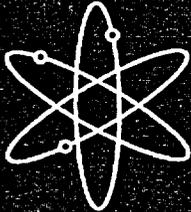




# **ANL/CANTIA: A Computer Code for Steam Generator Integrity Assessments**



**Argonne National Laboratory**



**U.S. Nuclear Regulatory Commission  
Office of Nuclear Regulatory Research  
Washington, DC 20555-0001**



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Prepared by  
S. Majumdar

Argonne National Laboratory  
9700 South Cass Avenue  
Argonne, IL 60439

J. Davis, NRC Project Manager

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Office of Nuclear Regulatory Research  
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# **ANL/CANTIA: A Computer Code for Steam Generator Integrity Assessments**

by

Saurin Majumdar

## **Abstract**

This report summarizes the work carried out to modify and expand the capability of the steam generator integrity code CANTIA originally developed for CANDU reactors. The basic algorithms for the Monte Carlo simulation, the random initiation of cracks, the effect of inservice inspection including the probability of detection (POD) of cracks, and the inclusion of plugging criteria for defective tubes have been retained. Additional ligament rupture, unstable burst, and leak rate models for Alloy 600 tubes that have been developed or validated at Argonne National Laboratory have been incorporated into the code. Fracture mechanics models for crack growth rate based on stress corrosion cracking data from the literature have also been added. The basic treatment of flaw growth has been changed from one- to two-dimensional, and crack growth calculations have been made more rigorous.

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## **Executive Summary**

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This report summarizes work carried out to modify and expand the capability of the steam generator integrity assessment code CANTIA (CANDU Tube Inspection Assessment). CANTIA was developed by Dominion Engineering, Inc. under contract from Atomic Energy Control Board of Canada [now the Canadian Nuclear Safety Commission] to simulate the effects of tube inspection and maintenance strategies on the operation of steam generators for CANDU reactors. The integrity and leak rate models in CANTIA were specifically intended for CANDU steam generators.

Under the Nuclear Regulatory Commission sponsored Integrated Steam Generator Tube Integrity Program (ISGTIP-2), Argonne National Laboratory has developed and/or validated several models for predicting ligament rupture, unstable burst, and leak rate of flawed Alloy 600 tubes. It was decided to use CANTIA as a vehicle for incorporating these integrity and leak rate models into an integrity assessment code. Several other modifications were also made in ANL/CANTIA. The source language of the code was updated to Visual BASIC 6. The treatment of the basic flaw was changed from one-dimensional to two-dimensional and the calculation routines for crack growth were made more rigorous. Two well-known stress corrosion crack growth models from the literature were included as options, and a simple residual stress model has been added. ANL/CANTIA can handle either axial or circumferential cracks, but not both simultaneously.

Preliminary trial runs demonstrated that it is very difficult to grow stress corrosion cracks in SG tubes by pressure stress alone. Several trial runs with residual stress were conducted to demonstrate the importance of probability of detection (POD) and initiation of new cracks on rupture and leak rate probabilities.

A list of future modifications to further improve the capability of the code is included.

## **Acknowledgments**

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## List of Acronyms

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ANL	Argonne National Laboratory
BWR	Boiling water reactor
CANTIA	CANDU Tube Inspection Assessment
COA	Crack opening area
COD	Crack opening displacement
EC	Eddy current
ISGTIP-2	Integrated Steam Generator Tube Integrity Program
ISI	In-service inspection
NRC	(U.S.) Nuclear Regulatory Commission
PNNL	Pacific Northwest National Laboratory
POD	Probability of detection
PWR	Pressurized water reactor
PWSCC	Primary water stress corrosion cracking
RT	Room temperature
SCC	Stress corrosion cracking
SG	Steam generator
TSP	Tube support plate
TW	Throughwall

## List of Symbols

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A	crack opening area
A, n	crack growth rate constants
B	constant for defining stress intensity factor
a	crack depth
$a_c$	critical crack length
a, b	parameters for linear-logistic distribution and flaw size measurement model
b, $\theta$	parameters for Weibull distribution
$B(\alpha_1, \alpha_2)$	beta function
c, $c_e$	half crack and half effective crack lengths
E	Young's modulus
$f(x)$	function of x
h	wall thickness
K, $K_I$	stress intensity factor
K	flow stress parameter
$K_{th}$	threshold stress intensity factor
k, $\lambda$	parameters for gamma function
m	bulging factor
$m_p$	ligament stress magnification factor
N, k, P	parameters for negative binomial distribution
P	pressure
$P_{burst}$ , $P_{cr}$	unstable burst pressure
$p(k)$	probability of observing k flaws
Q	leak rate

$R_m, R_o, R_i$	mean radius (or radius of curvature), outer radius, and inner radius of tube
$S$	stress
$S_y, S_u$	yield and ultimate tensile strengths
$T, T_f$	temperature and failure temperature
$t, t_{\text{initial}}$	time and initial time
$t$	wall thickness
$t, x$	integration variables
$\alpha, \beta$	parameters for log-logistic distribution
$\alpha_1, \alpha_2$	parameters for beta function
$\Delta p$	pressure differential
$\delta, \lambda$	parameters for Gumbel distribution
$\delta$	flow stress temperature correction factor
$\Gamma(x)$	gamma function
$\mu, \sigma$	parameters for normal and lognormal distributions
$\rho$	density of water
$\sigma$	stress, hoop stress
$\bar{\sigma}$	flow stress
$\sigma_{\text{lig}}$	ligament stress
$\sigma_m, \sigma_b$	membrane and bending stresses
$\sigma_y, \sigma_u$	yield and ultimate tensile strengths
$\theta$	half circumferential crack angle

# 1 Introduction

---

The Nuclear Regulatory Commission (NRC) is developing a "performance-based" regulatory framework to assure steam generator tube integrity. Instead of just meeting prescribed rules on allowable flaw sizes for tubes that have been inspected, evaluations and assessments are necessary to show that adequate levels of integrity can be maintained until the next scheduled outage. The industry has developed codes and procedures to carry out these assessments. It would be desirable to have a comprehensive validated model that integrates all important aspects of integrity evaluations starting from in-service inspection results and ending with a total leak rate at the end of an operating cycle under various assumed conditions. ANL/CANTIA is intended to provide a tool that could be used for independent assessment of steam generator integrity.

Under contract from the Atomic Energy Control Board of Canada [now the Canadian Nuclear Safety Commission], Dominion Engineering, Inc.<sup>1</sup> developed a Monte Carlo-based code called CANTIA (CANDU Tube Inspection Assessment) to simulate the effects of tube inspection and maintenance strategies on the safe operation of CANDU design nuclear steam generators. The integrity and leak rate models in CANTIA were specifically intended for the CANDU steam generators in Canada. A decision was made to use CANTIA as a framework for the development of a comprehensive integrated model of steam generator integrity and to incorporate into CANTIA the integrity and leak rate models that have been developed at ANL under the Integrated Steam Generator Tube Integrity Program (ISGTIP-2) sponsored by the NRC. The original CANTIA was written in Visual Basic 3.0, and a copy of the program, together with the user's manual were obtained by ANL from the AECCB. The program was updated to Visual BASIC 6.0 to run in a Windows NT environment and was then modified to incorporate the integrity and leak rate models developed at ANL. The basic Monte Carlo simulation portion of the code, together with much of the input format, were retained in the modified CANTIA code, renamed ANL/CANTIA.

## 2 Description of CANTIA

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The CANTIA code uses Monte Carlo techniques to determine probabilities of steam generator tube failures under accident conditions and primary-to-secondary leak rates under normal and accident conditions in the future. An initial flaw size distribution is input and the program determines future flaw size distributions. The effect of inspections of the steam generator tubes at future points in time, and subsequent removal of defective tubes from the population on the probabilities of failure and leak rates and the future flaw size distributions is calculated. Thus the effect of different inspection and maintenance strategies on the probability of tube failure and primary-to-secondary leak rate can be determined.

CANTIA is designed to handle various defect types (including circumferential and axial stress corrosion cracks [SCCs], frets, and pits), though only one type of degradation can be modeled at a time. All tubes modeled in a trial are treated as being equally susceptible to the chosen degradation mode, so that the same distributions of growth rates, flaw initiation, etc., are used for all the tubes in the trial. If different distributions are believed to describe the degradation in different parts of the steam generator, then separate simulations should be run with the appropriate distributions for the portion of generator being modeled.

CANTIA uses a probabilistic failure model. It calculates a time-dependent flaw size and number distribution so that the probability of failure or the rate of leakage can be estimated. It uses a Monte Carlo approach; each important parameter is treated as a random variable with known or predictable median behavior and a known or predictable distribution of behavior (i.e., variation) around the median. Both the median and variance of each random variable are specified by the user, or, if desired, a fixed (deterministic) value can be used. For each Monte Carlo trial, the value of each variable is chosen randomly in accordance with the selected distribution function, or the fixed value is used, so that the trials reflect the variability of the actual situation. A large enough number of trials (chosen by the user) are then run for each analysis to provide a stable statistical distribution of the results.

For each Monte Carlo trial, CANTIA determines flaw sizes, growth rates, inspection results, material properties, etc. for each tube, and tracks the progression of the flaws in each tube throughout the model time period. After all trials are run, the conditions from each trial at each time of interest are compiled to determine the distributions of flaw sizes, inspection results, leak rates, and tube failures at the times of interest. The steps used in the process are as follows:

- (1) All of the input parameters are checked to ensure that they are valid for the assumptions selected by the user (e.g., valid numbers are entered for the selected measurement error distribution). They are then imported into the calculational portion of the program, and the necessary arrays and variables are set up for use by the program.
- (2) If the user has entered a "measured" initial flaw distribution as opposed to an "actual" one, the "actual" flaw distribution is estimated from the measured flaw distribution density  $f(x)$  by dividing  $f(x)$  by the probability of detection function  $POD(x)$  and then renormalizing. Thus the number of flaws initially present is increased to account for the undetected flaws. Before dividing by the  $POD$ , the measured distribution is shifted to account for systematic measurement errors. The "actual" flaw size distribution is then

renormalized so its cumulative distribution is equal to 1 at the maximum flaw size, and the total number of flaws in the susceptible tube population is determined by dividing the number of flaws present in the inspected tube sample by the fraction of the susceptible population inspected.

- (3) Next, the individual trials are begun. CANTIA randomly selects a flaw size from the "actual" flaw size distribution (whether entered by the user or calculated from the measured flaw size distribution and POD) for each tube with a flaw at the initial time. Initiation times for flaws in tubes without initial flaws are also randomly selected; the size of the flaw at the time of initiation is selected by the user. Flaw growth rates are then randomly selected for each tube in the modeled population, and the size of the flaw on each tube at each future time of interest is calculated. For a particular flaw, the growth rate parameters are constant for all future times of interest in the trial (i.e., the growth rate parameters do not change during a trial). However, if a flaw size dependent growth rate model is selected, the flaw growth rate will change in a deterministic way with time. Any necessary tube material or tube dimensional properties are also randomly selected for each tube at this time; they also will remain constant throughout the trial.
- (4) CANTIA then determines the conditions in the steam generator at each time of interest. It begins by calculating the primary-to-secondary leak rate through each flaw under normal and accident conditions and assessing whether or not each flaw would cause its tube to fail under accident conditions at the first chronological time of interest (as input by the user). Next, inspections are performed if either the time of interest is a scheduled inspection time (as entered by the user), or the primary-to-secondary leak rate under normal conditions is larger than the allowed maximum (as entered by the user). Inspections are modeled with an initial sample size and expansion rule parameters and POD and measurement error distributions selected by the user, and are performed until either all of the tubes are inspected or no additional expansions of the tube sample size are required by the inspection expansion rules. Detected flaws that are larger than the plugging limit are then "repaired" by removing the tube from the sample population. This process is repeated for each additional time of interest.
- (5) Once the calculations of flaw size distributions, leak rates, inspection results, etc. at each time of interest are complete, CANTIA adds the results of the trial to the Monte Carlo data set. Additional trials are then performed. After all the trials are completed, the statistical-model outputs desired by the user (e.g., probability of one or more tube failure, flaw size distribution) are calculated for each time of interest and the results are saved to a text file (if the user desires) and the program is terminated.

## **2.1 Description of Input Data for CANTIA**

The input data needed for running CANTIA (version 1.1) are as follows:

### **2.1.1 General Data**

These relate to general data needed to run the probabilistic model.

Plant and Defect Information. The first set of data includes plant information, i.e., plant name, number of steam generators and total number of tubes. This information is only for reference and does not affect the model calculations. The second set of data includes defect information, i.e., defect type, location and number of susceptible tubes. The first two are for information only. The number of susceptible tubes is important to the execution of the model because it determines how many tubes will be simulated by the model.

