Westinghouse Presentation on ZIRLO Characterization Plant (Slide Presentation of July 11, 2002)

June 2002

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ZIRLO[™] Characterization Plan

Westinghouse Electric Company

Presented by: Hemant Shah and Ron Kesterson

July 11, 2002

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ZIRLO[™] Characterization Plan

- Meeting Objective
 - Present Low Tin ZIRLO[™] Characterization plan to support license extension for Low Tin ZIRLO[™] cladding consistent with presentations to NRC in 2001 and 2002
 - Obtain feedback on scope of planned efforts

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ZIRLOTM Characterization Plan

- Program Objective
 - By performing Low Tin ZIRLO[™] Characterization, we will demonstrate that Low Tin ZIRLO[™] is not a new material, but a minor change within the technical envelope of a well-proven ZIRLO[™] cladding

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ZIRLOTM Characterization Plan

- Background
 - Westinghouse intent to license Low Tin ZIRLO[™] presented to NRC on Oct 29, 2001
 - Strategy to develop Low Tin ZIRLO[™] characteristics database defined
 - –Low Tin ZIRLO[™] characteristics will be demonstrated to be compatible with standard ZIRLO[™] properties
 - Westinghouse intent to license Low Tin ZIRLO[™] and strategy reiterated to NRC on May 14-15, 2002 semi-annual meeting
 - -General approach seemed reasonable

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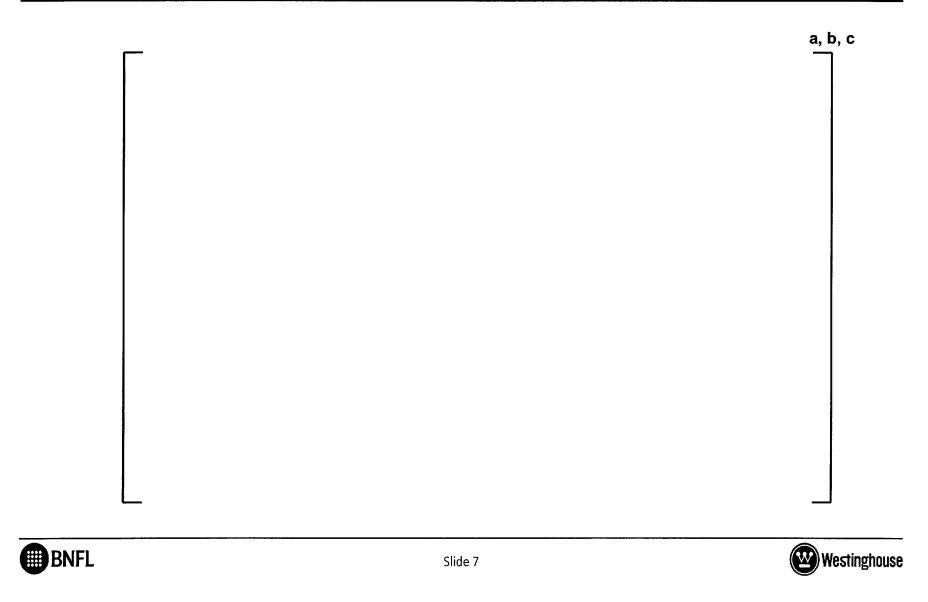
ZIRLO[™] Characterization Plan

Changes in fabrication	Benefit or impact
Change tin level range from [] ^{a, c}	Reduce Corrosion
esting	
Ex-core	Provide data used in reload evaluation
In-core - Exposure in LTA	Gather PIE data to validate models and demonstrate benefits

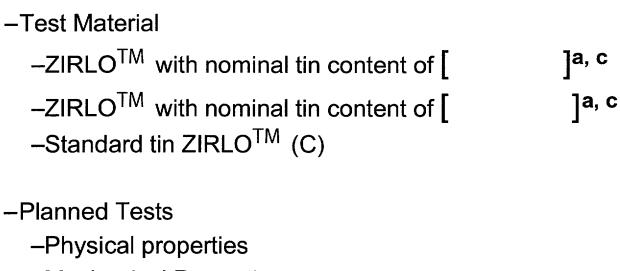
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ZIRLOTM Characterization Plan



