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U. S. Nuclear Regulatory Commission
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South Texas Project
Unit 1
Docket No. STN 50-498
Unit 1 Cycle 11 Core Operating Limits Report

In accordance with Technical Specification 6.9.1.6.d, the attached Core Operating Limits Report is submitted for South Texas Project Unit 1 Cycle 11.

If there are any questions concerning this report, please contact Mr. S. M. Head at (361) 972-7136 or me at (361) 972-7795.


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Attachment: Unit 1 Cycle 11 Core Operating Limits Report

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**SOUTH TEXAS
UNIT 1 CYCLE 11**

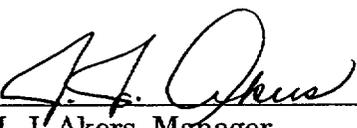
CORE OPERATING LIMITS REPORT

October 2001

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Attachment to CAB-01-289, Rev. 1

1.0 CORE OPERATING LIMITS REPORT

Revision 1 changes to this report are shown in bold and italic font.

This Core Operating Limits Report for STPEGS Unit 1 Cycle 11 has been prepared in accordance with the requirements of Technical Specification 6.9.1.6. The core operating limits have been developed using the NRC-approved methodologies specified in Technical Specification 6.9.1.6.

The Technical Specifications affected by this report are:

- | | | |
|----|-----------|--|
| 1) | 2.1 | SAFETY LIMITS |
| 2) | 2.2 | LIMITING SAFETY SYSTEM SETTINGS |
| 3) | 3/4.1.1.3 | MODERATOR TEMPERATURE COEFFICIENT LIMITS |
| 4) | 3/4.1.3.5 | SHUTDOWN ROD INSERTION LIMITS |
| 5) | 3/4.1.3.6 | CONTROL ROD INSERTION LIMITS |
| 6) | 3/4.2.1 | AFD LIMITS |
| 7) | 3/4.2.2 | HEAT FLUX HOT CHANNEL FACTOR |
| 8) | 3/4.2.3 | NUCLEAR ENTHALPY RISE HOT CHANNEL FACTOR |
| 9) | 3/4.2.5 | DNB PARAMETERS |

2.0 OPERATING LIMITS

The cycle-specific parameter limits for the specifications listed in Section 1.0 are presented below.

2.1 SAFETY LIMITS (Specification 2.1):

- 2.1.1 The combination of THERMAL POWER, pressurizer pressure, and the highest operating loop coolant temperature (T_{avg}) shall not exceed the limits shown in Figure 1.

2.2 LIMITING SAFETY SYSTEM SETTINGS (Specification 2.2):

- 2.2.1 The Loop design flow for Reactor Coolant Flow-Low is 98,000 gpm.
- 2.2.2 The Over-temperature ΔT and Over-power ΔT setpoint parameter values are listed below:

Over-temperature ΔT Setpoint Parameter Values

- τ_1 measured reactor vessel ΔT lead/lag time constant, $\tau_1 = 8$ sec
 τ_2 measured reactor vessel ΔT lead/lag time constant, $\tau_2 = 3$ sec
 τ_3 measured reactor vessel ΔT lag time constant, $\tau_3 = 0$ sec
 τ_4 measured reactor vessel average temperature lead/lag time constant, $\tau_4 = 28$ sec
 τ_5 measured reactor vessel average temperature lead/lag time constant, $\tau_5 = 4$ sec
 τ_6 measured reactor vessel average temperature lag time constant, $\tau_6 = 0$ sec
 K_1 Overtemperature ΔT reactor trip setpoint, $K_1 = 1.14$
 K_2 Overtemperature ΔT reactor trip setpoint T_{avg} coefficient, $K_2 = 0.028/^\circ\text{F}$
 K_3 Overtemperature ΔT reactor trip setpoint pressure coefficient, $K_3 = 0.00143/\text{psig}$
 T' Nominal full power T_{avg} , $T' \leq 592.0$ $^\circ\text{F}$
 P' Nominal RCS pressure, $P' = 2235$ psig
 $f_1(\Delta I)$ is a function of the indicated difference between top and bottom detectors of the power-range neutron ion chambers; with gains to be selected based on measured instrument response during plant startup tests such that;
- (1) For $q_t - q_b$ between -70% and $+8\%$, $f_1(\Delta I) = 0$, where q_t and q_b are percent RATED THERMAL POWER in the top and bottom halves of the core respectively, and $q_t + q_b$ is total THERMAL POWER in percent of RATED THERMAL POWER;
 - (2) For each percent that the magnitude of $q_t - q_b$ exceeds -70% , the ΔT Trip Setpoint shall be automatically reduced by 0.0% of its value at RATED THERMAL POWER.
 - (3) For each percent that the magnitude of $q_t - q_b$ exceeds $+8\%$, the ΔT Trip Setpoint shall be automatically reduced by 2.65% of its value at RATED THERMAL POWER.

