

May 15, 1990

Docket Nos. 50-352  
and 50-353

Mr. George A. Hunger, Jr.  
Director-Licensing, MC 5-2A-5  
Philadelphia Electric Company  
Nuclear Group Headquarters  
Correspondence Control Desk  
P.O. Box No. 195  
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Dear Mr. Hunger:

SUBJECT: REMOVAL OF CYCLE SPECIFIC PARAMETER LIMITS, REQUEST NO. 89-13  
(TAC NOS. 76053 AND 76054)

RE: LIMERICK GENERATING STATION, UNITS 1 AND 2

The Commission has issued the enclosed Amendment No. 37 to Facility Operating License No. NPF-39 and Amendment No. 4 to Facility Operating License No. NPF-85 for the Limerick Generating Station, Units 1 and 2. These amendments consist of changes to the Technical Specifications (TSs) in response to your application dated February 23, 1990.

These amendments change the TSs to remove cycle specific parameter limits in accordance with NRC Generic Letter 88-16.

A copy of our Safety Evaluation is also enclosed. Notice of Issuance will be included in the Commission's biweekly Federal Register notice.

Sincerely,

Original signed by  
Richard J. Clark

Richard J. Clark, Project Manager  
Project Directorate I-2  
Division of Reactor Projects I/II  
Office of Nuclear Reactor Regulation

Enclosures:

1. Amendment No. 37 to  
License No. NPF-39  
Amendment No. 4 to  
License No. NPF-85
2. Safety Evaluation

cc w/enclosures:  
See next page

[76053/4]

PDI-2/PA  
MO'Brien  
5/15/90

PDI-2/PM  
RClark:mj  
04/04/90

SRXB  
DBFieno  
4/16/90

OGC  
4/12/90

PDI-2/D  
WButler  
5/15/90

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PDR ADDCK 05000352  
P PDR

RF01  
11c



UNITED STATES  
NUCLEAR REGULATORY COMMISSION  
WASHINGTON, D. C. 20555  
May 15, 1990

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and 50-353

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Sincerely,

A handwritten signature in black ink, which appears to read "Richard J. Clark", is written over a circular stamp or seal.

Richard J. Clark, Project Manager  
Project Directorate I-2  
Division of Reactor Projects I/II  
Office of Nuclear Reactor Regulation

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cc w/enclosures:  
See next page

Mr. George A. Hunger, Jr.  
Philadelphia Electric Company

Limerick Generating Station  
Units 1 & 2

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UNITED STATES  
NUCLEAR REGULATORY COMMISSION  
WASHINGTON, D. C. 20555

PHILADELPHIA ELECTRIC COMPANY

DOCKET NO. 50-352

LIMERICK GENERATING STATION, UNIT 1

AMENDMENT TO FACILITY OPERATING LICENSE

Amendment No. 37  
License No. NPF-39

1. The Nuclear Regulatory Commission (the Commission) has found that
  - A. The application for amendment by Philadelphia Electric Company (the licensee) dated February 23, 1990, complies with the standards and requirements of the Atomic Energy Act of 1954, as amended (the Act), and the Commission's rules and regulations set forth in 10 CFR Chapter I;
  - B. The facility will operate in conformity with the application, the provisions of the Act, and the rules and regulations of the Commission;
  - C. There is reasonable assurance (i) that the activities authorized by this amendment can be conducted without endangering the health and safety of the public, and (ii) that such activities will be conducted in compliance with the Commission's regulations;
  - D. The issuance of this amendment will not be inimical to the common defense and security or to the health and safety of the public; and
  - E. The issuance of this amendment is in accordance with 10 CFR Part 51 of the Commission's regulations and all applicable requirements have been satisfied.
2. Accordingly, the license is amended by changes to the Technical Specifications as indicated in the attachment to this license amendment, and paragraph 2.C.(2) of Facility Operating License No. NPF-39 is hereby amended to read as follows:

Technical Specifications

The Technical Specifications contained in Appendix A and the Environmental Protection Plan contained in Appendix B, as revised through Amendment No. 37, are hereby incorporated into this license. Philadelphia Electric Company shall operate the facility in accordance with the Technical Specifications and the Environmental Protection Plan.

9006080303 900515  
PDR ADDCK 05000352  
P PDC

3. This license amendment is effective as of its date of issuance.

FOR THE NUCLEAR REGULATORY COMMISSION

/s/  
Walter R. Butler, Director  
Project Directorate I-2  
Division of Reactor Projects I/II

Attachment:  
Changes to the Technical  
Specifications

Date of Issuance: May 15, 1990

PDI-2/LA  
M. Brien  
5/1/90

PDI-2/PM  
RClark:ma  
04/04/90

OGC *CB*  
4/12/90

PDI-2/D  
WButler  
5/15/90 *WB*

3. This license amendment is effective as of its date of issuance.

FOR THE NUCLEAR REGULATORY COMMISSION

*Walter R. Butler*

Walter R. Butler, Director  
Project Directorate 1-2  
Division of Reactor Projects I/II

Attachment:  
Changes to the Technical  
Specifications

Date of Issuance: May 15, 1990

ATTACHMENT TO LICENSE AMENDMENT NO. 37

FACILITY OPERATING LICENSE NO. NPF-39

DOCKET NO. 50-352

Replace the following pages of the Appendix A Technical Specifications with the attached page. The revised pages are identified by Amendment number and contain vertical lines indicating the area of change. Overleaf pages are provided to maintain document completeness.\*