● Low Tin ZIRLO TM Ex-Core Testing



- -Mechanical Properties
- -Microstructure
- -High Temperature/LOCA Tests

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• Summary of Basic Properties Characterization

Physical tests

Density Emissivity - oxidized and unoxidized Specific Heat Thermal Conductivity Thermal Expansion Axial / longitudinal Diametrical/hoop or transverse Alpha-Beta Transition Temperature **Mechanical Tests: Axial Mechanical Test:** Yield Strength Ultimate strength Elongation at failure Modulus of elasticity

Poisson's ratio axial/diametral

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ZIRLOTM Characterization Plan

• Summary of Basic Properties Characterization (Cont'd)

Hoop Burst Test:

- Yield Strength
- Ultimate strength
- Strain at failure
- Modulus of elasticity

Biaxial Burst Test:

- Ultimate strength
- Microhardness Traverse
- Fatigue
- Microstructure:
 - Particle Size

High Temperature/LOCA tests:

- Quench Tests Ring Compression Tests Metal-Water Reaction (High Temperature)**
- Burst Test (Strain & Temperature @ burst)
- LOCA creep





ZIRLO[™] Characterization Plan

Physical properties

-Density (A, B)

- » Immersion Method
- » At Room Temperature with extrapolation to higher temperature based on measured value of thermal expansion

-Emissivity (A, C)

- » Oxidized and unoxidized Condition
- » ASTM Method C-835
- » Minimum 500 C and maximum 1200 C

-Specific Heat (A,B,C)

- » ASTM method E1269-01
- » From Room Temperature to 1200 C

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Physical properties (Cont'd)

-Thermal Conductivity (A, C)

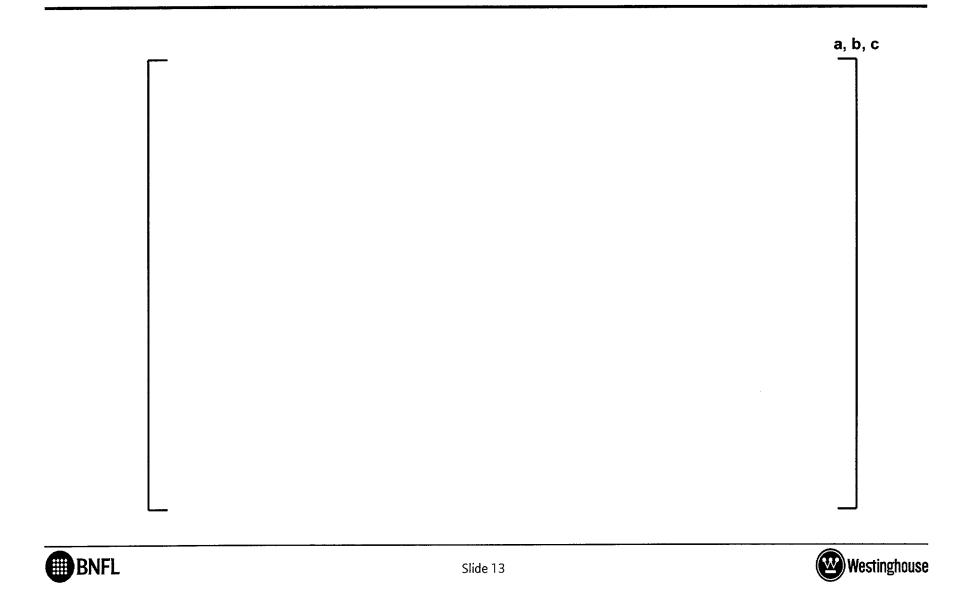
- » Modified Kohlaruse technique
- » Up to 1210 C

