------------|---------------------|---------------------|------------------|------------------|-------------------------------|---------------|
| Instrument   | 235           | 1-0-1 H             | 129414                    | 4           | F                   | Probe: <u> </u>     | 3-106            | # 12891          | 4                             |               |
| Cal Due: _   |               | 8-2-03              |                           |             | (                   | Cal Due:            | 2                | -2-03            |                               |               |
| Source       | ID: Te 99     | E                   | lean Source<br>Count Rate |             | 3 N                 | lean +2 σ<br>Value: | 4791             | Mean<br>V        | alue: 44                      | 195           |
| Radial<br>Ty | lion<br>pe: B | S                   | igma Value                | 74          | N                   | lean +3 σ<br>Value: | 4864             |                  | $1 - 3 \sigma$<br>alue: $4 9$ | 2/            |
|              |               | Background          |                           |             |                     | Source              | Check            |                  | Res                           | ults          |
| Date         | Time          | Count<br>Time (min) | Gross<br>Counts           | BKGD<br>CPM | Count<br>Time (min) | Gross<br>Counts     | W/I 2 σ<br>Value | W/I 3 σ<br>Value | LLD                           | SAT/<br>UNSAT |
| 9.5.02       | 1705          |                     |                           |             | 1                   | 4650                | ~                | ~                |                               | Sut           |
| 9-6-02       | 0700          | 5                   | 1698                      | 340         | i                   | 4544                |                  |                  | 69                            | Sat           |
| 9-6-02       | 1300          |                     |                           |             | 1                   | 4635                |                  | -                | -                             | Sat           |
| 9-9-02       | 0615          | 5                   | 1747                      | 349         | 1                   | 4605                |                  | -                | 70                            | Sat           |
| 4.9-02       | 1640          |                     | <u> </u>                  | ÷           | 1                   | 4778                |                  | J                |                               | Set           |
| 9-10.02      | 0715          | 5                   | 1695                      | 239         | 1                   | 4557                | V                | ~                | 69                            | Sat<br>Sot    |
| 4-10-02      | 1650          |                     |                           | -           | 1                   | 4781                | -                | -                |                               | Sot           |
| 9-11-02      | 0650          | 5                   | 1509                      | 302         |                     | 4530                |                  | -                | 66                            | Sat           |
| 9-11-02      | 1615          | affal               | }                         |             |                     | 4631                |                  | $\smile$         |                               | Sat           |
| 9-12.0)      | 0630          | -່າງ                | 1576                      | 315         | 1                   | 4510                |                  |                  | 67                            | Sat           |
| 9.12.02      | 16000         |                     | (                         |             |                     | 4568                | <u> </u>         | L                |                               | Sut           |
| 9-16-02      | 0610          | 5                   | 1503                      | 301         | <u>'</u> ı          | 4501                |                  | -                | 66                            | Sat           |
| 9-16-02      | 1600.         |                     |                           | -           | 1                   | 4650                | 1                |                  | _                             | Sat           |
| 9.17.02      | 0615          | 5                   | 1605                      | 221         | 11                  | 4548                | ~                |                  | 68                            |               |
| 9-17-02      |               |                     | <u> </u>                  |             |                     | 4589                | /                | -                |                               | しい            |
| 9-18.02      | 0705          | 5                   | 1541                      | 308         | <u> </u>            | 4466                | _                |                  | 66                            | 507           |