Over-power ΔT Setpoint Parameter Values

- τ_1 measured reactor vessel ΔT lead/lag time constant, $\tau_1 = 8$ sec
 τ_2 measured reactor vessel ΔT lead/lag time constant, $\tau_2 = 3$ sec
 τ_3 measured reactor vessel ΔT lag time constant, $\tau_3 = 0$ sec
 τ_6 measured reactor vessel average temperature lag time constant, $\tau_6 = 0$ sec
 τ_7 Time constant utilized in the rate-lag compensator for T_{avg} , $\tau_7 = 10$ sec
 K_4 Overpower ΔT reactor trip setpoint, $K_4 = 1.08$
 K_5 Overpower ΔT reactor trip setpoint T_{avg} rate/lag coefficient, $K_5 = 0.02/^\circ\text{F}$ for increasing average temperature, and $K_5 = 0$ for decreasing average temperature
 K_6 Overpower ΔT reactor trip setpoint T_{avg} heatup coefficient $K_6 = 0.002/^\circ\text{F}$ for $T > T''$ and, $K_6 = 0$ for $T \leq T''$
 T'' Indicated full power T_{avg} , $T'' \leq 592.0$ $^\circ\text{F}$
 $f_2(\Delta I) = 0$ for all (ΔI)

2.3 MODERATOR TEMPERATURE COEFFICIENT (Specification 3.1.1.3):

- 2.3.1 The BOL, ARO, MTC shall be less positive than the limits shown in Figure 2.
 2.3.2 The EOL, ARO, HFP, MTC shall be less negative than $-6.12 \times 10^{-4} \Delta k/k/^\circ F$.
 2.3.3 The 300 ppm, ARO, HFP, MTC shall be less negative than $-5.36 \times 10^{-4} \Delta k/k/^\circ F$ (300 ppm Surveillance Limit).

where: BOL stands for Beginning-of-Cycle Life,
 EOL stands for End-of-Cycle Life,
 ARO stands for All Rods Out,
 HFP stands for Hot Full Power (100% RATED THERMAL POWER)
 HFP vessel average temperature is 592 °F.

2.4 ROD INSERTION LIMITS (Specification 3.1.3.5 and 3.1.3.6):

- 2.4.1 All banks shall have the same Full Out Position (FOP) of at least 250 steps withdrawn but not exceeding 259 steps withdrawn.
 2.4.2 The Control Banks shall be limited in physical insertion as specified in Figure 3.
 2.4.3 Individual Shutdown bank rods are fully withdrawn when the Bank Demand Indication is at the FOP and the Rod Group Height Limiting Condition for Operation is satisfied (T.S. 3.1.3.1).

2.5 AXIAL FLUX DIFFERENCE (Specification 3.2.1):

- 2.5.1 AFD limits as required by Technical Specification 3.2.1 are determined by CAOC Operations with an AFD target band of +5, -10%.
 2.5.2 The AFD shall be maintained within the ACCEPTABLE OPERATION portion of Figure 4, as required by Technical Specifications.

2.6 HEAT FLUX HOT CHANNEL FACTOR (Specification 3.2.2):

- 2.6.1 $F_q^{RTP} = 2.55$.
 2.6.2 $K(Z)$ is provided in Figure 5.
 2.6.3 The F_{xy} limits for RATED THERMAL POWER (F_{xy}^{RTP}) within specific core planes shall be:
 2.6.3.1 Less than or equal to 2.102 for all core planes containing Bank "D" control rods, and
 2.6.3.2 Less than or equal to the appropriate core height-dependent value from Table 1 for all unrodded core planes.
 2.6.3.3 $PF_{xy} = 0.2$.

These F_{xy} limits were used to confirm that the heat flux hot channel factor $F_q(Z)$ will be limited by Technical Specification 3.2.2 assuming the most-limiting axial power distributions expected to result for the insertion and removal of Control Banks C and D during operation, including the accompanying variations in the axial xenon and power distributions, as described in WCAP-8385. Therefore, these F_{xy} limits provide assurance that the initial conditions assumed in the LOCA analysis are met, along with the ECCS acceptance criteria of 10 CFR 50.46.