Remove

Insert

i	i
ii	ii*
v	v
vi	vi
via	-
-	-
xxvii	xxvii
xxviii	xxviii*
1-1	1-1*
1-2	1-2
3/4 2-1	3/4 2-1
3/4 2-2	3/4 2-2
3/4 2-3	-
3/4 2-4	-
3/4 2-5	-
3/4 2-6	-
3/4 2-6a	-
3/4 2-6b	-
3/4 2-6c	-
-	-
3/4 2-7	3/4 2-7*
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ATTACHMENT TO LICENSE AMENDMENT NO. 37

FACILITY OPERATING LICENSE NO. NPF-39

DOCKET NO. 50-352

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3/4 3-60a

3/4 3-60a

3/4 3-60b

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B 3/4 2-1

B 3/4 2-1

B 3/4 2-2

B 3/4 2-2\*

B 3/4 2-3

B 3/4 2-3\*

B 3/4 2-4

B 3/4 2-4

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## 1.0 DEFINITIONS

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The following terms are defined so that uniform interpretation of these specifications may be achieved. The defined terms appear in capitalized type and shall be applicable throughout these Technical Specifications.

### ACTION

- 1.1 ACTION shall be that part of a Specification which prescribes remedial measures required under designated conditions.

### AVERAGE PLANAR EXPOSURE

- 1.2 The AVERAGE PLANAR EXPOSURE shall be applicable to a specific planar height and is equal to the sum of the exposure of all the fuel rods in the specified bundle at the specified height divided by the number of fuel rods in the fuel bundle.

### AVERAGE PLANAR LINEAR HEAT GENERATION RATE

- 1.3 The AVERAGE PLANAR LINEAR HEAT GENERATION RATE (APLHGR) shall be applicable to a specific planar height and is equal to the sum of the LINEAR HEAT GENERATION RATES for all the fuel rods in the specified bundle at the specified height divided by the number of fuel rods in the fuel bundle.

### CHANNEL CALIBRATION

- 1.4 A CHANNEL CALIBRATION shall be the adjustment, as necessary, of the channel output such that it responds with the necessary range and accuracy to known values of the parameter which the channel monitors. The CHANNEL CALIBRATION shall encompass the entire channel including the sensor and alarm and/or trip functions, and shall include the CHANNEL FUNCTIONAL TEST. The CHANNEL CALIBRATION may be performed by any series of sequential, overlapping or total channel steps such that the entire channel is calibrated.

### CHANNEL CHECK

- 1.5 A CHANNEL CHECK shall be the qualitative assessment of channel behavior during operation by observation. This determination shall include, where possible, comparison of the channel indication and/or status with other indications and/or status derived from independent instrument channels measuring the same parameter.

### CHANNEL FUNCTIONAL TEST

- 1.6 A CHANNEL FUNCTIONAL TEST shall be:

- a. Analog channels - the injection of a simulated signal into the channel as close to the sensor as practicable to verify OPERABILITY including alarm and/or trip functions and channel failure trips.
- b. Bistable channels - the injection of a simulated signal into the sensor to verify OPERABILITY including alarm and/or trip functions.

The CHANNEL FUNCTIONAL TEST may be performed by any series of sequential, overlapping or total channel steps such that the entire channel is tested.

## DEFINITIONS

### CORE ALTERATION

- 1.7 CORE ALTERATION shall be the addition, removal, relocation or movement of fuel, sources, or reactivity controls within the reactor pressure vessel with the vessel head removed and fuel in the vessel. Normal movement of the SRMs, IRMs, TIPS, or special movable detectors is not considered a CORE ALTERATION. Suspension of CORE ALTERATIONS shall not preclude completion of the movement of a component to a safe conservative position.

### CORE OPERATING LIMITS REPORT

- 1.7a The CORE OPERATING LIMITS REPORT (COLR) is the unit-specific document that provides the core operating limits for the current operating reload cycle. These cycle-specific core operating limits shall be determined for each reload cycle in accordance with Specifications 6.9.1.9 thru 6.9.1.12. Plant operation within these limits is addressed in individual specifications.

### CRITICAL POWER RATIO

- 1.8 The CRITICAL POWER RATIO (CPR) shall be the ratio of that power in the assembly which is calculated by application of the (GEXL) correlation to cause some point in the assembly to experience boiling transition, divided by the actual assembly operating power.

### DOSE EQUIVALENT I-131

- 1.9 DOSE EQUIVALENT I-131 shall be that concentration of I-131, microcuries per gram, which alone would produce the same thyroid dose as the quantity and isotopic mixture of I-131, I-132, I-133, I-134, and I-135 actually present. The thyroid dose conversion factors used for this calculation shall be those listed in Table III of TID-14844, "Calculation of Distance Factors for Power and Test Reactor Sites."

### $\bar{E}$ -AVERAGE DISINTEGRATION ENERGY

- 1.10  $\bar{E}$  shall be the average, weighted in proportion to the concentration of each radionuclide in the reactor coolant at the time of sampling, of the sum of the average beta and gamma energies per disintegration, in MeV, for isotopes, with half lives greater than 15 minutes, making up at least 95% of the total noniodine activity in the coolant.

