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October 2, 2001
BW010102

U.S. Nuclear Regulatory Commission
ATTN: Document Control Desk
Washington, DC 20555-0001

Braidwood Station, Unit 1
Facility Operating License No. NPF-72
NRC Docket No. STN 50-456

Subject: Core Operating Limits Report, Braidwood Unit 1 Cycle 10 Sequence Number 3

The purpose of this letter is to transmit the Core Operating Limits Report (COLR) for Braidwood Unit 1 Cycle 10 Sequence Number 3, in accordance with Technical Specification 5.6.5, "Core Operating Limits Report (COLR)." This revision of the COLR was recently implemented in support of a reload cycle.

If you have any questions regarding this matter, please contact Ms. A. Ferko, Regulatory Assurance Manager at (815) 417-2699.

Respectfully,

James D. von Suskil
Site Vice President
Braidwood Station

Attachment: Core Operating Limits Report, Braidwood Unit 1 Cycle 10 Sequence Number 3

cc: Regional Administrator – NRC Region III
NRC Senior Resident Inspector – Braidwood Station

A001

bcc: Braidwood Station Project Manager, NRR - NRC
Nicholas Reynolds – Winston & Strawn
Office of Nuclear Facility Safety – Illinois of Department of Nuclear Safety
Vice President – Licensing and Regulatory Affairs
Regulatory Assurance Manager - Braidwood Station
Director, Licensing – MidWest Regional Operating Group
Manager, Licensing – Braidwood and Byron Stations
Braidwood Nuclear Licensing Administrator
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ATTACHMENT 1

Core Operating Limits Report

Braidwood Unit 1, Cycle 10, Sequence Number 3

NUCLEAR FUEL MANAGEMENT DEPARTMENT
TRANSMITTAL OF DESIGN INFORMATION

☒ SAFETY RELATED ☐ NON-SAFETY RELATED ☐ REGULATORY RELATED	Originating Organization ☒ Nuclear Fuel Management ☐ Other (specify) _____	TODI No. NFM0100083 Seq. No. 3 Page 1 of 17

Station Braidwood Unit 1 Cycle 10 Generic _____

To: Lonnie K. Kepley - Braidwood

Subject Braidwood Unit 1 Cycle 10 Core Operating Limits Report in ITS Format and W(z) Function

P. Moravek Preparer	Preparer's Signature	9/26/01 Date
T. Stevens Reviewer	Reviewer's Signature	9/26/01 Date
D. Redden NFM Supervisor	NFM Supervisor's Signature	9/26/01 Date

Status of Information:
☒ Verified
☐ Unverified
☐ Engineering Judgement

Method and Schedule of Verification for Unverified TODIs: _____

Description of Information:

Attached is the Braidwood Unit 1 Cycle 10 Core Operating Limits Report (COLR) in the ITS format and W(z) function. **The Sequence 3 of this TODI supersedes Sequence 2.**

Purpose of Information:

The attached Core Operating Limits Report (COLR) for Braidwood Station Unit 1 Cycle 10 has been prepared in accordance with the requirements of Technical Specification 5.6.5 (ITS). In this sequence, the description of LCO 3.4.1 was corrected in the COLR Sections 1.0 and 2.12. Braidwood Station is requested to perform a plant review of this document. Upon completion of the plant review, Braidwood Station is to transmit the COLR portion to the Nuclear Regulatory Commission pursuant to Technical Specification 5.6.5. Please provide NFM (Tyrone L. Stevens) with a copy of Braidwood Station's completed plant review and COLR submittal to the NRC.

Source of Information:

1. Westinghouse Letter 01-CB-G-151, "Braidwood Unit 1 Cycle 10 COLR Data", dated August 28, 2001.
2. Westinghouse Letter 01-CB-G-153, "Braidwood Unit 1 Cycle 10 COLR Revision 1", dated August 31, 2001.
3. TODI NFM0100062, Revision 1, "BR1C10 Reload Design Initiation", dated June 12, 2001.
4. NFS Calcnote PNDCN:00-003, Rev.0, "Evaluation of SPIL Using 224 Steps Rod Withdrawn as Definition of ARO"; dated May 11, 2000.
5. Westinghouse Letter 01-CB-G-132, "Braidwood 1 Cycle 10 BEACON DMM Model Delivery", dated July 27 2001.
6. Westinghouse Letter 01-CB-G-155, "Braidwood Unit 1 Cycle 10 Boron Concentration for Startup Physics Testing", dated September 7, 2001.

Supplemental Distribution: A. Ferko / L. S. Dworakowski (BR)

1.0 CORE OPERATING LIMITS REPORT

This Core Operating Limits Report (COLR) for Braidwood Station Unit 1 Cycle 10 has been prepared in accordance with the requirements of Technical Specification 5.6.5 (ITS).

The Technical Specifications affected by this report are listed below:

SL	2.1.1	Reactor Core Safety Limits (SLs)
LCO	3.1.1	SHUTDOWN MARGIN (SDM)
LCO	3.1.3	Moderator Temperature Coefficient (MTC)
LCO	3.1.4	Rod Group Alignment Limits
LCO	3.1.5	Shutdown Bank Insertion Limits
LCO	3.1.6	Control Bank Insertion Limits
LCO	3.1.8	PHYSICS TESTS Exceptions – MODE 2
LCO	3.2.1	Heat Flux Hot Channel Factor ($F_Q(Z)$)
LCO	3.2.2	Nuclear Enthalpy Rise Hot Channel Factor ($F^N_{\Delta H}$)
LCO	3.2.3	AXIAL FLUX DIFFERENCE (AFD)
LCO	3.2.5	Departure from Nucleate Boiling Ratio (DNBR)
LCO	3.3.1	Reactor Trip System (RTS) Instrumentation
LCO	3.3.9	Boron Dilution Protection System (BDPS)
LCO	3.4.1	Reactor Coolant System (RCS) Pressure, Temperature, and Flow Departure from Nucleate Boiling (DNB) Limits
LCO	3.9.1	Boron Concentration

The portions of the Technical Requirements Manual affected by this report are listed below:

TRM TLCO 3.1.b	Boration Flow Paths - Operating
TRM TLCO 3.1.d	Charging Pumps - Operating
TRM TLCO 3.1.f	Borated Water Sources - Operating
TRM TLCO 3.1.g	Position Indication System – Shutdown
TRM TLCO 3.1.h	Shutdown Margin (SDM) – MODE 1 and MODE 2 with keff ≥ 1.0
TRM TLCO 3.1.i	Shutdown Margin (SDM) – MODE 5
TRM TLCO 3.1.j	Shutdown and Control Rods
TRM TLCO 3.1.k	Position Indication System – Shutdown (Special Test Exception)

2.0 OPERATING LIMITS

The cycle-specific parameter limits for the specifications listed in Section 1.0 are presented in the following subsections. These limits are applicable for the entire cycle unless otherwise identified. These limits have been developed using the NRC-approved methodologies specified in Technical Specification 5.6.5.

