

May 31, 1995

Mr. J.P. O'Hanlon
Senior Vice President - Nuclear
Virginia Electric and Power Company
5000 Dominion Blvd.
Glen Allen, Virginia 23060

DISTRIBUTION:
See next page

Dear Mr. O'Hanlon:

SUBJECT: SURRY UNITS 1 AND 2 - ISSUANCE OF AMENDMENTS RE: CHEMICAL AND
VOLUME CONTROL SYSTEM AND SAFETY INJECTION SYSTEM
(TAC NOS. M89646 AND M89647)

The Commission has issued the enclosed Amendment No. 199 to Facility Operating License No. DPR-32 and Amendment No. 199 to Facility Operating License No. DPR-37 for the Surry Power Station, Unit Nos. 1 and 2, respectively. The amendments consist of changes to the Technical Specifications (TS) in response to your application transmitted by letter dated June 9, 1994.

These amendments would modify the Chemical and Volume Control System and the Safety Injection System TS.

A copy of the Safety Evaluation is also enclosed. The Notice of Issuance will be included in the Commission's biweekly Federal Register notice. This completes our efforts on this issue and we are, therefore, closing out TAC Nos. M89646 and M89647.

Sincerely,

Original signed by:

Bart C. Buckley, Senior Project Manager
Project Directorate II-1
Division of Reactor Projects - I/II
Office of Nuclear Reactor Regulation

Enclosures:

1. Amendment No. 199 to DPR-32
2. Amendment No. 199 to DPR-37
3. Safety Evaluation

cc w/enclosures:

See next page

Document Name - C:\AUTOS\WPDOCS\SU89646.AMD

To receive a copy of this document, indicate in the box: "C" = Copy without attachment/enclosure "E" = Copy with attachment/enclosure "N" = No copy

| | | | | | | | | |
|--------|----------------|---|----------------|---|-----------|---------|--|------|
| OFFICE | LA:PDII-1:DRPE | E | PM:PDII-1:DRPE | E | D:PDII-1 | OGC | | |
| NAME | EDunnington ED | | BBuckley BCB | | DMatthews | | | SRXB |
| DATE | 5/17/95 | | 5/17/95 | | 5/31/95 | 5/12/95 | | |

OFFICIAL RECORD COPY

070001

9509060316 950531
PDR ADOCK 05000280
P PDR

CP-1
DF01

DATED: May 31, 1995

AMENDMENT NO. 199 TO FACILITY OPERATING LICENSE NO. DPR-32 - SURRY UNIT 1
AMENDMENT NO. 199 TO FACILITY OPERATING LICENSE NO. DPR-37 - SURRY UNIT 2

Docket File
NRC & Local PDRs
PDII-1 Reading
S. Varga
J. Zwolinski
D. Matthews
B. Buckley
E. Dunnington
OGC
D. Hagan, TWFN, AEOD
G. Hill (4), TWFN, 5/C/3
C. Grimes, 11/F/23
ACRS (4)
OPA
OC/LFMB
A. Belisle, RII
D. Verrelli, RII



UNITED STATES
NUCLEAR REGULATORY COMMISSION
WASHINGTON, D.C. 20555-0001

May 31, 1995

Mr. J.P. O'Hanlon
Senior Vice President - Nuclear
Virginia Electric and Power Company
5000 Dominion Blvd.
Glen Allen, Virginia 23060

Dear Mr. O'Hanlon:

SUBJECT: SURRY UNITS 1 AND 2 - ISSUANCE OF AMENDMENTS RE: CHEMICAL AND
VOLUME CONTROL SYSTEM AND SAFETY INJECTION SYSTEM
(TAC NOS. M89646 AND M89647)

The Commission has issued the enclosed Amendment No. 199 to Facility Operating License No. DPR-32 and Amendment No. 199 to Facility Operating License No. DPR-37 for the Surry Power Station, Unit Nos. 1 and 2, respectively. The amendments consist of changes to the Technical Specifications (TS) in response to your application transmitted by letter dated June 9, 1994.

These amendments would modify the Chemical and Volume Control System and the Safety Injection System TS.

A copy of the Safety Evaluation is also enclosed. The Notice of Issuance will be included in the Commission's biweekly Federal Register notice. This completes our efforts on this issue and we are, therefore, closing out TAC Nos. M89646 and M89647.

Sincerely,

A handwritten signature in cursive script that reads "Bart C. Buckley".

Bart C. Buckley, Senior Project Manager
Project Directorate II-1
Division of Reactor Projects - I/II
Office of Nuclear Reactor Regulation

Docket Nos. 50-280 and 50-281

Enclosures:

1. Amendment No. 199 to DPR-32
2. Amendment No. 199 to DPR-37
3. Safety Evaluation

cc w/enclosures:
See next page

Mr. J. P. O'Hanlon
Virginia Electric and Power Company

Surry Power Station
Units 1 and 2

cc:

Michael W. Maupin, Esq.
Hunton and Williams
Riverfront Plaza, East Tower
951 E. Byrd Street
Richmond, Virginia 23219

Attorney General
Supreme Court Building
101 North 8th Street
Richmond, Virginia 23219

Mr. David Christian, Manager
Surry Power Station
Post Office Box 315
Surry, Virginia 23883

Mr. M. L. Bowling, Manager
Nuclear Licensing & Programs
Virginia Electric and Power Company
Innsbrook Technical Center
5000 Dominion Blvd.
Glen Allen, Virginia 23060

Senior Resident Inspector
Surry Power Station
U.S. Nuclear Regulatory Commission
5850 Hog Island Road
Surry, Virginia 23883

Chairman
Board of Supervisors of Surry County
Surry County Courthouse
Surry, Virginia 23683

Dr. W. T. Lough
Virginia State Corporation
Commission
Division of Energy Regulation
Post Office Box 1197
Richmond, Virginia 23209

Regional Administrator, Region II
U.S. Nuclear Regulatory Commission
101 Marietta Street N.W., Suite 2900
Atlanta, Georgia 30323

Robert B. Strobe, M.D., M.P.H.
State Health Commissioner
Office of the Commissioner
Virginia Department of Health
P.O. Box 2448
Richmond, Virginia 23218



UNITED STATES
NUCLEAR REGULATORY COMMISSION
WASHINGTON, D.C. 20555-0001

VIRGINIA ELECTRIC AND POWER COMPANY

DOCKET NO. 50-280

SURRY POWER STATION, UNIT NO. 1

AMENDMENT TO FACILITY OPERATING LICENSE

Amendment No. 199
License No. DPR-32

1. The Nuclear Regulatory Commission (the Commission) has found that:
 - A. The application for amendment by Virginia Electric and Power Company (the licensee) dated June 9, 1994, complies with the standards and requirements of the Atomic Energy Act of 1954, as amended (the Act) and the Commission's rules and regulations set forth in 10 CFR Chapter I;
 - B. The facility will operate in conformity with the application, the provisions of the Act, and the rules and regulations of the Commission;
 - C. There is reasonable assurance (i) that the activities authorized by this amendment can be conducted without endangering the health and safety of the public, and (ii) that such activities will be conducted in compliance with the Commission's regulations;
 - D. The issuance of this amendment will not be inimical to the common defense and security or to the health and safety of the public; and
 - E. The issuance of this amendment is in accordance with 10 CFR Part 51 of the Commission's regulations and all applicable requirements have been satisfied.

2. Accordingly, the license is amended by changes to the Technical Specifications as indicated in the attachment to this license amendment, and paragraph 3.B of Facility Operating License No. DPR-32 is hereby amended to read as follows:

(B) Technical Specifications

The Technical Specifications contained in Appendix A, as revised through Amendment No. 199, are hereby incorporated in the license. The licensee shall operate the facility in accordance with the Technical Specifications.

3. This license amendment is effective as of its date of issuance and shall be implemented within 30 days.

FOR THE NUCLEAR REGULATORY COMMISSION

B.C. Buckley for

David B. Matthews, Director
Project Directorate II-1
Division of Reactor Projects - I/II
Office of Nuclear Reactor Regulation

Attachment:
Changes to the Technical
Specifications

Date of Issuance: May 31, 1995



UNITED STATES
NUCLEAR REGULATORY COMMISSION
WASHINGTON, D.C. 20555-0001

VIRGINIA ELECTRIC AND POWER COMPANY

DOCKET NO. 50-281

SURRY POWER STATION, UNIT NO. 2

AMENDMENT TO FACILITY OPERATING LICENSE

Amendment No. 199
License No. DPR-37

1. The Nuclear Regulatory Commission (the Commission) has found that:
 - A. The application for amendment by Virginia Electric and Power Company (the licensee) dated June 9, 1994, complies with the standards and requirements of the Atomic Energy Act of 1954, as amended (the Act) and the Commission's rules and regulations set forth in 10 CFR Chapter I;
 - B. The facility will operate in conformity with the application, the provisions of the Act, and the rules and regulations of the Commission;
 - C. There is reasonable assurance (i) that the activities authorized by this amendment can be conducted without endangering the health and safety of the public, and (ii) that such activities will be conducted in compliance with the Commission's regulations;
 - D. The issuance of this amendment will not be inimical to the common defense and security or to the health and safety of the public;
and
 - E. The issuance of this amendment is in accordance with 10 CFR Part 51 of the Commission's regulations and all applicable requirements have been satisfied.

