Indian Point 2 Model – Steam Generator Tube Rupture Sequences

Table 1 shows the top 100 SGTR sequences with the failed split fractions for each sequence.

Each sequence includes an SISF split fraction that simply indicates that the sequence involves a loss of coolant from the primary system. This split fraction is a flag and has no quantitative value. It should also be noted that the sequences are shown in groups of two with the only difference being the inclusion of a SWS1 split fraction in one sequence of each pair. This SWS1 split fraction is required to properly reflect the fact that Indian Point 2 has two separate service water headers, either of which could be aligned to the essential or non-essential header at a given time. The two sequences therefore represent identical scenarios except that in one sequence, service water pumps 21, 22 and 23 are aligned to the essential header and in the other sequence, service water pumps 24, 25 and 26 are aligned to the essential header. Since either plant configuration is equally likely, the value of SWS1 is 0.5 and the sum of the two sequences represents the complete scenario.

Those sequences which are assigned to Plant Damage State 48A represent core damage sequences with an un-isolated secondary side while those sequences assigned to Plant Damage State 48B represent core damage sequences with the release through a modulating relief valve allowing radionuclide deposition and partitioning. Based on the expected core inventory release fractions associated with the two plant damage states, Plant Damage State 48B involves sufficient deposition and partitioning a large early release. The Plant Damage State totals in the baseline model are 1.35E-7 for PDS 48A and 8.7E-7 for PDS 48B.

Table 2 provides a more detailed description of the failures and successes included in the dominant SGTR sequences. Figure 3.1-5 of the Indian Point 2 IPE provides the SGTR event tree and the top events included in that tree. Those events are:

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- RW Refueling Water Storage Tank availability
- HP High Pressure Injection
- L1 Auxiliary Feedwater
- O3 Operator cools down and depressurizes without AFW
- OS Operator stops AFW to ruptured SG and isolates generator
- O4 Operator cools down and depressurizes with AFW before overfill
- O5 Operator cools down and depressurizes following overfill
- SO Isolation of the steam generator after overfill
- MU RWST makeup following successful depressurization
- AS Accumulator availability
- LP Low Pressure Injection
- LR Low Pressure Recirculation (Shut Down Cooling)
- RH Recirculation Heat Removal