For Unit 1 Cycle 11, the L(Z) penalty is not applied (i.e., L(Z) = 1.0 for all core elevations).

2.7 ENTHALPY RISE HOT CHANNEL FACTOR (Specification 3.2.3):

2.7.1 WITHOUT RCS Loop-specific Temperature Calibrations:

$$\begin{array}{ll} \textit{Standard Fuel}^1 & F_{\Delta H}^{RTP} = 1.46 \\ \text{VANTAGE 5H / RFA Fuel}^2 & F_{\Delta H}^{RTP} = 1.53 \end{array}$$

WITH RCS Loop-specific Temperature Calibrations:

$$\begin{array}{ll} \textit{Standard Fuel} & F_{\Delta H}^{RTP} = 1.49 \\ \text{VANTAGE 5H / RFA Fuel} & F_{\Delta H}^{RTP} = 1.557 \end{array}$$

$$2.7.2 \textit{ Standard Fuel / VANTAGE 5H / RFA Fuel} \quad PF_{\Delta H} = 0.3$$

2.8 DNB PARAMETERS (Specification 3.2.5):

2.8.1 The following DNB-related parameters shall be maintained within the following limits:³

- a. Reactor Coolant System $T_{avg} \leq 595 \text{ }^\circ\text{F}^4$,
- b. Pressurizer Pressure, $> 2200 \text{ psig}^5$,
- c. Minimum Measured Reactor Coolant System Flow $\geq 403,000 \text{ gpm}^6$.

3.0 REFERENCES

- 3.1 Letter from R. A. Wiley (Westinghouse) to Dave Hoppes (STPNOC), "Unit 1 Cycle 11 Core Operating Limits Report," 01TG-G-085, *Rev. 1* (ST-UB-NOC-01002182, *Rev. 1*), **October 2001**.
- 3.2 NUREG-1346, Technical Specifications, South Texas Project Unit Nos. 1 and 2.
- 3.3 STPNOC Calculation ZC-7035, Rev. 1, "Loop Uncertainty Calculation for RCS T_{avg} Instrumentation," October 19, 1998.
- 3.4 STPNOC Calculation ZC-7032, Rev. 3, "Loop Uncertainty Calculation for Narrow Range Pressurizer Pressure Monitoring Instrumentation," June 27, 2001.

¹ *Applies to Region 5.*

² *Applies to Regions 10A, 11A, 11B, 12A, 13A and 13B.*

³ A discussion of the processes to be used to take these readings is provided in the basis for Technical Specification 3.2.5.

⁴ Includes a 1.9 °F measurement uncertainty.

⁵ Limit not applicable during either a Thermal Power ramp in excess of 5% of RTP per minute or a Thermal Power step in excess of 10% RTP. Includes a 10.7 psi measurement uncertainty as read on the QDPS display per Reference 3.4.

⁶ Includes a 2.8% flow measurement uncertainty.