2. Accordingly, the license is amended by changes to the Technical Specifications as indicated in the attachment to this license amendment, and paragraph 3.B of Facility Operating License No. DPR-37 is hereby amended to read as follows:

(B) Technical Specifications

The Technical Specifications contained in Appendix A, as revised through Amendment No. 199, are hereby incorporated in the license. The licensee shall operate the facility in accordance with the Technical Specifications.

3. This license amendment is effective as of its date of issuance and shall be implemented within 30 days.

FOR THE NUCLEAR REGULATORY COMMISSION

B. C. Buckley for

David B. Matthews, Director
Project Directorate II-1
Division of Reactor Projects - I/II
Office of Nuclear Reactor Regulation

Attachment:
Changes to the Technical
Specifications

Date of Issuance: May 31, 1995

ATTACHMENT TO LICENSE AMENDMENT

AMENDMENT NO. 199 TO FACILITY OPERATING LICENSE NO. DPR-32

AMENDMENT NO. 199 TO FACILITY OPERATING LICENSE NO. DPR-37

DOCKET NOS. 50-280 AND 50-281

Revise Appendix A as follows:

Remove Pages

TS 3.1-4
TS 3.2-1
TS 3.2-2
TS 3.2-3
TS 3.2-3a
TS 3.2-4
TS 3.2-5
TS 3.2-6
TS 3.3-1 thru TS 3.3-7
TS 3.4-2
TS 3.4-4
TS Figure 3.8-1
TS 3.13-1 thru TS 3.13-5
TS 3.16-5
TS 4.1-7
TS 4.1-9b
TS 4.1-9d
TS 4.1-10
TS 4.5-2
TS 4.11-1 and TS 4.11-2

Insert Pages

TS 3.1-4
TS 3.2-1
TS 3.2-2
TS 3.2-3
- - -
TS 3.2-4
TS 3.2-5
- - -
TS 3.3-1 thru TS 3.3-5
TS 3.4-2
TS 3.4-4
TS Figure 3.8-1
TS 3.13-1 thru TS 3.13-2
TS 3.16-5
TS 4.1-7
TS 4.1-9b
TS 4.1-9d
TS 4.1-10
TS 4.5-2
TS 4.11-1 thru 4.11-4

4. Reactor Coolant Loops

- a. Loop stop valves shall not be closed in more than one loop unless the Reactor Coolant System is connected to the Residual Heat Removal System and the Residual Heat Removal System is OPERABLE.
- b. POWER OPERATION with less than three loops in service is prohibited. The following loop isolation valves shall have AC power removed and their breakers locked, sealed or otherwise secured in the open position during POWER OPERATION:

| <u>Unit No. 1</u> | <u>Unit No. 2</u> |
|-------------------|-------------------|
| MOV 1590 | MOV 2590 |
| MOV 1591 | MOV 2591 |
| MOV 1592 | MOV 2592 |
| MOV 1593 | MOV 2593 |
| MOV 1594 | MOV 2594 |
| MOV 1595 | MOV 2595 |

5. Pressurizer

- a. The reactor shall be maintained subcritical by at least 1% until the steam bubble is established and the necessary sprays and at least 125 KW of heaters are operable.
- b. With the pressurizer inoperable due to inoperable pressurizer heaters, restore the inoperable heaters within 72 hours or be in at least HOT SHUTDOWN within 6 hours and the Reactor Coolant System temperature and pressure less than 350°F and 450 psig, respectively, within the following 12 hours.
- c. With the pressurizer otherwise inoperable, be in at least HOT SHUTDOWN with the reactor trip breakers open within 6 hours and the Reactor Coolant System temperature and pressure less than 350°F and 450 psig, respectively, within the following 12 hours.

3.2. CHEMICAL AND VOLUME CONTROL SYSTEM

Applicability

Applies to the operational status of the Chemical and Volume Control System.

Objective

To define those conditions of the Chemical and Volume Control System necessary to ensure safe reactor operation.

Specification

- A. When fuel is in a reactor, there shall be at least one flow path to the core for boric acid injection. The minimum capability for boric acid injection shall be equivalent to that supplied from the refueling water storage tank.
- B. The reactor shall not be critical unless:
 - 1. At least two boron injection subsystems are OPERABLE consisting of:
 - a. A Chemical and Volume Control subsystem consisting of:
 - 1. One OPERABLE flow path,
 - 2. One OPERABLE charging pump,
 - 3. One OPERABLE boric acid transfer pump,
 - 4. The common OPERABLE boric acid storage system with:
 - a. A minimum contained borated water volume of 6000 gallons per unit,
 - b. A boron concentration of at least 7.0 weight percent but not more than 8.5 weight percent boric acid solution, and
 - c. A minimum solution temperature of 112°F.
 - d. An OPERABLE boric acid transfer pump for recirculation.

- b. A subsystem supplying borated water from the refueling water storage tank via a charging pump to the Reactor Coolant System consisting of:
 - 1. One OPERABLE flow path,
 - 2. One OPERABLE charging pump,
 - 3. The OPERABLE refueling water storage tank with:
 - a. A minimum contained borated water volume of 387,100 gallons,
 - b. A boron concentration of at least 2300 ppm but not more than 2500 ppm, and
 - c. A maximum solution temperature of 45°F.
- 2. One charging pump from the opposite unit is available with:
 - a. the pump being OPERABLE except for automatic initiation instrumentation,
 - b. offsite or emergency power may be inoperable when in COLD SHUTDOWN, and
 - c. the pump capable of being used for alternate shutdown with the opening of the charging pump cross-connect valves.
- C. The requirements of Specification 3.2.B may be modified as follows:
 - 1. With only one of the boron injection subsystems OPERABLE, restore at least two boron injection subsystems to OPERABLE status within 72 hours or be in at least HOT SHUTDOWN within the next 6 hours.
 - 2. With the refueling water storage tank inoperable, restore the tank to OPERABLE status within one hour or place the reactor in HOT SHUTDOWN within the next 6 hours.
 - a. For conditions where the RWST is inoperable due to boron concentration or solution temperature not being within the limits of Specification 3.3.A.1, restore the parameters to

within specified limits in 8 hours or place the reactor in HOT SHUTDOWN within the next 6 hours.

3. With no charging pump from the opposite unit available, return at least one of the opposite unit's charging pumps to available status in accordance with Specification 3.2.B.2 within 7 days or place the reactor in HOT SHUTDOWN within the next 6 hours.
- D. If the requirements of Specification 3.2.B are not satisfied as allowed by Specification 3.2.C, the reactor shall be placed in COLD SHUTDOWN within the following 30 hours.
- E. During REFUELING SHUTDOWN and COLD SHUTDOWN the following valves in the affected unit shall be locked, sealed, or otherwise secured in the closed position except during planned dilution or makeup activities:
1. During Unit 1 REFUELING SHUTDOWN and COLD SHUTDOWN:
 - a. Valve 1-CH-223, or
 - b. Valves 1-CH-212, 1-CH-215, and 1-CH-218.
 2. During Unit 2 REFUELING SHUTDOWN and COLD SHUTDOWN:
 - a. Valve 2-CH-223, or
 - b. Valves 2-CH-212, 2-CH-215, and 2-CH-218.
 3. Following a planned dilution or makeup activities, the valves listed in Specifications 3.2.E.1 and 3.2.E.2 above, for the affected unit, shall be locked, sealed, or otherwise secured in the closed position within 15 minutes.

Basis

The Chemical and Volume Control System provides control of the Reactor Coolant System boron inventory. This is normally accomplished by using boric acid transfer pumps which discharge to the suction of each unit's charging pumps. The Chemical and Volume Control System contains four boric acid transfer pumps. Two of these pumps are normally assigned to each unit but, valving and piping arrangements allow pumps to be shared such that three out of four pumps can service either unit. An alternate (not normally used) method of boration is to use the charging pumps taking suction directly from the refueling water storage tank. There are two sources of borated water available to the suction of the charging pumps through two different paths; one from the refueling water storage tank and one from the discharge of the boric acid transfer pumps.