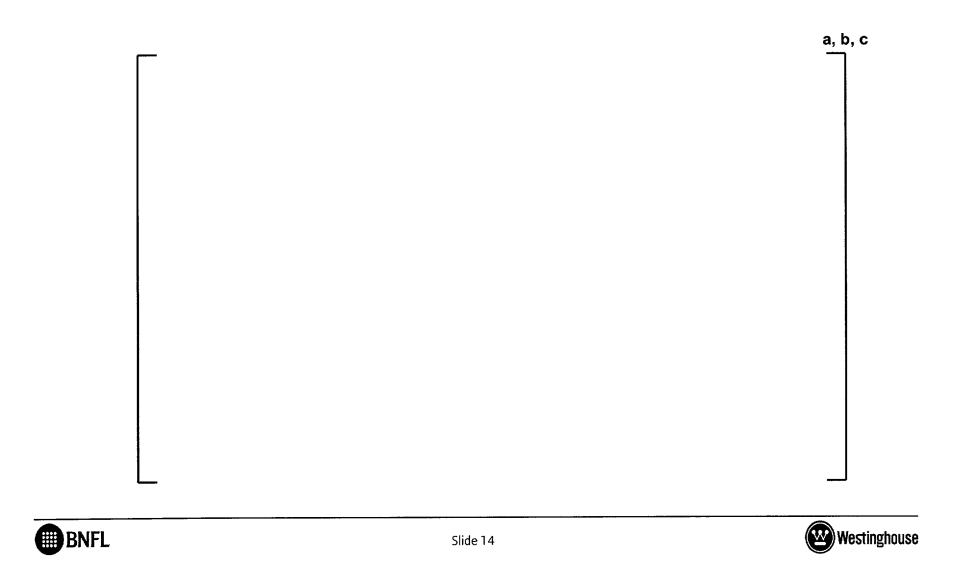
-Thermal Expansion (A, B, C)

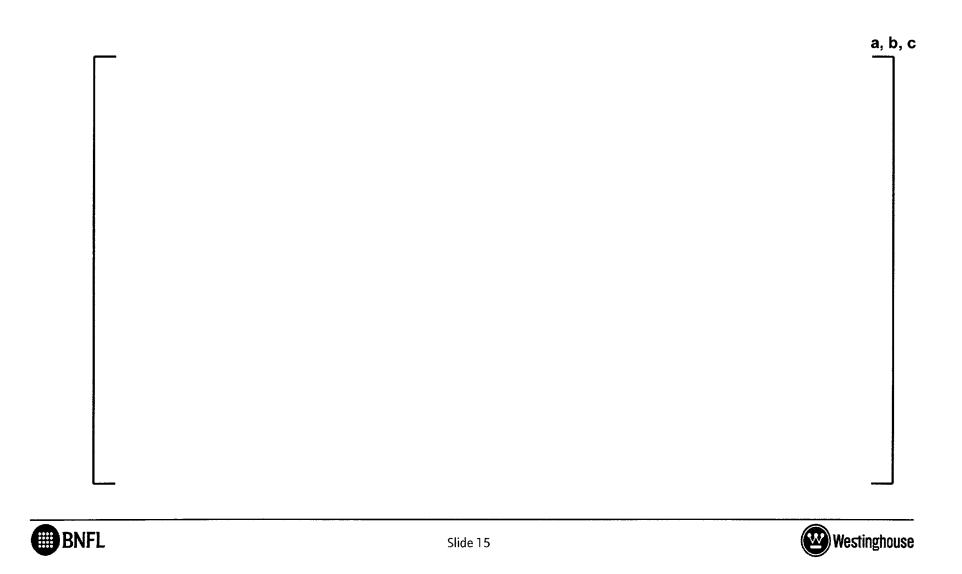
- » Alpha-Beta Transition temperature
- » Axial/longitudinal
- » Diametral/Hoop
- » From Room Temperature to 1200 C











Mechanical Properties (A, B, C)

-Axial Tensile Tests

» Properties:

Yield Strength Ultimate strength Elongation at failure Modulus of elasticity Poisson's ratio

» Temperatures:

RT: Connect with large Production Certification databases and prior data 390 °F (200 °C) Intermediate temperature to improve temperature-property curves 660 and 725 °F (350 and 385 °C) Near operating temperature for a range of reactors. 1110°F (600°C) Abnormal conditions.

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Mechanical Properties (Cont'd)

-Hoop Burst Test:

 Properties: Ultimate strength Elongation at failure Modulus of elasticity Temperatures: RT, 390, 660, 725°F (RT, 200, 350, 385°C)

-Biaxial Burst Test:

» Ultimate strength

Temperatures: RT, 390, 660, 725°F (RT, 200, 350, 385°C)

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Mechanical Properties (Cont'd)

-Fatigue (A)

- » Room temperature
- » Up to 10 million cycles
- » Tension and compression
- » 6 stress levels starting from [
-] ^{a, b, c} at 20 MPa interval

-Particle Size (A)

- » Size and distribution of intermetallic phase particles
- » Minimum of 100 particles to be photographed per sample





High Temperature/LOCA Tests (A, C)

-Quench Tests

- »Demonstrate acceptable cladding ductility under LOCA quench conditions.
- »Cladding will be rapidly oxidized in a high temperature steam environment to produce varying levels of oxide thickness.
- »The sample will be quenched to room temperature by submersion in water.