Number of Trials. Next the number of trials, which should be large enough to provide the minimum resolution desired for output values, is entered. For example, if a minimum resolution of  $10^{-4}$  (0.01%) is desired on the probability of tube failure, then the model should run at least 10,000 trials. Due to a limitation of Visual BASIC 3.0, the maximum possible number of trials in the original CANTIA was 32,767. This limitation no longer applies to ANL/CANTIA.

Planned Inspection Times. Next, the number of in-service inspections (ISIs) and the times at which ISIs will be performed are entered. These times are absolute times, not time intervals. If no planned inspections are to be modeled, 0 is entered in the number of inspections.

Additional Times of Interest. These are additional times (in addition to inspection times) at which the model should compute output values. No inspection will be performed at these additional times unless the primary-to-secondary leak rate under normal conditions exceeds the allowable maximum. For the model to work, at least one planned inspection time or time of interest should be entered.

Model Starting Time. To make it easier to calibrate the flaw initiation distribution, the model starting time should not be set to zero, but at a real operating time (e.g., 1).

### 2.1.2 Initial Flaw Size Distribution

This discussion relates to input for the initial flaw size distribution.

Measured vs. Assumed Flaw Size Distribution The user chooses whether the initial flaw size distribution is assumed or is a distribution of measured defect sizes determined from ISI. As mentioned earlier, if the distribution is the measured inspection results, the program will convolve these results with the POD function and the fraction of the susceptible population inspected to estimate the "actual" number and sizes of flaws in the susceptible population.

Flaw size Distribution Five statistical distributions are available to choose from—beta, gamma, Gumbel, lognormal, and Weibull. Alternatively, a histogram ("Binned Results") of frequency of flaw sizes can be entered. For a statistical distribution (but not an entered histogram), when CANTIA selects the initial sizes of flaws, it will truncate and renormalize the distribution at the value of the size of flaws at initiation. For example, if it is assumed that the flaws initiate at a size of 20% throughwall (TW), the initial flaw size distribution will be truncated and renormalized so all of the flaws present at the beginning will be sized at 20% TW or larger. For the binned data, the first bin of the histogram should not contain any flaw. For example, if the smallest flaw measured by inspection is 5% TW, the first bin should be 4% and the number of tubes should be 0. In this case, no initial flaw size smaller than 5% TW would be selected by CANTIA for tubes in the susceptible population.

The various statistical distribution functions available in CANTIA are:

*Beta Distribution*

The density function for the beta distribution is:

$$f(x) = \begin{cases} \frac{x^{\alpha_1-1}(1-x)^{\alpha_2-1}}{B(\alpha_1, \alpha_2)} & \text{if } 0 < x < 1, \\ 0 & \text{otherwise} \end{cases} \quad (1)$$

where  $B(\alpha_1, \alpha_2)$  is the beta function defined by

$$B(\alpha_1, \alpha_2) = \int_0^1 t^{\alpha_1-1}(1-t)^{\alpha_2-1} dt \text{ for any real numbers } \alpha_1 > 0 \text{ and } \alpha_2 > 0.$$

If beta distribution is selected, the user must enter the values of  $\alpha_1$  and  $\alpha_2$ . Note that the beta distribution is only defined from 0 to 1; therefore, it can be used only for fractional throughwall depth for flaw sizes. It cannot be used for axial length or circumferential extent.

*Gamma Distribution*

The density function for the gamma distribution is as follows:

$$f(x) = \begin{cases} \frac{\lambda(\lambda x)^{k-1} e^{-\lambda x}}{\Gamma(x)} & x > 0, \\ 0 & \text{otherwise} \end{cases} \quad (2)$$

where  $\Gamma(x)$  is the gamma function defined by

$$\Gamma(x) = \int_0^{\infty} t^{x-1} e^{-t} dt \text{ for any real number } x > 0.$$

If gamma distribution is selected, the user must enter the values of  $\lambda$  and  $k$ . Note that since the gamma function is defined for any positive value of  $x$ , it can be used for any flaw size parameter.

*Gumbel Distribution*

The density function for the Gumbel distribution is:

$$f(x) = \frac{\exp\left(-\frac{x-\lambda}{\delta}\right) \exp\left(-\exp\left[-\frac{x-\lambda}{\delta}\right]\right)}{\delta} \text{ for all real } x \quad (3)$$

and where  $\lambda$  can be any real number and  $\delta$  must be a positive real number.

If the Gumbel distribution is selected, the user must enter  $\lambda$  and  $\delta$ . Note that the Gumbel distribution is defined for any real value of  $x$ , so negative flaw sizes can occur when this distribution is chosen. However, since the flaw size distributions are truncated and

renormalized at the initiation size, negative values are unlikely to be returned. The user must verify that the truncated and renormalized distribution matches the actual distribution.

### *Lognormal Distribution*

The density function for the lognormal distribution is:

$$f(x) = \begin{cases} \frac{1}{x\sqrt{2\pi\sigma^2}} \exp\left(-\frac{(\ln x - \mu)^2}{2\sigma^2}\right) & x > 0, \\ 0 & \text{otherwise} \end{cases} \quad (4)$$

where  $\mu$  can be any real number and  $\sigma$  must be a positive real number. Note that  $\mu$  and  $\sigma$  are, respectively, the mean and standard deviation of  $\log(x)$ , so the mean and variance of the lognormal distribution are  $\exp(\mu + \sigma^2/2)$  and  $\exp(2\mu + \sigma^2)[\exp(\sigma^2) - 1]$ , respectively.

If the lognormal distribution is selected, the user will be required to input  $\mu$  and  $\sigma^2$ . Since the lognormal distribution is defined for any positive value of  $x$ , it can be used for any flaw size parameter.

### *Weibull Distribution*

The density function for the Weibull distribution is:

$$f(x) = \begin{cases} b\theta^{-b}x^{b-1}e^{-\left(\frac{x}{\theta}\right)^b} & x > 0, \\ 0 & \text{otherwise} \end{cases} \quad (5)$$

where  $b$  and  $\theta$  are both positive real numbers. The mean of the Weibull distribution is  $(\theta/b)\Gamma(1/b)$  and the mode of the Weibull distribution is

$$\begin{cases} \theta\left(\frac{b-1}{b}\right)^{1/b} & \text{if } b \geq 1, \\ 0 & \text{if } b < 1 \end{cases} \quad (6)$$

If the Weibull distribution is selected, the user will be required to input the values of  $b$  and  $\theta$ . Since the Weibull distribution is defined for any positive value of  $x$ , it can be used for any flaw size parameter.

### **2.1.3 Flaw Size Dimensions**

The modeling of flaw size in CANTIA is generally one dimensional, which is called the primary dimension. The primary dimension can be either percent throughwall depth, fractional depth, or axial length. Some of the failure models in CANTIA (e.g., Bruce 2 circumferential cracking model) requires a secondary dimension, which in the case of a circumferential crack would be circular arc length.

#### 2.1.4 Number of Flaws and Number of Tubes in Inspection Sample

For measured flaw sizes, the user must enter the number of tubes in the inspection sample and the number of flaws found. As noted previously, the program then calculates the actual number of flaws in the susceptible population by dividing the number of flaws found in the inspection by the POD(x) and the fraction of susceptible tubes inspected and renormalizing. CANTIA assumes that there is only one flaw present per tube. If the flaw size distribution is assumed rather than from an inspection, the assumed initial number of tubes with flaws is either a fixed number or chosen from a negative binomial distribution. The negative binomial distribution is chosen as representative of populations where failure is not random, i.e., that certain groups in the population are more prone to failure.

Use of a negative binomial distribution allows the initial number of tubes with flaws to vary during each trial. A negative binomial distribution with parameters N and P assumes that the probability of observing k flaws in a steam generator is

$$p(k) = \binom{N+k-1}{N-1} \left(\frac{P}{P+1}\right)^k \left(1 - \frac{P}{P+1}\right)^N \quad (7)$$

and the mean number of observed flaws is NP. If the negative binomial distribution is selected for the initial number of tubes in the susceptible population with flaws, N must be input as a positive integer and P must input as a positive real number.

Because CANTIA attempts to calculate the actual number of flaws by dividing the number of detected flaws by the POD and the fraction of susceptible tubes, the calculation can sometimes result in an "actual" number of flaws greater than the number of tubes in the susceptible population. In such cases CANTIA will assume that all of the tubes contain a flaw and the number of susceptible tubes is unchanged. Although this may suggest an unrealistic POD model or unrealistic inspection sample size, no explicit warning is given. To ensure that such a situation does not occur, it is best to require a printout of distribution of actual defect size at the starting time and to verify that all of the tubes in the susceptible population do not contain a flaw at the starting time.

#### 2.1.5 Eddy Current Inspection Parameters

CANTIA accepts parameters that describe the POD and measurement error of the EC inspection techniques.

Probability of Detection There are three choices for POD distribution in CANTIA: deterministic, log-logistic, and cumulative lognormal. The deterministic POD is a fixed value of POD for all flaw depths. The log-logistic distribution is of the following form:

$$\text{POD}(x) = \frac{\exp\{\alpha + \beta \ln(x)\}}{1 + \exp\{\alpha + \beta \ln(x)\}} \quad x > 0 \quad (8)$$

The cumulative lognormal probability function is of the form:

$$POD(x) = \frac{1}{2} \left[ 1 + \operatorname{erf} \left( \frac{\ln(x) - \mu}{\sqrt{2}\sigma} \right) \right] \quad (9)$$

where  $\mu$  and  $\sigma$  are the mean and standard deviation of  $\ln(x)$ . The probability of detection (POD) curves developed from the results of the round robin tests on the ANL mockup facility have been described in terms of the linear logistic function:

$$POD = \frac{1}{1 + e^{a+bx}} \quad (10)$$

The log logistic function has a behavior quite different from the linear logistic function, but the lognormal function can provide a good approximation to the linear logistic curves with an appropriate choice of the parameters  $\mu$  and  $\sigma$ . The POD curves for the tube support plate (TSP) inner and outer diameter (ID and OD) cracks, free span (FS) outer diameter cracks, and tube sheet inner diameter cracks are summarized in Table 1. Both maximum likelihood and 95th percentile one sided limits (95 OSL) are given. The root mean square errors between the linear logistic fits and the lognormal approximations range from 1.5–4.1%. Typical comparisons of the logistic and lognormal representations of POD curves are shown in Fig. 1. Because the lognormal must vanish at 0 for all values of  $\ln\mu$  and  $\ln\sigma$ , it cannot describe false call rates. However, in the steam generator case, these are typically fairly small, and the lognormal curves give reasonable representations of the POD curves.

Table 1 Linear logistic and lognormal fits to maximum likelihood POD and 95% confidence limit POD curves. RMS errors in the lognormal fits are 1.5–4.1%.

	Logistic POD		95 OSL		Lognormal POD			95 OSL		
	a	B	a	b	$\mu$	$\sigma$	RMS	$\mu$	$\sigma$	RMS
TSP ID	3.96	-20.34	4.56	-20.22	-1.67	0.41	2.2	-1.52	0.36	1.6
TSP OD	3.78	-8.83	3.91	-8.16	-0.89	0.43	3.4	-0.78	0.42	3.4
FS OD	5.97	-17.17	6.74	-14.15	-1.07	0.28	1.7	-0.76	0.25	1.5
TS Axial & Circ ID	2.98	-8.69	3.58	-7.66	-1.13	0.53	4.1	-0.81	0.46	3.4

Measurement Error Model EC measurement errors can be described in CANTIA by one of three models: deterministic, linear with normal error, and normal. The deterministic model assumes that the error in the measured size is constant for all flaws. For example, if the error is -10% TW, all flaws will be sized by the EC technique as 10% smaller than their actual size. The second choice for measurement error is linear with normal error. This model assumes that the measured flaw size is a linear function of the actual flaw size with a normally distributed error or that both systematic and random errors are present in the measured flaw size distribution. The model uses the following form:

$$\text{Size}_{\text{measured}} = a (\text{Size}_{\text{actual}}) + b + \text{error} \quad (11)$$

where a and b are constants, and the error is a normal distribution with zero mean and given variance.