- A. The boric acid transfer pumps can deliver the boric acid tank contents (7.0% solution of boric acid) to the charging pumps.
- B. The charging pumps can take suction from the volume control tank, the boric acid transfer pumps and the refueling water storage tank. Reference is made to Technical Specification 3.3.

The quantity of boric acid in storage from either the boric acid tanks or the refueling water storage tank is sufficient to borate the reactor coolant in order to reach COLD SHUTDOWN at any time during core life.

Approximately 6000 gallons of the 7.0% solution of boric acid are required to meet COLD SHUTDOWN conditions. Thus, a minimum of 6000 gallons in the boric acid tank is specified. An upper concentration limit of 8.5% boric acid in the tank is specified to maintain solution solubility at the specified low temperature limit of 112 degrees F.

The Boric Acid Tank(s) are supplied with level alarms which would annunciate if a leak in the system occurred.

For one-unit operation, it is required to maintain available one charging pump with a source of borated water on the opposite unit, the associated piping and valving, and the associated instrumentation and controls in order to maintain the capability to cross-connect the two unit's charging pump discharge headers. In the event the operating unit's charging pumps become inoperable, this permits the opposite unit's charging pump to be used to bring the disabled unit to COLD SHUTDOWN conditions. Initially, the need for the charging pump cross-connect was identified during fire protection reviews.

The requirement that certain valves remain closed during REFUELING SHUTDOWN and COLD SHUTDOWN conditions, except for planned boron dilution or makeup activities, provides assurance that an inadvertent boron dilution will not occur. This specification is not applicable at INTERMEDIATE SHUTDOWN, HOT SHUTDOWN, REACTOR CRITICAL, or POWER OPERATION.

References

UFSAR Sections 9.1 Chemical and Volume Control System

3.3 SAFETY INJECTION SYSTEM

Applicability

Applies to the operating status of the Safety Injection System.

Objective

To define those limiting conditions for operation that are necessary to provide sufficient borated water to remove decay heat from the core in emergency situations.

Specifications

- A. A reactor shall not be made critical unless:
 - 1. The refueling water storage tank (RWST) is OPERABLE with:
 - a. A contained borated water volume of at least 387,100 gallons.
 - b. A boron concentration of at least 2300 ppm but not greater than 2500 ppm.
 - c. A maximum solution temperature of 45° F.
 - 2. Each safety injection accumulator is OPERABLE with:
 - a. A borated water volume of at least 975 cubic feet but not greater than 1025 cubic feet.
 - b. A boron concentration of at least 2250 ppm.
 - c. A nitrogen cover-pressure of at least 600 psia.
 - d. The safety injection accumulator discharge motor operated valve blocked open by de-energizing AC power and the valves's breaker locked, sealed or otherwise secured in the open position when the reactor coolant system pressure is greater than 1000 psig.

3. Two safety injection subsystems are OPERABLE with subsystems comprised of:
 - a. One OPERABLE high head charging pump.
 - b. One OPERABLE low head safety injection pump.
 - c. An OPERABLE flow path capable of transferring fluid to the Reactor Coolant System when taking suction from the refueling water storage tank on a safety injection signal or from the containment sump when suction is transferred during the recirculation phase of operation.
- B. The requirements of Specification 3.3.A may be modified as follows:
1. With the refueling water storage tank inoperable, restore the tank to OPERABLE status within one hour or place the reactor in HOT SHUTDOWN within the next 6 hours.
 - a. For conditions where the RWST is inoperable due to boron concentration or solution temperature not being within the limits of Specification 3.3.A.1, restore the parameters to within specified limits in 8 hours or place the reactor in HOT SHUTDOWN within the next 6 hours.
 2. With one safety injection accumulator inoperable, restore the accumulator to OPERABLE status within 4 hours or place the reactor in HOT SHUTDOWN within the next 6 hours.
 - a. For conditions where one safety injection accumulator is inoperable due to boron concentration not being within the limits of Specification 3.3.A.2, restore the accumulator to within specified limits in 72 hours or place the reactor in HOT SHUTDOWN within the next 6 hours.
 - b. Power may be restored to any valve or breaker referenced in Specification 3.3.A.2.d for the purpose of testing or

maintenance provided that not more than one valve has power restored, and the testing and maintenance is completed and power removed within 4 hours.

3. With one safety injection subsystem inoperable, restore the inoperable subsystem to OPERABLE status within 72 hours or place the reactor in HOT SHUTDOWN within the next 6 hours.
- C. If the requirements of Specification 3.3.A are not satisfied as allowed by Specification 3.3.B, the reactor shall be placed in COLD SHUTDOWN in the following 30 hours.

Basis

The normal procedure for starting the reactor is, first, to heat the reactor coolant to near operating temperature by running the reactor coolant pumps. The reactor is then made critical by withdrawing control rods and/or diluting boron in the coolant. With this mode of startup the Safety Injection System is required to be OPERABLE as specified. During LOW POWER PHYSICS TESTS there is a negligible amount of energy stored in the system. Therefore, an accident comparable in severity to the Design Basis Accident is not possible, and the full capacity of the Safety Injection System would not be necessary.

The OPERABLE status of the subsystems is to be demonstrated by periodic tests, detailed in TS Section 4.11. A large fraction of these tests are performed while the reactor is operating in the power range. If a subsystem is found to be inoperable, it will be possible in most cases to effect repairs and restore the subsystem to full operability within a relatively short time. A subsystem being inoperable does not negate the ability of the system to perform its function, but it reduces the redundancy provided in the reactor design and thereby limits the ability to tolerate additional subsystem failures. In some cases, additional components (i.e., charging pumps) are installed to allow a component to be inoperable without affecting system redundancy.

If the inoperable subsystem is not repaired within the specified allowable time period, the reactor will initially be placed in HOT SHUTDOWN to provide for reduction of the decay heat from the fuel, and consequent reduction of cooling requirements after a postulated loss-of-coolant accident. If the malfunction(s) is not corrected the reactor will be placed in COLD SHUTDOWN following normal shutdown and cooldown procedures.

Assuming the reactor has been operating at full RATED POWER for at least 100 days, the magnitude of the decay heat production decreases as follows after a unit trip from full RATED POWER.

| <u>Time After Shutdown</u> | <u>Decay Heat. (% of RATED POWER)</u> |
|----------------------------|---------------------------------------|
| 1 min. | 3.7 |
| 30 min. | 1.6 |
| 1 hour | 1.3 |
| 8 hours | 0.75 |
| 48 hours | 0.48 |

Thus, the requirement for core cooling in case of a postulated loss-of-coolant accident, while in HOT SHUTDOWN, is reduced by orders of magnitude below the requirements for handling a postulated loss-of-coolant accident occurring during POWER OPERATION. Placing and maintaining the reactor in HOT SHUTDOWN significantly reduces the potential consequences of a loss-of-coolant accident, allows access to some of the Safety Injection System components in order to effect repairs, and minimizes the plant's exposure to thermal cycling.

Failure to complete repairs within 72 hours is considered indicative of unforeseen problems (i.e., possibly the need of major maintenance). In such a case, the reactor is placed in COLD SHUTDOWN.

The accumulators are able to accept leakage from the Reactor Coolant System without any effect on their operability. Allowable inleakage is based on the volume of water that can be added to the initial amount without exceeding the volume given in Specification 3.3.A.2.

The accumulators (one for each loop) discharge into the cold leg of the reactor coolant piping when Reactor Coolant System pressure decreases below accumulator pressure, thus assuring rapid core cooling for large breaks. The line from each accumulator is provided with a motor-operated valve to isolate the accumulator during reactor start-up and shutdown to preclude the discharge of the contents of the accumulator when not required.

Accumulator Motor Operated Discharge Isolation Valves

| <u>Unit No. 1</u> | <u>Unit No. 2</u> |
|-------------------|-------------------|
| MOV 1865A | MOV 2865A |
| MOV 1865B | MOV 2865B |
| MOV 1865C | MOV 2865C |

However, to assure that the accumulator valves satisfy the single failure criteria, they will be locked, sealed or otherwise secured open by de-energizing the valve motor operators when the reactor coolant pressure exceeds 1000 psig. The operating pressure of the Reactor Coolant System is 2235* psig and accumulator injection is initiated when this pressure drops to 600 psia. De-energizing the motor operator when the pressure exceeds 1000 psig allows sufficient time during normal startup operation to perform the actions required to de-energize the valve. This procedure will assure that there is an OPERABLE flow path from each accumulator to the Reactor Coolant System during POWER OPERATION and that safety injection can be accomplished.