High Temperature/LOCA Tests

-Ring Compression Tests

- » Measure ductility retained by cladding following rapid oxidation.
- » Cladding samples rapidly oxidized in a high temperature steam environment to produce varying levels of oxide thickness.
- » The oxidized samples will then be cut into rings and used as ring compression samples.
- » Compression testing provides quantifiable ductility data for cladding that has been severely oxidized.

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High Temperature/LOCA Tests (Cont'd)

-Metal-Water Reaction (High Temperature)

- » Cladding samples will be oxidized at high temperature to produce a uniform oxide coating
- $\ast\,$ The weight gain of the oxide will be recorded , oxidation rates calculated and compared with previous ZIRLO^{TM}\, data





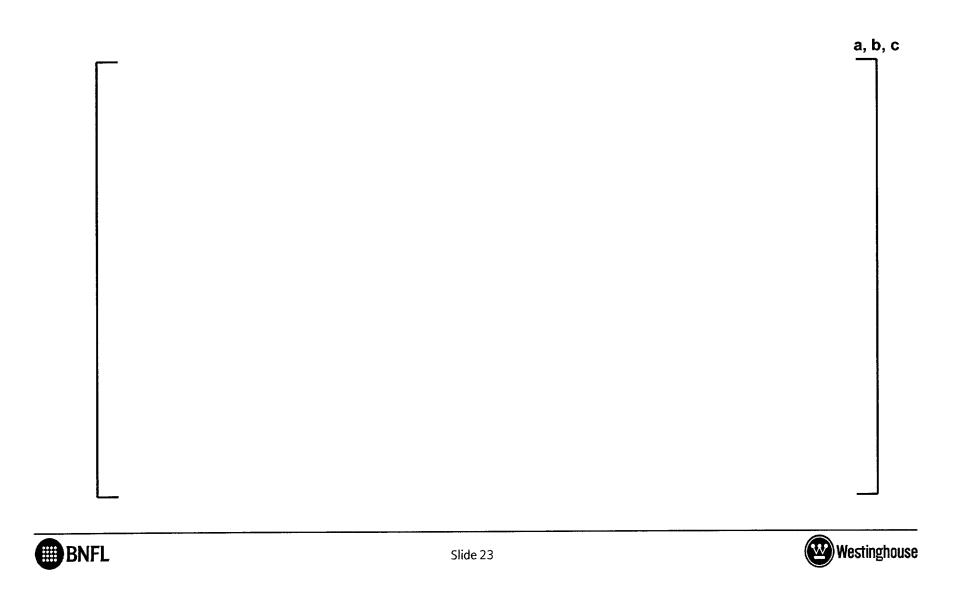
High Temperature/LOCA Tests (Cont'd)

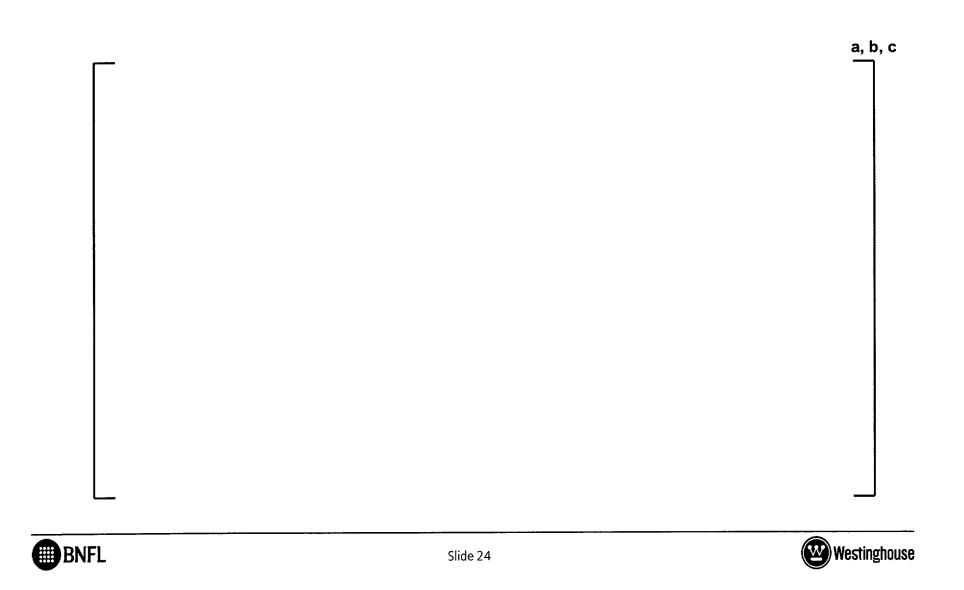
-Burst Test (Strain & Temperature @ burst)