### EMERGENCY CORE COOLING SYSTEM (ECCS) RESPONSE TIME

- 1.11 The EMERGENCY CORE COOLING SYSTEM (ECCS) RESPONSE TIME shall be that time interval from when the monitored parameter exceeds its ECCS actuation set-point at the channel sensor until the ECCS equipment is capable of performing its safety function, i.e., the valves travel to their required positions, pump discharge pressures reach their required values, etc. Times shall include diesel generator starting and sequence loading delays where applicable. The response time may be measured by any series of sequential, overlapping or total steps such that the entire response time is measured.

### END-OF-CYCLE RECIRCULATION PUMP TRIP SYSTEM RESPONSE TIME

- 1.12 The END-OF-CYCLE RECIRCULATION PUMP TRIP SYSTEM RESPONSE TIME shall be that time interval to complete suppression of the electric arc between the fully open contacts of the recirculation pump circuit breaker from initial movement of the associated:
- Turbine stop valves, and
  - Turbine control valves.



### 3/4.2 POWER DISTRIBUTION LIMITS

#### 3/4.2.1 AVERAGE PLANAR LINEAR HEAT GENERATION RATE

##### LIMITING CONDITION FOR OPERATION

---

3.2.1 All AVERAGE PLANAR LINEAR HEAT GENERATION RATES (APLHGRs) for each type of fuel as a function of axial location and AVERAGE PLANAR EXPOSURE shall be within limits based on applicable APLHGR limit values which have been determined by approved methodology for the respective fuel and lattice types for two recirculation loop operation. When hand calculations are required, the APLHGR for each type of fuel as a function of AVERAGE PLANAR EXPOSURE shall not exceed the limiting value for the most limiting lattice (excluding natural uranium) as shown in the CORE OPERATING LIMITS REPORT (COLR). During single loop operation, the APLHGR for each fuel type shall not exceed the above values multiplied by the reduction factors shown in the COLR.

APPLICABILITY: OPERATIONAL CONDITION 1, when THERMAL POWER is greater than or equal to 25% of RATED THERMAL POWER.

##### ACTION:

With an APLHGR exceeding the limiting value, initiate corrective action within 15 minutes and restore APLHGR to within the required limits within 2 hours or reduce THERMAL POWER to less than 25% of RATED THERMAL POWER within the next 4 hours.

##### SURVEILLANCE REQUIREMENTS

---

4.2.1 All APLHGRs shall be verified to be equal to or less than the limiting value

- a. At least once per 24 hours,
- b. Within 12 hours after completion of a THERMAL POWER increase of at least 15% of RATED THERMAL POWER, and
- c. Initially and at least once per 12 hours when the reactor is operating with a LIMITING CONTROL ROD PATTERN for APLHGR.
- d. The provisions of Specification 4.0.4 are not applicable.

Figures on pages  
3/4 2-2 thru 3/4 2-6c  
have been removed from Technical  
Specifications, and relocated to the  
CORE OPERATING LIMITS REPORT.

Technical Specifications pages  
3/4 2-3 thru 3/4 2-6c  
have been INTENTIONALLY OMITTED.

## POWER DISTRIBUTION LIMITS

### 3/4.2.2 APRM SETPOINTS

#### LIMITING CONDITION FOR OPERATION

3.2.2 The APRM flow biased neutron flux-upscale scram trip setpoint (S) and flow biased neutron flux-upscale control rod block trip setpoint ( $S_{RB}$ ) shall be established according to the following relationships:

	TRIP SETPOINT	ALLOWABLE VALUE
During two recirculation loop operation	$S \leq (0.58W + 59\%)T$ $S_{RB} \leq (0.58W + 50\%)T$	$S \leq (0.58W + 62\%)T$ $S_{RB} \leq (0.58W + 53\%)T$
During single recirculation loop operation	$S \leq (0.58W + 54\%)T$ $S_{RB} \leq (0.58W + 45\%)T$	$S \leq (0.58W + 57\%)T$ $S_{RB} \leq (0.58W + 48\%)T$

where: S and  $S_{RB}$  are in percent of RATED THERMAL POWER,

W = Loop recirculation flow as a percentage of the loop recirculation flow which produces a rated core flow of 100 million lbs/hr,

T = Lowest value of the ratio of FRACTION OF RATED THERMAL POWER divided by the CORE MAXIMUM FRACTION OF LIMITING POWER DENSITY.

T is applied only if less than or equal to 1.0.

APPLICABILITY: OPERATIONAL CONDITION 1, when THERMAL POWER is greater than or equal to 25% of RATED THERMAL POWER.

#### ACTION:

With the APRM flow biased neutron flux-upscale scram trip setpoint and/or the flow biased neutron flux-upscale control rod block trip setpoint less conservative than the value shown in the Allowable Value column for S or  $S_{RB}$ , as above determined, initiate corrective action within 15 minutes and adjust S and/or  $S_{RB}$  to be consistent with the Trip Setpoint values\* within 6 hours or reduce THERMAL POWER to less than 25% of RATED THERMAL POWER within the next 4 hours.

#### SURVEILLANCE REQUIREMENTS

4.2.2 The F RTP and the MFLPD shall be determined, the value of T calculated, and the most recent actual APRM flow biased neutron flux-upscale scram and flow biased neutron flux-upscale control rod block trip setpoints verified to be within the above limits or adjusted, as required:

- At least once per 24 hours,
- Within 12 hours after completion of a THERMAL POWER increase of at least 15% of RATED THERMAL POWER, and
- Initially and at least once per 12 hours when the reactor is operating with MFLPD greater than or equal to F RTP.
- The provisions of Specification 4.0.4 are not applicable.