The removal of power from the valves listed above will assure that the systems of which they are a part satisfy the single failure criterion.

* For Unit 2 Cycle 12, Reactor Coolant System nominal operating pressure may be reduced to 2135 psig.

- B. During POWER OPERATION the requirements of Specification 3.4.A may be modified to allow a subsystem or the following components to be inoperable. If the components are not restored to meet the requirements of Specification 3.4.A within the time period specified below, the reactor shall be placed in HOT SHUTDOWN within the next 6 hours. If the requirements of Specification 3.4.A are not satisfied within an additional 48 hours the reactor shall be placed in COLD SHUTDOWN within the following 30 hours.
1. One Containment Spray Subsystem may be inoperable, provided immediate attention is directed to making repairs and the subsystem can be restored to OPERABLE status within 24 hours.
 2. One outside Recirculation Spray Subsystem may be inoperable, provided immediate attention is directed to making repairs and the subsystem can be restored to OPERABLE status within 24 hours.
 3. One inside Recirculation Spray Subsystem may be inoperable, provided immediate attention is directed to making repairs and the subsystem can be restored to OPERABLE status within 72 hours.
 4. Refueling Water Storage Tank volume may be outside the limits of Specification 3.4.A.3 provided it is restored to within limits within one hour.
 - a. For conditions where the RWST is inoperable due to boron concentration or solution temperature not being within the limits specified, restore the parameters to within specified limits in 8 hours.

In addition to supplying water to the Containment Spray System, the refueling water storage tank is also a source of water for safety injection following an accident. This water is borated to a concentration which assures reactor shutdown by approximately 5 percent $\Delta k/k$ when all control rods assemblies are inserted and when the reactor is cooled down for refueling.

References

| | |
|----------------------|--|
| UFSAR Section 4 | Reactor Coolant System |
| UFSAR Section 6.3.1 | Containment Spray Subsystem |
| UFSAR Section 6.3.1 | Recirculation Spray Pumps and Coolers |
| UFSAR Section 6.3.1 | Refueling Water Chemical Addition Tank |
| UFSAR Section 6.3.1 | Refueling Water Storage Tank |
| UFSAR Section 14.5.2 | Design Basis Accident |
| UFSAR Section 14.5.5 | Containment Transient Analysis |

**ALLOWABLE AIR PARTIAL PRESSURE
SURRY POWER STATION UNITS 1 AND 2**

TC MINIMUM = 100 °F

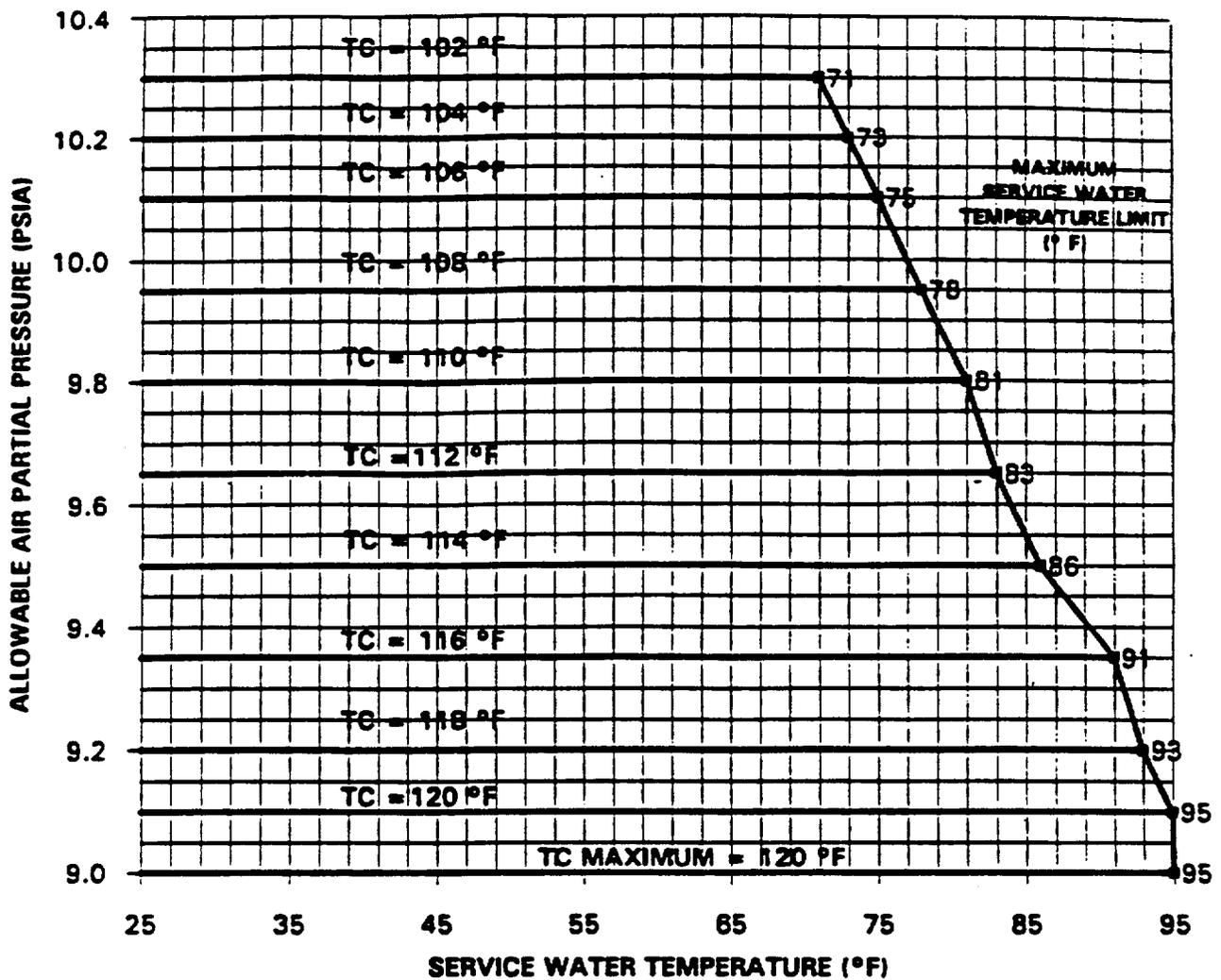


FIGURE NOTATION

TC - Containment average temperature

FIGURE NOTES

1. Refueling Water Storage Tank temperature $\leq 45^{\circ}\text{F}$, with an 8 hour AOT.
2. Allowable operating air partial pressure in the containment is a function of service water temperature.
3. Horizontal lines designate allowable air partial pressure per given containment average temperature.
4. Each containment temperature line is a maximum for the given air partial pressure.

3.13 COMPONENT COOLING SYSTEM

Applicability

Applies to the operational status of all subsystems of the Component Cooling System. The Component Cooling System consists of the Component Cooling Water Subsystem, Chilled Component Water Subsystem, Chilled Water Subsystem, and Neutron Shield Tank Cooling Water Subsystem.

Objective

To define limiting conditions for each subsystem of the Component Cooling System necessary to assure safe operation of each reactor unit of the station during startup, POWER OPERATION, or cooldown.

Specifications

- A. When a unit's Reactor Coolant System temperature and pressure exceed 350°F and 450 psig, respectively, or when a unit's reactor is critical operating conditions for the Component Cooling Water Subsystem shall be as follows:
1. For one unit operation, two component cooling water pumps and heat exchangers shall be OPERABLE.
 2. For two unit operation, three component cooling water pumps and heat exchangers shall be OPERABLE.
 3. The Component Cooling Water Subsystem shall be OPERABLE for immediate supply of cooling water to the following components, if required:
 - a. Two OPERABLE residual heat removal heat exchangers.
- B. During POWER OPERATION, Specification A-1, A-2, or A-3 above may be modified to allow one of the required components to be inoperable provided immediate attention is directed to making repairs. If the system is not restored within 24 hours to the requirements of Specification A-1,

A-2, or A-3, an operating reactor shall be placed in HOT SHUTDOWN within the next 6 hours. If the repairs are not completed within an additional 48 hours, the affected reactor shall be placed in COLD SHUTDOWN within the following 30 hours.

- C. Whenever the component cooling water radiation monitor is inoperable, the surge tank vent valve shall remain closed.