Figure 1

Reactor Core Safety Limits - Four Loops in Operation

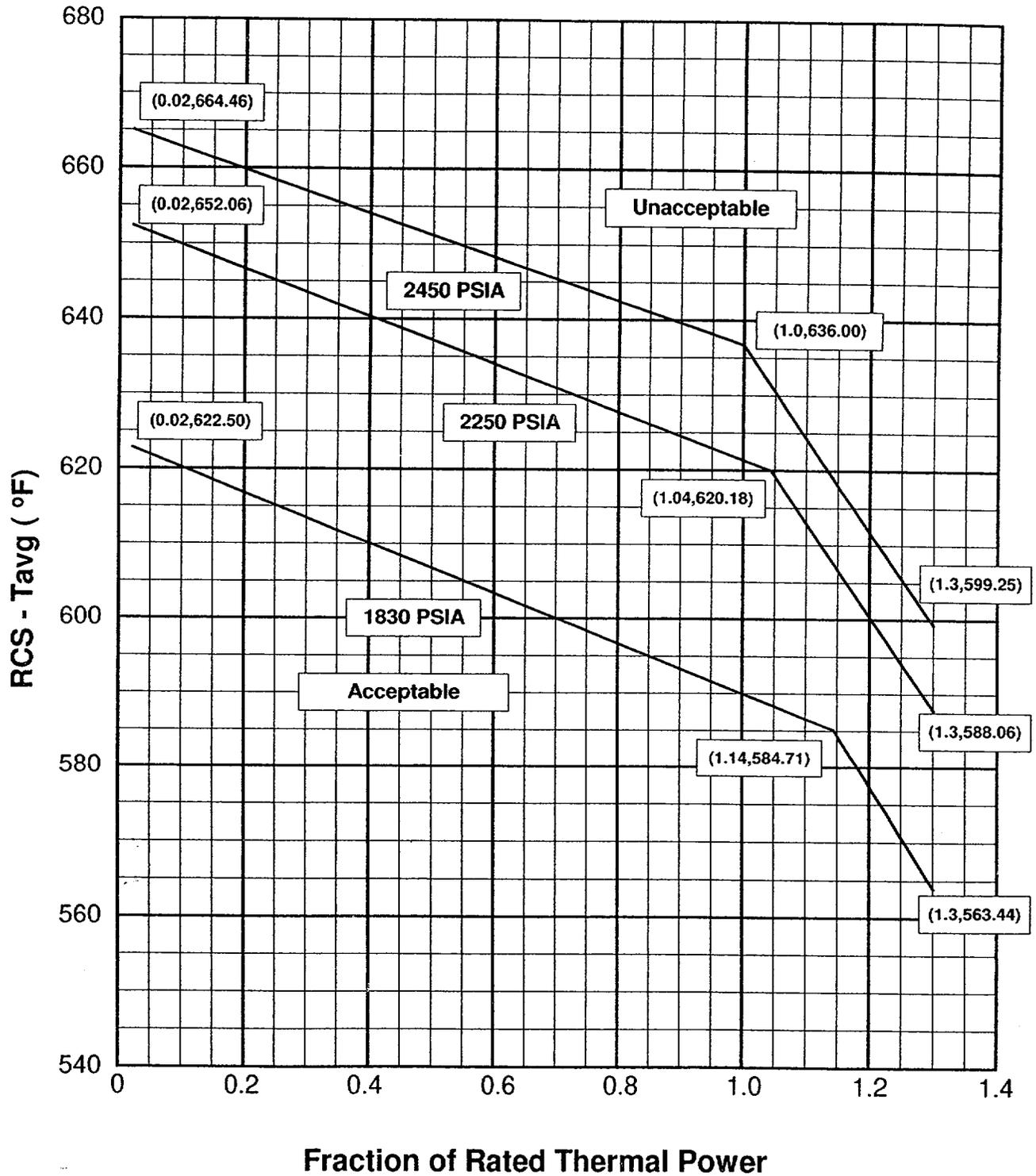


Figure 2
MTC versus Power Level

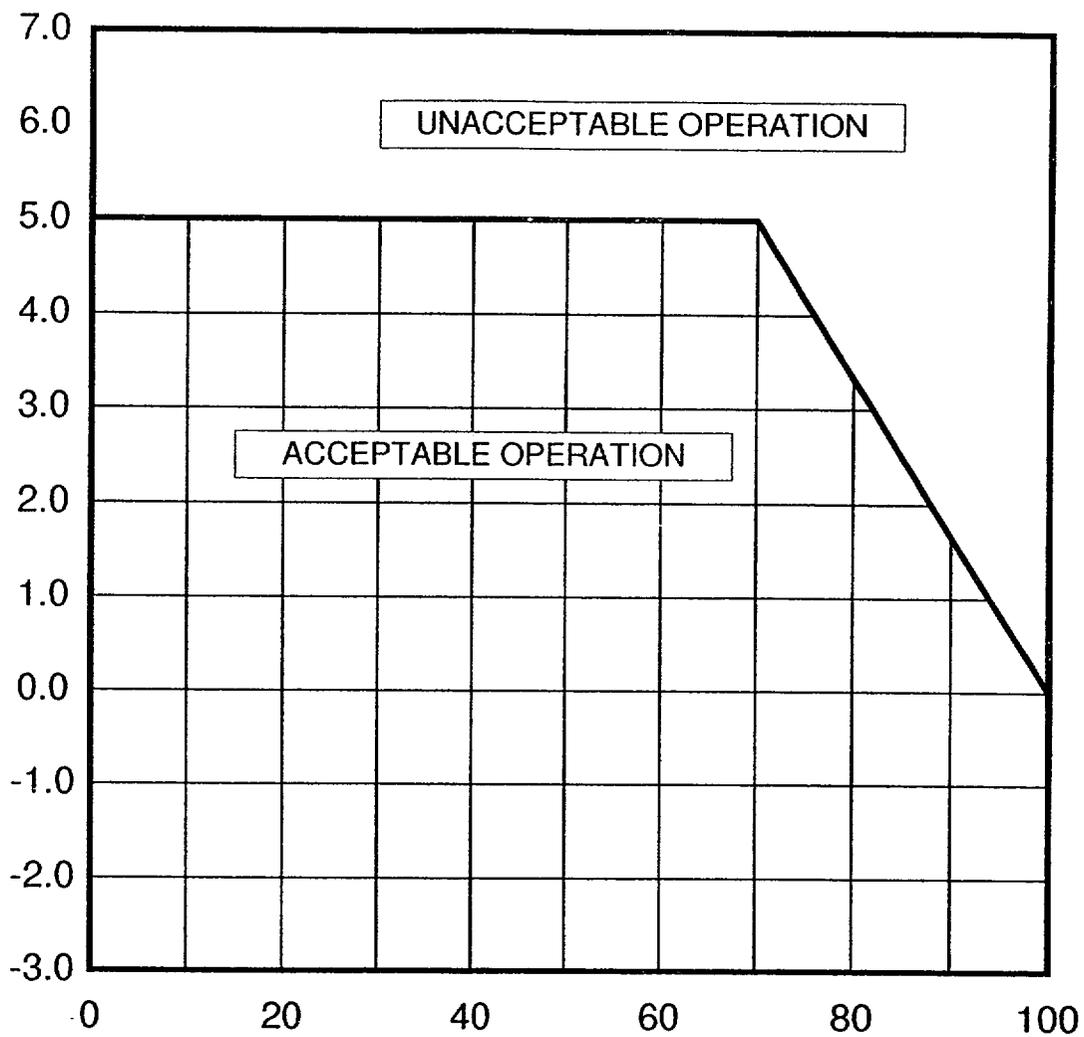


Figure 3

Control Rod Insertion Limits versus Power Level

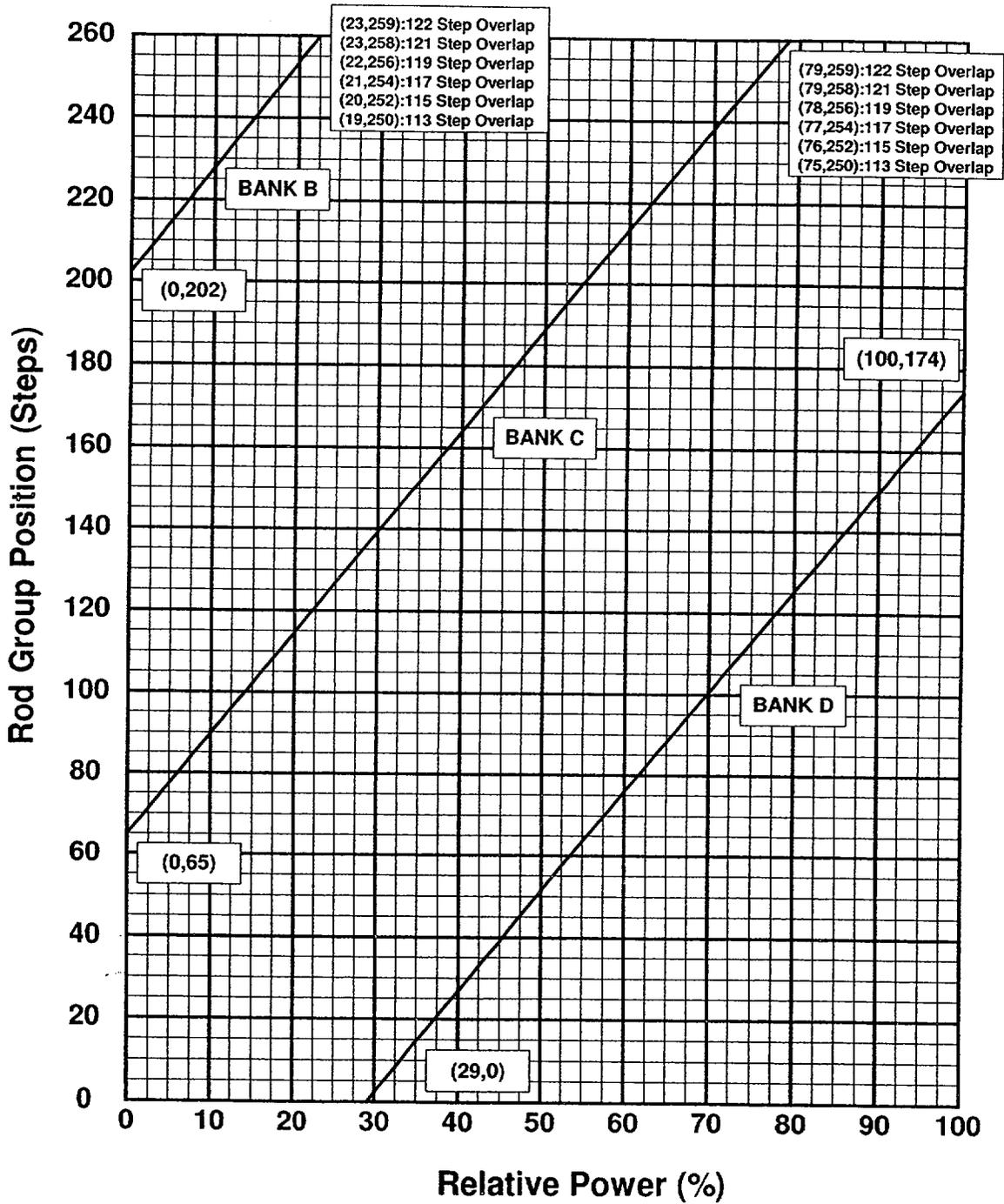


Figure 4

AFD Limits versus Rated Thermal Power

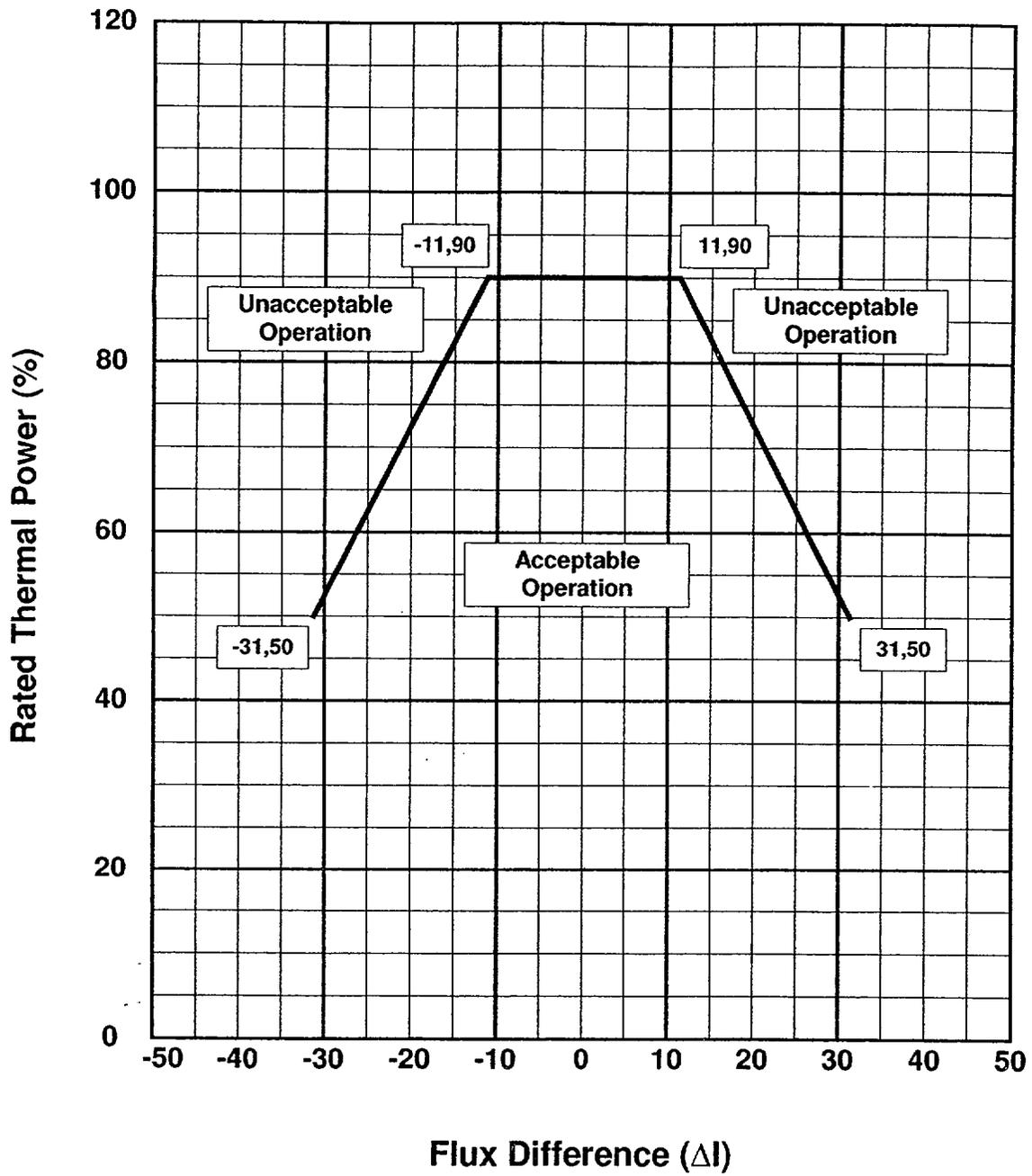


Figure 5

K(Z) - Normalized $F_q(Z)$ versus Core Height

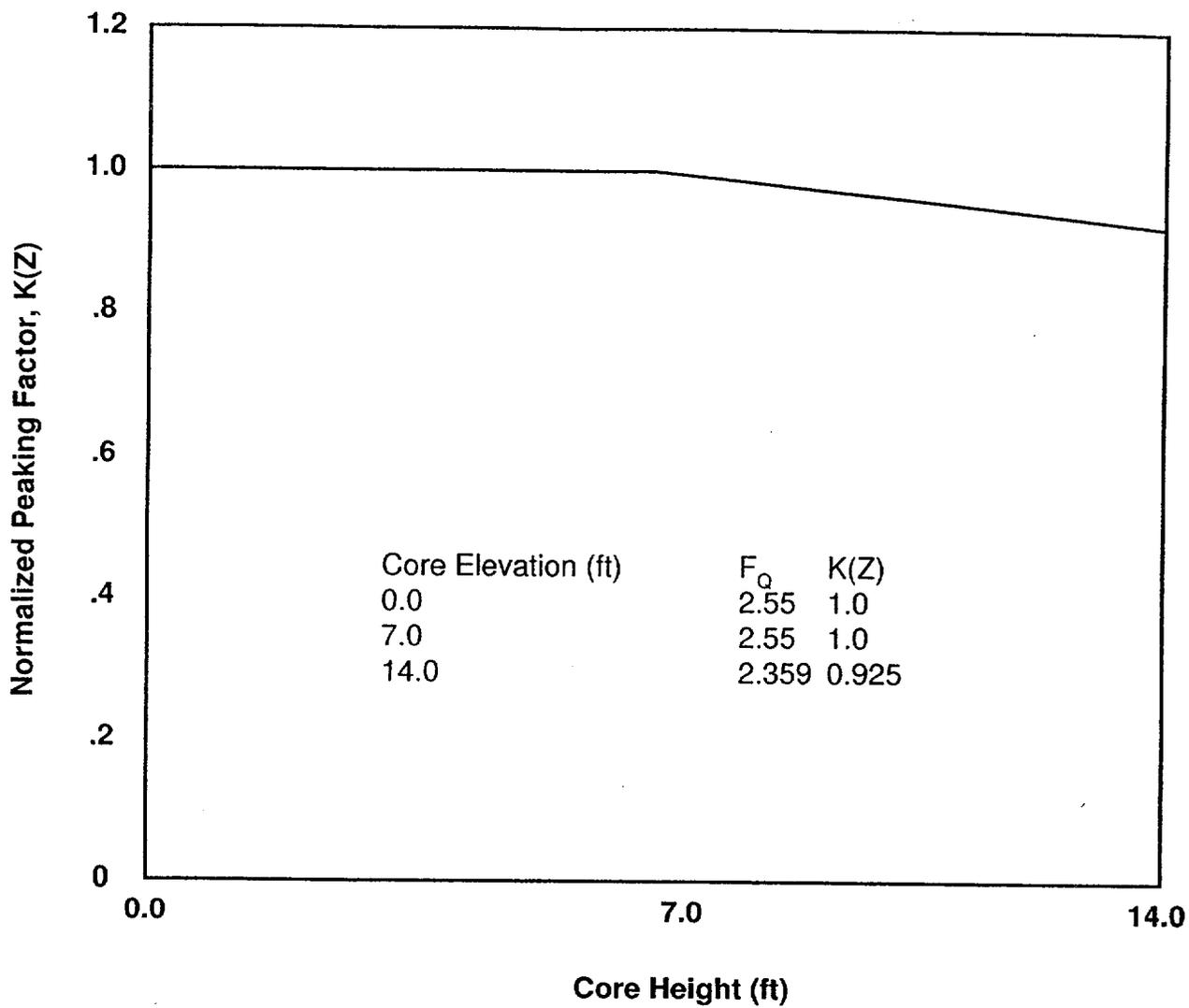


Table 1

Unrodded F_{xy} for Each Core Height*