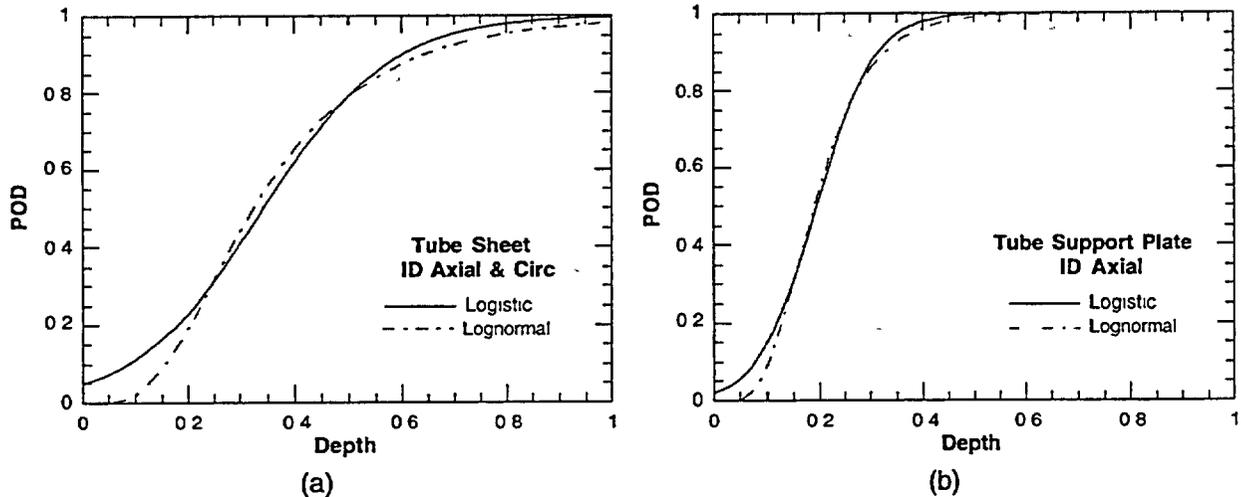


Figure 1. Comparison of the logistic and lognormal descriptions of maximum likelihood POD curves for (a) tube sheet ID axial and circumferential cracking and (b) tube support plate ID axial cracking.

The third choice for the EC measurement error model assumes that the error  $\epsilon$  in the measured flaw size is normally distributed:

$$\epsilon(x) = \frac{1}{\sqrt{2\pi\sigma^2}} \exp\left\{-\frac{(x-\mu)^2}{2\sigma^2}\right\} \text{ for all real } x, \quad (12)$$

where  $\mu$  is the mean error and can be any real number and  $\sigma^2$  is the variance and is a positive real number.

For an inspection, the program will calculate a measurement error for each measured flaw and will add this error to the actual flaw size to determine the measured flaw size. When any of these measurement models is used, some "detected" flaws may be calculated to have negative measured sizes, depending on the parameters entered (e.g., large standard deviation). If this occurs, CANTIA considers that the flaws were, in fact, not detected during the inspection, in effect slightly reducing the POD for the flaws.

### 2.1.6 Flaw Growth Distribution

All of the flaw growth models in CANTIA are one-dimensional (e.g., in the depth direction). Seven models for flaw growth calculations are available in CANTIA: deterministic, exponential, fracture mechanics, gamma, linear, normal, and quadratic. Four of these models, deterministic, exponential, gamma and normal, assume that the flaw growth rate is either independent of flaw size or a fixed percentage of the flaw size. If the growth rate is independent of the size, the program calculates the flaw sizes at future times as follows:

$$\text{Size}(t) = \text{Initial size} + (t - t_{\text{initial}}) \times \text{Growth rate} \quad (13)$$

On the other hand, if the growth rate is a percentage of the flaw size, the program calculates future flaw sizes as follows:

$$\text{Size}(t) = \text{Initial size} \left( 1 + \frac{\text{Growth Rate}}{100} \right)^{(t-t_{\text{initial}})} \quad (14)$$

Two of the distributions used to describe flaw growth, the gamma and normal distributions, have been discussed previously [Eqs. (2) and (12)] The other two are described below:

Deterministic Model. This model assumes that the all flaws grow exactly at the same rate.

Exponential Distribution. The growth rate distribution is :

$$f(x) = \begin{cases} \frac{1}{\mu} \exp \frac{-x}{\mu} & \text{if } x > 0 \\ 0 & \text{otherwise} \end{cases} \quad (15)$$

where  $\mu$ , the mean of the distribution, is a positive real number.

The remaining three models assume the flaw growth rate is a function of the crack size:

Linear Model. The linear model for the crack growth rate is:

$$\frac{d(\text{size})}{dt} = a(\text{size}) + b, \quad (16)$$

where a and b are constants, which are assumed to be normally distributed with a specified mean and variance.

Quadratic Model. The quadratic model is:

$$\frac{d(\text{size})}{dt} = a(\text{size})^2 + b(\text{size}) + d, \quad (17)$$

where a, b, and d are assumed to be normally distributed.

Fracture Mechanics Model. The fracture mechanics model is:

$$\frac{d(\text{size})}{dt} = AK^n, \quad (18)$$

where the stress intensity  $K = BS\sqrt{\text{size}}$ , A, B, and n are deterministic constants, and S is the nominal stress in the tube wall. The stress S is assumed to be normally distributed with a mean and variance.

If a growth rate model predicts a negative growth rate, CANTIA assumes that the flaw size is not changed.

### 2.1.7 Flaw Initiation Distribution

The flaw initiation model describes the rate over time at which new flaws initiate in the susceptible tube population. This rate is typically determined by analyzing the results of multiple inspections of the susceptible population. There are three options: no flaw initiation, lognormal distribution, and Weibull distribution. If the first option is chosen, the program will not allow any new flaws to initiate on tubes that are initially undamaged. If either the lognormal or Weibull distribution is chosen, the program will use the selected distribution to randomly select appropriate initiation times for flaws on those tubes that are undamaged at the starting time. Both lognormal and Weibull distributions have been discussed previously.

CANTIA initiates new flaws at a size defined by the user. This is the same size as is used to truncate the initial flaw size distribution.

### 2.1.8 Tube Failure Models

Seven failure models are available: a circumferential cracking maximum moment model, a tube burst due to fretting model, a critical flaw size model, the French tube burst due to axial primary water stress corrosion cracking (PWSCC) model, the Ontario Hydro tube burst due to axial cracking model, a tube burst due to pitting model, and the Slovene plastic collapse due to axial PWSCC model.

Because some of the models are plant-specific, their details will not be discussed here. Some of the more general failure models are as follows:

French Axial PWSCC Tube Burst Model. This model can be selected for unstable burst of isolated throughwall axial cracks away from the tubesheet and tube support plates (TSPs). The burst pressure is

$$P_{\text{burst}} = \frac{\bar{\sigma}t}{mR_i}, \quad (19)$$

where  $\bar{\sigma}$  is the circumferential flow stress at temperature calculated as 0.58 times the sum of yield and ultimate strengths at temperature,  $t$  is the wall thickness,  $R_i$  is the inner radius, and  $m$  is the bulging factor given by

$$m = \sqrt{1 + \frac{1.61c^2}{R_m t}}, \quad (20)$$

where  $R_m$  is the mean radius and  $c$  is the half crack length.

Slovene Axial PWSCC Plastic Collapse Model This model was developed to determine the critical length of an axial throughwall PWSCC flaw. The critical length is the length at which the crack fails by unstable crack propagation due to net section collapse. The critical crack length, assuming an elastic Poisson's ratio of 0.3, is given by

$$a_c = \left[ -0.709 + 1.155m - 7.056 \exp(-2.966m) \right] \sqrt{R_m t}, \quad (21)$$

where

$$m = \frac{\bar{\sigma}}{\sigma_m} = \frac{K(\sigma_y + \sigma_u)\delta}{P\left(\frac{R_m}{t} - 0.5\right)},$$

K is the flow stress factor, P is the pressure differential,  $\sigma_y$  and  $\sigma_u$  are the yield and ultimate strengths, respectively, and  $\delta$  is a flow stress temperature correction factor.

There is an additional equation to calculate the reinforcement effects of the tubesheet. This reinforcing factor, a correction factor for the flow stress factor K, is restricted to single cracks propagating from the tubesheet, and may not apply to multiple cracks or circumferential cracks. The reinforcement factor RF is given by

$$RF(a_c) = 1 + 10 \exp\left(-1.8 \frac{a_c}{\sqrt{R_m t}}\right). \quad (22)$$

The program first calculates a critical half-crack length and RF for each tube based on the pressure differential during accident conditions. It then recalculates the critical half-crack length using the above two formulas for  $a_c$  and m, after multiplying K by RF, and compares the length of an in-service flaw with the reinforced critical crack length to determine if the tube has failed or not.

### 2.1.9 Leak Rate Model

Three leak rate models were available in the original version of CANTIA: a Bruce 2 circumferential-cracking leak rate model, a model considering any "failed" tube to leak at a given rate, and a French lower-bound leak rate model for axial PWSCC. They have been retained in the present version. Because the Bruce 2 model is plant-specific, it will not be discussed here.

Fixed Leak Rate Model. This model assumes that all "failed" flaws (or flaws that are 100% TW leak at the same rate (entered by the user) under either normal or accident condition.

French Lower Bound Estimate. The French equations for lower-bound leak rate are as follows:

$$Q = 0.3A \sqrt{\frac{2\Delta p}{\rho}}, \quad (23)$$

where

$$A = \alpha(\lambda) \left(\frac{32}{3}\right) \left(\frac{K_I}{E\sqrt{2\pi}}\right) \left[(c + r_y)^{1.5} - r_y^{1.5}\right], \quad (24a)$$

$$\alpha(\lambda) = 1 + 0.1\lambda + 0.16\lambda^2, \quad (24b)$$

$$\lambda = [12(1 - \nu^2)]^{0.25} \left( \frac{c}{\sqrt{R_m t}} \right), \quad (24c)$$

$$K_I = \sigma \sqrt{\pi c}, \quad (24d)$$

$$\sigma = \frac{\Delta P R_I}{t}, \quad (24e)$$

$$\tau_y = \frac{1}{2\pi} \left( \frac{K_I}{\bar{\sigma}} \right)^2, \quad (24f)$$

$$\bar{\sigma} = 0.58(\sigma_y + \sigma_u) \quad (24g)$$

$\Delta P$  is the pressure differential,  $\rho$  is the density of the fluid,  $\nu$  is Poisson's ratio, and  $E$  is Young's modulus. The other variables were defined previously.

#### 2.1.10 Maximum Allowable Leak Rate

The program allows the user to enter a maximum allowable leak rate under normal operating conditions. If the total leak rate for all flaws exceeds this maximum limit, the program will simulate an in-service inspection at the time the leakage limit is exceeded even if a regular inspection is not planned at that time.

#### 2.1.11 Material and Tube Dimensional Properties

CANTIA allows the user to enter the mean and standard deviation of all mechanical properties and tube dimensional properties, which are assumed to be normally distributed. If a value should be fixed (e.g., tube thickness is fixed), standard deviation for that property should be entered as zero.

#### 2.1.12 Future Inspection Plans

The following entries for future inspection plans are available:

**Planned Sample Size.** The user must enter the fraction of tubes to be inspected at any future inspections, whether scheduled or unplanned (e.g., due to high leak rate). The user also has the option to inspect previously detected indications during each inspection; these will be in addition to the initial samples of tubes inspected. For example, if the initial fraction of 100 tubes to be inspected is 0.2, and flaws were detected in 30 tubes during previous outages,  $30 + 0.2 \times 100 = 50$  tubes will be inspected during the outage prior to expansion of the sample size.

**Plugging Limit.** The user must enter the plugging limit for future inspections. All flaws found during inspection and sized equal to or larger than the plugging limit will be plugged during future inspections.

Sample Expansion Rule. Six expansion rules are available: two local expansion rules based on detection of a single defect larger or smaller than a given size, two global expansion rules based on detecting a fraction of flaws larger or smaller than a given size, a global expansion rule based on detecting a given number of repairable flaws, and a maximum number of expansions after which all tubes must be inspected. CANTIA cannot treat local clustering within the susceptible tubes, because tubes are assumed to be statistically independent.

When the program first simulates an inspection, after inspecting an initial sample of tubes and all tubes with previously detected flaws (if desired), it will check whether any of the expansion rules apply. It will then determine the number of additional tubes to be inspected and inspect them. The results of additional inspections will then be checked against the selected expansion rules, and additional inspections will occur as long as any of the selected expansion rules apply, until 100% of inservice tubes are inspected, or until the maximum number of expansions (entered by user) are performed.

### 3 Features Added to CANTIA (ANL/CANTIA)

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All of the input data structure, failure and leak rate models, and in-service inspection options available in the original CANTIA are retained in ANL/CANTIA. The basic Monte Carlo simulation algorithm was also maintained without any modification. Features that were added to CANTIA are discussed in the following sections.

#### 3.1 Initial Flaw Size Distributions

A major feature added in ANL/CANTIA is the ability to treat the growth of two-dimensional cracks, i.e., cracks are allowed to grow (by stress corrosion) both in length as well and depth. Thus, the input in ANL/CANTIA requires an initial flaw depth distribution as well as an initial flaw length distribution. Currently, the depth is taken as the primary dimension, whereas the initial length distribution is entered in terms of a distribution in the aspect ratio (length/depth). The distribution for the aspect ratio can be any of the five statistical distributions: beta, gamma, Gumbel, lognormal, and Weibull. Alternatively, a fixed deterministic ratio can be chosen.