Basis

The Component Cooling System is an intermediate cooling system which serves both reactor units. It transfers heat from heat exchangers containing reactor coolant, other radioactive liquids, and other fluids to the Service Water System. The Component Cooling System is designed to (1) provide cooling water for the removal of residual and sensible heat from the Reactor Coolant System during shutdown, cooldown, and startup, (2) cool the containment recirculation air coolers and the reactor coolant pump motor coolers, (3) cool the letdown flow in the Chemical and Volume Control System during POWER OPERATION, and during residual heat removal for continued purification, (4) cool the reactor coolant pump seal water return flow, (5) provide cooling water for the neutron shield tank and (6) provide cooling to dissipate heat from other reactor unit components.

The Component Cooling Water Subsystem has four component cooling water pumps and four component cooling water heat exchangers. Each of the component cooling water heat exchangers is designed to remove during normal operation the entire heat load from one unit plus one half of the heat load common to both units. Thus, one component cooling water pump and one component cooling water heat exchanger are required for each unit which is at POWER OPERATION. Two pumps and two heat exchangers are normally operated during the removal of residual and sensible heat from one unit during cooldown. Failure of a single component may extend the time required for cooldown but does not affect the safe operation of the station.

References

UFSAR Section 5.3, Containment Systems
UFSAR Section 9.4, Component Cooling System
UFSAR Section 15.5.1.2, Containment Design Criteria

The diesel generators function as an on-site back-up system to supply the emergency buses. Each emergency bus provides power to the following operating Engineered Safeguards equipment:

- A. One containment spray pump
- B. One charging pump
- C. One low head safety injection pump
- D. One recirculation spray pump inside containment
- E. One recirculation spray pump outside containment
- F. One containment vacuum pump
- G. One motor-driven auxiliary steam generator feedwater pump
- H. One motor control center for valves, instruments, control air compressor, fuel oil pumps, etc.
- I. Control area air conditioning equipment - four air recirculating units, two water chilling units, one service water pump, and two chilled water circulating pumps
- J. One charging pump service water pump

TABLE 4.1-1 (Continued)

MINIMUM FREQUENCIES FOR CHECK, CALIBRATIONS, AND TEST OF INSTRUMENT CHANNELS

| <u>Channel Description</u> | <u>Check</u> | <u>Calibrate</u> | <u>Test</u> | <u>Remarks</u> |
|---|----------------|------------------|-------------|---|
| 10. Rod Position Bank Counters | S(1,2) Q(3) | N.A. | N.A. | 1) Each six inches of rod motion when data logger is out of service 2) With analog rod position 3) For the control banks, the bench-board indicators shall be checked against the output of the bank overlap unit |
| 11. Steam Generator Level | S | R | M | |
| 12. Charging Flow | N.A. | R | N.A. | |
| 13. Residual Heat Removal Pump Flow | N.A. | R | N.A. | |
| 14. Boric Acid Tank Level | *D | R | N.A. | |
| 15. Recirculation Mode transfer | | | | |
| a. Refueling Water Storage Tank Level-Low | S | R | M | |
| b. Automatic Actuation Logic and Actuation Relays | N.A. | N.A. | M | |
| 16. Volume Control Tank Level | N.A. | R | N.A. | |
| 17. Reactor Containment Pressure-CLS | *D | R | M(1) | 1) Isolation valve signal and spray signal |
| 18. Boric Acid Control | N.A. | R | N.A. | |
| 19. Containment Sump Level | N.A. | R | N.A. | |
| 20. Deleted | | | | |
| 21. Containment Pressure-Vacuum Pump System | S | R | N.A. | |
| 22. Steam Line Pressure | S | R | M | |

Amendment Nos. 199 and 199

TS 4.1-7

TABLE 4.1-2A

MINIMUM FREQUENCY FOR EQUIPMENT TESTS

| | <u>DESCRIPTION</u> | <u>TEST</u> | <u>FREQUENCY</u> | <u>FSAR SECTION REFERENCE</u> |
|-----|--|--|--|-------------------------------|
| 1. | Control Rod Assemblies | Rod drop times of all full length rods at hot conditions | Prior to reactor criticality: a. For all rods following each removal of the reactor vessel head b. For specially affected individual rods following any maintenance on or modification to the control rod drive system which could affect the drop time of those specific rods, and c. Each refueling shutdown. | 7 |
| 2. | Control Rod Assemblies | Partial movement of all rods | Quarterly | 7 |
| 3. | Refueling Water Chemical Addition Tank | Functional | Each refueling shutdown | 6 |
| 4. | Pressurizer Safety Valves | Setpoint | Per TS 4.0.5 | 4 |
| 5. | Main Steam Safety Valves | Setpoint | Per TS 4.0.5 | 10 |
| 6. | Containment Isolation Trip | * Functional | Each refueling shutdown | 5 |
| 7. | Refueling System Interlocks | * Functional | Prior to refueling | 9.12 |
| 8. | Service Water System | * Functional | Each refueling shutdown | 9.9 |
| 9. | Fire Protection Pump and Power Supply | Functional | Monthly | 9.10 |
| 10. | Primary System Leakage | * Evaluate | Daily | 4 |
| 11. | Diesel Fuel Supply | * Fuel Inventory | 5 days/week | 8.5 |
| 12. | Deleted | | | |
| 13. | Main Steam Line Trip Valves | Functional (Full Closure) | Before each startup (TS 4.7) The provisions of Specification 4.0.4 are not applicable. | 10 |

Amendment Nos. 199 and 199

TS 4.1-9b

TABLE 4.1-2A (CONTINUED)
MINIMUM FREQUENCY FOR EQUIPMENT TESTS

| <u>DESCRIPTION</u> | <u>TEST</u> | <u>FREQUENCY</u> | <u>UFSAR SECTION REFERENCE</u> |
|------------------------------------|---|---|--------------------------------|
| 19. Primary Coolant System | Functional | 1. Periodic leakage testing ^{(a)(b)} on each valve listed in Specification 3.1.C.7a shall be accomplished prior to entering POWER OPERATION after every time the plant is placed in COLD SHUTDOWN for refueling, after each time the plant is placed in COLD SHUTDOWN for 72 hours if testing has not been accomplished in the preceding 9 months, and prior to returning the valve to service after maintenance, repair or replacement work is performed. | |
| 20. Containment Purge MOV Leakage | Functional | Semi-Annual (Unit at power or shutdown) if purge valves are operated during interval ^(c) | |
| 21. Containment Hydrogen Analyzers | a. CHANNEL FUNCTIONAL TEST b. CHANNEL CALIBRATION <ol style="list-style-type: none"> 1. Sample gas used: One volume percent ($\pm 0.25\%$) hydrogen, balance nitrogen Four volume percent ($\pm 0.25\%$) hydrogen, balance nitrogen 2. CHANNEL CALIBRATION will include startup and operation of the Heat Tracing System | Once per 92 days Once per 18 months | |
| 22. RCS Flow | Flow \geq 273,000 gpm | Once per refueling cycle | 14 |
| 23. Delete | | | |

(a) To satisfy ALARA requirements, leakage may be measured indirectly (as from the performance of pressure indicators) if accomplished in accordance with approved procedures and supported by computations showing that the method is capable of demonstrating valve compliance with the leakage criteria.

(b) Minimum differential test pressure shall not be below 150 psid.

(c) Refer to Section 4.4 for acceptance criteria.

* See Specification 4.1.D

Amendment Nos. 199 and 199

TABLE 4.1-2B

MINIMUM FREQUENCIES FOR SAMPLING TESTS

| <u>DESCRIPTION</u> | <u>TEST</u> | <u>FREQUENCY</u> | <u>FSAR SECTION REFERENCE</u> |
|---|--|--|-------------------------------|
| 1. Reactor Coolant Liquid Samples | Radio-Chemical Analysis ⁽¹⁾ | Monthly ⁽⁵⁾ | |
| | Gross Activity ⁽²⁾ | 5 days/week ⁽⁵⁾ | 9.1 |
| | Tritium Activity | Weekly ⁽⁵⁾ | 9.1 |
| | *Chemistry (CL, F & O ₂) | 5 days/week | 4 |
| | *Boron Concentration | Twice/week | 9.1 |
| | \bar{E} Determination | Semiannually ⁽³⁾ | |
| | DOSE EQUIVALENT I-131 | Once/2 weeks ⁽⁵⁾ | |
| | Radio-iodine Analysis (including I-131, I-133 & I-135) | Once/4 hours ⁽⁶⁾ and ⁽⁷⁾ below | |
| 2. Refueling Water Storage | Chemistry (Cl & F) | Weekly | 6 |
| 3. Boric Acid Tanks | *Boron Concentration | Twice/Week | 9.1 |
| 4. Chemical Additive Tank | NaOH Concentration | Monthly | 6 |
| 5. Spent Fuel Pit | *Boron Concentration | Monthly | 9.5 |
| 6. Secondary Coolant | Fifteen minute degassed b and q activity | Once/72 hours | 10.3 |
| | DOSE EQUIVALENT I-131 | Monthly ⁽⁴⁾ | |
| | | Semiannually ⁽⁸⁾ | |
| 7. Stack Gas Iodine and Particulate Samples | *I-131 and particulate radioactive releases | Weekly | |

*See Specification 4.1.D

- (1) A radiochemical analysis will be made to evaluate the following corrosion products: Cr-51, Fe-59, Mn-54, Co-58, and Co-60.
- (2) A gross beta-gamma degassed activity analysis shall consist of the quantitative measurement of the total radioactivity of the primary coolant in units of $\mu\text{Ci/cc}$.

