



**Duke Energy Corporation**

McGuire Nuclear Station  
12700 Hagers Ferry Road  
Huntersville, NC 28078-9340

(704) 875-4800 OFFICE

(704) 875-4809 FAX

H. B. Barron  
Vice President

March 20, 2002

U. S. Nuclear Regulatory Commission  
Document Control Desk  
Washington, D.C. 20555

Subject: McGuire Nuclear Station,  
Docket No.50-369, 50-370  
Unit 2 Cycle 15  
Core Operating Limits Report (COLR)

Pursuant to McGuire Technical Specification 5.6.5.d, please find enclosed the McGuire Unit 2 Core Operating Limits Report (COLR). Revision 21 contains limits specific to the McGuire Unit 2 Cycle 15 core.

Questions regarding this submittal should be directed to Kay Crane, McGuire Regulatory Compliance at (704) 875-4306.

A handwritten signature in black ink, appearing to read 'H. B. Barron'.

H. B. Barron

Attachment

A001

U. S. Nuclear Regulatory Commission  
March 20, 2002  
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cc: Mr. R. E. Martin, Project Manager  
Office of Nuclear Reactor Regulation  
U.S. Nuclear Regulatory Commission  
Washington, D.C. 20555

Mr. Luis Reyes, Regional Administrator  
U. S. Nuclear Regulatory Commission  
Region II  
Atlanta Federal Center  
61 Forsyth St., SW, Suite 23T85  
Atlanta, GA 30323

Mr. Scott Shaeffer  
Senior Resident Inspector  
McGuire Nuclear Station

U.S. Nuclear Regulatory Commission  
March 20, 2002  
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bx: RGC File  
ECO50-ELL  
P. M. Abraham

**McGuire Unit 2 Cycle 15**  
**Core Operating Limits Report**  
**Revision 21**

**February 2002**

Calculation Number: MCC-1553.05-00-0358

**Duke Power Company**

	Date
Prepared By: <u>David S. Botz</u>	<u>2/12/02</u>
Checked By: <u>John R. Bortch</u>	<u>2/14/02</u>
Checked By: <u>Jan S. Muransky</u>	<u>2/12/02</u>
Approved By: <u>P.M. Abraham</u>	<u>2/12/02</u>

**QA Condition 1**

## **McGuire 2 Cycle 15 Core Operating Limits Report**

### **IMPLEMENTATION INSTRUCTIONS FOR REVISION 21**

Revision 21 of the McGuire Unit 2 COLR contains limits specific to the McGuire 2 Cycle 15 core and may become effective any time during the no-mode between Cycles 14 and 15.

This revision must become effective prior to entering Mode 6 that starts Cycle 15.

This COLR revision also incorporates a list of reports describing the analytical methods used in determining core operating limits. This addition is based upon a pending Technical Specification Amendment that requires the COLR to contain a complete list of the Technical Specification 5.6.5 reference topical reports used for parameters contained in the COLR. Inclusion of the reference list alleviates the need to revise the COLR following NRC approval of the Technical Specification amendment.

## McGuire 2 Cycle 15 Core Operating Limits Report

### REVISION LOG

<u>Revision</u>	<u>Issuance Date</u>	<u>Effective Pages</u>	<u>COLR</u>
Revisions 0-2	Superseded	N/A	M2C09
Revisions 3-6	Superseded	N/A	M2C10
Revisions 7-12	Superseded	N/A	M2C11
Revision 13-15	Superseded	N/A	M2C12
Revision 16-17	Superseded	N/A	M2C13
Revision 18-20	Superseded	N/A	M2C14
Revision 21	February 12, 2002	1-29	M2C15 – Orig. Issue

**McGuire 2 Cycle 15 Core Operating Limits Report**

**INSERTION SHEET FOR REVISION 21**

**Remove pages**

Pages 1-27, 27a and Appendix A

**Insert Rev. 21 pages**

Pages 1-29 and Appendix A

## McGuire 2 Cycle 15 Core Operating Limits Report

### 1.0 Core Operating Limits Report

This Core Operating Limits Report (COLR) has been prepared in accordance with the requirements of Technical Specification 5.6.5. The Technical Specifications that reference this report are listed below:

<u>TS</u> <u>Section</u>	<u>Technical</u> <u>Specifications</u>	<u>COLR</u> <u>Section</u>	<u>COLR</u> <u>Page</u>
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The Selected Licensee Commitments that reference this report are listed below:

<u>SLC</u> <u>Section</u>	<u>Selected License</u> <u>Commitments</u>	<u>COLR</u> <u>Section</u>	<u>COLR</u> <u>Page</u>
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### 1.1 Analytical Methods

The analytical methods used to determine core operating limits for parameters identified in Technical Specifications and previously reviewed and approved by the NRC as specified in Technical Specification 5.6.5 are as follows.

1. WCAP-9272-P-A, “WESTINGHOUSE RELOAD SAFETY EVALUATION METHODOLOGY,” (W Proprietary).

Revision 0  
Report Date: July 1985  
Not Used for M2C15

## McGuire 2 Cycle 15 Core Operating Limits Report

### 1.1 Analytical Methods Continued

2. WCAP-10054-P-A, "Westinghouse Small Break ECCS Evaluation Model using the NOTRUMP Code, " (W Proprietary).

Revision 0

Report Date: August 1985

Note: Amendments to this report are included in Ref. 12.

3. WCAP-10266-P-A, "THE 1981 VERSION OF WESTINGHOUSE EVALUATION MODEL USING BASH CODE", (W Proprietary).

Revision 2

Report Date: March 1987

Not Used for M2C15

4. WCAP-12945-P-A, Volume 1 and Volumes 2-5, "Code Qualification Document for Best-Estimate Loss of Coolant Analysis," (W Proprietary).

Revision: Volume 1 (Revision 2) and Volumes 2-5 (Revision 1)

Report Date: March 1998

5. BAW-10168P-A, "B&W Loss-of-Coolant Accident Evaluation Model for Recirculating Steam Generator Plants," (B&W Proprietary).

Revision 1

SER Date: January 22, 1991

Revision 2

SER Dates: August 22, 1996 and November 26, 1996.

Revision 3

SER Date: June 15, 1994.

Not Used for M2C15

6. DPC-NE-3000PA, "Thermal-Hydraulic Transient Analysis Methodology," (DPC Proprietary).

Revision 2

SER Date: October 14, 1998

7. DPC-NE-3001PA, "Multidimensional Reactor Transients and Safety Analysis Physics Parameter Methodology," (DPC Proprietary).

