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MAR 8 1984

Docket Nos. 50-348
and 50-364

Mr. F. L. Clayton
Senior Vice President
Alabama Power Company
Post Office Box 2641
Birmingham, Alabama 35291

Dear Mr. Clayton:

The Commission issued Amendment Nos. 37 and 27 to Facility Operating License Nos. NPF-2 and NPF-8 for the Joseph M. Farley Nuclear Plant Units 1 and 2 on December 30, 1983. Upon review of the issued amendments your staff noted two typographical errors made in your October 13, 1983 application. These errors are unrelated to the approved changes in the amendments.

On that basis, you requested reissuance of the two corrected pages for both units. You also requested our action as soon as possible to support the Unit 1 startup from the current refueling outage. Enclosed are corrected Technical Specification pages 3/4 2-8 and 3/4 2-9 which you should use to replace the pages issued on December 30, 1983. The pages are identified as "corrected page," Amendment No. 37 and No. 27, as appropriate.

Sincerely,

/s/ Edward A. Reeves

Edward A. Reeves, Project Manager
Operating Reactors Branch No. 1
Division of Licensing

Enclosure:
As stated

cc w/enclosure:
See attached list

ORB #1	ORB #1
EReeves/jm	S Varga
3/8 /84	3/8 /84

8403260326 840308
PDR ADOCK 05000348
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TABLE 2.2-1 (Continued)

REACTOR TRIP SYSTEM INSTRUMENTATION TRIP SETPOINTS

NOTATION

NOTE 1: Overtemperature $\Delta T \leq \Delta T_o[K_1-K_2 \frac{1+\tau_1 S}{1+\tau_2 S} (T-T')+K_3(P-P') -f_1 (\Delta I)]$

where: ΔT_o = Indicated ΔT at RATED THERMAL POWER

T = Average temperature, °F

T' $\leq$ 577.2°F (Maximum Reference T_{avg} at RATED THERMAL POWER)

P = Pressurizer pressure, psig

P' = 2235 psig (Nominal RCS operating pressure)

$\frac{1+\tau_1 S}{1+\tau_2 S}$ = The function generated by the lead-lag controller for T_{avg} dynamic compensation

$\tau 1$ & $\tau 2$ = Time constants utilized in the lead-lag controller for T_{avg} $\tau 1$ = 30 secs, $\tau 2$ = 4 secs.

S = Laplace transform operator, sec^{-1}.

Operation with 3 Loops	Operation with 2 Loops
K_1 = 1.22	K_1 = (values blank pending
K_2 = 0.0154	K_2 = NRC approval of
K_3 = 0.000635	K_3 = 2 loop operation)

and f_1 (ΔI) is a function of the indicated difference between top and bottom detectors of the power-range nuclear ion chambers; with gains to be selected based on measured instrument response during plant startup tests such that:

AMENDMENT NO. 37
CORRECTED PAGE

8403260329 840308
PDR ADOCK 05000348
P PDR

REACTOR TRIP SYSTEM INSTRUMENTATION TRIP SETPOINTS

NOTATION continued

(i) for $q_t = q_b$ between -35 percent and +9 percent, $f_1 (\Delta I) = 0$ (where q_t and q_b are percent RATED THERMAL POWER in the top and bottom halves of the core respectively, and $q_t = q_b$ is total THERMAL POWER in percent of RATED THERMAL POWER).

(ii) for each percent that the magnitude of $(q_t - q_b)$ exceeds -35 percent, the ΔT trip setpoint shall be automatically reduced by 1.37 percent of its value at RATED THERMAL POWER.

(iii) for each percent that the magnitude of $(q_t - q_b)$ exceeds +9 percent, the ΔT trip setpoint shall be automatically reduced by 1.60 percent of its value at RATED THERMAL POWER.

Note 2: Overpower $\Delta T \leq \Delta T_o [K_4 - K_5 \frac{\tau 3 S}{1+\tau_3 S} - K_6(T-T") - f_2 (\Delta I)]$

where:

ΔT_o = Indicated ΔT at RATED THERMAL POWER

T = Average temperature, °F

$T"$ = Reference T_{avg} at RATED THERMAL POWER (Calibration temperature for ΔT instrumentation, $\leq$ 577.2°F)

K_4 = 1.08

K_5 = 0.02/°F for increasing average temperature and 0 for decreasing average temperature

K_6 = 0.00109/°F for $T > T"$; $K_6 = 0$ for $T \leq T"$

$\frac{\tau 3 S}{1+\tau_3 S}$ = The function generated by the rate lag controller for T_{avg} dynamic compensation

TABLE 2.2-1 (Continued)

REACTOR TRIP SYSTEM INSTRUMENTATION TRIP SETPOINTS

NOTATION

NOTE 1: Overtemperature $\Delta T \leq \Delta T_o[K_1 - K_2 \frac{1+\tau_1 S}{1+\tau_2 S}(T-T') + K_3(P-P') - f_1(\Delta I)]$

where: ΔT_o = Indicated ΔT at RATED THERMAL POWER

T = Average temperature, °F

$T' \leq$ 577.2°F (Maximum Reference T_{avg} at RATED THERMAL POWER)

P = Pressurizer pressure, psig

P' = 2235 psig (Nominal RCS operating pressure)

$\frac{1+\tau_1 S}{1+\tau_2 S}$ = The function generated by the lead-lag controller for T_{avg} dynamic compensation

$\tau 1$ & $\tau 2$ = Time constants utilized in the lead-lag controller for T_{avg} $\tau 1$ = 30 secs, $\tau 2$ = 4 secs.

S = Laplace transform operator, sec^{-1}.

Operation with 3 Loops	Operation with 2 Loops
K_1 = 1.22	K_1 = (values blank pending
K_2 = 0.0154	K_2 = NRC approval of
K_3 = 0.000635	K_3 = 2 loop operation)

and $f_1(\Delta I)$ is a function of the indicated difference between top and bottom detectors of the power-range nuclear ion chambers; with gains to be selected based on measured instrument response during plant startup tests such that:

AMENDMENT NO. 27
CORRECTED PAGE

NOTATION continued

(i) for $q_t = q_b$ between -35 percent and +9 percent, $f_1(\Delta I) = 0$ (where q_t and q_b are percent RATED THERMAL POWER in the top and bottom halves of the core respectively, and $q_t = q_b$ is total THERMAL POWER in percent of RATED THERMAL POWER).

(ii) for each percent that the magnitude of $(q_t - q_b)$ exceeds -35 percent, the ΔT trip setpoint shall be automatically reduced by 1.37 percent of its value at RATED THERMAL POWER.

(iii) for each percent that the magnitude of $(q_t - q_b)$ exceeds +9 percent, the ΔT trip setpoint shall be automatically reduced by 1.60 percent of its value at RATED THERMAL POWER.

Note 2: Overpower $\Delta T \leq \Delta T_o \left[K_4 - K_5 \frac{\tau 3 S}{1+\tau_3 S} - K_6(T-T") - f_2(\Delta I)\right]$

where:

ΔT_o = Indicated ΔT at RATED THERMAL POWER

T = Average temperature, °F

$T"$ = Reference T_{avg} at RATED THERMAL POWER (Calibration temperature for ΔT instrumentation, $\leq$ 577.2°F)

K_4 = 1.08

K_5 = 0.02/°F for increasing average temperature and 0 for decreasing average temperature

K_6 = 0.00109/°F for $T > T"$; $K_6 = 0$ for $T \leq T"$

$\frac{\tau 3 S}{1+\tau_3 S}$ = The function generated by the rate lag controller for T_{avg} dynamic compensation