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United States Nuclear Regulatory Commission
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Gentlemen:

**CORE OPERATING LIMITS REPORT – CYCLE 12, REVISION 2
SALEM GENERATING STATION UNIT NO. 2
FACILITY OPERATING LICENSE DPR-75
DOCKET NO. 50-311**

In accordance with section 6.9.1.9 of the Salem Unit 2 Technical Specifications, PSEG Nuclear LLC submits Revision 2 of the Core Operating Limits Report (COLR) for Salem Unit 2 Cycle 12 (Report NFS-0185, Rev. 2) as Attachment 1 to this letter.

Revision 2 of the COLR incorporates information required to increase the core power level for operation to 3459 MWt at Salem Unit 2. The NRC approved the increase in core power to 3459 MWt by Amendment No. 224 to Facility Operating License No. DPR-75 for Salem Unit 2 on May 25, 2001.

If you have any questions regarding this submittal, please contact Mr. Brian Thomas at (856) 339-2022.

Sincerely,

A handwritten signature in cursive script that reads "G. Salamon".

G. Salamon
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Attachment

A001

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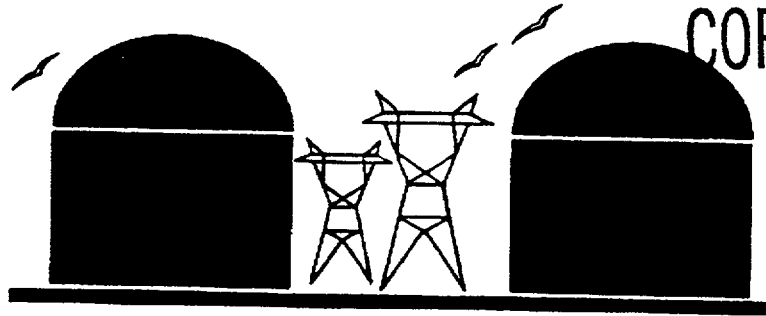
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Core Operating Limits Report for Salem Unit 2, Cycle 12

PSE&G
CONTROL

COPY # 0331



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TABLE OF CONTENTS

<u>Section Number</u>	<u>Section Title</u>	<u>Page Number</u>
	Table of Contents	2
	List of Figures	3
1.0	Core Operating Limits Report	4
2.0	Operating Limits	5
2.1	Moderator Temperature Coefficient (Specification 3/4.1.1.3)	5
2.2	Control Rod Insertion Limits (Specification 3/4.1.3.5)	6
2.3	Axial Flux Difference (Specification 3/4.2.1)	6
2.4	Heat Flux Hot Channel Factor – $F_q(z)$ (Specification 3/4.2.2)	6
2.5	Nuclear Enthalpy Rise Hot Channel Factor $F_{\Delta H}^N$ (Specification 3/4.2.3)	8
3.0	References	8

LIST OF FIGURES

<u>Figure Number</u>	<u>Figure Title</u>	<u>Page Number</u>
1	Rod Bank Insertion Limits vs. Thermal Power	9
2	Axial Flux Difference Limits as a Function of Rated Thermal Power	10
3	$K(z)$ – Normalized $F_q(z)$ as a Function of Core Height	11

1.0 CORE OPERATING LIMITS REPORT

This Core Operating Limits Report (COLR) for Salem Unit 2 Cycle 12 has been prepared in accordance with the requirements of Technical Specification 6.9.1.9.

The Technical Specifications affected by this report are listed below:

- 3/4.1.1.3 Moderator Temperature Coefficient
- 3/4.1.3.5 Control Rod Insertion Limits
- 3/4.2.1 Axial Flux Difference
- 3/4.2.2 Heat Flux Hot Channel Factor - $F_Q(Z)$
- 3/4.2.3 Nuclear Enthalpy Rise Hot Channel Factor - $F^N_{\Delta H}$

2.0 OPERATING LIMITS

The cycle-specific parameter limits for the specifications listed in Section 1.0 are presented in the following subsections. These limits have been developed using the NRC-approved methodologies specified in Technical Specification 6.9.1.9.

2.1 Moderator Temperature Coefficient (Specification 3/4.1.1.3)

2.1.1 The Moderator Temperature Coefficient (MTC) limits are:

The BOL/ARO/HZP-MTC shall be less positive than $0 \Delta k/k/^{\circ}F$.

