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12.0 OPERATING CONTROLS AND LIMITS

This chapter identifies operating controls and limits, technical parameters and surveillance requirements imposed to ensure the safe operation of the NAC-UMS[®] System.

Controls used by NAC International (NAC) as part of the NAC-UMS[®] design and fabrication are provided in the NAC Quality Assurance Manual and Quality Procedure. The NAC Quality Assurance Program is discussed in Chapter 13. If procurement and fabrication of the NAC-UMS[®] System is performed by others, a Quality Assurance Program prepared in accordance with 10 CFR 72 Subpart G shall be implemented. Site specific controls for the organization, administrative system, procedures, record keeping, review, audit and reporting necessary to ensure that the NAC-UMS[®] storage system installation is operated in a safe manner, are the responsibility of the user of the system.

12.1 Administrative and Operating Controls and Limits for the NAC-UMS[®] System

The NAC-UMS[®] Storage System is provided in the Standard and Advanced configurations. The Standard NAC-UMS[®] Storage System operating controls and limits are summarized in Table 12-1. The Advanced NAC-UMS[®] Storage System operating controls and limits are summarized in Table 12-2. Appendix 12A provides the proposed Limiting Conditions for Operations (LCO). The Approved Contents and Design Features for the NAC-UMS[®] System are presented in Technical Specification format. The bases for the specified controls and limits are presented in Appendix 12C.

Section 3.0 Appendix 12B presents Design Features that are important to the safe operation of the NAC-UMS[®] System, but that are not included as Technical Specifications. These include items which are singular events, those that cannot be readily determined or re-verified at the time of use of the system, or that are easily implemented, verified and corrected, if necessary, at the time the action is undertaken.

12.2 Administrative and Operating Controls and Limits for SITE SPECIFIC FUEL

This section describes the administrative and operating controls and limits placed on the loading of fuel assemblies that are unique to specific reactor sites. SITE SPECIFIC FUEL configurations result from conditions that occurred during reactor operations, participation in research and

development programs, testing programs intended to improve reactor operations, from the placement of control components or other items within the fuel assembly and from the disposition of damaged fuel assemblies or fuel rods.

SITE SPECIFIC FUEL assembly configurations are either shown to be bounded by the analysis of the design basis fuel configuration of the same type (PWR or BWR), or are shown to be acceptable contents by specific evaluation of the configuration. Separate evaluation may establish different limits, which are maintained by administrative controls for preferential loading. The preferential loading controls take advantage of design features to allow the loading of fuel configurations that may have higher burnup or additional hardware material that is not specifically considered in the design basis fuel evaluation.

Unless specifically excepted, SITE SPECIFIC FUEL must meet all of the conditions specified in either Table 12-1 for the Standard configuration or in Table 12-2 for the Advanced configuration.

12.2.1 Operating Controls and Limits for Maine Yankee SITE SPECIFIC FUEL

Maine Yankee fuel is stored in the Standard configuration of the NAC-UMS[®] Storage System. The fuel design used at Maine Yankee is the Combustion Engineering (CE) 14×14 fuel assembly. The CE 14×14 fuel assembly is one of those included in the design basis evaluation of the UMS[®] Storage System as shown in Table 12B2-2. The estimated Maine Yankee SITE SPECIFIC FUEL inventory is shown in Table 12B2-6. Except as noted in this section, the spent fuel in this inventory meets the Fuel Assembly Limits provided in Table 12B2-1.

As shown in Table 12B2-6, certain of the Maine Yankee fuel has characteristics, such as fuel assembly lattice configurations, different from STANDARD FUEL, from PWR INTACT FUEL ASSEMBLIES - including CONSOLIDATED FUEL, DAMAGED FUEL and fuel with higher burnup or enrichment, that differs from the characteristics of the fuel considered in the design basis. As shown in Table 12B2-6, certain fuel configurations must be preferentially loaded in corner or peripheral fuel tube positions in the fuel basket based on the shielding, criticality or thermal evaluation of the fuel configuration.

The corner positions are used for the loading of fuel configurations with missing fuel rods, and for DAMAGED FUEL and CONSOLIDATED FUEL in the MAINE YANKEE FUEL CAN. Specification for placement in the corner fuel tube positions results primarily from shielding or criticality evaluations of the designated fuel configurations.

Spent fuel having a burnup from 45,000 to 50,000 MWD/MTU is assigned to peripheral locations, and based on a cladding oxide layer thickness determination, may require loading in a Maine Yankee fuel can. The interior locations must be loaded with fuel that has lower burnup and/or longer cool times in order to maintain the design basis heat load and component temperature limits for the basket and canister.

The Fuel Assembly Limits for the Maine Yankee SITE SPECIFIC FUEL are shown in Table 12B2-7. Part A of the table lists the STANDARD, INTACT FUEL ASSEMBLY and SITE SPECIFIC FUEL that does not require preferential loading except as required by Section B 2.1.2 to assure that short-term fuel cladding temperature limits are not exceeded.

Part B of the table lists the SITE SPECIFIC FUEL configurations that require preferential loading due to the criticality, shielding or thermal evaluation. The loading pattern for Maine Yankee SITE SPECIFIC FUEL that must be preferentially loaded is presented in Section B 2.1.3. The preferential loading controls take advantage of design features of the UMS[®] Storage System to allow the loading of fuel configurations that may have higher burnup or additional hardware or fuel source material that is not specifically considered in the design basis fuel evaluation. The preferential loading required by Part B must also consider the preferential loading requirements of Section B 2.1.2 for short-term cladding temperature limits.

Fuel assemblies with a Control Element Assembly (CEA) or a CEA plug inserted are loaded in a Class 2 canister and basket due to the increased length of the assembly with either of these components installed. However, these assemblies are not restricted as to loading position within the basket.

The Transportable Storage Canister loading procedures for Maine Yankee SITE SPECIFIC FUEL will indicate that the loading of a fuel configuration with removed fuel or poison rods, or a MAINE YANKEE FUEL CAN, or fuel with burnup between 45,000 MWD/MTU and 50,000 MWD/MTU, is administratively controlled in accordance with the requirements of Section B 2.1.3.

	Applicable Technical			
Control or Limit	Specification	Condition or Item Controlled		
1. Fuel Characteristics	Table 12B2-1	Type and Condition		
	Table 12B2-2	Class, Dimensions and Weight for PWR Fuel		
	Table 12B2-3	Class, Dimensions and Weight for BWR Fuel		
	Table 12B2-4	Minimum Cooling Time for PWR Fuel		
	Table 12B2-5	Minimum Cooling Time for BWR Fuel		
	Table 12B2-7	Maine Yankee SITE SPECIFIC Loading		
	Table 12B2-8	Minimum Cooling Time for Maine Yankee Fuel – No CEA		
	Table 12B2-9	Minimum Cooling Time for Maine Yankee Fuel – With CEA		
2. Canister	LCO 3.1.4	Time in Transfer Cask		
Fuel Loading	Table 12B2-1	Weight and Number of Assemblies		
	Table 12B2-7	Maine Yankee Site Specific Fuel Loading		
	Table 12B2-4	Minimum Cooling Time for PWR Fuel		
	Table 12B2-5	Minimum Cooling Time for BWR Fuel		
Drying	LCO 3.1.2	Vacuum Drying Pressure		
Backfilling	LCO 3.1.3	Helium Backfill Pressure		
Sealing	LCO 3.1.5	Helium Leak Rate		
Vacuum	LCO 3.1.1	Time in Vacuum Drying		
External Surface	LCO 3.2.1	Level of Contamination		
Unloading	Note 1	Fuel Cooldown Requirement		
3. Concrete Cask	LCO 3.2.2	Surface Dose Rates		
	Note 1	Cask Spacing		
	Note 2	Cask Handling Height		
4. Surveillance	LCO 3.1.6	Heat Removal System		
5. Transfer Cask	B3.4.1(8)	Minimum Temperature		
	LCO 3.1.7	Canister Removal from the CONCRETE Cask		
6. ISFSI Concrete Pad	B3.4.1(6)	Seismic Event Performance		

Table 12-1 NAC-UMS[®] Standard System Controls and Limits

1. Procedure and/or limits are presented in the Operating Procedures of Chapter 8.

2. Lifting height and handling restrictions are provided in Section A5.6 of Appendix 12A.

	Applicable	
Control or Limit	Specification	Condition or Item Controlled
1. Fuel Characteristics	Table 12B2-1	Type and Condition
	Table 12B2-10	Class, Dimensions and Characteristics for PWR Fuel
	Table 12B2-11	Minimum Cooling Time for 700 Watt PWR Fuel
	Table 12B2-12	Minimum Cooling Time for 1,000 Watt PWR Fuel
	Table 12B2-13	Minimum Cooling Time for 1,100 Watt PWR Fuel
2. Canister	LCO 3.1.9	Time in Transfer Cask
Fuel Loading	Table 12B2-4	Weight and Number of Assemblies
	Table 12B2-11	Minimum Cooling Time for PWR Fuel
	Table 12B2-12	Minimum Cooling Time for PWR Fuel
	Table 12B2-13	Minimum Cooling Time for PWR Fuel
Drying	LCO 3.1.2	Vacuum Drying Pressure
Backfilling	LCO 3.1.3	Helium Backfill Pressure
Sealing	LCO 3.1.5	Helium Leak Rate
Vacuum	LCO 3.1.8	Time in Vacuum Drying
External Surface	LCO 3.2.1	Level of Contamination
Unloading	Note 1	Fuel Cooldown Requirement
3. Concrete Cask	LCO 3.2.2	Surface Dose Rates
	Note 1	Cask Spacing
	Note 2	Cask Handling Height
4. Surveillance	LCO 3.1.6	Heat Removal System
5. Transfer Cask	B3.4.1(8)	Minimum Temperature
	LCO 3.1.10	Canister Removal from the CONCRETE Cask
6. ISFSI Concrete Pad	B3.4.1(6)	Seismic Event Performance

Table 12-2	NAC-UMS [®]	Advanced Sy	stem Controls	and Limits
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1. Procedure and/or limits are presented in the Operating Procedures of Chapter 8.

2. Lifting height and handling restrictions are provided in Section A5.6 of Appendix 12A.

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APPENDIX 12A

TECHNICAL SPECIFICATIONS FOR THE NAC-UMS[®] SYSTEM

AMENDMENT NO. 2

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Definitions A 1.1

A 1.0 USE AND APPLICATION

A 1.1 Definitions

-----NOTE-----The defined terms of this section appear in capitalized type and are applicable throughout this Chapter 12. Definition Term ACTIONS shall be that part of a Specification that **ACTIONS** prescribes Required Actions to be taken under designated Conditions within specified Completion Times. See TRANSPORTABLE STORAGE CANISTER CANISTER The CANISTER HANDLING FACILITY includes CANISTER HANDLING FACILITY the following components and equipment: (1) a canister transfer station that allows the staging of the TRANSFER CASK with the CONCRETE CASK or transport cask to facilitate CANISTER lifts involving spent fuel handling not covered by 10 CFR 50; and (2) either a stationary lift device or mobile lifting device used to lift the TRANSFER CASK and CANISTER. See VERTICAL CONCRETE CASK CONCRETE CASK The facility within the perimeter fence licensed for INDEPENDENT SPENT FUEL storage of spent fuel within NAC-UMS® SYSTEMs STORAGE INSTALLATION (see also 10 CFR 72.3). (ISFSI) A fuel assembly or fuel rod with no fuel rod cladding INTACT FUEL defects, or with known or suspected fuel rod cladding (ASSEMBLY OR ROD) defects not greater than pinhole leaks or hairline (Undamaged Fuel) cracks.

FSAR – UMS[®] Universal Storage System Docket No. 72-1015

January 2002 **Revision UMSS-02A**

> Definitions A 1.1

LOADING

transfer

Term LOADING OPERATIONS

INITIAL PEAK PLANAR-AVERAGE ENRICHMENT

NAC-UMS[®] SYSTEM

OPERABLE

NAC-UMS[®] SYSTEM is secured on the transporter. LOADING OPERATIONS does not include poststorage operations, i.e., CANISTER operations between the TRANSFER CASK and the CONCRETE CASK or transport cask after STORAGE OPERATIONS.

being loaded with fuel assemblies.

LOADING OPERATIONS include all licensed activities on an NAC-UMS[®] SYSTEM while it is

OPERATIONS begin when the first fuel assembly is placed in the CANISTER and end when the

Definition

THE INITIAL PEAK PLANAR-AVERAGE ENRICHMENT is the maximum planar-average enrichment at any height along the axis of the fuel assembly. The 4.0 wt % ²³⁵U enrichment limit for BWR fuel applies along the full axial extent of the assembly. The INITIAL PEAK PLANAR-AVERAGE ENRICHMENT may be higher than the bundle (assembly) average enrichment.

NAC-UMS[®] SYSTEM includes the components approved for loading and storage of spent fuel assemblies at the ISFSI. The NAC-UMS® SYSTEM consists of a CONCRETE CASK, a TRANSFER CASK, and a CANISTER and is provided in the Standard and Advanced configurations.

The CONCRETE CASK heat removal system is OPERABLE if the difference between the ISFSI ambient temperature and the average outlet air temperature is $\leq 102^{\circ}$ F for the Standard PWR CANISTER, \leq 92°F for the Standard BWR CANISTER, or $\leq 112^{\circ}$ F for the Advanced PWR CANISTER.

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January 2002 Revision UMSS-02A

> Definitions A 1.1

	<u>A1.1</u>
Term	Definition
STORAGE OPERATIONS	STORAGE OPERATIONS include all licensed activities that are performed at the ISFSI, while an NAC-UMS [®] SYSTEM containing spent fuel is located on the storage pad within the ISFSI perimeter.
TRANSFER CASK	TRANSFER CASK is a shielded lifting device that holds the CANISTER during LOADING and UNLOADING OPERATIONS and during closure welding, vacuum drying, leak testing, and non- destructive examination of the CANISTER closure welds. The TRANSFER CASK is also used to transfer the CANISTER into and from the CONCRETE CASK and into the transport cask. The TRANSFER CASK is provided in the Standard, Advanced and 100-ton configurations. The three configurations are operationally similar.
TRANSPORT OPERATIONS	TRANSPORT OPERATIONS include all licensed activities involved in moving a loaded NAC-UMS [®] CONCRETE CASK and CANISTER to and from the ISFSI. TRANSPORT OPERATIONS begin when the NAC-UMS [®] SYSTEM is first secured on the transporter and end when the NAC-UMS [®] SYSTEM is at its destination and no longer secured on the transporter.
TRANSPORTABLE STORAGE CANISTER (CANISTER)	TRANSPORTABLE STORAGE CANISTER is the sealed container that consists of a fuel basket in a cylindrical canister shell that is welded to a baseplate, shield lid with welded port covers, and structural lid. The CANISTER provides the confinement boundary for the confined spent fuel. The CANISTER is provided in either the Standard or Advanced configurations. The CANISTER configurations are operationally identical.
Standard CANISTER	The Standard CANISTER holds a fuel tube and disk design basket having either 24 PWR loading positions or 56 BWR loading positions.
Advanced CANISTER	The Advanced CANISTER holds a tab and slot design basket having 32 PWR fuel loading positions.
	(continued)

Definitions A 1.1

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Term	Definition
TRANSFER OPERATIONS	TRANSFER OPERATIONS include all licensed activities involved in transferring a loaded CANISTER from a CONCRETE CASK to another CONCRETE CASK or to a TRANSPORT CASK.
UNLOADING OPERATIONS	UNLOADING OPERATIONS include all licensed activities on a NAC-UMS [®] SYSTEM to be unloaded of the contained fuel assemblies. UNLOADING OPERATIONS begin when the NAC-UMS [®] SYSTEM is no longer secured on the transporter and end when the last fuel assembly is removed from the NAC-UMS [®] SYSTEM.
VERTICAL CONCRETE CASK (CONCRETE CASK)	VERTICAL CONCRETE CASK is the cask that receives and holds the sealed CANISTER. It provides the gamma and neutron shielding and convective cooling of the spent fuel confined in the CANISTER. The CONCRETE CASK is provided in either the Standard or Advanced configurations. The two configurations are operationally identical.
Standard CONCRETE CASK	The Standard CONCRETE CASK stores only the Standard CANISTER.
Advanced CONCRETE CASK	The Advanced CONCRETE CASK may store either the Standard or Advanced CANISTER.
STANDARD FUEL	Irradiated fuel assemblies having the same configuration as when originally fabricated consisting generally of the end fittings, fuel rods, guide tubes, and integral hardware. For BWR fuel, the channel is considered to be integral hardware. The design basis fuel characteristics and analysis are based on the STANDARD FUEL configuration.

Definitions A 1.1

Term	Definition
DAMAGED FUEL	A fuel assembly or fuel rod with known or suspected cladding defects greater than pinhole leaks or hairline cracks.
	DAMAGED FUEL must be placed in a MAINE YANKEE FUEL CAN in the Standard CANISTER.
HIGH BURNUP FUEL	A fuel assembly having a burnup greater than 45,000 MWD/MTU.
	An intact HIGH BURNUP FUEL assembly in which no more than 1% of the fuel rods in the assembly have a peak cladding oxide thickness greater than 80 microns, and in which no more than 3% of the fuel rods in the assembly have a peak oxide layer thickness greater than 70 microns, as determined by measurement and statistical analysis, may be stored as INTACT FUEL.
	HIGH BURNUP FUEL assemblies not meeting the cladding oxide thickness criteria for INTACT FUEL or that have an oxide layer that has become detached or spalled from the cladding are stored as DAMAGED FUEL.
Maine Yankee HIGH BURNUP FUEL (45,000 <burnup 50,000)<="" td="" ≤=""><td>HIGH BURNUP FUEL which must be preferentially loaded in periphery positions of the Standard basket. HIGH BURNUP FUEL classified as damaged must be loaded in the MAINE YANKEE FUEL CAN.</td></burnup>	HIGH BURNUP FUEL which must be preferentially loaded in periphery positions of the Standard basket. HIGH BURNUP FUEL classified as damaged must be loaded in the MAINE YANKEE FUEL CAN.
Advanced Configuration HIGH BURNUP FUEL (45,000 <burnup 55,000)<="" td="" ≤=""><td>HIGH BURNUP FUEL which must be preferentially loaded in the Advanced basket based on fuel assembly heat load.</td></burnup>	HIGH BURNUP FUEL which must be preferentially loaded in the Advanced basket based on fuel assembly heat load.
FUEL DEBRIS	An intact or a partial fuel rod or an individual intact or partial fuel pellet not contained in a fuel rod. Fuel debris is inserted into a 9×9 array of tubes in a lattice that has approximately the same dimensions as a standard fuel assembly. FUEL DEBRIS is stored in a MAINE YANKEE FUEL CAN in the Standard CANISTER.

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> Definitions A 1.1

<u>Term</u>

CONSOLIDATED FUEL

SITE SPECIFIC FUEL

Definition

A nonstandard fuel configuration in which the individual fuel rods from one or more fuel assemblies are placed in a single container or a lattice structure that is similar to a fuel assembly. CONSOLIDATED FUEL is stored in a MAINE YANKEE FUEL CAN and may only loaded in the Standard CANISTER.

Spent fuel configurations that are unique to a site or reactor due to the addition of other components or reconfiguration of the fuel assembly at the site. It includes fuel assemblies, which hold nonfuel-bearing components, such as control components or instrument and plug thimbles, or which are modified as required by expediency in reactor operations, research and development or testing. Modification may consist of individual fuel rod removal, fuel rod replacement of similar or dissimilar material or enrichment, the installation, removal or replacement of burnable poison rods, or containerizing damaged fuel.

Site specific fuel includes irradiated fuel assemblies designed with variable enrichments and/or axial blankets, fuel that is consolidated and fuel that exceeds design basis fuel parameters.

MAINE YANKEE FUEL CAN A specially designed stainless steel screened can sized to hold INTACT FUEL, CONSOLIDATED FUEL, DAMAGED FUEL or FUEL DEBRIS. The screens preclude the release of gross particulate from the can into the canister cavity. The MAINE YANKEE FUEL CAN may only be loaded in a Class 1 canister in the Standard CANISTER.

Logical Connectors A 1.2

A 1.0 USE AND APPLICATION

A 1.2 Logical Connectors

PURPOSE The purpose of this section is to explain the meaning of logical connectors.

Logical connectors are used in Technical Specifications (TS) to discriminate between, and yet connect, discrete Conditions, Required Actions, Completion Times, Surveillances, and Frequencies. The only logical connectors that appear in Technical Specifications are "<u>AND</u>" and "<u>OR</u>." The physical arrangement of these connectors constitutes logical conventions with specific meanings.

BACKGROUND

Several levels of logic may be used to state Required Actions. These levels are identified by the placement (or nesting) of the logical connectors and by the number assigned to each Required Action. The first level of logic is identified by the first digit of the number assigned to a Required Action and the placement of the logical connector in the first level of nesting (i.e., left justified with the number of the Required Action). The successive levels of logic are identified by additional digits of the Required Action number and by successive indentations of the logical connectors.

When logical connectors are used to state a Condition, Completion Time, Surveillance, or Frequency, only the first level of logic is used; the logical connector is left justified with the statement of the Condition, Completion Time, Surveillance, or Frequency.

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Logical Connectors A 1.2

EXAMPLES The following examples illustrate the use of logical connectors.

EXAMPLES <u>EXAMPLE 1.2-1</u> ACTIONS

	CONDITION	REQ	UIRED ACTION	COMPLETION TIME
A.	LCO not met	A.1	Verify	
		AND		
		A.2	Restore	

In this example, the logical connector "<u>AND</u>" is used to indicate that when in Condition A, both Required Actions A.1 and A.2 must be completed.

EXAMPLES	EXAMPLE 1.2-2			
(commuce)	ACTIONS			
	CONDITION	REQUI	RED ACTION	COMPLETION TIME
	A. LCO not met	A.1	Stop	
		OR		
		A.2.1	Verify	
		AND		
		A.2.2		
		A.2.2.1	Reduce	
			<u>OR</u>	
		A.2.2.2	Perform	
		<u>OR</u>		
•		A.3	Remove	

This example represents a more complicated use of logical connectors. Required Actions A.1, A.2, and A.3 are alternative choices, only one of which must be performed as indicated by the use of the logical connector "<u>OR</u>" and the left justified placement. Any one of these three Actions may be chosen. If A.2 is chosen, then both A.2.1 and A.2.2 must be performed as indicated by the logical connector "<u>AND</u>." Required Action A.2.2 is met by performing A.2.2.1 or A.2.2.2. The indented position of the logical connector "<u>OR</u>" indicated that A.2.2.1 and A.2.2.2 are alternative choices, only one of which must be performed.

A 1.0 USE AND APPLICATION

A 1.3 Completion Times

PURPOSE The purpose of this section is to establish the Completion Time convention and to provide guidance for its use.

BACKGROUND Limiting Conditions for Operations (LCOs) specify the lowest functional capability or performance levels of equipment required for safe operation of the NAC-UMS[®] SYSTEM. The ACTIONS associated with an LCO state conditions that typically describe the ways in which the requirements of the LCO can fail to be met. Specified with each stated Condition are Required Action(s) and Completion Time(s).

DESCRIPTION The Completion Time is the amount of time allowed for completing a Required Action. It is referenced to the time of discovery of a situation (e.g., equipment or variable not within limits) that requires entering an ACTIONS Condition, unless otherwise specified, provided that the NAC-UMS[®] SYSTEM is in a specified Condition stated in the Applicability of the LCO. Prior to the expiration of the specified Completion Time, Required Actions must be completed. An ACTIONS Condition remains in effect and the Required Actions apply until the Condition no longer exists or the NAC-UMS[®] SYSTEM is not within the LCO Applicability.

Once a Condition has been entered, subsequent subsystems, components, or variables expressed in the Condition, discovered to be not within limits, will <u>not</u> result in separate entry into the Condition, unless specifically stated. The Required Actions of the Condition continue to apply to each additional failure, with Completion Times based on initial entry into the Condition.

Completion Times A 1.3

EXAMPLES The following examples illustrate the use of Completion Times with different types of Conditions and changing Conditions.

EXAMPLE 1.3-1

ACTIONS

	CONDITION	REQUIRED ACTION		COMPLETION TIME
В.	Required Action and associated Completion	B.1 <u>AND</u>	Perform Action B.1	12 hours
	Time not met	B.2	Perform Action B.2	36 hours

Condition B has two Required Actions. Each Required Action has its own Completion Time. Each Completion Time is referenced to the time that Condition B is entered.

The Required Actions of Condition B are to complete action B.1 within 12 hours <u>AND</u> complete action B.2 within 36 hours. A total of 12 hours is allowed for completing action B.1 and a total of 36 hours (not 48 hours) is allowed for completing action B.2 from the time that Condition B was entered. If action B.1 is completed within six hours, the time allowed for completing action B.2 is the next 30 hours because the total time allowed for completing action B.2 is 36 hours.

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Completion Times A 1.3

EXAMPLES

EXAMPLE 1.3-2

(continued)

ACTIONS

	CONDITION	REQUIRED ACTION		COMPLETION TIME
Α.	One System not within limit	A.1	Restore System to within limit	7 days
В.	Required Action and associated Completion Time not met	B.1 <u>AND</u>	Complete action B.1	12 hours
		B.2	Complete action B.2	36 hours

When a System is determined not to meet the LCO, Condition A is entered. If the System is not restored within seven days, Condition B is also entered, and the Completion Time clocks for Required Actions B.1 and B.2 start. If the System is restored after Condition B is entered, Conditions A and B are exited; therefore, the Required Actions of Condition B may be terminated.

Completion Times A 1.3

EXAMPLE 1.3-3

ACTIONS

EXAMPLES

(continued)

-----NOTE-----

Separate Condition entry is allowed for each component.

	CONDITION	REQUIRED ACTION		COMPLETION TIME
А.	LCO not met	A.1	Restore compliance with LCO	4 hours
B.	Required Action and associated Completion	B.1 <u>AND</u>	Complete action B.1	6 hours
	Time not met	B.2	Complete action B.2	12 hours

The Note above the ACTIONS table is a method of modifying how the Completion Time is tracked. If this method of modifying how the Completion Time is tracked was applicable only to a specific Condition, the Note would appear in that Condition rather than at the top of the ACTIONS Table.

The Note allows Condition A to be entered separately for each component, and Completion Times to be tracked on a per component basis. When a component is determined to not meet the LCO, Condition A is entered and its Completion Time starts. If subsequent components are determined to not meet the LCO, Condition A is entered for each component and separate Completion Times are tracked for each component.

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Completion Times A 1.3

EXAMPLES <u>EXAMPLE 1.3-3</u> (continued)

IMMEDIATEWhen "Immediately" is used as a Completion Time, the Required ActionCOMPLETIONshould be pursued without delay and in a controlled manner.TIME

Frequency A 1.4

A 1.0 USE AND APPLICATION

A 1.4 Frequency

PURPOSEThe purpose of this section is to define the proper use and application of
Frequency requirements.

DESCRIPTION Each Surveillance Requirement (SR) has a specified Frequency in which the Surveillance must be met in order to meet the associated Limiting Condition for Operation (LCO). An understanding of the correct application of the specified Frequency is necessary for compliance with the SR.

Each "specified Frequency" is referred to throughout this section and each of the Specifications of Section 3.0, Surveillance Requirement (SR) Applicability. The "specified Frequency" consists of requirements of the Frequency column of each SR.

Situations where a Surveillance could be required (i.e., its Frequency could expire), but where it is not possible or not desired that it be performed until sometime after the associated LCO is within its Applicability, represent potential SR 3.0.4 conflicts. To avoid these conflicts, the SR (i.e., the Surveillance or the Frequency) is stated such that it is only "required" when it can be and should be performed. With an SR satisfied, SR 3.0.4 imposes no restriction.

The use of "met" or "performed" in these instances conveys specific meanings. A Surveillance is "met" only after the acceptance criteria are satisfied. Known failure of the requirements of a Surveillance, even without a Surveillance specifically being "performed," constitutes a Surveillance not "met."

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> Frequency A 1.4

EXAMPLES The following examples illustrate the various ways that Frequencies are specified.

EXAMPLE 1.4-1

SURVEILLANCE REQUIREMENTS

SURVEILLANCE	FREQUENCY
Verify pressure within limit	12 hours

Example 1.4-1 contains the type of SR most often encountered in the Technical Specifications (TS). The Frequency specifies an interval (12 hours) during which the associated Surveillance must be performed at least one time. Performance of the Surveillance initiates the subsequent interval. Although the Frequency is stated as 12 hours, SR 3.0.2 allows an extension of the time interval to 1.25 times the interval specified in the Frequency for operational flexibility. The measurement of this interval continues at all times, even when the SR is not required to be met per SR 3.0.1 (such as when the equipment or variables are outside specified limits, or the facility is outside the Applicability of the LCO). If the interval specified by SR 3.0.2 is exceeded while the facility is in a condition specified in the Applicability of the LCO is not met in accordance with SR 3.0.1.

If the interval as specified by SR 3.0.2 is exceeded while the facility is not in a condition specified in the Applicability of the LCO for which performance of the SR is required, the Surveillance must be performed within the Frequency requirements of SR 3.0.2, prior to entry into the specified condition. Failure to do so would result in a violation of SR 3.0.4.

EXAMPLE 1.4-2

SURVEILLANCE REQUIREMENTS

SURVEILLANCE	FREQUENCY
Verify flow is within limits	Once within 12 hours prior to starting activity
	AND 24 hours thereafter

Example 1.4-2 has two Frequencies. The first is a one time performance Frequency, and the second is of the type shown in Example 1.4-1. The logical connector "<u>AND</u>" indicates that both Frequency requirements must be met. Each time the example activity is to be performed, the Surveillance must be performed within 12 hours prior to starting the activity.

The use of "once" indicates a single performance will satisfy the specified Frequency (assuming no other Frequencies are connected by "<u>AND</u>"). This type of Frequency does not qualify for the 25% extension allowed by SR 3.0.2.

"Thereafter" indicates future performances must be established per SR 3.0.2, but only after a specified condition is first met (i.e., the "once" performance in this example). If the specified activity is canceled or not performed, the measurement of both intervals stops. New intervals start upon preparing to restart the specified activity.

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LCO Applicability A 3.0

A 3.0 LIMITING CONDITION FOR OPERATION (LCO) APPLICABILITY

LCO 3.0.1	LCOs shall be met during specified conditions in the Applicability, except as provided in LCO 3.0.2.	
LCO 3.0.2	Upon failure to meet an LCO, the Required Actions of the associated Conditions shall be met, except as provided in LCO 3.0.5.	
	If the LCO is met or is no longer applicable prior to expiration of the specified Completion Time(s), completion of the Required Action(s) is not required, unless otherwise stated.	
LCO 3.0.3	Not applicable to a NAC-UMS [®] SYSTEM.	
LCO 3.0.4	When an LCO is not met, entry into a specified condition in th Applicability shall not be made except when the associated ACTION to be entered permit continued operation in the specified condition in the Applicability for an unlimited period of time. This Specification shall not prevent changes in specified conditions in the Applicabilit that are required to comply with ACTIONS or that are related to th unloading of an NAC-UMS [®] SYSTEM.	
	Exceptions to this Condition are stated in the individual Specifications. These exceptions allow entry into specified conditions in the Applicability where the associated ACTIONS to be entered allow operation in the specified conditions in the Applicability only for a limited period of time.	
LCO 3.0.5	Equipment removed from service or not in service in compliance with ACTIONS may be returned to service under administrative control solely to perform testing required to demonstrate it meets the LCO or that other equipment meets the LCO. This is an exception to LCO 3.0.2 for the System to return to service under administrative control to perform the testing.	

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SR Applicability A 3.0

A 3.0 SURVEILLANCE REQUIREMENT (SR) APPLICABILITY

SR 3.0.1 SRs shall be met during the specified conditions in the Applicability for individual LCOs, unless otherwise stated in the SR. Failure to meet a Surveillance, whether such failure is experienced during the performance of the Surveillance or between performances of the Surveillance, shall be a failure to meet the LCO. Failure to perform a Surveillance within the specified Frequency shall be a failure to meet the LCO, except as provided in SR 3.0.3. Surveillances do not have to be performed on equipment or variables outside specified limits.

SR 3.0.2 The specified Frequency for each SR is met if the Surveillance is performed within 1.25 times the interval specified in the Frequency, as measured from the previous performance or as measured from the time a specified condition of the Frequency is met.

For Frequencies specified as "once," the above interval extension does not apply. If a Completion Time requires periodic performance on a "once per..." basis, the above Frequency extension applies to each performance after the initial performance.

Exceptions to this Specification are stated in the individual Specifications.

SR 3.0.3

If it is discovered that a Surveillance was not performed within its specified Frequency, then compliance with the requirement to declare the LCO not met may be delayed from the time of discovery up to 24 hours or up to the limit of the specified Frequency, whichever is less. This delay period is permitted to allow performance of the Surveillance.

If the Surveillance is not performed within the delay period, the LCO must immediately be declared not met, and the applicable Condition(s) must be entered.

SR Applicability A 3.0

SR 3.0.3 (continued)	When the Surveillance is performed within the delay period and the Surveillance is not met, the LCO must immediately be declared not met, and the applicable Condition(s) must be entered.

SR 3.0.4 Entry into a specified Condition in the Applicability of an LCO shall not be made, unless the LCO's Surveillances have been met within their specified Frequency. This provision shall not prevent entry into specified conditions in the Applicability that are required to comply with Actions or that are related to the unloading of a NAC-UMS[®] SYSTEM. Standard CANISTER Maximum Time in Vacuum Drying A 3.1.1

A 3.1 NAC-UMS[®] SYSTEM Integrity

A 3.1.1 Standard CANISTER Maximum Time in Vacuum Drying

LCO 3.1.1 The following limits for vacuum drying time shall be met, as appropriate:

1. The time duration from completion of draining the CANISTER through completion of vacuum dryness testing and the introduction of helium backfill shall not exceed 10 hours for BWR fuel with the design basis 23 kW heat load or the time shown for PWR fuel with the specified heat load:

Total Heat	Time Limit	Total Heat	Time Limit
<u>Load (L) (kW)</u>	(Hours)	Load (L) (kW)	(Hours)
$20 < L \le 23$	10	$11 < L \leq 14$	23
$17.6 < L \le 20$	15	$8 < L \le 11$	30
$14 < L \le 17.6$	19	$L \leq 8$	34

2. The time duration from the end of 24 hours of in-pool cooling or of forced air cooling of the CANISTER through completion of vacuum dryness testing and the introduction of helium backfill shall not exceed 6 hours for the BWR configuration or the time shown for a specified PWR heat load:

Total Heat	Time Limit
<u>Load (L) (kW)</u>	(Hours)
$20 < L \le 23$	6
$14 < L \leq 20$	10
L ≤ 14	14

APPLICABILITY: Standard CANISTER during LOADING OPERATIONS
Standard CANISTER Maximum Time in Vacuum Drying A 3.1.1

ACTIONS

Separate Condition entry is allowed for each NAC-UMS[®] SYSTEM.