Revision 0

Report Date: November 1991

## McGuire 2 Cycle 15 Core Operating Limits Report

8. DPC-NE-3002A, "FSAR Chapter 15 System Transient Analysis Methodology".  
  
Revision 3  
SER Date: February 5, 1999
9. DPC-NE-2004P-A, "Duke Power Company McGuire and Catawba Nuclear Stations Core Thermal-Hydraulic Methodology using VIPRE-01," (DPC Proprietary).  
  
Revision 1  
SER Date: February 20, 1997
10. DPC-NE-2005P-A, "Thermal Hydraulic Statistical Core Design Methodology," (DPC Proprietary).  
  
Revision 1  
SER Date: November 7, 1996
11. DPC-NE-2008P-A, "Fuel Mechanical Reload Analysis Methodology Using TACO3," (DPC Proprietary).  
  
Revision 0  
SER Date: April 3, 1995
12. DPC-NE-2009-P-A, "Westinghouse Fuel Transition Report," (DPC Proprietary).  
  
Revision 0  
SER Date: September 22, 1999
13. DPC-NE-1004A, "Nuclear Design Methodology Using CASMO-3/SIMULATE-3P."  
  
Revision 1  
SER Date: April 26, 1996
14. DPC-NF-2010A, "Duke Power Company McGuire Nuclear Station Catawba Nuclear Station Nuclear Physics Methodology for Reload Design."  
  
Revision 0  
Report Date: June 1985
15. DPC-NE-2011PA, "Duke Power Company Nuclear Design Methodology for Core Operating Limits of Westinghouse Reactors," (DPC Proprietary).  
  
Revision 0  
Report Date: March 1990

## McGuire 2 Cycle 15 Core Operating Limits Report

### 2.0 Operating Limits

The cycle-specific parameter limits for the specifications listed in Section 1.0 are presented in the following subsections. These limits have been developed using the NRC approved methodologies specified in Section 1.1.

### 2.1 Requirements for Operational Mode 6

The following condition is required for operational mode 6.

2.1.1 The Reactivity Condition requirement for operational mode 6 is that  $k_{\text{eff}}$  must be less than, or equal to 0.95.

### 2.2 Shutdown Margin - SDM (TS 3.1.1, TS 3.1.4, TS 3.1.5, TS 3.1.6 and TS 3.1.8)

2.2.1 For TS 3.1.1, SDM shall be  $\geq 1.3\% \Delta K/K$  in mode 2 with  $k\text{-eff} < 1.0$  and in modes 3 and 4.

2.2.2 For TS 3.1.1, SDM shall be  $\geq 1.0\% \Delta K/K$  in mode 5.

2.2.3 For TS 3.1.4, SDM shall be  $\geq 1.3\% \Delta K/K$  in modes 1 and 2.

2.2.4 For TS 3.1.5, SDM shall be  $\geq 1.3\% \Delta K/K$  in mode 1 and mode 2 with any control bank not fully inserted.

2.2.5 For TS 3.1.6, SDM shall be  $\geq 1.3\% \Delta K/K$  in mode 1 and mode 2 with  $K\text{-eff} \geq 1.0$ .

2.2.6 For TS 3.1.8, SDM shall be  $\geq 1.3\% \Delta K/K$  in mode 2 during Physics Testing.

### 2.3 Moderator Temperature Coefficient - MTC (TS 3.1.3)

2.3.1 The Moderator Temperature Coefficient (MTC) Limits are:

The MTC shall be less positive than the upper limits shown in Figure 1. The BOC, ARO, HZP MTC shall be less positive than  $0.7E-04 \Delta K/K/^\circ F$ .

The EOC, ARO, RTP MTC shall be less negative than the  $-4.1E-04 \Delta K/K/^\circ F$  lower MTC limit.

## McGuire 2 Cycle 15 Core Operating Limits Report

### 2.3.2 The 300 ppm MTC Surveillance Limit is:

The measured 300 PPM ARO, equilibrium RTP MTC shall be less negative than or equal to  $-3.2E-04 \Delta K/K/^{\circ}F$ .

### 2.2.3 The 60 PPM MTC Surveillance Limit is:

The 60 PPM ARO, equilibrium RTP MTC shall be less negative than or equal to  $-3.85E-04 \Delta K/K/^{\circ}F$ .

Where: BOC = Beginning of Cycle (Burnup corresponding to the most positive MTC)  
EOC = End of Cycle  
ARO = All Rods Out  
HWP = Hot Zero Power  
RTP = Rated Thermal Power  
PPM = Parts per million (Boron)

## 2.4 Shutdown Bank Insertion Limit (TS 3.1.5)

2.4.1 Each shutdown bank shall be withdrawn to at least 226 steps. Shutdown banks are withdrawn in sequence and with no overlap.

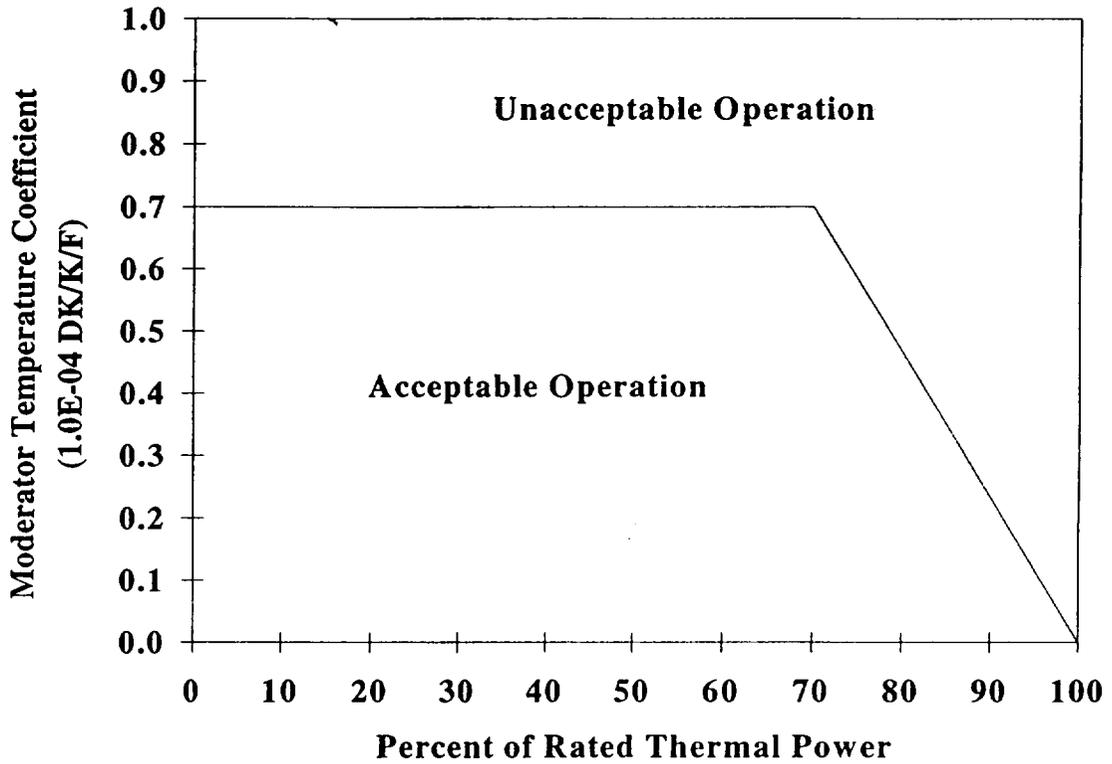
## 2.5 Control Bank Insertion Limits (TS 3.1.6)

