June 5, 2002

Mr. John T. Conway
Site Vice President
Nine Mile Point Nuclear Station, LLC
P.O. Box 63
Lycoming, NY 13093

SUBJECT: NINE MILE POINT NUCLEAR STATION, UNIT NO. 2 - REQUEST FOR ADDITIONAL INFORMATION REGARDING WELD KC-32 ON HIGH PRESSURE CORE SPRAY NOZZLE (TAC NO. MB4869)

Dear Mr. Conway:

The U.S. Nuclear Regulatory Commission (NRC) staff received a letter from Mr. K. S. Grewal expressing his concern about a crack at Weld KC-32 joining the high pressure core spray nozzle safe end to the safe end extension on the reactor pressure vessel. On May 21, 2002, we communicated by e-mail (publicly available in ADAMS Accession No. ML021410517) our need for additional information to complete a response to Mr. Grewal. On May 29, 2002, we held a telephone conference with your staff to discuss the issues. After the conference call, the NRC staff finalized the questions into a request for additional information (enclosure).

As discussed with your staff, we would appreciate your response by June 14, 2002. If you need clarification, please call me at 301-415-1451.

Sincerely,

/RA/

Peter S. Tam, Senior Project Manager, Section 1
Project Directorate I
Division of Licensing Project Management
Office of Nuclear Reactor Regulation

Docket No. 50-410

Enclosure: As stated

cc w/encl: See next page

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REQUEST FOR ADDITIONAL INFORMATION

NINE MILE POINT NUCLEAR STATION, UNIT NO. 2

REGARDING WELD KC-32 ON HIGH PRESSURE CORE SPRAY (HPCS) NOZZLE

Reference: Letter, K. S. Grewal to S. Collins of NRC, April 4, 2002

(1) Provide the results of ultrasonic testing (UT) performed in the spring 2002 refueling outage on weld KC-32, and compare the results with those of the previous post-MSIP [mechanical stress improvement process] inspections.

(2) Describe the UT equipment and procedures used in the inspection of weld KC-32 in the 2002 refueling outage, and identify the differences with those used in previous inspections. If different equipment and procedures were used, discuss their impact on the results of flaw size measurements.

(3) For comparison purposes, provide information on the following items pertaining to the UT inspections performed on weld K-32 after implementation of MSIP.

    (a) UT measurement uncertainties associated with the reported flaw length and depth during each post-MSIP inspection.

    (b) UT qualification requirements of the procedures/equipment/personnel that were used in the inspection of weld KC-32 during each post-MSIP inspection.

    (c) During each post-MSIP UT inspection, clarify whether the spring hanger for pipe support near weld KC-32 was pinned and describe the weight of shielding lead that were placed on the HPCS piping.

    (d) An estimation of upper bound compressive stresses on the flaw in weld KC-32 resulting from the weight of shielding lead with unpinned spring hangers, and the potential impact to the results of UT inspection due to these compressive stresses. Specifically, discuss the differences in resulting compressive stresses between pinned and un-pinned spring hanger configurations.

(4) Describe the design basis fatigue usage factor limit for the HPCS system. In addition, provide information pertaining to the thermal stratification stress of the HPCS piping adjoining the reactor pressure vessel nozzle, if any. Furthermore, describe how this thermal stratification stress is considered in the crack evaluation.

Enclosure

Nine Mile Point Nuclear Station
Unit No. 2
cc:

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