2.1 Reactor Core Safety Limits (SLs) (SL 2.1.1)

2.1.1 In Modes 1 and 2, the combination of Thermal Power, Reactor Coolant System (RCS) highest loop average temperature, and pressurizer pressure shall not exceed the limits specified in Figure 2.1.1.

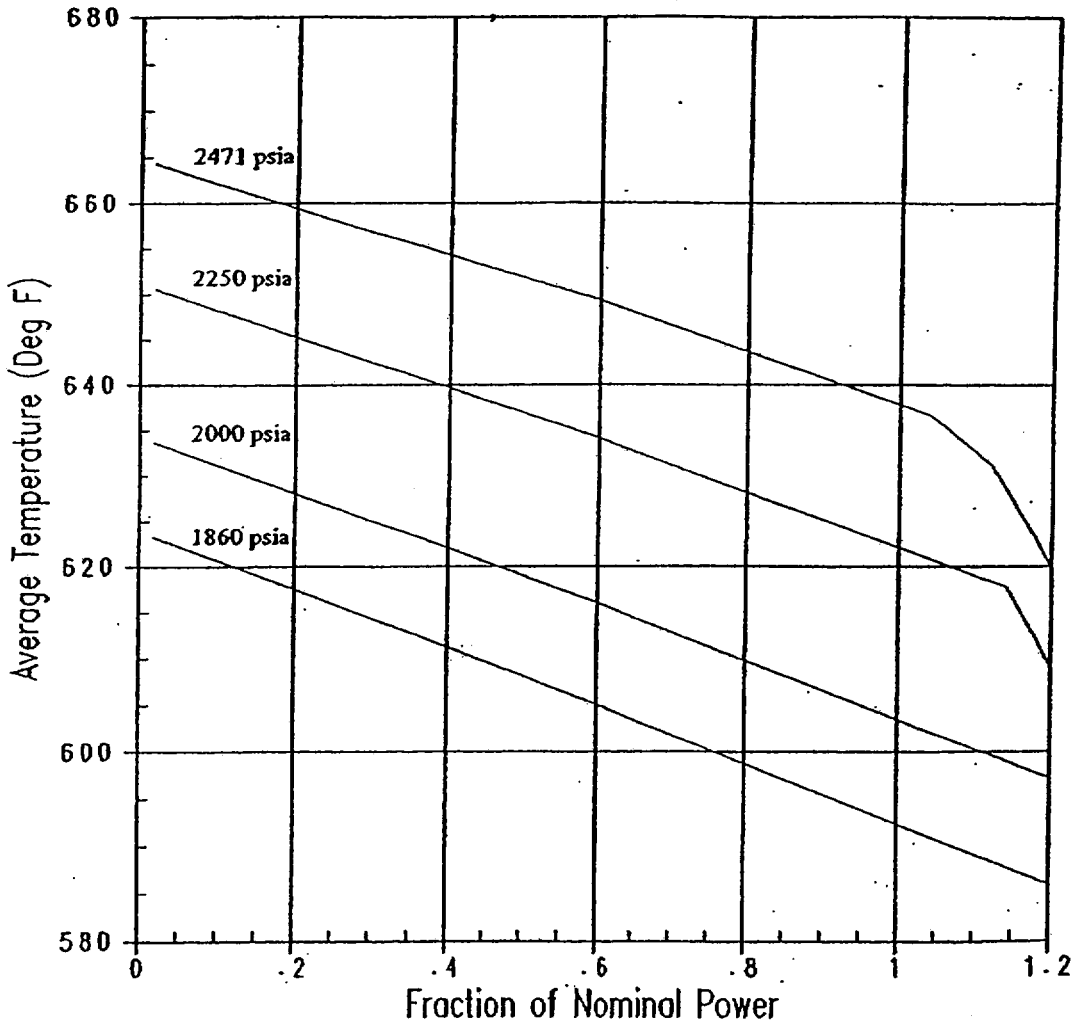


Figure 2.1.1: Reactor Core Limits

2.2 SHUTDOWN MARGIN (SDM)

The SDM limit for MODES 1, 2, 3, and 4 is:

2.2.1 The SDM shall be greater than or equal to 1.3% Δk/k (LCOs 3.1.1, 3.1.4, 3.1.5, 3.1.6, 3.1.8, 3.3.9; TRM TLCOs 3.1.b, 3.1.d, 3.1.f, 3.1.h, and 3.1.j).

The SDM limits for MODE 5 are:

2.2.2 SDM shall be greater than or equal to 1.3% Δk/k (LCO 3.1.1, LCO 3.3.9; TRM TLCOs 3.1.i and 3.1.j).

2.3 Moderator Temperature Coefficient (MTC) (LCO 3.1.3)

The Moderator Temperature Coefficient (MTC) limits are:

2.3.1 The BOL/ARO/HZP-MTC upper limit shall be $+2.14 \times 10^{-5}$ Δk/k/°F.

2.3.2 The EOL/ARO/HFP-MTC lower limit shall be -4.6×10^{-4} Δk/k/°F.

2.3.3 The EOL/ARO/HFP-MTC Surveillance limit at 300 ppm shall be -3.7×10^{-4} Δk/k/°F.

2.3.4 The EOL/ARO/HFP-MTC Surveillance limit at 60 ppm shall be -4.3×10^{-4} Δk/k/°F.

where: BOL stands for Beginning of Cycle Life
ARO stands for All Rods Out
HZP stands for Hot Zero Thermal Power
EOL stands for End of Cycle Life
HFP stands for Hot Full Thermal Power

