Docket Nos. 50-259/260/296

Mr. Hugh G. Parris Manager of Power Tennessee Valley Authority 500A Chestnut Street, Tower II Chattanooga, Tennessee 37401

Dear Mr. Parris:

On August 17, 1984, we issued Amendment No. 77, to Facility Operating License No. DPR-68 in response to your application of September 21, 1981 (TVA BFNP TS 167). There were errors on page 22 of that amendment. A corrected page 22 is enclosed. The effect of this correction is to restore Amendment 70 changes which were inadvertently not carried-over to Amendment 77.

Sincerely,

Original signed by: Richard J. Clark, Project Manager Operating Reactors Branch #2 Division of Licensing

Enclosures: As stated

cc w/enclosures:
See next page

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Mr. Hugh G. Parris Tennessee Valley Authority Browns Ferry Nuclear Plant, Units 1, 2 and 3

cc:

H. S. Sanger, Jr., Esquire General Counsel Tennessee Valley Authority 400 Commerce Avenue E 11B 330 Knoxville, Tennessee 37902

Mr. Ron Rogers Tennessee Valley Authority 400 Chestnut Street, Tower II Chattanooga, Tennessee 37401

Mr. Charles R. Christopher Chairman, Limestone County Commission Post Office Box 188 Athens, Alabama 35611

Ira L. Meyers, M.D. State Health Officer State Department of Public Health State Office Building Montgomery, Alabama 36130

Mr. H. N. Culver 249A HBD 400 Commerce Avenue Tennessee Valley Authority Knoxville, Tennessee 37902

James P. O'Reilly Regional Administrator Region II Office U. S. Nuclear Regulatory Commission 101 Marietta Street, Suite 3100 Atlanta, Georgia 30303 U. S. Environmental Protection Agency Region IV Office Regional Radiation Representative 345 Courtland Street, N. W. Atlanta, Georgia 30308

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Mr. Donald L. Williams, Jr. Tennessee Valley Authority 400 West Summit Hill Drive, W10B85 Knoxville, Tennessee 37902

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Mr. Oliver Havens U. S. Nuclear Regulatory Commission Reactor Training Center Osborne Office Center, Suite 200 Chattanooga, Tennessee 37411

James A. Coffey Site Director, BFNP Tennessee Valley Authority Post Office Box 2000 Decatur, Alabama 35602 a given point at constant recirculation flow rate, and thus to protect against the condition of a MCPR less than 1.07. This rod block trip setting, which is automatically varied with recirculation loop flow rate, prevents an increase in the reactor power level to excess values due to control rod The flow variable trip setting provides withdrawal. substantial margin from fuel damage, assuming a steady-state operation at the trip setting, over the entire recirculation The margin to the Safety Limit increases as the flow range. flow decreases for the specified trip setting versus flow relationship; therefore, the worst case MCPR which could occur during the steady-state operation is at 108% of rated thermal power because of the APRM rod block trip setting. The actual power distribution in the core is established by specified control rod sequences and is monitored continuously by the in-core LPRM system.

C. <u>Reactor Water Low Level Scram and Isolation</u> (Except Main Sceamlines)

The set point for the low level scram is above the bottom of the separator skirt. This level has been used in transient analyses dealing with coolant inventory decrease. The results reported in FSAR subsection 14.5 show that scram and isolation of all process lines (except main steam) at this level adequately protects the fuel and the pressure barrier, because MCPR is greater than 1.07 in all cases, and system pressure does not reach the safety valve settings. The scram setting is approximately 31 inches below the normal operating range and is thus adequate to avoid spurious scrams.

D. Turbine Stop Valve Closure Scram

The turbine stop valve closure trip anticipates the pressure- neutron flux and heat flux increases that would result from closure of the stop valves. With a trip setting of 10% of valve closure from full open, the resultant increase in heat flux is such that adequate thermal margins are maintained even during the worst case transient that assumes the turbine bypass valves remain closed. (Reference 2).

. Turbine Control Valve Fast Closure or Turbine Trip Scram

Turbine control valve fast closure or turbine trip scram anticipates the pressure, neutron flux, and heat flux increase that could repult from control valve fast closure due to load rejection or control valve closure due to turbine trip; each without bypass valve capability. The reactor protection system initiates a scram in less than 30 milliseconds after the start of control valve fast closure due to load rejection or control valve closure due to turbine trip. This scram is achieved by rapidly reducing hydraulic control

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Amendment No. 9, 78, 56, 70, 77

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