2.5.1 Control banks shall be within the insertion, sequence, and overlap limits shown in Figure 2. Specific control bank withdrawal and overlap limits as a function of the fully withdrawn position are shown in Table 1.

### McGuire 2 Cycle 15 Core Operating Limits Report

Figure 1

Moderator Temperature Coefficient Upper Limit Versus Power Level

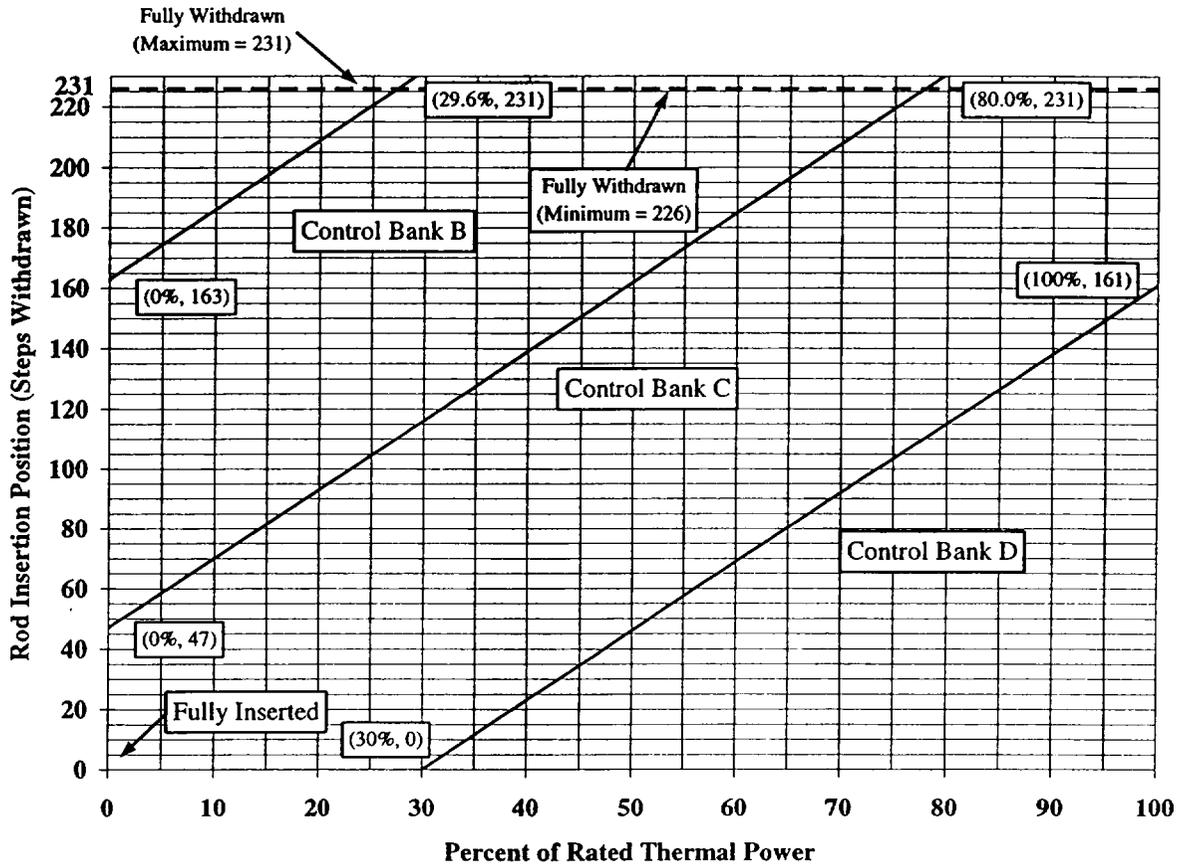


**NOTE:** Compliance with Technical Specification 3.1.3 may require rod withdrawal limits. Refer to OP/2/A/6100/22 Unit 2 Data Book for details.

McGuire 2 Cycle 15 Core Operating Limits Report

Figure 2

Control Bank Insertion Limits Versus Percent Rated Thermal Power



NOTE: Compliance with Technical Specification 3.1.3 may require rod withdrawal limits. Refer to OP/2/A/6100/22 Unit 2 Data Book for details.

**McGuire 2 Cycle 15 Core Operating Limits Report**

**Table 1  
RCCA Withdrawal Steps and Sequence**

<b>RCCAs Fully Withdrawn at 226 SWD</b>				<b>RCCAs Fully Withdrawn at 227 SWD</b>			
<b>Control Bank A</b>	<b>Control Bank B</b>	<b>Control Bank C</b>	<b>Control Bank D</b>	<b>Control Bank A</b>	<b>Control Bank B</b>	<b>Control Bank C</b>	<b>Control Bank D</b>
0 Start	0	0	0	0 Start	0	0	0
116	0 Start	0	0	116	0 Start	0	0
226 Stop	110	0	0	227 Stop	111	0	0
226	116	0 Start	0	227	116	0 Start	0
226	226 Stop	110	0	227	227 Stop	111	0
226	226	116	0 Start	227	227	116	0 Start
226	226	226 Stop	110	227	227	227 Stop	111

<b>RCCAs Fully Withdrawn at 228 SWD</b>				<b>RCCAs Fully Withdrawn at 229 SWD</b>			
<b>Control Bank A</b>	<b>Control Bank B</b>	<b>Control Bank C</b>	<b>Control Bank D</b>	<b>Control Bank A</b>	<b>Control Bank B</b>	<b>Control Bank C</b>	<b>Control Bank D</b>
0 Start	0	0	0	0 Start	0	0	0
116	0 Start	0	0	116	0 Start	0	0
228 Stop	112	0	0	229 Stop	113	0	0
228	116	0 Start	0	229	116	0 Start	0
228	228 Stop	112	0	229	229 Stop	113	0
228	228	116	0 Start	229	229	116	0 Start
228	228	228 Stop	112	229	229	229 Stop	113