2.4 Shutdown Bank Insertion Limits (LCO 3.1.5)

2.4.1 All shutdown banks shall be fully withdrawn to at least 224 steps.

2.5 Control Bank Insertion Limits (LCO 3.1.6)

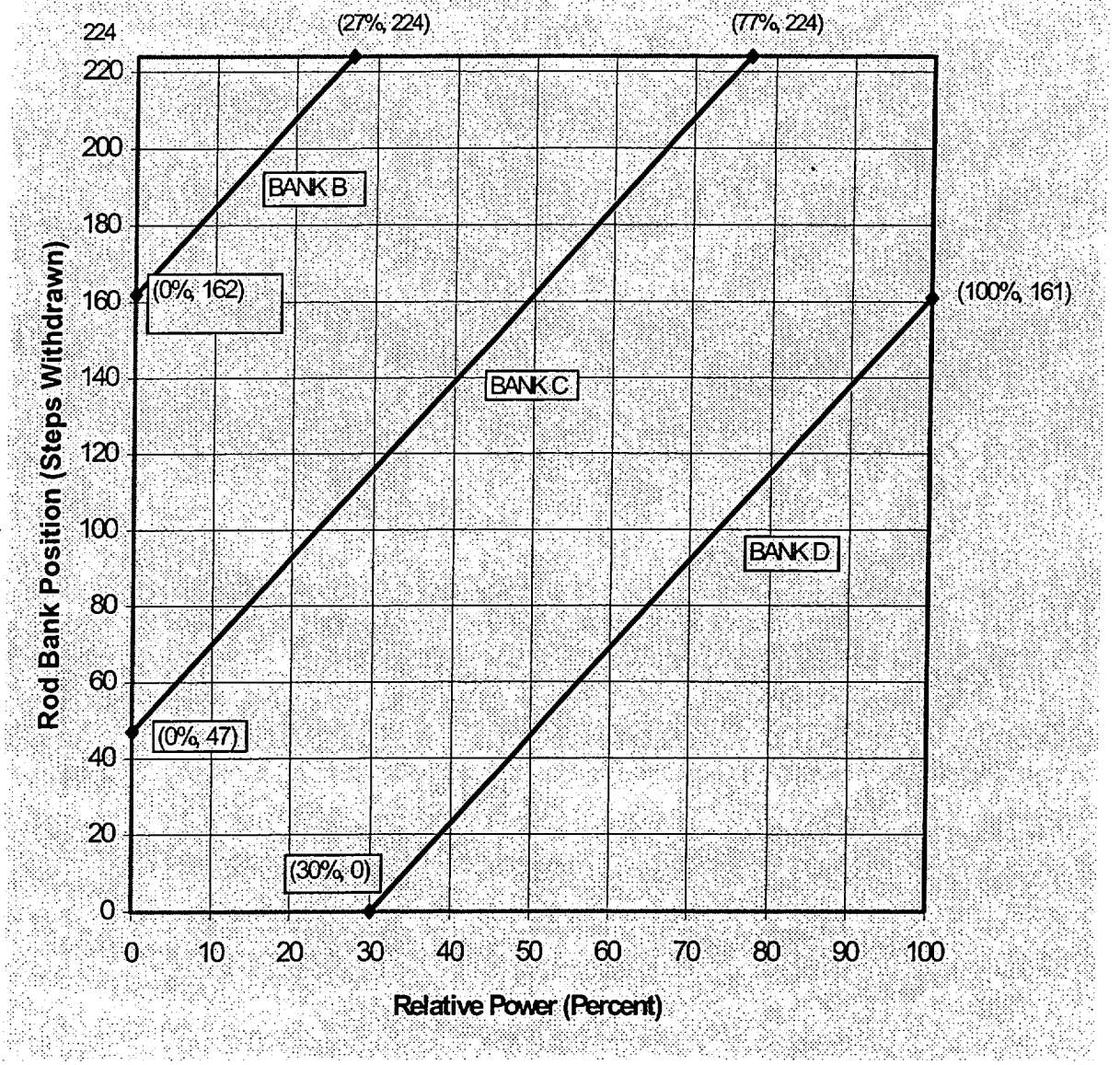
2.5.1 The control banks shall be limited in physical insertion as shown in Figure 2.5.1.

2.5.2 Each control bank shall be considered fully withdrawn from the core at greater than or equal to 224 steps.

2.5.3 The control banks shall be operated in sequence by withdrawal of Bank A, Bank B, Bank C and Bank D. The control banks shall be sequenced in reverse order upon insertion.

2.5.4 Each control bank not fully withdrawn from the core shall be operated with the 110 Step overlap limit.

Figure 2.5.1:
Control Bank Insertion Limits Versus Percent Rated Thermal Power



2.6 Heat Flux Hot Channel Factor ($F_Q(Z)$) (LCO 3.2.1)

2.6.1

$$F_Q(Z) \leq \frac{F_Q^{RTP}}{0.5} xK(Z) \quad \text{for } P \leq 0.5$$

$$F_Q(Z) \leq \frac{F_Q^{RTP}}{P} xK(Z) \quad \text{for } P > 0.5$$

where: P = the ratio of THERMAL POWER to RATED THERMAL POWER

F_Q^{RTP} = 2.60

K(Z) is provided in Figure 2.6.1.

2.6.2 W(Z) Values:

a) When PDMS is OPERABLE, W(Z) = 1.00000 for all axial points.

b) When PDMS is Inoperable, W(Z) is provided in Figures 2.6.2.a through 2.6.2.d.

The normal operation W(Z) values have been determined at burnups of 150, 6000, 14000, and 20000 MWD/MTU.

Table 2.6.2 shows the $F^C_Q(z)$ penalty factors that are greater than 2% per 31 Effective Full Power Days. These values shall be used to increase the $F^W_Q(z)$ as per Surveillance Requirement 3.2.1.2. A 2% penalty factor shall be used at all cycle burnups that are outside the range of Table 2.6.2.

Multiplication Factor = 1.02

2.6.3 Uncertainty:

The uncertainty, U_{FQ}, to be applied to the Heat Flux Hot Channel Factor $F_Q(Z)$ shall be calculated by the following formula

$$U_{FQ} = U_{qu} \bullet U_e$$

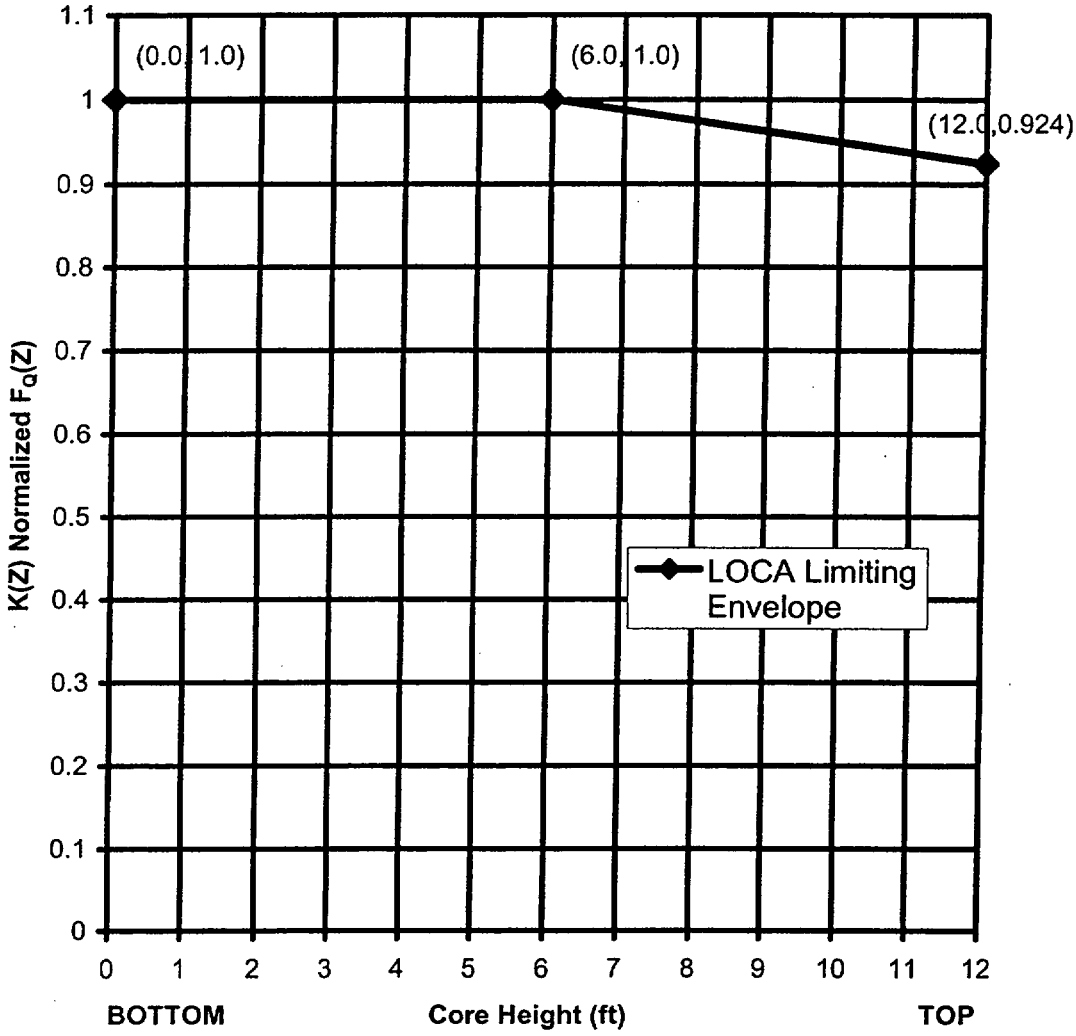
where:

U_{qu} = Base FQ measurement uncertainty = 1.05 when PDMS is inoperable.
U_e = Engineering uncertainty factor = 1.03

2.6.4 PDMS Alarms:

$F_Q(Z)$ Warning Setpoint ≥ 2% of $F_Q(Z)$ Margin
$F_Q(Z)$ Alarm Setpoint ≥ 0% of $F_Q(Z)$ Margin

Figure 2.6.1: K(Z) - Normalized $F_Q(Z)$ as a Function of Core Height



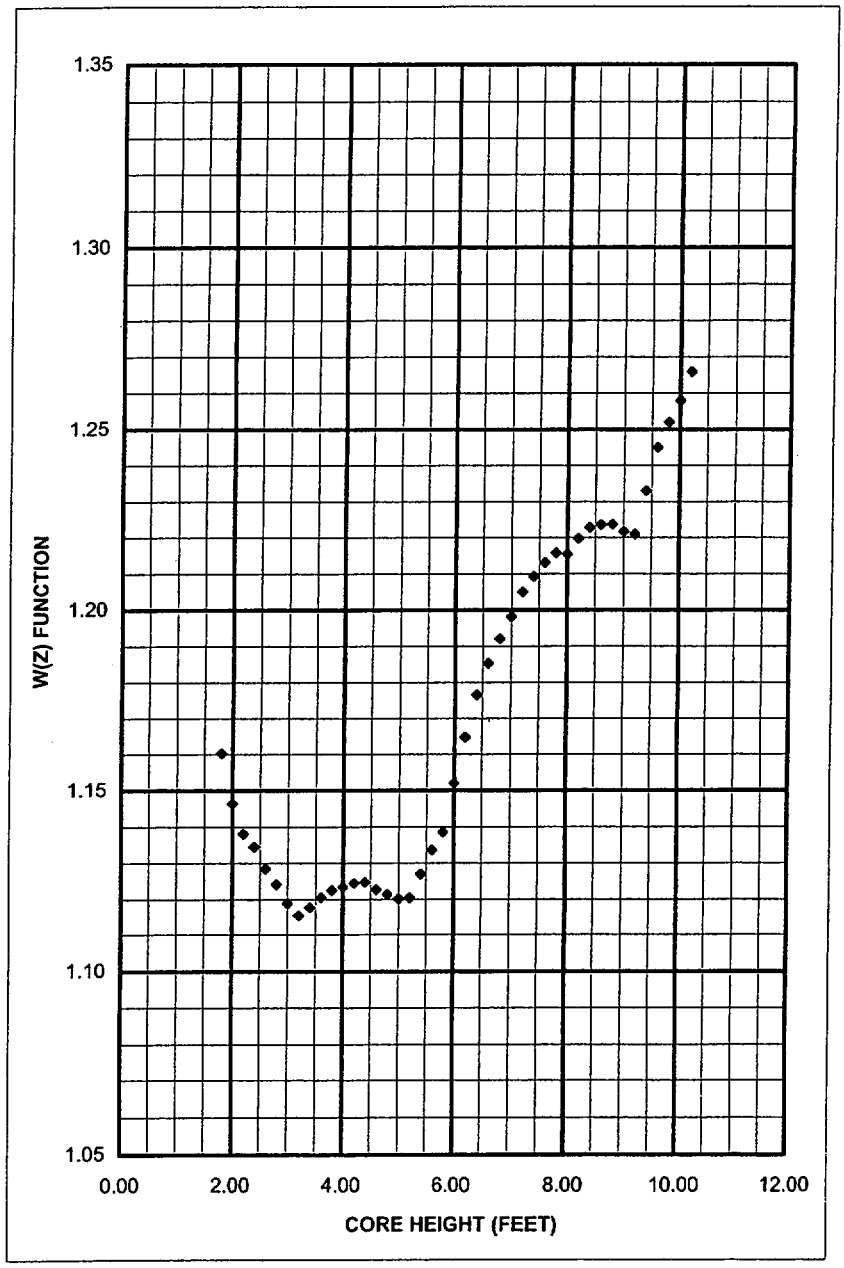
CORE OPERATING LIMITS REPORT (COLR) for BRAIDWOOD UNIT 1 CYCLE 10

Height Feet	MAX W(Z)
0.00	1.0000
0.20	1.0000
0.40	1.0000
0.60	1.0000
0.80	1.0000
1.00	1.0000
1.20	1.0000
1.40	1.0000
1.60	1.0000
1.80	1.1603
2.00	1.1464
2.20	1.1381
2.40	1.1345
2.60	1.1285
2.80	1.1242
3.00	1.1190
3.20	1.1155
3.40	1.1179
3.60	1.1206
3.80	1.1225
4.00	1.1234
4.20	1.1245
4.40	1.1248
4.60	1.1227
4.80	1.1214
5.00	1.1202
5.20	1.1205
5.40	1.1270
5.60	1.1336
5.80	1.1385
6.00	1.1521
6.20	1.1648
6.40	1.1765
6.60	1.1853
6.80	1.1921
7.00	1.1982
7.20	1.2050
7.40	1.2093
7.60	1.2131
7.80	1.2158
8.00	1.2154
8.20	1.2198
8.40	1.2228
8.60	1.2236
8.80	1.2237
9.00	1.2217
9.20	1.2210
9.40	1.2330
9.60	1.2450
9.80	1.2520
10.00	1.2580
10.20	1.2660
10.40	1.0000
10.60	1.0000
10.80	1.0000
11.00	1.0000
11.20	1.0000
11.40	1.0000
11.60	1.0000
11.80	1.0000
12.00	1.0000