Table 1						
Rank	Baseline	Conditional	Failed Split Fractions	Plant		
	SGTR CDF	SGTR CDF		Damage State		
1	2.54E-07	2E-05	//SISF/041*05A	PDS48E		
2	2.54E-07	2E-05	//SWS1*SISF/041*05A	PDS48		
3	8.59E-08	6.6E-06	//SWS1*SISF/OS1*O5E	PDS48		
4	8.59E-08	6.6E-06	//SISF/OS1*05E	PDS48		
5	5.06E-08	3.9E-06	//SISF/HP3*041*05G	PDS48		
6	5.06E-08	3.9E-06	//SWS1*SISF/HP3*O41*O5G	PDS48		
7	3.03E-08	2.3E-06	//SISF/OS1*SO1*LR2	PDS48/		
8	3.03E-08	2.3E-06	//SWS1*SISF/OS1*SO1*LR2	PDS48		
9	2.18E-08	1.7E-06	I/SWS1*SISF/HP3*L14	PDS48		
10	2.18E-08	1.7E-06	//SISF/HP3*L14	PDS48		
11	7.23E-09	5.6E-07	//SISF/OS1*05E*SO3	PDS48/		
12	7.23E-09	5.6E-07	//SWS1*SISF/OS1*O5E*SO3	PDS48		
13	6.48E-09	5E-07	//SWS1*SISF/RW2*OS1	PDS48/		
14	6.48E-09	5E-07	//SISF/RW2*OS1	PDS48/		
15	6.31E-09	4.9E-07	//SISF/OS1*S01*MU1	PDS48		
16	6.31E-09	4.9E-07	//SWS1*SISF/OS1*SO1*MU1	PDS48		
17	4.89E-09	3.8E-07	//SWS1*SISF/RW2*041	PDS48		
18	4.89E-09	3.8E-07	//SISF/RW2*O41	PDS48		
19	4.85E-09	3.7E-07	//SISF/L11*O31	PDS48		
20	4.85E-09	3.7E-07	//SWS1*SISF/L11*O31	PDS48		
21	3.18E-09	2.4E-07	//SISF/HP3*OS1*SO1	PDS48		
22	3.18E-09	2.4E-07	//SWS1*SISF/HP3*OS1*SO1	PDS48		
23	2.27E-09	1.7E-07	//SISF/041*S02*LR2	PDS48		
24	2.27E-09	1.7E-07	//SWS1*SISF/041*S02*LR2	PDS48		
25	2.23E-09	1.7E-07	//EA1B*SISF/041*05A	PDS48		
26	2.23E-09	1.7E-07	//EA1B*SWS1*SISF/041*05A	PDS48		
27	2.23E-09	1.7E-07	//EB1B*SISF/041*05A	PDS48		
28	2.23E-09	1.7E-07	//EB1B*SWS1*SISF/041*05A /	PDS48		
29	2.00E-09	1.5E-07	//EA1B*EBCB*SISF/HP6*O41*O5G	PDS48		
30	2.00E-09	1.5E-07	//EA1B*EBCB*SWS1*SISF/HP6*O41*O5G	PDS48		
31	1.30E-09	1E-07	//SISF/L11*SO4	PDS48		
32	1.30E-09	1E-07	//SWS1*SISF/L11*SO4	PDS48		
33	1.30E-09	1E-07	/MC26C1/SISF/O41*O5A	PDS48		
34	1.30E-09	1E-07	/MC26C1/SWS1*SISF/041*05A	PDS48		
35	9.89E-10	7.6E-08	//SISF/L11*LR4L	PDS48		
36	9.89E-10	7.6E-08	//SWS1*SISF/L11*LR4L	PDS48		
37	9.21E-10	7.1E-08	//SWS1*SISF/HP3*OS1*O53	PDS48		
38	9.21E-10	7.1E-08	//SISF/HP3*OS1*O53	PDS48		
39	9.03E-10	6.9E-08	//SISF/041*05A*S02	PDS48		
40	9.03E-10	6.9E-08	//SWS1*SISF/041*05A*S02	PDS48		
41	8.65E-10	6.7E-08	//EA1B*EBCB*SISF/HP6*L14	PDS48		
42	8.65E-10	6.7E-08	//EA1B*EBCB*SWS1*SISF/HP6*L14	PDS48		
43	7.55E-10	5.8E-08	//EA1B*SISF/OS1*O5E	PDS48 PDS48		
44	7.55E-10	5.8E-08				
45	7.55E-10	5.8E-08	-08 //EB1B*SISF/OS1*O5E			
46	7.55E-10	5.8E-08	08 //EB1B*SWS1*SISF/OS1*O5E			
47	6.08E-10	4.7E-08	08 //SWS1*SISF/HP3*OS1*LR2			
48	6.08E-10	4.7E-08	//SISF/HP3*OS1*LR2	PDS48		
49	4.73E-10	3.6E-08	//SISF/O41*SO2*MU1	PDS48		
50	4.73E-10	3.6E-08	//SWS1*SISF/041*S02*MU1	PDS48		
51	4.56E-10	3.5E-08	/MC26A1/SISF/OS1*SO1*LRF	PDS48		
52	4.56E-10	3.5E-08	/MC26A1/SWS1*SISF/OS1*SO1*LRF	PDS48		