#### 3.2 Flaw Growth Model

The basic flaw considered in the original CANTIA is a one-dimensional flaw, e.g., an infinitely long shallow part-throughwall crack with a stress intensity factor  $K$  given by  $K = BS\sqrt{\text{size}}$ , where the user must specify constants  $B$  and  $S$ . In the ANL/CANTIA, we consider an initially elliptical two-dimensional surface flaw of length  $2c$  and depth  $a$ . ANL/CANTIA then computes, by numerical integration (4<sup>th</sup> order Runge-Kutta), the growth (by stress corrosion) of the crack both through the wall and in length, up to the point where it becomes a throughwall crack. CANTIA then follows the growth (by stress corrosion) of the throughwall crack until unstable rupture.

##### 3.2.1 Stress Intensity Factor for Part-Throughwall Cracks

The stress intensity factors for a part-throughwall axial or circumferential crack at its deepest point and at the surface are the solutions given by Newman and Raju<sup>3</sup> for a flat plate of width =  $2w$  and thickness =  $t$ . For axial cracks, the solutions should be reasonable for shallow cracks for which bulging effects are small. For circumferential cracks, the solution should be reasonable for cases either when the tubes are constrained against bending or the cracks are short so that effects due to tube bending are negligible. The equations for the stress intensity factor  $K_I$  of a part-throughwall crack in a flat plate are:

$$K_I = (\sigma_m + H\sigma_b) \sqrt{\frac{\pi a}{Q}} F\left(\frac{a}{t}, \frac{a}{c}, \frac{c}{w}, \phi\right) \quad 0 < \frac{a}{c} \leq 1, \quad 0 \leq \frac{a}{t} < 1, \quad \frac{c}{w} < 0.5, \quad \text{and} \quad 0 \leq \phi < 90, \quad (25)$$

where  $\sigma_m$  and  $\sigma_b$  are the membrane and bending stresses, respectively, and  $\phi = 0$  and  $\phi = 90^\circ$  represent the surface crack tip and the crack tip at the deepest point, respectively. For axial cracks and short circumferential cracks in steam generator tubes,  $c/w = 0$  is a good approximation. The rest of the terms are:

$$Q = 1 + 1.464 \left( \frac{a}{c} \right)^{1.65}, \quad (26a)$$

$$F = \left[ M_1 + M_2 \left( \frac{a}{t} \right)^2 + M_3 \left( \frac{a}{t} \right)^4 \right] f_\phi f_w g, \quad (26b)$$

$$M_1 = 1.13 - 0.09 \left( \frac{a}{c} \right), \quad (26c)$$

$$M_2 = -0.54 + \frac{0.89}{0.2 + \frac{a}{c}}, \quad (26d)$$

$$M_3 = 0.5 - \frac{1.0}{0.65 + \frac{a}{c}} + 14 \left( 1.0 - \frac{a}{c} \right)^{24}, \quad (26e)$$

$$f_\phi = \left[ \left( \frac{a}{c} \right)^2 \cos^2 \phi + \sin^2 \phi \right]^{1/4}, \quad (26f)$$

$$f_w = \left( \frac{a}{t} \right)^{1/4}, \quad (26g)$$

$$g = 1 + \left[ 0.1 + 0.3 \left( \frac{a}{t} \right)^2 \right] (1 - \sin \phi)^2, \quad (26h)$$

$$H = H_1 + (H_2 - H_1)(\sin \phi)^p, \quad (26i)$$

$$p = 0.2 + \frac{a}{c} + 0.6 \left( \frac{a}{t} \right), \quad (26j)$$

$$H_1 = 1 - 0.34 \frac{a}{t} - 0.11 \frac{a}{c} \left( \frac{a}{t} \right), \quad (26k)$$

$$H_2 = 1 + G_1 \left( \frac{a}{t} \right) + G_2 \left( \frac{a}{t} \right)^2, \quad (26l)$$

$$G_1 = -1.22 - 0.12 \left( \frac{a}{c} \right), \quad (26m)$$

$$G_2 = 0.55 - 1.05 \left( \frac{a}{c} \right)^{0.75} + 0.47 \left( \frac{a}{c} \right)^{1.5}. \quad (26n)$$

### 3.2.2 Stress Intensity Factor for Throughwall Cracks

For throughwall axial cracks, the stress intensity factor is

$$K_I = m\sigma\sqrt{\pi c} \quad (27)$$

where  $m$  is the bulging factor:<sup>4</sup>

$$m = 0.614 + 0.48\lambda + 0.386 \exp(-1.25\lambda), \quad (28a)$$

and

$$\lambda = [12(1 - \nu^2)]^{\frac{1}{4}} \frac{c}{\sqrt{R_m t}} = \frac{1.82c}{\sqrt{R_m t}}. \quad (28b)$$

In the current version of ANL/CANTIA, the stress intensity factor for a throughwall circumferential crack of angular length  $2\theta$  is given by

$$K_I = \sigma_m F_m \sqrt{\pi R_m \theta}, \quad (29)$$

where

$$\sigma_m = \frac{pR_I}{2t}, \quad (30a)$$

$$F_m = \begin{cases} 1 + 0.1501\gamma^{1.5} & \text{for } \gamma \leq 2 \\ 0.8875 + 0.2625\gamma & \text{for } 2 \leq \gamma \leq 5 \end{cases} \quad (30b)$$

$$\gamma = \theta \sqrt{\frac{R_m}{t}}. \quad (30c)$$

### 3.2.3 Stress Corrosion Crack Growth Rate

In ANL/CANTIA we have provided two models for stress corrosion crack growth rates: one due to Scott<sup>5</sup> and the other due to Ford and Andresen.<sup>6</sup> It is assumed that the same equation can predict crack growth rates in the thickness and the length directions. Scott's model for PWSCC gives the crack growth rate (in  $\mu\text{m}/\text{h}$ ) as a function of stress intensity factor (in  $\text{MPa}\sqrt{\text{m}}$ ):

$$\frac{da}{dt} = 1.008 \times 10^{-2} (K_I - K_{th})^{1.16} \quad (31)$$

where  $K_{th}$  is a threshold stress intensity factor (typically  $\approx 9 \text{ MPa}\sqrt{\text{m}}$ )

Ford and Andresen<sup>6</sup> developed the following equation for crack growth rate (in  $\mu\text{m}/\text{h}$ ) as a function of stress intensity factor (in  $\text{MPa}\sqrt{\text{m}}$ ):

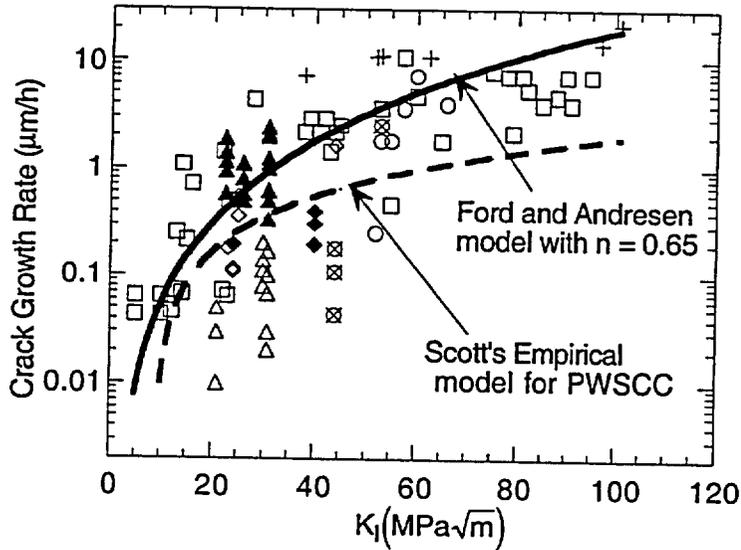


Figure 2. Collected literature data on crack growth rate vs. stress intensity factor for Alloy 600 in simulated primary water together with those predicted by Scott's empirical model for PWSCC and Ford and Andresen model.

$$\frac{da}{dt} = (2.808 \times 10^5 n^{3.6}) (6 \times 10^{-14} K^4)^n \quad (32)$$

where  $n$  is a constant. Although developed for SCC of stainless steels in BWRs, it gives reasonable agreement with the Alloy 600 crack growth rates in PWR environments with  $n=0.65$ .

Figure 2 shows a comparison of available data<sup>7</sup> on PWSCC with the crack growth rates predicted by the models of Scott and Ford-Andresen. In ANL/CANTIA, the user has the option of choosing one of the crack growth rate models provided in the original CANTIA as well as either the Scott or Ford-Andresen models. In all cases, the crack growth rate is assumed to be normally distributed with a mean crack growth rate already incorporated in the program and a variance provided by the user.

### 3.3 Failure Models

In addition to the failure models provided in the original CANTIA, ANL/CANTIA also includes as additional options the ANL ligament rupture model<sup>8</sup> and the unstable-rupture model due to Erdogan.<sup>4</sup>

#### 3.3.1 Axial Crack Failure Models

For throughwall axial cracks the unstable burst pressure for a throughwall axial crack is predicted by Erdogan<sup>4</sup> to be

$$m\sigma = \bar{\sigma} \quad (33)$$

where  $\sigma$  is the nominal hoop stress (calculated using the mean radius and thickness of the tube),  $\bar{\sigma} = \text{flow stress} = k(S_y + S_u)$  (with  $k = 0.5 - 0.6$ ), and  $m$  as defined by Eq. (28a).

For part-throughwall cracks the ANL ligament rupture model was developed from statistical analyses of the tests conducted at Pacific Northwest National Laboratory (PNNL)<sup>9</sup>

and analysis of severe accident tests conducted at ANL<sup>10</sup> on flawed steam generator tubes. The ANL ligament rupture model predicts ligament rupture to occur when

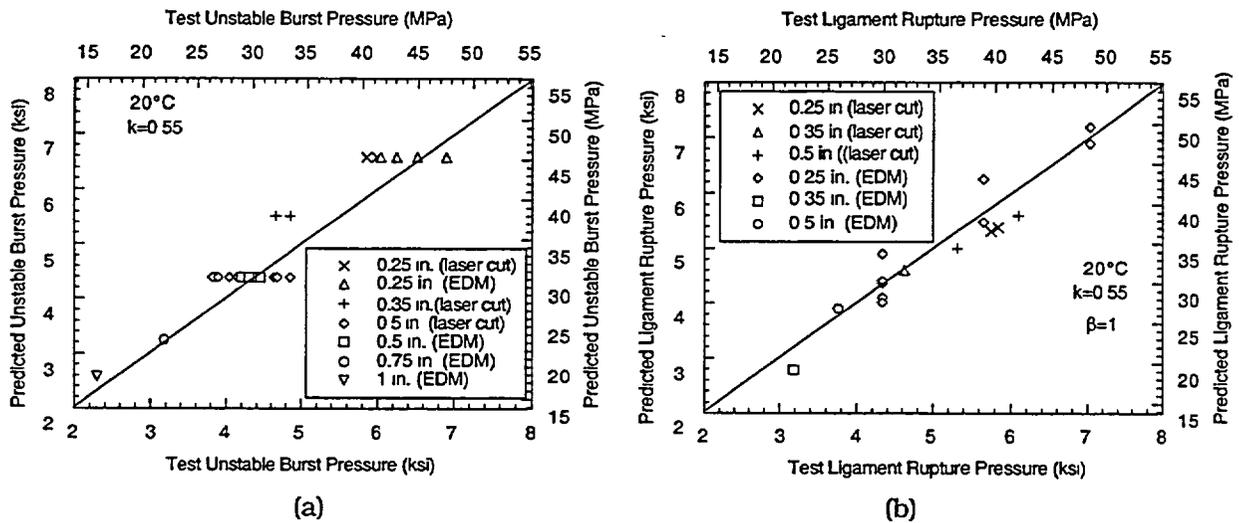


Figure 3. Predicted vs observed (a) unstable burst pressures and (b) ligament rupture pressures of Alloy 600 tubes with machined notches.

$$m_p \sigma = \bar{\sigma}, \quad (34)$$

where the stress magnification factor  $m_p$  is given by

$$m_p = \frac{1 - \alpha \frac{a}{mt}}{1 - \frac{a}{t}}, \quad (35a)$$

$$\alpha = 1 + \beta \left( \frac{a}{t} \right)^2 \left( 1 - \frac{1}{m} \right), \quad \beta \approx 1, \quad (35b)$$

$$\sigma = \Delta p \frac{R_m}{t} \quad (35c)$$

The above failure models for both throughwall and part-throughwall axial cracks have also been validated with many tests on electrodischarge machined (EDM) and laser-cut notches conducted at ANL (Figs. 3a and b). An "equivalent rectangular crack" method has been developed to predict failure pressures of stress corrosion cracks that are nonplanar and irregular in shape.<sup>8</sup>

### 3.3.2 Circumferential Crack Failure Models

For throughwall cracks of angular length  $2\theta$  the unstable burst pressure is based on a net section plastic collapse approach (assuming the tube to be constrained against bending)

$$\sigma_m = \frac{\Delta p R_m}{2t} = \left(1 - \frac{\theta}{\pi}\right) \bar{\sigma} \quad (36)$$