<b>RCCAs Fully Withdrawn at 230 SWD</b>				<b>RCCAs Fully Withdrawn at 231 SWD</b>			
<b>Control Bank A</b>	<b>Control Bank B</b>	<b>Control Bank C</b>	<b>Control Bank D</b>	<b>Control Bank A</b>	<b>Control Bank B</b>	<b>Control Bank C</b>	<b>Control Bank D</b>
0 Start	0	0	0	0 Start	0	0	0
116	0 Start	0	0	116	0 Start	0	0
230 Stop	114	0	0	231 Stop	115	0	0
230	116	0 Start	0	231	116	0 Start	0
230	230 Stop	114	0	231	231 Stop	115	0
230	230	116	0 Start	231	231	116	0 Start
230	230	230 Stop	114	231	231	231 Stop	115

## McGuire 2 Cycle 15 Core Operating Limits Report

### 2.6 Heat Flux Hot Channel Factor - $F_Q(X,Y,Z)$ (TS 3.2.1)

2.6.1  $F_Q(X,Y,Z)$  steady-state limits are defined by the following relationships:

$$\begin{aligned} F_Q^{RTP} * K(Z)/P & \quad \text{for } P > 0.5 \\ F_Q^{RTP} * K(Z)/0.5 & \quad \text{for } P \leq 0.5 \end{aligned}$$

where,

$$P = (\text{Thermal Power})/(\text{Rated Power})$$

Note: The measured  $F_Q(X,Y,Z)$  shall be increased by 3% to account for manufacturing tolerances and 5% to account for measurement uncertainty when comparing against the LCO limits. The manufacturing tolerance and measurement uncertainty are implicitly included in the  $F_Q$  surveillance limits as defined in COLR Sections 2.6.5 and 2.6.6.

2.6.2  $F_Q^{RTP} = 2.50 \times K(\text{BU})$

2.6.3  $K(Z)$  is the normalized  $F_Q(X,Y,Z)$  as a function of core height. The  $K(Z)$  function for both Mk-BW and Westinghouse RFA fuel is provided in Figure 3.

2.6.4  $K(\text{BU})$  is the normalized  $F_Q(X,Y,Z)$  as a function of burnup.  $K(\text{BU})$  for both MkBW and Westinghouse RFA fuel is 1.0 for all burnups.

The following parameters are required for core monitoring per the Surveillance Requirements of Technical Specification 3.2.1:

2.6.5  $[F_Q^L(X,Y,Z)]^{OP} = \frac{F_Q^D(X,Y,Z) * M_Q(X,Y,Z)}{UMT * MT * TILT}$

where:

$[F_Q^L(X,Y,Z)]^{OP}$  = Cycle dependent maximum allowable design peaking factor that ensures that the  $F_Q(X,Y,Z)$  LOCA limit will be preserved for operation within the LCO limits.  $[F_Q^L(X,Y,Z)]^{OP}$  includes allowances for calculation and measurement uncertainties.

$F_Q^D(X,Y,Z)$  = Design power distribution for  $F_Q$ .  $F_Q^D(X,Y,Z)$  is provided in Table 4, Appendix A, for normal operating conditions and in

## McGuire 2 Cycle 15 Core Operating Limits Report

Table 5, Appendix A for power escalation testing during initial startup operation.

$M_Q(X,Y,Z)$  = Margin remaining in core location X,Y,Z to the LOCA limit in the transient power distribution.  $M_Q(X,Y,Z)$  is provided in Table 4, Appendix A for normal operating conditions and in Table 5, Appendix A for power escalation testing during initial startup operation.

UMT = Total Peak Measurement Uncertainty. (UMT = 1.05)

MT = Engineering Hot Channel Factor. (MT = 1.03)

TILT = Peaking penalty that accounts for the peaking increase from an allowable quadrant power tilt ratio of 1.02. (TILT = 1.035)

Note:  $[F_Q^L(X,Y,Z)]^{OP}$  is the parameter identified as  $F_Q^{MAX}(X,Y,Z)$  in DPC-NE-2011PA.

$$2.6.6 \quad [F_Q^L(X,Y,Z)]^{RPS} = \frac{F_Q^D(X,Y,Z) * M_C(X,Y,Z)}{UMT * MT * TILT}$$

where:

$[F_Q^L(X,Y,Z)]^{RPS}$  = Cycle dependent maximum allowable design peaking factor that ensures that the  $F_Q(X,Y,Z)$  Centerline Fuel Melt (CFM) limit will be preserved for operation within the LCO limits.  $[F_Q^L(X,Y,Z)]^{RPS}$  includes allowances for calculation and measurement uncertainties.

$F_Q^D(X,Y,Z)$  = Design power distributions for  $F_Q$ .  $F_Q^D(X,Y,Z)$  is provided in Table 4, Appendix A for normal operating conditions and in Table 5, Appendix A for power escalation testing during initial startup operation.

## McGuire 2 Cycle 15 Core Operating Limits Report

$M_C(X,Y,Z)$  = Margin remaining to the CFM limit in core location X,Y,Z from the transient power distribution.  $M_C(X,Y,Z)$  calculations parallel the  $M_Q(X,Y,Z)$  calculations described in DPC-NE-2011PA, except that the LOCA limit is replaced with the CFM limit.  $M_C(X,Y,Z)$  is provided in Table 6, Appendix A for normal operating conditions and in Table 7, Appendix A for power escalation testing during initial startup operation.

UMT = Total Peak Measurement Uncertainty (UMT = 1.05)

MT = Engineering Hot Channel Factor (MT = 1.03)

TILT = Peaking penalty that accounts for the peaking increase from an allowable quadrant power tilt ratio of 1.02. (TILT = 1.035)

NOTE:  $[F_Q^L(X,Y,Z)]^{RPS}$  is the parameter identified as  $F_Q^{MAX}(X,Y,Z)$  in DPC-NE-2011PA, except that  $M_Q(X,Y,Z)$  is replaced by  $M_C(X,Y,Z)$ .