|              | EFF = .1   | 95 Da               | aily Instr                | umentati    | ion Oper                                     | ational C            | heck Sh          | eet                                   |                   |               |
|--------------|------------|---------------------|---------------------------|-------------|----------------------------------------------|----------------------|------------------|---------------------------------------|-------------------|---------------|
| Instrument:  | 233        | 50 - 1              | #1294                     | 14          | F                                            | Probe: <u>43</u>     | 8-106            | # 12891                               | 4                 |               |
| Cal Due:     |            | . 8-2               | -03                       |             | (                                            | Cal Due:             | 2-2              | -03                                   |                   |               |
| Source       | ID: 7/1 23 |                     | lean Source<br>Count Rate | -           |                                              | flean +2 σ<br>Value: | 799              | Mean<br>V                             | alue:             | ,79           |
| Radiat<br>Ty | ion<br>pe: | s<br>جر             | Sigma Value               | : 30        | ,. N                                         | /lean +3 σ<br>Value: | 829              | Mean<br>V                             | i -3 σ<br>alue: 6 | 49            |
|              |            | Background          |                           |             |                                              | Source               | Check            |                                       | Res               | sults         |
| Date         | Time       | Count<br>Time (min) | Gross<br>Counts           | BKGD<br>CPM | Count<br>Time (min)                          | Gross<br>Counts      | W/I 2 σ<br>Value | W/I 3 σ<br>Value                      | LLD               | SAT/<br>UNSAT |
| 9.5.02       | 1705       | <br>                |                           |             |                                              | 725                  | ~                | ~                                     |                   | set<br>Sat    |
| 9-6-02       | 0700       | 5                   | 9                         | 1,8         | <u>     i                               </u> | 735                  |                  |                                       | 8                 | Sat           |
| 9.6.02       | 1300       |                     |                           |             | <u> </u>                                     | 741                  |                  |                                       |                   | Sat           |
| 9-9-02       | 0615       | 5                   | 11                        | 2.2         |                                              | 744                  |                  |                                       | 8                 | Sat           |
| 9.9.02       | 1640       |                     |                           |             | L (                                          | 743                  | <u> </u>         | <u> </u>                              |                   | Sat           |
| 9-10-02      | 0720       |                     | 12                        | 2.4         |                                              | 745                  | <u> </u>         | <u> </u>                              | 9                 | Sat           |
| 9-10-02      | 1650       |                     |                           |             | /                                            | 698                  |                  |                                       |                   | 3 ct          |
| 9-11-02      | 0650       | 5                   | 14                        | 2.8         | /                                            | 687                  |                  |                                       | 9                 | Sat           |
| 9.11.02      | 1615       |                     |                           |             | l                                            | 729                  | ~                |                                       |                   | Set           |
| 9-12-02      | 0635       | 5                   | <u> </u>                  | 2.2         | <u> </u>                                     | 739                  |                  |                                       | 8                 | Sat           |
| 9.12.00      | 1620       | <u>~</u>            |                           |             |                                              | 695                  | ~                | <u> </u>                              |                   | Sat           |
| 9-16-02      | 0635       | 5                   | 7                         | 1.4         | <u> </u>                                     | 738                  |                  |                                       | 7                 | 5at           |
| 9-16-02      | 1630       | -                   |                           | -           |                                              | 704                  |                  |                                       |                   | Sat           |
| 9-17.02      | 0620       | 5                   | 8                         | 1.6         | <u> </u>                                     | 739                  | 5                | 5                                     | . 8               | Sat           |
| 9-17-02      | 1645       |                     |                           |             | ļ(                                           | 712                  | ~                |                                       |                   | Sut           |
| 9-18-02      | 0705       | 5                   | 15                        | 3           |                                              | 1 708                |                  | · · · · · · · · · · · · · · · · · · · | 9                 | Sat           |

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## Ludlum Model 19 Micro-Rem