	CONDITION	REQUIRED ACTION	COMPLETION TIME
A.	LCO time limits not met	A.1 Commence filling CANISTER with helium	2 hours
	·	<u>AND</u> A.2.1 Submerge TRANSFER CASK with helium filled loaded CANISTER in spent fuel pool.	2 hours
		AND A.2.2 Maintain TRANSFER CASK and CANISTER in spent fuel pool for a minimum of 24 hours	Prior to restart of LOADING OPERATIONS
		OR A.3.1 Commence supplying air to the TRANSFER CASK annulus fill/drain lines at a rate of 375 CFM and a maximum temperature of 76°F	2 hours
		<u>AND</u> A.3.2 Maintain airflow for a minimum of 24 hours	Prior to restart of LOADING OPERATIONS

SURVEILLANCE REQUIREMENTS

	SURVEILLANCE	FREQUENCY
SR 3.1.1.1	Monitor elapsed time from completion of CANISTER draining operations until start of helium backfill	Once after completion of CANISTER draining <u>AND</u> As required to meet time limit.
SR 3.1.1.2	Monitor elapsed time from the end of in- pool cooling or of forced-air cooling until restart of helium backfill	Once at end of in-pool cooling or of forced-air cooling <u>AND</u> As required to meet time limit.

CANISTER Vacuum Drying Pressure A 3.1.2

A 3.1 NAC-UMS[®] SYSTEM Integrity

A 3.1.2 CANISTER Vacuum Drying Pressure

LCO 3.1.2 The CANISTER vacuum drying pressure shall be ≤ 10 mm of mercury (Hg). Vacuum pressure shall be held for a minimum of 10 minutes with pressure remaining below 10 mm of mercury during the 10-minute period.

APPLICABILITY: Standard or Advanced CANISTER during LOADING OPERATIONS

ACTIONS

-----NOTE-----

10-minute period shall commence following system pressure stabilization at a vacuum pressure at or below 10 mm Hg. Separate Condition entry is allowed for each NAC-UMS[®] SYSTEM.

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CONDITION	REQUIRED ACTION	COMPLETION TIME		
A. CANISTER vacuum drying pressure limit not met	A.1 Establish CANISTER cavity vacuum drying pressure within limit	25 days		
 B. Required Action and associated Completion Time not met 	B.1 Remove all fuel assemblies from the NAC-UMS [®] SYSTEM	5 days		
SURVEILLANCE REQUIREMENTS				
SURVEI	LLANCE	FREQUENCY		
SD 2 1 2 1				

CANISTER Vacuum and Helium Backfill Pressure A 3.1.3

A 3.1 NAC-UMS[®] SYSTEM Integrity

A 3.1.3 CANISTER Vacuum and Helium Backfill Pressures

LCO 3.1.3 The CANISTER helium backfill pressure shall be 0 (+3, -0) psig. Prior to helium backfill, the CANISTER vacuum pressure shall be $\leq 3 \text{ mm of}$ mercury.

APPLICABILITY: Standard or Advanced CANISTER during LOADING OPERATIONS

ACTIONS

-----NOTE-----

Separate Condition entry is allowed for each NAC-UMS[®] SYSTEM.

CONDITION	REQUIRED ACTION	COMPLETION TIME	
A. CANISTER vacuum or helium backfill pressure limit not met	A.1 Establish CANISTER vacuum or helium backfill pressure within limit	25 days	
B. Required Action and associated Completion Time not met	B.1 Remove all fuel assemblies from the NAC-UMS [®] SYSTEM	5 days	

SURVEILLANCE REQUIREMENTS

	SURVEILLANCE	FREQUENCY
SR 3.1.3.1	Verify CANISTER vacuum and helium backfill pressures are within limits.	Prior to TRANSPORT OPERATIONS.

Standard CANISTER Maximum Time in TRANSFER CASK A 3.1.4 NAC-UMS[®] SYSTEM Integrity A 3.1 A 3.1.4 Standard CANISTER Maximum Time in TRANSFER CASK The following limits for the Standard CANISTER time in TRANSFER LCO 3.1.4 CASK shall be met, as appropriate: 1. The time duration from completion of backfilling the CANISTER with helium through completion of the CANISTER transfer operation from the TRANSFER CASK to the CONCRETE CASK shall not exceed 24 hours for the design basis BWR heat load of 23 kW or the time shown below for a specific PWR heat load: Total PWR Heat **Time Limit** Load (L) (kW)(Hours) $20 < L \le 23$ 16 $17.6 < L \le 20$ 20 $14 < L \le 17.6$ 48 $L \le 14$ Not Limited 2. The time duration from completion of in-pool or external forced air cooling of the CANISTER through completion of the CANISTER transfer operation from the TRANSFER CASK to the CONCRETE CASK shall not exceed 15 hours for the BWR configuration or the time shown below for a specific PWR heat load:

Total PWR Heat	Time Limit
<u>Load (L) (kW)</u>	(Hours)
$20 < L \le 23$	6
$17.6 < L \le 20$	16
$14 < L \le 17.6$	20
$L \le 14$	Not Limited

The LCO time limits are also applicable if SR 3.1.5.1 was not met during vacuum drying operations.

APPLICABILITY:

Standard CANISTER during LOADING OPERATIONS

Standard CANISTER Maximum Time in TRANSFER CASK A 3.1.4

 Sen	arate Condition entry	is allowe	NOTE d for each NAC-UMS [®] SYSTEM.	
Sep	CONDITION		REQUIRED ACTION	COMPLETION TIME
А.	LCO time limits not met	A.1.1 P h s	Place TRANSFER CASK with belium filled loaded CANISTER in pent fuel pool	2 hours
		AND A.1.2 M OR	Maintain TRANSFER CASK and CANISTER in spent fuel pool for a ninimum of 24 hours	Prior to restart of LOADING OPERATIONS
		A.2.1	Commence supplying air to the TRANSFER CASK annulus fill/drain lines at a rate of 375 CFM and a maximum temperature of 76°F	2 hours
		<u>AND</u> A.2.2	Maintain airflow for a minimum of 24 hours OR	Prior to restart of LOADING OPERATIONS
		A.2.3	Maintain airflow during operations.	During LOADING OPERATIONS

Standard CANISTER Maximum Time in TRANSFER CASK A 3.1.4

SURVEILLANCE REQUIREMENTS			
	SURVEILLANCE	FREQUENCY	
SR 3.1.4.1 Monitor elapsed time from completion of helium backfill until completion of transfer of loaded CANISTER into CONCRETE CASK		Once at completion of helium backfill <u>AND</u> 4 hours thereafter	
SR 3.1.4.2 Monitor elapsed time from completion of in-pool or forced-air cooling until completion of transfer of loaded CANISTER into CONCRETE CASK		Once at completion of cooling operations <u>AND</u> 4 hours thereafter	

CANISTER Helium Leak Rate A 3.1.5

A 3.1	NAC-UMS [®] SY	YSTEM Integrity
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A 3.1.5 CANISTER Helium Leak Rate

LCO 3.1.5 The CANISTER shield lid to CANISTER shell confinement weld shall be tested to demonstrate a helium leak rate less than 2×10^{-7} cm³/sec (helium). The test sensitivity shall be 1×10^{-7} cm³/sec (helium).

APPLICABILITY: Standard and Advanced CANISTER during LOADING OPERATIONS

ACTIONS

-----NOTE-----NOTE-----

Separate Condition entry is allowed for each NAC-UMS[®] SYSTEM.

CONDITION	REQUIRED ACTION	COMPLETION TIME
A. CANISTER helium leak rate limit not met	A.1 Establish CANISTER helium leak rate within limit	25 days
 B. Required Action and associated Completion Time not met 	B.1 Remove all fuel assemblies from the NAC-UMS [®] SYSTEM	5 days

SURVEILLANCE REQUIREMENTS

<u></u>	SURVEILLANCE	FREQUENCY
SR 3.1.5.1	Verify CANISTER helium leak rate is within limit	Once prior to TRANSPORT OPERATIONS.

CONCRETE CASK Heat Removal System A 3.1.6

A 3.1	NAC-UMS [®] SYSTEM	
A 3.1.6	CONCRE	ETE CASK Heat Removal System
LCO 3.1.6		The CONCRETE CASK Heat Removal System shall be OPERABLE.
APPLICABIL	ITY:	Standard and Advanced CONCRETE CASKS during STORAGE OPERATIONS
ACTIONS		
NOTE		
Separate Condition entry is allowed for each NAC-UMS [®] SYSTEM.		

CONDITION	REQUIRED ACTION	COMPLETION TIME
A. CONCRETE CASK Heat Removal System inoperable	A.1 Restore CONCRETE CASK Heat Removal System to OPERABLE status	8 hours
B. Required Action A.1 and associated Completion Time not met	B.1 Perform SR 3.1.6.1	Immediately and every 6 hours thereafter
	AND	
	B.2 Restore CONCRETE CASK Heat Removal System to OPERABLE status	12 hours

SURVEILLANCE REQUIREMENTS

	SURVEILLANCE	FREQUENCY
SR 3.1.6.1	Verify the difference between the average CONCRETE CASK air outlet temperature and ISFSI ambient temperature is $\leq 102^{\circ}$ F for the Standard PWR CANISTER, $\leq 92^{\circ}$ F for the Standard BWR CANISTER and $\leq 112^{\circ}$ F for the Advanced PWR CANISTER.	24 hours

Standard CANISTER Removal from the CONCRETE CASK A 3.1.7

A 3.1 NAC-UMS[®] SYSTEM Integrity

A 3.1.7 Standard CANISTER Removal from the CONCRETE CASK

- LCO 3.1.7 The following limits for TRANSFER OPERATIONS shall be met, as appropriate:
 - The time duration for holding the Standard CANISTER in the TRANSFER CASK shall not exceed 24 hours for the design basis BWR heat load of 23 kW or the time shown below for a specific PWR heat load:

Total PWR Heat	Time Limit
<u>Load (L) (kW)</u>	(Hours)
$20 < L \le 23$	16
$17.6 < L \le 20$	20
$14 < L \le 17.6$	48
$L \le 14$	Not Limited

2. The time duration for holding the Standard CANISTER in the TRANSFER CASK using external forced air cooling of the CANISTER is not limited.

APPLICABILITY: Standard CANISTER during TRANSFER OPERATIONS

ACTIONS

-----NOTE-----

Separate Condition entry is allowed for each NAC-UMS[®] SYSTEM.

Separate Condition entry to this LCO is allowed following each 24-hour period of continuous forced air cooling.

Standard CANISTER Removal from the CONCRETE CASK A 3.1.7

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CONDITION	REQUIRED ACTION	COMPLETION TIME
A. Loaded CANISTER held in TRANSFER CASK	A.1.1 Load CANISTER into operable CONCRETE CASK	4 hours
0	OR A.2.1 Load CANISTER into TRANSPORT CASK	4 hours
	OR A.3.1 Perform A.1.1 or A.2.1 following a minimum of 24-hours of forced air cooling	4 hours
B. Required Actions in A and associated Completion Time not met	B.1.1 Commence supplying air to the TRANSFER CASK annulus fill/drain lines at a rate of 375 CFM and a maximum temperature of 76°F	2 hours
	AND B.2.1 Maintain forced air cooling. Condition A of this LCO may be re- entered after 24 hours of forced air cooling <u>OR</u>	24 hours
	B.2.2 Maintain forced air cooling during operations.	During TRANSFER OPERATIONS

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Standard CANISTER Removal from the CONCRETE CASK A 3.1.7

SURVEILLANCE REQUIREMENTS			
	SURVEILLANCE	FREQUENCY	
SR 3.1.7.1	Monitor elapsed time from closing of the TRANSFER CASK bottom shield doors until unloading of the CANISTER from the TRANSFER CASK	Once at closing of the TRANSFER CASK bottom shield doors <u>AND</u> 2 hours thereafter	
SR 3.1.7.2	Monitor continuous forced air cooling operation until unloading of the CANISTER from the TRANSFER CASK	Once at start of cooling operations <u>AND</u> 6 hours thereafter	

Advanced CANISTER Maximum Time in Vacuum Drying A 3.1.8

A 3.1 NAC-UMS[®] SYSTEM Integrity

LCO 3.1.8

A 3.1.8 Advanced CANISTER Maximum Time in Vacuum Drying

The following limits for vacuum drying time shall be met, as appropriate:

1. The time duration from completion of draining the Advanced CANISTER through completion of vacuum dryness testing and the introduction of helium backfill shall not exceed the time shown for PWR fuel with the specified heat load:

Total Heat	Time Limit	
<u>Load (L) (kW)</u>	(Hours)	
$27 < L \leq 29.2$	44	
$25 < L \le 27$	50	
$22 < L \le 25$	74	
$18 < L \leq 22$	96	
$L \le 18$	Not Limited	

2. The time duration from the end of 24 hours of in-pool cooling; or of 48 hours of forced air cooling for heat loads of 25 kW or more; or of 24 hours of forced air cooling for heat loads less than 25 kW, the Advanced CANISTER through completion of vacuum dryness testing and the introduction of helium backfill shall not exceed the time shown for the specified heat load:

Heat Load	In-Pool	Forced Air
<u>L (kW)</u>	(Hours)	(Hours)
$27 < L \le 29.2$	20	14
$25 < L \le 27$	25	20
$22 < L \le 25$	46	22
$18 < L \le 22$	68	40

APPLICABILITY:

The Advanced CANISTER during LOADING OPERATIONS

Advanced CANISTER Maximum Time in Vacuum Drying A 3.1.8

ACTIONS

Separate Condition entry is allowed for each NAC-UMS[®] SYSTEM.

	CONDITION	REQUIRED ACTION	COMPLETION TIME
А.	LCO time limits not met	A.1.1 Commence filling CANISTER with helium	2 hours
		AND A.1.2 Submerge TRANSFER CASK with helium filled loaded CANISTER in spent fuel pool.	2 hours
		AND A.1.3 Maintain TRANSFER CASK and CANISTER in spent fuel pool for a minimum of 24 hours.	Prior to restart of LOADING OPERATIONS
		A.2.1 Commence supplying air to the TRANSFER CASK annulus fill/drain lines at a maximum temperature of 76°F.	2 hours
		AND	
		A.2.2 Maintain airflow of 500 CFM for a minimum of 48 hours for heat loads greater than, or equal to, 25 kW. OR	Prior to restart of LOADING OPERATIONS
		A.2.3 Maintain airflow of 375 CFM for a minimum of 24 hours for heat loads less than 25 kW.	

Advanced CANISTER Maximum Time in Vacuum Drying A 3.1.8

SURVEILLAN	ICE REQUIREMENTS	
	SURVEILLANCE	FREQUENCY
SR 3.1.8.1	Monitor elapsed time from completion of CANISTER draining operations until start of helium backfill	Once after completion of CANISTER draining <u>AND</u> As required to meet time limit
SR 3.1.8.2	Monitor elapsed time from the end of in- pool cooling or of forced-air cooling until restart of helium backfill	Once at end of in-pool cooling or of forced-air cooling <u>AND</u> As required to meet time limit.

Advanced CANISTER Maximum Time in TRANSFER CASK A 3.1.9

A 3.1 NAC-UMS[®] SYSTEM Integrity

A 3.1.9 Advanced CANISTER Maximum Time in TRANSFER CASK

LCO 3.1.9 The following limits for the Advanced CANISTER time in TRANSFER CASK shall be met, as appropriate:

1. The time duration from completion of backfilling the Advanced CANISTER with helium through completion of the CANISTER transfer operation from the TRANSFER CASK to the CONCRETE CASK shall not exceed the time shown below for a specific heat load:

Total Heat	Time Limit
<u>Load (L) (kW)</u>	(Hours)
$27 < L \leq 29.2$	30
$25 < L \le 27$	40
L ≤ 25	Not Limited

2. The time duration from the end of 24 hours of in-pool cooling or 48 hours of external forced air cooling of the Advanced CANISTER through completion of the CANISTER transfer operation from the TRANSFER CASK to the Advanced CONCRETE CASK shall not exceed the time shown below for a specific heat load:

Total Heat	Time Limit
<u>Load (L) (kW)</u>	(Hours)
$27 < L \leq 29.2$	30
$25 < L \le 27$	40

3. The time duration for holding the Advanced CANISTER in the TRANSFER CASK using external forced air cooling of the CANISTER is not limited.

The LCO time limits are also applicable if SR 3.1.8.1 was not met during vacuum drying operations.

APPLICABILITY: The Advanced Canister During LOADING OPERATIONS

Advanced CANISTER Maximum Time in TRANSFER CASK A 3.1.9

ACTIONS				
Sep	Separate Condition entry is allowed for each NAC-UMS [®] SYSTEM.			
	CONDITION	REQUIRED ACTION	COMPLETION TIME	
А.	LCO time limits not met	A.1.1 Place TRANSFER CASK with helium filled loaded CANISTER in spent fuel pool	2 hours	
		AND A.1.2 Maintain TRANSFER CASK and CANISTER in spent fuel pool for a minimum of 24 hours OR	Prior to restart of LOADING OPERATIONS	
		A.2.1 Commence supplying air to the TRANSFER CASK annulus fill/drain lines at a rate of 500 CFM and a maximum temperature of 76°F <u>AND</u>	2 hours	
		A.2.2 Maintain airflow for a minimum of 48 hours	Prior to restart of LOADING OPERATIONS	
		A.3.1 Commence supplying air to the TRANSFER CASK annulus fill/drain lines at a rate of 500 CFM and a maximum temperature of 76°F. <u>AND</u>	2 hours	
		A.3.2 Maintain airflow during operations.	During LOADING OPERATIONS	

Advanced CANISTER Maximum Time in TRANSFER CASK A 3.1.9

SURVEILLANCE REQUIREMENTS

	SURVEILLANCE	FREQUENCY
SR 3.1.9.1	Monitor elapsed time from completion of helium backfill until completion of transfer of loaded CANISTER into CONCRETE CASK	Once at completion of helium backfill <u>AND</u> 4 hours thereafter
SR 3.1.9.2	Monitor elapsed time from completion of in-pool or forced-air cooling until completion of transfer of loaded CANISTER into CONCRETE CASK	Once at completion of cooling operations <u>AND</u> 4 hours thereafter

Advanced CANISTER Removal from the CONCRETE CASK A 3.1.10

A 3.1 NAC-UMS[®] SYSTEM Integrity

A 3.1.10 Advanced CANISTER Removal from the CONCRETE CASK

- LCO 3.1.10 The following limits for TRANSFER OPERATIONS shall be met, as appropriate:
 - 1. The time duration for holding the Advanced CANISTER in the TRANSFER CASK shall not exceed the time shown below for a specific PWR heat load:

Total Heat	Time Limit
Load (L) (kW)	<u>(Hours)</u>
$27 < L \le 29.2$	30
$25 < L \le 27$	40
L ≤ 25	Not Limited

2. The time duration for holding the Advanced CANISTER in the TRANSFER CASK using external forced air cooling of the CANISTER is not limited.

APPLICABILITY: The Advanced Canister During TRANSFER OPERATIONS

ACTIONS

-----NOTE-----

Separate Condition entry is allowed for each NAC-UMS[®] SYSTEM.

Separate Condition entry to this LCO is allowed following each 24-hour period of continuous forced air cooling.

Advanced CANISTER Removal from CONCRETE CASK A 3.1.10

REQUIRED ACTION	COMPLETION TIME
A.1.1 Load CANISTER into operable CONCRETE CASK	4 hours
OR A.2.1 Load CANISTER into TRANSPORT CASK	4 hours
OR A.3.1 Perform A.1.1 or A.2.1 following a minimum of 48 hours of forced air cooling	4 hours
B.1.1 Commence supplying air to the TRANSFER CASK annulus fill/drain lines at a rate of 500 CFM and a maximum temperature of 76°F	2 hours
AND B.2.1 Maintain forced air cooling. Condition A of this LCO may be re- entered after 48 hours of forced air cooling <u>OR</u> B.2.2 Maintain air cooling during operations.	24 hours During TRANSFER OPERATIONS
	REQUIRED ACTION A.1.1 Load CANISTER into operable CONCRETE CASK OR A.2.1 Load CANISTER into TRANSPORT CASK OR A.3.1 Perform A.1.1 or A.2.1 following a minimum of 48 hours of forced air cooling B.1.1 Commence supplying air to the TRANSFER CASK annulus fill/drain lines at a rate of 500 CFM and a maximum temperature of 76°F AND B.2.1 Maintain forced air cooling. Condition A of this LCO may be reentered after 48 hours of forced air cooling B.2.2 Maintain air cooling during operations.

Advanced CANISTER Removal from the CONCRETE CASK A 3.1.10

SURVEILLANCE REQUIREMENTS		
	SURVEILLANCE	FREQUENCY
SR 3.1.10.1	Monitor elapsed time from closing of the TRANSFER CASK bottom shield doors until unloading of the CANISTER from the TRANSFER CASK	Once at closing of the TRANSFER CASK bottom shield doors <u>AND</u> 2 hours thereafter
SR 3.1.10.2	Monitor continuous forced air cooling operation until unloading of the CANISTER from the TRANSFER CASK	Once at start of cooling operations <u>AND</u> 6 hours thereafter

CANISTER Surface Contamination A 3.2.1

A 3.2 NAC-UMS [®] SYSTEM Radiation Prote	ection
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A 3.2.1	CANISTER Surface	Contamination

LCO 3.2.1 Removable contamination on the accessible exterior surfaces of the CANISTER or accessible interior surfaces of the TRANSFER CASK shall each not exceed:

- a. $10,000 \text{ dpm}/100 \text{ cm}^2$ from beta and gamma sources; and
- b. $100 \text{ dpm}/100 \text{ cm}^2$ from alpha sources.

APPLICABILITY: Standard or Advanced CANISTER during LOADING OPERATIONS

ACTIONS

-----NOTE-----

Separate Condition entry is allowed for each NAC-UMS[®] SYSTEM.

CONDITION	REQUIRED ACTION	COMPLETION TIME
A. CANISTER or TRANSFER CASK removable surface contamination limits not met	A.1 Restore CANISTER and TRANSFER CASK removable surface contamination to within limits	7 days

CANISTER Surface Contamination A 3.2.1

SURVEILLANCE REQUIREMENTS FREQUENCY SURVEILLANCE FREQUENCY SR 3.2.1.1 Verify that the removable contamination on the accessible exterior surfaces of the CANISTER is within limits Once, prior to TRANSPORT OPERATIONS SR 3.2.1.2 Verify that the removable contamination on the accessible interior surfaces of the TRANSFER CASK does not exceed limits Once, prior to TRANSPORT OPERATIONS

CONCRETE CASK Average Surface Dose Rate A 3.2.2

A 3.2 NAC-UMS[®] SYSTEM Radiation Protection

A 3.2.2 CONCRETE CASK Average Surface Dose Rates

- LCO 3.2.2 The average surface dose rates of each CONCRETE CASK shall not exceed the following limits unless required ACTIONS A.1 and A.2 are met.
 - a. 50 mrem/hour (neutron + gamma) on the side (on the concrete surfaces);
 - b. 100 mrem/hour (neutron + gamma) on the top;
 - c. 100 mrem/hour (neutron + gamma) at air inlets.
 - d. 300 mrem/hour (neutron + gamma) at air outlets.

APPLICABILITY: Standard or Advanced CANISTER during LOADING OPERATIONS

ACTIONS

-----NOTE-----

Separate Condition entry is allowed for each NAC-UMS[®] SYSTEM.

CONDITION	REQUIRED ACTION	COMPLETION TIME
A. CONCRETE CASK average surface dose rate limits not met	A.1 Administratively verify correct fuel loading	24 hours

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CONCRETE CASK Average Surface Dose Rate A 3.2.2

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CONDITION	REQUIRED ACTION	COMPLETION TIME
	A.2 Perform analysis to verify compliance with the ISFSI offsite radiation protection requirements of 10 CFR 20 and 10 CFR 72	7 days
B. Required Action and associated Completion Time not met.	B.1 Remove all fuel assemblies from the NAC-UMS [®] SYSTEM	30 days

SURVEILLANCE REQUIREMENTS

	SURVEILLANCE	FREQUENCY
SR 3.2.2.1	Verify average surface dose rates of CONCRETE CASK loaded with a CANISTER containing fuel assemblies are within limits. Dose rates shall be measured at the locations shown in Figure 12A3-1.	Once after completion of transfer of CANISTER into CONCRETE CASK and prior to beginning STORAGE OPERATIONS.

CONCRETE CASK Average Surface Dose Rate A 3.2.2

Figure 12A3-1 CONCRETE CASK Surface Dose Rate Measurement



Measure dose rates at eight target points (0, 45, 90, 135, 180, 225, 270 and 315 degrees) on each plane, at center of each inlet and outlet and at a point in between each inlet and outlet.



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A 5.0 ADMINISTRATIVE CONTROLS AND PROGRAMS

A 5.1 <u>Training Program</u>

A training program for the NAC-UMS[®] Universal Storage System shall be developed under the general licensee's systematic approach to training (SAT). Training modules shall include comprehensive instructions for the operation and maintenance of the NAC-UMS[®] Universal Storage System and the independent spent fuel storage installation (ISFSI).

A 5.2 Pre-Operational Testing and Training Exercises

A dry run training exercise on loading, closure, handling, unloading, and transfer of the NAC-UMS[®] Storage System shall be conducted by the licensee prior to the first use of the system to load spent fuel assemblies. The training exercise shall not be conducted with spent fuel in the CANISTER. The dry run may be performed in an alternate step sequence from the actual procedures, but all steps must be performed. The dry run shall include, but is not limited to the following:

- a. Moving the CONCRETE CASK into its designated loading area
- b. Moving the TRANSFER CASK containing the empty CANISTER into the spent fuel pool
- c. Loading one or more dummy fuel assemblies into the CANISTER, including independent verification
- d. Selection and verification of fuel assemblies requiring preferential loading
- e. Installing the shield lid
- f. Removal of the TRANSFER CASK from the spent fuel pool
- g. Closing and sealing of the CANISTER to demonstrate pressure testing, vacuum drying, helium backfilling, welding, weld inspection and documentation, and leak testing
- h. TRANSFER CASK movement through the designated load path
- i. TRANSFER CASK installation on the CONCRETE CASK
- j. Transfer of the CANISTER to the CONCRETE CASK

A 5.2 Pre-Operational Testing and Training Exercises (continued)

- k. CONCRETE CASK shield plug and lid installation
- 1. Transport of the CONCRETE CASK to the ISFSI
- m. CANISTER unloading, including reflooding and weld removal or cutting
- n. CANISTER removal from the CONCRETE CASK

Appropriate mockup fixtures may be used to demonstrate and/or to qualify procedures, processes or personnel in welding, weld inspection, vacuum drying, helium backfilling, leak testing and weld removal or cutting.

A 5.3 Special Requirements for the First System Placed in Service

The heat transfer characteristics and performance of the NAC-UMS[®] SYSTEM will be recorded by air inlet and outlet temperature measurements of the first system placed in service with a heat load equal to or greater than 10 kW. A letter report summarizing the results of the measurements will be submitted to the NRC in accordance with 10 CFR 72.4 within 30 days of placing the loaded cask on the ISFSI pad. The report will include a comparison of the calculated temperatures of the NAC-UMS[®] SYSTEM heat load to the measured temperatures. A report is not required to be submitted for the NAC-UMS[®] SYSTEMs that are subsequently loaded, provided that the performance of the first system placed in service with a heat load ≥ 10 kW, is demonstrated by the comparison of the calculated temperatures.

A 5.4 Surveillance After an Off-Normal, Accident, or Natural Phenomena Event

A Response Surveillance is required following off-normal, accident or natural phenomena events. The NAC-UMS[®] SYSTEMs in use at an ISFSI shall be inspected within 4 hours after the occurrence of an off-normal, accident or natural phenomena event in the area of the ISFSI. This inspection must specifically verify that all the CONCRETE CASK inlets and outlets are not blocked or obstructed. At least one-half of the inlets and outlets on each CONCRETE CASK must be cleared of blockage or debris within 24 hours to restore air circulation.

The CONCRETE CASK and CANISTER shall be inspected if they experience a drop or a tipover.

A 5.5 Radioactive Effluent Control Program

The program implements the requirements of 10 CFR 72.44(d).

- a. The NAC-UMS[®] SYSTEM does not create any radioactive materials or have any radioactive waste treatment systems. Therefore, specific operating procedures for the control of radioactive effluents are not required. LCO 3.1.5, CANISTER Helium Leak Rate, provides assurance that there are no radioactive effluents from the NAC-UMS[®] SYSTEM.
- b. This program includes an environmental monitoring program. Each general license user may incorporate NAC-UMS[®] SYSTEM operations into their environmental monitoring program for 10 CFR Part 50 operations.
- c. An annual report shall be submitted pursuant to 10 CFR 72.44(d)(3).

A 5.6 NAC-UMS[®] SYSTEM Transport Evaluation Program

This program provides a means for evaluating various transport configurations and transport route conditions to ensure that the design basis drop limits are met. For lifting of the loaded TRANSFER CASK or CONCRETE CASK using devices that are integral to a structure governed by 10 CFR Part 50 regulations, 10 CFR 50 requirements apply. This program is not applicable when the TRANSFER CASK or CONCRETE CASK is in the fuel building or is being handled by a device providing support from underneath (i.e., on a rail car, heavy haul trailer, air pads, etc.).

Pursuant to 10 CFR 72.212, this program shall evaluate the site specific transport route conditions.

a. The lift height above the transport surface shall not exceed the limits in Table 12A5-1. Also, the program shall ensure that the transport route conditions outside the fuel building (i.e., surface hardness and pad thickness) are equivalent to or less limiting than those prescribed for the reference pad surface which forms the basis for the values cited in FSAR Sections 11.2.12.3 and 11.2.15.1.1.

A 5.6 NAC-UMS[®] SYSTEM Transport Evaluation Program (continued)

- b. For site specific transport conditions which are not bounded by the surface characteristics in FSAR Sections 11.2.12.3 and 11.2.15.1.1, the program may evaluate the site specific conditions to ensure that the impact loading due to design basis drop events does not exceed 60g. This alternative analysis shall be commensurate with the drop analyses described in the Safety Analysis Report for the NAC-UMS[®] SYSTEM. The program shall ensure that these alternative analyses are documented and controlled.
- c. The TRANSFER CASK and CONCRETE CASK may be lifted to those heights necessary to perform cask handling operations, including CANISTER transfer, provided the lifts are made with structures and components designed in accordance with the criteria specified in Section B3.5 of Appendix B to CoC No. 1015, as applicable.

A 5.7 Verification of Oxide Layer Thickness on High Burnup Fuel

A verification program is required to determine the oxide layer thickness on high burnup fuel by measurement or by statistical analysis. A fuel assembly having a burnup between 45,000 MWD/MTU and 50,000 MWD/MTU is classified as high burnup. The verification program shall be capable of classifying high burnup fuel as INTACT FUEL or DAMAGED FUEL based on the following criteria:

- 1. A HIGH BURNUP FUEL assembly may be stored as INTACT FUEL provided that no more than 1% of the fuel rods in the assembly have a peak cladding oxide thickness greater than 80 microns, and that no more than 3% of the fuel rods in the assembly have a peak oxide layer thickness greater than 70 microns, and that the fuel assembly is otherwise INTACT FUEL.
- 2. A HIGH BURNUP FUEL assembly not meeting the cladding oxide thickness criteria for INTACT FUEL or that has an oxide layer that is detached or spalled from the cladding is classified as DAMAGED FUEL.

A fuel assembly, having a burnup between 45,000 and 50,000 MWD/MTU, must be preferentially loaded in periphery positions of the Standard basket. For the Advanced configuration, fuel assemblies, having a burnup between 45,000 and 55,000 MWD/MTU, must be preferentially loaded based on heat load.

A 5.8 <u>Control of Boron Concentration in Pool Water During Advanced CANISTER</u> Loading and Unloading

The criticality analysis for fuel loading in the Advanced configuration shows that PWR fuel with initial enrichment up to 4.6 wt % ²³⁵U requires that the water in the canister have a boron concentration of at least 2,000 parts per million of boron in solution in the water. Fuel with initial enrichments above 4.6 wt % ²³⁵U requires that the water in the canister have a boron concentration of at least 2,300 parts per million of boron in solution in the water. This water must be used to flood the canister cavity during underwater PWR fuel loading and unloading. The boron in the pool water ensures sufficient thermal neutron absorption to preserve criticality control during fuel loading in the basket. Measurement of pool water boron concentration must be done prior to the submergence of the canister in the pool. The pool boron concentration remains above the required concentration any time that the concentration of boron might be diluted by the influx of unborated water. Water temperature shall be at least 5°F above the temperature necessary to ensure boron solubility.

TRANSFER CASK and CONCRETE CASK Lifting Requirements Table 12A5-1

Table 12A5-1 TRANSFER CASK and CONCRETE CASK Lifting Requirements

Item	Orientation	Lifting Height Limit
Standard TRANSFER CASK	Horizontal	None Established
Advanced TRANSFER CASK	Horizontal	None Established
100-Ton TRANSFER CASK	Horizontal	< 53 inches
TRANSFER CASK	Vertical	None Established ¹
CONCRETE CASK ²	Horizontal	Not Permitted
CONCRETE CASK ²	Vertical	< 24 inches

Note:

- 1. See Technical Specification A5.6(c).
- 2. Applicable to Standard and Advanced configurations.

APPENDIX 12B

APPROVED CONTENTS AND DESIGN FEATURES FOR THE NAC-UMS[®] SYSTEM

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B 2.0 APPROVED CONTENTS

B 2.1 Fuel Specifications and Loading Conditions

The NAC-UMS[®] SYSTEM is designed to provide passive dry storage of canistered PWR and BWR spent fuel. The system requires few operating controls. The principal controls and limits for the NAC-UMS[®] SYSTEM are satisfied by the selection of fuel for storage that meets the Approved Contents presented in this section and in Tables 12B2-1 through 12B2-5 for the Standard NAC-UMS[®] SYSTEM and in Tables 12B2-10 through 12B2-13 for the Advanced NAC-UMS[®] SYSTEM.

This section also permits the loading of fuel assemblies that are unique to specific reactor sites. SITE SPECIFIC FUEL assembly configurations are either shown to be bounded by the analysis of the standard NAC-UMS[®] System design basis fuel assembly configuration of the same type (PWR or BWR), or are shown to be acceptable contents by specific evaluation of the configuration.

The separate specific evaluation may establish different limits, which are maintained by administrative controls for preferential loading. The preferential loading controls allow the loading of fuel configurations that may have higher burnup, additional hardware material or unique configurations as compared to the standard NAC-UMS[®] System design basis spent fuels.

Unless specifically excepted, SITE SPECIFIC FUEL must meet all of the controls and limits specified for the NAC-UMS[®] System, as presented in Table 12-1 for the Standard configuration and in Table 12-2 for the Advanced configuration.

If any Fuel Specification or Loading Conditions of this section are violated, the following actions shall be completed:

- The affected fuel assemblies shall be placed in a safe condition.
- Within 24 hours, notify the NRC Operations Center.
- Within 30 days, submit a special report that describes the cause of the violation and actions taken to restore or demonstrate compliance and prevent recurrence.