The EOL/ARO/RTP-MTC shall be less negative than $-4.5 \times 10^{-4} \Delta k/k/^{\circ}F$.

2.1.2 The MTC Surveillance limit is:

The 300 ppm/ARO/RTP-MTC should be less negative than or equal to $-3.8 \times 10^{-4} \Delta k/k/^{\circ}F$.

where: BOL stands for Beginning of Cycle Life

ARO stands for All Rods Out

HZP stands for Hot Zero THERMAL POWER

EOL stands for End of Cycle Life

RTP stands for Rated THERMAL POWER

2.2 Control Rod Insertion Limits (Specification 3/4.1.3.5)

2.2.1 The control rod banks shall be limited in physical insertion as shown in Figure 1.

2.3 Axial Flux Difference (Specification 3/4.2.1)

[Constant Axial Offset Control (CAOC) Methodology]

2.3.1 The Axial Flux Difference (AFD) target band is +6%, -9%.

2.3.2 The AFD Acceptable Operation Limits are provided in Figure 2.

2.4 Heat Flux Hot Channel Factor - $F_Q(Z)$ (Specification 3/4.2.2)

[F_{xy} Methodology]

$$F_Q(Z) \leq \frac{F_Q^{RTP}}{P} * K(Z) \text{ for } P > 0.5$$

$$F_Q(Z) \leq \frac{F_Q^{RTP}}{0.5} * K(Z) \text{ for } P \leq 0.5$$

where: $P = \frac{\text{THERMAL POWER}}{\text{RATED THERMAL POWER}}$

2.4.1 $F_Q^{RTP} = 2.40$

2.4.2 $K(Z)$ is provided in Figure 3.

2.4.3 $F_{xy}^L = F_{xy}^{RTP} [1.0 + PF_{xy}(1.0 - P)]$

where: $F_{xy}^{RTP} = 1.77$ for the unrodded core planes

2.13 for the core plane containing Bank D control rods

$PF_{xy} = 0.3$

- 2.4.4 If the Power Distribution Monitoring System (PDMS) is used for core power distribution surveillance and is OPERABLE, as defined in Technical Specification 3.3.3.14, the uncertainty, U_{FQ} , to be applied to the Heat Flux Hot Channel Factor $F_Q(z)$ shall be calculated by the following formula:

$$U_{FQ} = \left(1.0 + \frac{U_Q}{100.0} \right) \cdot U_e$$

where:

U_Q = Uncertainty for power peaking factor as defined in equation 5-19 of Reference 1.

U_e = Engineering uncertainty factor.
= 1.03

Note: U_{FQ} = PDMS Surveillance Report Core Monitor Fxy Uncertainty in %.

- 2.4.5 If the INCORE movable detectors are used for core power distribution surveillance, the uncertainty, U_{FQ} , to be applied to the Heat Flux Hot Channel Factor $F_Q(z)$ shall be calculated by the following formula:

$$U_{FQ} = U_{qu} \cdot U_e$$

where:

U_{qu} = Base F_Q measurement uncertainty.
= 1.05

U_e = Engineering uncertainty factor.
= 1.03

2.5 Nuclear Enthalpy Rise Hot Channel Factor - $F_{\Delta H}^N$ (Specification 3/4.2.3)

$$F_{\Delta H}^N = F_{\Delta H}^{RTP} [1.0 + PF_{\Delta H} (1.0 - P)]$$

where: $P = \frac{\text{THERMAL POWER}}{\text{RATED THERMAL POWER}}$

2.5.1 If RTP = 3411 MWt; then,

$$F_{\Delta H}^{RTP} = 1.65$$

If RTP > 3411 MWt and RTP ≤ 3459 MWt; then,

$$F_{\Delta H}^{RTP} (\text{RFA with IFM}) = 1.65 \text{ and } F_{\Delta H}^{RTP} (\text{V5H without IFM}) = 1.57$$

2.5.2 $PF_{\Delta H} = 0.3$

2.5.3 If the Power Distribution Monitoring System (PDMS) is used for core power distribution surveillance and is OPERABLE, as defined in Technical Specification 3.3.3.14, the uncertainty, $U_{F_{\Delta H}}$, to be applied to the Nuclear Enthalpy Rise Hot Channel Factor, $F_{\Delta H}^N$, shall be calculated by the following formula:

$$U_{F_{\Delta H}} = 1.0 + \frac{U_{\Delta H}}{100.0}$$

where:

$U_{\Delta H}$ = Uncertainty for enthalpy rise as defined in equation 5-19 of Reference 1.