Braidwood Unit 1 Cycle 10

Figure 2.6.2.a

Summary of W(Z) Function at 150 MWD/MTU
(Top and Bottom 15% Excluded per WCAP-10216)



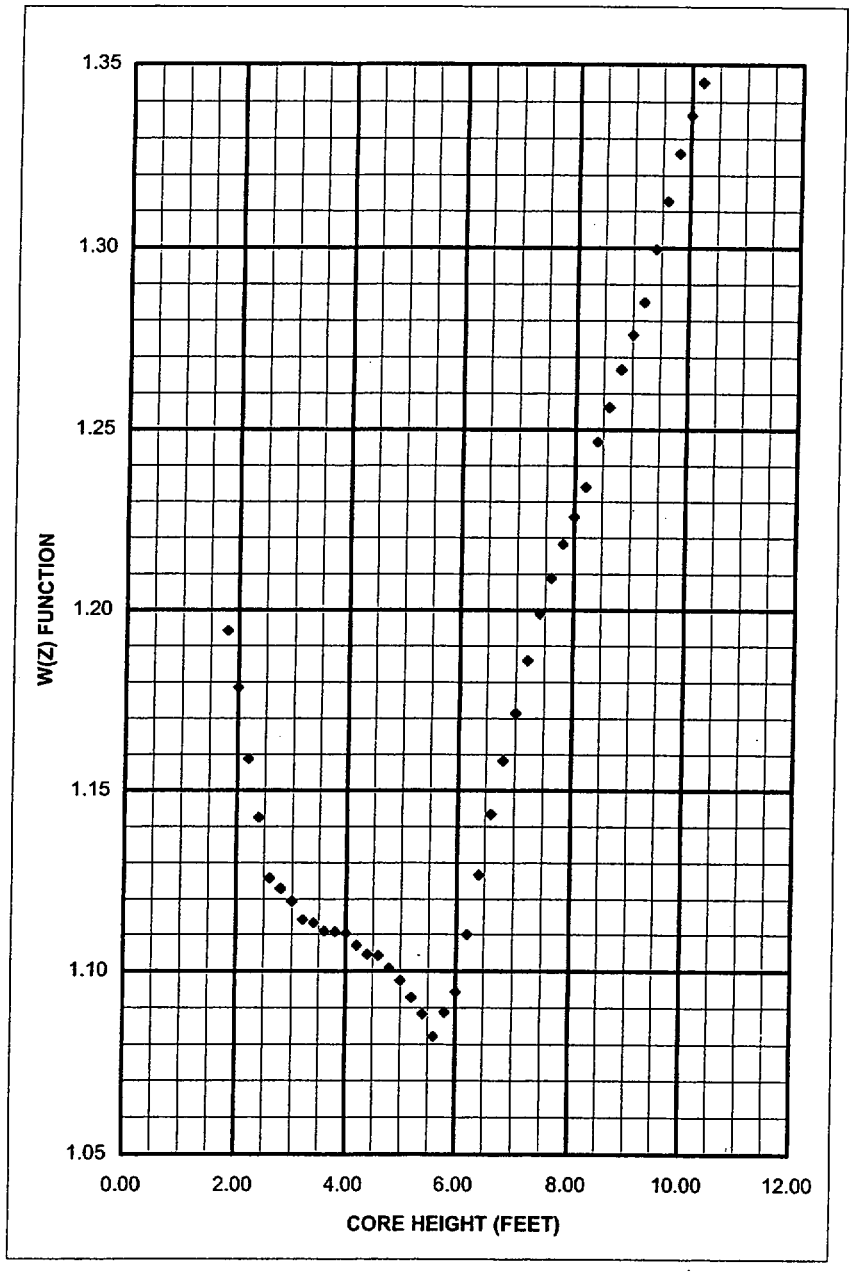
CORE OPERATING LIMITS REPORT (COLR) for BRAIDWOOD UNIT 1 CYCLE 10

Height Feet	MAX W(Z)
0.00	1.0000
0.20	1.0000
0.40	1.0000
0.60	1.0000
0.80	1.0000
1.00	1.0000
1.20	1.0000
1.40	1.0000
1.60	1.0000
1.80	1.1942
2.00	1.1785
2.20	1.1588
2.40	1.1425
2.60	1.1258
2.80	1.1229
3.00	1.1194
3.20	1.1141
3.40	1.1132
3.60	1.1109
3.80	1.1107
4.00	1.1103
4.20	1.1070
4.40	1.1046
4.60	1.1042
4.80	1.1008
5.00	1.0974
5.20	1.0928
5.40	1.0883
5.60	1.0821
5.80	1.0887
6.00	1.0944
6.20	1.1100
6.40	1.1267
6.60	1.1434
6.80	1.1582
7.00	1.1715
7.20	1.1860
7.40	1.1989
7.60	1.2088
7.80	1.2182
8.00	1.2258
8.20	1.2341
8.40	1.2467
8.60	1.2563
8.80	1.2666
9.00	1.2762
9.20	1.2851
9.40	1.2996
9.60	1.3128
9.80	1.3259
10.00	1.3363
10.20	1.3452
10.40	1.0000
10.60	1.0000
10.80	1.0000
11.00	1.0000
11.20	1.0000
11.40	1.0000
11.60	1.0000
11.80	1.0000
12.00	1.0000

Braidwood Unit 1 Cycle 10

Figure 2.6.2.b

Summary of W(Z) Function at 6000 MWD/MTU
(Top and Bottom 15% Excluded per WCAP-10216)