B 2.1.1 Fuel to be Stored in the Standard NAC-UMS[®] SYSTEM

INTACT FUEL ASSEMBLIES meeting the limits specified in Tables 12B2-1 through 12B2-5 may be stored in the Standard NAC-UMS[®] SYSTEM.

B 2.1.2 Preferential Fuel Loading

The normal temperature distribution in the loaded Standard CANISTER results in the basket having the highest temperature at its center and lowest temperature at the outer edge. Considering this temperature distribution, spent fuel with the shortest cooling time (and, therefore, having a higher allowable cladding temperature) is placed in the center of the basket. Fuel with the longest cooling time (and, therefore, having a lower allowable cladding temperature) is placed in the periphery of the basket.

Using a similar argument, fuel assemblies with cooling times between the highest and lowest cooling times of the designated fuel, are placed in intermediate fuel positions.

Loading of the fuel assemblies designated for a given Standard CANISTER must be administratively controlled to ensure that the dry storage fuel cladding temperature limits are not exceeded for any fuel assembly, unless all of the designated fuel assemblies have a cooling time of 7 years of more. Fuel assemblies, all of which have a cooling time of 7 years, or more, do not require preferential loading, because analyses have shown that the fuel cladding temperature limits will always be met for those CANISTERS.

Standard CANISTERS containing fuel assemblies with cooling times from 5 to 7 years must be preferentially loaded based on cooling time. By controlling the placement of the fuel assemblies with the shortest cooling time (thermally hottest), preferential loading ensures that the allowable fuel cladding temperature for a given fuel assembly is not exceeded. The preferential loading of fuel into the CANISTER based on cooling time is described as follows.

For the Standard PWR fuel basket configuration, shown in Figure 12B2-1, fuel positions are numbered using the drain line as the reference point. Fuel positions 9, 10, 15 and 16 are considered to be basket center positions for the purpose of meeting the preferential loading requirement. The fuel with the shortest cooling times from among the fuel designated for loading in the CANISTER will be placed in the center positions. A single fuel assembly having the shortest cooling time may be loaded in any of these four positions. Fuel positions 1, 2, 3, 6, 7, 12, 13, 18, 19, 22, 23 and 24 are periphery positions, where fuel with the longest cooling times will be placed. Fuel with the longest cooling times may be loaded in any of these 12 positions. Similarly, designated fuel assemblies with cooling times in the midrange of the shortest and longest cooling times will be loaded in the intermediate fuel positions -4, 5, 8, 11, 14, 17, 20 and 21.

For the Standard BWR fuel basket configuration, shown in Figure 12B2-2, fuel positions are also numbered using the drain line as the reference point. Fuel positions 23, 24, 25, 32, 33 and 34 are considered to be basket center positions for the purpose of meeting the preferential loading requirement. The fuel with the shortest cooling times from among the fuel designated for loading in the CANISTER will be placed in the center positions. However, the single fuel assembly having the shortest cooling time will be loaded in either position 24 or position 33. Fuel positions 1, 2, 3, 4, 5, 6, 12, 13, 19, 20, 28, 29, 37, 38, 44, 45, 51, 52, 53, 54, 55 and 56 are periphery positions, where fuel with the longest cooling times will be placed. Fuel with the longest cooling times may be loaded in any of these 23 positions. Designated fuel assemblies with cooling times in the midrange of the shortest and longest cooling times will be divided into two tiers. The fuel assemblies with the shorter cooling times in the midrange will be loaded in the inner intermediate fuel positions - 15, 16, 17, 22, 26, 31, 35, 40, 41, and 42. Fuel assemblies with the longer cooling times in the midrange will be loaded in the outer intermediate fuel positions - 7, 8, 9, 10, 11, 14, 18, 21, 27, 30, 36, 39, 43, 46, 47, 48, 49 and 50. These loading patterns result in the placement of fuel such that the shortest-cooled fuel is in the center of the basket and the longest-cooled fuel is on the periphery. Based on engineering evaluations, this loading pattern ensures that fuel assembly allowable cladding temperatures are satisfied.

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B 2.1.3 Maine Yankee SITE SPECIFIC FUEL Preferential Loading

The estimated Maine Yankee SITE SPECIFIC FUEL inventory is shown in Table 12B2-6. Maine Yankee SITE SPECIFIC FUEL meeting the limits specified in Tables 12B2-7 through 12B2-9 may only be stored in the Standard configuration of the NAC-UMS[®] SYSTEM. As shown in this table, certain of the Maine Yankee fuel configurations must be preferentially loaded in specific basket fuel tube positions of the Standard CANISTER.

Corner positions are used for CONSOLIDATED FUEL, certain HIGH BURNUP FUEL and DAMAGED FUEL or FUEL DEBRIS loaded in a MAINE YANKEE FUEL CAN, for fuel assemblies with missing fuel rods, burnable poison rods or fuel assemblies with fuel rods that have been replaced by hollow Zircaloy rods. Designation for placement in corner positions results primarily from shielding or criticality evaluations of these fuel configurations. CONSOLIDATED FUEL is conservatively designated for a corner position, even though analysis shows that these lattices could be loaded in any basket position. Corner positions are positions 3, 6, 19, and 22 in Figure 12B2-1.

Preferential loading is also used for HIGH BURNUP fuel not loaded in the MAINE YANKEE FUEL CAN. This fuel is assigned to peripheral locations, positions 1, 2, 3, 6, 7, 12, 13, 18, 19, 22, 23, and 24 in Figure 12B2-1. The interior locations must be loaded with fuel that has lower burnup and/or longer cool times to maintain the design basis heat load and component temperature limits for the basket and canister, and the spent fuel short-term temperature limits, as described in Section B 2.1.2.

One of the three loading patterns (Standard, 1.05 kW (periphery), or 0.958 kW (periphery)) shown in Table 12B2-8 must be used to load each canister. Once selected, all of the spent fuel in that canister must be loaded in accordance with that pattern. Within a pattern, mixing of enrichment and cool time is allowed, but no mixing of loading patterns is permitted. For example, choosing a Perf (1.05) pattern restricts the interior fuel to the cool times shown in the Perf (1.05i) column, and the peripheral fuel to the cool times shown in the Perf (1.05p) column.

Fuel assemblies with a control element assembly (CEA) inserted will be loaded in a Class 2 Standard CANISTER and basket due to the increased length of the assembly with the CEA installed. However, these assemblies are not restricted as to loading position within the basket. Fuel assemblies with non-fuel items installed in corner guide tubes of the fuel assembly must

also have a CEA flow plug installed and must be loaded in a basket corner fuel position in a Class 2 Standard CANISTER.

The Transportable Storage Canister loading procedures indicate that loading of a fuel configuration with removed fuel or poison rods, CONSOLIDATED FUEL, or a MAINE YANKEE FUEL CAN with DAMAGED FUEL, FUEL DEBRIS or HIGH BURNUP FUEL may be done only in the Standard CANISTER, and that loading is administratively controlled in accordance with Section B 2.1.

B 2.1.4 Fuel to be Stored in the Advanced NAC-UMS[®] SYSTEM

INTACT FUEL ASSEMBLIES meeting the limits specified in Tables 12B2-10 through 12B2-13 may be stored in the Advanced NAC-UMS[®] SYSTEM. The maximum decay heat load for the storage of all types of PWR fuel assemblies is 29.2 kW (12 Assemblies at 0.7 kW, 12 Assemblies at 1.0 kW and 8 Assemblies at 1.1 kW) based on a three-zone loading pattern as shown in Figure 12B2-3. The maximum heat load in each zone is 8.4 kW in Zone A, 12 kW in Zone B and 8.8 kW in Zone C.

Spent fuel is loaded in the Advanced canister based on controlling fuel peak cladding temperature, thereby, controlling fuel cladding creep strain. The three zone loading pattern is established to limit the maximum peak cladding temperature.

Loading of the fuel assemblies designated for a given Advanced CANISTER must be administratively controlled to ensure that the dry storage fuel cladding temperature limits are not exceeded for any fuel assembly. The fuel assembly loading zones for the Advanced PWR basket are shown in Figure 12B2-3. Fuel loading zone A is restricted to fuel assemblies having a maximum heat load of 700 watts. Within this zone, fuel assemblies must meet the cool time, burnup and enrichment limits shown in Table 12B2-11. Similarly, for zones B and C, for fuel assemblies having maximum heat loads of 1,000 watts and 1,100 watts, respectively, the fuel must meet the applicable cool time, burnup and enrichment limits shown in Tables 12B2-12 and 12B2-13, respectively.

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Figure 12B2-1

Standard PWR Basket Fuel Loading Positions





Standard BWR Basket Fuel Loading Positions





Figure 12B2-3	Maximum Allowable Assembly Heat Load by Advanced PWR Canister Zone
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Advanced Canister	Zone A	Zone B	Zone C
Maximum Allowed Heat Load per Assembly	$\leq 0.7 \text{ kW}$	$\leq 1.0 \text{ kW}$	$\leq 1.1 \text{ kW}$

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Table 12B2-1

Fuel Assembly Limits

- I. NAC-UMS[®] Standard CANISTER: PWR FUEL
 - A. Allowable Contents
 - 1. Uranium oxide PWR INTACT FUEL ASSEMBLIES listed in Table 12B2-2 and meeting the following specifications:

а.	Cladding Type:	Zircaloy with thickness as specified in Table 12B2-2 for the applicable fuel assembly class			
b.	Enrichment:	Maximum and minimum enrichments are 4.2 and 1.9 wt % ²³⁵ U, respectively. Fuel enrichment, burnup and cool time are related as shown in Table 12B2-4.			
c.	Decay Heat Per Assembly:	\leq 958.3 watts			
d.	Post-irradiation Cooling Time and Average Burnup Per Assembly:	As specified in Table 12B2-4			
e.	Nominal Fresh Fuel Assembly Length (in.):	≤ 178.3			
f.	Nominal Fresh Fuel Assembly Width (in.):	≤ 8.54			
g.	Fuel Assembly Weight (lbs.):	<u>≤ 1,515</u>			

- B. Quantity per CANISTER: Up to 24 PWR INTACT FUEL ASSEMBLIES.
- C. PWR INTACT FUEL ASSEMBLIES may contain thimble plugs and burnable poison inserts (Class 1 and Class 2 contents).
- D. PWR INTACT FUEL ASSEMBLIES shall not contain control components.
- E. Stainless steel spacers may be used in CANISTERS to axially position PWR INTACT FUEL ASSEMBLIES that are shorter than the available cavity length to facilitate handling.
- F. Unenriched fuel assemblies are not authorized for loading.
- G. The minimum length of the PWR INTACT FUEL ASSEMBLY internal structure and bottom end fitting and/or spacers shall ensure that the minimum distance to the fuel region from the base of the CANISTER is 3.2 inches.
- H. PWR INTACT FUEL ASSEMBLIES with one or more grid spacers missing or damaged such that the unsupported length of the fuel rods does not exceed 60 inches. End fitting damage including damaged or missing hold-down springs is allowed, as long as the assembly can be handled safely by normal means.

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		Table 12B2	2-1		
		Fuel Assembly Limits	s (continued)		
II. NAC-UMS [®] Standard CANISTER: BWR FUEL					
	A.	Allowable Contents			
	1.	Uranium oxide BWR INTACT FUE	L ASSEMBLIES listed in Table 12B2-3		
		and meeting the following specificat	tions:		
		a. Cladding Type:	Zircaloy with thickness as specified in Table 12B2-3 for the applicable fuel assembly class.		
		b. Enrichment:	Maximum and minimum INITIAL PEAK PLANAR-AVERAGE ENRICHMENTS are 4.0 and 1.9 wt % ²³⁵ U, respectively. Fue enrichment, burnup and cooling time are related as shown in Table 12B2-5.		
		c. Decay Heat per Assembly:	\leq 410.7 watts		
		d. Post-irradiation Cooling Time and Average Burnup Per Assembly:	As specified in Table 12B2-5 and for the applicable fuel assembly class.		
		e. Nominal Fresh Fuel Design Assembly Length (in.):	≤ 176.1		
		f. Nominal Fresh Fuel Design Assembly Width (in.):	<u>≤</u> 5.51		
		g. Fuel Assembly Weight (lbs):	\leq 683, including channels		
	B.	Quantity per CANISTER: Up to 5	6 BWR INTACT FUEL ASSEMBLIES		
	C.	BWR INTACT FUEL ASSEMB	LIES can be unchanneled or channeled with		
		Zircaloy channels.			
	D.	BWR INTACT FUEL ASSEMB be loaded.	LIES with stainless steel channels shall not		
	E.	Stainless steel fuel spacers may BWR INTACT FUEL ASSEMBI length to facilitate handling.	be used in CANISTERS to axially position LIES that are shorter than the available cavity		
	F.	Unenriched fuel assemblies are no	ot authorized for loading.		

Table 12B2-1

Fuel Assembly Limits (continued)

- G. The minimum length of the BWR INTACT FUEL ASSEMBLY internal structure and bottom end fitting and/or spacers shall ensure that the minimum distance to the fuel region from the base of the CANISTER is 6.2 inches.
- III. NAC-UMS[®] Advanced CANISTER: PWR FUEL

b. Enrichment:

- A. Allowable Contents
 - 1. Uranium oxide PWR INTACT FUEL ASSEMBLIES listed in Table 12B2-10 and meeting the following specifications:
 - a. Cladding Type:

Zircaloy with thickness as specified in Table 12B2-10 for the applicable fuel assembly class

Maximum and minimum enrichments are 5.0 and 1.7 wt % ²³⁵U, respectively. Fuel enrichment, burnup and cool time are related as shown in Tables 12B2-11 through 12B2-13.

For enrichments up to 4.6 wt $\%^{235}$ U, a boron concentration of 2,000 ppm is required for water in the CANISTER. For enrichments greater than 4.6 wt $\%^{235}$ U, a boron concentration of 2,300 ppm is required.

For variable enrichment fuel assemblies, maximum enrichment represents the peak rod enrichment.

As specified in Tables 12B2-11 through 12B2-13.

 ≤ 178.3

< 8.54

based on fuel assembly heat load.

c. Decay Heat Per Assembly: $\leq 1,100$ watts

 d. Post-irradiation Cooling Time and Average Burnup Per Assembly:

- e. Nominal Fresh Fuel Assembly Length (in.):
- f. Nominal Fresh Fuel Assembly Width (in.):
- g. Fuel Assembly Weight (lbs.): $\leq 1,602$

Table 12B2-1 Fuel Assembly Limits (continued)

- B. Quantity per CANISTER: Up to 32 PWR INTACT FUEL ASSEMBLIES.
- C. PWR INTACT FUEL ASSEMBLIES may contain thimble plugs and burnable poison inserts (Class 1 and Class 2 contents).
- D. PWR INTACT FUEL ASSEMBLIES shall not contain control components.
- E. Stainless steel spacers may be used in CANISTERS to axially position PWR INTACT FUEL ASSEMBLIES that are shorter than the available cavity length to facilitate handling.
- F. Unenriched fuel assemblies are not authorized for loading.
- G. PWR INTACT FUEL ASSEMBLIES with a burnup between 45,000 and 55,000 MWD/MTU meeting the requirements of Section A 5.7(1).
- H. The minimum length of the PWR INTACT FUEL ASSEMBLY internal structure and bottom end fitting and/or spacers shall ensure that the minimum distance to the fuel region from the base of the CANISTER is 1.5 inches.
- I. PWR INTACT FUEL ASSEMBLIES with one or more grid spacers missing or damaged such that the unsupported length of the fuel rods does not exceed 60 inches. End fitting damage including damaged or missing hold-down springs is allowed, as long as the assembly can be handled safely by normal means.

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										Min. Guide
Fuel			Max.	No of	Max.	Min. Rod	Min. Clad	Max. Pellet	Max. Active	Tube Thick
Class ¹	Vendor ²	Агтау	MTU	Fuel Rods	Pitch (in)	Dia. (in)	Thick (in)	Dia.(in)	Length (in)	(in)
1	CE	14×14	0.404	176	0.590	0.438	0.024	0.380	137.0	0.034
1	Ex/ANF	14×14	0.369	179	0.556	0.424	0.030	0.351	142.0	0.034
1	WE	14×14	0.362	179	0.556	0.400	0.024	0.345	144.0	0.034
1	WE	14×14	0.415	179	0.556	0.422	0.022	0.368	145.2	0.034
1	WE, Ex/ANF	15×15	0.465	204	0.563	0.422	0.024	0.366	144.0	0.015
1	Ex/ANF	17×17	0.413	264	0.496	0.360	0.025	0.303	144.0	0.016
1	WE	17×17	0.468	264	0.496	0.374	0.022	0.323	144.0	0.016
1	WE	17×17	0.429	264	0.496	0.360	0.022	0.309	144.0	0.016
2	B&W	15×15	0.481	208	0.568	0.430	0.026	0.369	144.0	0.016
2	B&W	17×17	0.466	264	0.502	0.379	0.024	0.324	143.0	0.017
3	CE	16×16	0.442	2364	0.506	0.382	0.023	0.3255	150.0	0.035
1	Ex/ANF ³	14×14	0.375	179	0.556	0.417	0.030	0.351	144.0	0.036
1	CE ³	15×15	0.432	216	0.550	0.418	0.026	0.358	132.0	
1	Ex/ANF ³	15×15	0.431	216	0.550	0.417	0.030	0.358	131.8	
1	CE ³	16×16	0.403	236	0.506	0.382	0.023	0.3255	136.7	0.035

Table 12B2-2 PWR Fuel Assembly Characteristics for the Standard CANISTER

- Note: Parameters shown are nominal pre-irradiation values.
 Maximum Initial Enrichment: 4.2 wt % ²³⁵U. All fuel rods are Zircaloy clad.
- 2. Vendor ID indicates the source of assembly base parameters, which are nominal, pre-irradiation values. Loading of assemblies meeting above limits is not restricted to the vendor(s) listed.
- 3. 14×14, 15×15 and 16×16 fuel manufactured for Prairie Island, Palisades and St. Lucie 2 cores, respectively. These are not generic fuel assemblies provided to multiple reactors.
- 4. Some fuel rod positions may be occupied by burnable poison rods or solid filler rods.

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Fuel	Vendor ⁴	Аттау	Max. MTU	No of Fuel Rods	Max. Pitch (in)	Min. Rod Dia. (in)	Min. Clad Thick (in)	Max. Pellet Dia.(in)	Max. Active Length (in) ²
A ⁵	Fy/ANF	7×7	0.196	48	0.738	0.570	0.036	0.490	144.0
4	Ex/ANE	8×8	0.177	63	0.641	0.484	0.036	0.405	145.2
4	Ex/ANF	9 × 9	0.173	79	0.572	0.424	0.030	0.357	145.2
4	GE	7 × 7	0.199	49	0.738	0.570	0.036	0.488	144.0
4	GE	7 × 7	0.198	49	0.738	0.563	0.032	0.487	144.0
4	GE	8 × 8	0.173	60	0.640	0.484	0.032	0.410	145.2
4	GE	8 × 8	0.179	62	0.640	0.483	0.032	0.410	145.2
4	GE	8 × 8	0.186	63	0.640	0.493	0.034	0.416	144.0
5	Ex/ANF	8×8	0.180	62	0.641	0.484	0.036	0.405	150.0
5	Ex/ANF	9×9	0.167	74 ³	0.572	0.424	0.030	0.357	150.0
56	Ex/ANF	9×9	0.178	79 ³	0.572	0.424	0.030	0.357	150.0
5	GE	7 × 7	0.198	49	0.738	0.563	0.032	0.487	144.0
5	GE	8×8	0.179	60	0.640	0.484	0.032	0.410	150.0
5	GE	8×8	0.185	62	0.640	0.483	0.032	0.410	150.0
5	GE	8×8	0.188	63	0.640	0.493	0.034	0.416	146.0
5	GE	9×9	0.186	74 ³	0.566	0.441	0.028	0.376	150.0
5	GE	9×9	0.198	79 ³	0.566	0.441	0.028	0.376	150.0

BWR Fuel Assembly Characteristics for the Standard CANISTER Table 12B2-3

Note: Parameters shown are nominal pre-irradiation values.

1. Maximum Initial Peak Planar Average Enrichment 4.0 wt % ²³⁵U. All fuel rods are Zircaloy clad.

2. 150 inch active fuel length assemblies contain 6" natural uranium blankets on top and bottom.

3. Shortened active fuel length in some rods.

4. Vendor ID indicates the source of assembly base parameters, which are nominal, pre-irradiation values. Loading of assemblies meeting above limits is not restricted to the vendor(s) listed.

5. UMS Class 4 and 5 for BWR 2/3 fuel.

6. Assembly width including channel. Unchanneled or channeled assemblies may be loaded based on a maximum channel thickness of 120 mil.

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Table 12B2-4Minimum Cooling Time Versus Burnup/Initial Enrichment for PWR Fuel in
the Standard CANISTER

	r							
Minimum								
Initial	Bı	ırnup ≤30	GWD/M	TU	30<	Burnup ≤	35 GWD/	MTU
Enrichment	Minin	num Cool	ing Time	[years]	Minin	num Cooli	ing Time	[years]
wt % ²³⁵ U (E)	14×14	15×15	16×16	17×17	14×14	15×15	16×16	17×17
$1.9 \le E < 2.1$	5	5	5	5	7	7	5	7
$2.1 \le E < 2.3$	5	5	5	5	7	6	5	6
$2.3 \le E < 2.5$	5	5	5	5	6	6	5	6
$2.5 \le E < 2.7$	5	5	5	5	6	6	5	6
$2.7 \le E < 2.9$	5	5	5	5	6	5	5	5
$2.9 \le E < 3.1$	5	5	5	5	5	5	5	5
$3.1 \le E < 3.3$	5	5	5	5	5	5	5	5
$3.3 \le E < 3.5$	5	5	5	5	5	5	5	5
$3.5 \le E < 3.7$	5	5	5	5	5	5	5	5
$3.7 \le E \le 4.2$	5	5	5	5	5	5	5	5
Minimum								
Initial	35<	Burnup ≤	40 GWD/I	MTU	40< 1	Burnup ≤4	45 GWD/.	MTU
Enrichment	Minin	num Cooli	ng Time	[years]	Minimum Cooling Time [years]			
wt % ²³⁵ U (E)	14×14	15×15	16×16	17×17	14×14	15×15	16×16	17×17
$1.9 \le E < 2.1$	10	10	7	10	15	15	11	15
$2.1 \le E < 2.3$	9	9	7	9	14	13	10	13
$2.3 \le E < 2.5$	8	8	6	8	12	13	10	12
$2.5 \le E < 2.7$	8	8	6	8	11	13	10	12
$2.7 \le E < 2.9$	7	8	6	8	10	12	9	12
$2.9 \le E < 3.1$	7	8	6	8	9	12	9	11
$3.1 \le E < 3.3$	6	8	6	7	8	12	9	10
$3.3 \le E < 3.5$	6	8	6	7	8	12	9	10
$3.5 \le E < 3.7$	6	8	6	6	8	11	9	10
				1				

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 $3.7 \le E \le 4.0$

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Minimum Cooling Time Versus Burnup/Initial Enrichment for BWR Fuel in Table 12B2-5 the Standard CANISTER

Minimum							
Initial	Burn	up ≤30 GWI)/MTU	30< Burnup ≤35 GWD/MTU			
Enrichment	Minimur	n Cooling Ti	me [years]	Minimum	Cooling Tin	ne [years]	
wt % ²³⁵ U (E)	7×7 8×8 9×9			7×7	8×8	9×9	
$1.9 \le E < 2.1$	5	5	5	8	7	7	
$2.1 \le E < 2.3$	5	5	5	6	6	6	
$2.3 \le E < 2.5$	5	5	5	5	- 5	5	
$2.5 \le E < 2.7$	5	5	5	5	5	5	
$2.7 \le E < 2.9$	5	5	5	5	5	5	
$2.9 \le E < 3.1$	5	5	5	5	5	5	
$3.1 \le E < 3.3$	5	5	5	5	5	5	
$3.3 \le E < 3.5$	5	5	5	5	5	5	
$3.5 \le E < 3.7$	5	5	5	5	5	5	
$3.7 \le E \le 4.0$	5	5	5	5	5	5	
	· · · · · · · · · · · · · · · · · · ·						
Minimum							
Initial	35< Bu	rnup ≤40 GV	VD/MTU	40< Bur	nup ≤45 GW	D/MTU	
Enrichment	Minimu	m Cooling Ti	ime [years]	Minimun	n Cooling Tin	ne [years]	
wt % ²³⁵ U (E)	7×7	8×8	9×9	7×7	8×8	9×9	
$1.9 \le E < 2.1$	16	14	15	26	24	25	
$2.1 \le E < 2.3$	13	12	12	23	21	22	
$2.3 \le E < 2.5$	9	8	8	18	16	17	
$2.5 \le E < 2.7$	8	7	7	15	14	14	
$2.7 \le E < 2.9$	7	6	6	13	11	12	
$2.9 \le E < 3.1$	6	6	6	11	10	10	
$3.1 \le E < 3.3$	6	5	6	9	8	9	
$3.3 \le E < 3.5$	6	5	6	8	7	8	
256527	6	5	6	7	7	7	

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Table 12B2-6	Maine Yankee Site Specific Fuel Canister Loading Position Summary
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Site Specific Spent Fuel Configurations ¹	Est. Number of Assemblies ²	Canister Loading Position ⁷
Total Number of Fuel Assemblies ³	1,434	Any
Inserted Control Element Assembly (CEA)	168	Any
Inserted In-Core Instrument (ICI) Thimble	138	Any
Consolidated Fuel	2	Corner ⁴
Fuel Rod Replaced by Rod Enriched to 1.95 wt %	3	Any
Fuel Rod Replaced by Stainless Steel Rod or Zircaloy Rod	18	Any
Fuel Rods Removed	10	Corner ⁴
Variable Enrichment ⁶	72	Any
Variable Enrichment and Axial Blanket ⁶	68	Any
Burnable Poison Rod Replaced by Hollow Zircaloy Rod	80	Corner ⁴
Damaged Fuel in MAINE YANKEE FUEL CAN	12	Corner ⁴
Burnup between 45,000 and 50,000 MWD/MTU	90	Periphery ⁵
MAINE YANKEE FUEL CAN	As Required	Corner ⁴
Inserted Start-up Source	4	Corner ⁴
Inserted CEA Finger Tip or ICI String Segment	1	Corner ⁴

- 1. All spent fuel, including that held in a Maine Yankee fuel can, must conform to the loading limits presented in Tables 12B2-8 and 12B2-9 for cool time.
- 2. The number of fuel assemblies in some categories may vary depending on future fuel inspections.
- 3. Includes these site specific spent fuel configurations and standard fuel assemblies. Standard fuel assemblies may be loaded in any canister position.
- 4. Basket corner positions are positions 3, 6, 19, and 22 in Figure 12B2-1. Corner positions are also periphery positions.
- 5. Basket periphery positions are positions 1, 2, 3, 6, 7, 12, 13, 18, 19, 22, 23, and 24 in Figure 12B2-1. Periphery positions include the corner positions.
- 6. Variably enriched fuel assemblies have a maximum burnup of less than 30,000 MWD/MTU and enrichments greater than 1.9 wt %. The minimum required cool time for these assemblies is 5 years.
- 7. Maine Yankee Site Specific Fuel may be loaded only in the Standard Canister.

Table 12B2-7

Maine Yankee Site Specific Fuel Limits

A. Allowable Contents

- 1. Combustion Engineering 14 × 14 PWR INTACT FUEL ASSEMBLIES meeting the specifications presented in Tables 12B2-1, 12B2-2 and 12B2-4 loaded in the Standard CANISTER.
- 2. PWR INTACT FUEL ASSEMBLIES may contain inserted Control Element Assemblies (CEA), In-Core Instrument (ICI) Thimbles or CEA Flow Plugs. CEAs or CEA Plugs may not be inserted in damaged fuel assemblies, consolidated fuel assemblies or assemblies with irradiated stainless steel replacement rods. Fuel assemblies with a CEA or CEA Plug inserted must be loaded in a Standard Class 2 CANISTER and cannot be loaded in a Standard Class 1 CANISTER. Fuel assemblies without an inserted CEA or CEA Plug, including those with inserted ICI Thimbles, must be loaded in a Standard Class 1 CANISTER.
- 3. PWR INTACT FUEL ASSEMBLIES with fuel rods replaced with stainless steel or Zircaloy rods or with Uranium oxide rods nominally enriched up to 1.95 wt %.
- 4. PWR INTACT FUEL ASSEMBLIES with fuel rods having variable enrichments with a maximum fuel rod enrichment up to 4.21 wt % ²³⁵U and that also have a maximum planar average enrichment up to 3.99 wt % ²³⁵U.
- 5. PWR INTACT FUEL ASSEMBLIES with annular axial end blankets. The axial end blanket enrichment may be up to 2.6 wt % ²³⁵U.
- 6. PWR INTACT FUEL ASSEMBLIES with solid filler rods or burnable poison rods occupying up to 16 of 176 fuel rod positions.
- 7. PWR INTACT FUEL ASSEMBLIES with one or more grid spacers missing or damaged such that the unsupported length of the fuel rods does not exceed 60 inches or with end fitting damage, including damaged or missing hold-down springs, as long as the assembly can be handled safely by normal means.
- B. Allowable Contents requiring preferential loading based on shielding, criticality or thermal constraints. The preferential loading requirement for these fuel configurations is as described in Table 12B2-6.
 - 1. PWR INTACT FUEL ASSEMBLIES with up to 176 fuel rods missing from the fuel assembly lattice.
 - 2. PWR INTACT FUEL ASSEMBLIES with a burnup between 45,000 and 50,000 MWD/MTU meeting the requirements of Section A 5.7(1).

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Table 12B2-7

Maine Yankee Site Specific Fuel Limits (continued)

- 3. PWR INTACT FUEL ASSEMBLIES with a burnable poison rod replaced by a hollow Zircaloy rod.
- 4. INTACT FUEL ASSEMBLIES with a start-up source in a center guide tube. The assembly must be loaded in a basket corner position and must be loaded in a Standard Class 1 CANISTER. Only one (1) start-up source may be loaded in any fuel assembly or any CANISTER.
- 5. PWR INTACT FUEL ASSEMBLIES with CEA ends (finger tips) and/or ICI segment inserted in corner guide tube positions. The assembly must also have a CEA plug installed. The assembly must be loaded in a basket corner position and must be loaded in a Standard Class 2 CANISTER.
- 6. INTACT FUEL ASSEMBLIES may be loaded in a MAINE YANKEE FUEL CAN.
- 7. FUEL enclosed in a MAINE YANKEE FUEL CAN. The MAINE YANKEE FUEL CAN can only be loaded in a Standard Class 1 CANISTER. The contents that must be loaded in the MAINE YANKEE FUEL CAN are:
 - a) PWR fuel assemblies with up to two INTACT or DAMAGED FUEL rods inserted in each fuel assembly guide tube or with up to two burnable poison rods inserted in each guide tube. The rods inserted in the guide tubes cannot be from a different fuel assembly. The maximum number of rods in the fuel assembly (fuel rods plus inserted rods, including burnable poison rods) is 176.
 - b) A DAMAGED FUEL ASSEMBLY with up to 100% of the fuel rods classified as damaged and/or damaged or missing assembly hardware components. A DAMAGED FUEL ASSEMBLY cannot have an inserted CEA or other non-fuel component.
 - c) Individual INTACT or DAMAGED FUEL rods in a rod type structure, which may be a guide tube, to maintain configuration control.
 - d) FUEL DEBRIS consisting of fuel rods with exposed fuel pellets or individual intact or partial fuel pellets not contained in fuel rods.

Table 12B2-7Maine Yankee Site Specific Fuel Limits (continued)

- e) CONSOLIDATED FUEL lattice structure with a 17×17 array formed by grids and top and bottom end fittings connected by four solid stainless steel rods. Maximum contents are 289 fuel rods having a total lattice weight $\leq 2,100$ pounds. A CONSOLIDATED FUEL lattice cannot have an inserted CEA or other non-fuel component. Only one CONSOLIDATED FUEL lattice may be stored in any CANISTER.
- f) HIGH BURNUP FUEL assemblies not meeting the criteria of Section A 5.7(1).
- C. Unenriched fuel assemblies are not authorized for loading.
- D. A Standard canister preferentially loaded in accordance with Table 12B2-8 may only contain fuel assemblies selected from the same loading pattern.

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Table 12B2-8Loading Table for Maine Yankee CE 14 × 14 Fuel with No Non-Fuel Material –
Required Cool Time in Years Before Assembly is Acceptable

	Bur	nup ≤ 30 GWD/N	ITU - Minimum (Cool Time [years]	for ¹
Enrichment	Standard ²	Pref (0.958i)	Pref (0.958p)	Pref (1.05i)	Pref (1.05p)
$1.9 \le E \le 2.1$	5	5	5	5	5
$2.1 \le E < 2.3$	5	5	5	5	5
$2.3 \le E < 2.5$	5	5	5	5	5
$2.5 \le E < 2.7$	5	5	5	5	5
$2.7 \le E < 2.9$	5	5	5	5	5
$2.9 \le E < 3.1$	5	5	5	5	5
$3.1 \le E < 3.3$	5	5	5	5	5
$3.3 \le E < 3.5$	5	5	5	5	5
$3.5 \le E < 3.7$	5	5	5	5	5
$3.7 \le E \le 4.2$	5	5	5	5	5
	30 < B	Surnup ≤ 35 GWI)/MTU - Minimu	m Cool Time [yea	rs] for
Enrichment	Standard ²	Pref (0.958i)	Pref (0.958p)	Pref (1.05i)	Pref (1.05p)
$1.9 \le E < 2.1$	5	5	5	5	5
$2.1 \le E < 2.3$	5	5	5	5	5
$2.3 \le E < 2.5$	5	5	5	5	5
$2.5 \le E \le 2.7$	5	5	5	5	5
$2.7 \le E < 2.9$	5	5	5	5	5
$2.9 \le E < 3.1$	5	5	5	5	5
$3.1 \le E < 3.3$	5	5	5	5	5
$3.3 \le E < 3.5$	5	5	5	5	5
$3.5 \le E < 3.7$	5	5	5	5	5
$3.7 \le E \le 4.2$	5	5	5	5	5
	35 < B	urnup ≤ 40 GWI)/MTU - Minimu	m Cool Time [yea	rs] for
Enrichment	Standard ²	Pref (0.958i)	Pref (0.958p)	Pref (1.05i)	Pref (1.05p)
$1.9 \le E \le 2.1$	7	7	6	15	5
$2.1 \le E < 2.3$	6	6	6	15	5
$2.3 \le E \le 2.5$	6	6	5	14	5
$2.5 \le E < 2.7$	5	5	5	14	5
$2.7 \le E < 2.9$	5	5	5	14	5
$2.9 \le E < 3.1$	5	5	5	6	5
$3.1 \le E < 3.3$	5	5	5	6	5
$3.3 \le E < 3.5$	5	5	5	6	5
$3.5 \le E < 3.7$	5	5	5	6	5
$3.7 \le E \le 4.2$	5	5	5	6	5

1. Cool times for preferential loading of fuel assemblies with a decay heat of either 0.958 or 1.05 kw per assembly, loaded in either interior (i) or periphery (p) basket positions. All of the fuel assemblies in a canister must be selected using the same preferential loading pattern (Standard, 0.958 kW or 1.05 kW).