#### Routine Performance and Background Data Form

| Instrument ID # | 1: 225     | 26 Cal                 | . Due: /-,                                                                    | 29-03                    | Source IE                                    | Source ID #: C5 - 137 A6143 |            |  |  |  |
|-----------------|------------|------------------------|-------------------------------------------------------------------------------|--------------------------|----------------------------------------------|-----------------------------|------------|--|--|--|
| Mean Source V   | 'alue: /60 | Me                     | Mean plus + 20% Value:         192         Mean plus - 20% Value:         128 |                          |                                              |                             |            |  |  |  |
|                 | T          |                        |                                                                               | ~ 1                      |                                              | ·····                       |            |  |  |  |
|                 | ,          |                        | 4 Meter                                                                       |                          |                                              | Background                  | Sat/Unsat  |  |  |  |
| Date            | Time       | 25 μrem<br>(sat/unsat) | 50 μrem<br>(sat/unsat)                                                        | 250 μrem<br>+/-20% value | 500 μrem<br>+/-20% value                     | Reading                     | SavOnsat   |  |  |  |
| 8-30-07         | 0700       |                        |                                                                               | 160                      | A                                            | /                           | SAT        |  |  |  |
| 9.3.02          | 0630       |                        |                                                                               | 150                      | /                                            | 10                          | sat        |  |  |  |
| 9-4-07          | 0610       |                        |                                                                               | 160                      | /                                            |                             | Sat        |  |  |  |
| 9-5-02          | 0600       |                        |                                                                               | 160                      | /                                            | 10                          | Sot        |  |  |  |
| 9.6.02          | 0635       |                        |                                                                               | 160                      |                                              | 10                          | Sat        |  |  |  |
| 9-9-02          | 0 6 1 0    |                        |                                                                               | 160                      | /                                            | 10                          | Sat        |  |  |  |
| 9-10.02         |            |                        |                                                                               | 160                      |                                              | 15                          | Sat        |  |  |  |
| 9-11-02         | 0625       |                        |                                                                               | 160                      |                                              | 11                          | Sat        |  |  |  |
| 9-12-02         | 0610       | N                      | 1/                                                                            | 160                      | N/                                           | 11                          | Sat        |  |  |  |
| 9-16-02         | 0600       |                        | X A                                                                           | 150                      | A                                            |                             | sat        |  |  |  |
| 9-17.02         | 0610       |                        |                                                                               | 140                      |                                              | . 12                        | Sat        |  |  |  |
| 9-18-02         | 0640       |                        |                                                                               | 160                      | <u>                                     </u> | 12                          | Sat        |  |  |  |
| 9-19-02         | 0615       |                        |                                                                               | 150                      | /                                            | 10                          | Sat        |  |  |  |
| 9-23-02         | 0635       |                        |                                                                               | 160                      | ļ/                                           | 9                           | Jal<br>Sat |  |  |  |
| 9-24-02         | 0675       |                        |                                                                               | 160                      | _/                                           | 10                          | Sat        |  |  |  |
| 9-25-07         | 0650       | ./                     |                                                                               | 140                      | <u>  /</u>                                   | 10                          | Sait       |  |  |  |
| 9-26.02         | 0640       |                        |                                                                               | 140                      | /                                            | 8.                          | Set        |  |  |  |
| 9-30-02         | 0640       |                        |                                                                               | 140                      | 1/                                           | 8                           | Sat        |  |  |  |
| 10-1-02         | 0630       | /                      |                                                                               | 140                      | V                                            | 9                           | Sat        |  |  |  |

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## Daily Instrumentation Operational Check Sheet