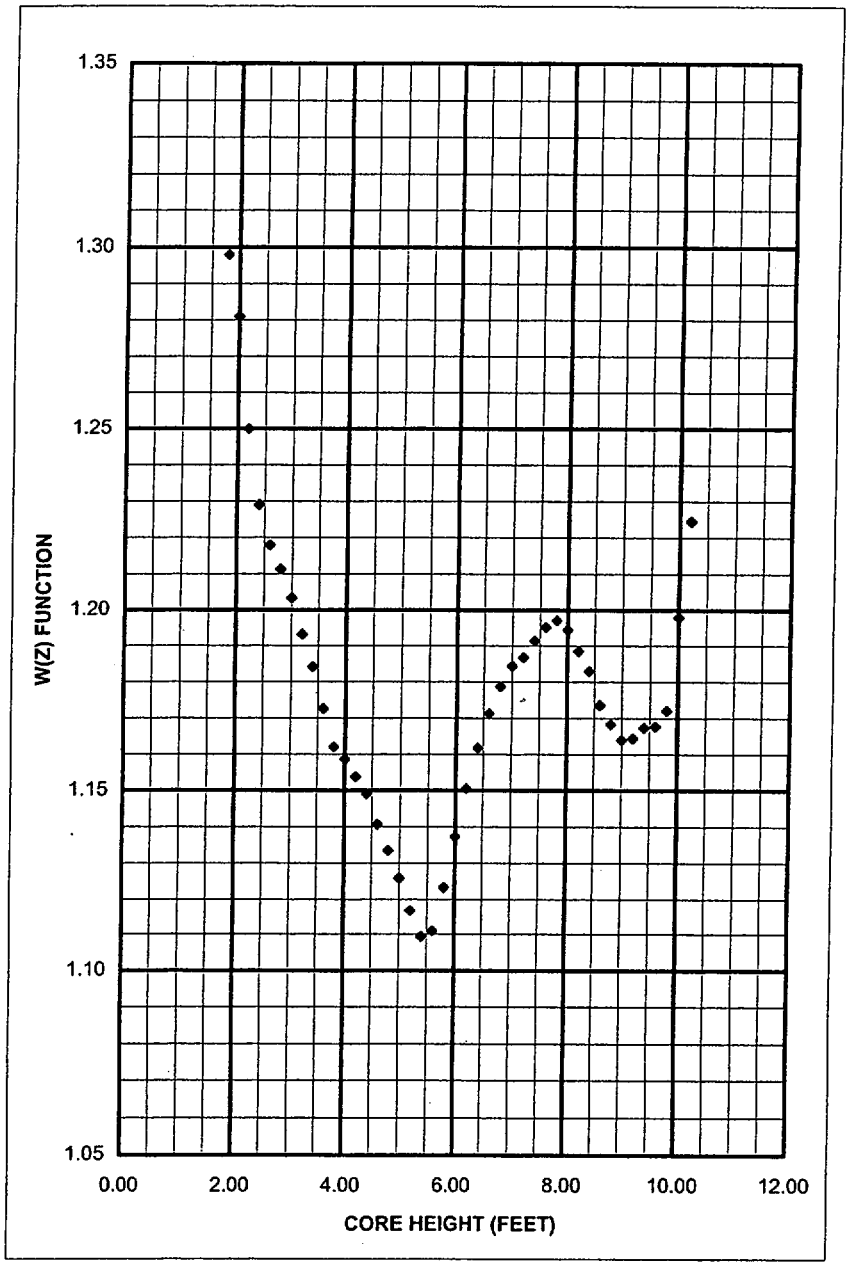


Height Feet	MAX W(Z)
0.00	1.0000
0.20	1.0000
0.40	1.0000
0.60	1.0000
0.80	1.0000
1.00	1.0000
1.20	1.0000
1.40	1.0000
1.60	1.0000
1.80	1.2980
2.00	1.2810
2.20	1.2500
2.40	1.2290
2.60	1.2179
2.80	1.2113
3.00	1.2033
3.20	1.1932
3.40	1.1841
3.60	1.1726
3.80	1.1620
4.00	1.1586
4.20	1.1538
4.40	1.1490
4.60	1.1406
4.80	1.1335
5.00	1.1259
5.20	1.1168
5.40	1.1094
5.60	1.1109
5.80	1.1233
6.00	1.1372
6.20	1.1506
6.40	1.1618
6.60	1.1713
6.80	1.1787
7.00	1.1844
7.20	1.1868
7.40	1.1914
7.60	1.1952
7.80	1.1971
8.00	1.1944
8.20	1.1885
8.40	1.1830
8.60	1.1736
8.80	1.1683
9.00	1.1639
9.20	1.1644
9.40	1.1674
9.60	1.1677
9.80	1.1720
10.00	1.1980
10.20	1.2245
10.40	1.0000
10.60	1.0000
10.80	1.0000
11.00	1.0000
11.20	1.0000
11.40	1.0000
11.60	1.0000
11.80	1.0000
12.00	1.0000

Braidwood Unit 1 Cycle 10

Figure 2.6.2.c

Summary of W(Z) Function at 14000 MWD/MTU
(Top and Bottom 15% Excluded per WCAP-10216)



Height Feet	MAX W(Z)
0.00	1.0000
0.20	1.0000
0.40	1.0000
0.60	1.0000
0.80	1.0000
1.00	1.0000
1.20	1.0000
1.40	1.0000
1.60	1.0000
1.80	1.2378
2.00	1.2237
2.20	1.2128
2.40	1.2033
2.60	1.1925
2.80	1.1831
3.00	1.1739
3.20	1.1634
3.40	1.1653
3.60	1.1670
3.80	1.1677
4.00	1.1669
4.20	1.1644
4.40	1.1618
4.60	1.1553
4.80	1.1607
5.00	1.1659
5.20	1.1714
5.40	1.1739
5.60	1.1874
5.80	1.2059
6.00	1.2214
6.20	1.2349
6.40	1.2455
6.60	1.2521
6.80	1.2568
7.00	1.2586
7.20	1.2545
7.40	1.2504
7.60	1.2415
7.80	1.2315
8.00	1.2197
8.20	1.2029
8.40	1.1862
8.60	1.1666
8.80	1.1490
9.00	1.1329
9.20	1.1214
9.40	1.1300
9.60	1.1760
9.80	1.2160
10.00	1.2530
10.20	1.2870
10.40	1.0000
10.60	1.0000
10.80	1.0000
11.00	1.0000
11.20	1.0000
11.40	1.0000
11.60	1.0000
11.80	1.0000
12.00	1.0000

Braidwood Unit 1 Cycle 10

Figure 2.6.2.d

Summary of W(Z) Function at 20000 MWD/MTU
(Top and Bottom 15% Excluded per WCAP-10216)