### 2.6.7 KSLOPE = 0.0725

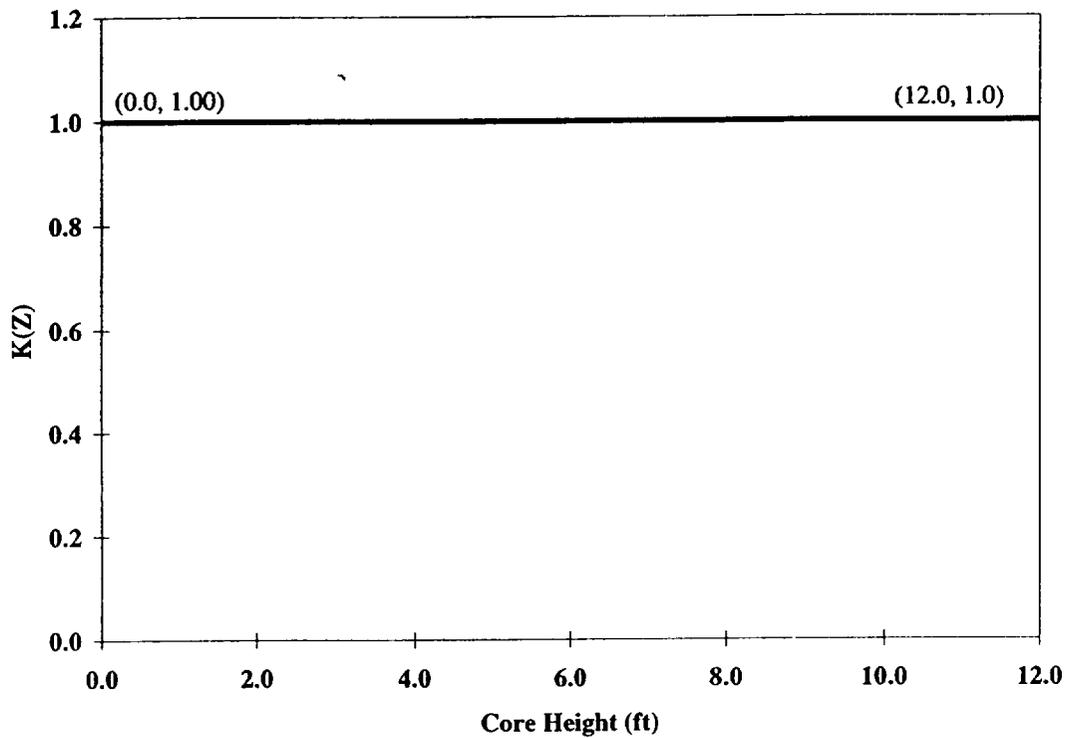
where:

KSLOPE is the adjustment to the  $K_1$  value from the OTΔT trip setpoint required to compensate for each 1% that  $F_Q^M(X,Y,Z)$  exceeds  $[F_Q^L(X,Y,Z)]^{RPS}$ .

### 2.6.8 $F_Q(X,Y,Z)$ penalty factors for Technical Specification Surveillance's 3.2.1.2 and 3.2.1.3 are provided in Table 2.

### McGuire 2 Cycle 15 Core Operating Limits Report

**Figure 3**  
 **$K(Z)$ , Normalized  $F_Q(X, Y, Z)$  as a Function of**  
**Core Height for Mk-BW and Westinghouse RFA Fuel**



## McGuire 2 Cycle 15 Core Operating Limits Report

**Table 2**

**$F_Q(X,Y,Z)$  and  $F_{\Delta H}(X,Y)$  Penalty Factors**

**For Technical Specification Surveillance's 3.2.1.2, 3.2.1.3 and 3.2.2.2**

<b><u>Burnup (EFPD)</u></b>	<b><u><math>F_Q(X,Y,Z)</math> Penalty Factor (%)</u></b>	<b><u><math>F_{\Delta H}(X,Y,Z)</math> Penalty Factor (%)</u></b>
0	2.00	2.00
4	2.97	2.00
12	2.72	2.00
25	2.00	2.00
50	2.00	2.00
75	2.00	2.00
100	2.00	2.00
125	2.00	2.00
150	2.00	2.00
175	2.00	2.00
200	2.00	2.00
225	2.00	2.00
250	2.00	2.00
275	2.00	2.00
300	2.00	2.00
535	2.00	2.00

**Note:** Linear interpolation is adequate for intermediate cycle burnups. All cycle burnups outside of the range of the table shall use a 2% penalty factor for both  $F_Q(X,Y,Z)$  and  $F_{\Delta H}(X,Y)$  for compliance with the Technical Specification Surveillances 3.2.1.2, 3.2.1.3 and 3.2.2.2.

## McGuire 2 Cycle 15 Core Operating Limits Report

### 2.7 Nuclear Enthalpy Rise Hot Channel Factor - $F_{\Delta H}(X,Y)$ (TS 3.2.2)

The  $F_{\Delta H}$  steady-state limits referred to in Technical Specification 3.2.2 is defined by the following relationship.

$$2.7.1 \quad [F_{\Delta H}^L(X, Y)]^{LCO} = \text{MARP}(X, Y) * \left[ 1.0 + \frac{1}{\text{RRH}} * (1.0 - P) \right]$$

where:

$[F_{\Delta H}^L(X, Y)]^{LCO}$  is defined as the steady-state, maximum allowed radial peak.  
 $[F_{\Delta H}^L(X, Y)]^{LCO}$  includes allowances for calculation-measurement uncertainty.

$\text{MARP}(X, Y) =$  Cycle-specific operating limit Maximum Allowable Radial Peaks.  $\text{MARP}(X, Y)$  radial peaking limits are provided in Table 3.

$$P = \frac{\text{Thermal Power}}{\text{Rated Thermal Power}}$$

$\text{RRH} =$  Thermal Power reduction required to compensate for each 1% that the measured radial peak,  $F_{\Delta H}^M(X, Y)$ , exceeds the limit.

$$\text{RRH} = 3.34 \quad (0.0 < P \leq 1.0)$$

The following parameters are required for core monitoring per the Surveillance requirements of Technical Specification 3.2.2.

$$2.7.2 \quad [F_{\Delta H}^L(X, Y)]^{SURV} = \frac{F_{\Delta H}^D(X, Y) \times M_{\Delta H}(X, Y)}{\text{UMR} \times \text{TILT}}$$

where:

$[F_{\Delta H}^L(X, Y)]^{SURV} =$  Cycle dependent maximum allowable design peaking factor that ensures that the  $F_{\Delta H}(X, Y)$  limit will be preserved for operation within the LCO limits.  $[F_{\Delta H}^L(X, Y)]^{SURV}$  includes allowances for calculation-measurement uncertainty.

## McGuire 2 Cycle 15 Core Operating Limits Report

$F_{\Delta H}^D(X,Y)$  = Design radial power distribution for  $F_{\Delta H}$ .  $F_{\Delta H}^D(X,Y)$  is provided in Table 8, Appendix A for normal operation and in Table 9, Appendix A for power escalation testing during initial startup operation.