2. By verifying that each motor-operated valve in the recirculation spray flow paths performs satisfactorily when tested in accordance with Specification 4.0.5.
 3. At least once per 10 years, coincident with the closest refueling outage, by performing an air or smoke flow test and verifying each spray nozzle is unobstructed.
- C. Each weight-loaded check valve in the containment spray and outside containment recirculation spray subsystems shall be demonstrated OPERABLE at least once each refueling period, by cycling the valve one complete cycle of full travel and verifying that each valve opens when the discharge line of the pump is pressurized with air and seats when a vacuum is applied.
- D. A visual inspection of the containment sump and the inside containment recirculation spray pump wells and the engineered safeguards suction inlets shall be performed at least once each refueling period and/or after major maintenance activities in the containment. The inspection should verify that the containment sump and pump wells are free of debris that could degrade system operation and that the sump components (i.e., trash racks, screens) are properly installed and show no sign of structural distress or excessive corrosion.

4.11 SAFETY INJECTION SYSTEM TESTS

Applicability

Applies to the operational testing of the Safety Injection System.

Objective

To verify that the Safety Injection System will respond promptly and perform its design functions, if required.

Specifications

- A. The refueling water storage tank (RWST) shall be demonstrated OPERABLE:
 - 1. At least once per day by verifying the RWST solution temperature.
 - 2. At least once per week by:
 - a. Verifying the RWST contained borated water volume, and
 - b. Verifying the RWST boron concentration.

- B. Each safety injection accumulator shall be demonstrated OPERABLE:
 - 1. At least once per 12 hours by:
 - a. Verifying the contained borated water volume is within specified limits, and
 - b. Verifying the nitrogen cover-pressure is within specified limits.

2. At least once per 31 days and within 6 hours after each solution volume increase of greater than or equal to 1% of tank volume by verifying the boron concentration of the accumulator solution.
 - a. This surveillance is not required when the volume increase makeup source is the RWST.

C. Each Safety Injection Subsystem shall be demonstrated OPERABLE:

1. By verifying, that on recirculation flow, each low head safety injection pump performs satisfactorily when tested in accordance with Specification 4.0.5.
2. By verifying that each charging pump performs satisfactorily when tested in accordance with Specification 4.0.5.
3. By verifying that each motor-operated valve in the safety injection flow path performs satisfactorily when tested in accordance with Specification 4.0.5.
4. Prior to POWER OPERATION by:

- a. Verifying that the following motor operated valves are blocked open by de-energizing AC power to the valves motor operator and tagging the breaker in the off position:

| <u>Unit 1</u> | <u>Unit 2</u> |
|---------------|---------------|
| MOV-1890C | MOV-2890C |

- b. Verifying that the following motor operated valves are blocked closed by de-energizing AC power to the valves motor operator and the breaker is locked, sealed or otherwise secured in the off position:

| <u>Unit 1</u> | <u>Unit 2</u> |
|---------------|---------------|
| MOV-1869A | MOV-2869A |
| MOV-1869B | MOV-2869B |
| MOV-1890A | MOV-2890A |
| MOV-1890B | MOV-2890B |

- c. Power may be restored to any valve or breaker referenced in Specifications 4.11.C.4.a and 4.11.C.4.b for the purpose of testing or maintenance provided that not more than one valve has power restored at one time, and the testing and maintenance is completed and power removed within 24 hours.
5. At least once per REFUELING SHUTDOWN by:
- a. Verifying that each automatic valve capable of receiving a safety injection signal, actuates to its correct position upon receipt of a safety injection test signal. The charging and low head safety injection pumps may be immobilized for this test.
 - b. Verifying that each charging pump and safety injection pump circuit breaker actuates to its correct position upon receipt of a safety injection test signal. The charging and low head safety injection pumps may be immobilized for this test.
 - c. Verifying, by visual inspection, that each low head safety injection pump suction inlet from the containment sump is free of debris that could degrade system operation. Perform each refueling outage and/or after major maintenance activities in the containment.

Basis

Complete system tests cannot be performed when the reactor is operating because a safety injection signal causes containment isolation. The method of assuring operability of these systems is therefore to combine system tests to be performed during refueling shutdowns, with more frequent component tests, which can be performed during reactor operation.

The system tests demonstrate proper automatic operation of the Safety Injection System. A test signal is applied to initiate automatic operation action and verification is made that the components receive the safety injection signal in the proper sequence. The test may be performed with the pumps blocked from starting. The test demonstrates the operation of the valves, pump circuit breakers, and automatic circuitry.

During reactor operation, the instrumentation which is depended on to initiate safety injection is checked periodically, and the initiating circuits are tested in accordance with Specification 4.1. In addition, the active components (pumps and valves) are to be periodically tested to check the operation of the starting circuits and to verify that the pumps are in satisfactory running order. The test interval is determined in accordance with ASME Section XI. The accumulators are a passive safeguard.

References

UFSAR Section 6.2, Safety Injection System



UNITED STATES
NUCLEAR REGULATORY COMMISSION

WASHINGTON, D.C. 20555-0001

SAFETY EVALUATION BY THE OFFICE OF NUCLEAR REACTOR REGULATION
RELATED TO AMENDMENT NO. 199 TO FACILITY OPERATING LICENSE NO. DPR-32
AND AMENDMENT NO. 199 TO FACILITY OPERATING LICENSE NO. DPR-37
VIRGINIA ELECTRIC AND POWER COMPANY
SURRY POWER STATION, UNIT NOS. 1 AND 2
DOCKET NOS. 50-280 AND 50-281

1.0 INTRODUCTION

By letter dated June 9, 1994, the Virginia Electric and Power Company (the licensee or VEPCO) requested a license amendment for the Surry Units 1 and 2 plants that would change the Technical Specifications (TS). The proposed changes would modify, in part, the Chemical and Volume Control System specifications and the Safety Injection System TS.

The proposed changes to the TS are in part due to a modification to the operation of the charging pumps. The Surry Power Station's charging pumps are dual purpose pumps. As components of the Chemical and Volume Control System (CVCS), they provide normal charging to the Reactor Coolant System (RCS). As part of the emergency core cooling system, they provide high head safety injection when required. The pump manufacturer, Byron Jackson, has proposed a once-through process flow cooling arrangement for the Surry charging pump mechanical seals. This modification eliminates the need for the existing mechanical seal coolers, charging pump component cooling subsystem and intermediate seal coolers, by providing a seal cooling supply from the low pressure stages of the charging pump casing. Elimination of the charging pump component cooling subsystem and implementation of the proposed modifications requires changes to Surry TS.

Changes are proposed to restructure the CVCS specifications and the Safety Injection System (SI) specifications consistent with the proposed modification of the charging pump seal cooling, elimination of the charging pump component cooling subsystem, and prior removal of the boron injection tank.

The requirement to maintain two channels of heat tracing operable is being deleted and a minimum boric acid solution temperature is being specified.

The specifications have been restructured to address operability requirements on a subsystem basis rather than an individual component basis. The restructuring of the Specifications continues to ensure that no single failure can disable both emergency core cooling trains and the criteria of 10 CFR 50.46 remain satisfied.

Certain requirements are being relocated or deleted as follows:

1. The Specification 3.3 requirement regarding RCS loop stop valves is being relocated to Specification 3.1, Reactor Coolant System.
2. The Specification 3.3 requirement for total system leakage outside containment is being deleted.
3. The requirement to position and remove AC power from specified SI System motor operated valves (existing Specifications 3.3.A.8 and 3.3A.9) is relocated to surveillance specification 4.11, SI System Tests.