- » [] sections of cladding are internally pressurized with argon.
- » Rapid temperature transients are produced by infra-red heating of the cladding to simulate LOCA conditions.
- » The burst temperature and physical condition of the tube following burst are recorded and used to calculate strain at burst.









High Temperature/LOCA Tests (Cont'd)

-LOCA creep

- » Cladding tube sections are held at a constant temperature and pressure.
- » Temperatures will be chosen to provide test in all the alpha, alpha/beta, and beta phase ranges.
- » The diametral strain of the cladding will be measured as a function of time providing data about the creep behavior of the alloy.
- » Testing different temperature and pressure combinations will provide data on the cladding creep performance under LOCA conditions.





- Low Tin ZIRLO TM Licensing
 - –A complete set of ZIRLO[™] base material properties updated with Low Tin ZIRLO[™]
 - –Regions will be licensed to all current criteria. Current models will be justified and compared to test data. Information will be submitted for review and approval in addenda to WCAP-12610-P-A and CENPD 404-P-A to expand ZIRLO[™] definition to cover low tin condition for region introduction

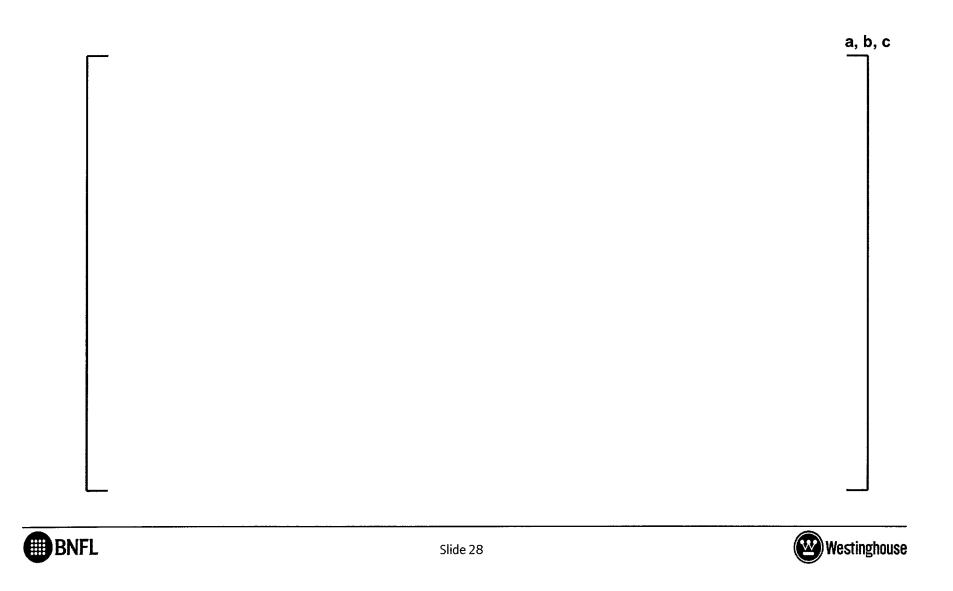


ZIRLOTM Characterization Plan

- Planned Changes in ZIRLO TM Specification
 - -Are minor similar to past changes in Zirc-4
 - -Provide greater corrosion margin and higher fuel duty capability
 - -Will be submitted for review in addendum's to existing topicals with updated material properties
 - WCAP-12610-P-A and CENPD 404-P-A