$M_{\Delta H}(X,Y)$  = The margin remaining in core location X,Y relative to the Operational DNB limits in the transient power distribution.  $M_{\Delta H}(X,Y)$  is provided in Table 8, Appendix A for normal operation and in Table 9, Appendix A for power escalation testing during initial startup operation.

UMR = Uncertainty value for measured radial peaks, (UMR= 1.04). UMR is set to 1.0 since a factor of 1.04 is implicitly included in the variable  $M_{\Delta H}(X,Y)$ .

TILT = Peaking penalty that accounts for the peaking increase for an allowable quadrant power tilt ratio of 1.02, (TILT = 1.035).

NOTE:  $[F_{\Delta H}^L(X,Y)]^{SURV}$  is the parameter identified as  $F_{\Delta H}(X,Y)^{MAX}$  in DPC-NE-2011PA.

### 2.7.3 RRH = 3.34

where:

RRH = Thermal power reduction required to compensate for each 1% that the measured radial peak,  $F_{\Delta H}^M(X,Y)$  exceeds its limit.

### 2.7.4 TRH = 0.04

where:

TRH = Reduction in the OTΔT  $K_1$  setpoint required to compensate for each 1% that the measured radial peak,  $F_{\Delta H}^M(X,Y)$  exceeds its limit.

2.7.5  $F_{\Delta H}(X,Y)$  penalty factors for Technical Specification Surveillance 3.2.2.2 are provided in Table 2.

## 2.8 Axial Flux Difference – AFD (TS 3.2.3)

2.8.1 The Axial Flux Difference (AFD) Limits are provided in Figure 4.

**McGuire 2 Cycle 15 Core Operating Limits Report**

**Table 3  
Maximum Allowable Radial Peaks (MARPS)  
(Applicable to Both MkBW and RFA Fuel)**

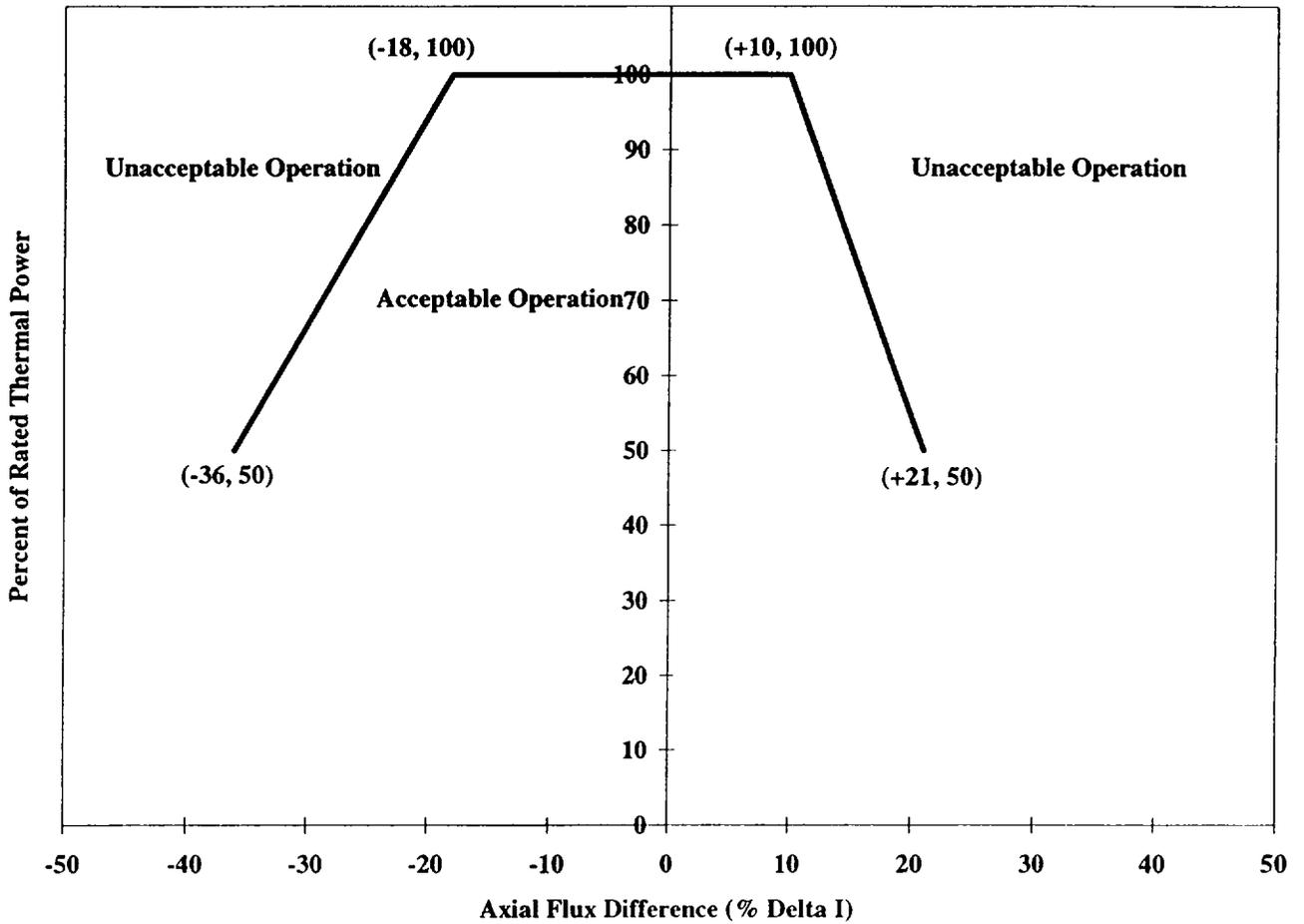
<u>Core Ht. (ft)</u>	<u>Axial Peak -----&gt;</u>						
	<u>1.05</u>	<u>1.10</u>	<u>1.20</u>	<u>1.30</u>	<u>1.40</u>	<u>1.50</u>	<u>1.60</u>
0.12	1.687	1.716	1.782	1.838	1.888	1.933	1.863
1.20	1.684	1.715	1.776	1.830	1.878	1.896	1.839
2.40	1.683	1.711	1.767	1.819	1.858	1.845	1.789
3.60	1.681	1.707	1.758	1.802	1.810	1.795	1.742
4.80	1.678	1.701	1.747	1.785	1.759	1.744	1.692
6.00	1.674	1.695	1.733	1.748	1.703	1.692	1.643
7.20	1.669	1.687	1.716	1.696	1.649	1.633	1.587
8.40	1.664	1.675	1.685	1.643	1.595	1.579	1.534
9.60	1.656	1.660	1.635	1.585	1.543	1.529	1.487
10.80	1.645	1.633	1.587	1.535	1.488	1.476	1.434
12.00	1.620	1.592	1.538	1.490	1.442	1.432	1.394