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	Table 1						
Rank	Baseline SGTR CDF	Conditional SGTR CDF	Failed Split Fractions				
53	4.56E-10	3.5E-08	/MC26B1/SISF/OS1*SO1*LRF	PC			
54	4.56E-10	3.5E-08	/MC26B1/SWS1*SISF/OS1*SO1*LRF	P			
55	4.45E-10	3.4E-08	//EA1B*SISF/HP3*O41*O5G	PL			
56	4.45E-10	3.4E-08	//EA1B*SWS1*SISF/HP3*O41*O5G	P			
57	4.45E-10	3.4E-08	//EB1B*SISF/HP3*O41*O5G	PC			
58	4.45E-10	3.4E-08	//EB1B*SWS1*SISF/HP3*O41*O5G	P			
59	4.39E-10	3.4E-08	/MC26C1/SISF/OS1*O5E	P			
60	4.39E-10	3.4E-08	/MC26C1/SWS1*SISF/OS1*O5E	PI			
61	4.28E-10	3.3E-08	//SWS1*SISF*CC1/OS1*SO1*RHF	P			
62	4.28E-10	3.3E-08	//SISF*CC1/OS1*SO1*RHF	P			
63	3.48E-10	2.7E-08	//EA1B*EBCB*SISF/HP6*OS1*LP10	P			
64	3.48E-10	2.7E-08	//EA1B*EBCB*SWS1*SISF/HP6*OS1*LP10	P			
65	3.38E-10	2.6E-08	/X31*G2F/SISF/O41*O5A	P			
66	3.38E-10	2.6E-08	/X31*G2F/SWS1*SISF/O41*O5A	P			
67	3.14E-10	2.4E-08	/W21*G2F/SISF/O41*O5A	PE			
68	3.14E-10	2.4E-08	W21*G2F/SWS1*SISF/O41*O5A	PL			
69	2.66E-10	2E-08	//EA1B*SISF/OS1*SO1*LR2	P			
70	2.66E-10	2E-08	//EA1B*SWS1*SISF/OS1*SO1*LR2	PI			
71	2.66E-10	2E-08	//EB1B*SISF/OS1*SO1*LR2	P			
72	2.66E-10	2E-08	//EB1B*SWS1*SISF/OS1*SO1*LR2 /MC26C1/SISF/HP3*O41*O5G				
73	2.59E-10	2E-08					
74	2.59E-10	2E-08	/MC26C1/SWS1*SISF/HP3*O41*O5G	P			
75	1.92E-10	1.5E-08	//EA1B*SISF/HP3*L14	P			
76	1.92E-10	1.5E-08	//EA1B*SWS1*SISF/HP3*L14	PI			
77	1.92E-10	1.5E-08	//EB1B*SISF/HP3*L14	PI			
78	1.92E-10	1.5E-08	//EB1B*SWS1*SISF/HP3*L14	PI			
79	1.80E-10	1.4E-08	//SISF/HP3*041*05G*S02	P			
80	1.80E-10	1.4E-08	//SWS1*SISF/HP3*O41*O5G*SO2	PI			
81	1.72E-10	1.3E-08	//SWS1*SISF/HP3*L14*SO5	PI			
82	1.72E-10	1.3E-08	//SISF/HP3*L14*SO5	PI			
83	1.55E-10	1.2E-08	/MC26C1/SISF/OS1*SO1*LR2	PI			
84	1.55E-10	1.2E-08	/MC26C1/SWS1*SISF/OS1*SO1*LR2	PI			
85	1.28E-10	9.8E-09	/Z61*X3F*G2F*G3E*A6F*A3F*MC26BF*MC26CF*MC27F/SWS1*SISF/L13*LRF	PI			
86	1.27E-10	9.8E-09	/Z61*X3F*G2F*G3E*A6F*A3F*MC26BF*MC26CF*MC27F/SISF*SAF/L13*LRF	P			
87	1.27E-10	9.8E-09	//SWS1*SISF/HP3*OS1*AS1	PI			
88	1.27E-10	9.8E-09	//SISF/HP3*OS1*AS1	PI			
89	1.25E-10	9.6E-09	//SISF/HP3*O41*LR2	PI			
90	1.25E-10	9.6E-09	//SWS1*SISF/HP3*O41*LR2	P			
91	1.24E-10	9.5E-09	//SISF/OS1*SO1*RH1	P			
92	1.24E-10	9.5E-09	//SWS1*SISF/OS1*SO1*RH1	P			
93	1.15E-10	8.8E-09	/X31*G2F/SISF/OS1*O5E	P			
94	1.15E-10	8.8E-09	/X31*G2F/SWS1*SISF/OS1*O5E	P			
95	1.13E-10	8.7E-09	//EA1B*EBCB*SISF/HP6*OS1*SO1	P			
96	1.13E-10	8.7E-09	//EA1B*EBCB*SWS1*SISF/HP6*OS1*SO1	P			
97	1.12E-10	8.6E-09	/MC26C1/SISF/HP3*L14	P			
98	1.12E-10	8.6E-09	/MC26C1/SWS1*SISF/HP3*L14	P			
99	1.06E-10	8.2E-09	/W21*G2F/SISF/OS1*O5E	PI			
100	1.06E-10	8.2E-09	/W21*G2F/SWS1*SISF/OS1*O5E	P			