ZIRLOTM Characterization Plan



- Byron LTA 1st Cycle (high Duty, High FDI) Rod oxide Data Summary
 - Low tin ZIRLOTM : []a, c
 - Standard ZIRLOTM : []a, c

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ZIRLOTM Characterization Plan

• Low Tin ZIRLO[™] Introduction

Planned Schedule

-First NRC meeting to layout planned licensing path

 $- Low \, Tin \, ZIRLO^{{\rm TM}} \, Characterization \, plan$

—Submit Low Tin ZIRLO[™] Addenda to
—WCAP-12610-P-A
—CENPD 404-P-A

–NRC Approval of Low Tin ZIRLO[™] Addenda

-Region introduction of low tin ZIRLO[™]

- Oct 29, 2001
- July, 2002
- Dec. 2002
- July, 2003
- []a, c

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ZIRLOTM Characterization

• Summary

- Low tin ZIRLOTM Characterization consistent with earlier presentations
- Basic material properties characterization will be expanded
- \bullet Low Tin ZIRLOTM characteristics will be demonstrated to be compatible with standard ZIRLOTM

properties and submitted as addenda to current WCAPs (WCAP-12610-P-A, CENPD 404-

P-A)

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Westinghouse Presentation on DNB Testing (Slide Presentation of July 11, 2002)

June 2002

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Westinghouse DNB Testing

Gerald Sieradzki July 11, 2002





<u>Outline</u>

- Closing of Columbia Test Facility (HTRF)
- Requirements of DNB Testing
- Alternate Test Facilities
- Westinghouse Qualification Process
- Potential Licensing Applications





Closing of Columbia HTRF

- Columbia HTRF is closing down by 6/30/03
- All <u>W</u> DNB test data supporting NRC approved DNB correlations were obtained from HTRF
- Closing down of HTRF has major impacts on future safety analysis in the U.S.





Requirements of DNB Testing

- <u>W</u> uses NRC-approved FCEP (WCAP-12488-A) for evaluating fuel design changes
- Fuel changes not covered by FCEP may require DNB tests



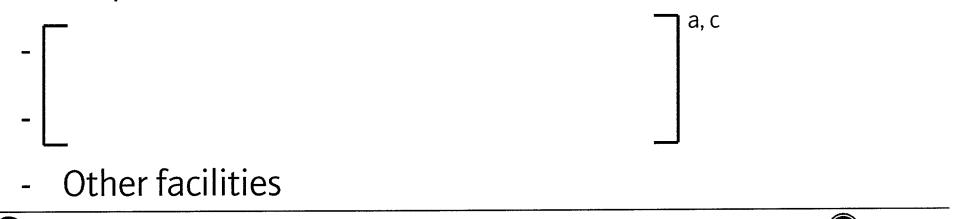
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Slide 5

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Alternate Test Facilities

- <u>W</u> is actively evaluating alternate DNB test facilities
- All alternate facilities are [
- Primary facility under consideration is [1^{a, c}
- Backup facilities include:



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Slide 6

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a, c

Westinghouse Qualification Process

- Over the years, <u>W</u> has developed a process for qualifying test facilities and data for safety analyses
 - Personnel qualification
 - Testing procedures
 - Data collection and reduction
 - Test bundle manufacturing, etc.





Westinghouse Qualification Process (continued)

- The process was applied to Columbia HTRF and [1^{a, c}
- The process will include [1^{a, c}
- This same process will be applied to alternate test facilities
- NRC participation during qualification DNB testing of an alternate facility is welcomed

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Slide 8

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Potential Licensing Applications

- DNB test data collected from an alternate test facility will meet <u>W</u> QMS requirements
- DNB test data on future fuel designs will be used for qualification of 95/95 DNBR limit
 - An existing NRC-approved DNB correlation
 - Minor adjustment to a DNB correlation
 - A new DNB correlation

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Summary

- Because of the closing down of Columbia HTRF, <u>W</u> is evaluating alternate DNB test facilities to meet regulatory requirements for future fuel design changes
- <u>W</u> intends to apply its proven qualification process to any alternate test facility
- DNB data from an alternate test facility will be used for justifying the 95/95 DNBR limit of a DNB correlation







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