| EFF-, 231              |                                                                          |                     |                 |             |                                                                                                                  |                    |                  |                  |      |               |
|------------------------|--------------------------------------------------------------------------|---------------------|-----------------|-------------|------------------------------------------------------------------------------------------------------------------|--------------------|------------------|------------------|------|---------------|
| Instrument:            | 2929                                                                     | - 11-               | 5563            | <u> </u>    | P                                                                                                                | Probe:             | 3-10 =           | 12721            | 6    |               |
| Cal Due:               |                                                                          | 6-14-0              | 3               |             | Cal Due: 6 - 1 4 - 0 3                                                                                           |                    |                  |                  |      | ,<br>         |
| Source ID: Mean Source |                                                                          |                     |                 |             | $\begin{array}{c c} Mean + 2 \sigma \\ \hline \end{array} & \\ Value: & 382 \gamma \\ Value: & 3620 \end{array}$ |                    |                  |                  | 620  |               |
|                        | RadiationBSigma Value:5 /Mean +3 σMean -3 σType:B5 /Value:3875Value:3569 |                     |                 |             |                                                                                                                  |                    |                  |                  |      |               |
| Background             |                                                                          |                     |                 |             |                                                                                                                  | Source Check Resul |                  |                  |      | ults          |
| Date                   | Time                                                                     | Count<br>Time (min) | Gross<br>Counts | BKGD<br>CPM | Count<br>Time (min)                                                                                              | Gross<br>Counts    | W/I 2 σ<br>Value | W/I 3 σ<br>Value | LLD  | SAT/<br>UNSAT |
| 9-6-02                 | 0630                                                                     | 60                  | 4169            | 69          | 1                                                                                                                | 3815               |                  |                  | 31   | Sat           |
| 9-9-02                 | 0600                                                                     | 60                  | 4333            | 72          | 1                                                                                                                | 3757               |                  |                  | 3 /  | Sat           |
| 4.10.02                | 0600                                                                     | 60                  | 4425            | 74          | 1                                                                                                                | 7624               | <u> </u>         |                  | 32   | <u>Sat</u>    |
| 9-11-02                | 0615                                                                     | 100                 | 4358            | 73          | 1                                                                                                                | 3661               |                  |                  | 3 æ  | Sat           |
| 9-12-02                |                                                                          | 60                  | 4351            | 73          |                                                                                                                  | 3757               | -                | -                | 31   | Set           |
| 9.16-02                |                                                                          | 60                  | 4245            | 71          |                                                                                                                  | 3775               |                  |                  |      |               |
| 4.17.02                | 0605                                                                     | 60                  | 4404            | 73          | 1                                                                                                                | 3732               | ~                | ~                | 31   | Sat.          |
| 9-18-02                | 0530                                                                     | 60                  | 4388            | 73          | 1                                                                                                                | 3785               | <u> </u>         |                  | 31   | Sat           |
| 9-19-02                | 0600                                                                     | 60                  | 4503            | 75          | 1                                                                                                                | 3802               | -                |                  | 32   | Sat           |
| 9-23-02                |                                                                          | 60                  | 4339            | 72          |                                                                                                                  | 3767               | ~                |                  | 31   | _Sat_         |
| 9-24-02                |                                                                          | 60                  | 4332            | 72          | <u> </u>                                                                                                         | 3776               |                  |                  | 31   | Sal           |
| 9-25-02                | 1                                                                        | 60                  | 4425            | 74          |                                                                                                                  | 3641               | <u> </u>         |                  | 31   | 5at<br>Set    |
| 9-26-02                | 0720                                                                     | 60                  | 4229            | 70          | 1(                                                                                                               | 3759               |                  |                  | 30.7 |               |
| 9-30-02                | 0620                                                                     | 60                  | 4278            | 71          | 1                                                                                                                | 3687               | <u></u>          |                  | 30.9 | Sat           |
| 10-1-07                | 0670                                                                     | 60                  | 4312            | 72          | 1                                                                                                                | 3651               |                  |                  | 31   | Sat           |
| 10-2-02                | 0620                                                                     | 60                  | 4196            | 70          | 1 1                                                                                                              | 3784               | -                | —                | 30,7 | Suit          |

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## **Daily Instrumentation Operational Check Sheet**