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	Table 2				
Rank	Sequence	Sequence CDF	Discussion of Split Fractions		
1 2	//SISF/O41*O5A //SWS1*SISF/O41*O5A	2.54E-07 2.54E-07	In this sequence, the operator has successfully isolated the SG and terminated auxiliary feedwater flow to the ruptured steam generator (Top Event OS). Following successful isolation, the operator must still depressurize and cool down the RCS (Split Fraction O41). In this sequence, he fails to do so prior to overfill. Split Fraction O5A represents the continued attempt to depressurize and cool down the RCS after the initial failure in O41 and prior to RWST depletion. The relief and safety valves are again challenged (Top Event SO) during this time with the condition of two phase flow increasing the likelihood of the safety valve failing to re-close. In this sequence, depressurization (O5) is not successful but isolation prior to RWST depletion (SO) is successful. As a result, primary to secondary leakage is assumed to continue through the modulating relief valve and eventually the RWST is depleted. Since makeup flow to the RWST is insufficient for this tube rupture flow rate and the RCS remains at high pressure and cannot be transitioned to shutdown cooling, core damage occurs. Since the releases are through a modulating valve, this sequence allows enough source term reduction through deposition and partitioning to keep releases below the LERF level and is assigned to Plant Damage State 48B.		
3	//SWS1*SISF/OS1*O5E //SISF/OS1*O5E	8.59E-08 8.59E-08	In this sequence, split fraction OS1 fails, which represents failure of the operator to isolate and terminate feedwater flow to the ruptured SG prior to overfill. Split Fraction O5E represents late depressurization (following overfill and prior to RWST depletion). This split fraction differs from O5A, however, since there are no previously successful top events involving operator action and cognitive errors must therefore be included. As in the previous sequence, depressurization is not successful but isolation prior to RWST depletion is successful, core damage occurs, releases are through a modulating relief valve and the sequence is assigned to Plant Damage State 48B.		

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	Table 2				
Rank	Sequence	Sequence CDF	Discussion of Split Fractions		
5	//SISF/HP3*O41*O5G	5.06E-08	Split Fraction HP3 represents initial failure of high pressure injection.		
6	//SWS1*SISF/HP3*O41*O5G	5.06E-08	Split Fraction O41 is the same action described above.		
			The operators will continue cool down and depressurization actions under top event O5 and since high pressure injection is not available, they will at a certain point be directed to initiate a rapid cool down of the RCS to achieve core cooling recovery using the low pressure injection system. Split fraction O5G models this action including the additional equipment needed to accomplish the more rapid cool down.		
			In this sequence, depressurization to allow low pressure injection is not successful, but isolation prior to core damage is successful. As a result, releases following core damage are through a modulating relief valve and this sequence is assigned to Plant Damage State 48B.		
7	//SISF/OS1*SO1*LR2	3.03E-08	In this sequence, split fraction OS1 fails, which represents failure of the operator to isolate the various leakage paths to and from the ruptured steam generator and terminate feed water flow to		
8	//SWS1*SISF/OS1*SO1*LR2	3.03E-08	the ruptured SG prior to overfill.		
			Split fraction SO1, which represents inability to isolate following overfill, also fails.		
			Top event O5, depressurization and cool down the RCS to the point where shutdown cooling can be implemented, prior to RWST depletion, is successful. However, split fraction LR2 fails, which represents the inability to actually implement shutdown cooling following depressurization. It should be noted that the current model assumes that both RWST makeup (MU) and shut down cooling (LR) are required to prevent core damage following successful depressurization. This is a substantial conservatism since with successful makeup, the extended time available would make any failure of shutdown cooling highly likely to be recoverable and with successful implementation of shutdown cooling, little or no additional makeup is required.		
			Given the current modeling, this sequence represents core damage with a continuously open path to the environment and is assigned to Plant Damage State 48.		