2. Fuel assemblies with cool times from 5 to 7 years must be preferentially loaded based on cool time, with fuel with the shortest cool time in the basket interior, in accordance with Section B2.1.2.

Table 12B2-8	Loading Table for Maine Yankee CE 14 × 14 Fuel with No Non-Fuel Material –
	Required Cool Time in Years Before Assembly is Acceptable (continued)

	$40 < Burnup \le 45 GWD/MTU - Minimum Cool Time [years] for1$								
Enrichment	Standard ²	Pref(0.958i)	Pref(0.958p)	Pref(1.05i)	Pref(1.05p)				
$1.9 \le E \le 2.1$	11	20	7	Not Allowed	6				
$2.1 \le E < 2.3$	9	15	7	Not Allowed	6				
$2.3 \le E < 2.5$	8	15	6	Not Allowed	6				
$2.5 \le E < 2.7$	8	15	6	Not Allowed	6				
$2.7 \le E < 2.9$	8	14	6	Not Allowed	6				
$2.9 \le E < 3.1$	8	14	6	Not Allowed	6				
$3.1 \le E < 3.3$	7	14	6	Not Allowed	5				
$3.3 \le E < 3.5$	6	14	6	Not Allowed	5				
$3.5 \le E \le 3.7$	6	13	6	Not Allowed	5				
$3.7 \le E \le 4.2$	6	13	6	Not Allowed	5				
	45 < Bu	rnup ≤ 50 GWD/	MTU - Minimu	m Cool Time [ye	ars] for				
Enrichment	Standard	Pref(0.958i)	Pref(0.958p)	Pref(1.05i)	Pref(1.05p)				
$1.9 \le E < 2.1$	Not Allowed	Not Allowed	8	Not Allowed	7				
$2.1 \le E < 2.3$	Not Allowed	Not Allowed	8	Not Allowed	7				
$2.3 \le E < 2.5$	Not Allowed	Not Allowed	8	Not Allowed	7				
$2.5 \le E < 2.7$	Not Allowed	Not Allowed	8	Not Allowed	7				
$2.7 \le E < 2.9$	Not Allowed	Not Allowed	8	Not Allowed	7				
$2.9 \le E < 3.1$	Not Allowed	Not Allowed	8	Not Allowed	7				
$3.1 \le E < 3.3$	Not Allowed	Not Allowed	7	Not Allowed	7				
$3.3 \le E < 3.5$	Not Allowed	Not Allowed	7	Not Allowed	6				
$3.5 \le E < 3.7$	Not Allowed	Not Allowed	7	Not Allowed	6				
37 < E < 4.2	Not Allowed	Not Allowed	7	Not Allowed	6				

- 1. Cool times for preferential loading of fuel assemblies with a decay heat of either 0.958 or 1.05 kw per assembly, loaded in either interior (i) or periphery (p) basket positions. All of the fuel assemblies in a canister must be selected using the same preferential loading pattern.
- 2. Fuel assemblies with cool times from 5 to 7 years must be preferentially loaded based on cool time, with fuel with the shortest cool time in the basket interior, in accordance with Section B2.1.2.

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Table 12B2-9Loading Table for Maine Yankee CE 14 × 14 Fuel Containing CEACooled to Indicated Time

	≤ 30 GWD/MTU Burnup - Minimum Cool Time in Years for							
Enrichment	No CEA (Class 1)	5 Year CEA	10 Year CEA	15 Year CEA	20 Year CEA			
$1.9 \le E \le 2.1$	5	5	5	5	5			
$2.1 \le E \le 2.3$	5	5	5	5	5			
$2.3 \le E \le 2.5$	5	5	5	5	5			
$2.5 \le E < 2.7$	5	5	5	5	5			
$2.7 \le E \le 2.9$	5	5	5	5	5			
$2.9 \le E < 3.1$	5	5	5	5	5			
$3.1 \le E < 3.3$	5	5	5	5	5			
$3.3 \le E \le 3.5$	5	5	5	5	5			
$3.5 \le E < 3.7$	5	5	5	5	5			
$3.7 \le E \le 4.2$	5	5	5	5	5			
	30 < Bur	$nup \le 35 \text{ GWD/M}$	ITU - Minimum C	ool Time in Years	for			
Enrichment	No CEA (Class 1)	5 Year CEA	10 Year CEA	15 Year CEA	20 Year CEA			
$1.9 \le E \le 2.1$	5	5	5	5	5			
$2.1 \le E < 2.3$	5	5	5	5	5			
$2.3 \le E \le 2.5$	5	5	5	5	5			
$2.5 \le E < 2.7$	5	5	5	5	5			
2.7 ≤ E < 2.9	5	5	5	5	5			
$2.9 \le E < 3.1$	5	5	5	5	5			
$3.1 \le E < 3.3$	5	5	5	5	5			
$3.3 \le E < 3.5$	5	5	5	5	5			
3.5 ≤ E < 3.7	5	5	5	5	5			
3.7 ≤ E ≤ 4.2	5	5	5	5	5			
1	35 < Burnun < 40 GWD/MTU - Minimum Cool Time in Vears for							
	35 < Bur	$nup \le 40 \text{ GWD/}N$	ITU - Minimum C	ool Time in Years	for			
Enrichment	35 < Bur No CEA (Class 1)	$\frac{\text{nup} \le 40 \text{ GWD/N}}{5 \text{ Year CEA}}$	1TU - Minimum C 10 Year CEA	ool Time in Years 15 Year CEA	for 20 Year CEA			
Enrichment 1.9 ≤ E < 2.1	35 < Bur No CEA (Class 1) 7	$\frac{\text{nup} \le 40 \text{ GWD/N}}{5 \text{ Year CEA}}$	ITU - Minimum C 10 Year CEA 7	ool Time in Years 15 Year CEA 7	for 20 Year CEA 7			
Enrichment 1.9 ≤ E < 2.1 2.1 ≤ E < 2.3	35 < Bur No CEA (Class 1) 7 6	nup ≤ 40 GWD/M 5 Year CEA 7 6	ITU - Minimum C 10 Year CEA 7 6	ool Time in Years 15 Year CEA 7 6	for 20 Year CEA 7 6			
Enrichment 1.9 ≤ E < 2.1 2.1 ≤ E < 2.3 2.3 ≤ E < 2.5	35 < Bur No CEA (Class 1) 7 6 6	nup ≤ 40 GWD/N 5 Year CEA 7 6 6 	1TU - Minimum C 10 Year CEA 7 6 6	001 Time in Years 15 Year CEA 7 6 6 6	for 20 Year CEA 7 6 6			
Enrichment $1.9 \le E < 2.1$ $2.1 \le E < 2.3$ $2.3 \le E < 2.5$ $2.5 \le E < 2.7$	35 < Bur No CEA (Class 1) 7 6 6 5 5	nup ≤ 40 GWD/N 5 Year CEA 7 6 5 5	1TU - Minimum C 10 Year CEA 7 6 6 5	ool Time in Years 15 Year CEA 7 6 6 5	for 20 Year CEA 7 6 6 5 			
Enrichment $1.9 \le E < 2.1$ $2.1 \le E < 2.3$ $2.3 \le E < 2.5$ $2.5 \le E < 2.7$ $2.7 \le E < 2.9$	35 < Bur No CEA (Class 1) 7 6 5 5	nup ≤ 40 GWD/N 5 Year CEA 7 6 6 5 5 5	1TU - Minimum C 10 Year CEA 7 6 6 5 5 5	ool Time in Years 15 Year CEA 7 6 6 5 5 5	for 20 Year CEA 7 6 6 5 5 5			
Enrichment $1.9 \le E < 2.1$ $2.1 \le E < 2.3$ $2.3 \le E < 2.5$ $2.5 \le E < 2.7$ $2.7 \le E < 2.9$ $2.9 \le E < 3.1$	35 < Bur No CEA (Class 1) 7 6 5 5 5	nup ≤ 40 GWD/N 5 Year CEA 7 6 5 5 5 5	1TU - Minimum C 10 Year CEA 7 6 6 5 5 5 5 5	ool Time in Years 15 Year CEA 7 6 6 5 5 5 5	for 20 Year CEA 7 6 6 5 5 5 5			
Enrichment $1.9 \le E < 2.1$ $2.1 \le E < 2.3$ $2.3 \le E < 2.5$ $2.5 \le E < 2.7$ $2.7 \le E < 2.9$ $2.9 \le E < 3.1$ $3.1 \le E < 3.3$	35 < Bur No CEA (Class 1) 7 6 5 5 5 5 5	$nup \leq 40 \text{ GWD/N}$ 5 Year CEA 7 6 6 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	1TU - Minimum C 10 Year CEA 7 6 6 5 5 5 5 5 5	ool Time in Years 15 Year CEA 7 6 6 5 5 5 5 5 5	for 20 Year CEA 7 6 5 5 5 5 5 5			
Enrichment $1.9 \le E < 2.1$ $2.1 \le E < 2.3$ $2.3 \le E < 2.5$ $2.5 \le E < 2.7$ $2.7 \le E < 2.9$ $2.9 \le E < 3.1$ $3.1 \le E < 3.3$ $3.3 \le E < 3.5$	35 < Bur No CEA (Class 1) 7 6 5 5 5 5 5 5 5 5 5	$nup \leq 40 \text{ GWD/N}$ 5 Year CEA 7 6 6 5 5 5 5 5 5 5 5 6	1TU - Minimum C 10 Year CEA 7 6 6 5 5 5 5 5 5 5 5 5 5 5 5 5	ool Time in Years 15 Year CEA 7 6 5 5 5 5 5	for 20 Year CEA 7 6 6 5 5 5 5 5 5 5 5 5 5 5 5 5			
Enrichment $1.9 \le E < 2.1$ $2.1 \le E < 2.3$ $2.3 \le E < 2.5$ $2.5 \le E < 2.7$ $2.7 \le E < 2.9$ $2.9 \le E < 3.1$ $3.1 \le E < 3.3$ $3.3 \le E < 3.5$ $3.5 \le E < 3.7$	35 < Bur No CEA (Class 1) 7 6 5 5 5 5 5 5 5 5 5 5 5 5	nup ≤ 40 GWD/N 5 Year CEA 7 6 6 5 5 5 5 5 5 5 5 5 5 5 5 5	1TU - Minimum C 10 Year CEA 7 6 6 5 5 5 5 5 5 5 5 5 5 5 5 5	5 5 6 6 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	for 20 Year CEA 7 6 6 5 5 5 5 5 5 5 5 5 5 5 5 5			
Enrichment $1.9 \le E < 2.1$ $2.1 \le E < 2.3$ $2.3 \le E < 2.5$ $2.5 \le E < 2.7$ $2.7 \le E < 2.9$ $2.9 \le E < 3.1$ $3.1 \le E < 3.3$ $3.3 \le E < 3.5$ $3.5 \le E < 3.7$ $3.7 \le E \le 4.2$	35 < Bur	nup ≤ 40 GWD/N 5 Year CEA 7 6 5 5 5 5 5 5 5 5 5 5 5 5 5	1TU - Minimum C 10 Year CEA 7 6 6 5 5 5 5 5 5 5 5 5 5 5 5 5	5 5 6 6 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	for 20 Year CEA 7 6 6 5 5 5 5 5 5 5 5 5 5 5 5 5			
Enrichment $1.9 \le E < 2.1$ $2.1 \le E < 2.3$ $2.3 \le E < 2.5$ $2.5 \le E < 2.7$ $2.7 \le E < 2.9$ $2.9 \le E < 3.1$ $3.1 \le E < 3.3$ $3.3 \le E < 3.5$ $3.5 \le E < 3.7$ $3.7 \le E \le 4.2$	35 < Bur No CEA (Class 1) 7 6 5 5 5 5 5 5 5 5 5 5 5 40 < Bur	nup ≤ 40 GWD/N 5 Year CEA 7 6 6 5 5 5 5 5 5 5 5 1 5 5 5 5 5 5 5 5 5 5 5 5 5	1TU - Minimum C 10 Year CEA 7 6 5 5 5 5 5 5 5 5 5 5 5 5 5	ool Time in Years 15 Year CEA 7 6 5 5 5 5 5 5 5 5 5 5 5 5 5	for 20 Year CEA 7 6 5 5 5 5 5 5 5 5 5 5 5 5 5			
Enrichment $1.9 \le E < 2.1$ $2.1 \le E < 2.3$ $2.3 \le E < 2.5$ $2.5 \le E < 2.7$ $2.7 \le E < 2.9$ $2.9 \le E < 3.1$ $3.1 \le E < 3.3$ $3.3 \le E < 3.5$ $3.5 \le E < 3.7$ $3.7 \le E \le 4.2$ Enrichment	35 < Bur No CEA (Class 1) 7 6 6 5 5 5 5 5 5 5 5 6 6 6 6 5 5 40 < Bur	nup ≤ 40 GWD/N 5 Year CEA 7 6 6 5 5 5 5 5 5 5 1 5 5 5 1 5 5 5 5 5 5 5 5 5 5 5 5 5	1TU - Minimum C 10 Year CEA 7 6 6 5 5 5 5 5 5 5 5 5 5 5 5 5	Second Time in Years 15 Year CEA 7 6 5 6 7 6 7 6 7 6 7 6 7 <	for 20 Year CEA 7 6 5 5 5 5 5 5 5 5 5 5 5 5 5			
Enrichment $1.9 \le E < 2.1$ $2.1 \le E < 2.3$ $2.3 \le E < 2.5$ $2.5 \le E < 2.7$ $2.7 \le E < 2.9$ $2.9 \le E < 3.1$ $3.1 \le E < 3.3$ $3.3 \le E < 3.5$ $3.5 \le E < 3.7$ $3.7 \le E \le 4.2$ Enrichment $1.9 \le E < 2.1$	35 < Bur No CEA (Class 1) 7 6 6 6 5 5 5 5 5 5 5 5 5 5 40 < Bur	nup ≤ 40 GWD/N 5 Year CEA 7 6 5 5 5 5 5 5 5 1 1 1 1 1 1 1 1 1 1 1 1 1	1TU - Minimum C 10 Year CEA 7 6 5 5 5 5 5 5 5 5 5 5 1TU - Minimum C 10 Year CEA 11	Second Time in Years 15 Year CEA 7 6 5 15 Year CEA 11	for 20 Year CEA 7 6 5 5 5 5 5 5 5 5 5 5 5 5 5			
Enrichment $1.9 \le E < 2.1$ $2.1 \le E < 2.3$ $2.3 \le E < 2.5$ $2.5 \le E < 2.7$ $2.7 \le E < 2.9$ $2.9 \le E < 3.1$ $3.1 \le E < 3.3$ $3.3 \le E < 3.5$ $3.5 \le E < 3.7$ $3.7 \le E \le 4.2$ Enrichment $1.9 \le E < 2.1$ $2.1 \le E < 2.3$	35 < Bur No CEA (Class 1) 7 6 6 6 5 5 5 5 5 5 5 5 5 5 40 < Bur	nup ≤ 40 GWD/N 5 Year CEA 7 6 5 5 5 5 5 5 5 1 1 1 9 9 1 9 1 9 1 1 9 1 9 1 1 9 1 1 1 1 9 1 1 1 1 1 1 1 1 1 1 1 1 1	1TU - Minimum C 10 Year CEA 7 6 5 5 5 5 5 5 5 5 1TU - Minimum C 10 Year CEA 11 9	Second Time in Years 15 Year CEA 7 6 5 6 7 6 7 5 5 5 5 5 6 7 6 7 6 7 6 7 6 7 6 7 <	for 20 Year CEA 7 6 5 5 5 5 5 5 5 5 5 5 5 5 5			
Enrichment $1.9 \le E < 2.1$ $2.1 \le E < 2.3$ $2.3 \le E < 2.5$ $2.5 \le E < 2.7$ $2.7 \le E < 2.9$ $2.9 \le E < 3.1$ $3.1 \le E < 3.3$ $3.3 \le E < 3.5$ $3.5 \le E < 3.7$ $3.7 \le E \le 4.2$ Enrichment $1.9 \le E < 2.1$ $2.1 \le E < 2.3$ $2.3 \le E < 2.5$	35 < Bur No CEA (Class 1) 7 6 6 5 5 5 5 5 5 5 5 5 5 0 6 6 6 5 5 5 5 0 5 0 6 0 8 0 8	nup ≤ 40 GWD/N 5 Year CEA 7 6 5 5 5 5 5 5 5 1 5 1 5 1 5 1 5 5 5 5 5 5 5 5 5 5 5 5 5	1TU - Minimum C 10 Year CEA 7 6 5 5 5 5 5 1TU - Minimum C 10 Year CEA 11 9 8	Second Time in Years 15 Year CEA 7 6 5 6 7 6 5 5 5 6 7 5 5 5 6 7 6 7 6 7 6 7 6 7 7 7 7 7 <	for 20 Year CEA 7 6 5 5 5 5 5 5 5 5 5 5 5 5 5			
Enrichment $1.9 \le E < 2.1$ $2.1 \le E < 2.3$ $2.3 \le E < 2.5$ $2.5 \le E < 2.7$ $2.7 \le E < 2.9$ $2.9 \le E < 3.1$ $3.1 \le E < 3.3$ $3.3 \le E < 3.5$ $3.5 \le E < 3.7$ $3.7 \le E \le 4.2$ Enrichment $1.9 \le E < 2.1$ $2.1 \le E < 2.3$ $2.3 \le E < 2.5$ $2.5 \le E < 2.7$	35 < Bur No CEA (Class 1) 7 6 6 5 5 5 5 5 5 5 5 5 40 < Bur	nup ≤ 40 GWD/N 5 Year CEA 7 6 5 5 5 5 5 5 5 5 5 5 10 9 8 8	1TU - Minimum C 10 Year CEA 7 6 5 5 5 5 5 1TU - Minimum C 10 Year CEA 11 9 8 8 8	Second Time in Years 15 Year CEA 7 6 5 5 5 5 5 5 5 5 5 6 7 6 6 5 5 5 5 5 5 5 6 7 6 6 5 5 5 5 6 7 6 7 5 5 5 6 7 6 7 7 7 6 7 6 7 8 8	for 20 Year CEA 7 6 5 5 5 5 5 5 5 5 5 5 5 5 5			
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Enrichment $1.9 \le E < 2.1$ $2.1 \le E < 2.3$ $2.3 \le E < 2.5$ $2.5 \le E < 2.7$ $2.7 \le E < 2.9$ $2.9 \le E < 3.1$ $3.1 \le E < 3.3$ $3.3 \le E < 3.5$ $3.5 \le E < 3.7$ $3.7 \le E \le 4.2$ Enrichment $1.9 \le E < 2.1$ $2.1 \le E < 2.3$ $2.3 \le E < 2.5$ $2.5 \le E < 2.7$ $2.7 \le E < 2.9$ $2.9 \le E < 3.1$ $3.1 \le E < 3.3$ $3.3 \le E < 3.5$	35 < Bur No CEA (Class 1) 7 6 6 5 5 5 5 5 5 5 5 5 5 0 6 0 6 0 7 0 6	nup ≤ 40 GWD/N 5 Year CEA 7 6 5 5 5 5 5 5 5 5 5 5 11 9 8 8 7 6	1TU - Minimum C 10 Year CEA 7 6 5 5 5 5 5 5 1TU - Minimum C 10 Year CEA 11 9 8 8 8 8 8 8 8 8 8 8 7	Second Time in Years 15 Year CEA 7 6 5 5 5 5 5 5 5 5 5 6 7 6 6 5 5 5 5 5 5 6 5 5 5 5 5 5 5 5 6 7	for 20 Year CEA 7 6 5 5 5 5 5 5 5 5 5 5 5 5 5			
Enrichment $1.9 \le E < 2.1$ $2.1 \le E < 2.3$ $2.3 \le E < 2.5$ $2.5 \le E < 2.7$ $2.7 \le E < 2.9$ $2.9 \le E < 3.1$ $3.1 \le E < 3.3$ $3.3 \le E < 3.5$ $3.5 \le E < 3.7$ $3.7 \le E \le 4.2$ Enrichment $1.9 \le E < 2.1$ $2.1 \le E < 2.3$ $2.3 \le E < 2.5$ $2.5 \le E < 2.7$ $2.7 \le E < 2.9$ $2.9 \le E < 3.1$ $3.1 \le E < 3.3$ $3.3 \le E < 3.5$ $3.5 \le E < 3.7$	35 < Bur No CEA (Class 1) 7 6 6 5 5 5 5 5 5 5 5 5 5 0 6 0 6 0 7 0 8 8 8 7 6 6 6	nup ≤ 40 GWD/N 5 Year CEA 7 6 5 5 5 5 5 5 5 5 5 6 7 6 8 8 7 6 6 6 6 6	1TU - Minimum C 10 Year CEA 7 6 5 5 5 5 5 5 1TU - Minimum C 10 Year CEA 11 9 8 8 8 8 8 8 8 8 8 7 6	Second Time in Years 15 Year CEA 7 6 5 5 5 5 5 5 5 5 5 6 7 6 7 5 5 5 5 5 7 8 8 8 8 7 6	for 20 Year CEA 7 6 5 5 5 5 5 5 5 5 5 5 5 5 5			

Fuel Class	Array ^{1,2,3}	Max. MTU	No of Fuel Rods ⁴	Max. Pitch (in)	Min. Rod Dia. (in)	Min. Clad Thick (in) ⁵	Max. Pellet Dia.(in)	Max. Active Length (in)	Min. Guide Tube Thick (in)
1	14×14	0.4124	176	0.5800	0.440	0.0260	0.3805	137.0	0.036
1	14×14	0.3873	176	0.5800	0.440	0.0260	0.3815	128.0	0.026
1	14×14	0.3741	179	0.5560	0.400	0.0243	0.3505	144.0	0.017
1	14×14	0.4144	179	0.5560	0.417	0.0218	0.3674	145.2	0.017
1	15×15	0.4423	204	0.5630	0.417	0.0265	0.3570	144.0	0.017
1	15×15	0.4671	204	0.5630	0.422	0.0242	0.3669	144.0	0.015
1	15×15	0.4341	216	0.5500	0.415	0.0240	0.3590	132.0	0.0165
1	16×16	0.4025	236	0.5060	0.382	0.0250	0.3250	136.7	0.026
1	17×17	0.4282	264	0.4960	0.360	0.0225	0.3088	144.0	0.015
1	17×17	0.4691	264	0.4960	0.372	0.0205	0.3232	144.0	0.014
2	15×15	0.4807	208	0.5680	0.430	0.0265	0.3686	144.0	0.016
2	15×15	0.4954	208	0.5680	0.428	0.0230	0.3742	144.0	0.014
2	15×15	0.4642	208	0.5680	0.414	0.0220	0.3622	144.0	0.014
2	17×17	0.4749	264	0.5020	0.377	0.0220	0.3252	144.0	0.0175
3	16×16	0.4417	236	0.5063	0.382	0.0250	0.3250	150.0	0.035

PWR Fuel Assembly Characteristics for the Advanced CANISTER Table 12B2-10

Maximum initial enrichment up to 4.6 wt $\%^{235}$ U with a boron concentration of 2,000 ppm in pool and canister water. For enrichments greater than 4.6 wt $\%^{235}$ U, a boron concentration of 2,300 ppm is required. 1.

Fuel assembly parameters are based on bounding values that may not correspond to the parameters of a specific assembly. 2.

Assemblies meeting these limits may contain a flow mixer, an ICI thimble, or a burnable poison rod insert. 3.

Some fuel rod positions may be occupied by burnable poison rods or solid filler rods. 4.

All fuel rods are Zircaloy clad. 5.

Table 12B2-11Minimum Cooling Time versus Burnup/Initial Enrichment for PWR FuelAssembly Heat Loads ≤ 700 W in the Advanced CANISTER

Minimum Initial Enrichment	Mir	Burnup ≤30 GWD/MTU Minimum Cooling Time [years]				30< Burnup ≤35 GWD/MTU Minimum Cooling Time [years]			
wt % ²³⁵ U (E)	14×14	15×15	16×16	17×17	14×14	15×15	16×16	17×17	
$1.7 \le E \le 1.9$	6	7	6	7	7	9	7	8	
$1.9 \le E < 2.1$	6	6	6	6	7	8	7	8	
$2.1 \le E < 2.3$	6	6	6	6	. 7	8	7	8	
$2.3 \le E < 2.5$	5	6	6	6	7	8	7	8	
$2.5 \le E < 2.7$	5	6	6	6	7	8	7	8	
$2.7 \le E < 2.9$	5	6	6	6	6	8	7	8	
$2.9 \le E < 3.1$	5	6	6	6	6	8	7	8	
$3.1 \le E < 3.3$	5	6	6	6	6	8	7	8	
$3.3 \le E < 3.5$	5	6	6	6	6	8	7	8	
$3.5 \le E < 3.7$	5	6	6	6	6	8	7	8	
$3.7 \le E < 3.9$	5	6	6	6	6	8	7	7	
$3.9 \le E < 4.1$	5	6	5	6	6	7	7	7	
$4.1 \le E < 4.3$	5	6	5	6	6	7	7	7	
$4.3 \le E < 4.5$	5	6	5	6	6	7	7	7	
$4.5 \le E < 4.7$	5	. 6	5	6	6	7	6	7	
$4.7 \le E < 4.9$	5	6	5	6	6	7	6	7	
E ≥ 4.9	5	6	5	6	6	7	6	7	
-									
Minimum Initial	35	s ≤ Burnup ≤	40 GWD/M	TU	40	< Burnup ≤4	45 GWD/M'	ΓU	
Minimum Initial Enrichment	35 Mii	i< Burnup ≤ nimum Cool	40 GWD/M ing Time [ye	TU ears]	40 Min	< Burnup ≤4 imum Cooli	45 GWD/M' ing Time [ye	ΓU ars]	
Minimum Initial Enrichment wt % ²³⁵ U (E)	35 Min 14×14	S< Burnup ≤ nimum Cool 15×15	40 GWD/M ing Time [yo 16×16	TU ears] 17×17	40 Min 14×14	< Burnup ≤4 imum Cooli 15×15	45 GWD/M′ ing Time [ye 16×16	ΓU ears] 17×17	
$\begin{array}{l} \mbox{Minimum Initial} \\ \mbox{Enrichment} \\ \mbox{wt \%} \ ^{235}\mbox{U (E)} \\ \hline 1.7 \le \mbox{E} < 1.9 \end{array}$	35 Min 14×14	S< Burnup ≤ nimum Cool 15×15 -	40 GWD/M ing Time [yo 16×16	TU ears] 17×17	40 Min 14×14 -	< Burnup ≤ imum Cooli 15×15 -	45 GWD/M' ng Time [ye 16×16	ΓU ars] 17×17 -	
Minimum Initial Enrichment wt % 235 U (E) $1.7 \le E < 1.9$ $1.9 \le E < 2.1$	35 Min 14×14 - 9	S< Burnup ≤ nimum Cool 15×15 - 12	40 GWD/M ing Time [y 16×16 - 10	TU ears] 17×17 - 12	40 Min 14×14 -	< Burnup ≤4 imum Cooli 15×15 - -	45 GWD/M' ng Time [ye 16×16 -	ΓU ars] 17×17 - -	
Minimum Initial Enrichment wt % 235 U (E) $1.7 \le E < 1.9$ $1.9 \le E < 2.1$ $2.1 \le E < 2.3$	35 Min 14×14 - 9 9	S< Burnup ≤ nimum Cool 15×15 - 12 12	40 GWD/M ing Time [yo 16×16 - 10 10	TU ears] 17×17 - 12 11	40 Min 14×14 - -	< Burnup ≤ imum Cooli 15×15 - - -	45 GWD/M' ing Time [ye 16×16 - -	ΓU ars] 17×17 - - -	
Minimum Initial Enrichment wt % 235 U (E) $1.7 \le E < 1.9$ $1.9 \le E < 2.1$ $2.1 \le E < 2.3$ $2.3 \le E < 2.5$	35 Min 14×14 - 9 9 9 9	S< Burnup ≤ nimum Cool 15×15 - 12 12 12 12	40 GWD/M ing Time [yd 16×16 - 10 10 9	TU ears] 17×17 - 12 11 11	40 Min 14×14 - - - 12	< Burnup ≤ imum Cooli 15×15 - - - 17	45 GWD/M' ng Time [ye 16×16 - - - 13	ΓU ears] 17×17 - - - 16	
Minimum Initial Enrichment wt % 235 U (E) $1.7 \le E < 1.9$ $1.9 \le E < 2.1$ $2.1 \le E < 2.3$ $2.3 \le E < 2.5$ $2.5 \le E < 2.7$	35 Min 14×14 - 9 9 9 9 8	S< Burnup ≤ nimum Cool 15×15 - 12 12 12 12 12 11	40 GWD/M ing Time [ye 16×16 - 10 10 9 9	TU ears] 17×17 - 12 11 11 11	40- Min 14×14 - - - 12 12 12	< Burnup Se imum Cooli 15×15 - - - 17 16	45 GWD/M' ng Time [ye 16×16 - - 13 13	ΓU ears] - - - - 16 16	
Minimum Initial Enrichment wt % 235 U (E) $1.7 \le E < 1.9$ $1.9 \le E < 2.1$ $2.1 \le E < 2.3$ $2.3 \le E < 2.5$ $2.5 \le E < 2.7$ $2.7 \le E < 2.9$	35 Min 14×14 - 9 9 9 9 9 9 8 8 8	S< Burnup ≤ nimum Cool 15×15 - 12 12 12 12 11 11	40 GWD/M ing Time [yo 16×16 - 10 10 9 9 9 9	TU ears] 17×17 - 12 11 11 11 11	40- Min 14×14 - - - 12 12 12 11	< Burnup Se imum Cooli 15×15 - - - 17 16 16	45 GWD/M' ng Time [ye 16×16 - - 13 13 13	ΓU ars] - - - 16 16 16 16	
Minimum Initial Enrichment wt % 235 U (E) $1.7 \le E < 1.9$ $1.9 \le E < 2.1$ $2.1 \le E < 2.3$ $2.3 \le E < 2.5$ $2.5 \le E < 2.7$ $2.7 \le E < 2.9$ $2.9 \le E < 3.1$	35 Min 14×14 - 9 9 9 9 8 8 8 8 8	S< Burnup ≤ nimum Cool 15×15 - 12 12 12 12 11 11 11	40 GWD/M ing Time [yd 16×16 - 10 10 9 9 9 9 9	TU ears] 17×17 - 12 11 11 11 11 11	40 Min 14×14 - - 12 12 11 11	< Burnup <	45 GWD/M' ng Time [ye 16×16 - - 13 13 13 13 12	ΓU ears] - - - 16 16 16 16 15	
Minimum Initial Enrichment wt % 235 U (E) $1.7 \le E < 1.9$ $1.9 \le E < 2.1$ $2.1 \le E < 2.3$ $2.3 \le E < 2.5$ $2.5 \le E < 2.7$ $2.7 \le E < 2.9$ $2.9 \le E < 3.1$ $3.1 \le E < 3.3$	35 Min 14×14 - 9 9 9 9 9 9 9 8 8 8 8 8 8 8	S< Burnup ≤ nimum Cool 15×15 - 12 12 12 12 11 11 11 11	40 GWD/M ing Time [ye 16×16 - 10 10 9 9 9 9 9 9 9 9	TU ears] 17×17 - 12 11 11 11 11 11 11 11 11	40- Min 14×14 - - - 12 12 12 11 11 11	< Burnup Se imum Cooli 15×15 - - 17 16 16 16 16 16	45 GWD/M' ng Time [ye 16×16 - - 13 13 13 13 12 12	ΓU ars] 17×17 - - - 16 16 16 16 15 15	
Minimum Initial Enrichment wt % 235 U (E) $1.7 \le E < 1.9$ $1.9 \le E < 2.1$ $2.1 \le E < 2.3$ $2.3 \le E < 2.5$ $2.5 \le E < 2.7$ $2.7 \le E < 2.9$ $2.9 \le E < 3.1$ $3.1 \le E < 3.3$ $3.3 \le E < 3.5$	35 Min 14×14 - 9 9 9 9 9 9 9 8 8 8 8 8 8 8 8 8 8 8	S< Burnup ≤ nimum Cool 15×15 - 12 12 12 12 11 11 11 11 11	40 GWD/M ing Time [yd 16×16 - 10 10 9 9 9 9 9 9 9 9 9 9 9 9	TU ears] 17×17 - 12 11 11 11 11 11 11 10 10	40- Min 14×14 - - 12 12 11 11 11 11 11	< Burnup Section 4	45 GWD/M' ng Time [ye 16×16 - - 13 13 13 13 12 12 12 12	ΓU ars] 17×17 - - 16 16 16 16 15 15 15	
Minimum Initial Enrichment wt % 235 U (E) $1.7 \le E < 1.9$ $1.9 \le E < 2.1$ $2.1 \le E < 2.3$ $2.3 \le E < 2.5$ $2.5 \le E < 2.7$ $2.7 \le E < 2.9$ $2.9 \le E < 3.1$ $3.1 \le E < 3.3$ $3.3 \le E < 3.5$ $3.5 \le E < 3.7$	35 <u>Min</u> 14×14 - 9 9 9 9 9 8 8 8 8 8 8 8 8 8 8 8 8 8 8	S Burnup ≤ nimum Cool 15×15 - - 12 12 12 12 11 11 11 11 11 11 11 11 11 11	40 GWD/M ing Time [yd 16×16 - 10 10 9 9 9 9 9 9 9 9 9 9 9 9 9	TU ears] 17×17 - 12 11 11 11 11 11 11 10 10 10	40- Min 14×14 - - 12 12 11 11 11 11 11 11	< Burnup Se imum Cooli 15×15 - - 17 16 16 16 16 16 15 15	45 GWD/M' ng Time [ye 16×16 - - - 13 13 13 13 12 12 12 12 12	ΓU ears] 17×17 - - 16 16 16 16 15 15 15 15 15	
Minimum Initial Enrichment wt % 235 U (E) $1.7 \le E < 1.9$ $1.9 \le E < 2.1$ $2.1 \le E < 2.3$ $2.3 \le E < 2.5$ $2.5 \le E < 2.7$ $2.7 \le E < 2.9$ $2.9 \le E < 3.1$ $3.1 \le E < 3.3$ $3.3 \le E < 3.5$ $3.5 \le E < 3.7$ $3.7 \le E < 3.9$	35 Min 14×14 - 9 9 9 9 9 9 9 9 9 9 9 9 9 8 8 8 8 8 8	S< Burnup ≤ nimum Cool 15×15 - 12 12 12 12 12 11 11 11 11 11 11 11 10 10	40 GWD/M ing Time [ye 16×16 - 10 10 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 8	TU ears] 17×17 - 12 11 11 11 11 11 11 10 10 10 10 10	40- Min 14×14 - - 12 12 12 11 11 11 11 11 11 11 10	< Burnup Se imum Cooli 15×15 - - 17 16 16 16 16 16 15 15 15 15	45 GWD/M' ng Time [ye 16×16 - - 13 13 13 13 12 12 12 12 12 12 12	ΓU ars] 17×17 - - - 16 16 16 16 15 15 15 15 15 15 14	
Minimum Initial Enrichment wt % ^{235}U (E) $1.7 \le E < 1.9$ $1.9 \le E < 2.1$ $2.1 \le E < 2.3$ $2.3 \le E < 2.5$ $2.5 \le E < 2.7$ $2.7 \le E < 2.9$ $2.9 \le E < 3.1$ $3.1 \le E < 3.3$ $3.3 \le E < 3.5$ $3.5 \le E < 3.7$ $3.7 \le E < 3.9$ $3.9 \le E < 4.1$	35 Min 14×14 - - 9 9 9 9 9 9 9 9 9 8 8 8 8 8 8 8 8 8	S< Burnup ≤ nimum Cool 15×15 - 12 12 12 12 11 11 11 11 11 11 11 10 10 10	40 GWD/M ing Time [ye 16×16 - 10 10 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	TU ears] 17×17 - 12 11 11 11 11 11 11 10 10 10 10 10 10	40- Min 14×14 - - 12 12 11 11 11 11 11 11 11 10 10	< Burnup Section 4 Section	45 GWD/M' ng Time [ye 16×16 - - 13 13 13 13 12 12 12 12 12 12 12 12 12	ΓU aars] 17×17 - - 16 16 16 16 15 15 15 15 15 14 14	
Minimum Initial Enrichment wt % ^{235}U (E) $1.7 \le E < 1.9$ $1.9 \le E < 2.1$ $2.1 \le E < 2.3$ $2.3 \le E < 2.5$ $2.5 \le E < 2.7$ $2.7 \le E < 2.9$ $2.9 \le E < 3.1$ $3.1 \le E < 3.3$ $3.3 \le E < 3.5$ $3.5 \le E < 3.7$ $3.7 \le E < 3.9$ $3.9 \le E < 4.1$ $4.1 \le E < 4.3$	35 Min 14×14 - - 9 9 9 9 9 9 8 8 8 8 8 8 8 8 8 8 8 8	S< Burnup ≤ nimum Cool 15×15 - 12 12 12 12 12 11 11 11 11 11 11 11 10 10 10 10	40 GWD/M ing Time [y- 16×16 - 10 10 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	TU ears] 17×17 - 12 11 11 11 11 11 10 10 10 10 10 10 10 10	40- Min 14×14 - - 12 12 12 11 11 11 11 11 11 10 10 10	< Burnup ≤ imum Cooli 15×15 - - 17 16 16 16 16 16 15 15 15 15 15 15	45 GWD/M' ng Time [ye 16×16 - - - 13 13 13 13 12 12 12 12 12 12 12 12 12 12 12 12	ΓU ears] 17×17 - - - 16 16 16 16 15 15 15 15 15 15 14 14 14	
Minimum Initial Enrichment wt % 235 U (E) $1.7 \le E < 1.9$ $1.9 \le E < 2.1$ $2.1 \le E < 2.3$ $2.3 \le E < 2.5$ $2.5 \le E < 2.7$ $2.7 \le E < 2.9$ $2.9 \le E < 3.1$ $3.1 \le E < 3.3$ $3.3 \le E < 3.5$ $3.5 \le E < 3.7$ $3.7 \le E < 3.9$ $3.9 \le E < 4.1$ $4.1 \le E < 4.3$ $4.3 \le E < 4.5$	35 Min 14×14 - 9 9 9 9 9 9 9 9 9 9 9 8 8 8 8 8 8 8 8	S Burnup ≤ nimum Cool 15×15 - 12 12 12 12 11 11 11 11 10 10 10 10 10 10 10 10	40 GWD/M ing Time [yd 16×16 - 10 10 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 8 8 8 8 8 8	TU ears] 17×17 - 12 11 11 11 11 11 10 10 10 10 10 10 10 10	40- Min 14×14 - - 12 12 12 11 11 11 11 11 11 10 10 10 10 10	< Burnup Seimum Cooli 15×15 - - 17 16 16 16 16 15 15 15 15 15 15 15 15 15 15	45 GWD/M' ng Time [ye 16×16 - - - 13 13 13 13 13 12 12 12 12 12 12 12 12 12 12 12 12 12	ΓU ars] 17×17 - - - 16 16 16 16 16 15 15 15 15 15 15 15 14 14 14 14	
Minimum Initial Enrichment wt % ^{235}U (E) $1.7 \le E < 1.9$ $1.9 \le E < 2.1$ $2.1 \le E < 2.3$ $2.3 \le E < 2.5$ $2.5 \le E < 2.7$ $2.7 \le E < 2.9$ $2.9 \le E < 3.1$ $3.1 \le E < 3.3$ $3.3 \le E < 3.5$ $3.5 \le E < 3.7$ $3.7 \le E < 3.9$ $3.9 \le E < 4.1$ $4.1 \le E < 4.3$ $4.3 \le E < 4.5$ $4.5 \le E < 4.7$	35 Min 14×14 - - 9 9 9 9 9 9 9 9 8 8 8 8 8 8 8 8 8 8	S< Burnup ≤ nimum Cool 15×15 - 12 12 12 12 12 11 11 11 11 11 11 10 10 10 10 10 10 10	40 GWD/M ing Time [ye 16×16 - 10 10 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	TU ears] 17×17 - 12 11 11 11 11 11 11 10 10 10 10 10 10 10	40- Min 14×14 - - 12 12 12 11 11 11 11 11 11 11 10 10 10 10 10 10	< Burnup Section 15×15 - - - - - 17 16 16 16 16 15 15 15 15 15 15 14 14 14	45 GWD/M' ng Time [ye 16×16 - - - 13 13 13 13 13 12 12 12 12 12 12 12 12 12 12 12 12 12	ΓU ars] 17×17 - - - - - - - - - - - - - - - - - - -	
Minimum Initial Enrichment wt % ^{235}U (E) $1.7 \le E < 1.9$ $1.9 \le E < 2.1$ $2.1 \le E < 2.3$ $2.3 \le E < 2.5$ $2.5 \le E < 2.7$ $2.7 \le E < 2.9$ $2.9 \le E < 3.1$ $3.1 \le E < 3.3$ $3.3 \le E < 3.5$ $3.5 \le E < 3.7$ $3.7 \le E < 3.9$ $3.9 \le E < 4.1$ $4.1 \le E < 4.3$ $4.3 \le E < 4.5$ $4.5 \le E < 4.7$ $4.7 \le E < 4.9$	35 Min 14×14 - - 9 9 9 9 9 8 8 8 8 8 8 8 8 8 8 8 8 8	S< Burnup ≤ nimum Cool 15×15 - - 12 12 12 12 11 11 11 11 11 11 10 10 10 10 10 10 10 10 10 10 10 10	40 GWD/M ing Time [ye 16×16 - - 10 10 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	TU ears] 17×17 - 12 11 11 11 11 11 10 10 10 10 10 10 10 10	40- Min 14×14 - - 12 12 12 11 11 11 11 11 11 11 10 10 10 10 10 10	< Burnup	45 GWD/M' ng Time [ye 16×16 - - - 13 13 13 13 12 12 12 12 12 12 12 12 12 12 12 12 12	ΓU ars] 17×17 - - - - - - - - - - - - - - - - - - -	