For a part-throughwall crack the ligament rupture pressure was obtained by modifying Kurihara's results for piping<sup>11</sup> and is given by

$$\sigma_m = \frac{\Delta p R_m}{2t} = \frac{\bar{\sigma}}{m_p}, \quad (37)$$

where

$$m_p = \frac{1}{\left[ m + \left( \frac{\theta}{\pi} \right) \left( 1 - \frac{a}{t} - m \right) \right]}, \quad (38a)$$

$$m = \frac{1 - \frac{a}{t}}{1 - \frac{a}{Nt}}, \quad (38b)$$

$$N = 1 + \lambda \left( \frac{\theta}{\pi} \right)^\gamma. \quad (38c)$$

Analysis of Kurihara's data showed that  $\lambda = 0.2$  and  $\gamma = 0.2$  fitted his data to the ANL equation fairly well.<sup>8</sup>

### 3.4 Leak Rate Models

In addition to the leak rate models available in the original CANTIA, ANL/CANTIA provides a leak rate model based on simple orifice flow through a crack with an opening area  $A$  with a coefficient of discharge  $C_d = 0.6$ .

$$Q = 0.6A \sqrt{\frac{2\Delta p}{\rho}}, \quad (39)$$

where  $A$  is the crack opening area,  $\Delta p$  is the pressure differential, and  $\rho$  is the mass density. This model has been used successfully to predict leak rates in experiments conducted at room temperature and 282°C on specimens with EDM notches and stress corrosion cracks at ANL down to a leak rate of ~ 0.1 gal/min. The correlation will break down at lower levels of leak rates for very tight stress corrosion cracks, particularly at elevated temperatures where flashing may occur inside the cracks; but such a limit has not yet been established. The crack opening area is calculated from a model developed by Zahoor<sup>12</sup> and validated by finite element analyses and tests at ANL. It is very similar to the French lower bound leak model, but gives higher flow rates, since it assumes the flow is not limited by choking.

### 3.4.1 Crack Opening Area for Axial Cracks

Zahoor's model<sup>12</sup> for the crack opening area  $A$  of an axial throughwall crack of length  $2c$  is:

$$A = 2\pi c_e^2 V_o \sigma / E, \quad (40)$$

where

$$\sigma = \text{hoop stress} = \Delta p R_m / t, \quad (41a)$$

$\Delta p$  = differential pressure across tube wall,

$E$  = Young's modulus,

$R_m$  and  $t$  = mean radius and thickness of tube, respectively,

$$V_o = 1 + 0.64935\lambda_e^2 - 8.9683 \times 10^{-3}\lambda_e^4 + 1.33873 \times 10^{-4}\lambda_e^6, \quad (41b)$$

$$\lambda_e^2 = c_e^2 / R_m t, \quad (41c)$$

$$c_e = c \left[ 1 + \frac{F}{2} \left( \frac{\sigma}{\sigma_y} \right)^2 \right], \quad (41d)$$

$$F = 1 + 1.2987\lambda^2 - 2.6905 \times 10^{-2}\lambda^4 + 5.3549 \times 10^{-4}\lambda^6, \quad (41e)$$

$$\lambda^2 = c^2 / R_m t, \quad (41f)$$

$\sigma_y$  = yield strength.

The above approach for calculating crack opening areas and leak rates has been validated by pressure and leak rate tests conducted at ANL on axial EDM notched specimen at room temperature as well as at 282°C (Figs.4a-b).<sup>8</sup>

### 3.4.2 Crack Opening Area for Circumferential Cracks

For a throughwall circumferential crack of angular length  $2\theta$ , Zahoor's expression<sup>12</sup> for the crack opening area is:

$$A = 2\pi R_m t B \frac{\sigma_m}{E}, \quad (42)$$

where

$$B = \begin{cases} \lambda_e^2 + 0.16\lambda_e^4 & \lambda_e \leq 1 \\ 0.02 + 0.81\lambda_e^2 + 0.3\lambda_e^3 + 0.03\lambda_e^4 & \lambda_e > 1 \end{cases}, \quad (43a)$$

$$\lambda_e = c_e \sqrt{\frac{R_m}{t}} \quad (43b)$$

$$c_e = \theta \left[ 1 + \frac{1}{2} F^2 \left( \frac{\sigma_m}{\sigma_y} \right)^2 \right] \quad (43c)$$

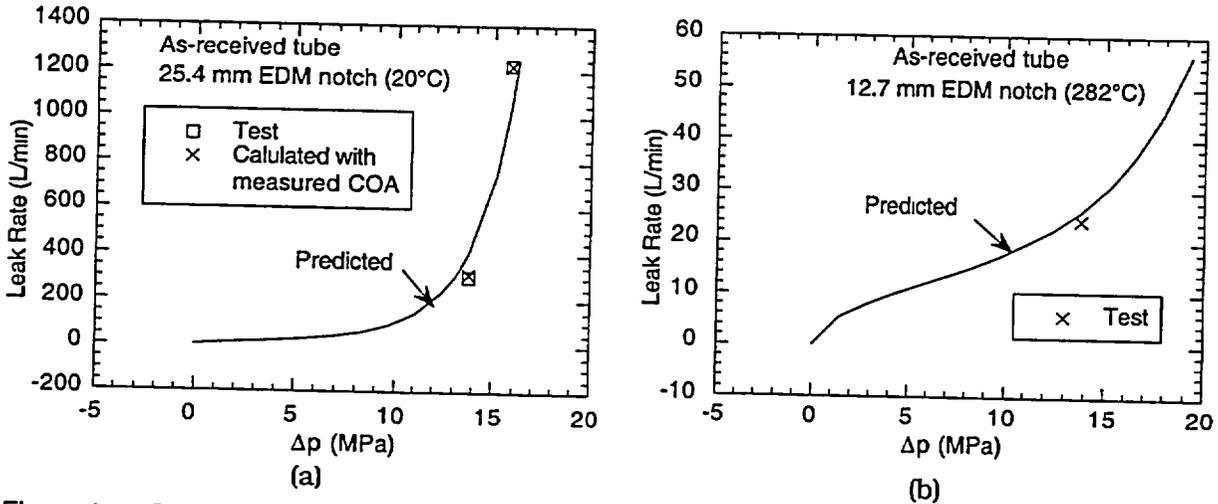


Figure 4. Comparison of calculated (solid line) vs. experimentally measured (symbols) leak rates for as-received 22-mm (7/8 in.)-diameter tubes with (a) 25.4 mm (1 in.) axial EDM notch at 20°C and (b) 12.7 mm (0.5 in.) axial EDM notch at 282°C. Cross symbols (x) in Fig. 4a denote calculated leak rates using posttest measured crack opening areas.

$$F = \begin{cases} 1 + 0.1501\lambda^{1.5} & \lambda \geq 2 \\ 0.8875 + 0.2625\lambda & \lambda < 2 \end{cases} \quad (43d)$$

$$\lambda = \theta \sqrt{\frac{R_m}{t}}, \quad (43e)$$

$$\sigma_m = \Delta p \frac{R_m}{2t}. \quad (43f)$$

### 3.5 Residual stress

In ANL/CANTIA, the peak residual stress value (mean and variance) is entered by the user. Currently, the residual stress is idealized as a membrane stress that is reduced linearly with increasing crack depth until it is zero at 100% crack depth. Unless the initial crack depths are very deep, pressure stresses alone cannot grow the stress corrosion cracks through the tube wall without the assistance of residual stresses. However, the current residual stress model in ANL/CANTIA is highly simplified and should be made more realistic in the future.

## 4 Examples Run with ANL/CANTIA

To verify that the basic algorithms added in ANL/CANTIA are free from error, several deterministic cases were run for a tube with a single crack for which results can be obtained analytically. Although ANL/CANTIA is a probabilistic program, it can be made to simulate a deterministic case by choosing small standard deviations for all parameters, setting  $POD = 1$  with no in-service inspection, and choosing a very narrow distribution of initial crack sizes. For the purpose of this exercise, a tube of 0.875 in. OD and 0.05 in. wall thickness was chosen, and it was assumed that  $\Delta P_{norm} = 1.3$  ksi,  $\Delta P_{MSLB} = 2.5$  ksi,  $T = 288^\circ\text{C}$ , initial crack depth = 0.25 and initial crack length = 0.5 in. (initial aspect ratio = 40). Calculations showed that, for the assumed initial crack size, the pressure-induced stress was insufficient to drive the crack through the thickness because  $K_I < K_{th}$ . To obtain non-trivial results, two values of initial residual stress were assumed: 30 ksi and 40 ksi. Results from a deterministic analysis are plotted in Fig. 5. One thousand simulations were used for the Monte Carlo analyses of the same initial crack. Results from two thousand simulations were essentially the same. Evolution of the distribution of crack depths with time for the two residual stresses are plotted in Figs. 6 and 7. A comparison of Figs. 6 and 7 with Fig. 5 shows that the results are compatible, as expected. This is further confirmed by comparison of the deterministically calculated crack depth with crack depth at peak probability calculated by ANL/CANTIA, as plotted in Figs. 8a and b. Evolutions of the distributions of crack length with time are plotted in Figures 9a and b. Even for the assumed small standard deviations, there is a small but finite probability of significant crack length increase with time. As a result, in the absence of ISI, there is a finite probability of burst, as shown in Fig. 10.

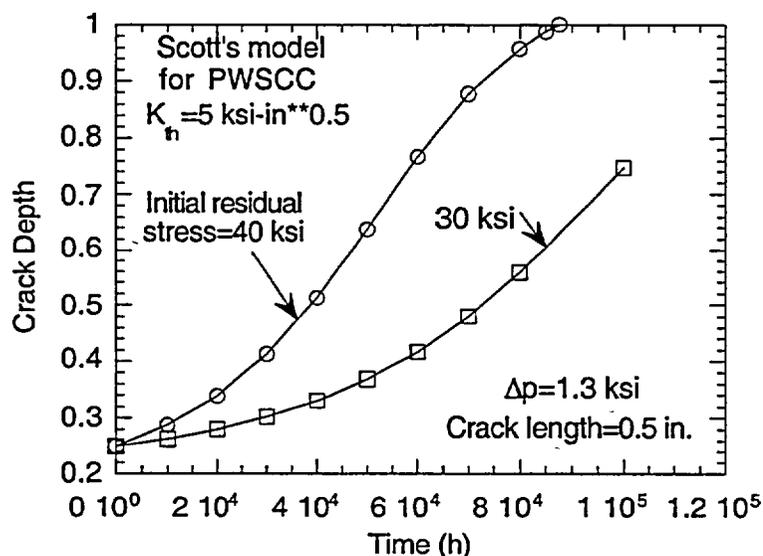


Figure 5. Variation of crack depth with time calculated deterministically for two values of initial residual stress. Initial crack was 0.5 in. long and 25% deep.

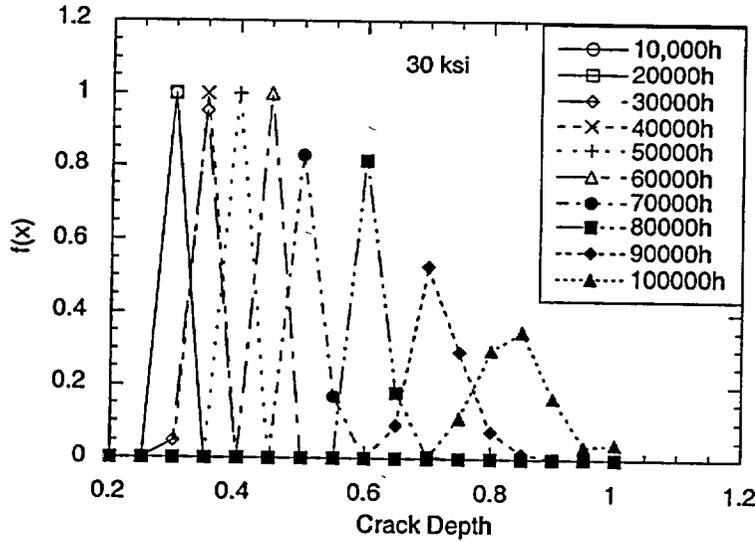


Figure 6:  
Variation of the distribution of crack depth (bin size = 0.05) with time for initial residual stress of 30 ksi.