\*With MFLPD greater than the F RTP, rather than adjusting the APRM setpoints, the APRM gain may be adjusted such that the APRM readings are greater than or equal to 100% times MFLPD, provided that the adjusted APRM reading does not exceed 100% of RATED THERMAL POWER and a notice of adjustment is posted on the reactor control panel.

## POWER DISTRIBUTION LIMITS

### 3/4.2.3 MINIMUM CRITICAL POWER RATIO

#### LIMITING CONDITION FOR OPERATION

3.2.3 The MINIMUM CRITICAL POWER RATIO (MCPR) shall be equal to or greater than the MCPR limit times the  $K_f$ , both values shown in the CORE OPERATING LIMITS REPORT, provided that the end-of-cycle recirculation pump trip (EOC-RPT) system is OPERABLE per Specification 3.3.4.2, with:

$$\tau = \frac{(\tau_{ave} - \tau_B)}{\tau_A - \tau_B}$$

where:

$\tau_A$  = 0.86 seconds, control rod average scram insertion time limit to notch 39 per Specification 3.1.3.3,

$$\tau_B = 0.672 + 1.65 \left[ \frac{N_1}{\sum_{i=1}^n N_i} \right]^{1/2} (0.016),$$

$$\tau_{ave} = \frac{\sum_{i=1}^n N_i \tau_i}{\sum_{i=1}^n N_i},$$

$n$  = number of surveillance tests performed to date in cycle,

$N_i$  = number of active control rods measured in the  $i^{th}$  surveillance test,

$\tau_i$  = average scram time to notch 39 of all rods measured in the  $i^{th}$  surveillance test, and

$N_1$  = total number of active rods measured in Specification 4.1.3.2.a.

#### APPLICABILITY:

OPERATIONAL CONDITION 1, when THERMAL POWER is greater than or equal to 25% of RATED THERMAL POWER.

## POWER DISTRIBUTION LIMITS

### LIMITING CONDITION FOR OPERATION (Continued)

#### ACTION

- a. With the end-of-cycle recirculation pump trip system inoperable per Specification 3.3.4.2, operation may continue provided that, within 1 hour, MCPR is determined to be greater than or equal to the MCPR limit as a function of the average scram time (shown in the CORE OPERATING LIMITS REPORT) EOC-RPT inoperable curve, times the  $k_f$  shown in the CORE OPERATING LIMITS REPORT.
- b. With MCPR less than the applicable MCPR limit shown in the CORE OPERATING LIMITS REPORT, initiate corrective action within 15 minutes and restore MCPR to within the required limit within 2 hours or reduce THERMAL POWER to less than 25% of RATED THERMAL POWER within the next 4 hours.

#### SURVEILLANCE REQUIREMENTS

##### 4.2.3 MCPR, with:

- a.  $\tau = 1.0$  prior to performance of the initial scram time measurements for the cycle in accordance with Specification 4.1.3.2, or
- b.  $\tau$  as defined in Specification 3.2.3 used to determine the limit within 72 hours of the conclusion of each scram time surveillance test required by Specification 4.1.3.2,

shall be determined to be equal to or greater than the applicable MCPR limit determined from the CORE OPERATING LIMITS REPORT.

- a. At least once per 24 hours,
- b. Within 12 hours after completion of a THERMAL POWER increase of at least 15% of RATED THERMAL POWER, and
- c. Initially and at least once per 12 hours when the reactor is operating with a LIMITING CONTROL ROD PATTERN for MCPR.
- d. The provisions of Specification 4.0.4 are not applicable.

Figures on pages  
3/4 2-10 thru 3/4 2-11  
have been removed  
from Technical Specifications,  
and relocated to the  
CORE OPERATING LIMITS REPORT.

Technical Specifications pages  
3/4 2-10a thru 3/4 2-11  
have been INTENTIONALLY OMITTED.

## POWER DISTRIBUTION LIMITS

### 3/4.2.4 LINEAR HEAT GENERATION RATE

#### LIMITING CONDITION FOR OPERATION

---

3.2.4 The LINEAR HEAT GENERATION RATE (LHGR) for each fuel type shall not exceed the value in the CORE OPERATING LIMITS REPORT.

APPLICABILITY: OPERATIONAL CONDITION 1, when THERMAL POWER is greater than or equal to 25% of RATED THERMAL POWER.

#### ACTION:

With the LHGR of any fuel rod exceeding the limit, initiate corrective action within 15 minutes and restore the LHGR to within the limit within 2 hours or reduce THERMAL POWER to less than 25% of RATED THERMAL POWER within the next 4 hours.

#### SURVEILLANCE REQUIREMENTS

---

4.2.4 LHGRs shall be determined to be equal to or less than the limit:

- a. At least once per 24 hours,
- b. Within 12 hours after completion of a THERMAL POWER increase of at least 15% of RATED THERMAL POWER, and
- c. Initially and at least once per 12 hours when the reactor is operating on a LIMITING CONTROL ROD PATTERN for LHGR.
- d. The provisions of Specification 4.0.4 are not applicable.