Note: 700 Watt assemblies may be loaded in all loading positions (Figure 12B2-3).

Table 12B2-11

Minimum Cooling Time versus Burnup/Initial Enrichment for PWR Fuel Assembly Heat Loads \leq 700 W in the Advanced CANISTER (Continued)

Minimum Initial Enrichment	45 Mi	45< Burnup ≤50 GWD/MTU Minimum Cooling Time [years]				50< Burnup ≤55 GWD/MTU Minimum Cooling Time [years]			
wt % ²³⁵ U (E)	14×14	15×15	16×16	17×17	14×14	15×15	16×16	17×17	
$1.7 \le E < 1.9$	-	-	-	-	-	-	-	-	
$1.9 \le E < 2.1$	-	-	-	-	-		-	-	
$2.1 \le E < 2.3$	-	-	-	-	-	-	-	-	
$2.3 \le E < 2.5$	-	•	-	-	-	-	-	-	
$2.5 \le E < 2.7$	-	-	-	-	-		-	-	
$2.7 \le E < 2.9$	16	22	18	22		-	-		
$2.9 \le E < 3.1$	16	22	17	21	-	-		-	
$3.1 \le E < 3.3$	15	22	17	21	21	27	23	27	
$3.3 \le E < 3.5$	15	21	17	21	20	27	22	26	
$3.5 \le E < 3.7$	15	21	16	20	20	27	22	26	
$3.7 \le E \le 3.9$	15	21	16	20	20	27	22	26	
3.9 < E < 4.1	14	21	16	20	20	26	21	26	
4.1 < E < 4.3	14	20	16	20	19	26	21	26	
$4.3 \le E \le 4.5$	14	20	16	20	19	26	21	25	
$4.5 \le E < 4.7$	14	20	16	19	19	26	21	25	
$4.7 \le E < 4.9$	14	20	15	19	19	26	21	25	
E > 4.9	14	20	15	19	18	26	20	25	

Note: 700 Watt assemblies may be loaded in all loading positions (Figure 12B2-3).

Table 12B2-12	Minimum Cooling Time versus Burnup/Initial Enrichment for PWR Fuel
	Assembly Heat Loads $\leq 1,000$ W in the Advanced CANISTER

Minimum Initial Enrichment	Mi	Burnup ≤30 GWD/MTU Minimum Cooling Time [years]				30< Burnup ≤35 GWD/MTU Minimum Cooling Time [years]			
wt % ²³⁵ U (E)	14×14	15×15	16×16	17×17	14×14	15×15	16×16	17×17	
$1.7 \le E < 1.9$	5	5	5	5	5	6	5	6	
$1.9 \le E < 2.1$	5	5	5	5	5	5	5	5	
$2.1 \le E < 2.3$	5	5	5	5	5	5	5	5	
$2.3 \le E < 2.5$	5	5	5	5	5	5	5	5	
$2.5 \le E < 2.7$	5	5	5	5	5	5	5	5	
$2.7 \le E < 2.9$	5	5	5	5	5	5	5	5	
$2.9 \le E < 3.1$	5	5	5	5	5	5	5	5	
$3.1 \le E < 3.3$	5	5	5	5	5	5	5	5	
$3.3 \le E < 3.5$	5	5	5	5	5	5	5	5	
$3.5 \le E < 3.7$	5	5	5	5	5	5	5	5	
$3.7 \le E < 3.9$	5	5	5	5	5	5	5	5	
$3.9 \le E < 4.1$	5	5	5	5	5	5	5	5	
$4.1 \le E < 4.3$	5	5	5	5	5	5	5	5	
$4.3 \le E < 4.5$	5	5	5	5	5	5	5	5	
$4.5 \le E < 4.7$	5	5	5	5	5	5	5	5	
$4.7 \le E < 4.9$	5	5	5	5	5	5	5	5	
E ≥ 4.9	5	5	5	5	5	5	5	5	
Minimum Initial Enrichment	35< Burnup ≤40 GWD/MTU40< Burnup ≤45 GWD/MTUMinimum Cooling Time (years)Minimum Cooling Time (years)					ru ars]			
1 11 0/ 235TI (E)	14-14	15.15	16.16	17.17	14.14	15.15	16.16	17.17	

Enrichment	- Si Mir	nimum Coo	ling Time [y	ears]	Minimum Cooling Time [years]			
wt % ²³⁵ U (E)	14×14	15×15	16×16	17×17	14×14	15×15	16×16	17×17
$1.7 \le E < 1.9$	-	-	-	-	-	-	-	-
$1.9 \le E < 2.1$	6	7	6	7	-	-	-	-
$2.1 \le E < 2.3$	6	6	6	6	-	-	-	-
$2.3 \le E < 2.5$	5	6	6	6	6	8	7	8
$2.5 \le E < 2.7$	5	6	6	6	6	8	7	8
$2.7 \le E < 2.9$	5	6	6	6	6	8	7	7
$2.9 \le E < 3.1$	5	6	6	6	6	7	7	7
$3.1 \le E < 3.3$	5	6	6	6	6	7	7	7
$3.3 \le E < 3.5$	5	6	5	6	6	7	6	7
$3.5 \le E < 3.7$	5	6	5	6	6	7	6	7
$3.7 \le E < 3.9$	5	6	5	6	6	7	6	7
$3.9 \le E < 4.1$	5	6	5	6	6	7	6	7
$4.1 \le E < 4.3$	5	6	5	6	6	7	6	7
$4.3 \le E < 4.5$	5	6	5	6	6	7	6	7
$4.5 \le E < 4.7$	5	6	5	6	6	7	6	7
$4.7 \le E < 4.9$	5	. 6	5	6	6	7	6	7
E ≥ 4.9	5	6	5	6	6	7	6	7

Note: Assemblies with Heat Loads 700 W < $HL \le 1,000$ W are restricted to Zone B loading positions (Figure 12B2-3).

Table 12B2-12Minimum Cooling Time versus Burnup/Initial Enrichment for PWR Fuel
Assembly Heat Loads $\leq 1,000$ W in the Advanced CANISTER
(Continued)

Minimum Initial Enrichment	45< Burnup ≤50 GWD/MTU Minimum Cooling Time [years]				50< Burnup ≤55 GWD/MTU Minimum Cooling Time [years]			
wt % ²³⁵ U (E)	14×14	15×15	16×16	17×17	14×14	15×15	16×16	17×17
$1.7 \le E \le 1.9$	-	-	-	-	-	-	-	-
$1.9 \le E < 2.1$	-	-	-	-	-	-	-	-
$2.1 \le E \le 2.3$	-	-	-	-	-	-	-	-
$2.3 \le E < 2.5$	-	-	-	-	-	-	-	-
$2.5 \le E < 2.7$	-	-	-	-	-	-	-	-
$2.7 \le E \le 2.9$	8	10	8	10	-	-	-	-
$2.9 \le E < 3.1$	7	10	8	9	-	•	-	-
$3.1 \le E < 3.3$	7	9	8	9	9	13	10	12
$3.3 \le E < 3.5$	7	9	8	9	9	12	10	12
$3.5 \le E < 3.7$	7	9	8	9	9	12	10	12
$3.7 \le E < 3.9$	7	9	8	9	9	12	9	11
$3.9 \le E < 4.1$	7	9	7	9	8	12	9	11
$4.1 \le E < 4.3$	7	9	7	8	8	11	9	11
$4.3 \le E < 4.5$	7	9	7	8	8	11	9	11
$4.5 \le E < 4.7$	7	8	7	8	8	11	9	11
$4.7 \le E < 4.9$	7	8	7	8	8	11	9	11
E ≥ 4.9	7	8	7	8	8	11	9	10

Note: Assemblies with Heat Loads 700 W < $HL \le 1,000$ W are restricted to Zone B loading positions (Figure 12B2-3).

Table 12B2-13Minimum Cooling Time versus Burnup/Initial Enrichment for PWR Fuel
Assembly Heat Loads $\leq 1,100$ W in the Advanced CANISTER

Minimum Initial Enrichment	Burnup ≤30 GWD/MTU Minimum Cooling Time [years]			30< Burnup ≤35 GWD/MTU Minimum Cooling Time [years]				
wt % ²³⁵ U (E)	14×14	15×15	16×16	17×17	14×14	15×15	16×16	17×17
$1.7 \le E < 1.9$	5	5	5	5	5	5	5	5
$1.9 \le E < 2.1$	5	5	5	5	5	5	5	5
$2.1 \le E < 2.3$	5	5	5	5	5	5	5	5
$2.3 \le E < 2.5$	5	5	5	5	5	5	5	5
$2.5 \le E < 2.7$	5	5	5	5	5	5	5	5
$2.7 \le E \le 2.9$	5	5	5	5	5	5	5	5
$2.9 \le E < 3.1$	5	5	5	5	5	5	5	5
$3.1 \le E < 3.3$	5	5	5	5	5	5	5	5
$3.3 \le E < 3.5$	5	5	5	5	5	5	5	5
$3.5 \le E < 3.7$	5	5	5	5	5	5	5	5
$3.7 \le E < 3.9$	5	5	5	5	5	5	5	5
$3.9 \le E < 4.1$	5	5	5	5 -	5	5	5	5
$4.1 \le E < 4.3$	5	5	5	5	5	5	5	5
$4.3 \le E < 4.5$	5	5	5	5	5	5	5	5
$4.5 \le E < 4.7$	5	5	5	5	5	5	5	5
$4.7 \le E < 4.9$	5	5	5	5	5	5	5	5
E ≥ 4.9	5	5	5	5	5	5	5	5
Minimum Initial Enrichment	35< Burnup ≤40 GWD/MTU Minimum Cooling Time (years)				40< Burnup ≤45 GWD/MTU Minimum Cooling Time (vegrs)			
wt $\%^{235}$ U(E)	14×14 15×15 16×16 17×17			14×14	15×15	16×16	17×17	
17 < F < 19	-			-		-	-	-
	5	6	5	6				

$1.7 \le E \le 1.9$	-	-	-	-	-	-	-	-
$1.9 \le E < 2.1$	5	6	5	6	-	-	-	-
$2.1 \le E < 2.3$	5	6	5	6	-	-	-	-
$2.3 \le E < 2.5$	5	6	5	6	6	7	6	7
$2.5 \le E < 2.7$	5	6	5	6	6	7	6	7
$2.7 \le E < 2.9$	5	6	5	6	6	7	6	7
$2.9 \le E < 3.1$	5	6	5	6	6	7	6	7
$3.1 \le E < 3.3$	5	5	5	5	5	6	6	6
$3.3 \le E < 3.5$	5	5	5	5	5	6	6	6
$3.5 \le E < 3.7$	5	5	5	5	5	6	6	6
$3.7 \le E < 3.9$	5	5	5	5	5	6	6	6
$3.9 \le E < 4.1$	5	5	5	5	5	6	6	6
$4.1 \le E < 4.3$	5	5	5	5	5	6	6	6
$4.3 \le E < 4.5$	5	5	5	5	5	6	5	6
$4.5 \le E < 4.7$	5	5	5	5	5	6	5	6
$4.7 \le E < 4.9$	5	5	5	5	5	6	5	6
E ≥ 4.9	5	5	5	5	5	6	5	6

Note: Assemblies with Heat Loads 1,000 W < HL \leq 1,100 W are restricted to Zone C loading positions (Figure 12B2-3).

Table 12B2-13Minimum Cooling Time versus Burnup/Initial Enrichment for PWR Fuel
Assembly Heat Loads $\leq 1,100$ W in the Advanced CANISTER
(Continued)

Minimum Initial Enrichment	45< Burnup ≤50 GWD/MTU Minimum Cooling Time [years]				50< Burnup ≤55 GWD/MTU Minimum Cooling Time [years]			
wt % ²³⁵ U (E)	14×14	15×15	16×16	17×17	14×14	15×15	16×16	17×17
1.7 ≤ E < 1.9	-	-	-	-	-	-	-	-
$1.9 \le E < 2.1$	-	-	-	-	-	-	-	-
$2.1 \le E < 2.3$	-	-	-	-	-	-		
$2.3 \le E < 2.5$	-	-	-	-	-	-	-	
$2.5 \le E < 2.7$	-	-		-	-	-	-	-
$2.7 \le E < 2.9$	7	8	7	8	-	-	-	
$2.9 \le E < 3.1$	7	8	7	8	-	-	-	-
$3.1 \le E < 3.3$	6	8	7	8	8	10	8	10
$3.3 \le E < 3.5$	6	8	7	8	8	10	8	10
$3.5 \le E < 3.7$	6	8	7	8	7	10	8	9
$3.7 \le E < 3.9$	6	8	7	7	7	9	8	9
$3.9 \le E < 4.1$	6	7	7	7	7	9	8	9
$4.1 \le E < 4.3$	6	7	6	7	7	9	8	9
$4.3 \le E < 4.5$	6	7	6	7	7	9	8	9
$4.5 \le E < 4.7$	6	7	6	7	7	9	8	9
$4.7 \le E < 4.9$	6	7	6	7	7	9	. 7	9
E ≥ 4.9	6	7	6	7	7	9	7	9

Note: Assemblies with Heat Loads 1,000 W < HL \leq 1,100 W are restricted to Zone C loading positions (Figure 12B2-3).

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Design Features B 3.0

B 3.0 DESIGN FEATURES

B 3.1 Site

B 3.1.1 Site Location

The NAC-UMS[®] SYSTEM is authorized for general use by 10 CFR 50 license holders at various site locations under the provisions of 10 CFR 72, Subpart K.

B 3.2 Design Features Important for Criticality Control

B 3.2.1 Standard CANISTER-INTACT FUEL ASSEMBLIES

- a) Minimum ¹⁰B loading in the BORAL neutron absorbers:
 - 1. $PWR 0.025 g/cm^2$
 - 2. BWR 0.011 g/cm²
- b) Minimum length of INTACT FUEL ASSEMBLY internal structure and bottom end fitting and/or spacers shall ensure the minimum distance to the fuel region from the base of the CANISTER is:
 - 1. PWR 3.2 inches
 - 2. BWR 6.2 inches

B 3.2.2 Advanced CANISTER-INTACT FUEL ASSEMBLIES

a) Minimum ¹⁰B loading in the METAMIC neutron absorbers:
 1. PWR - 0.019g/cm²

b) Minimum length of INTACT FUEL ASSEMBLY internal structure and bottom end fitting and/or spacers shall ensure the minimum distance to the fuel region from the base of the CANISTER is:
 1. PWR - 1.5 inches

- c) Soluble boron concentration in the PWR spent fuel pool water:
 - 1. Fuel with enrichment up to, or equal to, 4.6 wt % 235 U, \geq 2,000 ppm
 - 2. Fuel with enrichment above 4.6 wt % 235 U, \geq 2,300 ppm
- d) Minimum borated water temperature shall be at least 5°F higher than that needed to ensure boron solubility.

Design Features B 3.0

B 3.3 Codes and Standards

The American Society of Mechanical Engineers Boiler and Pressure Vessel Code (ASME Code), 1995 Edition with Addenda through 1995, is the governing Code for the NAC-UMS[®] CANISTER.

The American Concrete Institute Specifications ACI-349 (1985) and ACI-318 (1995) govern the NAC-UMS[®] CONCRETE CASK design and construction, respectively.

The American National Standards Institute ANSI N14.6 (1993) and NUREG-0612 govern the NAC-UMS[®] TRANSFER CASK design, operation, fabrication, testing, inspection and maintenance.

B 3.3.1 <u>Alternatives to Codes, Standards, and Criteria</u> Table 12B3-1 lists alternatives to the ASME Code for the design of the NAC-UMS[®] SYSTEM.

B 3.3.2 Construction/Fabrication Alternatives to Codes, Standards, and Criteria

Proposed alternatives to ASME Code, Section III, 1995 Edition with Addenda, through 1995, including alternatives listed in Specification B3.3.1, may be used when authorized by the Director of the Office of Nuclear Material Safety and Safeguards or designee. The request for such alternatives should demonstrate that:

- 1. The proposed alternatives would provide an acceptable level of quality and safety, or
- 2. Compliance with the specified requirements of ASME Code, Section III, 1995 Edition with Addenda through 1995, would result in hardship or unusual difficulty without a compensating increase in the level of quality and safety.

Requests for alternatives shall be submitted in accordance with 10 CFR 72.4.
Table 12B3-1 List of ASME Code Alternatives for the NAC-UMS[®] SYSTEM

Component	Reference ASME Code Section/Article	Code Requirement	Alternative, Justification and Compensatory Measures
CANISTER	NB-1100	Statement of requirements for Code stamping of components.	CANISTER is designed and will be fabricated in accordance with ASME Code, Section III, Subsection NB to the maximum practical extent, but Code stamping is not required. The completion of an ASME Design Specification, Design Report and Overpressure Protection Report are not required.
CANISTER	NB-2000	Requirements to be supplied by ASME- approved material supplier.	Materials will be supplied by NAC- approved suppliers with Certified Material Test Reports (CMTRs) in accordance to NB-2000 requirements.
CANISTER Shield Lid and Structural Lid Welds	NB-4243	Full penetration welds required for Category C joints (flat head to main shell per NB-3352.3).	Shield lid and structural lid to CANISTER shell welds are not full penetration welds. These field welds are performed independently to provide a redundant closure. Leaktightness of the CANISTER is verified by testing.
CANISTER Structural Lid Weld	NB-4421	Requires removal of backing ring.	Structural lid to CANISTER shell weld uses a spacer ring that is not removed. The spacer ring permits completion of the groove weld; it is not considered in any analyses; and it has no detrimental effect on the CANISTER's function.
CANISTER Vent Port Cover and Drain Port Cover to Shield Lid Welds; Shield Lid to Canister Shell Weld	NB-5230	Radiographic (RT) or ultrasonic (UT) examination required.	Root and final surface liquid penetrant examination to be performed per ASME Code Section V, Article 6, with acceptance in accordance with ASME Code, Section III, NB-5350.

Table 12B3-1 List of ASME Code Alternatives for the NAC-UMS® SYSTEM (continued)

Component	Reference ASME Code Section/Article	Code Requirement	Alternatives, Justification and Compensatory Measures
CANISTER Structural Lid to Shell Weld	NB-5230	Radiographic (RT) or ultrasonic (UT) examination required.	The CANISTER structural lid to CANISTER shell closure weld is performed in the field following fuel assembly loading. The structural lid-to- shell weld will be verified by either ultrasonic (UT) or progressive liquid penetrant (PT) examination. If progressive PT examination is used, at a minimum, it must include the root and final layers and each approximately 3/8 inch of weld depth. If UT examination is used, it will be followed by a final surface PT examination. For either UT or PT examination, the maximum, undetectable flaw size is demonstrated to be smaller than the critical flaw size. The critical flaw size is determined in accordance with ASME Code, Section XI methods. The examination of the weld will be performed by qualified personnel per ASME Code Section V, Articles 5 (UT) and 6 (PT) with acceptance per ASME Code Section III, NB-5332 (UT) per 1997 Addenda, and NB-5350 for (PT)

Table 12B3-1 List of ASME Code Alternatives for the NAC-UMS® SYSTEM (continued)

Component	Reference ASME Code Section/Article	Code Requirement	Alternative, Justification and Compensatory Measures
CANISTER Vessel and Shield Lid	NB-6111	All completed pressure retaining systems shall be pressure tested.	The CANISTER shield lid to shell weld is performed in the field following fuel assembly loading. The CANISTER is then pneumatically (air-over-water) pressure tested as defined in Chapter 9 and described in Chapter 8. Accessibility for leakage inspections precludes a Code compliant hydrostatic test. The shield lid- to-shell weld is also leak tested to the leak- tight criteria of ANSI N14.5. The vent port and drain port cover welds are examined by root and final PT examination. The structural lid enclosure weld is examined by progressive PT or UT and final surface PT.
CANISTER Vessel	NB-7000	Vessels are required to have overpressure protection.	No overpressure protection is provided. The function of the CANISTER is to confine radioactive contents under normal, off-normal, and accident conditions of storage. The CANISTER vessel is designed to withstand a maximum internal pressure considering 100% fuel rod failure and maximum accident temperatures.

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Table 12B3-1 List of ASME Code Alternatives for the NAC-UMS® SYSTEM (continued)

Component	Reference ASME Code Section/Article	Code Requirement	Alternative, Justification and Compensatory Measures
CANISTER Vessel	NB-8000	States requirements for nameplates, stamping and reports per NCA-8000.	The NAC-UMS [®] SYSTEM is marked and identified in accordance with 10 CFR 72 requirements. Code stamping is not required. The QA data package will be in accordance with NAC's approved QA program. The completion of an ASME Design Specification, Design Report and Overpressure Protection Report are not required.
CANISTER Basket Assembly	NG-2000	Requires materials to be supplied by ASME approved material supplier.	Materials to be supplied by NAC- approved suppliers with CMTRs in accordance with NG-2000 requirements.
CANISTER Basket Assembly	NG-8000	States requirements for nameplates, stamping and reports per NCA-8000.	The NAC-UMS [®] SYSTEM will be marked and identified in accordance with 10 CFR 72 requirements. No Code stamping is required. The CANISTER basket data package will be in accordance with NAC's approved QA program.
CANISTER Vessel and Basket Assembly Material	NB-2130/ NG-2130	States requirements for certification of material organizations and materials to NCA-3861 and NCA-3862, respectively.	The NAC-UMS [®] CANISTER and Basket Assembly component materials are procured in accordance with the specifications for materials in ASME Code Section II with Certified Material Test Reports. The component materials will be obtained from NAC approved Suppliers in accordance with NAC's approved QA program.

B 3.4 Site Specific Parameters and Analyses

This section presents site-specific parameters and analytical bases that must be verified by the NAC-UMS[®] SYSTEM user. The parameters and bases presented in Section B.3.4.1 are those applied in the design basis analysis. The parameters and bases used in the evaluation of SITE SPECIFIC FUEL are presented in the appropriate sections below.

B 3.4.1 Design Basis Site Specific Parameters and Analyses

The design basis site-specific parameters and analyses that require verification by the NAC-UMS[®] SYSTEM user are:

- 1. The temperature of 76°F is the maximum average yearly temperature. The 3-day average ambient temperature shall be 106°F or less.
- 2. The allowed temperature extremes, averaged over a 3-day period, shall be greater than -40°F and less than 133°F.
- 3. The design basis earthquake horizontal and vertical seismic acceleration levels at the top surface of the ISFSI pad are bounded by the values shown:

	Coefficient	Horizontal g-level in each of Two	Corresponding Vertical
Configuration	of Friction	Orthogonal Directions	g-level (upward)
Standard	0.35	0.26	$0.26 \times 0.667 = 0.173$ g
Standard	0.40	0.30	$0.30 \times 0.667 = 0.200$ g
Advanced	0.40	0.30	$0.30 \times 0.667 = 0.200$ g

- 4. The analyzed flood condition of 15 fps water velocity and a height of 50 feet of water (full submergence of the loaded cask) are not exceeded.
- 5. The potential for fire and explosion shall be addressed, based on site-specific considerations. This includes the condition that the fuel tank of the cask handling equipment used to move the loaded CONCRETE CASK onto or from the ISFSI site contains no more than 50 gallons of fuel.

B 3.4.1 Design Basis Site Specific Parameters and Analyses (continued)

- 6. In addition to the requirements of 10 CFR 72.212(b)(2)(ii), the ISFSI pad(s) and foundation shall meet the design basis earthquake horizontal and vertical seismic acceleration levels at the top surface of the ISFSI pad as specified in B3.4.1 (3).
- 7. In cases where engineered features (i.e., berms, shield walls) are used to ensure that requirements of 10 CFR 72.104(a) are met, such features are to be considered important to safety and must be evaluated to determine the applicable Quality Assurance Category on a site specific basis.
- 8. TRANSFER CASK OPERATIONS shall only be conducted with surrounding air temperatures $\ge 0^{\circ}$ F.
- 9. The VERTICAL CONCRETE CASK shall only be lifted by the lifting lugs with surrounding air temperatures $\ge 0^{\circ}$ F.

B 3.4.2 Maine Yankee Site Specific Parameters and Analyses

The design basis site-specific parameters and analyses that require verification by Maine Yankee are:

- 1. The temperature of 76°F is the maximum average yearly temperature. The 3-day average ambient temperature shall be 106°F or less.
- 2. The allowed temperature extremes, averaged over a 3-day period, shall be greater than -40°F and less than 133°F.
- 3. The design basis earthquake horizontal and vertical seismic acceleration levels at the top surface of the ISFSI pad are bounded by the values shown:

Horizontal g-level in each of	Corresponding Vertical
Two Orthogonal Directions	g-level (upward)
0.38g	$0.38 \times 0.667 = 0.253$ g

- 4. The analyzed flood condition of 15 fps water velocity and a height of 50 feet of water (full submergence of the loaded cask) are not exceeded.
- 5. The potential for fire and explosion shall be addressed, based on site-specific considerations. This includes the condition that the fuel tank of the cask handling equipment used to move the loaded CONCRETE CASK onto or from the ISFSI site contains no more than 50 gallons of fuel.
- 6. Physical testing shall be conducted to demonstrate that the coefficient of friction between the concrete cask and ISFSI pad surface is at least 0.5.

B 3.4.2 Maine Yankee Site Specific Parameters and Analyses (continued)

7. In addition to the requirements of 10 CFR 72.212(b)(2)(ii), the ISFSI pad(s) and foundation shall meet the design basis earthquake horizontal and vertical seismic acceleration levels at the top surface of the ISFSI pad as specified in B 3.4.2 (3).

The surface of the ISFSI pad shall have a broom finish or brushed surface as defined in ACI 116R-90 and described in Sections 7.12 and 7.13.4 of ACI 302.1R.

- 8. In cases where engineered features (i.e., berms, shield walls) are used to ensure that requirements of 10 CFR 72.104(a) are met, such features are to be considered important to safety and must be evaluated to determine the applicable Quality Assurance Category on a site specific basis.
- 9. TRANSFER CASK OPERATIONS shall only be conducted with surrounding air temperatures $\ge 0^{\circ}$ F.

B 3.5 CANISTER HANDLING FACILITY (CHF)

B 3.5.1 TRANSFER CASK and CANISTER Lifting Devices

Movements of the TRANSFER CASK and CANISTER outside of the 10 CFR 50 licensed facilities, when loaded with spent fuel are not permitted unless the movements are made with a CANISTER HANDLING FACILITY designed, operated, fabricated, tested, inspected and maintained in accordance with the guidelines of NUREG-0612, "Control of Heavy Loads at Nuclear Power Plants" and the below clarifications. This Technical Specification does not apply to handling heavy loads under a 10 CFR 50 license.

B 3.5.2 CANISTER HANDLING FACILITY Structure Requirements

B 3.5.2.1 CANISTER Station and Stationary Lifting Devices

- The weldment structure of the CANISTER HANDLING FACILITY shall be designed to comply with the stress limits of ASME Code, Section III, Subsection NF, Class 3 for linear structures. The applicable loads, load combinations, and associated service condition definitions are provided in Table 12B3-2. All compression loaded members shall satisfy the buckling criteria of ASME Code, Section III, Subsection NF.
- 2. If a portion of the CANISTER HANDLING FACILITY structure is constructed of reinforced concrete, then the factored load combinations set forth in ACI-318 (1995) for the loads defined in Table 12B3-2 shall apply.
- 3. The TRANSFER CASK and CANISTER lifting device used with the CANISTER HANDLING FACILITY shall be designed, fabricated, operated, tested, inspected and maintained in accordance with NUREG-0612, Section 5.1.

B 3.5.2.1 <u>CANISTER HANDLING Station and Stationary Lifting Devices</u> (continued)

4. The CHF design shall incorporate an impact limiter for CANISTER lifting and movement if a qualified single failure proof crane is not used. The impact limiter must be designed and fabricated to ensure that, if a CANISTER is dropped, the confinement boundary of the CANISTER would not be breached.