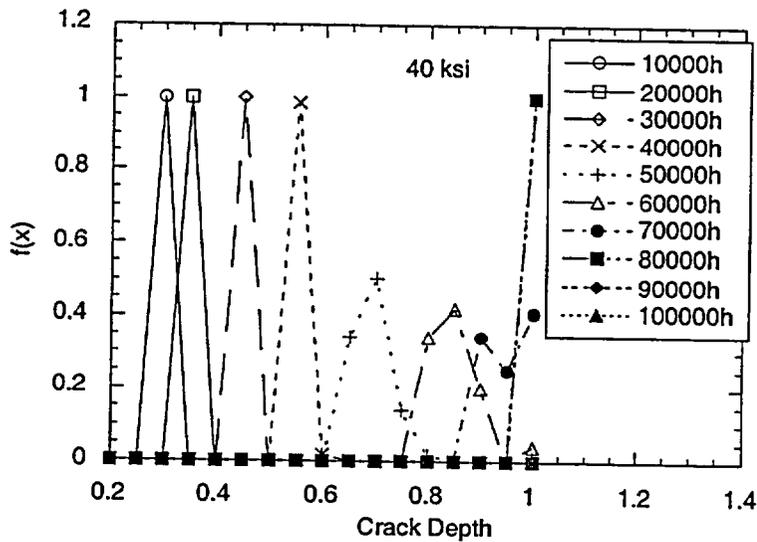


Figure 7.  
Variation of the distribution of crack depth (bin size = 0.05) with time for initial residual stress of 40 ksi.

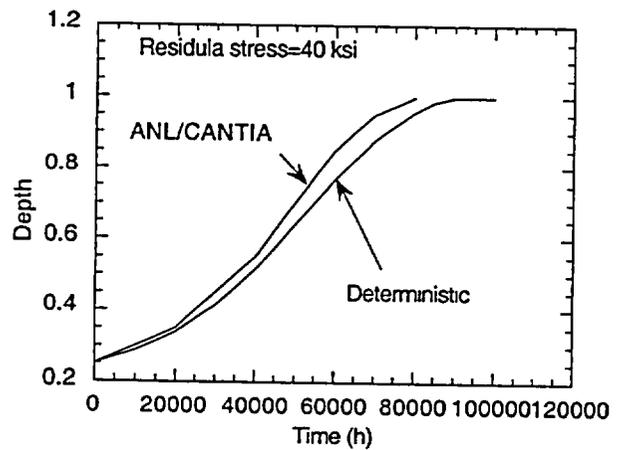
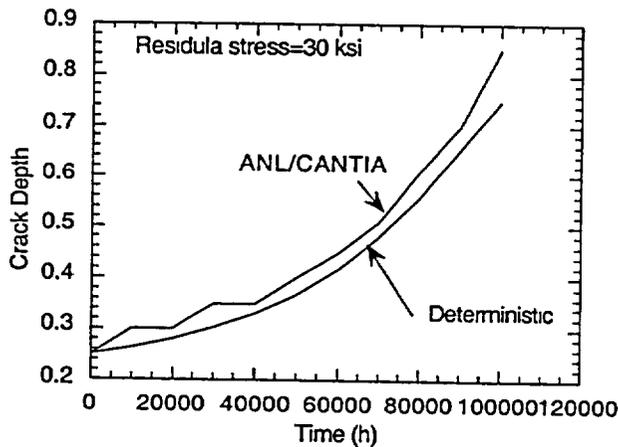


Figure 8. Comparison of deterministically calculated crack depth with the crack depth at peak probability calculated by ANL/CANTIA for initial residual stress of (a) 30 ksi and (b) 40 ksi.

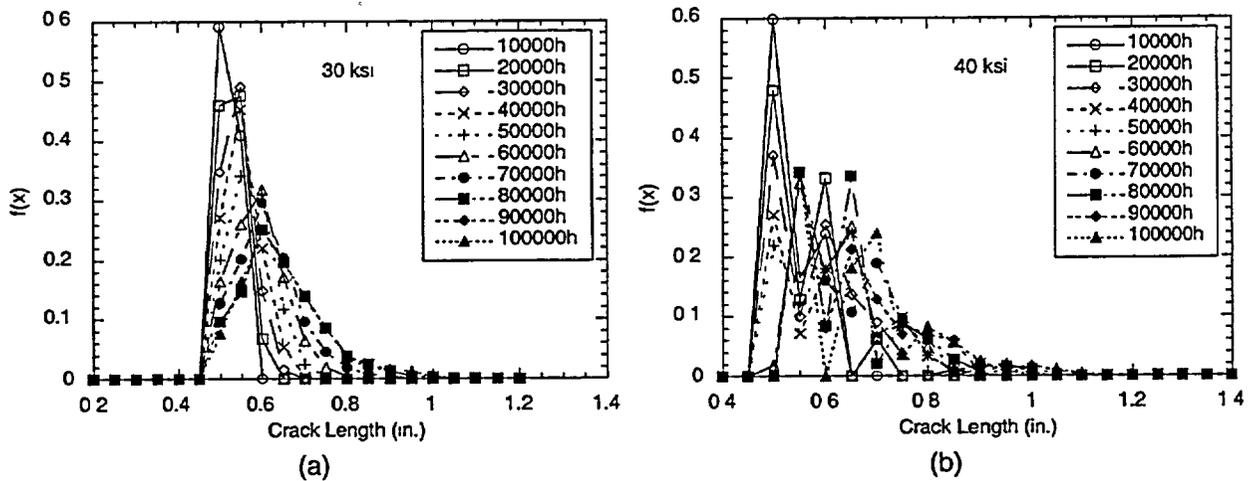


Figure 9. Variation of the distribution of crack length (bin size = 0.05 in.) with time for initial residual stresses of (a) 30 ksi and (b) 40 ksi.

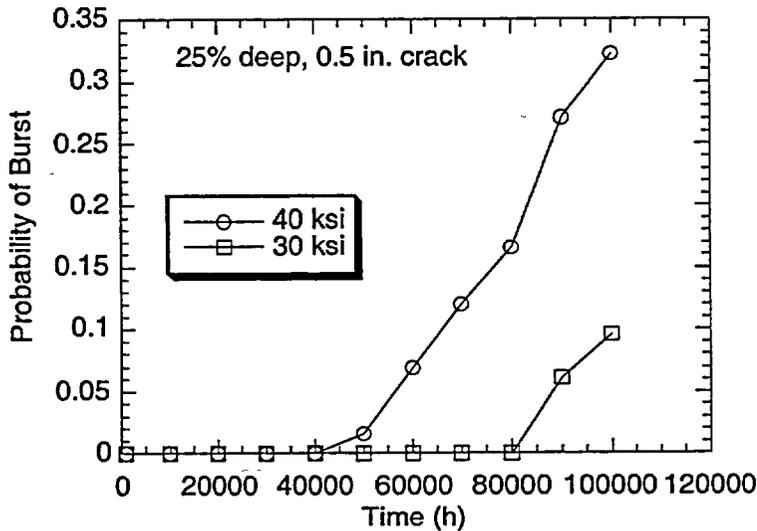


Figure 10. Variation of probability of burst of one or more tubes with time for two values of initial residual stresses. Note that no ISI was assumed.

#### 4.1 Effect of POD

First, we evaluated the effect of fixed POD on the failure probabilities or more precisely the conditional probability of failure under a design basis accident. Evolution of the probability of one or more tube ruptures with time is plotted in Fig. 11 for the case when  $POD = 0.9$ . Variations of distributions of crack depth and crack length with time for the same  $POD$  are plotted in Figs. 12a and 12b, respectively. Similar results are plotted in Fig. 13 and Figs. 14a and b for a  $POD = 0.6$  and in Fig. 15 and Figs. 16a and b for a  $POD$  of 0.01, respectively.

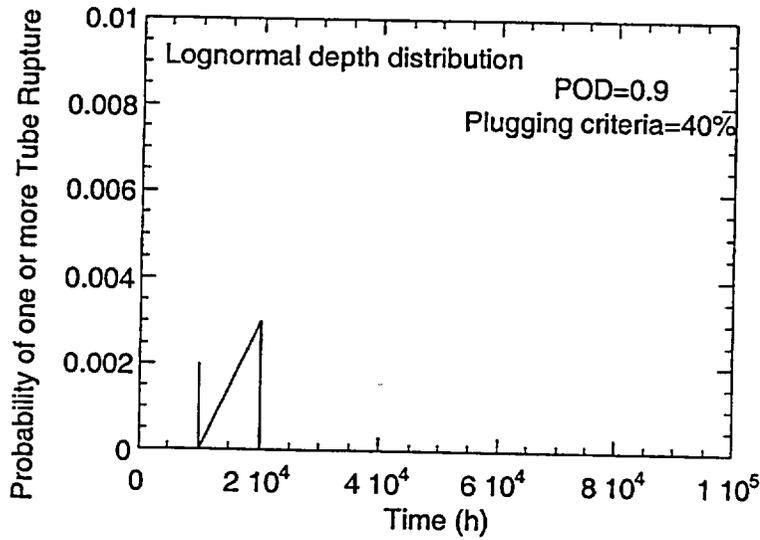


Figure 11.  
Variation of probability of burst of one or more tubes with time for initial residual stress = 30 ksi for a POD = 0.9 and inspection interval of 10,000 h.

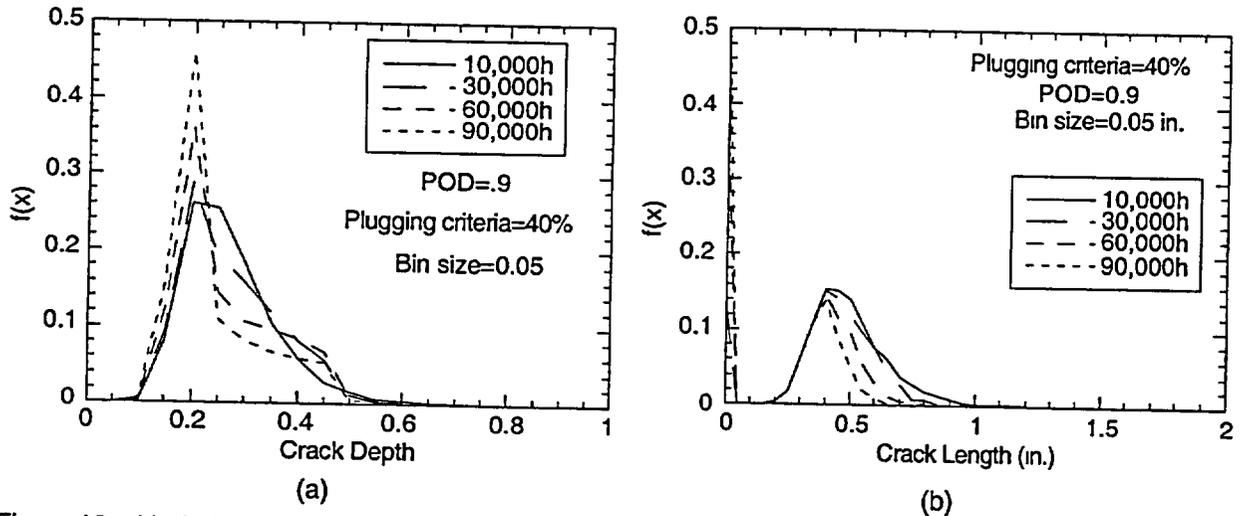


Figure 12. Variation of the distribution of (a) crack depth and (b) crack length with time for initial residual stress of 30 ksi and POD = 0.9.

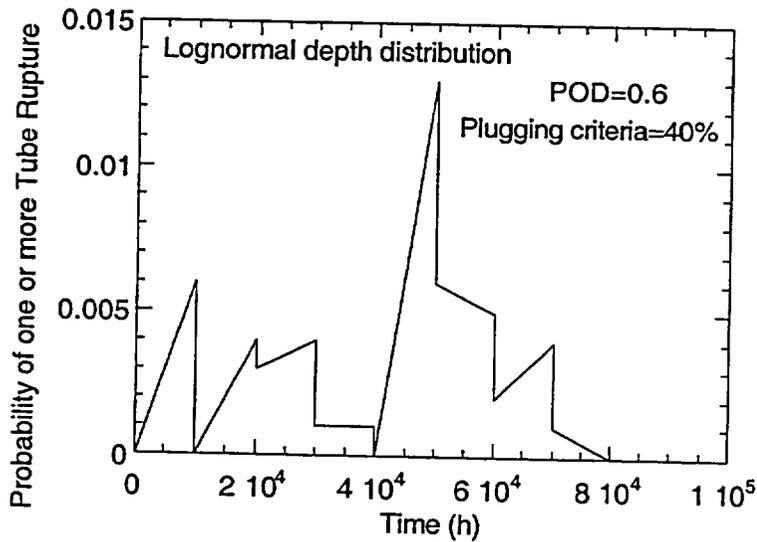


Figure 13.  
Variation of probability of burst of one or more tubes with time for initial residual stress = 30 ksi for a POD = 0.6 and inspection interval of 10,000 h.