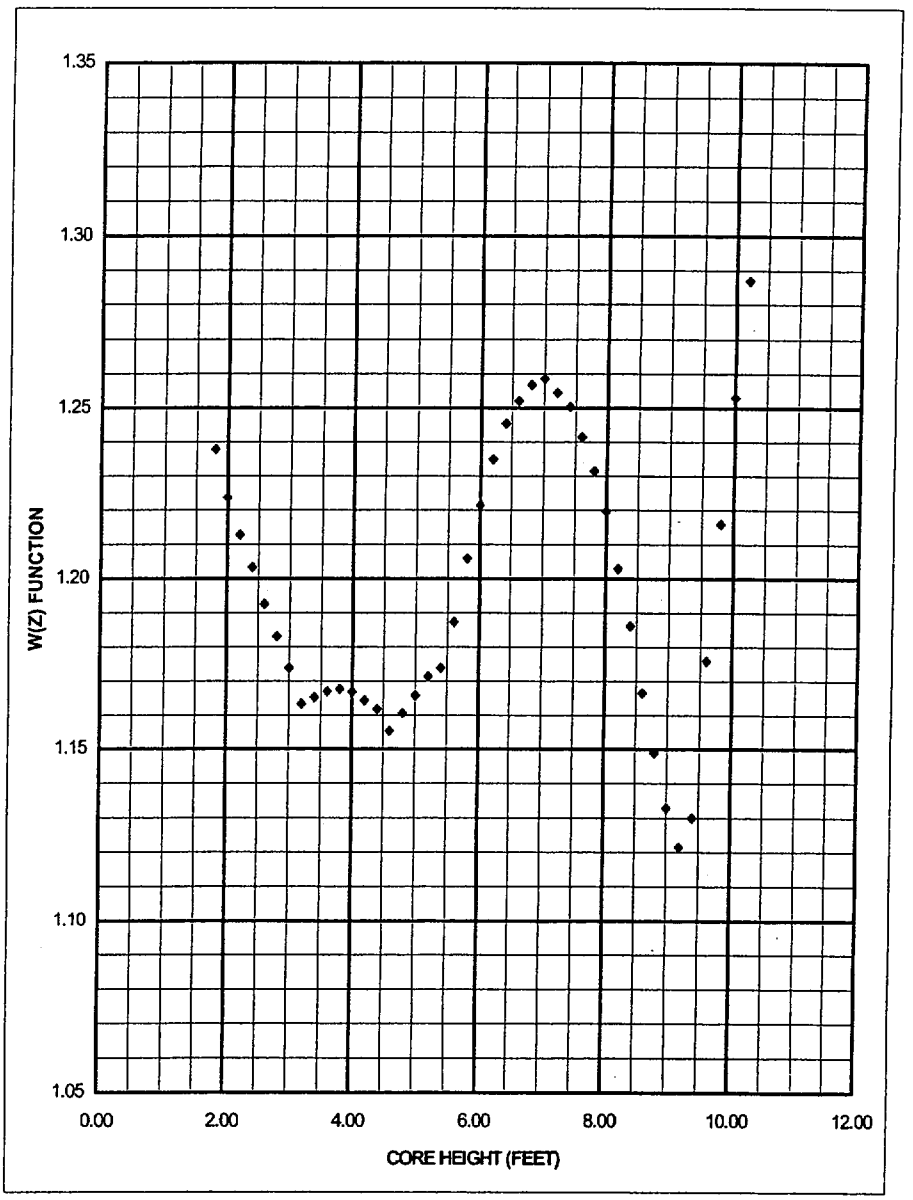


Table 2.6.2

Fq Margin Decreases in Excess of 2% per 31 EFPD

Cycle Burnup (MWD/MTU)	Max % Decrease in Fq Margin
665	2.00
837	2.19
1008	3.19
1180	4.14
1351	4.99
1523	5.72
1695	6.13
1866	5.93
2038	5.59
2210	5.14
2381	4.63
2553	4.11
2724	3.63
2896	3.23
3068	2.91
3239	2.66
3411	2.45
3583	2.27
3754	2.08
3926	2.00
13365	2.00
13537	2.08
13708	2.27
13880	2.43
14052	2.55
14223	2.62
14395	2.64
14567	2.61
14738	2.53
14910	2.40
15081	2.24
15253	2.06
15425	2.00

Note: All cycle burnups outside the range of the table shall use a 2% decrease in Fq margin for compliance with the 3.2.1.2 Surveillance Requirements. Linear interpolation is adequate for intermediate cycle burnups.

2.7 Nuclear Enthalpy Rise Hot Channel Factor ($F^N_{\Delta H}$) (LCO 3.2.2)

2.7.1 $F^N_{\Delta H} \leq F^{RTP}_{\Delta H}[1.0 + PF_{\Delta H}(1.0 - P)]$

where: P = the ratio of THERMAL POWER to RATED THERMAL POWER
$F^{RTP}_{\Delta H} = 1.70$
$PF_{\Delta H} = 0.3$

2.7.2 Uncertainty when PDMS is inoperable

The uncertainty, $U_{F\Delta H}$, to be applied to the Nuclear Enthalpy Rise Hot Channel Factor $F_{\Delta H}{}^N$ shall be calculated by the following formula:

$U_{F\Delta H} = U_{F\Delta Hm}$

where:

$U_{F\Delta Hm}$ = Base $F^N_{\Delta H}$ measurement uncertainty = 1.04

2.7.3 PDMS Alarms:

$F^N_{\Delta H}$ Warning Setpoint ≥ 2% of $F^N_{\Delta H}$ Margin
$F^N_{\Delta H}$ Alarm Setpoint ≥ 0% of $F^N_{\Delta H}$ Margin

2.8 AXIAL FLUX DIFFERENCE (AFD) (LCO 3.2.3)

2.8.1 When PDMS is Inoperable, the AXIAL FLUX DIFFERENCE (AFD) Acceptable Operation Limits are provided in Figure 2.8.1 or the latest valid PDMS Surveillance Report, whichever is more conservative.