For Cycle Burnups Less Than 9000 MWD/MTU

Core Height (Ft.)	Unrodded F_{xy}	Core Height (Ft.)	Unrodded F_{xy}
14.00	5.123	6.80	1.948
13.80	4.303	6.60	1.932
13.60	3.482	6.40	1.920
13.40	2.661	6.20	1.909
13.20	2.291	6.00	1.898
13.00	2.061	5.80	1.894
12.80	2.096	5.60	1.895
12.60	2.092	5.40	1.894
12.40	2.082	5.20	1.896
12.20	2.057	5.00	1.900
12.00	2.027	4.80	1.907
11.80	2.007	4.60	1.916
11.60	2.002	4.40	1.924
11.40	2.002	4.20	1.929
11.20	2.001	4.00	1.933
11.00	1.999	3.80	1.933
10.80	1.994	3.60	1.926
10.60	1.990	3.40	1.922
10.40	1.986	3.20	1.915
10.20	1.985	3.00	1.901
10.00	1.985	2.80	1.886
9.80	1.986	2.60	1.854
9.60	1.988	2.40	1.816
9.40	1.989	2.20	1.774
9.20	1.990	2.00	1.755
9.00	1.991	1.80	1.744
8.80	1.994	1.60	1.740
8.60	1.999	1.40	1.735
8.40	2.007	1.20	1.744
8.20	2.016	1.00	1.780
8.00	2.024	0.80	1.933
7.80	2.032	0.60	2.351
7.60	2.030	0.40	2.901
7.40	2.006	0.20	3.451
7.20	1.980	0.00	4.001
7.0	1.962		

* For Unit 1 Cycle 11, the L(Z) penalty is not applied (i.e., $L(Z) = 1.0$ for all core elevations).

Table 2