B 3.5.2.2 Mobile Lifting Devices

If a mobile lifting device is used as the lifting device, in lieu of a stationary lifting device, it shall meet the guidelines of NUREG-0612, Section 5.1, with the following clarifications:

- Mobile lifting devices shall have a minimum safety factor of two over the allowable load table for the lifting device in accordance with the guidance of NUREG-0612, Section 5.1.6(1)(a) and shall be capable of stopping and holding the load during a Design Basis Earthquake (DBE) event.
- Mobile lifting devices shall conform to the requirements of ANSI B30.5, "Mobile and Locomotive Cranes," in lieu of the requirements of ANSI B30.2, "Overhead and Gantry Cranes."
- 3. Mobile cranes are not required to meet the requirements of NUREG-0612, Section 5.1.6(2) for new cranes.

Table 12B3-2Load Combinations and Service Condition Definitions for the CANISTERHANDLING FACILITY (CHF) Structure

Load Combination	ASME Section III Service Condition for Definition of Allowable Stress	Comment
D*		All primary load bearing
	Level A	members must satisfy Level A
D + S		stress limits
$D + M + W'^{1}$		Factor of safety against
		overturning shall be ≥ 1.1
D + F		
	Level D	
D + E		
D + Y		

- D = Crane hook dead load
- D* = Apparent crane hook dead load
- S = Snow and ice load for the CHF site
- M = Tornado missile load of the CHF site¹
- W' = Tornado wind load for the CHF site¹
- F = Flood load for the CHF site
- E = Seismic load for the CHF site
- Y = Tsunami load for the CHF site

Note:

1. Tornado missile load may be reduced or eliminated based on a PRA for the CHF site.

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APPENDIX 12C

TECHNICAL SPECIFICATION BASES FOR THE NAC-UMS[®] SYSTEM

Appendix 12C

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Introduction C 1.0

C 1.0 Introduction

This Appendix presents the design or operational condition, or regulatory requirement, which establishes the bases for the Technical Specifications provided in Appendix 12A.

The section and paragraph numbering used in this Appendix is consistent to the numbering used in Appendix 12A, Technical Specifications for the NAC-UMS[®] SYSTEM, and Appendix 12B, Approved Contents and Design Features for the NAC-UMS[®] System.

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Approved Contents C 2.0

C 2.0 <u>APPROVED CONTENTS</u>

C 2.1 Fuel to be Stored in the NAC-UMS[®] SYSTEM

- BASES
- BACKGROUND The NAC-UMS[®] SYSTEM design requires specifications for the spent fuel to be stored, such as the type of spent fuel, minimum and maximum allowable enrichment prior to irradiation, maximum burnup, minimum acceptable post-irradiation cooling time prior to storage, maximum decay heat, and condition of the spent fuel (i.e., INTACT FUEL). Other important limitations are the dimensions and weight of the fuel assemblies.

The approved contents, which can be loaded into the NAC-UMS[®] SYSTEM are specified in Section B2.0 of Appendix 12B.

Specific limitations for the NAC-UMS[®] SYSTEM are specified in Table 12B2-1 of Appendix 12B. These limitations support the assumptions and inputs used in the thermal, structural, shielding, and criticality evaluations performed for the NAC-UMS[®] SYSTEM.

Actions required to respond to violations of any Approved Contents limits are provided in Section B2.1 of Appendix 12B.

APPLICABLE To ensure that the shield lid is not placed on a CANISTER containing SAFETY ANALYSES an unauthorized fuel assembly, facility procedures require verification of the loaded fuel assemblies to ensure that the correct fuel assemblies have been loaded in the canister.

APPROVED CONTENTS <u>C 2.1.1</u>

Approved Contents Section B2.0 refers to Table 12B2-1 in Appendix 12B for the specific fuel assembly characteristics for the PWR or BWR fuel assemblies authorized for loading into either the Standard or Advanced configurations of the NAC-UMS[®] SYSTEM. These fuel assembly characteristics include parameters such as cladding material, minimum and maximum enrichment, decay heat generation, post-irradiation cooling time, burnup, and fuel assembly length, width, and weight. Tables 12B2-2 through 12B2-5 are referenced from Table 12B2-1 and provide additional specific fuel characteristic limits for the fuel assemblies based on the fuel assembly class type, enrichment, burnup and cooling time for the Standard configuration.

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Approved Contents C 2.0

APPROVED CONTENTS (continued)	The fuel assembly characteristic limits of Tables 12B2-1 through 12B2-5 must be met to ensure that the thermal, structural, shielding, and criticality analyses supporting the Standard NAC-UMS [®] SYSTEM are bounding. Maine Yankee fuel is stored in the Standard configuration. Characteristics for the Maine Yankee fuel are provided in Tables 12B2-6 through 12B2-9. For the Advanced configuration, fuel assembly characteristics are presented in Tables 12B2-10 through 12B2-13. These tables are referenced in Table 12B2-1. The fuel assembly characteristic limits presented in these tables must be met to ensure that the thermal, structural, shielding, and criticality analyses supporting the Advanced NAC-UMS [®] SYSTEM are bounding.
	<u>C 2.1.2</u> Approved Contents Section B2.0 in Appendix 12B requires preferential loading of fuel assemblies with significantly different post-irradiation cooling times. This preferential loading is required to limit the heatup that a cooler assembly undergoes due to being surrounded by hotter fuel assemblies. For the purposes of complying with this Approved Contents limit, only fuel assemblies with post-irradiation cooling times differing by one year or greater need to be loaded preferentially. This is based on the fact that the heat-up phenomenon can only occur with significant differences in decay heat generation characteristics between adjacent fuel assemblies having different post-irradiation cooling times.
APPROVED CONTENT LIMITS AND VIOLATIONS	<u>C 2.2.1</u> If any Approved Contents limit of B2.1.1 through B2.1.4 in Appendix 12B is violated, the limitations on fuel assemblies to be loaded are not met. Action must be taken to place the affected fuel assembly(s) in a safe condition. This safe condition may be established by returning the affected fuel assembly(s) to the spent fuel pool. However, it is acceptable for the affected fuel assemblies to temporarily remain in the NAC-UMS [®] SYSTEM, in a wet or dry condition, if that is determined to be a safe condition.
	<u>C 2.2.2 and C 2.2.3</u> NRC notification of the Approved Contents limit violation is required within 24 hours. A written report on the violation must be submitted to the NRC within 30 days. This notification and written report are independent of any reports and notification that may be required by 10 CFR 72.216.
REFERENCES	1. SAR, Sections 2.1, 4.4; Chapters 5 and 6.

LCO Applicability C 3.0

C 3.0 LIMITING CONDITION FOR OPERATION (LCO) APPLICABILITY

BASES

- LCOs LCO 3.0.1, 3.0.2, 3.0.4, and 3.0.5 establish the general requirements applicable to all Specifications and apply at all times, unless otherwise stated.
- LCO 3.0.1 LCO 3.0.1 establishes the Applicability statement within each individual Specification as the requirement for when the LCO is required to be met (i.e., when the NAC-UMS[®] SYSTEM is in the specified conditions of the Applicability statement of each Specification).
- LCO 3.0.2 LCO 3.0.2 establishes that upon discovery of a failure to meet an LCO, the associated ACTIONS shall be met. The Completion Time of each Required Action for an ACTIONS Condition is applicable from the point in time that an ACTIONS Condition is entered. The Required Actions establish those remedial measures that must be taken within the specified Completion Times when the requirements of an LCO are not met. This Specification establishes that:
 - a. Completion of the Required Actions within the specified Completion Times constitutes compliance with a Specification; and,
 - b. Completion of the Required Actions is not required when an LCO is meet within the specified Completion Time, unless otherwise specified.

There are two basic Required Action types. The first Required Action type specifies a time limit, the Completion Time to restore a system or component or to restore variables to within specified limits, in which the LCO must be met. Whether stated as a Required Action or not, correction of the entered Condition is an action that may always be considered upon entering ACTIONS. The second Required Action type specifies the remedial measures that permit continued activities that are not further restricted by the Completion Time. In this case, compliance with the Required Actions provides an acceptable level of safety for continued operation.

LCO Applicability C 3.0

LCO 3.0.2 (continued)	Completing the Required Actions is not required when an LCO is met or is no longer applicable, unless otherwise stated in the individual Specifications.	
	The Completion Times of the Required Actions are also applicable when a system or component is removed from service intentionally. The reasons for intentionally relying on the ACTIONS include, but are not limited to, performance of Surveillance, preventive maintenance, corrective maintenance, or investigation of operational problems. Entering ACTIONS for these reasons must be done in a manner that does not compromise safety. Intentional entry into ACTIONS should not be made for operational convenience.	
LCO 3.0.3	This specification is not applicable to the NAC-UMS [®] SYSTEM because it describes conditions under which a power reactor must be shut down when an LCO is not met and an associated ACTION is not met or provided. The placeholder is retained for consistency with the power reactor technical specifications.	
LCO 3.0.4	LCO 3.0.4 establishes limitations on changes in specified conditions in the Applicability when an LCO is not met. It precludes placing the facility in a specified condition stated in that Applicability (e.g., Applicability desired to be entered) when the following exist:	
	a. NAC-UMS [®] SYSTEM conditions are such that the requirements of the LCO would not be met in the Applicability desired to be entered; and	
	b. Continued noncompliance with the LCO requirements, if the Applicability were entered, would result in NAC-UMS [®] SYSTEM activities being required to exit the Applicability desired to be entered to comply with the Required Actions.	
	Compliance with Required Actions that permit continued operation for an unlimited period of time in a specified condition provides an acceptable level of safety for continued operation. This is without regard to the status of the NAC-UMS [®] SYSTEM. Therefore, in such cases, entry into a specified condition in the Applicability may be made in accordance with the provisions of the Required Actions.	

LCO Applicability C 3.0

LCO 3.0.4 (continued)	The provisions of this Specification should not be interpreted as endorsing the failure to exercise the good practice of restoring systems or components before entering an associated specified condition in the Applicability.
	The provisions of LCO 3.0.4 shall not prevent changes in specified conditions in the Applicability that are required to comply with ACTIONS. In addition, the provisions of LCO 3.0.4 shall not prevent changes in specified conditions in the Applicability that are related to the unloading of the NAC-UMS [®] SYSTEM.
	Exceptions to LCO 3.0.4 are stated in the individual Specifications. Exceptions may apply to all the ACTIONS or to a specific Required Action of a Specification.
LCO 3.0.5	LCO 3.0.5 establishes the allowance for restoring equipment to service under administrative controls when it has been removed from service or determined to not meet the LCO to comply with the ACTIONS. The sole purpose of the Specification is to provide an exception to LCO 3.0.2 (e.g. to not comply with the applicable Required Action[s]) to allow the performance of testing to demonstrate:
	a. The equipment being returned to service meets the LCO; or
	b. Other equipment meets the applicable LCOs.
	The administrative controls ensure the time the equipment is returned to service in conflict with the requirements of the ACTIONS is limited to the time absolutely necessary to perform the allowed testing. This Specification does not provide time to perform any other preventive or corrective maintenance.

C 3.0 SURVEILLANCE REQUIREMENT (SR) APPLICABILITY

BASES		
Surveillance Requirements (SRs)	SR 3.0.1 through SR 3.0.4 establish the general requirements applicable to all Specifications and apply at all times, unless otherwise stated.	
SR 3.0.1	SR 3.0.1 establishes the requirement that SRs must be met during the specified conditions in the Applicability for which the requirements of the LCO apply, unless otherwise specified in the individual SRs. This Specification is to ensure that Surveillance is performed to verify that systems and components meet the LCO and variables are within specified limits. Failure to meet Surveillance within the specified Frequency, in accordance with SR 3.0.2, constitutes a failure to meet an LCO.	
	Systems and components are assumed to meet the LCO when the associated SRs have been met. Nothing in this Specification, however, is to be construed as implying that systems or components meet the associated LCO when:	
	a. The systems or components are known to not meet the LCO, although still meeting the SRs; or,	
	b. The requirements of the Surveillance(s) are known to be not met between required Surveillance performances.	
	Surveillances do not have to be performed when the NAC-UMS [®] SYSTEM is in a specified condition for which the requirements of the associated LCO are not applicable, unless otherwise specified.	
	Surveillances, including those invoked by Required Actions, do not have to be performed on equipment that has been determined to not meet the LCO because the ACTIONS define the remedial measures that apply. Surveillances have to be met and performed in accordance with SR 3.0.2, prior to returning equipment to service. Upon completion of maintenance, appropriate post maintenance testing is required. This includes ensuring applicable Surveillances are not failed and their most recent performance is in accordance with SR 3.0.2. Post maintenance	

SR Applicability C 3.0

SR 3.0.1 (continued)	testing may not be possible in the current specified conditions in the Applicability, due to the necessary NAC-UMS [®] SYSTEM parameters not having been established. In these situations, the equipment may be considered to meet the LCO provided testing has been satisfactorily completed to the extent possible and the equipment is not otherwise believed to be incapable of performing its function. This will allow operation to proceed to a specified condition where other necessary post maintenance tests can be completed.
SR 3.0.2	SR 3.0.2 establishes the requirements for meeting the specified Frequency for Surveillances and any Required Action with a Completion Time that requires the periodic performance of the Required Action on a "once per" interval.
	This extension facilitates Surveillance scheduling and considers facility conditions that may not be suitable for conducting the Surveillance (e.g., transient conditions or other ongoing Surveillance or maintenance activities).
	The 25% extension does not significantly degrade the reliability that results from performing the Surveillance at its specified Frequency. This is based on the recognition that the most probable result of any particular Surveillance being performed is the verification of

conformance with the SRs. The exceptions to SR 3.0.2 are those Surveillances for which the 25% extension of the interval specified in the Frequency does not apply. These exceptions are stated in the individual Specifications as a Note in the Frequency stating, "SR 3.0.2 is not applicable."

As stated in SR 3.0.2, the 25% extension also does not apply to the initial portion of a periodic Completion Time that requires performance on a "once per..." basis. The 25% extension applies to each performance after the initial performance. The initial performance of the Required Action, whether it is a particular Surveillance or some other remedial action, is considered a single action with a single Completion time. One reason for not allowing the 25% extension to this Completion Time is that such an action usually verifies that no loss of function has occurred by checking the status of redundant or diverse components or accomplishes the function of the affected equipment in an alternative manner.

SR Applicability C 3.0

SR 3.0.2 (continued)	The provisions of SR 3.0.2 are not intended to be used repeatedly, merely as an operational convenience to extend Surveillance intervals or periodic Completion Time intervals beyond those specified.
SR 3.0.3	SR 3.0.3 establishes the flexibility to defer declaring affected equipment as not meeting the LCO or an affected variable outside the specified limits when a Surveillance has not been completed within the specified Frequency. A delay period of up to 24 hours or up to the limit of the specified Frequency, whichever is less, applies from the point in time that it is discovered that the Surveillance has not been performed in accordance with SR 3.0.2, and not at the time that the specified Frequency was not met.
	This delay period provides adequate time to complete Surveillances that have been missed. This delay period permits the completion of a Surveillance before complying with Required Actions or other remedial measures that might preclude completion of the Surveillance.
	The basis for this delay period includes: consideration of facility conditions, adequate planning, availability of personnel, the time required to perform the Surveillance, the safety significance of the delay in completing the required Surveillance, and the recognition that the most probable result of any particular Surveillance being performed is the verification of conformance with the requirements. When a Surveillance with a Frequency, based not on time intervals, but upon specified NAC-UMS [®] SYSTEM conditions, is discovered not to have been performed when specified, SR 3.0.3 allows the full delay period of 24 hours to perform the Surveillance.
	SR 3.0.3 also provides a time limit for completion of Surveillances that become applicable as a consequence of changes in the specified conditions in the Applicability imposed by the Required Actions.
	Failure to comply with specified Frequencies for SRs is expected to be an infrequent occurrence. Use of the delay period established by SR 3.0.3 is a flexibility, which is not intended to be used as an operational convenience to extend Surveillance intervals.

(continued)

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SR Applicability C 3.0

SR 3.0.3 (continued)	If a Surveillance is not completed within the allowed delay period, then the equipment is considered to not meet the LCO or the variable is considered outside the specified limits and the Completion Times of the Required Actions for the applicable LCO Conditions begin immediately upon expiration of the delay period. If a Surveillance is failed within the delay period, then the equipment does not meet the LCO, or the variable is outside the specified limits and the Completion Times of the Required Actions for the applicable LCO Conditions begin immediately upon the failure of the Surveillance.
SR 3.0.4	SR 3.0.4 establishes the requirement that all applicable SRs must be met before entry into a specified condition in the Applicability.
	This Specification ensures that system and component requirements and variable limits are met before entry into specified conditions in the Applicability for which these systems and components ensure safe operation of NAC-UMS [®] SYSTEM activities.
	The provisions of this Specification should not be interpreted as endorsing the failure to exercise the good practice of restoring systems or components before entering an associated specified condition in the Applicability.
	However, in certain circumstances, failing to meet an SR will not result in SR 3.0.4 restricting a change in specified condition. When a system, subsystem, division, component, device, or variable is outside its specified limits, the associated SR(s) are not required to be performed per SR 3.0.1, which states that Surveillances do not have to be performed on equipment that has been determined to not meet the LCO.
	(continued)

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SR Applicability C 3.0

SR 3.0.4 (continued) When equipment does not meet the LCO, SR 3.0.4 does not apply to the associated SR(s), since the requirement for the SR(s) to be performed is removed. Therefore, failing to perform the Surveillance(s) within the specified Frequency does not result in a SR 3.0.4 restriction to changing specified conditions of the Applicability. However, since the LCO is not in this situation, LCO 3.0.4 will govern any restrictions that may be (or may not) apply to specified condition changes.

The provisions of SR 3.0.4 shall not prevent changes in specified conditions in the Applicability that are required to comply with ACTIONS. In addition, the provisions of LCO 3.0.4 shall not prevent changes in specified conditions in the Applicability that are related to the unloading of the NAC-UMS[®] SYSTEM.

The precise requirements for performance of SRs are specified such that exceptions to SR 3.0.4 are not necessary. The specific time frames and conditions necessary for meeting the SRs are specified in the Frequency, in the Surveillance, or both. This allows performance of Surveillances, when the prerequisite condition(s) specified in a Surveillance procedure require entry into the specified condition in the Applicability of the associated LCO, prior to the performance or completion of a Surveillance. A Surveillance that could not be performed until after entering LCO Applicability, would have its Frequency specified such that is not "due" until the specific conditions needed are met.

Alternately, the Surveillance may be stated in the form of a Note as not required (to be met or to be performed) until a particular event, condition, or time has been reached. Further discussion of the specific formats of SRs' annotation is found in Section 1.4, Frequency.

C 3.1 NAC-UMS[®] SYSTEM Integrity

C 3.1.1 Standard CANISTER Maximum Time in Vacuum Drying

BASES

A TRANSFER CASK with an empty Standard configuration BACKGROUND CANISTER is placed into the spent fuel pool and loaded with fuel assemblies meeting the requirements of the Approved Contents limits. A shield lid is then placed on the CANISTER. The TRANSFER CASK and CANISTER are raised out of the spent fuel pool. The TRANSFER CASK and CANISTER are then moved into the cask decontamination area, where dose rates are measured and the CANISTER shield lid is welded to the CANISTER shell and the lid weld is examined, pressure tested, and leak tested. The water is drained from the CANISTER, and CANISTER cavity vacuum drying is performed. The CANISTER cavity is then backfilled with helium. Additional dose rates are measured, and the CANISTER vent port and drain port covers and structural lid are installed and welded. Nondestructive examinations are performed on the welds. Contamination measurements are completed prior to moving the TRANSFER CASK and CANISTER in position to transfer the CANISTER to the After the CANISTER is transferred, the CONCRETE CASK. CONCRETE CASK is then moved to the ISFSI. Limiting the elapsed time from the end of Standard CANISTER draining operations through dryness verification testing and subsequent backfilling of the CANISTER with helium ensures that the short-term temperature limits established in the Safety Analyses Report for the spent fuel cladding and CANISTER materials are not exceeded.

APPLICABLE Limiting the total time for loaded Standard CANISTER vacuum drying Operations ensures that the short-term temperature limits for the fuel cladding and CANISTER materials are not exceeded. If vacuum drying operations are not completed in the required time period, the CANISTER is backfilled with helium and the TRANSFER CASK and loaded CANISTER are submerged in the spent fuel pool for a minimum of 24 hours, or the TRANSFER CASK may be supplied with forced air cooling for 24 hours.

APPLICABLE SAFETY ANALYSIS (continued)	Analyses reported in the Safety Analysis Report conclude that spent fuel cladding and CANISTER material short-term temperature limits will not be exceeded for total elapsed time in the vacuum drying operation and in the TRANSFER CASK with the CANISTER filled with helium. Since the rate of heat up is slower for lower total heat loads, the time required to reach component limits is longer than for the design basis heat load. Consequently, longer time limits are specified for heat loads below the design basis for the PWR fuel configuration as shown in LCO 3.1.1. As shown in the LCO, for total heat loads not specified, the time limit for the next higher specified heat load is conservatively applied. Analysis also shows that the fuel cladding and CANISTER component temperatures are well below the allowable temperatures for the time durations specified from the end of in-pool cooling, or end of forced air cooling, the CANISTER through the completion of the vacuum drying and for the time specified in LCO 3.1.4 for the CANISTER in the TRANSFER CASK when backfilled with helium.
LCO	Limiting the length of time for vacuum drying operations for the CANISTER ensures that the spent fuel cladding and CANISTER material temperatures remain below the short-term temperature limits for the NAC-UMS [®] SYSTEM.
APPLICABILITY	The elapsed time restrictions for vacuum drying operations on a loaded Standard CANISTER apply during LOADING OPERATIONS from the completion point of CANISTER draining operations through the completion point of the CANISTER dryness verification testing. The LCO is not applicable to TRANSPORT OPERATIONS or STORAGE OPERATIONS.
ACTIONS	A note has been added to the ACTIONS, which states that, for this LCO, separate Condition entry is allowed for each NAC-UMS [®] SYSTEM. This is acceptable, since the Required Actions for each Condition provide appropriate compensatory measures for each NAC-UMS [®] SYSTEM not meeting the LCO. Subsequent NAC-UMS [®] SYSTEMS that do not meet the LCO are governed by subsequent Condition entry and application of associated Required Actions.

ACTIONS (continued) A.1.1

If the LCO time limit is exceeded, the CANISTER will be backfilled with helium to a pressure of 0 psig (+1,-0).

<u>AND</u>

<u>A.2.1</u>

The TRANSFER CASK and loaded CANISTER shall be submerged in the spent fuel pool for in-pool cooling operations.

<u>AND</u>

<u>A.2.2</u>

The TRANSFER CASK and loaded CANISTER shall be maintained submerged in the spent fuel pool for a minimum of 24 hours prior to the restart of LOADING OPERATIONS.

<u>OR</u>

<u>A.3.1</u>

A cooling airflow of 375 CFM at a maximum temperature of 76°F shall be initiated. The airflow will be routed to the annulus fill/drain lines of the TRANSFER CASK and will flow through the annulus and cool the CANISTER.

<u>AND</u>

<u>A.3.2</u>

The cooling airflow shall be maintained for a minimum of 24 hours prior to restart of LOADING OPERATIONS.

SURVEILLANCE SR 3.1.1.1 REQUIREMENTS The element time shall be maniformed from a lation

The elapsed time shall be monitored from completion of CANISTER draining through completion of the CANISTER vacuum dryness verification testing. Monitoring the elapsed time ensures that helium backfill and in-pool cooling operations can be initiated in a timely manner during LOADING OPERATIONS to prevent fuel cladding and Standard CANISTER materials from exceeding short-term temperature limits.

SR 3.1.1.2

The elapsed time shall be monitored from the end of in-pool cooling through completion of the CANISTER vacuum dryness verification testing. Monitoring the elapsed time ensures that helium backfill and in-pool cooling operations can be initiated in a timely manner during LOADING OPERATIONS to prevents fuel cladding and Standard CANISTER materials from exceeding short-term temperature limits.

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REFERENCES 1. SAR Sections 4.4 and 8.1.

CANISTER Vacuum Drying Pressure C 3.1.2

- C 3.1 NAC-UMS[®] SYSTEM Integrity
- C 3.1.2 CANISTER Vacuum Drying Pressure
- BASES

BACKGROUND	A TRANSFER CASK with an empty CANISTER is placed into the spent fuel pool and loaded with fuel assemblies meeting the requirements of the Approved Contents Limits. A shield lid is then placed on the CANISTER. The TRANSFER CASK and CANISTER are raised out of the spent fuel pool. The TRANSFER CASK and CANISTER are then moved into the cask decontamination area, where dose rates are measured and the CANISTER shield lid is welded to the CANISTER shell and the lid weld is examined, pressure tested, and leak tested. The water is drained from the CANISTER, and CANISTER cavity vacuum drying is performed. The CANISTER cavity is then backfilled with helium. Additional dose rates are measured, and the CANISTER vent port and drain port covers and structural lid are installed and welded. Non-destructive examinations are performed on the welds. Contamination measurements are completed prior to moving the TRANSFER CASK and CANISTER in position to transfer the CANISTER to the CONCRETE CASK. After the CANISTER is transferred, the CONCRETE CASK is then moved to the ISFSI.
	CANISTER cavity vacuum drying is utilized to remove residual moisture from the CANISTER cavity after the water is drained from the CANISTER. Any water not drained from the CANISTER cavity evaporates due to the vacuum. This is aided by the temperature increase, due to the heat generation of the fuel.
APPLICABLE SAFETY ANALYSIS	The confinement of radioactivity (including fission product gases, fuel fines, volatiles, and crud) during the storage of design basis spent fuel in the CANISTER is ensured by the multiple confinement boundaries and systems. The barriers relied on are: the fuel pellet matrix, the metallic fuel cladding tubes where the fuel pellets are contained, and the CANISTER where the fuel assemblies are stored. Long-term integrity of the fuel and cladding depends on storage in an inert atmosphere. This is accomplished by removing water from the CANISTER and backfilling the cavity with helium. The thermal analysis assumes that the CANISTER cavity is dried and filled with helium.

CANISTER Vacuum Drying Pressure C 3.1.2

APPLICABLE	The heat-up of the CANISTER and contents will occur during
APPLICABLE SAFETY ANALYSIS (continued)	The heat-up of the CANISTER and contents will occur during CANISTER vacuum drying, but is controlled by LCO 3.1.1 or 3.1.8, based on the CANISTER configuration. Dryness of the CANISTER (e.g., no free water) is verified by holding a vacuum of 10 mm Hg or less for a period of not less than 10 minutes with no pressure rise during the 10 minute period after the pressure stabilizes. Operation of the valves to isolate the system can cause fluctuation in the measure pressure. The time period should start after the pressure stabilizes below 10 mm Hg. The vapor pressure of water at 70°F is approximately 30 mm Hg. Selecting a pressure that is 1/3 of the vapor pressure at 70°F ensures that all of the free water in the CANISTER is removed without excursion to a low vacuum condition that could lead to icing. The actual temperature in the loaded CANISTER is expected to be above 70°F, which would result in a higher vapor pressure. Consequently, the vacuum pressure of 10 mm Hg is conservatively selected. Holding the vacuum pressure for 10 minutes demonstrates that there is no free water since the presence of any free water results in a pressure of at least 30 mm Hg within the CANISTER. The removal of oxidizing gases that could lead to fuel cladding deterioration is assured by deep vacuum excursion to 3 mm Hg (minimum). After this vacuum condition is achieved the CANISTER is backfilled with helium to one atmosphere. After the backfill, the CANISTER is subjected again to a 3 mm Hg vacuum condition. The CANISTER is then backfilled with helium and sealed. The removal of oxidizing gases and the establishment of an inert atmosphere in the CANISTER is then backfilled with helium and sealed.
	controlled by LCO 3.1.3. These vacuum cycles ensure that the canister contents are dry and that the atmosphere in the canister is essentially free (< one mole) of any gases that could attack the fuel cladding, as recommended by PNL-6365.
LCO	A vacuum pressure of 10 mm Hg indicates that liquid water has evaporated and been removed from the CANISTER cavity. Removing water from the CANISTER cavity helps to ensure the long-term maintenance of fuel cladding integrity.
APPLICABILITY	Cavity vacuum drying is performed during LOADING OPERATIONS before the TRANSFER CASK holding the CANISTER is moved to transfer the CANISTER into the CONCRETE CASK. Therefore, the vacuum requirements do not apply after the CANISTER is backfilled with helium and leak tested prior to TRANSPORT OPERATIONS and STORAGE OPERATIONS. The vacuum drying pressure applies to the Standard and Advanced CANISTERs, as the CANISTERs have the same vacuum condition requirement.

CANISTER Vacuum Drying Pressure C 3.1.3

ACTIONS

A note has been added to the ACTIONS, which states that, for this LCO, separate Condition entry is allowed for each CANISTER. This is acceptable, since the Required Actions for each Condition provide appropriate compensatory measures for each CANISTER not meeting the LCO. Subsequent CANISTERs that do not meet the LCO are governed by subsequent Condition entry and application of associated Required Actions.

<u>A.1</u>

If the CANISTER cavity vacuum drying pressure limit cannot be met, actions must be taken to meet the LCO. Failure to successfully complete cavity vacuum drying could have many causes, such as failure of the vacuum drying system, inadequate draining, ice clogging of the drain lines, or leaking CANISTER welds. The Completion Time is sufficient to determine and correct most failure mechanisms. Excessive heat-up of the CANISTER and contents is precluded by LCO 3.1.1 for the Standard CANISTER and LCO 3.1.8 for the Advanced CANISTER.

<u>B.1</u>

If the CANISTER fuel cavity cannot be successfully vacuum dried, the fuel must be placed in a safe condition. Corrective actions may be taken after the fuel is placed in a safe condition to perform the A.1 action provided that the initial conditions for performing A.1 are met. A.1 may be repeated as necessary prior to performing B.1. The time frame for completing B.1 can not be extended by re-performing A.1. The Completion Time is reasonable, based on the time required to reflood the CANISTER, perform fuel cooldown operations, cut the shield lid weld, move the TRANSFER CASK into the spent fuel pool, and remove the CANISTER shield lid in an orderly manner and without challenging personnel. SR 3.1.2.1 SURVEILLANCE The long-term integrity of the stored fuel is dependent on storage in a REQUIREMENTS dry, inert environment. Cavity dryness is demonstrated by evacuating the cavity to a very low absolute pressure and verifying that the pressure is held over a specified period of time. A low vacuum pressure is an indication that the cavity is dry. The surveillance must be performed prior to TRANSPORT OPERATIONS. This allows

sufficient time to backfill the CANISTER cavity with helium, while minimizing the time the fuel is in the CANISTER without water or the assumed inert atmosphere in the cavity.

REFERENCES 1. SAR Sections 4.4, 7.1 and 8.1.

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CANISTER Vacuum and Helium Backfill Pressure C 3.1.3

C 3.1 NAC-UMS[®] SYSTEM Integrity

C 3.1.3 CANISTER Vacuum and Helium Backfill Pressure

BASES

BACKGROUND A TRANSFER CASK with an empty CANISTER is placed into the spent fuel pool and loaded with fuel assemblies meeting the requirements of the Approved Contents limits. A shield lid is then placed on the CANISTER. The TRANSFER CASK and CANISTER are raised out of the spent fuel pool. The TRANSFER CASK and CANISTER are then moved into the cask decontamination area, where dose rates are measured and the CANISTER shield lid is welded to the CANISTER shell and the lid weld is examined, pressure tested, and The water is drained from the CANISTER, and leak tested. CANISTER cavity vacuum drying is performed. The CANISTER cavity is then backfilled with helium. Additional dose rates are measured, and the CANISTER vent port and drain port covers and structural lid are installed and welded. Non-destructive examinations are performed on the welds. Contamination measurements are completed prior to moving TRANSFER CASK and CANISTER in position to transfer the CANISTER to the CONCRETE CASK. After the CANISTER is transferred, the CONCRETE CASK is then moved to the ISFSI. Backfilling of the CANISTER cavity with helium promotes heat transfer from the spent fuel to the CANISTER structure and the inert atmosphere protects the fuel cladding. Providing a helium pressure equal to atmospheric pressure ensures that there will be no in-leakage of air over

APPLICABLE SAFETY ANALYSIS The confinement of radioactivity (including fission product gases, fuel fines, volatiles, and crud) during the storage of spent fuel in the CANISTER is ensured by the multiple confinement boundaries and systems. The barriers relied on are: the fuel pellet matrix, the metallic fuel cladding tubes where the fuel pellets are contained, and the CANISTER where the fuel assemblies are stored. Long-term integrity of the fuel and cladding depends on the ability of the NAC-UMS[®] SYSTEM to remove heat from the CANISTER and reject it to theenvironment. This is accomplished by removing water from the CANISTER cavity and backfilling the cavity with an inert gas.

the life of the CANISTER, which might be harmful to the heat transfer

features of the NAC-UMS[®] SYSTEM and harmful to the fuel.

CANISTER Vacuum and Helium Backfill Pressure C 3.1.3

APPLICABLE SAFETY ANALYSIS (continued)	Removal of free water from the CANISTER is controlled by LCO 3.1.2. The removal of oxidizing gases that could lead to fuel cladding deterioration is assured by deep vacuum excursion to 3 mm Hg (minimum). After this vacuum condition is achieved the CANISTER is backfilled with helium to one atmosphere. After the backfill, the CANISTER is subjected again to a 3 mm Hg vacuum condition. The CANISTER is then backfilled with helium to one atmosphere (0 [+3, - 0] psig) and sealed. These vacuum cycles ensure that the canister contents are dry and that the atmosphere in the canister is essentially free (< one mole) of any oxidizing gases, as recommended by PNL-6365. The heat-up of the CANISTER and contents will continue following backfilling with helium, but is controlled by LCO 3.1.4. The heat-up of the CANISTER and contents will continue following with helium, but is controlled by LCO 3.1.4. The heat-up of the CANISTER and contents will continue following backfilling with helium, but is controlled by LCO 3.1.4. The heat-up of the CANISTER and contents will continue following backfilling with helium, but is controlled by LCO 3.1.4. The heat-up of the CANISTER and contents will continue following backfilling with helium, but is controlled by LCO 3.1.4. The heat-up of the CANISTER and contents will continue following backfilling with helium, but is controlled by LCO 3.1.4. The heat-up of the CANISTER and contents will continue following backfilling with helium, but is controlled by LCO 3.1.4. The heat-up of the CANISTER and by LCO 3.1.9 for the Advanced CANISTER.
	cavity is dried and filled with dry helium.
LCO	Backfilling the CANISTER cavity with helium at a pressure equal to atmospheric pressure ensures that there is no air in-leakage into the CANISTER, which could decrease the heat transfer properties and result in increased cladding temperatures and damage to the fuel cladding over the storage period. The helium backfill pressure was selected based on a minimum helium purity of 99.9% to ensure that the CANISTER internal pressure and heat transfer from the CANISTER to the environment are maintained consistent with the design and analysis basis of the CANISTER.
APPLICABILITY	Helium backfill is performed during LOADING OPERATIONS, before the TRANSFER CASK and CANISTER are moved to the CONCRETE CASK for transfer of the CANISTER. Therefore, the backfill pressure requirements do not apply after the CANISTER is backfilled with helium and leak tested prior to TRANSPORT OPERATIONS and STORAGE OPERATIONS. The vacuum drying pressure applies to the Standard and Advanced CANISTERs, as the CANISTERs have the same helium backfill requirement.
ACTIONS	A note has been added to the ACTIONS, which states that, for this LCO, separate Condition entry is allowed for each CANISTER. This is acceptable, since the Required Actions for each Condition provide appropriate compensatory measures for each CANISTER not meeting the LCO. A note has been added to the ACTIONS, which states that,

CANISTER Vacuum and Helium Backfill Pressure C 3.1.3

ACTIONS (continued) for this LCO, separate Condition entry is allowed for each CANISTER. This is acceptable, since the Required Actions for each Condition provide appropriate compensatory measures for each CANISTER not meeting the LCO. Subsequent CANISTERs that do not meet the LCO are governed by subsequent condition entry and application of associated Required Actions.