2.5.4 If the INCORE movable detectors are used for core power distribution surveillance, the uncertainty, $U_{F_{\Delta H}}$, to be applied to the Nuclear Enthalpy Rise Hot Channel Factor $F_{\Delta H}^N$ shall be calculated by the following formula:

$$U_{F_{\Delta H}} = U_{F_{\Delta Hm}}$$

where:

$U_{F_{\Delta Hm}}$ = Base $F_{\Delta H}$ measurement uncertainty.
= 1.04

3.0 REFERENCES

1. WCAP-12472-P-A, BEACON Core Monitoring and Operations Support System, August 1994.

FIGURE 1

ROD BANK INSERTION LIMITS vs. THERMAL POWER

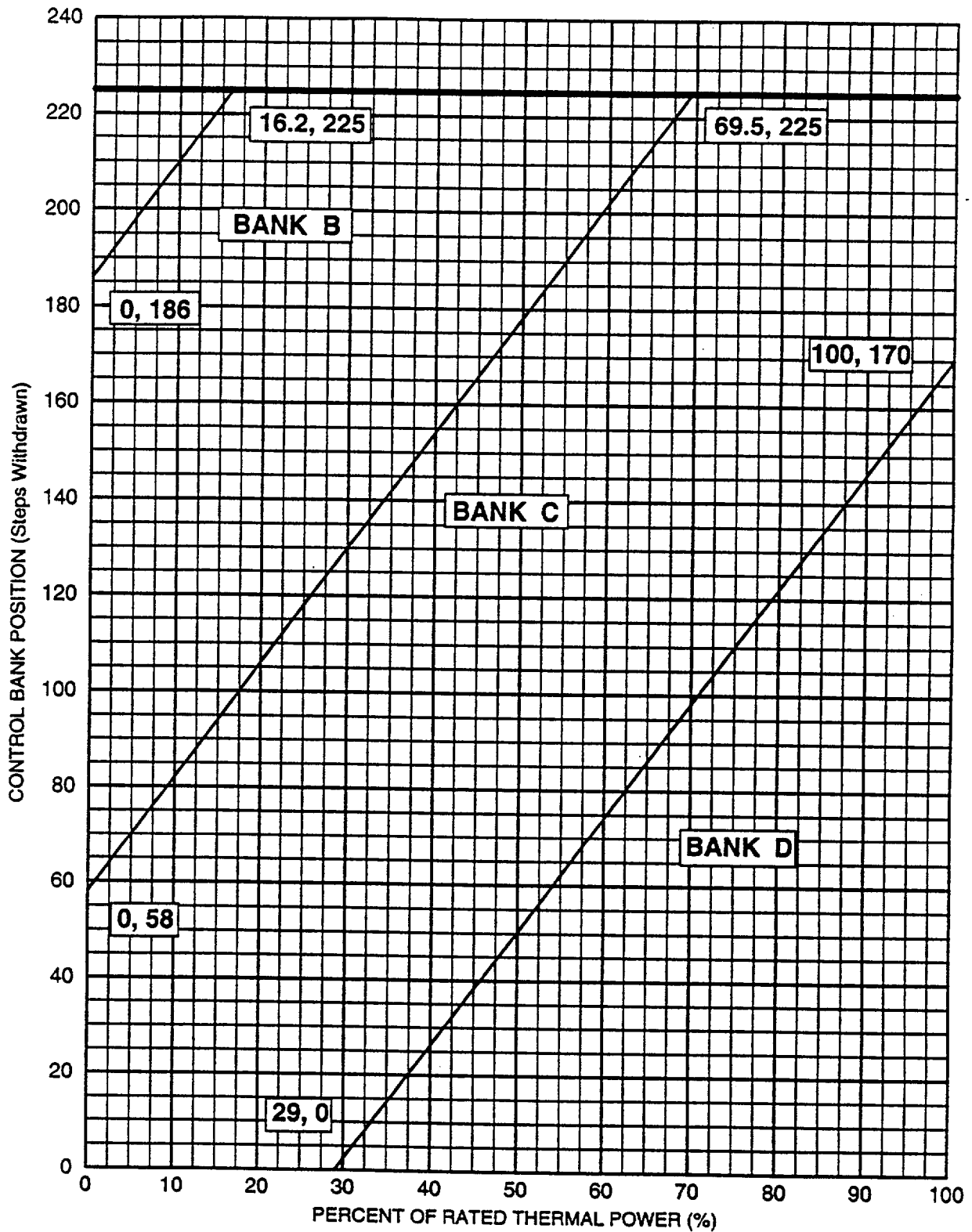


FIGURE 2

AXIAL FLUX DIFFERENCE LIMITS AS A FUNCTION OF
RATED THERMAL POWER

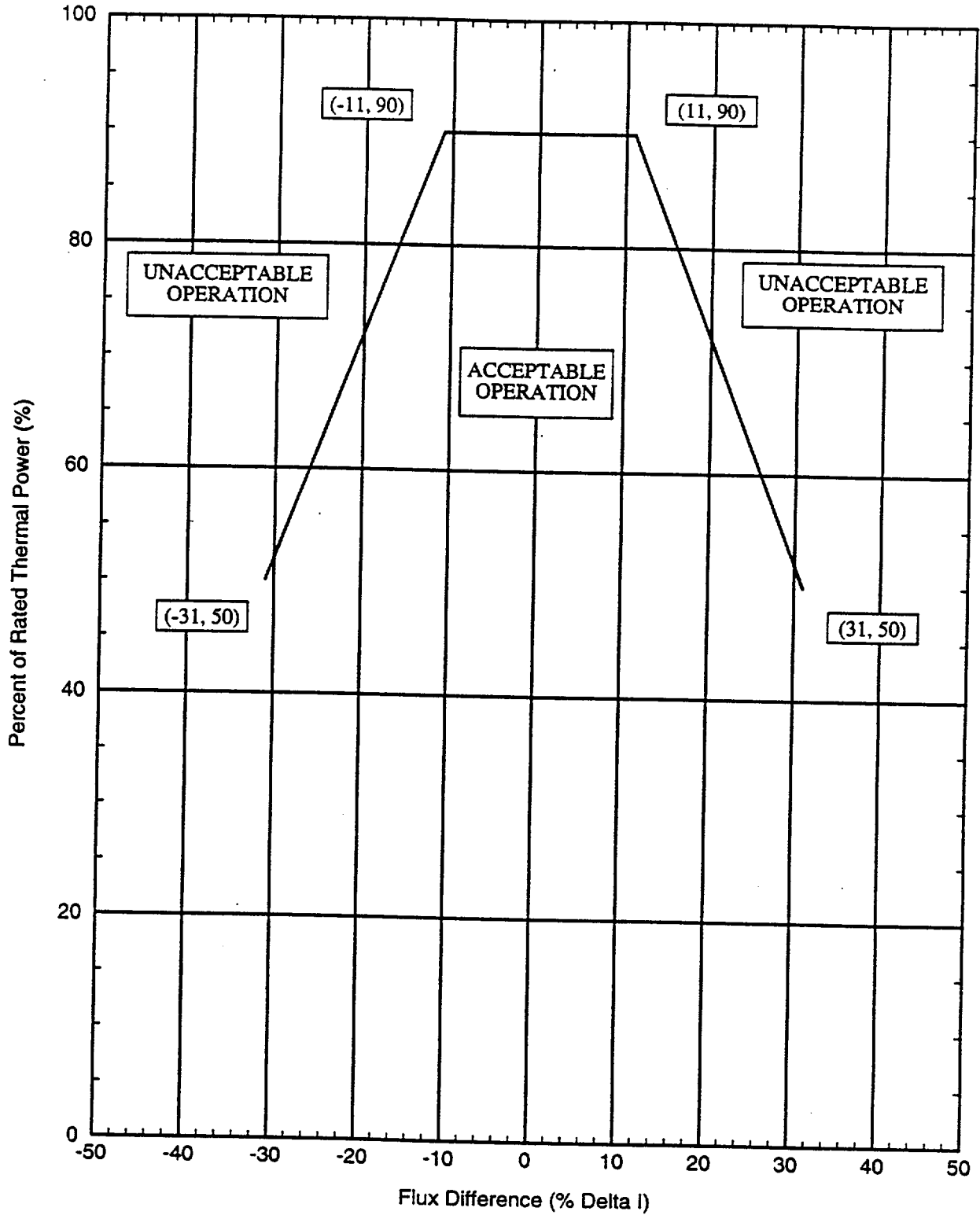


FIGURE 3

K(Z) - NORMALIZED FQ(Z) AS A FUNCTION OF CORE HEIGHT