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	Table 2				
Rank	Sequence	Sequence CDF	Discussion of Split Fractions		
9	//SWS1*SISF/HP3*L14	2.18E-08	Split Fraction HP3 represents initial failure of high pressure injection.		
10	//SISF/HP3*L14	2.18E-08	Similar to sequences 5 and 6 above, this sequence represents failure to depressurize to recover core injection following a failure of the high pressure injection system. In this case, however, the failure to depressurize is a result of failure of the Auxiliary Feedwater System (Split Fraction L14) under the more demanding success criteria for this action (both motor driven AFW pumps required).		
			Although depressurization to allow low pressure injection is not successful resulting in core damage, isolation prior to core damage is successful. As a result, releases following core damage are through a modulating relief valve and this sequence is assigned to Plant Damage State 48B.		
11	//SISF/OS1*O5E*SO3	7.23E-09	In this sequence, split fraction OS1 fails, which represents failure of the operator to isolate and terminate feed water flow to the ruptured SG prior to overfill.		
12	//SWS1*SISF/OS1*O5E*SO3	7.23E-09	Split Fraction O5E represents late depressurization (following overfill and prior to RWST depletion). Split fraction SO3, which represents inability to isolate following overfill, accounting for dependencies with O5E, also fails.		
			Since both depressurization and isolation prior to RWST depletion are failed, core damage occurs with a continuously open path to the environment and is assigned to Plant Damage State 48A.		
13	//SWS1*SISF/RW2*OS1	6.48E-09	In this sequence, split fraction RW2, the Refueling Water Storage Tank supply to the core injection systems, fails. This fails high pressure injection and eliminates the ability to recove core cooling by depressurizing and using low pressure injection.		
14	//SISF/RW2*OS1	6.48E-09			
			Split fraction OS1 also fails, representing operator failure to isolate and terminate feed water flow to the ruptured SG, allowing continued loss of primary coolant. Given failure of all injection, early core damage is assumed and later actions to depressurize (O5) and isolate (SO) are bypassed.		
			Since core damage occurs with a continuously open path to the environment, this sequence is assigned to Plant Damage State 48A.		

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	Table 2					
Rank	Sequence	Sequence CDF	Discussion of Split Fractions			
15 //SISF/OS1*SO1*MU1 16 //SWS1*SISF/OS1*SO1*MU1		6.31E-09 6.31E-09	In this sequence, split fraction OS1 fails, which represents failure of the operator to isolate the various leakage paths to and from the ruptured steam generator and terminate feed water flow to the ruptured SG prior to overfill. Split fraction SO1, which represents inability to isolate following overfill, also fails. Top event O5, depressurization and cool down the RCS to the point where shutdown cooling can be implemented, prior to RWST depletion, is successful. Switchover to shutdown cooling has not yet been challenged and the model assumes some make up to the RWST is required. Split fraction MU1 represents the inability to provide that make up and this sequence therefore leads to core damage. Since this sequence represents core damage with a continuously open path to the environment, i is assigned to Plant Damage State 48A.			
17 18	//SWS1*SISF/RW2*O41 //SISF/RW2*O41	4.89E-09 4.89E-09	In this sequence, split fraction RW2, the Refueling Water Storage Tank supply to the core injection systems, fails. This fails high pressure injection and eliminates the ability to recover core cooling by depressurizing and using low pressure injection. Steam generator isolation (Split fraction OS1) succeeds but split fraction O41, depressurization and cool down, fails, allowing continued loss of primary coolant. Given failure of all injection, early core damage is assumed. Since core damage occurs with releases through a modulating relief valve, this sequence is assigned to Plant Damage State 48B.			
19 20	//SISF/L11*O31 //SWS1*SISF/L11*O31	4.85E-09 4.85E-09	In this sequence, auxiliary feed water (split fraction L11) fails along with the operator actions to depressurize and cool down in the absence of auxiliary feed water (split fraction O31). This is assumed to lead directly to core damage and this sequence is assigned to Plant Damage State 48A.			
21 22	//SISF/HP3*OS1*SO1 //SWS1*SISF/HP3*OS1*SO1	3.18E-09 3.18E-09	In this sequence, high pressure injection (HP3) has failed as well as steam generator isolation (split fractions OS1 and SO1). This is assumed to lead directly to core damage with a continuously open path to the environment and this sequence is assigned to Plant Damage State 48A.			