**TABLE 3.3.6-1 (Continued)**  
**CONTROL ROD WITHDRAWAL BLOCK INSTRUMENTATION**

**ACTION STATEMENTS**

- ACTION 60 -** Declare the RBM inoperable and take the ACTION required by Specification 3.1.4.3.
- ACTION 61 -** With the number of OPERABLE channels one or more less than required by the Minimum OPERABLE Channels per Trip Function requirement, place at least one inoperable channel in the tripped condition within one hour.
- ACTION 62 -** With the number of OPERABLE channels less than required by the Minimum OPERABLE Channels per Trip Function requirement, place the inoperable channel in the tripped condition within one hour.
- ACTION 63 -** With the number of OPERABLE channels less than required by the Minimum OPERABLE Channels per Trip Function requirement, initiate a red block.

**NOTES**

- \* With THERMAL POWER  $\geq$  30% of RATED THERMAL POWER.
- \*\* With more than one control rod withdrawn. Not applicable to control rods removed per Specification 3.9.10.1 or 3.9.10.2.
- \*\*\* These channels are not required when sixteen or fewer fuel assemblies, adjacent to the SDAs, are in the core.
- (a) The RBM shall be automatically bypassed when a peripheral control rod is selected or the reference APRM channel indicates less than 30% of RATED THERMAL POWER.
- (b) This function shall be automatically bypassed if detector count rate is  $> 100$  cps or the IRM channels are on range 3 or higher.
- (c) This function is automatically bypassed when the associated IRM channels are on range 3 or higher.
- (d) This function is automatically bypassed when the IRM channels are on range 3 or higher.
- (e) This function is automatically bypassed when the IRM channels are on range 1.



TABLE 3.3.6-2  
CONTROL ROD BLOCK INSTRUMENTATION SETPOINTS

<u>TRIP FUNCTION</u>	<u>TRIP SETPOINT</u>	<u>ALLOWABLE VALUE</u>
1. <u>ROD BLOCK MONITOR****</u>		
a. Upscale		
1) During two recirculation loop operation		
a. Flow Biased*	$\leq 0.66 W + (N-66)\%$ , with a maximum of, $\leq N\%$	$\leq 0.66 W + (N-63)\%$ , with a maximum of, $\leq (N+3)\%$
b. High Flow Clamped	$\leq N\%$	
2) During single recirculation loop operation		
a. Flow Biased*	$\leq 0.66 W + (N-72)\%$ , with a maximum of, $\leq N\%$	$\leq 0.66 W + (N-69)\%$ , with a maximum of, $\leq (N+3)\%$
b. High Flow Clamped	$\leq N\%$	
b. Inoperative	N.A.	N.A.
c. Downscale	$\geq 5\%$ of RATED THERMAL POWER	$\geq 3\%$ of RATED THERMAL POWER
2. <u>APRM</u>		
a. Flow Biased Neutron Flux - Upscale		
1) During two recirculation loop operation	$\leq 0.58 W + 50\%^*$	$\leq 0.58 W + 53\%^*$
2) During single recirculation loop operation	$\leq 0.58 W + 45\%^*$	$\leq 0.58 W + 48\%^*$
b. Inoperative	N.A.	N.A.
c. Downscale	$> 4\%$ of RATED THERMAL POWER	$> 3\%$ of RATED THERMAL POWER
d. Neutron Flux - Upscale, Startup	$\leq 12\%$ of RATED THERMAL POWER	$\leq 14\%$ of RATED THERMAL POWER
3. <u>SOURCE RANGE MONITORS</u>		
a. Detector not full in	N.A.	N.A.
b. Upscale	$< 1 \times 10^5$ cps	$< 1.6 \times 10^5$ cps
c. Inoperative	N.A.	N.A.
d. Downscale	$\geq 3$ cps**	$\geq 1.8$ cps**
4. <u>INTERMEDIATE RANGE MONITORS</u>		
a. Detector not full in	N.A.	N.A.
b. Upscale	$< 108/125$ divisions of full scale	$< 110/125$ divisions of full scale
c. Inoperative	N.A.	N.A.
d. Downscale	$> 5/125$ divisions of full scale	$> 3/125$ divisions of full scale
5. <u>SCRAM DISCHARGE VOLUME</u>		
a. Water Level-High		
a. Float Switch	$\leq 257' 5 \frac{9}{16}"$ elevation***	$\leq 257' 7 \frac{9}{16}"$ elevation

TABLE 3.3.6-2 (Continued)