Portions of the changes include certain line-item improvements identified in GL 93-05, Item 7.1, Item 7.4 and NUREG-1366. The licensee has proposed the following changes:

1. A surveillance requirement has been added (new Specification 4.11.B) to verify safety injection accumulator boron concentration, volume and nitrogen cover-pressure.
2. A requirement to verify boron concentration within 6 hours of a specified solution volume increase has been added but is not required when the volume increase makeup source is the reactor water storage tank (RWST). The minimum RWST boron concentration is equal to or greater than the minimum required safety injection accumulator boron concentration limit.
3. The SI accumulator instrument channel surveillance requirements for level and pressure will be deleted.

2.0 BACKGROUND

The CVCS is designed to provide boric acid solution through the charging pumps to the RCS for reactivity control and to compensate for minor leakage of reactor coolant. The CVCS also has the capability to achieve Cold Shutdown of both units from any operating condition with one control rod assembly withdrawn at any time in core life, and has the capability to achieve Refueling Shutdown from Cold Shutdown. The SI system functions to provide adequate emergency core cooling, thereby maintaining core geometry and clad integrity during the unlikely event of postulated accidents. This system includes passive safety injection accumulators, high head charging, and low-head injection subsystems. To ensure operability of the CVCS and SI systems, the pumps and various components are tested on a surveillance frequency as required by the TS.

In an evaluation documented in NUREG-1366, the NRC made a comprehensive examination of surveillance requirements in TS that require testing at power. The NRC staff found that, while the majority of testing at power is important,

safety can be improved, equipment degradation decreased, and an unnecessary burden on personnel resources eliminated by reducing the amount of testing at power that is required by TS. Based on the results of the evaluation documented in NUREG-1366, the NRC issued Generic Letter 93-05, dated September 27, 1993, which, as discussed below, identified certain line item improvements.

3.0 EVALUATION

The changes, which are described below, include: (1) modification of the high head charging pumps seal cooling subsystem, (2) restructuring of the CVCS and SI System Specifications, (3) relocation of certain specification requirements within existing specifications, (4) specification of a minimum boric acid solution temperature in lieu of heat tracing channel operability, and (5) minor wording changes which are administrative in nature for consistency in terminology, capitalization of defined terms and clarification.

3.1 Charging Pump

The passive design charging pump modification uses effluents from the charging pump low pressure stages to provide the function of the charging pump component cooling water subsystem. This modification provides for the elimination of the charging pump component cooling water subsystem including pumps, heat exchangers, piping, and support sundries. Based on the licensee's engineering evaluation of the manufacturer's proposed modification and the pump seal manufacturer's concurrence with the modification, they have determined this modification to be acceptable with no reduction in the pump's safety-related function. Therefore, there is no decrease in the systems ability to mitigate the consequences of any accident identified in the safety analysis report. The CVCS and SI System, including their subsystems and components, are required to be operable in accordance with the Specification 1.0.D definition of "operable," allowing for the elimination of redundant language regarding piping, valves and control board indication. The operability requirements of the common boric acid storage system were clarified with requirements for boric acid solution volume, concentration, and temperature specified to support operability on a subsystem basis.

The requirement for a charging pump from the opposite unit to be available (existing TS 3.2.B.1, 3.2.B.6, 3.2.E and footnote page TS 3.2-2) prior to reactor critical has been clarified. The requirements identifying availability of the opposite unit's charging pump and explaining its meaning, were previously identified in a footnote and throughout the specification. The availability requirements of the opposite unit's charging pumps are now included as a specific requirement within the specification (new specification 3.2.B.2).

Specification 3.2.F, addressing dilutions during refueling, shutdown, and cold shutdown conditions, is clarified. An administrative change is made to restructure the specification by numbering the requirement that the specified valves be locked, sealed, or otherwise secured within 15 minutes following planned dilutions and makeup activities (new specification 3.2.E.3).

Based on the NRC staff evaluation, we find the proposed changes acceptable.

3.2 Restructure of CVCS, SI and Associated Specifications

VEPCO stated that the changes proposed to restructure the CVCS and the SI system specifications are consistent with the proposed modifications of the charging pump seal cooling, and elimination of the charging pump component cooling subsystem. The proposed changes relate to the following:

3.2.1 Outage Times

An allowed outage time of 72 hours, as a reasonable time for repair of affected components, is specified for conditions where a CVCS subsystem or SI System subsystem becomes inoperable. This is consistent with NUREG-0453, NRC Memorandum, "Recommended Interim Revisions to LCOs for ECCS Components," dated December 1, 1975, and NUREG-1431. A reliability analysis (reference NRC memo above) has shown that the impact of having one subsystem inoperable is sufficiently small to justify continued operation for 72 hours. Following this guidance, VEPCO has deleted the presently specified allowed period of 48 hours between achieving Hot Shutdown and initiation of Cold Shutdown procedures. Therefore, the proposed changes do not increase the required allowed outage times to achieve Cold Shutdown.

Based on the NRC staff evaluation, we find the proposed changes acceptable.

3.2.2 Allowed Outage Times Engineering Evaluation

VEPCO stated that the allowed outage times are based upon engineering evaluation of the changes being made and are consistent with the safety analysis and NUREG-0452. Specific parameters for refueling water storage tank borated water volume, concentration, and temperature were added for consistency within the Specifications. An allowed outage time of 8 hours was added for conditions where the refueling water storage tank is inoperable due to the boron concentration or solution temperature not being within specified limits consistent with NUREG-1431. This is acceptable based on a safety analysis showing that the outage time of 8 hours does not impact the plant accident analysis. The refueling water storage tank contents remain available for injection or sprays during the 8-hour period allowed for restoring the temperature and boron concentration to within specified limits. The changes ensure that the refueling water storage tank remains capable of providing a sufficient supply of borated water for injection by the emergency core cooling system in the event of a loss of cooling accident (LOCA) and that the reactor will remain subcritical in Cold Shutdown consistent with LOCA analyses.

Clarification is made to TS Figure 3.8-1, Figure Notes, Item 1, by adding reference to the 8-hour allowed outage time for conditions where the RWST temperature is not within specified limits.

An allowed outage time of 1 hour is added for conditions where the RWST becomes inoperable due to volume. The allowed outage time of 1 hour is

consistent with SI specification 3.3.B.10 which allows the RWST to be inoperable for 1 hour. The allowed outage time of 1 hour is also consistent with NUREG-0452 for the boric acid flow path from the RWST to the RCS.

Based on the NRC staff evaluation, we find the proposed changes acceptable.

3.2.3 Line-item Improvements Identified in GL 93-05

The proposed changes include certain line-item improvements identified in GL 93-05. The requested changes to the SI accumulator surveillance requirements for boron concentration, boron solution volume, and nitrogen cover-pressure are consistent with GL 93-05, Item 7.1, Item 7.4 and NUREG-1366. An allowed outage time of 72 hours is specified for the condition where one accumulator is inoperable due to boron concentration not being within specified limits, consistent with NUREG-1431.

A surveillance requirement has been added which verifies the borated water volume and nitrogen cover-pressure at least once per 12 hours consistent with NUREG-1431 and GL 93-05, Item 7.4. This surveillance was previously performed each shift in accordance with Specification Table 4.1-1, Item 20. As identified in GL 93-05, Item 7.4, the NRC staff had recognized that accumulator instrumentation operability is not directly related to the capability of the SI accumulators to perform their safety function, and permitted the surveillance requirement for this instrumentation to be relocated from the TS. The SI accumulator instrumentation surveillance requirements will be maintained within station procedures in accordance with the administrative requirements of Specification 6.4.

An accumulator boron concentration surveillance of at least once per 31 days has been specified, consistent with NUREG-1431 and GL 93-05, Item 7.1. This surveillance was previously performed monthly in accordance with Specification Table 4.1-2B, Item 8. A surveillance requirement was added to verify boron concentration within 6 hours of each solution volume increase of greater than or equal to 1% of accumulator tank volume consistent with NUREG-1431 and GL 93-05, Item 7.1. As permitted in GL 93-05, Item 7.1, this surveillance is not required when the volume makeup source is the RWST.

Based on the NRC staff evaluation, we find the proposed changes acceptable.

3.3 Relocation of Certain Specification Requirements

To support restructuring of these specifications, certain requirements are being relocated as follows:

3.3.1 RCS Loop Stop Valves

The Specification 3.3 requirement regarding RCS loop stop valves is being relocated to Specification 3.1, Reactor Coolant System, with no change in the specified requirements. However, Section 3.1.A.4 is revised to add a requirement that during power operation specified loop stop valves shall have

AC power removed and the breakers tagged open.

Based on the NRC staff evaluation, we find the proposed changes acceptable.