| •                           | EFF : . 3   | 47.                 | any mou                   | umentat     | ion oper            |                      | SHECK SH         | eel              |                        |             |
|-----------------------------|-------------|---------------------|---------------------------|-------------|---------------------|----------------------|------------------|------------------|------------------------|-------------|
|                             | :           |                     | 5563                      |             | i                   | Probe:               | 43-10            | #127             | 216                    |             |
| Cal Due: _                  |             | 6-                  | 14-03                     | <u></u>     | (                   | Cal Due:             |                  | 6-14.            | -03                    | <u> </u>    |
| Source                      | 1D: 7/2 23  | 0 <sup>#</sup> 3937 | Mean Source<br>Count Rate |             |                     | /lean +2 σ<br>Value: | 1448             |                  | n -2 σ<br>/alue: / 3   | 04          |
| Radiat<br>Ty                | lion<br>pe: | <u>ک</u> '          | Sigma Value               | .36         | N                   | /lean +3 σ<br>Value: | 1484             | <i>n</i>         | n -3 σ<br>/alue:   / · | 268         |
| Background Source Check Res |             |                     |                           |             |                     |                      | Res              | ults             |                        |             |
| Date                        | Time        | Count<br>Time (min) | Gross<br>Counts           | BKGD<br>CPM | Count<br>Time (min) | Gross<br>Counts      | W/I 2 σ<br>Value | W/I 3 σ<br>Value | LLD                    | ·SAT<br>UNS |
| 96-02                       | 0635        | 60                  | 12                        | . 2         |                     | 1371                 |                  |                  | 4                      | Sat         |
| 9-9-02                      | 0600        | 60                  | 10                        | .17         |                     | 1431                 |                  |                  | 4                      | Se          |
| 9-10:02                     | 0600        | 60                  | 8                         | .13         |                     | 1268                 |                  | <u> </u>         | 4                      | Sai         |
| 9-11-02                     | 0615        | 60                  |                           | .18         |                     | 1329                 |                  |                  | . 4                    | Sai         |
| 9-12-02                     |             | 60                  | 11.15 mg                  | .18 07 M    | <i>i</i>            | 1408                 |                  |                  | 4-5NB                  | ەك          |
| 9-16-02                     | 0615        | 60                  | 10                        | .17         |                     | 1350                 |                  |                  | '4                     | يک          |
| 9.17.02                     | 0605        | 40                  | 7                         |             | I                   | 1427                 |                  |                  | 4                      |             |
| 9-18-02                     | 0630        | 60                  | 13                        | . 22        |                     | 1369                 |                  |                  | 4.5                    | _San        |
| 9-19-02                     | 0600        |                     | 8                         | ,13         | /                   | 1353                 |                  |                  | <u> </u>               | <u> </u>    |
| 9-23-02                     | 0630        | 60                  | 20                        | ,33         | /                   | 1402                 |                  | ~                | 5'                     | _Sa         |
| 9-24-02                     | 0620        | 60                  | 11                        | .18         | <i> </i>            | 1388                 | -                |                  | 4                      | <u> </u>    |
| 9-25.02                     | 0620        | 60                  | 13                        | ,22         | <u> </u>            | 1357                 |                  |                  | 5                      | <u> </u>    |
| 9-26.02                     | 0720        | 60                  | 12                        | . 2         | (                   | 1436                 |                  | <u> </u>         | 4.5                    | <u> </u>    |
| 9-30.02                     | 0620        | 60                  | 10                        | .17         | <i> </i>            | 1443                 | /                | -                | 4.4                    | <u> </u>    |
| 10-1-02                     | 0620        | 60                  | P                         | -15_        | (                   | (374                 |                  | <u> </u>         | 4.3                    | <u> </u>    |
| 10-2-02                     | 0620        | 60                  | 10                        | .17         | l(                  | 1357                 | -                |                  | 4.4                    | <u> </u>    |

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Sat Sat Sat Sut Sex Sut Sat Sat Sal ΣM. Sa Sat Sat Sat Sa Sa

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Appendix G

# Background Assessment Data Molycorp Washington, PA

#### **Background Assessment**

MACTEC performed material-specific backgrounds for poured concrete with its three large-area gas flow instruments. The most conservative backgrounds values were selected and used for all background subtracts for direct (static) type surveys performed.