<u>Core Ht. (ft)</u>	<u>Axial Peak -----&gt;</u>					
	<u>1.70</u>	<u>1.80</u>	<u>1.90</u>	<u>2.10</u>	<u>3.00</u>	<u>3.25</u>
0.12	1.807	1.723	1.645	1.543	1.218	1.153
1.20	1.815	1.740	1.664	1.548	1.188	1.123
2.40	1.772	1.715	1.659	1.561	1.170	1.108
3.60	1.721	1.667	1.617	1.555	1.213	1.141
4.80	1.674	1.624	1.574	1.510	1.227	1.182
6.00	1.627	1.579	1.533	1.465	1.197	1.148
7.20	1.571	1.527	1.488	1.424	1.165	1.116
8.40	1.522	1.479	1.440	1.373	1.134	1.089
9.60	1.476	1.436	1.399	1.337	1.110	1.065
10.80	1.427	1.390	1.355	1.294	1.075	1.033
12.00	1.389	1.356	1.327	1.273	1.061	1.017

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Figure 4

Percent of Rated Thermal Power Versus Percent Axial Flux Difference Limits



**NOTE:** Compliance with Technical Specification 3.2.1 may require more restrictive AFD limits. Refer to OP/2/A/6100/22 Unit 2 Data Book of more details.

**McGuire 2 Cycle 15 Core Operating Limits Report**

**2.9 Reactor Trip System Instrumentation Setpoints (TS 3.3.1) Table 3.3.1-1**

**2.9.1 Overtemperature  $\Delta T$  Setpoint Parameter Values**

<u>Parameter</u>	<u>Value</u>
Overtemperature $\Delta T$ reactor trip setpoint	$K_1 \leq 1.1978$
Overtemperature $\Delta T$ reactor trip heatup setpoint penalty coefficient	$K_2 = 0.0334/^{\circ}\text{F}$
Overtemperature $\Delta T$ reactor trip depressurization setpoint penalty coefficient	$K_3 = 0.001601/\text{psi}$
Time constants utilized in the lead-lag compensator for $\Delta T$	$\tau_1 \geq 8 \text{ sec.}$ $\tau_2 \leq 3 \text{ sec.}$
Time constant utilized in the lag compensator for $\Delta T$	$\tau_3 \leq 2.0 \text{ sec.}$
Time constants utilized in the lead-lag compensator for $T_{\text{avg}}$	$\tau_4 \geq 28 \text{ sec.}$ $\tau_5 \leq 4 \text{ sec.}$
Time constant utilized in the measured $T_{\text{avg}}$ lag compensator	$\tau_6 \leq 2.0 \text{ sec.}$
$f_1(\Delta I)$ "positive" breakpoint	$= 19.0 \% \Delta I$
$f_1(\Delta I)$ "negative" breakpoint	$= \text{N/A}^*$
$f_1(\Delta I)$ "positive" slope	$= 1.769 \% \Delta T / \% \Delta I$
$f_1(\Delta I)$ "negative" slope	$= \text{N/A}^*$

\* The  $f_1(\Delta I)$  "negative" breakpoint and the  $f_1(\Delta I)$  "negative" slope are not applicable since the  $f_1(\Delta I)$  function is not required below the  $f_1(\Delta I)$  "positive" breakpoint of 19.0%  $\Delta I$ .

## McGuire 2 Cycle 15 Core Operating Limits Report

### 2.9.2 Overpower $\Delta T$ Setpoint Parameter Values

<u>Parameter</u>	<u>Value</u>
Overpower $\Delta T$ reactor trip setpoint	$K_4 \leq 1.086359$
Overpower $\Delta T$ reactor trip heatup setpoint penalty coefficient	$K_6 = 0.001179/^\circ\text{F}$
Time constants utilized in the lead-lag compensator for $\Delta T$	$\tau_1 \geq 8 \text{ sec.}$ $\tau_2 \leq 3 \text{ sec.}$
Time constant utilized in the lag compensator for $\Delta T$	$\tau_3 \leq 2.0 \text{ sec.}$
Time constant utilized in the measured $T_{\text{avg}}$ lag compensator	$\tau_6 \leq 2.0 \text{ sec.}$
Time constant utilized in the rate-lag controller for $T_{\text{avg}}$	$\tau_7 \geq 5 \text{ sec.}$
$f_2(\Delta I)$ "positive" breakpoint	$= 35.0 \% \Delta I$
$f_2(\Delta I)$ "negative" breakpoint	$= -35.0 \% \Delta I$
$f_2(\Delta I)$ "positive" slope	$= 7.0 \% \Delta T_{\text{d}} / \% \Delta I$
$f_2(\Delta I)$ "negative" slope	$= 7.0 \% \Delta T_{\text{d}} / \% \Delta I$

## McGuire 2 Cycle 15 Core Operating Limits Report

### 2.10 Accumulators (TS 3.5.1)

#### 2.10.1 Boron concentration limits during modes 1 and 2, and mode 3 with RCS pressure >1000 psi:

<u>Parameter</u>	<u>Limit</u>
Cold Leg Accumulator minimum boron concentration.	2,475 ppm
Cold Leg Accumulator maximum boron concentration.	2,875 ppm

### 2.11 Refueling Water Storage Tank - RWST (TS 3.5.4)

#### 2.11.1 Boron concentration limits during modes 1, 2, 3, and 4:

<u>Parameter</u>	<u>Limit</u>
Refueling Water Storage Tank minimum boron concentration.	2,675 ppm
Refueling Water Storage Tank maximum boron concentration.	2,875 ppm

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### 2.12 Spent Fuel Pool Boron Concentration (TS 3.7.14)

2.12.1 Minimum boron concentration limit for the spent fuel pool. Applicable when fuel assemblies are stored in the spent fuel pool.

<u>Parameter</u>	<u>Limit</u>
Spent fuel pool minimum boron concentration.	2,675 ppm

### 2.13 Refueling Operations - Boron Concentration (TS 3.9.1)

2.13.1 Minimum boron concentration limit for the filled portions of the Reactor Coolant System, refueling canal, and refueling cavity for mode 6 conditions. The minimum boron concentration limit and plant refueling procedures ensure that the Keff of the core will remain within the mode 6 reactivity requirement of  $K_{eff} \leq 0.95$ .