CONTROL ROD BLOCK INSTRUMENTATION SETPOINTS

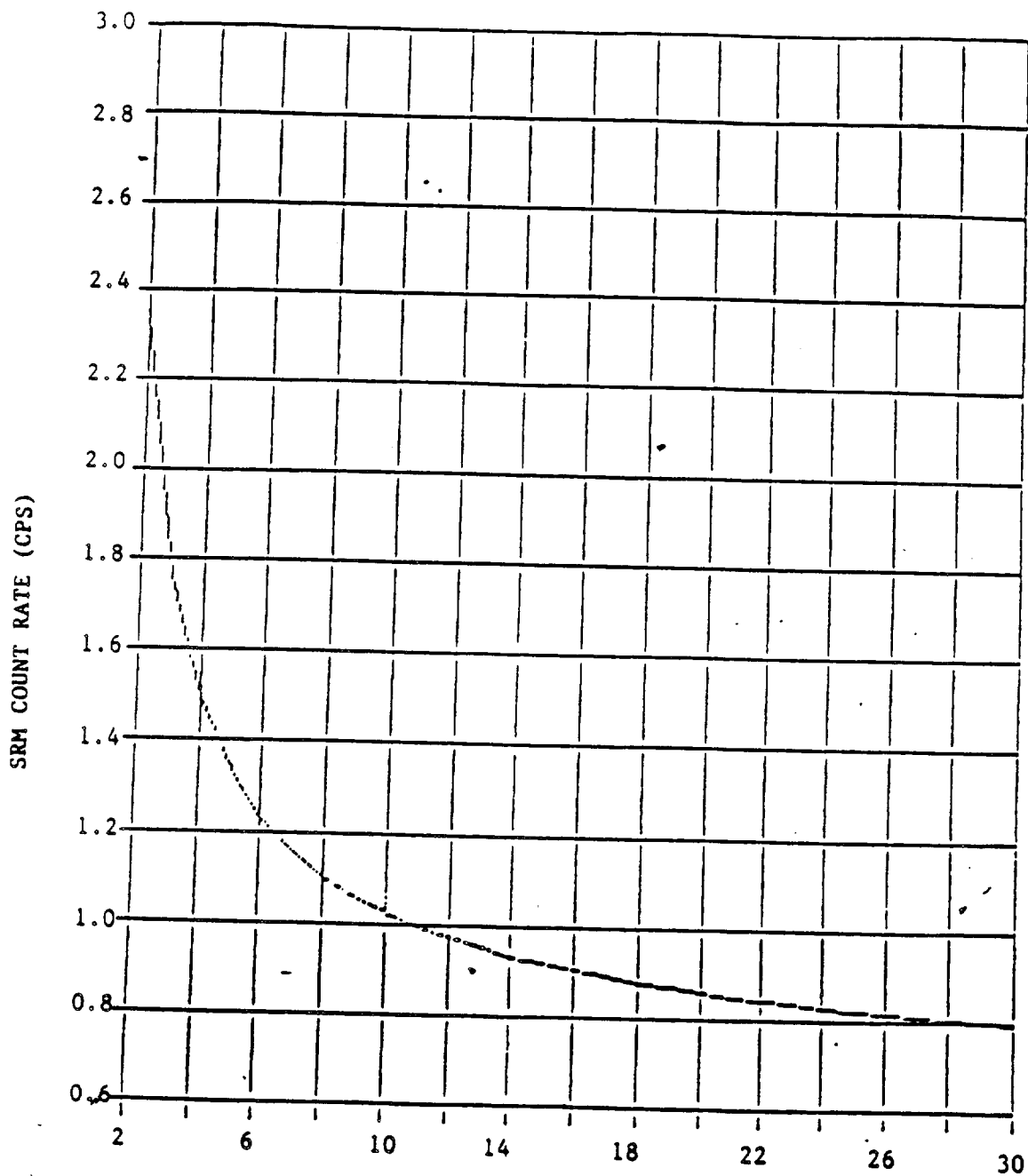
<u>TRIP FUNCTION</u>	<u>TRIP SETPOINT</u>	<u>ALLOWABLE VALUE</u>
6. <u>REACTOR COOLANT SYSTEM RECIRCULATION FLOW</u>		
a. Upscale	< 111% of rated flow	< 114% of rated flow
b. Inoperative	N.A.	N.A.
c. Comparator	< 10% flow deviation	< 11% flow deviation
7. <u>REACTOR MODE SWITCH SHUTDOWN POSITION</u>	N.A.	N.A.

\*The rod block function varies as a function of recirculation loop drive flow (W). The trip setting of the Average Power Range Monitor rod block function must be maintained in accordance with Specification 3.2.2.

\*\*May be reduced provided the Source Range Monitor has an observed count rate and signal-to-noise ratio on or above the curve shown in Figure 3.3.6-1.

\*\*\*Equivalent to 13 gallons/scram discharge volume.

\*\*\*\*The value of N is shown in the CORE OPERATING LIMITS REPORT in accordance with Specifications 6.9.1.9 thru 6.9.1.12.



SIGNAL TO NOISE RATIO  
SRM COUNT RATE VERSUS SIGNAL TO NOISE RATIO

FIGURE 3.3.6-1

## 3/4.2 POWER DISTRIBUTION LIMITS

### BASES

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#### 3/4.2.1 AVERAGE PLANAR LINEAR HEAT GENERATION RATE

This specification assures that the peak cladding temperature (PCT) following the postulated design basis Loss-of-Coolant Accident (LOCA) will not exceed the limits specified in 10 CFR 50.46 and that the fuel design analysis limits specified in NEDE-24011-P-A (Reference 2) will not be exceeded.

Mechanical Design Analysis: NRC approved methods (specified in Reference 2) are used to demonstrate that all fuel rods in a lattice operating at the bounding power history, meet the fuel design limits specified in Reference 2. No single fuel rod follows, or is capable of following, this bounding power history. This bounding power history is used as the basis for the fuel design analysis MAPLHGR limit.

LOCA Analysis: A LOCA analysis is performed in accordance with 10 CFR 50 Appendix K to demonstrate that the permissible planar power (MAPLHGR) limits comply with the ECCS limits specified in 10 CFR 50.46. The analysis is performed for the most limiting break size, break location, and single failure combination for the plant.

The MAPLHGR limit as shown in the CORE OPERATING LIMITS REPORT is the most limiting composite of the fuel mechanical design analysis MAPLHGR and the ECCS MAPLHGR limit.