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Table 2				
Rank	Sequence	Sequence CDF	Discussion of Split Fractions	
23 24	//SISF/O41*SO2*LR2 //SWS1*SISF/O41*SO2*LR2	2.27E-09 2.27E-09	In this sequence, the operator has successfully isolated the SG and terminated auxiliary feed water flow to the ruptured steam generator (Top Event OS). Early depressurization and cool down of the RCS (Split Fraction O41) fails, however. Split fraction SO2, which represents inability to isolate following overfill, also fails.	
			Top event O5, depressurization and cool down the RCS to the point where shutdown cooling can be implemented, prior to RWST depletion, is successful. However, split fraction LR2 fails, which represents the inability to actually implement shutdown cooling following depressurization.	
			This sequence represents core damage with a continuously open path to the environment and is assigned to Plant Damage State 48A.	
25	//EA1B*SISF/O41*O5A	2.23E-09	These sequences are identical to sequences 1 and 2 except that they include failure of automatic SI actuation signals.	
26	//EA1B*SWS1*SISF/O41*O5A	2.23E-09		
27	//EB1B*SISF/041*05A	2.23E-09	Since there is no dependence on automatic SI for the O41 and O5A functions, these sequences simply represent the complement of the above sequences, since RISKMAN modeling accounts for the success probability of the SI actuation in those sequences	
28	//EB1B*SWS1*SISF/041*05A	2.23E-09	Consistent with sequences 1 and 2, these sequences are assigned to Plant Damage State 48B	
29	//EA1B*EBCB*SISF/HP6*O41 *O5G	2.00E-09	These sequences are identical to sequences 5 and 6 except that they include failure of both trai of automatic SI actuation signals. Since top event HP represents high pressure injection, whic has a dependency on the automatic actuation signal, the split fraction used (HP6) reflects the	
30	//EA1B*EBCB*SWS1*SISF/H P6*O41*O5G			

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Table 2			
Rank	Sequence	Sequence CDF	Discussion of Split Fractions
31 32	//SISF/L11*SO4 //SWS1*SISF/L11*SO4	1.30E-09 1.30E-09	In these sequences, AFW fails (L11) but the operator successfully depressurizes and cools down (O31) using the ruptured steam generator and a Pressurizer PORV, avoiding steam generator overfill.
	a		Early operator action to stop AFW is not required given failure of L11 and top event OS is bypassed. Isolation is challenged in SO and fails in this sequence. Although RWST makeup and shutdown cooling are possible since depressurization and cool down is successful, they are not credited in these sequences.
			This is conservatively modeled as a core damage sequence and, given failure of SO, this sequence is assigned to Plant Damage State 48A.
33	//SISF/O41*O5A	1.30E-09	These sequences are identical to sequences 1 and 2 except that they include failure of automatic SI actuation signals.
34	//SWS1*SISF/O41*O5A	1.30E-09	Since there is no dependence on automatic SI for the O41 and O5A functions, these sequences simply represent the complement of the above sequences, since RISKMAN modeling accounts for the success probability of the SI actuation in those sequences
			Consistent with sequences 1 and 2, these sequences are assigned to Plant Damage State 48B

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