3.3.2 Total System Leakage Outside of Containment

The Specification 3.3 requirement for total system leakage outside containment is being deleted. The requirements for reducing leakage from systems located outside containment are identified in administrative controls in Specification 6.4.K and Chapter 6 of the UFSAR. Deletion of this requirement and similar requirements in Specification 3.3.B.9, 3.4.A.6, 3.4.B.4, 4.5.B.4 and 4.11.A.4.d eliminates the existing confusion and redundancy, and maintains total uncollected system leakage requirements within existing administrative controls consistent with the requirements contained in Specification 6.4.K and with NUREG-0452.

Based on the NRC staff evaluation, we find the proposed changes acceptable.

3.3.3 Uncollected System Leakage

The NRC Safety Evaluation for Amendment 162 (Surry Unit 1) and Amendment 161 (Surry 2), regarding total system uncollected leakage, determined that the associated changes were "a non-required change" and that there are "no requirements in the Westinghouse Standardized Technical Specification for total leakage limits allowed for the Recirculation Spray (RS) System and for periodic verification of system leakage within limits for the RS and Safety Injection (SI) systems." Consequently, VEPCO proposes to delete the uncollected system leakage requirements in Specification 3.3.A.12, 3.3.B.9, 3.4.A.6, 3.4.B.4, 4.5.B.4 and 4.11.A.4.d and their associated Basis for the SI and the RS System.

Based on the NRC staff evaluation, we find the proposed changes acceptable.

3.3.4 Safety Injection System and Reactor Coolant System Motor Operated Valves

The requirement for certain SI system motor operated valves to be de-energized in a specified position prior to power operation is being relocated to the SI surveillance section, Specification 4.11, consistent with restructuring the SI specification and NUREG-0452 for similar valves. An administrative surveillance is added which involves tagging each valve's breaker in the off position once the valve has been properly positioned and de-energized. De-energizing these valves in their proper position and tagging the valves' breaker ensure that they cannot change position as a result of an active failure or be inadvertently misaligned. These actions ensure the flow path from the emergency core cooling pumps to the reactor coolant system is maintained and that misalignment of these valves does not render both emergency core cooling system trains inoperable.

Specification 3.3.A.8 and 3.3.A.9 requirements for removal of AC power to specified valves are relocated as an additional surveillance requirement. Surveillance Specification 4.11.C.4 is added with minor wording changes to specify additional verification requirements for tagging the valves' breakers to be locked, sealed, or otherwise secured in the off position. This is consistent with applicable portions of NUREG-0452 and NUREG-1431.

The requirement to have the SI accumulator discharge valves blocked open (existing Specification 3.3.A.10) has been appropriately relocated to the requirement for SI accumulator operability, with an additional requirement that the valves' breakers be locked, sealed, or otherwise secured in the open position (new Specification 3.3.A.2.d).

Reference to the SI accumulator discharge motor-operated valves receiving an open signal (page TS 3.3-7) is deleted. These valves are required by Specification (new Specification 3.3.A.2.d) to be de-energized in the open position when RCS pressure exceeds 1,000 psig. While de-energized, they do not receive an open signal, and do not require an open signal to perform their SI function.

The charging pump surveillance requirements (existing Specification 4.11.A.2), are changed to delete the words "on recirculation flow," and are renumbered (new Specification 4.11.C.2). During testing, these pumps are flow tested to the RCS. The motor-operated valve surveillance requirements (existing Specification 4.11.A.3) have not changed and are renumbered (new Specification 4.11.C.3).

A surveillance requirement has been added to demonstrate each SI subsystem is operable by verifying: (1) specified motor-operated valves are blocked open by de-energizing AC power to the valve operators (existing Specification 3.3.A.8), and (2) specified motor-operated valves are blocked closed by de-energizing AC power to the valve operators (existing Specification 3.3.A.9). An additional requirement is added for the valves' breakers to be locked, sealed or otherwise secured in the off position after de-energizing AC power.

The requirements for RCS loop isolation valves (existing Specification 3.3.A.11) have been relocated to Specification 3.1.A.4. A requirement is added to have the valves' breakers to be locked, sealed, or otherwise secured in the open position after AC power is removed.

Minor wording changes are made for consistency by using the terminology "actuates to its correct position upon receipt of a safety injection test signal" when referring to surveillance testing of automatic valves capable of receiving an SI signal and pump circuit breakers during refueling shutdown (new Specifications 4.11.C.5.a and 4.11.C.5.b).

Based on the NRC staff evaluation, we find the proposed changes acceptable.

3.4 Heat Tracing vs. Minimum Solution Temperature

The heat tracing requirements in Specification 3.3, Chemical and Volume Control System, existed to support operation of the boron injection tank and its higher boric acid concentrations and solution temperatures. The boric acid concentration was previously reduced and the boron injection tank (BIT) operability requirements were previously removed in Amendment 95 (Unit 1) and Amendment 95 (Unit 2). However, the heat tracing operability requirements of Specification 3.3 were not previously deleted when the boric acid concentration was reduced and the BIT operability requirements were removed. Chapter 9.1 of the UFSAR does not require heat tracing to be operable for proper functioning of the CVCS. Therefore, the licensee states that heat tracing is not required for the operability of the SI System nor does it affect the ability of the SI System to mitigate the consequences of any postulated accident identified in the safety analysis. It is therefore proposed to delete the requirement in Specification 3.3 to maintain two channels of heat tracing operable. However, a minimum boric acid solution temperature is specified.

In lieu of specifying heat tracing channel operability requirements in Specification 3.3, a minimum solution temperature is being specified consistent with NUREG-1431 for similar system parameters. The heat tracing will be maintained in accordance with station procedures and continue to be administratively controlled in accordance with Specification 6.4. Temperature monitoring circuitry is provided with automatic actuation of undertemperature and overtemperature alarms indicated in the Main Control Room. A minimum temperature limit of 112 degrees Fahrenheit ensures that the solution does not reach the boric acid precipitation point.

Based on the NRC staff evaluation, we find the proposed changes acceptable.

3.5 Administrative Changes

There are miscellaneous changes throughout the Technical Specifications for capitalization of defined terms, consistency in terminology, and clarity.

Clarification is made to TS Figure 3.8-1, Figure Notes, Item 1, by adding reference to the 8-hour allowed outage time for conditions where the RWST temperature is not within specified limits.

The licensee has stated that the restructuring of the CVCS and SI System specifications on a subsystem basis, as described above, maintains the capability of ensuring that the reactor can be made subcritical from any operating condition and provide sufficient shutdown margin to preclude inadvertent criticality when in the shutdown condition. Also, with the above changes the SI System subsystems continue to maintain sufficient boration capability to mitigate reactivity transients within the design limits associated with postulated accident conditions, including inadvertent depressurization, a loss-of-coolant accident, or steam line rupture. The two SI System subsystems ensure that sufficient emergency core cooling capability

will be available in the event of LOCA assuming the loss of one subsystem through any single failure consideration. Either subsystem operating in conjunction with the accumulators remains capable of supplying sufficient core cooling to limit the peak cladding temperatures within acceptable limits in accordance with the loss-of-coolant accident analysis.

The staff has found the above TS changes to be acceptable for the reasons explained above, including consistency with NUREG-0452, NUREG-1431, and GL-93-05.

4.0 STATE CONSULTATION

In accordance with the Commission's regulations, the Virginia State official was notified of the proposed issuance of the amendments. The State official had no comment.

5.0 ENVIRONMENTAL CONSIDERATION

These amendments change a requirement with respect to installation or use of a facility component located within the restricted area as defined in 10 CFR Part 20. The NRC staff has determined that the amendments involve no significant increase in the amounts, and no significant change in the types, of any effluents that may be released offsite, and that there is no significant increase in individual or cumulative occupational radiation exposure. The Commission has previously issued a proposed finding that these amendments involve no significant hazards consideration and there has been no public comment on such finding (59 FR 37089). Accordingly, these amendments meet the eligibility criteria for categorical exclusion set forth in 10 CFR 51.22(c)(9). Pursuant to 10 CFR 51.22(b) no environmental impact statement or environmental assessment need be prepared in connection with the issuance of these amendments.

6.0 CONCLUSION

The staff has reviewed the licensee's submittal to support the changes to the Technical Specifications related to the Chemical and Volume Control System and Safety Injection System. Our evaluation in Section 3.0 has found the TS changes to be acceptable.

The Commission has concluded, based on the considerations discussed above, that: (1) there is reasonable assurance that the health and safety of the public will not be endangered by operation in the proposed manner, (2) such activities will be conducted in compliance with the Commission's regulations, and (3) the issuance of these amendments will not be inimical to the common defense and security or to the health and safety of the public.

Principal Contributors: H. Balukjian and B. Buckley

Date: May 31, 1995