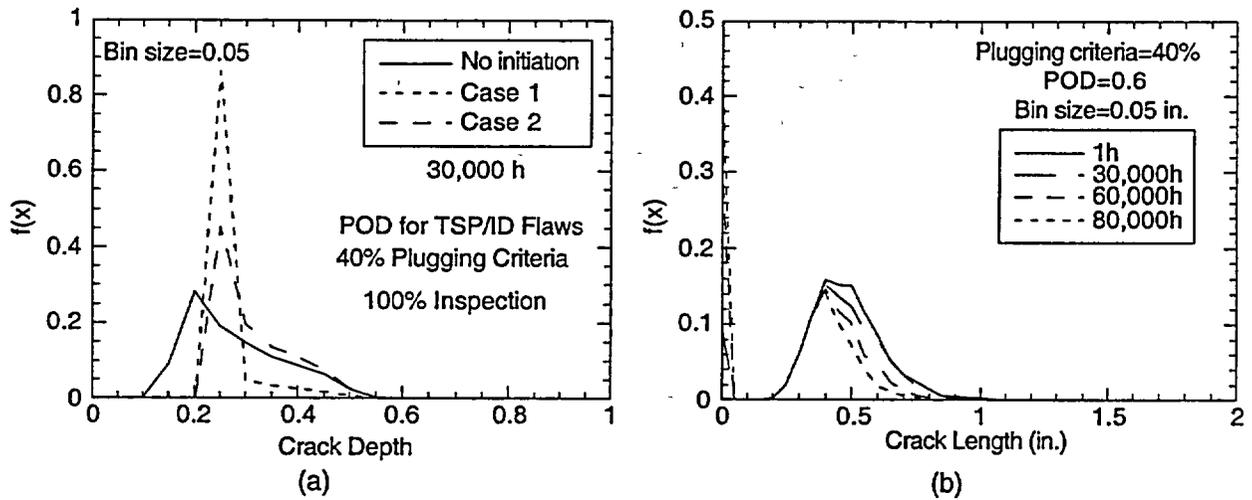


Figure 14. Variation of the distribution of (a) crack depth and (b) crack length with time for initial residual stress of 30 ksi and POD = 0.6.

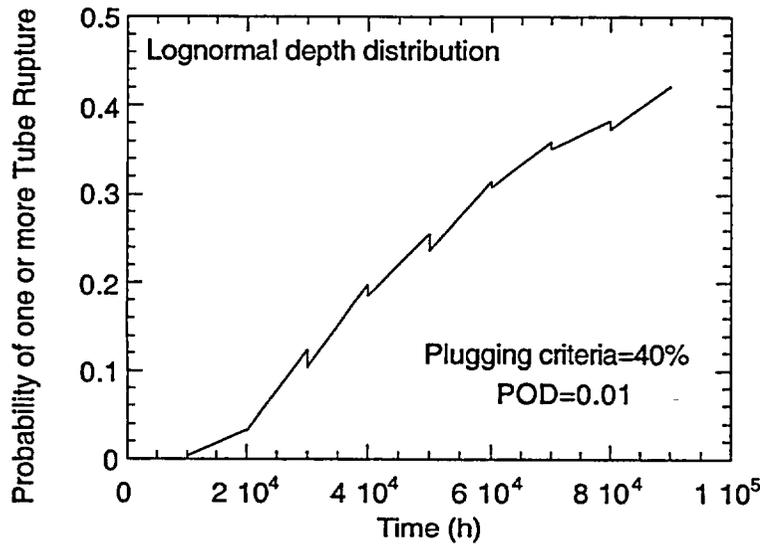


Figure 15. Variation of probability of burst of one or more tubes with time for initial residual stress = 30 ksi for a POD = 0.01 and inspection interval of 10,000 h.

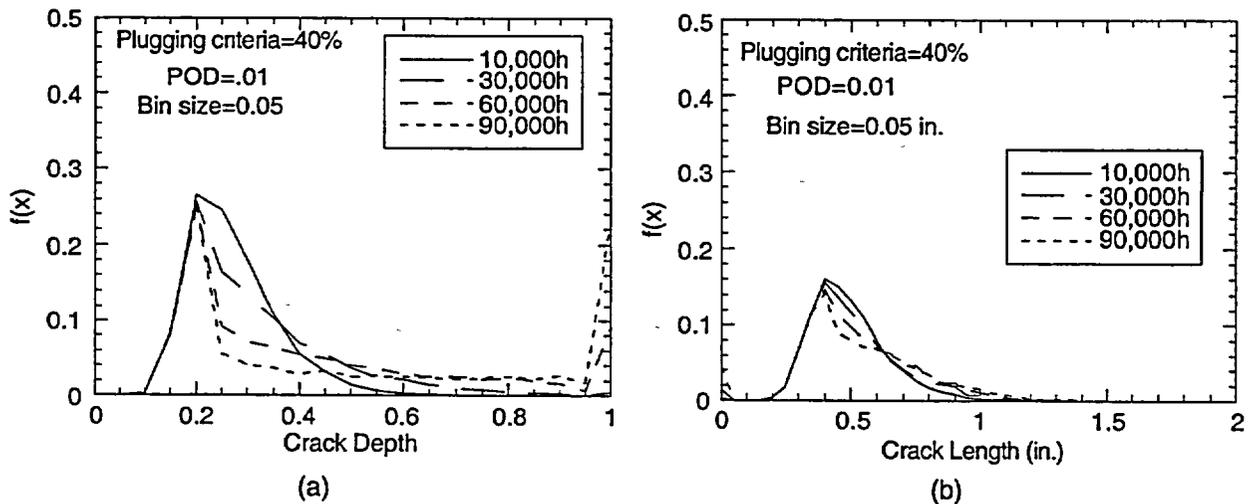


Figure 16. Variation of the distribution of (a) crack depth and (b) crack length with time for initial residual stress of 30 ksi and POD = 0.01.

As expected, the probability of one or more tube rupture increases with decreasing POD. Peaks and valleys in Fig. 13 represent the effect of plugging on the probability of tube rupture. The probability of tube rupture is very small for POD = 0.9. For POD = 0.6, the probability of one or more tube rupture peaks at an intermediate time. In the case of POD = 0.01, the probability of one or more tube rupture increases monotonically with time. The locations of the peak in the probability of crack depth and crack length change very little with time or POD. The spikes in the probability of crack length at zero crack length represent plugged tubes. Similarly, the spike in the probability at a crack depth of 100% in Fig. 16a represent cracks that become throughwall. As expected, the probability for plugging is essentially zero when the POD = 0.01.

Next, we explored the difference between assuming a fixed probability of crack detection (POD = 0.6) and assuming a POD curve determined for TSP/ID flaws in the recent ANL mockup round robin on the probability of one or more tube rupture. Although the ANL round robin POD was best-fitted with a linear logistic curve (not available as an option in the current ANL/CANTIA), a good approximation to the POD curve can also be obtained with a lognormal curve (Fig. 1), which is one of the options in ANL/CANTIA. This lognormal curve for POD was used in the calculations and 100% tube inspection was assumed. A steam generator with 10 susceptible tubes each containing a single crack was considered. A lognormal distribution of initial crack depth was assumed with a fixed initial length to depth aspect ratio of 40 in. No new cracks were assumed to initiate during the lifetime of the steam generator. The Scott model with a conservative threshold stress intensity factor  $K_{th} = 5 \text{ ksi}\sqrt{\text{in}}$  was used to determine crack growth rates. For the purpose of this exercise,  $\Delta P_{norm} = 1.3 \text{ ksi}$ ,  $\Delta P_{MSLB} = 2.5 \text{ ksi}$ ,  $T = 288^\circ\text{C}$ , an in-service-inspection interval of 10,000h with a 40% plugging criterion, and a total life of 80,000 h were assumed. Also, an initial membrane residual stress of 30 ksi was used and the residual stress was assumed to relax linearly with crack depth reducing to zero when crack depth = 100%.

One thousand simulations were used for the Monte Carlo analyses. The variations of distributions of crack depth and crack length with time for the assumed PODs are plotted in Figs. 17a and 17b, respectively. Because of plugging, the depth and length at peak probability decrease slightly with time. Also, plugging causes a spike in the probability distribution of crack length at zero crack length. Evolution of the probability of one or more tube rupture with time is plotted in Fig. 18 for both POD curves. The discontinuous drops in the probability of rupture curve are caused by plugging of tubes. The probability of tube rupture is basically zero ( $< 0.001$ ) beyond two equivalent full power years (EFPY) of operation if the full POD curve is used. On the other hand, if a fixed POD = 0.6 is used, the probability of tube rupture does not reduce to zero until 9 EFPY of operation. Of course, these conclusions are valid only for cases where no new cracks are allowed to initiate during the lifetime of the steam generator.

As expected, the probability of one or more tube ruptures is greater when a fixed POD is used than when the full POD curve is used. The crack depth and length distributions are quite similar for both POD curves, although the probability of plugging (spike at zero crack length in Fig. 17b) is greater when the full POD curve is used.

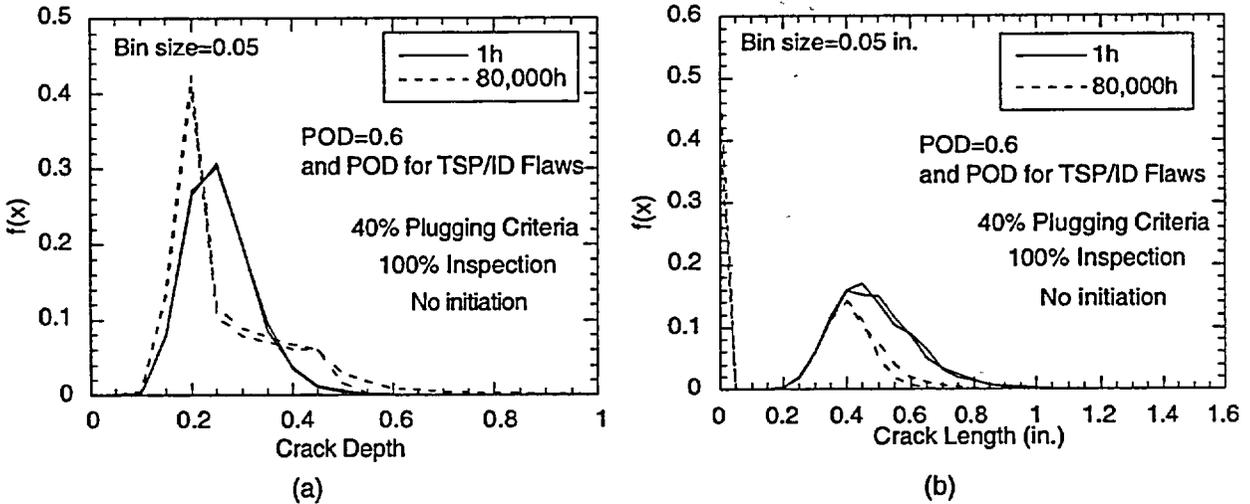


Figure 17. Variation of the distribution of (a) crack depth (bin size = 0.05) and (b) crack length (bin size = 0.05 in.) with time for initial residual stress of 30 ksi and using POD curve for TSP ID flaws (Fig. 1) and a constant POD = 0.6.

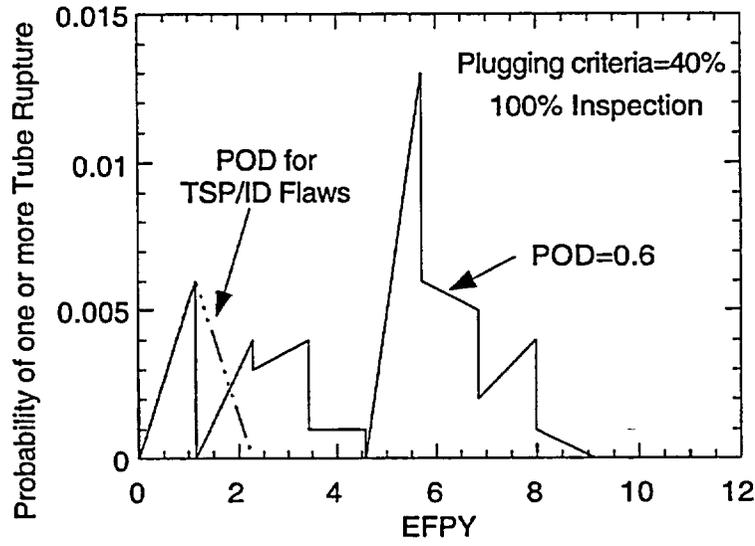


Figure 18. Variation of probability of rupture of one or more tubes with time for a constant POD = 0.6 and a POD curve for TSP/ID flaws and assuming no new flaw initiation.