<u>A.1</u>

B.1

If the backfill pressure cannot be established within limits, actions must be taken to meet the LCO. The Completion Time is sufficient to determine and correct most failures, which would prevent backfilling of the CANISTER cavity with helium. These actions include identification and repair of helium leak paths or replacement of the helium backfill equipment.

ACTIONS

If the CANISTER cavity cannot be backfilled with helium to the specified pressure, the fuel must be placed in a safe condition. Corrective actions may be taken after the fuel is placed in a safe condition to perform the A.1 action provided that the initial conditions for performing A.1 are met. A.1 may be repeated as necessary prior to performing B.1. The time frame for completing B.1 can not be extended by reperforming A.1. The Completion Time is reasonable based on the time required to re-flood the CANISTER, perform cooldown operations, cut the CANISTER shield lid weld, move the TRANSFER CASK and CANISTER into the spent fuel pool, remove the CANISTER shield lid, and remove the spent fuel assemblies in an orderly manner and without challenging personnel.

SURVEILLANCE REQUIREMENTS

<u>SR 3.1.3.1</u>

1.

The long-term integrity of the stored fuel is dependent on storage in a dry, inert atmosphere and maintenance of adequate heat transfer mechanisms. Filling the CANISTER cavity with helium at a pressure in the range specified in LCO 3.1.3 will ensure that there will be no air in-leakage, which could potentially damage the fuel. This pressure of helium gas is sufficient to maintain fuel cladding temperatures within acceptable levels. Backfilling of the CANISTER cavity must be performed successfully on each CANISTER before placing it in storage. The Surveillance must be performed prior to TRANSPORT OPERATIONS. This allows sufficient time to backfill the cavity with helium, while minimizing the time the loaded CANISTER is in the TRANSFER CASK without the assumed inert atmosphere in the cavity. The CANISTER can be maintained in a safe condition based on the use of FORCED AIR COOLING or WATER COOLING.

REFERENCES

SAR Sections 4.4, 7.1 and 8.1.
- C 3.1 NAC-UMS[®] SYSTEM Integrity
- C 3.1.4 Standard CANISTER Maximum Time in the TRANSFER CASK
- BASES

BACKGROUND

A TRANSFER CASK with an empty Standard CANISTER is placed into the spent fuel pool and loaded with fuel assemblies meeting the requirements of the Approved Contents limits. A shield lid is then placed on the CANISTER. The TRANSFER CASK and CANISTER are raised out of the spent fuel pool. The TRANSFER CASK and CANISTER are then moved into the cask decontamination area, where dose rates are measured and the CANISTER shield lid is welded to the CANISTER shell and the lid weld is examined, pressure tested, and The water is drained from the CANISTER, and leak tested. CANISTER cavity vacuum drying is performed. The CANISTER cavity is then backfilled with helium. Additional dose rates are measured, and the CANISTER vent port and drain port covers and structural lid are installed and welded. Non-destructive examinations are performed on the welds. Contamination measurements are completed prior to moving TRANSFER CASK and CANISTER in position to transfer the CANISTER to the CONCRETE CASK. After the CANISTER is transferred, the CONCRETE CASK is then moved to the ISFSI.

Backfilling the CANISTER cavity with helium promotes heat transfer from the fuel and the inert atmosphere protects the fuel cladding. Limiting the total time the loaded CANISTER is in the TRANSFER CASK, prior to its placement in the CONCRETE CASK, ensures that the short-term temperature limits established in the Safety Analysis Report for the spent fuel cladding and CANISTER materials are not exceeded.

APPLICABLE SAFETY ANALYSIS

Limiting the total time that a loaded Standard CANISTER backfilled with helium may be in the TRANSFER CASK, prior to placement in the CONCRETE CASK, ensures that the short-term temperature limits for the spent fuel cladding and CANISTER materials are not exceeded. Upon placement of the loaded CANISTER in the CONCRETE CASK, the temperatures of the CANISTER and stored spent fuel will return to normal storage condition values due to the more efficient passive heat transfer characteristics of the CONCRETE

	APPLICABLE SAFETY ANALYSIS (continued)	CASK. Ensuring temperatures are maintained below short-term limits for a limited time period and returning them to values below long-term limits will prevent damage to the spent fuel cladding and the CANISTER materials.
		Analyses reported in the Safety Analysis Report conclude that spent fuel cladding and Standard CANISTER material short-term temperature limits will not be exceeded for the total elapsed times specified. Since the rate of heat up is slower for lower total heat loads, the time required
		to reach component limits is longer than for the design basis heat load. Consequently, longer time limits are specified for PWR fuel heat loads below the design basis heat load. As shown in the LCO, for total heat loads not specified, the time limit for the next higher specified heat load is conservatively applied. Analysis also shows that the fuel cladding and CANISTER component temperatures are below their allowable temperatures for the time durations specified with the CANISTER in the TRANSFER CASK and backfilled with helium when the CANISTER is cooled in-pool or using forced air.
-		The basis for forced air cooling is an inlet maximum air temperature of 76°F which is the maximum normal ambient air temperature in the thermal analysis. The specified 375 CFM air flow rate exceeds the CONCRETE CASK natural convective cooling flow rate by a minimum of 10 percent. This comparative analysis conservatively excludes the higher flow velocity resulting from the smaller annulus between the TRANSFER CASK and Standard CANISTER, which would result in improved heat transfer from the CANISTER.
_	LCO	Limiting the length of time that the loaded CANISTER backfilled with helium is allowed to remain in the TRANSFER CASK ensures that the spent fuel cladding and CANISTER material temperatures remain below the short-term temperature limits established in the SAR for the NAC-UMS [®] SYSTEM. The time duration is a function of the design of the TRANSFER CASK and the Standard NAC-UMS [®] SYSTEM.
	APPLICABILITY	The elapsed time restrictions on the loaded Standard CANISTER apply during LOADING OPERATIONS from the completion point of the CANISTER vacuum dryness verification through completion of the transfer from the TRANSFER CASK to the CONCRETE CASK. The elapsed time restriction on the loaded Advanced CANISTER are provided in LCO 3.1.9.

ACTIONS

A note has been added to the ACTIONS, which states that, for this LCO, separate Condition entry is allowed for each NAC-UMS[®] SYSTEM. This is acceptable, since the Required Actions for each Condition provide appropriate compensatory measures for each NAC-UMS[®] SYSTEM not meeting the LCO. Subsequent NAC-UMS[®] SYSTEMS that do not meet the LCO are governed by subsequent Condition entry and application of associated Required Actions.

<u>A.1.1</u>

If either LCO time limit is exceeded, the TRANSFER CASK containing the loaded Standard CANISTER backfilled with helium will be returned to the spent fuel pool to allow the cooler spent fuel pool water to reduce the TRANSFER CASK, CANISTER, and spent fuel cladding temperatures to below long-term temperature limits.

<u>AND</u>

<u>A.1.2</u>

The TRANSFER CASK and loaded Standard CANISTER shall be kept in the spent fuel pool for a minimum of 24 hours prior to restart of LOADING OPERATIONS.

<u>OR</u>

ACTIONS (continued) A.2.1

A cooling airflow of 375 CFM at a maximum temperature of 75°F shall be initiated. The airflow will be routed to the annulus fill/drain lines in the TRANSFER CASK and will flow through the annulus and cool the CANISTER.

<u>AND</u>

<u>A.2.2</u>

The cooling airflow shall be maintained for a minimum of 24 hours prior to restart of LOADING OPERATIONS.

<u>OR</u>

<u>A.2.3</u>

A cooling airflow of 375 CFM at a maximum temperature of 76°F shall be maintained while LOADING OPERATIONS continue. However, operations may be ended if required by other considerations. The airflow will be routed to the annulus fill/drain lines of the TRANSFER CASK and will flow through the annulus and cool the CANISTER.

SURVEILLANCE REQUIREMENTS

SR 3.1.4.1

The elapsed time from completion of CANISTER dryness verification until CANISTER transfer operations into the CONCRETE CASK are completed shall be monitored. The SR ensures that CANISTER material and fuel cladding short-term temperature limits are not exceeded.

SR 3.1.4.2

The elapsed time from the completion of in-pool or forced air cooling until CANISTER transfer operations into the CONCRETE CASK are completed shall be monitored. This SR ensures that CANISTER materials and fuel cladding short-term temperature limits are not exceeded. This SR is also applicable to the maximum time the CANISTER backfilled with helium can be loaded in the TRANSFER CASK if forced air or in-pool cooling operations were performed during vacuum drying operations under LCO 3.1.1.

REFERENCES 1. SAR Sections 4.4 and 8.1.

CANISTER Helium Leak Rate C 3.1.5

- C 3.1 NAC-UMS[®] SYSTEM Integrity
- C 3.1.5 CANISTER Helium Leak Rate
- BASES

1	BACKGROUND	A TRANSFER CASK with an empty CANISTER is placed into the spent fuel pool and loaded with fuel assemblies meeting the requirements of the Approved Contents limits. A shield lid is then placed on the CANISTER. The TRANSFER CASK and CANISTER are raised out of the spent fuel pool. The TRANSFER CASK and CANISTER are then moved into the cask decontamination area, where dose rates are measured and the CANISTER shield lid is welded to the CANISTER shell and the lid weld is examined, pressure tested, and leak tested. The water is drained from the CANISTER, and CANISTER cavity vacuum drying is performed. The CANISTER cavity is then backfilled with helium. Additional dose rates are measured, and the CANISTER vent port and drain port covers and structural lid are installed and welded. Nondestructive examinations are performed on the welds. Contamination measurements are completed prior to moving TRANSFER CASK and CANISTER in position to transfer the CANISTER to the CONCRETE CASK. After the CANISTER is transferred, the CONCRETE CASK is then moved to the ISFSI.
		Backfilling the CANISTER cavity with helium promotes heat transfer from the fuel to the CANISTER shell. The inert atmosphere protects the fuel cladding. Prior to transferring the CANISTER to the CONCRETE CASK, the CANISTER helium leak rate is verified to meet leaktight requirements to ensure that the fuel and helium backfill gas is confined.
	APPLICABLE SAFETY ANALYSIS	The confinement of radioactivity (including fission product gases, fuel fines, volatiles, and crud) during the storage of spent fuel in the CANISTER is ensured by the multiple confinement boundaries and systems. The barriers relied on are: the fuel pellet matrix, the metallic fuel cladding tubes where the fuel pellets are contained, and the CANISTER where the fuel assemblies are stored. Long-term integrity of the fuel and cladding depends on maintaining an inert atmosphere, and maintaining the cladding temperatures below established long-term limits. This is accomplished by removing water from the CANISTER and backfilling the cavity with helium. The heat-up of the CANISTER and contents will continue following backfilling the cavity and leak testing the shield lid-to-shell weld, but is controlled by LCO 3.1.4 for the Standard CANISTER and by LCO 3.1.9 for the Advanced CANISTER.

CANISTER Helium Leak Rate C 3.1.5

LCO Verifying that the CANISTER cavity helium leak rate is below the leaktight limit specified in LCO 3.1.5 ensures that the CANISTER shield lid is sealed. Verifying that the helium leak rate is below leaktight levels will also ensure that the assumptions in the accident analyses and radiological evaluations are maintained.

APPLICABILITY The leaktight helium leak rate verification is performed during LOADING OPERATIONS before the TRANSFER CASK and integral CANISTER are moved for transfer operations to the CONCRETE CASK. TRANSPORT OPERATIONS would not commence if the CANISTER helium leak rate was not below the test sensitivity. Therefore, CANISTER leak rate testing is not required during TRANSPORT OPERATIONS or STORAGE OPERATIONS. The allowable helium leak rate applies to the Standard and Advanced CANISTERs, as the CANISTERs have the same helium leak rate requirement to demonstrate a leaktight condition.

ACTIONS

A note has been added to the ACTIONS, which states that, for this LCO, separate Condition entry is allowed for each CANISTER. This is acceptable, since the Required Actions for each Condition provide appropriate compensatory measures for each CANISTER not meeting the LCO. Subsequent CANISTERs that do not meet the LCO are governed by subsequent Condition entry and application of associated Required Actions.

<u>A.1</u>

If the helium leak rate limit is not met, actions must be taken to meet the LCO. The Completion Time is sufficient to determine and correct most failures, which could cause a helium leak rate in excess of the limit. Actions to correct a failure to meet the helium leak rate limit would include, in ascending order of performance, 1) verification of helium leak test system performance; 2) inspection of weld surfaces to locate helium leakage paths using a helium sniffer probe; and 3) weld repairs, as required, to eliminate the helium leakage. Following corrective actions, the helium leak rate verification shall be reperformed.

CANISTER Helium Leak Rate C 3.1.5

ACTIONS (continued) <u>B.1</u>

If the CANISTER leak rate cannot be brought within the limit, the fuel must be placed in a safe condition. Corrective actions may be taken after the fuel is placed in a safe condition to perform the A.1 action provided that the initial conditions for performing A.1 are met. A.1 may be repeated as necessary prior to performing B.1. The time frame for completing B.1 can not be extended by re-performing A.1. The Completion Time is reasonable based on the time required to re-flood the CANISTER, perform fuel cooldown operations, cut the CANISTER shield lid weld, move the TRANSFER CASK into the spent fuel pool, remove the CANISTER shield lid, and remove the spent fuel assemblies in an orderly manner and without challenging personnel.

SURVEILLANCE REQUIREMENTS SR 3.1.5.1

The primary design consideration of the CANISTER is that it is leaktight to ensure that off-site dose limits are not exceeded and to ensure that the helium remains in the CANISTER during long-term storage. Long-term integrity of the stored fuel is dependent on storage in a dry, inert environment.

Verifying that the helium leak rate meets leaktight requirements must be performed successfully on each CANISTER prior to TRANSPORT OPERATIONS. The Surveillance Frequency allows sufficient time to backfill the CANISTER cavity with helium and performs the leak test, while minimizing the time the fuel is in the CANISTER and loaded in the TRANSFER CASK.

REFERENCES 1. SAR Sections 7.1 and 8.1.

CONCRETE CASK Heat Removal System C 3.1.6

C 3.1 NAC-UMS[®] SYSTEM Integrity

C 3.1.6 CONCRETE CASK Heat Removal System

BASES

BACKGROUND The CONCRETE CASK Heat Removal System is a passive, air-cooled convective heat transfer system, which ensures that heat from the CANISTER is transferred to the environment by the upward flow of air through the CONCRETE CASK. Relatively cool air is drawn into the annulus between the CONCRETE CASK and the CANISTER through the four air inlets at the bottom of the CONCRETE CASK. The CANISTER transfers its heat from the CANISTER surface to the air via natural convection. The buoyancy created by the heating of the air creates a chimney effect and the air flows back into the environment through the four air outlets at the top of the CONCRETE CASK.

APPLICABLE SAFETY ANALYSIS The thermal analyses of the CONCRETE CASK take credit for the decay heat from the spent fuel assemblies being ultimately transferred to the ambient environment surrounding the CONCRETE CASK. Transfer of heat away from the fuel assemblies ensures that the fuel cladding and CANISTER component temperatures do not exceed applicable limits. Under normal storage conditions, the four air inlets and four air outlets are unobstructed and full air flow (i.e., maximum heat transfer for the given ambient temperature) occurs.

Analyses have been performed for the complete obstruction of all of the air inlets and outlets. The complete blockage of all air inlets and outlets stops air cooling of the CANISTER. The CANISTER will continue to radiate heat to the relatively cooler inner shell of the CONCRETE CASK. With the loss of air cooling, the CANISTER component temperatures will increase toward their respective short-term temperature limits. The limiting component is the CANISTER basket support and heat transfer disks, which, by analysis, approach their temperature limits in 24 hours, if no action is taken to restore air flow to the heat removal system.

LCO

The CONCRETE CASK Heat Removal System must be verified to be OPERABLE to preserve the assumptions of the thermal analyses.

CONCRETE CASK Heat Removal System C 3.1.6

LCO (continued) Operability of the heat removal system ensures that the decay heat generated by the stored fuel assemblies is transferred to the environment at a sufficient rate to maintain fuel cladding and CANISTER component temperatures within design limits.

APPLICABILITY The LCO is applicable during STORAGE OPERATIONS. Once a CONCRETE CASK containing a CANISTER loaded with spent fuel has been placed in storage, the heat removal system must be OPERABLE to ensure adequate heat transfer of the decay heat away from the fuel assemblies. The operability of heat removal system applies to the Standard and Advanced CONCRETE CASKs, as the CONCRETE CASKs have the same heat removal requirement.

ACTIONS A note has been added to ACTIONS which states that, for this LCO, separate Condition entry is allowed for each CONCRETE CASK. This is acceptable since the Required Actions for each Condition provide appropriate compensatory measures for each CONCRETE CASK not meeting the LCO. Subsequent CONCRETE CASKs that do not meet the LCO are governed by subsequent Condition entry and application of associated Required Actions.

<u>A.1</u>

If the heat removal system has been determined to be inoperable, it must be restored to OPERABLE status within 8 hours. Eight hours is reasonable based on the accident analysis which shows that the limiting CONCRETE CASK component temperatures will not reach their temperature limits for 24 hours after a complete blockage of all inlet air ducts.

<u>B.1</u>

SR 3.1.6.1 is performed to document the continuing status of the operability of the CONCRETE CASK Heat Removal System.

<u>B.2.1</u>

Efforts must continue to restore the heat removal system to OPERABLE status by removing the air flow obstruction(s) unless optional Required Action B.2.2 is being implemented.

CONCRETE CASK Heat Removal System C 3.1.6

ACTIONS (continued)

B.2.1 (continued)

This Required Action must be completed in 12 hours. The Completion Time reflects a conservative total time period without any cooling of 24 hours. The results of the thermal analysis of this accident show that the fuel cladding temperature does not reach its short-term temperature limit for more than 24 hours. It is also unlikely that an unforeseen event could cause complete blockage of all four air inlets and outlets immediately after the last successful Surveillance.

SURVEILLANCE REQUIREMENTS

<u>SR 3.1.6.1</u>

The long-term integrity of the stored fuel is dependent on the ability of the CONCRETE CASK to reject heat from the CANISTER to the environment. The temperature rise between ambient and the CONCRETE CASK air outlets shall be monitored to verify operability of the heat removal system. Blocked air inlets or outlets will reduce air flow and increase the temperature rise experienced by the air as it removes heat from the CANISTER. Based on the analyses, provided the air temperature rise is less than the limits stated in the SR, adequate air flow and, therefore, adequate heat transfer is occurring to provide assurance of long-term fuel cladding integrity. The reference ambient temperature used to perform this Surveillance shall be measured at the ISFSI facility.

The Frequency of 24 hours is reasonable based on the time necessary for CONCRETE CASK components to heat up to unacceptable temperatures assuming design basis heat loads, and allowing for corrective actions to take place upon discovery of the blockage of the air inlets and outlets.

REFERENCES 1. SAR Chapter 4 and Chapter 11, Section 11.2.13.

C 3.1 NAC-UMS[®] SYSTEM Integrity

C 3.1.7 Standard CANISTER Removal from the CONCRETE CASK

BASES

BACKGROUND A loaded Standard CANISTER is removed from a CONCRETE CASK using the TRANSFER CASK, so that the CANISTER may be transferred to another CONCRETE CASK or transferred to a TRANSPORT CASK for purposes of transport. The CANISTER is removed from the CONCRETE CASK using the procedure provided in Section 8.2. Once in the TRANSFER CASK, the CANISTER begins to heat up due to the decay heat of the contents and the reduced heat transfer provided by the TRANSFER CASK compared to the CONCRETE CASK.

> The Standard CANISTER time in the TRANSFER CASK is limited when forced air cooling is not used to ensure that the short-term temperature limits established in the Safety Analysis Report for the spent fuel cladding and CANISTER materials are not exceeded.

> If forced air cooling is maintained, then the CANISTER time in the TRANSFER CASK is not limited, since the short-term temperature limits of the spent fuel cladding and of the CANISTER components are not exceeded.

APPLICABLE SAFETY ANALYSIS Limiting the total time that a loaded Standard CANISTER backfilled with helium may be in the TRANSFER CASK, prior to unloading the CANISTER from the TRANSFER CASK, ensures that the short-term temperature limits for the spent fuel cladding and CANISTER materials are not exceeded. Upon placement of the loaded CANISTER in the CONCRETE CASK or TRANSPORT CASK, the temperatures of the CANISTER and stored spent fuel will return to normal storage or transport condition values due to the more efficient passive heat transfer characteristics of the CONCRETE CASK or TRANSPORT CASK.

APPLICABLE SAFETY ANALYSIS (continued)

This ensures that temperatures are maintained below short-term limits for a limited time period. Returning these temperatures to values below long-term limits will prevent damage to the spent fuel cladding and the CANISTER materials.

From calculated temperatures reported in the Safety Analysis Report, it can be concluded that spent fuel cladding and CANISTER material short-term temperature limits will not be exceeded for a total elapsed time of greater than 24 hours for the BWR configuration, or for the time shown for PWR fuel, if the loaded Standard CANISTER backfilled with helium is in the TRANSFER CASK. If the time limit is met, forced airflow cooling is used to ensure cooling of the CANISTER. The analysis provided in the Safety Analysis Report shows that the spent fuel cladding and CANISTER temperatures will be at or below their long-term limits, as long as the cooling airflow is maintained. This forced airflow provides a similar rate of cooling to that provided by the passive airflow cooling provided by the CONCRETE CASK. Consequently, there is no time limit associated with the continued forced air cooling of the CANISTER while it is in the TRANSFER CASK. The basis for forced air cooling is an inlet maximum air temperature of 76°F, which is the maximum normal ambient air temperature in the thermal analysis. The specified 375 CFM air flow rate exceeds the CONCRETE CASK natural convective cooling flow rate by a minimum of 10 percent. This comparative analysis conservatively excludes the higher flow velocity resulting from the smaller annulus between the TRANSFER CASK and CANISTER, which would result in improved heat transfer from the CANISTER.

If forced air flow is continuously maintained for a period of 24 hours, or longer, then the temperatures of the spent fuel cladding and CANISTER components are at the values calculated for the CONCRETE CASK normal conditions. Consequently, forced air cooling may be ended, allowing a new entry into Condition A. This provides a new minimum 4-hour period in which continuation of the TRANSFER OPERATIONS may occur.

Limiting the length of time that the loaded Standard CANISTER backfilled with helium is allowed to remain in the TRANSFER CASK without forced air cooling ensures that the spent fuel cladding and CANISTER material temperatures remain below the short-term temperature limits established in the SAR for the NAC-UMS[®] SYSTEM. Once forced air cooling is established, the amount of time the CANISTER resides in the TRANSFER CASK is not limited since the cooling provided by the forced air is equivalent to the passive cooling that is provided by the CONCRETE CASK or TRANSPORT CASK.

If forced air flow is continuously maintained for a period of 24 hours, or longer, then the temperatures of the spent fuel cladding and CANISTER components are at, or below, the values calculated for the CONCRETE CASK normal conditions. Therefore, forced air cooling may be ended, allowing a new entry into Condition A of this LCO. This provides a new minimum 4-hour period in which continuation of TRANSFER OPERATIONS may occur.

APPLICABILITY

LCO

The elapsed time restrictions on the loaded Standard CANISTER apply during TRANSFER OPERATIONS from the completion point of the closing of the TRANSFER CASK shield doors through completion of the unloading of the CANISTER from the TRANSFER CASK.

The elapsed time restrictions on the loaded Advanced CANISTER are provided in LCO 3.1.10.

ACTIONS

A note has been added to the ACTIONS, which states that, for this LCO, separate Condition entry is allowed for each NAC-UMS[®] SYSTEM. This is acceptable, since the Required Actions for each Condition provide appropriate compensatory measures for each NAC-UMS[®] SYSTEM not meeting the LCO. Subsequent NAC-UMS[®] SYSTEMS that do not meet the LCO are governed by subsequent Condition entry and application of associated Required Actions.

Separate Condition A re-entry is also permitted after 24-hours of continuous forced air cooling in accordance with this LCO.

<u>A.1.1</u>

If the CANISTER can be loaded into an operable CONCRETE CASK without the LCO time limit being exceeded, then no further action is required since the spent fuel cladding and CANISTER component short-term temperature limits are not exceeded.

<u>OR</u>

<u>A.2.1</u>

If the CANISTER can be loaded into a TRANSPORT CASK without the LCO time limit being exceeded, then no further action is required since the spent fuel cladding and CANISTER component short-term temperature limits are not exceeded.

<u>OR</u> -

<u>A.3.1</u>

If forced air flow is continuously maintained for a period of 24 hours, or longer, then the temperatures of the spent fuel cladding and CANISTER components are at, or below, the values calculated for the CONCRETE CASK normal conditions. Consequently, forced air cooling may be ended, allowing a new entry into Condition A of this LCO, if required by other considerations. This provides a new minimum 4-hour period in which continuation or completion of TRANSFER OPERATIONS may occur.

ACTIONS (continued) <u>B.1.1</u>

Commence supplying air to the TRANSFER CASK annulus using the fill/drain lines at a rate of 375 CFM and a maximum temperature of 76°F. This action provides the equivalent cooling that would be provided by the passive heat removal systems of the CONCRETE CASK or TRANSPORT CASK in normal operations. Consequently, no short-term spent fuel cladding or CANISTER component temperature limits are exceeded.

<u>AND</u>

<u>B.2.1</u>

Maintain the airflow established by B.1.1 for the time period that the CANISTER remains in the TRANSFER CASK. This action provides the equivalent cooling that would be provided by the passive heat removal systems of the CONCRETE CASK or TRANSPORT CASK in normal operations. Consequently, no short-term spent fuel cladding or CANISTER component temperature limits are exceeded.

SURVEILLANCE REQUIREMENTS

SR 3.1.7.1

This SR ensures that the time that the CANISTER is in the TRANSFER CASK does not exceed the 4-hour limit without the use of forced air cooling of the CANISTER. This ensures that the short-term temperature limits of the spent fuel cladding and CANISTER components is not exceeded.

SR 3.1.7.2

This SR ensures that short-term temperature limits of the spent fuel cladding and CANISTER components are not exceeded by initiating and maintaining forced air cooling of the CANISTER in the TRANSFER CASK if the time limits established by Condition A are not met. Forced air cooling is maintained until unloading of the CANISTER from the TRANSFER CASK.

REFERENCES 1. SAR Sections 4.4 and 8.2.

Advanced CANISTER Maximum Time in Vacuum Drying C 3.1.8

C 3.1 NAC-UMS[®] SYSTEM Integrity

C 3.1.8 Advanced CANISTER Maximum Time in Vacuum Drying

BASES

BACKGROUND A TRANSFER CASK with an empty Advanced configuration CANISTER is placed into the spent fuel pool and loaded with fuel assemblies meeting the requirements of the Approved Contents limits. A shield lid is then placed on the CANISTER. The TRANSFER CASK and CANISTER are raised out of the spent fuel pool. The TRANSFER CASK and CANISTER are then moved into the cask decontamination area, where dose rates are measured and the CANISTER shield lid is welded to the CANISTER shell and the lid weld is examined, pressure tested, and leak tested. The water is drained from the CANISTER, and CANISTER cavity vacuum drying is performed. The CANISTER cavity is then backfilled with helium. Additional dose rates are measured, and the CANISTER vent port and drain port covers and structural lid are installed and welded. Nondestructive examinations are performed on the welds. Contamination measurements are completed prior to moving the TRANSFER CASK and CANISTER in position to transfer the CANISTER to the CONCRETE CASK. After the CANISTER is transferred, the CONCRETE CASK is then moved to the ISFSI.

Limiting the elapsed time from the end of Advanced CANISTER draining operations through dryness verification testing and subsequent backfilling of the CANISTER with helium ensures that the short-term temperature limits established in the Safety Analyses Report for the spent fuel cladding and CANISTER materials are not exceeded.

APPLICABLE Limiting the total time for loaded Advanced CANISTER vacuum drying operations ensures that the short-term temperature limits for the fuel cladding and CANISTER materials are not exceeded. If vacuum drying operations are not completed in the required time period, the CANISTER is backfilled with helium and the TRANSFER CASK and loaded CANISTER are submerged in the spent fuel pool for a minimum of 24 hours, or the TRANSFER CASK may be supplied with forced air cooling for 48 hours for heat loads ≥ 25 kW, or 24 hours for heat loads less than 25 kW.

Advanced CANISTER Maximum Time in Vacuum Drying C 3.1.8

APPLICABLE SAFETY ANALYSIS (continued)	The air flow rate must be 500 CFM for heat loads greater than or equal to 25 kW, but may be reduced to 375 CFM for heat loads less than 25 kW. Analyses reported in the Safety Analysis Report conclude that spent fuel cladding and CANISTER material short-term temperature limits will not be exceeded for total elapsed time in the vacuum drying operation and in the TRANSFER CASK with the CANISTER filled with helium. Since the rate of heat up is slower for lower total heat loads, the time required to reach component limits is longer than for the design basis heat load. Consequently, longer time limits are specified for heat loads below the design basis for the PWR fuel configuration as shown in LCO 3.1.1. As shown in the LCO, for total heat loads not specified, the time limit for the next higher specified heat load is conservatively applied. Analysis also shows that the fuel cladding and CANISTER component temperatures are well below the allowable temperatures for the time durations specified from the end of in-pool cooling, or end of forced air cooling, of the CANISTER through the completion of the vacuum drying and for the time specified in LCO 3.1.4 for the CANISTER in the TRANSFER CASK when backfilled with helium.
LCO	Limiting the length of time for vacuum drying operations for the CANISTER ensures that the spent fuel cladding and CANISTER material temperatures remain below the short-term temperature limits for the NAC-UMS [®] SYSTEM.
APPLICABILITY	The elapsed time restrictions for vacuum drying operations on a loaded Advanced CANISTER apply during LOADING OPERATIONS from the completion point of CANISTER draining operations through the completion point of the CANISTER dryness verification testing. The LCO is not applicable to TRANSPORT OPERATIONS or STORAGE OPERATIONS.
ACTIONS	A note has been added to the ACTIONS, which states that, for this LCO, separate Condition entry is allowed for each NAC-UMS [®] SYSTEM. This is acceptable, since the Required Actions for each Condition provide appropriate compensatory measures for each NAC-UMS [®] SYSTEM not meeting the LCO. Subsequent NAC-UMS [®] SYSTEMS that do not meet the LCO are governed by subsequent Condition entry and application of associated Required Actions.

Advanced CANISTER Maximum Time in Vacuum Drying C 3.1.8 ACTIONS (continued) A.1.1 If the LCO time limit is exceeded, the CANISTER will be backfilled with helium to a pressure of 0 psig (+1,-0). AND A.1.2 The TRANSFER CASK and loaded CANISTER shall be submerged in the spent fuel pool for in-pool cooling operations. AND A.1.3 The TRANSFER CASK and loaded CANISTER shall be maintained submerged in the spent fuel pool for a minimum of 24 hours prior to the restart of LOADING OPERATIONS. OR A.2.1 A cooling airflow at a maximum temperature of 76°F shall be initiated. The airflow will be routed to the annulus fill/drain lines of the TRANSFER CASK and will flow through the annulus and cool the CANISTER. AND A.2.2 The cooling airflow of 500 CFM shall be maintained for a minimum of 48 hours for heat loads greater than, or equal to, 25 kW prior to restart of LOADING OPERATIONS. <u>OR</u>

<u>A.2.3</u>

The cooling airflow of 375 CFM shall be maintained for a minimum of 24 hours for heat loads less than 25 kW prior to restart of LOADING OPERATIONS.

Advanced CANISTER Maximum Time in Vacuum Drying C 3.1.8

SURVEILLANCE REQUIREMENTS

SR 3.1.8.1

The elapsed time shall be monitored from completion of CANISTER draining through completion of the CANISTER vacuum dryness verification testing. Monitoring the elapsed time ensures that helium backfill and in-pool cooling operations can be initiated in a timely manner during LOADING OPERATIONS to prevent fuel cladding and Advanced CANISTER materials from exceeding short-term temperature limits.

SR 3.1.8.2

1.

The elapsed time shall be monitored from the end of in-pool cooling through completion of the CANISTER vacuum dryness verification testing. Monitoring the elapsed time ensures that helium backfill and in-pool cooling operations can be initiated in a timely manner during LOADING OPERATIONS to prevents fuel cladding and Advanced CANISTER materials from exceeding short-term temperature limits.

REFERENCES

SAR Sections 4.4 and 8.1.

- C 3.1 NAC-UMS[®] SYSTEM Integrity
- C 3.1.9 Advanced CANISTER Maximum Time in the TRANSFER CASK
- BASES

BACKGROUND A TRANSFER CASK with an empty Advanced CANISTER is placed into the spent fuel pool and loaded with fuel assemblies meeting the requirements of the Approved Contents limits. A shield lid is then placed on the CANISTER. The TRANSFER CASK and CANISTER are raised out of the spent fuel pool. The TRANSFER CASK and CANISTER are then moved into the cask decontamination area, where dose rates are measured and the CANISTER shield lid is welded to the CANISTER shell and the lid weld is examined, pressure tested, and The water is drained from the CANISTER, and leak tested. CANISTER cavity vacuum drying is performed. The CANISTER cavity is then backfilled with helium. Additional dose rates are measured, and the CANISTER vent port and drain port covers and structural lid are installed and welded. Non-destructive examinations are performed on the welds. Contamination measurements are completed prior to moving TRANSFER CASK and CANISTER in position to transfer the CANISTER to the CONCRETE CASK. After the CANISTER is transferred, the CONCRETE CASK is then moved to the ISFSI.

Backfilling the CANISTER cavity with helium promotes heat transfer from the fuel and the inert atmosphere protects the fuel cladding. Limiting the total time the loaded CANISTER is in the TRANSFER CASK, prior to its placement in the CONCRETE CASK, ensures that the short-term temperature limits established in the Safety Analysis Report for the spent fuel cladding and CANISTER materials are not exceeded.