**Unrodded F_{xy} for Each Core Height*
For Cycle Burnups Greater Than or Equal to 9000 MWD/MTU**

Core Height (Ft.)	Unrodded F_{xy}	Core Height (Ft.)	Unrodded F_{xy}
14.00	5.186	6.80	2.125
13.80	4.443	6.60	2.122
13.60	3.665	6.40	2.112
13.40	2.858	6.20	2.101
13.20	2.456	6.00	2.088
13.00	2.180	5.80	2.075
12.80	2.153	5.60	2.063
12.60	2.109	5.40	2.051
12.40	2.082	5.20	2.041
12.20	2.072	5.00	2.031
12.00	2.053	4.80	2.023
11.80	2.035	4.60	2.016
11.60	2.031	4.40	2.006
11.40	2.034	4.20	1.995
11.20	2.036	4.00	1.982
11.00	2.038	3.80	1.970
10.80	2.039	3.60	1.958
10.60	2.040	3.40	1.947
10.40	2.040	3.20	1.936
10.20	2.038	3.00	1.924
10.00	2.037	2.80	1.911
9.80	2.036	2.60	1.879
9.60	2.039	2.40	1.852
9.40	2.045	2.20	1.841
9.20	2.053	2.00	1.831
9.00	2.057	1.80	1.820
8.80	2.059	1.60	1.813
8.60	2.060	1.40	1.827
8.40	2.065	1.20	1.815
8.20	2.074	1.00	1.822
8.00	2.085	0.80	2.066
7.80	2.096	0.60	2.542
7.60	2.105	0.40	3.117
7.40	2.114	0.20	3.656
7.20	2.121	0.00	4.121
7.00	2.125		

* For Unit 1 Cycle 11, the L(Z) penalty is not applied (i.e., L(Z) = 1.0 for all core elevations).