<u>Parameter</u>	<u>Limit</u>
Minimum Boron concentration of the Reactor Coolant System, the refueling canal, and the refueling cavity.	2,675 ppm

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### 2.14 Borated Water Source – Shutdown (SLC 16.9.14)

#### 2.14.1 Volume and boron concentrations for the Boric Acid Tank (BAT) and the Refueling Water Storage Tank (RWST) during modes 5 and 6.

<u>Parameter</u>	<u>Limit</u>
Boric Acid Tank minimum contained borated water volume	10,599 gallons 13.6% Level
Note: When cycle burnup is > 455 EFPD, Figure 6 may be used to determine the required BAT minimum level.	
Boric Acid Tank minimum boron concentration	7,000 ppm
Boric Acid Tank minimum water volume required to maintain SDM at 7,000 ppm	2,300 gallons
Refueling Water Storage Tank minimum contained borated water volume	47,700 gallons 41 inches
Refueling Water Storage Tank minimum boron concentration	2,675 ppm
Refueling Water Storage Tank minimum water volume required to maintain SDM at 2,675 ppm	8,200 gallons

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### 2.15 Borated Water Source - Operating (SLC 16.9.11)

#### 2.15.1 Volume and boron concentrations for the Boric Acid Tank (BAT) and the Refueling Water Storage Tank (RWST) during modes 1, 2, 3, and mode 4:

<u>Parameter</u>	<u>Limit</u>
Boric Acid Tank minimum contained borated water volume	22,049 gallons 38.0% Level
<div style="border: 1px solid black; padding: 5px; margin: 10px auto; width: fit-content;"> <p>Note: When cycle burnup is &gt; 455 EFPD, Figure 6 may be used to determine the required BAT minimum level.</p> </div>	
Boric Acid Tank minimum boron concentration	7,000 ppm
Boric Acid Tank minimum water volume required to maintain SDM at 7,000 ppm	13,750 gallons
Refueling Water Storage Tank minimum contained borated water volume	96,607 gallons 103.6 inches
Refueling Water Storage Tank minimum boron concentration	2,675 ppm
Refueling Water Storage Tank maximum boron concentration (TS 3.5.4)	2875 ppm
Refueling Water Storage Tank minimum water volume required to maintain SDM at 2,675 ppm	57,107 gallons

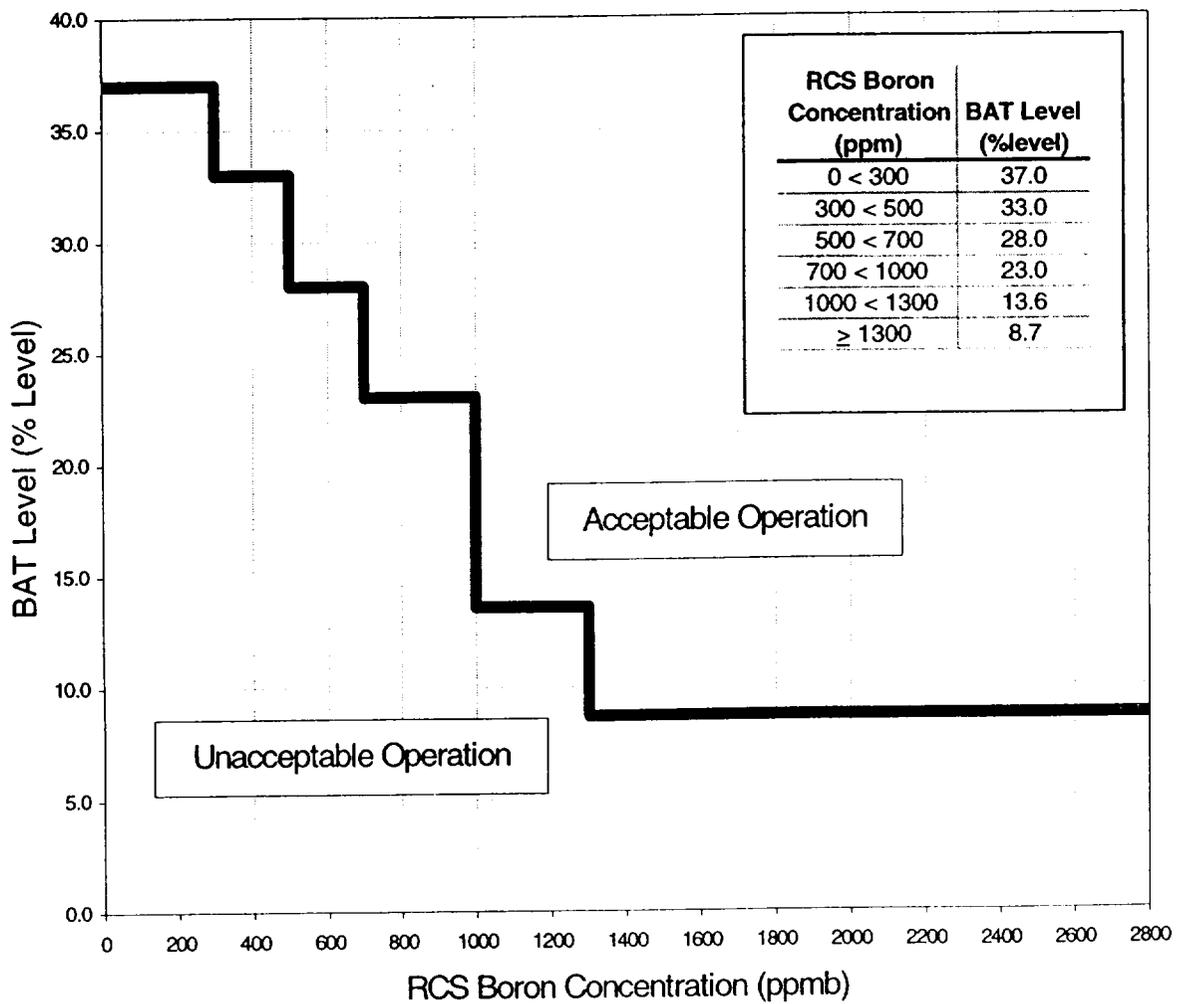
### McGuire 2 Cycle 15 Core Operating Limits Report

Figure 6

#### Boric Acid Storage Tank Indicated Level Versus RCS Boron Concentration

(Valid When Cycle Burnup is > 455 EFPD)

This figure includes additional volumes listed in SLC 16.9.14 and 16.9.11



## McGuire 2 Cycle 15 Core Operating Limits Report

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**NOTE:** Data contained in the Appendix to this document was generated in the McGuire 2 Cycle 15 Maneuvering Analysis calculation file, MCC-1553.05-00-0349. The Plant Nuclear Engineering Section will control this information via computer file(s) and should be contacted if there is a need to access this information.