APPLICABLE SAFETY ANALYSIS Limiting the total time that a loaded Advanced CANISTER backfilled with helium may be in the TRANSFER CASK, prior to placement in the CONCRETE CASK, ensures that the short-term temperature limits for the spent fuel cladding and CANISTER materials are not exceeded. Upon placement of the loaded CANISTER in the CONCRETE CASK, the temperatures of the CANISTER and stored spent fuel will return to normal storage condition values due to the more efficient passive heat transfer characteristics of the CONCRETE

CASK. Ensuring temperatures are maintained below short-term limits APPLICABLE for a limited time period and returning them to values below long-term SAFETY ANALYSIS limits will prevent damage to the spent fuel cladding and the (continued) CANISTER materials. Analyses reported in the Safety Analysis Report conclude that spent fuel cladding and Advanced CANISTER material short-term temperature limits will not be exceeded for the total elapsed times specified. Since the rate of heat up is slower for lower total heat loads, the time required to reach component limits is longer than for the design basis heat load. Consequently, longer time limits are specified for PWR fuel heat loads below the design basis heat load. As shown in the LCO, for total heat loads not specified, the time limit for the next higher specified heat load is conservatively applied. Analysis also shows that the fuel cladding and CANISTER component temperatures are below their allowable temperatures for the time durations specified with the CANISTER in the TRANSFER CASK and backfilled with helium when the CANISTER is cooled in-pool or using forced air. The basis for forced air cooling is an inlet maximum air temperature of 76°F which is the maximum normal ambient air temperature in the thermal analysis. The specified 500 CFM air flow rate exceeds the CONCRETE CASK natural convective cooling flow rate by a minimum of 10 percent. This comparative analysis conservatively excludes the higher flow velocity resulting from the smaller annulus between the TRANSFER CASK and Advanced CANISTER, which would result in improved heat transfer from the CANISTER. LCO Limiting the length of time that the loaded CANISTER backfilled with helium is allowed to remain in the TRANSFER CASK ensures that the spent fuel cladding and CANISTER material temperatures remain below the short-term temperature limits established in the SAR for the NAC-UMS[®] SYSTEM. The time duration is a function of the design of the TRANSFER CASK and the Advanced NAC-UMS[®] SYSTEM. The elapsed time restrictions on the loaded Advanced CANISTER APPLICABILITY apply during LOADING OPERATIONS from the completion point of the CANISTER vacuum dryness verification through completion of the transfer from the TRANSFER CASK to the CONCRETE CASK. The elapsed time restriction on the loaded Standard CANISTER are provided in LCO 3.1.4.

ACTIONS

A note has been added to the ACTIONS, which states that, for this LCO, separate Condition entry is allowed for each NAC-UMS[®] SYSTEM. This is acceptable, since the Required Actions for each Condition provide appropriate compensatory measures for each NAC-UMS[®] SYSTEM not meeting the LCO. Subsequent NAC-UMS[®] SYSTEMS that do not meet the LCO are governed by subsequent Condition entry and application of associated Required Actions.

<u>A.1.1</u>

If either LCO time limit is exceeded, the TRANSFER CASK containing the loaded Advanced CANISTER backfilled with helium will be returned to the spent fuel pool to allow the cooler spent fuel pool water to reduce the TRANSFER CASK, CANISTER, and spent fuel cladding temperatures to below long-term temperature limits.

<u>AND</u>

<u>A.1.2</u>

The TRANSFER CASK and loaded Advanced CANISTER shall be kept in the spent fuel pool for a minimum of 24 hours prior to restart of LOADING OPERATIONS.

ACTIONS (continued)	<u>A.2.1</u> A cooling airflow of 500 CFM at a maximum temperature of 76°F shall be initiated. The airflow will be routed to the annulus fill/drain lines in the TRANSFER CASK and will flow through the annulus and cool the CANISTER.
	AND
	<u>A.2.2</u> The cooling airflow shall be maintained for a minimum of 24 hours prior to restart of LOADING OPERATIONS.
	OR
	<u>A.2.3</u> A cooling airflow of 500 CFM at a maximum temperature of 76°F shall be maintained while LOADING OPERATIONS continue. However, operations may be ended if required by other considerations. The airflow will be routed to the annulus fill/drain lines of the TRANSFER CASK and will flow through the annulus and cool the CANISTER.
SURVEILLANCE REQUIREMENTS	SR 3.1.9.1
	The elapsed time from completion of CANISTER dryness verification until CANISTER transfer operations into the CONCRETE CASK are completed shall be monitored. The SR ensures that CANISTER material and fuel cladding short-term temperature limits are not exceeded.
	SR 3.1.9.2
·	The elapsed time from the completion of in-pool or forced air cooling until CANISTER transfer operations into the CONCRETE CASK are completed shall be monitored. This SR ensures that CANISTER materials and fuel cladding short-term temperature limits are not exceeded. This SR is also applicable to the maximum time the CANISTER backfilled with helium can be loaded in the TRANSFER CASK if forced air or in-pool cooling operations were performed during vacuum drying operations under LCO 3.1.1.
REFERENCES	1. SAR Sections 4.4 and 8.1.

	Advanced CANISTER Removal from the CONCRETE CASK C 3.1.10
C 3.1 <u>NAC-U</u>	JMS [®] SYSTEM Integrity
C 3.1.10	Advanced CANISTER Removal from the CONCRETE CASK
BASES	
BACKGROUND	A loaded Advanced CANISTER is removed from a CONCRETE CASK using the TRANSFER CASK, so that the CANISTER may be transferred to another CONCRETE CASK or transferred to a TRANSPORT CASK for purposes of transport. The CANISTER is removed from the CONCRETE CASK using the procedure provided in Section 8.2. Once in the TRANSFER CASK, the CANISTER begins to heat up due to the decay heat of the contents and the reduced heat transfer provided by the TRANSFER CASK compared to the CONCRETE CASK.
	The Advanced CANISTER time in the TRANSFER CASK is limited when forced air cooling is not used to ensure that the short-term temperature limits established in the Safety Analysis Report for the spent fuel cladding and CANISTER materials are not exceeded.
	If forced air cooling is maintained, then the CANISTER time in the TRANSFER CASK is not limited, since the short-term temperature limits of the spent fuel cladding and of the CANISTER components are not exceeded.
APPLICABLE SAFETY ANALYSIS	Limiting the total time that a loaded Advanced CANISTER backfilled with helium may be in the TRANSFER CASK, prior to unloading the CANISTER from the TRANSFER CASK, ensures that the short-term temperature limits for the spent fuel cladding and CANISTER materials are not exceeded. Upon placement of the loaded CANISTER in the CONCRETE CASK or TRANSPORT CASK, the temperatures of the CANISTER and stored spent fuel will return to normal storage or transport condition values due to the more efficient passive heat transfer characteristics of the CONCRETE CASK or TRANSPORT CASK.

APPLICABLE SAFETY ANALYSIS (continued)

This ensures that temperatures are maintained below short-term limits for a limited time period. Returning these temperatures to values below long-term limits will prevent damage to the spent fuel cladding and the CANISTER materials.

From calculated temperatures reported in the Safety Analysis Report, it can be concluded that spent fuel cladding and CANISTER material short-term temperature limits will not be exceeded for a total elapsed time of greater than 24 hours for PWR fuel, if the loaded Advanced CANISTER backfilled with helium is in the TRANSFER CASK. If the time limit is met, forced airflow cooling is used to ensure cooling of the CANISTER. The analysis provided in the Safety Analysis Report shows that the spent fuel cladding and CANISTER temperatures will be at or below their long-term limits, as long as the cooling airflow is maintained. This forced airflow provides a similar rate of cooling to that provided by the passive airflow cooling provided by the CONCRETE CASK. Consequently, there is no time limit associated with the continued forced air cooling of the CANISTER while it is in the TRANSFER CASK. The basis for forced air cooling is an inlet maximum air temperature of 76°F, which is the maximum normal ambient air temperature in the thermal analysis. The specified 375 CFM air flow rate exceeds the CONCRETE CASK natural convective cooling flow rate by a minimum of 10 percent. This comparative analysis conservatively excludes the higher flow velocity resulting from the smaller annulus between the TRANSFER CASK and CANISTER, which would result in improved heat transfer from the CANISTER.

If forced air flow is continuously maintained for a period of 24 hours, or longer, then the temperatures of the spent fuel cladding and CANISTER components are at the values calculated for the CONCRETE CASK normal conditions. Consequently, forced air cooling may be ended, allowing a new entry into Condition A. This provides a new minimum 4-hour period in which continuation of the TRANSFER OPERATIONS may occur.

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Advanced CANISTER Removal from the CONCRETE CASK C 3.1.10

Limiting the length of time that the loaded Advanced CANISTER backfilled with helium is allowed to remain in the TRANSFER CASK without forced air cooling ensures that the spent fuel cladding and CANISTER material temperatures remain below the short-term temperature limits established in the SAR for the NAC-UMS[®] SYSTEM. Once forced air cooling is established, the amount of time the CANISTER resides in the TRANSFER CASK is not limited since the cooling provided by the forced air is equivalent to the passive cooling that is provided by the CONCRETE CASK or TRANSPORT CASK.

> If forced air flow is continuously maintained for a period of 24 hours, or longer, then the temperatures of the spent fuel cladding and CANISTER components are at, or below, the values calculated for the CONCRETE CASK normal conditions. Therefore, forced air cooling may be ended, allowing a new entry into Condition A of this LCO. This provides a new minimum 4-hour period in which continuation of TRANSFER OPERATIONS may occur.

APPLICABILITY

LCO

The elapsed time restrictions on the loaded Advanced CANISTER apply during TRANSFER OPERATIONS from the completion point of the closing of the TRANSFER CASK shield doors through completion of the unloading of the CANISTER from the TRANSFER CASK.

The elapsed time restrictions on the loaded Standard CANISTER are provided in LCO 3.1.7.

ACTIONS

A note has been added to the ACTIONS, which states that, for this LCO, separate Condition entry is allowed for each NAC-UMS[®] SYSTEM. This is acceptable, since the Required Actions for each Condition provide appropriate compensatory measures for each NAC-UMS[®] SYSTEM not meeting the LCO. Subsequent NAC-UMS[®] SYSTEMS that do not meet the LCO are governed by subsequent Condition entry and application of associated Required Actions.

Separate Condition A re-entry is also permitted after 24-hours of continuous forced air cooling in accordance with this LCO.

<u>A.1.1</u>

If the CANISTER can be loaded into an operable CONCRETE CASK without the LCO time limit being exceeded, then no further action is required since the spent fuel cladding and CANISTER component short-term temperature limits are not exceeded.

<u>OR</u>

<u>A.2.1</u>

If the CANISTER can be loaded into a TRANSPORT CASK without the LCO time limit being exceeded, then no further action is required since the spent fuel cladding and CANISTER component short-term temperature limits are not exceeded.

<u>OR</u>

<u>A.3.1</u>

If forced air flow is continuously maintained for a period of 24 hours, or longer, then the temperatures of the spent fuel cladding and CANISTER components are at, or below, the values calculated for the CONCRETE CASK normal conditions. Consequently, forced air cooling may be ended, allowing a new entry into Condition A of this LCO, if required by other considerations. This provides a new minimum 4-hour period in which continuation or completion of TRANSFER OPERATIONS may occur.

Advanced CANISTER Removal from the CONCRETE CASK C 3.1.10

ACTIONS (continued) <u>B.1.1</u>

Commence supplying air to the TRANSFER CASK annulus using the fill/drain lines at a rate of 500 CFM and a maximum temperature of 76°F. This action provides the equivalent cooling that would be provided by the passive heat removal systems of the CONCRETE CASK or TRANSPORT CASK in normal operations. Consequently, no short-term spent fuel cladding or CANISTER component temperature limits are exceeded.

<u>AND</u>

<u>B.2.1</u>

Maintain the airflow established by B.1.1 for the time period that the CANISTER remains in the TRANSFER CASK. This action provides the equivalent cooling that would be provided by the passive heat removal systems of the CONCRETE CASK or TRANSPORT CASK in normal operations. Consequently, no short-term spent fuel cladding or CANISTER component temperature limits are exceeded.

SURVEILLANCE REQUIREMENTS SR 3.1.10.1

This SR ensures that the time that the CANISTER is in the TRANSFER CASK does not exceed the 4-hour limit without the use of forced air cooling of the CANISTER. This ensures that the short-term temperature limits of the spent fuel cladding and CANISTER components is not exceeded.

SR 3.1.10.2

This SR ensures that short-term temperature limits of the spent fuel cladding and CANISTER components are not exceeded by initiating and maintaining forced air cooling of the CANISTER in the TRANSFER CASK if the time limits established by Condition A are not met. Forced air cooling is maintained until unloading of the CANISTER from the TRANSFER CASK.

REFERENCES 1. SAR Sections 4.4 and 8.2.

CANISTER Surface Contamination C 3.2.1

C 3.2	NAC-UMS® SYSTEM Radiation Protection
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C 3.2.1 CANISTER Surface Contamination

BASES

BACKGROUND	A TRANSFER CASK containing an empty CANISTER is immersed in the spent fuel pool in order to load the spent fuel assemblies. The
	external surfaces of the CANISTER are maintained clean by the application of clean water to the annulus of the TRANSFER CASK.
	However, there is potential for the surface of the CANISTER to
	become contaminated with the radioactive material in the spent fuel
	pool water. This contamination is removed prior to moving the
	CONCRETE CASK containing the CANISTER to the ISFSI in order to
	minimize the radioactive contamination to personnel or the
	environment. This allows the ISFSI to be entered without additional
	radiological controls to prevent the spread of contamination and
	reduces personnel dose due to the spread of loose contamination or sirbarra contamination. This is consistent with ALARA practices
	andonie containmation. This is consistent with ALANCE practices.

APPLICABLE The radiation protection measures implemented at the ISFSI are based SAFETY ANALYSIS on the assumption that the exterior surfaces of the CANISTER are not contaminated. Failure to decontaminate the surfaces of the CANISTER could lead to higher-than-projected occupational dose and potential site contamination.

The analysis is applicable to both the Standard and Advanced CANISTER, since the two configurations have the same surface area and are loaded and handled in the same manner.

LCO Removable surface contamination on accessible exterior surfaces of the CANISTER and accessible interior surfaces of the TRANSFER CASK are limited to 10,000 dpm/100 cm² from beta and gamma sources and 100 dpm/100 cm² from alpha sources. Only loose contamination is controlled, as fixed contamination will not result from the CANISTER loading process. Experience has shown that these limits are low enough to prevent the spread of contamination to clean areas and are significantly less than the levels, which would cause significant personnel skin dose.

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CANISTER Surface Contamination C 3.2.1

LCO (continued) LCO 3.2.1 requires removable contamination to be within the specified limits for the accessible exterior surfaces of the CANISTER and accessible interior surfaces of the TRANSFER CASK. The location and number of CANISTER and TRANSFER CASK surface swipes used to determine compliance with this LCO are determined based on standard industry practice and the user's plant-specific contamination measurement program for objects of this size. Accessible portions of the CANISTER are the upper portion of the CANISTER external shell wall accessible after draining of the TRANSFER CASK annulus and the top surface of the structural lid. The user shall determine a reasonable number and location of swipes for the accessible portion of the CANISTER. The objective is to determine a removable contamination value representative of the entire upper circumference of the CANISTER and the structural lid, while implementing sound ALARA practices.

> Verification swipes and measurements of removable surface contamination levels on the accessible interior surfaces of the TRANSFER CASK shall be performed following transfer of the CANISTER to the CONCRETE CASK. These measurements will provide indirect evidence that the inaccessible surfaces of the CANISTER do not have removable contamination levels exceeding the limit.

APPLICABILITY Verification that the accessible exterior surface contamination of the Standard or Advanced CANISTER and accessible interior surface contamination of the TRANSFER CASK are less than the LCO limits is performed during LOADING OPERATIONS. This occurs before TRANSPORT OPERATIONS and STORAGE OPERATIONS. Measurement of the CANISTER and TRANSFER CASK surface contamination is unnecessary during UNLOADING OPERATIONS as surface contamination would have been measured prior to moving the subject CANISTER to the ISFSI.

CANISTER Surface Contamination C 3.2.1

ACTIONS

A note has been added to the ACTIONS, which states that, for this LCO, separate Condition entry is allowed for each CANISTER LOADING OPERATION. This is acceptable, since the Required Actions for each Condition provide appropriate compensatory measures for each CANISTER and TRANSFER CASK not meeting the LCO. Subsequent CANISTERs that do not meet the LCO are governed by subsequent Condition entry and application of associated Required Actions.

<u>A.1</u>

If the removable surface contamination of the CANISTER that has been loaded with spent fuel or the TRANSFER CASK is not within the LCO limits, action must be initiated to decontaminate the CANISTER and TRANSFER CASK, and bring the removable surface contamination to within limits. The Completion Time of 7 days is appropriate, given that the time needed to complete the decontamination is indeterminate and surface contamination does not affect the safe storage of the spent fuel assemblies.

SURVEILLANCE REQUIREMENTS

SR 3.2.1.1

This SR verifies that the removable surface contamination on the accessible exterior surfaces of the CANISTER is less than the limits in the LCO. The Surveillance is performed using smear surveys to detect removable surface contamination. The Frequency requires performing the verification prior to initiating TRANSPORT OPERATIONS in order to confirm that the CANISTER can be moved to the ISFSI without spreading loose contamination.

CANISTER Surface Contamination C 3.2.1

SURVEILLANCE REQUIREMENTS (continued)

SR 3.2.1.2

This SR verifies that the removable surface contamination on the accessible interior surfaces of the TRANSFER CASK is less than the limits, thereby providing indirect confirmation that the removable surface contamination on the inaccessible surfaces of the CANISTER are within the limits. It also confirms the proper functioning of the annulus clean water fill system. The Surveillance is performed using smear surveys to detect removable surface contamination. The Frequency requires performing the verification prior to TRANSPORT OPERATIONS, which ensures a potentially contaminated CANISTER is not placed at the ISFSI.

REFERENCES

1. SAR Section 8.1.

CONCRETE CASK Average Surface Dose Rate C 3.2.2

C 3.2 NAC-UMS[®] SYSTEM Radiation Protection

C 3.2.2 CONCRETE CASK Average Surface Dose Rates

- BASES
- BACKGROUND The regulations governing the operation of an ISFSI set limits on the control of occupational radiation exposure and radiation doses to the general public. Occupational radiation exposure should be kept as low as reasonably achievable (ALARA) and within the limits of 10 CFR Part 20. Radiation doses to the public are limited for both normal and accident conditions in accordance with 10 CFR 72.
- APPLICABLE The CONCRETE CASK average surface dose rates are not an SAFETY ANALYSIS assumption in any accident analysis, but are used to ensure compliance with regulatory limits on occupational dose and dose to the public. The analysis is applicable to both the Standard and Advanced CONCRETE CASK, since the two configurations have the same surface dose rate limits.
- LCO The limits on CONCRETE CASK average surface dose rates are based on the Safety Analysis Report shielding analysis of the NAC-UMS[®] SYSTEM. The limits are selected to minimize radiation exposure to the public and to maintain occupational dose ALARA to personnel working in the vicinity of the NAC-UMS[®] SYSTEM. The LCO specifies sufficient locations for taking dose rate measurements to ensure the dose rates measured are indicative of the effectiveness of the shielding materials.
- APPLICABILITY The CONCRETE CASK average surface dose rates apply during STORAGE OPERATIONS. These limits ensure that the CONCRETE CASK average surface dose rates during STORAGE OPERATIONS are bounded by the shielding safety analyses. Radiation doses during STORAGE OPERATIONS are monitored by the NAC-UMS[®] SYSTEM user in accordance with the plant-specific radiation protection program as required by 10 CFR 72.212(b)(6) and 10 CFR 20.

ACTIONS A note has been added to the ACTIONS, which states that, for this LCO, separate Condition entry is allowed for each loaded CONCRETE CASK. This is acceptable, since the Required Actions for each Condition provide appropriate compensatory measures for each CONCRETE CASK not meeting the LCO. Subsequent NAC-UMS[®]

CONCRETE CASK Average Surface Dose Rate C 3.2.2

ACTIONS (continued) SYSTEMs that do not meet the LCO are governed by subsequent Condition entry and application of associated Required Actions.

<u>A.1</u>

If the CONCRETE CASK average surface dose rates are not within limits, it could be an indication that a fuel assembly that did not meet the Approved Contents Limits in Section B2.0 of Appendix 12B was inadvertently loaded into the CANISTER. Administrative verification of the CANISTER fuel loading, by means such as review of video recordings and records of the loaded fuel assembly serial numbers, can establish whether a misloaded fuel assembly is the cause of the out-oflimit condition. The Completion time is based on the time required to perform such a verification.

<u>A.2</u>

If the CONCRETE CASK average surface dose rates are not within limits and it is determined that the CONCRETE CASK was loaded with the correct fuel assemblies, an analysis may be performed. This analysis will determine if the CONCRETE CASK would result in the ISFSI offsite or occupational calculated doses exceeding regulatory limits in 10 CFR Part 72 or 10 CFR Part 20, respectively. If it is determined that the measured average surface dose rates do not result in the regulatory limits being exceeded, STORAGE OPERATIONS may continue.

<u>B.1</u>

If it is verified that the fuel was misloaded, or that the ISFSI offsite radiation protection requirements of 10 CFR Part 20 or 10 CFR Part 72 will not be met with the CONCRETE CASK average surface dose rates above the LCO limit, the fuel assemblies must be placed in a safe condition in the spent fuel pool. The Completion Time is reasonable, based on the time required to transport the CONCRETE CASK, transfer the CANISTER to the TRANSFER CASK, remove the structural lid and vent and drain port cover welds, perform fuel cooldown operations, cut the shield lid weld, move the TRANSFER CASK and CANISTER into the spent fuel pool, remove the shield lid, and remove the spent fuel assemblies in an orderly manner and without challenging personnel.

CONCRETE CASK Average Surface Dose Rate C 3.2.2

SURVEILLALNCE SR 3.2.2.1 REQUIREMENTS

This SR ensures that the CONCRETE CASK average surface dose rates are within the LCO limits after transfer of the CANISTER into the CONCRETE CASK and prior to the beginning of STORAGE OPERATIONS. This Frequency is acceptable as corrective actions can be taken before off-site dose limits are compromised. The surface dose rates are measured approximately at the locations indicated on Figure 12A3-1, following standard industry practices for determining average surface dose rates for large containers.

REFERENCES

1. 10 CFR Parts 20 and 72.

2. SAR Sections 5.1 and 8.2.

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13.0 QUALITY ASSURANCE

13.1 Introduction

The NAC International (NAC) Quality Assurance (QA) Program is designed and administered to meet all Quality Assurance criteria of 10 CFR 72, Subpart G [1], 10 CFR 50, Appendix B [2], 10 CFR 71, Subpart H [3], and NQA-1 (Basic and Supplemental Requirements) [4]. The program is defined in a QA Program description document that has been reviewed and approved by the Nuclear Regulatory Commission (Approval No. 0018).

The NAC Quality Assurance Program is described in a Quality Assurance Manual. This Quality Assurance Manual, as approved by the company's President and Chief Executive Officer, contains policy as to how NAC intends to comply with the applicable regulatory QA criteria. Detailed implementing quality procedures are used to provide the procedural direction to comply with the policy of the QA Manual.

Employing a graded methodology as described in USNRC Regulatory Guide 7.10 [5], NAC applies quality controls to items and activities consistent with their safety significance. Table 13.1-1 identifies the NAC Quality Assurance Manual sections, which address the applicable quality criteria.

A synopsis of the NAC Quality Assurance Program is presented in Section 13.2.

Table 13.1-1 Correlation of Regulatory Quality Assurance Criteria to NAC Quality Assurance Program

	Regulatory Quality Assurance Criteria [*]	Corresponding NAC QA Manual
		Section Number
I.	Organization	1
II.	Quality Assurance Program	2
III.	Design Control	3
IV.	Procurement Document Control	4
V.	Procedures, Instructions, and Drawings	5
VI.	Document Control	6
VII.	Control of Purchased Items and Services	7
VIII.	Identification and Control of Material, Parts and	8
	Components	
IX.	Control of Special Processes	9
Х.	Inspection	10
XI.	Test Control	11
XII.	Control of Measuring and Test Equipment	12
XIII.	Handling, Storage and Shipping	13
XIV.	Inspection, Test and Operating Status	14
XV.	Control of Nonconforming Items	15
XVI.	Corrective Action	16
XVII.	Records	17
XVIII.	Audits	18

^{*}The criteria are obtained from 10 CFR 50 Appendix B; 10 CFR 71 Subpart H; and 10 CFR 72 Subpart G.

13.2 NAC Quality Assurance Program Synopsis

Eighteen applicable Quality Assurance criteria are identified in 10 CFR 72, Subpart G; 10 CFR 50, Appendix B; 10 CFR 71, Subpart H; and ASME NQA-1 (Basic and Supplemental Requirements). NAC compliance with each of these criteria is addressed below.

13.2.1 Organization

The President and Chief Executive Officer of NAC has the ultimate authority and responsibility over all organizations and their functions within the corporation. However, the President delegates and empowers qualified personnel with the authority and responsibility over selected key areas, as identified in the NAC Organization Chart, Figure 13.2-1.

The Vice President, Quality, is responsible for definition, development, implementation and administration of the NAC Quality Assurance Program. The Quality Assurance organization is independent from other organizations within NAC and has complete authority to assure adequate and effective program execution, including problem identification, satisfactory corrective action implementation and the authority to stop work, if necessary. The Vice President, Quality, reports directly to the President and Chief Executive Officer of NAC. The Vice President, Quality, has sufficient expertise in the field of quality to direct the quality function and will be capable of qualifying as a lead auditor.

Strategic Business Unit (SBU) Vice Presidents direct operations, utilizing project teams as appropriate for a particular work scope. SBU Vice Presidents are responsible to the President and Chief Executive Officer for the proper implementation of the NAC Quality Assurance Program.

13.2.2 Quality Assurance Program

NAC has established a Quality Assurance Program that meets the requirements of 10 CFR 72, Subpart G, 10 CFR 50 Appendix B, 10 CFR 71, Subpart H, and NQA-1. Employing a grading methodology consistent with U.S. NRC Regulatory Guide 7.10, the Quality Assurance Program provides control over activities affecting quality from the design to fabrication, operation, and maintenance of nuclear products and services for nuclear applications. The Quality Assurance Program is documented in the Quality Assurance Manual and implemented via Quality Procedures. These Quality Procedures are approved by the Vice President, Quality, and the President and Chief Executive Officer, as well as the Vice President from each SBU performing activities within the scope of the NAC Quality Assurance Manual.

Personnel assigned responsibilities by the Quality Assurance Program may delegate performance of activities associated with that responsibility to other personnel in their group when those individuals are qualified to perform those activities by virtue of their education, experience and training. Such delegations need not be in writing. The person assigned responsibility by the Quality Assurance Program retains full accountability for the activities.

13.2.3 Design Control

The established Quality Procedures covering design control assure that the design activity is planned, controlled, verified and documented so that applicable regulatory and design basis requirements are correctly translated into specifications, drawings, and procedures with appropriate acceptance criteria for inspection and test delineated.

When computer software is utilized to perform engineering calculations, verifications of the computational accuracy are performed, and error tracking of the software is controlled in accordance with approved Quality Procedures.

Design interface control is established and adequate to assure that the review, approval, release, distribution and revision of design documents involving interfaces are performed by appropriately trained, cognizant design personnel using approved procedures.

Design verification is performed by individuals other than those who performed the original design. These verifications may include design reviews, alternate calculations or qualification tests. Selection of the design verification method is based on regulatory, contractual or design complexity requirements. When qualification testing is selected, the "worst case" scenario will be utilized. The verification may be performed by the originator's supervisor, provided the supervisor did not specify a singular design approach, rule out certain design considerations, or establish the design inputs used in the design, unless the supervisor is the only individual in the organization competent to perform the verification. When verification is provided by the supervisor, the need shall be so documented in advance and evaluated after performance by internal audit.

Design changes are controlled and require the same review and approvals as the original design.

13.2.4 Procurement Document Control

Procurement documents and their authorized changes are generated, reviewed and approved in accordance with the Quality Procedures. These procedures assure that all purchased material, components, equipment and services adhere to design specification, regulatory and contractual requirements including Quality Assurance Program and documentation requirements.

NAC Quality Assurance personnel review and approve NAC purchase documents invoking compliance with the Quality Assurance Program for inclusion of appropriate quality-related requirements and compliance with the NAC Quality Assurance Program.

13.2.5 Procedures, Instructions, and Drawings

All activities affecting quality are delineated in the Quality Procedures, Specifications, Inspection/Verification Plans or on appropriate drawings. These documents are developed via approved Quality Procedures and include appropriate quantitative and qualitative acceptance criteria. These documents are reviewed and approved by Quality Assurance personnel prior to use.

13.2.6 Document Control

All documents affecting quality, including revisions thereto, are reviewed and approved by authorized personnel, and are issued and controlled in accordance with Quality Procedures by those persons or groups assigned responsibility for the document to be controlled. Transmittal forms, with provisions for receipt acknowledgment, are utilized and controlled document distribution logs are maintained.

All required support documentation for prescribed activities is available at the work location prior to initiation of the work effort.

13.2.7 <u>Control of Purchased Items and Services</u>

Items and services affecting quality are procured from qualified and approved suppliers. These suppliers have been evaluated and selected in accordance with the Quality Procedures based upon their capability to comply with applicable regulatory and contractual requirements.

Objective evidence attesting to the quality of items and services furnished by NAC suppliers is provided with the delivered item or service, and is based on contract requirements and item or service complexity. This vendor documentation requirement is delineated in the procurement documents.

Source inspection, receipt inspection, vendor audits and vendor surveillance are performed as required to assure product quality, documentation integrity, and supplier compliance to the procurement, regulatory and contractual requirements.

13.2.8 Identification and Control of Material, Parts, and Components

Identification is maintained either on the item or in quality records traceable to the item throughout fabrication and construction to prevent the use of incorrect or defective items.

Identification, in accordance with drawings and inspection plans, is verified by Quality Assurance personnel prior to releasing the item for further processing or delivery.

13.2.9 <u>Control of Special Processes</u>

Special processes, such as welding, heat treating and nondestructive testing, are performed in accordance with applicable codes, standards, specifications and contract requirements by qualified personnel. NAC and NAC suppliers' special process procedures and personnel certifications are reviewed and approved by NAC Quality Assurance prior to their use.

13.2.10 Inspection

NAC has an established and documented inspection program that identifies activities affecting quality and verifies their conformance with documented instructions, plans, procedures and drawings.

Inspections are performed by individuals other than those who performed the activity being inspected. Inspection personnel report directly to the Vice President, Quality.

Process monitoring may also be used in conjunction with identified inspections, if beneficial to achieve required quality.

Mandatory inspection hold points are used to assure verification of critical characteristics. Such hold points are delineated in appropriate process control documents.

13.2.11 <u>Test Control</u>

NAC testing requirements are developed and applied in order to demonstrate satisfactory performance of the tested items to design/contract requirements.

The NAC test program is established to assure that preoperational or operational tests are performed in accordance with written test procedures. Test procedures developed in accordance with approved Quality Procedures identify test prerequisites, test equipment and instrumentation and suitable environmental test conditions. Test procedures are reviewed and approved by NAC Quality Assurance personnel.

Test results are documented, evaluated and accepted by qualified personnel as required by the Quality Assurance inspection instructions prepared for the test, as approved by cognizant quality personnel.

13.2.12 Control of Measuring and Testing Equipment

Control of measuring and testing equipment/instrumentation is established to assure that devices used in activities affecting quality are calibrated and properly adjusted at specified time intervals to maintain their accuracy.

Calibrated equipment is identified and traceable to calibration records, which are maintained. Calibration accuracy is traceable to national standards when such standards exist. The basis of calibration shall always be documented.

Whenever measuring and testing equipment is found to be out of calibration, an evaluation shall be made and documented of the validity of inspection or test results performed and of the acceptability of items inspected or tested since the previous calibration.

13.2.13 <u>Handling, Storage and Shipping</u>

Requirements for handling, storage and shipping are documented in specifications and applicable procedures or instructions. These requirements are designed to prevent damage or deterioration to items and materials.

Information pertaining to shelf life, environment, packaging, temperature, cleaning and preservation are also delineated as required.

Quality Assurance Surveillance/Inspection personnel are responsible for verifying that approved handling, storage, and shipping requirements are met.

13.2.14 Inspection, Test and Operating Status

Procedures are established to indicate the means of identifying inspection and test status on the item and/or on records traceable to the item. These procedures assure identification of items that have satisfactorily passed required inspections and/or tests, to preclude inadvertent bypassing of inspection/test.

Inspection, test, and operating status indicators may only be applied or modified by Quality Assurance personnel or with formal Quality Assurance concurrence.

13.2.15 Control of Nonconforming Items

NAC has established and implemented procedures that assure appropriate identification, segregation, documentation, notification and disposition of items that do not conform to specified requirements. These measures prevent inadvertent usage of the item and assure appropriate authorization or approval of the item's disposition.

All nonconformances are reviewed and accepted, rejected, repaired or reworked in accordance with documented approved procedures. If necessary, a Review Board is convened, consisting of engineering, licensing, quality, operations and testing personnel to provide disposition of nonconforming conditions.

NAC procurement documents provide for control, review and approval of nonconformances noted on NAC items, including associated dispositions.

13.2.16 <u>Corrective Action</u>

Conditions adverse to quality, such as failures, malfunctions, deficiencies, defective material/ equipment, and nonconformances are promptly identified, documented and corrected.

Significant conditions adverse to quality will have their cause determined and sufficient corrective action taken to preclude recurrence. These conditions are documented and reported to the Vice President, Quality, who assures awareness by the President and Chief Executive Officer.

13.2.17 <u>Records</u>

NAC maintains a records system in accordance with approved procedures to assure that documented objective evidence pertaining to quality related activities is identifiable, retrievable and retained to meet regulatory and contract requirements, including retention duration, location and responsibility.

Quality records include, but are not limited to, inspection and test reports, audit reports, quality personnel qualifications, design documents, purchase orders, supplier evaluations, fabrication documents, nonconformance reports, drawings, specifications, etc. Quality Assurance maintains a complete list of records and provides for record storage and disposition to meet regulatory and contractual requirements.

13.2.18 <u>Audits</u>

Approved Quality Procedures provide for a comprehensive system of planned and periodic audits performed by qualified personnel, independent of activities being audited. These audits are performed in accordance with written procedures and are intended to verify program adequacy, effective implementation and compliance, both internally and at Quality Category A (USNRC Regulatory Guide 7.10) [5] approved-supplier locations. Internal audits are conducted annually, and approved suppliers are audited on a triennial basis, as a minimum.





13.3 <u>References</u>

- 1. U.S. Code of Federal Regulations, "Quality Assurance," Part 71, Title 10, Subpart H.
- 2. U.S. Code of Federal Regulations, "Quality Assurance Criteria for Nuclear Power Plants and Fuel Reprocessing Plants," Part 50, Title 10, Appendix B.
- 3. U.S. Code of Federal Regulations, "Quality Assurance Requirements," Part 72, Title 10, Subpart G.
- 4. ASME NQA-1-1994, Part 1, Basic and Supplemental Requirements (as referenced by the ASME Code, including latest accepted addenda), Quality Assurance Program Requirements for Nuclear Facility Applications.
- 5. U.S. Nuclear Regulatory Commission, "Establishing Quality Assurance Program for Packaging Used in the Transport of Radioactive Material," Regulatory Guide 7.10, Revision 1, June 1986.

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