Only the most limiting MAPLHGR values are shown in the CORE OPERATING LIMITS REPORT for multiple lattice fuel. Compliance with the specific lattice MAPLHGR operating limits, which are available in Reference 3, is ensured by use of the process computer.

The MAPLHGR limits shall be reduced to the value shown in the CORE OPERATING LIMITS REPORT times the two recirculation loop operation limit when in single recirculation loop operation. The constant factor shown in the CORE OPERATING LIMITS REPORT is derived from LOCA analyses initiated from single loop operation to account for earlier boiling transition at the limiting fuel node compared to the standard LOCA evaluations.

## POWER DISTRIBUTION LIMITS

### BASES

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#### 3/4.2.2 APRM SETPOINTS

The fuel cladding integrity Safety Limits of Specification 2.1 were based on a power distribution which would yield the design LHGR at RATED THERMAL POWER. The flow biased neutron flux-upscale scram trip setpoint and flow biased neutron flux-upscale control rod block functions of the APRM instruments must be adjusted to ensure that the MCPR does not become less than the Safety Limit MCPR or that  $> 1\%$  plastic strain does not occur in the degraded situation. The scram and rod block setpoints are adjusted in accordance with the formula in this specification when the combination of THERMAL POWER and CMFLPD indicates a higher peaked power distribution to ensure that an LHGR transient would not be increased in the degraded condition.

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LINERICK - UNIT 1

B 1/4 2-3

Amendment No. 7

AUG 1 - 1961

## POWER DISTRIBUTION LIMITS

### BASES

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#### 3/4.2.3 MINIMUM CRITICAL POWER RATIO

The required operating limit MCPRs at steady-state operating conditions as specified in Specification 3.2.3 are derived from the established fuel cladding integrity Safety Limit MCPR, and an analysis of abnormal operational transients. For any abnormal operating transient analysis evaluation with the initial condition of the reactor being at the steady-state operating limit, it is required that the resulting MCPR does not decrease below the Safety Limit MCPR at any time during the transient assuming instrument trip setting given in Specification 2.2.

To assure that the fuel cladding integrity Safety Limit is not exceeded during any anticipated abnormal operational transient, the most limiting transients have been analyzed to determine which result in the largest reduction in CRITICAL POWER RATIO (CPR). The type of transients evaluated were loss of flow, increase in pressure and power, positive reactivity insertion, and coolant temperature decrease.

The evaluation of a given transient begins with the system initial parameters shown in FSAR Table 15.0-2 that are input to a GE-core dynamic behavior transient computer program. The codes used to evaluate transients are discussed in Reference 2.

The purpose of the  $K_f$  factor shown in the CORE OPERATING LIMITS REPORT is to define operating limits at other than rated core flow conditions. At less than 100% of rated flow the required MCPR is the product of the MCPR and the  $K_f$  factor. The  $K_f$  factors assure that the Safety Limit MCPR will not be violated during a flow increase transient resulting from a motor-generator speed control failure. The  $K_f$  factors may be applied to both manual and automatic flow control modes.

The  $K_f$  factors values shown in the CORE OPERATING LIMITS REPORT were developed generically and are applicable to all BWR/2, BWR/3, and BWR/4 reactors. The  $K_f$  factors were derived using the flow control line corresponding to RATED THERMAL POWER at rated core flow.

For the manual flow control mode, the  $K_f$  factors were calculated such that for the maximum flow rate, as limited by the pump scoop tube set point and the corresponding THERMAL POWER along the rated flow control line, the limiting bundle's relative power was adjusted until the MCPR changes with different core flows. The ratio of the MCPR calculated at a given point of core flow, divided by the operating limit MCPR, determines the  $K_f$ .

## POWER DISTRIBUTION LIMITS

### BASES

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#### MINIMUM CRITICAL POWER RATIO (Continued)

For operation in the automatic flow control mode, the same procedure was employed except the initial power distribution was established such that the MCPR was equal to the operating limit MCPR at RATED THERMAL POWER and rated thermal flow.

The  $K_f$  factors shown in the CORE OPERATING LIMITS REPORT are conservative for the General Electric Boiling Water Reactor plant operation because the operating limit MCPRs of Specification 3.2.3 are greater than the original 1.20 operating limit MCPR used for the generic derivation of  $K_f$ .

At THERMAL POWER levels less than or equal to 25% of RATED THERMAL POWER, the reactor will be operating at minimum recirculation pump speed and the moderator void content will be very small. For all designated control rod patterns which may be employed at this point, operating plant experience indicates that the resulting MCPR value is in excess of requirements by a considerable margin. During initial start-up testing of the plant, a MCPR evaluation will be made at 25% of RATED THERMAL POWER level with minimum recirculation pump speed. The MCPR margin will thus be demonstrated such that future MCPR evaluation below this power level will be shown to be unnecessary. The daily requirement for calculating MCPR when THERMAL POWER is greater than or equal to 25% of RATED THERMAL POWER is sufficient since power distribution shifts are very slow when there have not been significant power or control rod changes. The requirement for calculating MCPR when a limiting control rod pattern is approached ensures that MCPR will be known following a change in THERMAL POWER or power shape, regardless of magnitude, that could place operation at a thermal limit.

#### 3/4.2.4 LINEAR HEAT GENERATION RATE

This specification assures that the Linear Heat Generation Rate (LHGR) in any rod is less than the design linear heat generation even if fuel pellet densification is postulated.