Background measurements for poured concrete and metal/drywall were calculated from surveys obtained at the Canton Volunteer Fire Department Station 52-1, Canton Township, PA on their poured concrete surfaces and their building structure. A mean value for each instrument was calculated. The most conservative background value was selected and used by the Health Physics technicians for all instrument background subtractions.

Included in this appendix are the results of MACTEC's background assessment data

Poured Concrete Surfaces

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#### Ludium Model 2350-1 (126190) with 43-106 (133871)

|                    | Beta - Direc | ct Measurer   | nents (cpm) | Alpha - Direct Measurements (cpm) |
|--------------------|--------------|---------------|-------------|-----------------------------------|
|                    | Unshield     | <u>Shield</u> | Net         | Net                               |
|                    | 500          | 350           | 150         | 9                                 |
|                    | 418          | 314           | 104         | 6                                 |
|                    | 447          | 326           | 121         | 8                                 |
|                    | 494          | 312           | 182         | 5                                 |
|                    | 483          | 351           | 132         | 3                                 |
|                    | 466          | 306           | 160         | 6                                 |
|                    | 478          | 347           | 131         | 9                                 |
|                    | 469          | 327           | 142         | 8                                 |
|                    | 426          | 353           | 73          | 12                                |
|                    | 429          | 343           | 86          | 7                                 |
|                    | 499          | 349           | 150         | 10                                |
|                    | 462          | 330           | 132         | 9                                 |
|                    | 496          | 372           | 124         | 8                                 |
|                    | 491          | 336           | 155         | 9                                 |
|                    | 458          | 295           | 163         | 12                                |
|                    | 527          | 337           | 190         | 11                                |
|                    | 464          | 327           | 137         | 13                                |
|                    | 521          | 302           | 219         | 12                                |
|                    | 492          | 323           | 169         | 4                                 |
|                    | 484          | 319           | 165         | 8                                 |
| Mean (cpm)         | 144          |               |             | 8                                 |
| Stand<br>Deviation | 34.4         |               |             | 2.8                               |
| n <sub>b</sub>     | 4            |               |             | 8                                 |

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**Poured Concrete Surfaces** 

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Ludlum Model 2350-1 (129414) with 43-106 (128914)

Beta - Direct Measurements (cpm)

|                    | <u>Unshield</u> | <u>Shield</u> | <u>Net</u> |
|--------------------|-----------------|---------------|------------|
|                    | 492             | 301           | 191        |
|                    | 479             | 348           | 131        |
|                    | 496             | 306           | 190        |
|                    | 537             | 340           | 197        |
|                    | 610             | 316           | 294        |
|                    | 465             | 302           | 163        |
|                    | 547             | 331           | 216        |
|                    | 509             | 335           | 174        |
|                    | 510             | 355           | 155        |
|                    | 541             | 346           | 195        |
|                    | 563             | 320           | 243        |
|                    | 517             | 341           | 176        |
|                    | 505             | 375           | 130        |
|                    | 530             | 352           | 178        |
|                    | 520             | 370           | 150        |
|                    | 518             | 332           | 186        |
|                    | 519             | 411           | 108        |
|                    | 506             | 365           | 141        |
|                    | 570             | 360           | 210        |
|                    | 534             | 343           | 191        |
|                    |                 |               |            |
| Mean (cpm)         | 181             |               |            |
|                    |                 |               |            |
| Stand<br>Deviation | 42.0            |               |            |
| Deviation          |                 |               |            |
| n.                 | 4               |               |            |
| n <sub>b</sub>     | *               |               |            |

**Poured Concrete Surfaces** 

Ludlum Model 2350-1 (95359) with 43-106 (133866)