## 4.2 Effect of Crack Initiation

Until now we have assumed no new crack initiation with time. To explore the effect of crack initiation on failure probabilities, we assumed two cumulative Weibull distributions for crack initiation times (Fig. 19), denoted by Case 1 and Case 2. Case 1 represents a steam generator that has very low crack initiation resistance, while Case 2 represents an steam generator with greater initiation resistance. Each new crack initiated has a deterministic initial depth of 0.2 of the wall thickness and deterministic initial aspect ratio of 40 (i.e., initial length = 0.4 in.). For the purpose of calculation, a steam generator with 50 susceptible tubes was considered and initially 10 tubes were assumed to contain a crack with a lognormal size distribution. The evolution of the distributions for the number of cracks with time for the two cases are plotted in Figs. 20a and b. The evolution of the distributions of crack depth for

various cases are presented in Figs 21a and b and similar presentations for crack length are given in Figs. 22a and b. Note that allowing new cracks to initiate changes the distributions slightly compared to a case without new crack initiation. However, for the POD curve (TSP/ID flaws) and plugging criteria (40%) assumed (with 100% inspection), the distributions are not significantly different for the two cases in which new cracks are allowed to initiate. The probability of one or more tube rupture or for leak rate > 1 gpm under normal operation for all cases have been calculated to be very small (< 0.001).

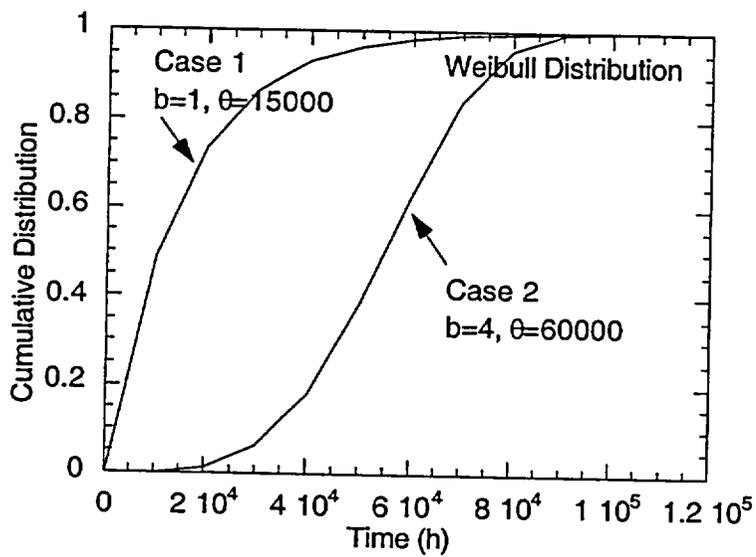


Figure 19. Two cases of cumulative Weibull distributions assumed for crack initiation times.

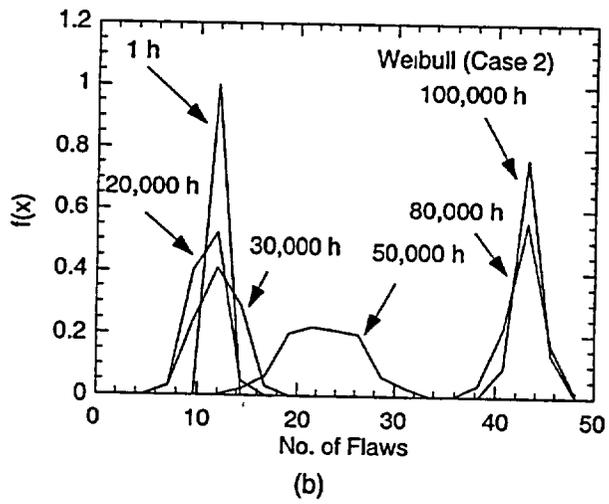
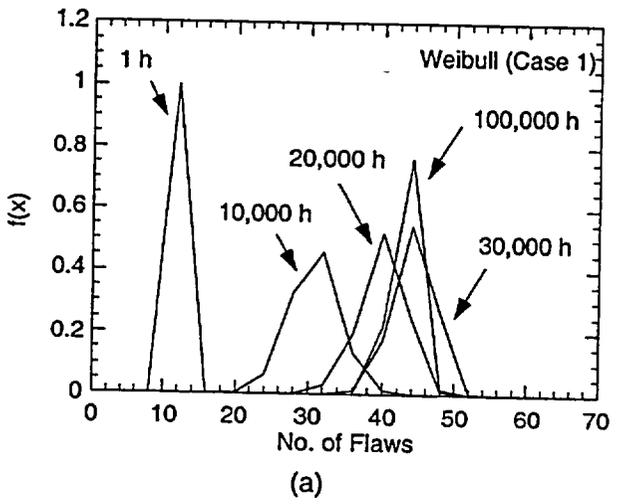


Figure 20. Evolution of the distribution for the number of flaws with time for Weibull initiation (a) case 1 and (b) case 2.

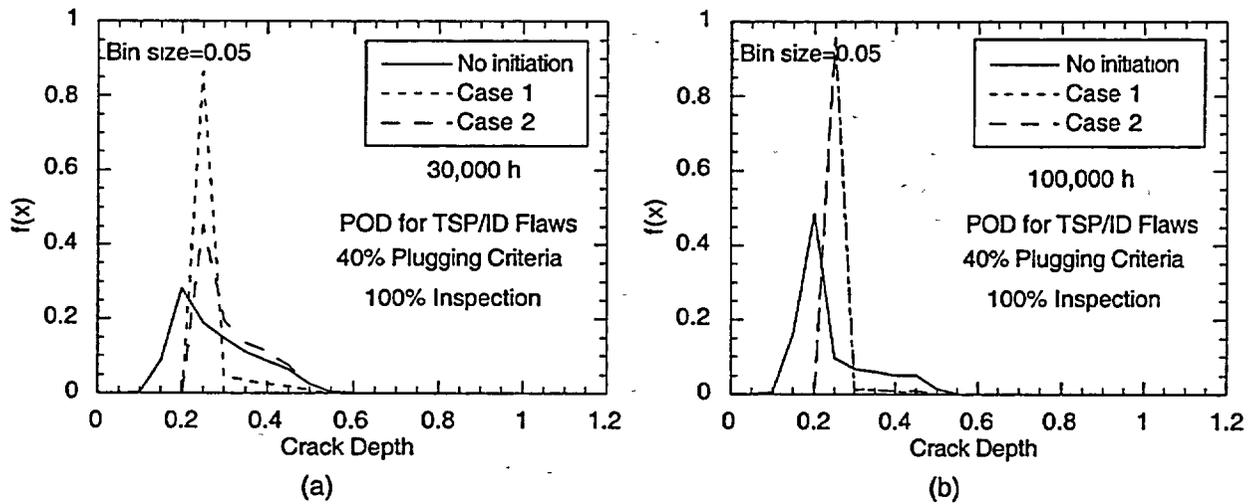


Figure 21. Distributions of crack depth calculated without initiation and with Weibull initiation case 1 and case 2 at (a) 30,000 h and (b) 100,000 h.

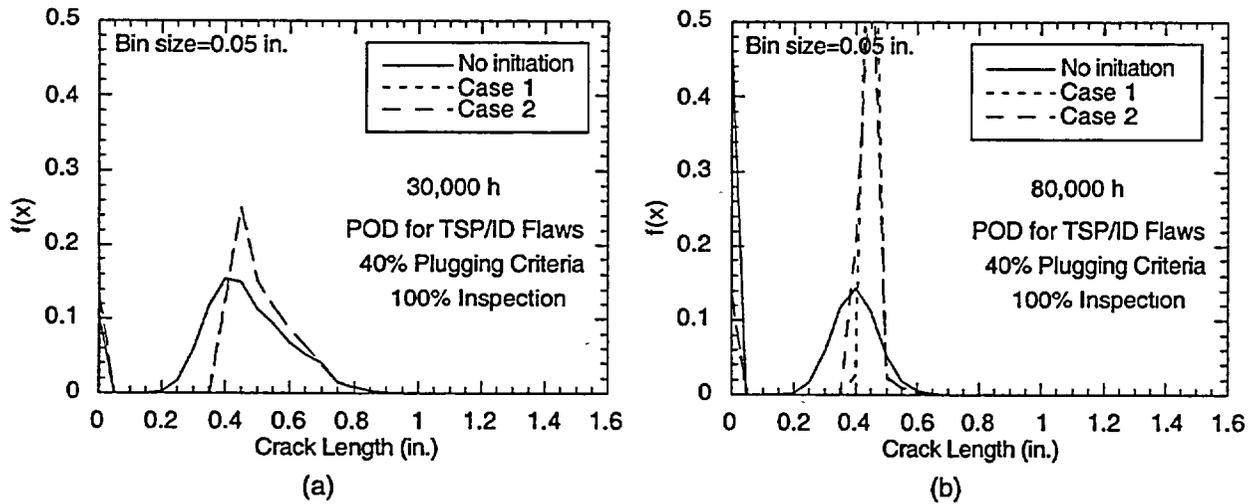


Figure 22. Distributions of crack length calculated without initiation and with Weibull initiation case 1 and case 2 at (a) 30,000 h and (b) 80,000 h.

## **5 Conclusions and Recommendations for Future Work**

The Monte Carlo-based code CANTIA to simulate the effects of tube inspection and maintenance strategies on the safe operation of CANDU design nuclear steam generators has been updated with several new features. The ANL failure and leak rate models have been added as options. Stress corrosion crack growth can now be calculated in terms of both depth and length simultaneously. The Scott and Ford-Andresen models for stress corrosion crack growth rates have been added as options. A simple residual stress model has been included.

The ANL/CANTIA code has been checked extensively for axial cracks. Several sample trial runs have been conducted to explore the effect of POD and new crack initiation on the rupture and leak rate probabilities. The circumferential crack models have not been checked as thoroughly and may require more debugging. Several other improvements in the code may be warranted in the future:

- (1) Water chemistry is accounted for in the model only by the users choice of input values for crack growth and initiation parameters. More complete phenomenological models of crack initiation and growth are needed to get a more realistic picture of steam generator behavior.
- (2) Currently, the initiation of new cracks is assumed to occur randomly in time, but the initiated crack is assumed to be of a fixed size independent of temperature, stress, and any other environmental parameters. A more refined initiation model should be developed in the future.
- (5) Trial runs with ANL/CANTIA have shown that in the case of PWSCC it is very difficult to grow stress corrosion cracks by pressure-induced stress alone without the help of residual stress. In practice, residual stresses are almost always involved wherever early stress corrosion cracks are detected in steam generators. The current residual stress model in ANL/CANTIA is very simplified. Because of the important role of the residual stresses, a more realistic model for residual stress should be developed.
- (6) The Scott and Ford-Andresen model are reasonable phenomenological descriptions of PWSCC growth rate in the regime controlled by fracture mechanics. Other phenomenological models, such as internal oxidation model, hydrogen embrittlement model, etc. should be added. In addition better phenomenological descriptions of the growth and maturation of crack networks that cannot be described in terms of fracture mechanics need to be developed and incorporated.
- (7) Flaw geometries in the current ANL/CANTIA are characterized by a depth and a length both in terms of growth and failure. Recent work at ANL and elsewhere have indicated that the "equivalent rectangular crack" method, which essentially provides an effective length and depth, can estimate the ligament rupture pressure and leak rates from fairly complex depth profiles. Whether the growth of stress corrosion cracks can be predicted or even crudely estimated from analysis of the "equivalent rectangular crack" by using fracture mechanics methodology has not yet been established. A methodology for predicting growth rates of complex stress corrosion cracks needs to be developed. Until

then, determining an effective length and depth through the equivalent rectangular crack method developed for integrity analyses appears to be a reasonable approach.

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10 SUPPLEMENTARY NOTES

J. Davis, NRC Project Manager

11. ABSTRACT *(200 words or less)*

This report summarizes the work carried out to modify and expand the capability of the steam generator integrity code CANTIA originally developed for CANDU reactors. The basic algorithms for the Monte Carlo simulation, the random initiation of cracks, the effect of inservice inspection including the probability of detection of cracks, and the inclusion of plugging criteria for defective tubes have been retained. Additional ligament rupture, unstable burst, and leak rate models for Alloy 600 tubes that have been developed or validated at Argonne National Laboratory have been incorporated into the code. Fracture mechanics models for crack growth rate based on stress corrosion cracking data from the literature have also been added. The basic treatment of flaw growth has been changed from one- to two-dimensional, and crack growth calculations have been made more rigorous.

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stress corrosion cracks  
Monte Carlo simulation

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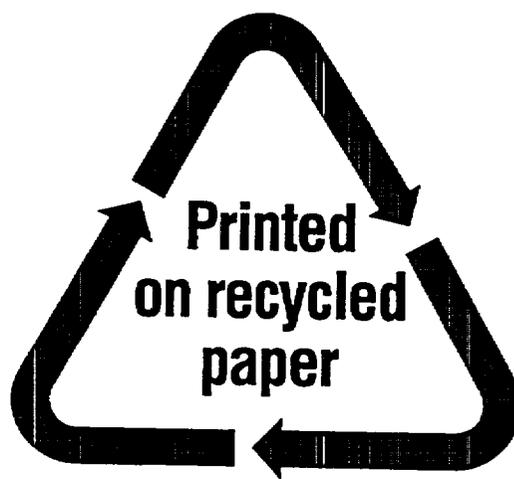
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