WOLF CREEK
NUCLEAR OPERATING CORPORATION

Warren B. Wood
General Counsel and Secretary

MAR 7 2002

GC 02-0011

U. S. Nuclear Regulatory Commission
ATTN: Document Control Desk
Washington, D. C. 20555

References: 1. Letter ET 01-0008 dated April 3, 2001, from R. A. Muench, WCNOC, to USNRC

2. Letter ET 01-0030 dated October 22, 2001, from R. A. Muench, WCNOC, to USNRC

3. Letter ET 01-0036 dated December 18, 2001, from R. A. Muench, WCNOC, to USNRC.

Subject: Docket No. 50-482: Supplemental Information for the Relocation of Technical Specification Cycle Specific Parameters to the Core Operating Limits Report

Gentlemen:

Reference 1 proposed changes to relocated Reactor Coolant System (RCS) related cycle-specific parameter limits from the Technical Specifications to the CORE OPERATING LIMITS REPORT (COLR). The justification to implement the expansion of the COLR is provided in Westinghouse WCAP-14483-A, "Generic Methodology for Expanding Core Operating Limits Report." The changes proposed in Reference 1 are consistent with Nuclear Regulatory Commission (NRC) approved Industry/Technical Specification Task Force (TSTF) Standard Technical Specification Change Traveler, TSTF-339, Rev. 2. References 2 and 3 provided supplemental information in response to questions raised by the Staff.

On February 28, 2002, Wolf Creek Nuclear Operating Corporation (WCNOC) personnel identified a potential error with the proposed change to the $f_1(\Delta I)$ equation in Technical Specification Table 3.3.1-1. The current $f_1(\Delta I)$ equation is specified, in part, as follows:

$$f_1(\Delta I) \qquad -0.0227 \{ 23\% + (q_t - q_b)\} \qquad \text{when } q_t - q_b < -23\% \text{ RTP}$$

Reference 1 proposed to change the "+" sign to a "-" sign. This change was based on a proposed method of defining the $f_1(\Delta I)$ breakpoints and slopes in the COLR. Upon further review it was identified that the change proposed to the $f_1(\Delta I)$ equation would result in an inconsistent application of the breakpoints and slopes.

A001

The Attachment provides a revised markup of Technical Specification page 3.3-19. The correction to the proposed changes to the Technical Specifications do not impact the conclusions of the No Significant Hazards Consideration Determination provided in Reference 1.

A copy of this correspondence, with attachment, is being provided to the designated Kansas State Official. There are no regulatory commitments contained in this submittal. If you should have any questions regarding this submittal, please contact me at (620) 364-8831, extension 4005, or Mr. Tony Harris at (620) 364-4038.

Very truly yours,

Warren B. Wood

WBW/rlr
Attachment

cc: V. L. Cooper (KDHE), w/a
        J. N. Donohew (NRC), w/a
        D. N. Graves (NRC), w/a
        E. W. Merschoff (NRC), w/a
        Senior Resident Inspector (NRC), w/a

STATE OF KANSAS   )
) SS
COUNTY OF COFFEY)

Warren B. Wood, of lawful age, being first duly sworn upon oath says that he is General Counsel and Secretary of Wolf Creek Nuclear Operating Corporation; that he has read the foregoing document and knows the contents thereof; that he has executed the same for and on behalf of said Corporation with full power and authority to do so; and that the facts therein stated are true and correct to the best of his knowledge, information and belief.

By _Warren B. Wood_

Warren B. Wood
General Counsel and Secretary

SUBSCRIBED and sworn to before me this 6th day of March , 2002.

Cindy Novinger
Notary Public

Expiration Date _July 8, 2002_

ATTACHMENT I

TECHNICAL SPECIFICATION CORRECTION

Table 3.3.1-1 (page 5 of 6)
Reactor Trip System Instrumentation

Note 1: Overtemperature ΔT

The Overtemperature ΔT Function Allowable Value shall not exceed the following Trip Setpoint by more than 1.3% of ΔT span.

$$\Delta T \frac{(1+\tau_1 s)}{(1+\tau_2 s)}\left(\frac{1}{1+\tau_3 s}\right) \le \Delta T_0 \left\{ K_1 - K_2 \frac{(1+\tau_4 s)}{(1+\tau_5 s)}\left[T\left(\frac{1}{(1+\tau_6 s)}\right) - T' \right] + K_3 (P - P') - f_1(\Delta I) \right\}$$

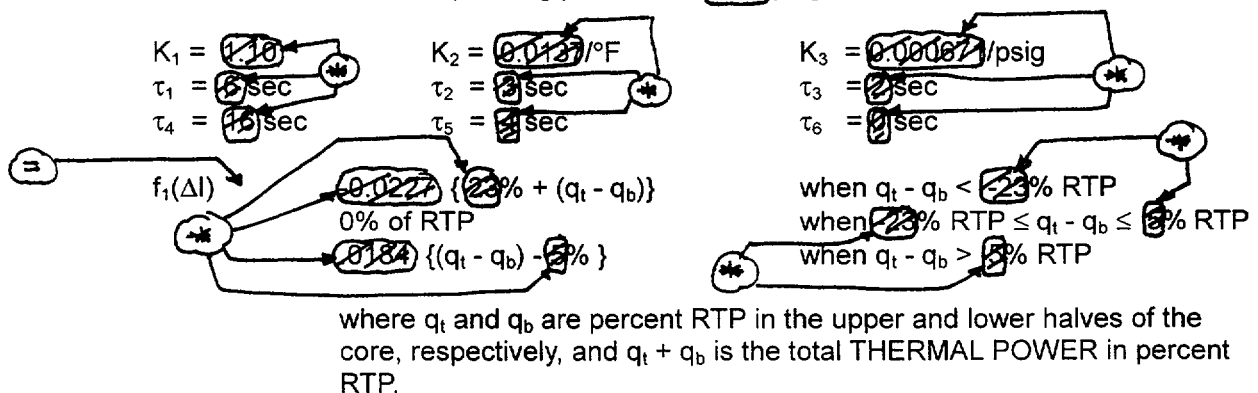Where: ΔT is measured RCS ΔT, °F.

ΔT$_0$ is the indicated ΔT at RTP, °F.

s is the Laplace transform operator, sec^{-1}.

T is the measured RCS average temperature, °F.

T′ is the nominal T$_{avg}$ at RTP, ≤ 588.5 °F.

P is the measured pressurizer pressure, psig.

P′ is the nominal RCS operating pressure ≥ 2235 psig.

K_1 = 1.10 K_2 = 0.0137 /°F K_3 = 0.000671 /psig

τ_1 = 8 sec τ_2 = 3 sec τ_3 = 2 sec

τ_4 = 15 sec τ_5 = 4 sec τ_6 = 2 sec

$f_1(\Delta I)$ 0.022 {23% + (q$_t$ - q$_b$)}   when q$_t$ - q$_b$ < 23% RTP

0% of RTP   when 23% RTP ≤ q$_t$ - q$_b$ ≤ 8% RTP

0.184 {(q$_t$ - q$_b$) - 8% }   when q$_t$ - q$_b$ > 8% RTP

where q$_t$ and q$_b$ are percent RTP in the upper and lower halves of the core, respectively, and q$_t$ + q$_b$ is the total THERMAL POWER in percent RTP.

The values denoted with * are specified in the COLR.