2.8.2 When PDMS is OPERABLE, no AFD Acceptable Operation Limits are applicable.

2.9 Departure from Nucleate Boiling Ratio (DNBR) (LCO 3.2.5)

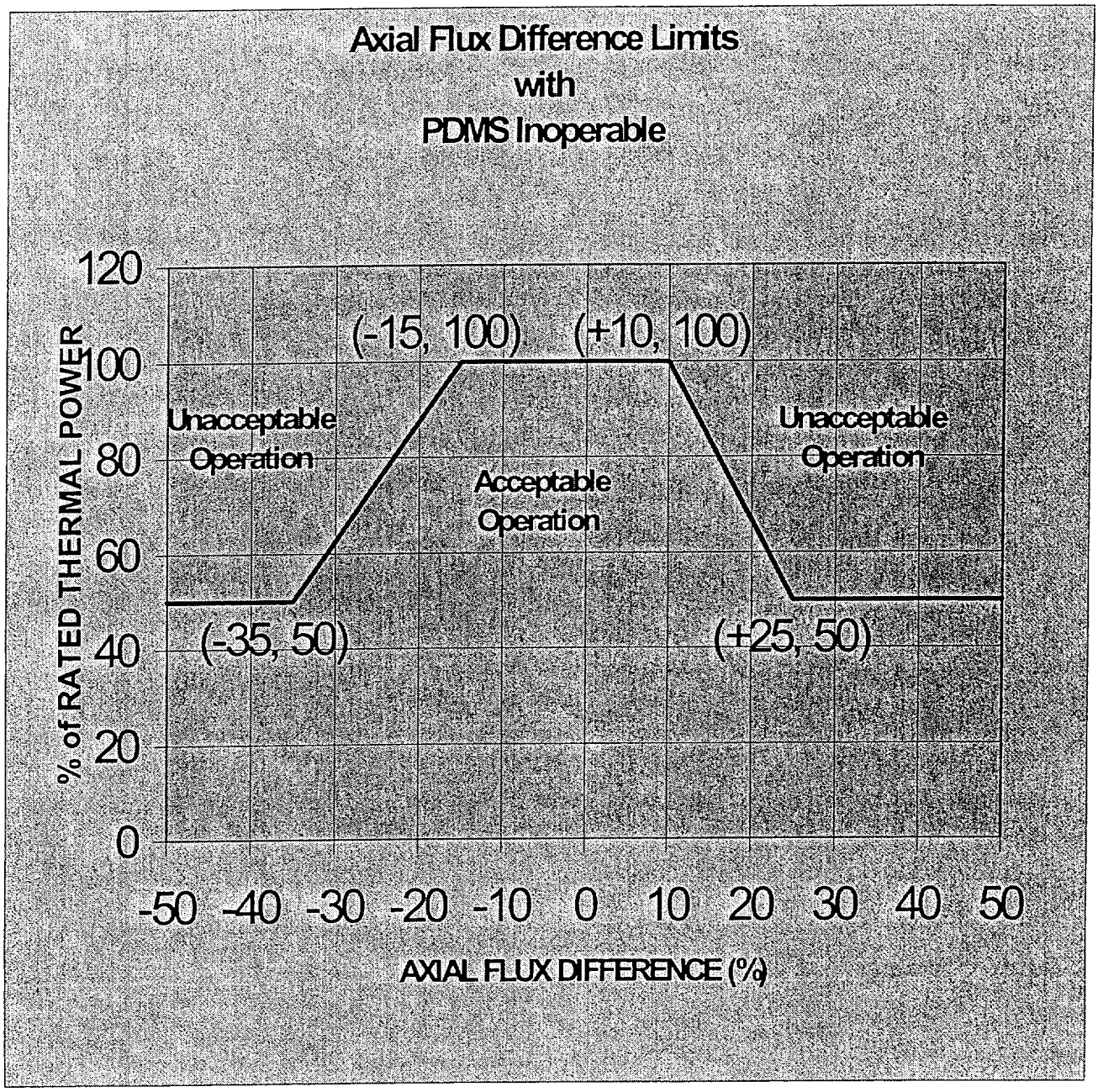
2.9.1 $DNBR_{APSL} \geq 1.536$

The Axial Power Shape Limiting DNBR ($DNBR_{APSL}$) is applicable with THERMAL POWER ≥ 50% RTP when PDMS is OPERABLE.

2.9.2 PDMS Alarms:

DNBR Warning Setpoint ≥ 2% of DNBR Margin
DNBR Alarm Setpoint ≥ 0% of DNBR Margin

Figure 2.8.1 Axial Flux Difference Limits as a Function of Rated Thermal Power



2.10 Reactor Trip System (RTS) Instrumentation (LCO 3.3.1) - Overtemperature ΔT Setpoint Parameter Values

2.10.1 The Overtemperature ΔT reactor trip setpoint K_1 shall be equal to 1.325.

2.10.2 The Overtemperature ΔT reactor trip setpoint T_{avg} coefficient K_2 shall be equal to 0.0297 / °F.

2.10.3 The Overtemperature ΔT reactor trip setpoint pressure coefficient K_3 shall be equal to 0.00181 / psig.

2.10.4 The nominal T_{avg} at RTP (indicated) T' shall be less than or equal to 588.0 °F.

2.10.5 The nominal RCS operating pressure (indicated) P' shall be equal to 2235 psig.

2.10.6 The measured reactor vessel ΔT lead/lag time constant τ_1 shall be equal to 8 sec.

2.10.7 The measured reactor vessel ΔT lead/lag time constant τ_2 shall be equal to 3 sec.

2.10.8 The measured reactor vessel ΔT lag time constant τ_3 shall be less than or equal to 2 sec.

2.10.9 The measured reactor vessel average temperature lead/lag time constant τ_4 shall be equal to 33 sec.

2.10.10 The measured reactor vessel average temperature lead/lag time constant τ_5 shall be equal to 4 sec.

2.10.11 The measured reactor vessel average temperature lag time constant τ_6 shall be less than or equal to 2 sec.

2.10.12 The $f_1(\Delta I)$ "positive" breakpoint shall be +10% ΔI.

2.10.13 The $f_1(\Delta I)$ "negative" breakpoint shall be -18% ΔI.

2.10.14 The $f_1(\Delta I)$ "positive" slope shall be +3.47% / % ΔI.

2.10.15 The $f_1(\Delta I)$ "negative" slope shall be -2.61% / % ΔI.

2.11 Reactor Trip System (RTS) Instrumentation (LCO 3.3.1) - Overpower ΔT Setpoint Parameter Values

2.11.1 The Overpower ΔT reactor trip setpoint K_4 shall be equal to 1.072.

2.11.2 The Overpower ΔT reactor trip setpoint T_{avg} rate/lag coefficient K_5 shall be equal to 0.02 / °F for increasing T_{avg}.

2.11.3 The Overpower ΔT reactor trip setpoint T_{avg} rate/lag coefficient K_5 shall be equal to 0 / °F for decreasing T_{avg}.

2.11.4 The Overpower ΔT reactor trip setpoint T_{avg} heatup coefficient K_6 shall be equal to 0.00245 / °F when $T > T''$.

2.11.5 The Overpower ΔT reactor trip setpoint T_{avg} heatup coefficient K_6 shall be equal to 0 / °F when $T \leq T''$.

2.11.6 The nominal T_{avg} at RTP (indicated) T'' shall be less than or equal to 588.0 °F

2.11.7 The measured reactor vessel ΔT lead/lag time constant τ_1 shall be equal to 8 sec.

2.11.8 The measured reactor vessel ΔT lead/lag time constant τ_2 shall be equal to 3 sec.

2.11.9 The measured reactor vessel ΔT lag time constant τ_3 shall be less than or equal to 2 sec.

2.11.10 The measured reactor vessel average temperature lag time constant τ_6 shall be less than or equal to 2 sec.

2.11.11 The measured reactor vessel average temperature rate/lag time constant τ_7 shall be equal to 10 sec.

2.11.12 The $f_2(\Delta I)$ "positive" breakpoint shall be 0 for all ΔI.

2.11.13 The $f_2(\Delta I)$ "negative" breakpoint shall be 0 for all ΔI.

2.11.14 The $f_2(\Delta I)$ "positive" slope shall be 0 for all ΔI.

2.11.15 The $f_2(\Delta I)$ "negative" slope shall be 0 for all ΔI.

2.12 Reactor Coolant System (RCS) Pressure, Temperature, and Flow Departure from Nucleate Boiling (DNB) Limits (LCO 3.4.1)

2.12.1 The pressurizer pressure shall be greater than or equal to 2209 psig.

2.12.2 The RCS average temperature (T_{avg}) shall be less than or equal to 593.1 °F.

2.12.3 The RCS total flow rate shall be greater than or equal to 380,900 gpm.

2.13 Boron Concentration

2.13.1 The refueling boron concentration shall be greater than or equal to 1670 ppm (LCO 3.9.1).

2.13.2 The Reactor Coolant System boron concentration shall be greater than or equal to 1722 ppm prior to initial criticality of Cycle 10, or greater than or equal to 1972 ppm at all other times in core life, to maintain adequate shutdown margin for MODES 3, 4, and 5 during performance of rod drop time measurements and during the surveillance of Digital Rod Position Indication (DRPI) for OPERABILITY (TRM TLCOs 3.1.g and 3.1.k).