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Docket Nos. 50-280
and 50-281

Mr. Stanley Ragone
Vice President
Virginia Electric and
Power Company
P. O. Box 26666
Richmond, Virginia 23261

DO NOT REMOVE

*Change #8
Rev. 1*

Dear Mr. Ragone:

On July 17, 1973, we issued Change No. 8 to the Technical Specifications of Facility Operating Licenses Nos. DPR 32 and 37, for Surry Power Station Units 1 and 2. This change authorized operation at a reduced primary system pressure (2000 psia) to minimize fuel collapse during the first fuel cycle.

Subsequently, your letter of August 1, 1973, indicated that you had been advised by Westinghouse Electric Corporation that new values were required in the equation which is used to establish the over-temperature ΔT trip setpoints for reduced pressure operation. You stated that the original setpoints, determined for a primary system pressure of 2250 psia, were overly conservative to the point of not allowing normal operation at the authorized power level.

We have reviewed the new setpoint values contained in corrected page 2.3-2 of the Technical Specifications enclosed with your August 1 letter, and recognize the problem associated with the setpoint values contained in the original page 2.3-2 of Change No. 8 transmitted by our letter dated July 17, 1973. Although the evaluation contained in our July 17 letter remains unchanged, we have concluded that operation of the reactor in the manner proposed in your letter dated August 1, 1973, does not involve a significant hazards consideration and that there is reasonable assurance that the health and safety of the public will not be endangered.

Mr. Stanley Ragone

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Accordingly, replace page TS 2.3-2 of Change No. 8 to the Technical Specifications of Facility Operating Licenses Nos. DPR 32 and 37, dated July 17, 1973, with the enclosed revised page TS 2.3-2, designated Change No. 8, Revision 1, dated August , 1973.

Sincerely,

R. C. DeYoung, Assistant Director
for Pressurized Water Reactors
Directorate of Licensing

Enclosure:
Page TS 2.3-2

cc: George D. Gibson, Esq.
Hunton, Williams, Gay,
and Gibson
P. O. Box 1535
Richmond, Virginia 23213

FOR CONCURRENCES SEE DOCKET NO. 50-280

OFFICE ▶	PWR-1	AD/PWRs				
SURNAME ▶	Lee	RCDeYoung				
DATE ▶	8/2/73	8/2/73				

CHANGE NO. 8
REVISION 1

(d) Overtemperature T

$$\Delta T < \Delta T_0 [K_1 - K_2 (T - T') + K_3 (P - P') - f(\Delta I)]$$

where

ΔT_0 = Indicated ΔT at rated thermal power, °F

T = Average coolant temperature, °F

T' = 563.5 °F

P = Pressurizer pressure, psig

P' = 1985 psig

K_1 = 1.095 (for 3 loop operation and 2 loop operation with the loop stop valves closed in the inoperable loop)

= 1.036 (for 2 loop operation with the loop stop valves open in the inoperable loop)

K_2 = 0.0139 (for 3 loop operation and 2 loop operation with the loop stop valves closed in the inoperable loop)

= 0.0139 (for 2 loop operation with the loop stop valves open in the inoperable loop)

K_3 = 0.000751 (for 3 loop operation and 2 loop operation with the loop stop valves closed in the inoperable loop)

= 0.000944 (for 2 loop operation with the loop stop valves open in the inoperable loop)

ΔI = $q_t - q_b$, where q_t and q_b are the percent power in the top and bottom halves of the core respectively, and $q_t + q_b$ is total core power in percent of rated power

f(ΔI) = function of ΔI , percent of rated core power as shown in Figure 2.3-1

(e) Overpower T

$$\Delta T < \Delta T_0 [K_4 - K_5 \frac{dT}{dt} - K_6 (T - T') - f(\Delta I)]$$

CHANGE NO. 8
REVISION 1

8-1

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