Beta - Direct Measurements (cpm)

|                    | <u>Unshield</u> | <u>Shield</u> | <u>Net</u> |
|--------------------|-----------------|---------------|------------|
|                    | 460             | 330           | 130        |
|                    | 482             | 397           | 85         |
|                    | 592             | 381           | 211        |
|                    | 589             | 381           | 208        |
|                    | 561             | 344           | 217        |
|                    | 555             | 408           | 147        |
|                    | 491             | 388           | 103        |
|                    | 511             | 392           | 119        |
|                    | 643             | 409           | 234        |
|                    | 606             | 375           | 231        |
|                    | 563             | 429           | 134        |
|                    | 590             | 386           | 204        |
|                    | 703             | 407           | 296        |
|                    | 682             | 389           | 293        |
|                    | 551             | 370           | 181        |
|                    | 518             | 332           | 186        |
|                    | 601             | 411           | 190        |
|                    | 599             | 365           | 234        |
|                    | 520             | 403           | 117        |
|                    | 522             | 407           | 115        |
| Mean (cpm)         | 182             |               |            |
| Stand<br>Deviation | 61.1            |               |            |
| n <sub>b</sub>     | 8               |               |            |

**Poured Concrete Surfaces** 

#### Ludlum Model 2350-1 (95356) with 43-68 (91046)

|                    | Beta - Direc    | t Measuren | nents (cpm) | Alpha - Direct Measurements (cpm) |  |  |
|--------------------|-----------------|------------|-------------|-----------------------------------|--|--|
|                    | <u>Unshield</u> | Shield     | Net         | Net                               |  |  |
|                    | 460             | 330        | 130         | 10                                |  |  |
|                    | 482             | 397        | 85          | 14                                |  |  |
|                    | 592             | 381        | 211         | 15                                |  |  |
|                    | 589             | 381        | 208         | 12                                |  |  |
|                    | 561             | 348        | 213         | 23                                |  |  |
|                    | 555             | 408        | 147         | 11                                |  |  |
|                    | 491             | 388        | 103         | 13                                |  |  |
|                    | 511             | 392        | 119         | 6                                 |  |  |
|                    | 1014            | 409        | 605         | 18                                |  |  |
|                    | 606             | 375        | 231         | 17                                |  |  |
|                    | 523             | 429        | 94          | 12                                |  |  |
|                    | 590             | 386        | 204         | 14                                |  |  |
|                    | 703             | 407        | 296         | 17                                |  |  |
|                    | 662             | 389        | 273         | 13                                |  |  |
|                    | 551             | 408        | 143         | 10                                |  |  |
|                    | 518             | 346        | 172         | 7                                 |  |  |
|                    | 478             | 349        | 129         | 12                                |  |  |
|                    | 465             | 345        | 120         | 5                                 |  |  |
|                    | 520             | 403        | 117         | 14                                |  |  |
|                    | 522             | 407        | 115         | 13                                |  |  |
| Mean (cpm)         | 186             |            |             | 13                                |  |  |
| Stand<br>Deviation | 115.5           |            |             | 4.2                               |  |  |
| n <sub>b</sub>     | 29              |            |             | 8                                 |  |  |

**Poured Concrete Surfaces** 

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#### Ludlum Model 2350-1 (117563) with 43-106 (128912)

|                    | Beta - Direc | t Measurer    | ments (cpm) | Alpha - Direct Measurements (cpm) |
|--------------------|--------------|---------------|-------------|-----------------------------------|
|                    | Unshield     | <u>Shield</u> | Net         | Net                               |
|                    | 549          | 429           | 120         | 14                                |
|                    | 641          | 449           | 192         | 13                                |
|                    | 629          | 487           | 142         | 9                                 |
|                    | 630          | 501           | 129         | 16                                |
|                    | 651          | 498           | 153         | 14                                |
|                    | 629          | 480           | 149         | 10                                |
|                    | 634          | 494           | 140         | 8                                 |
|                    | 684          | 467           | 217         | 5                                 |
|                    | 728          | 458           | 270         | 11                                |
|                    | 741          | 576           | 165         | 10                                |
| Mean (cpm)         | 168          |               |             | 11                                |
| Stand<br>Deviation | 46.3         |               |             | 3.3                               |
| n <sub>b</sub>     | 6            |               |             | 7                                 |