#### References:

1. General Electric Company Analytical Model for Loss-of-Coolant Analysis in Accordance with 10 CFR 50, Appendix K, NEDE-20566, November 1975.
2. "General Electric Standard Application for Reactor Fuel," NEDE-24011-P-A (latest approved revision).
3. "Basis of MAPLHGR Technical Specifications for Limerick Unit 1," NEDO-31401, February 1987 (as amended).
4. Deleted.
5. Increased Core Flow and Partial Feedwater Heating Analysis for Limerick Generating Station Unit 1 Cycle 1, NEDC-31323, October 1986 including Errata and Addenda Sheet No. 1 dated November 6, 1986.



## ADMINISTRATIVE CONTROLS

### ANNUAL RADIOLOGICAL ENVIRONMENTAL OPERATING REPORT

covering all sampling locations keyed to a table giving distances and directions from the centerline of the reactor plant; the results of licensee participation in the Interlaboratory Comparison Program, required by Specification 3.12.3; discussion of all deviations from the Sampling Schedule of Table 4.12.1-1; and discussion of all analyses in which the LLD required by Table 4.12.1-1 was not achievable.

### SEMIANNUAL RADIOACTIVE EFFLUENT RELEASE REPORT\*

6.9.1.8 Routine Semiannual Radioactive Effluent Release Reports covering the operation of the unit during the previous 6 months of operation shall be submitted within 60 days after January 1 and July 1 of each year. The period of the first report shall begin with the date of initial criticality.

The Semiannual Radioactive Effluent Release Reports shall include a summary of the quantities of radioactive liquid and gaseous effluents and solid waste released from the facility as outlined in Regulatory Guide 1.21, "Measuring, Evaluating, and Reporting Radioactivity in Solid Wastes and Releases of Radioactive Materials in Liquid and Gaseous Effluents from Light-Water-Cooled Nuclear Power Plants," Revision 1, June 1974, with data summarized on a quarterly basis following the format of Appendix B thereof.

The Semiannual Radioactive Effluent Release Report to be submitted 60 days after January 1 of each year shall include an annual summary of hourly meteorological data collected over the previous year. This annual summary may be either in the form of an hour-by-hour listing on magnetic tape of wind speed, wind direction and atmospheric stability, and precipitation (if measured), or in the form of joint frequency distributions of wind speed, wind direction, atmospheric stability.\*\* This same report shall include an assessment of the radiation doses due to the radioactive liquid and gaseous effluents released from the unit or station during the previous calendar year. This same report shall also include an assessment of the radiation doses from radioactive liquid and gaseous effluents to MEMBERS OF THE PUBLIC due to their activities inside the SITE BOUNDARY (Figures 5.1.3-1a and 5.1.3-1b) during the report period. All assumptions used in making these assessments (i.e., specific activity, exposure time and location) shall be included in these reports. The assessment of radiation doses shall be performed in accordance with the methodology and parameters of the OFFSITE DOSE CALCULATION MANUAL (ODCM).

\*A single submittal may be made for a multiple unit station. The submittal should combine those sections that are common to all units at the station.

\*\*In lieu of submission with the first half year Semiannual Radioactive Effluent Release Report, the licensee has the option of retaining this summary of required meteorological data on site in a file that shall be provided to the NRC upon request.

## ADMINISTRATIVE CONTROLS

### SEMIANNUAL RADIOACTIVE EFFLUENT RELEASE REPORT (Continued)

The Semiannual Radioactive Effluent Release Report to be submitted 60 days after January 1 of each year shall also include an assessment of radiation doses to the likely most exposed MEMBER OF THE PUBLIC from reactor releases and other nearby uranium fuel cycle sources (including doses from primary effluent pathways and direct radiation) for the previous calendar year to show conformance with 40 CFR Part 190, Environmental Radiation Protection Standards for Nuclear Power Operation. Acceptable methods for calculating the dose contribution from liquid and gaseous effluents are given in Regulatory Guide 1.109, Rev. 1, October 1977.

The Semiannual Radioactive Effluent Release Reports shall include the following information for each type of solid waste (as defined in 10 CFR Part 61) shipped offsite during the report period:

- a. Container volume,
- b. Total curie quantity (specify whether determined by measurement or estimate,
- c. Principal radionuclides (specify whether determined by measurement or estimate),
- d. Source of waste and processing employed (e.g., dewatered spent resin, compacted dry waste, evaporator bottoms),
- e. Type of container (e.g., LSA, Type A, Type B, Large Quantity), and
- f. SOLIDIFICATION agent or absorbent (e.g., cement; urea formaldehyde).

The Semiannual Radioactive Effluent Release Reports shall include a list and description of unplanned releases from the site to UNRESTRICTED AREAS of radioactive materials in gaseous and liquid effluents made during the reporting period.

The Semiannual Radioactive Effluent Release Reports shall include any changes made during the reporting period to the PROCESS CONTROL PROGRAM (PCP) and to the ODCM, as well as a listing of new locations for dose calculations and/or environmental monitoring identified by the land use census pursuant to Specification 3.12.2.

## ADMINISTRATIVE CONTROLS

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### CORE OPERATING LIMITS REPORT

6.9.1.9 Core Operating Limits shall be established prior to each reload cycle, or prior to any remaining portion of a reload cycle, and shall be documented in the CORE OPERATING LIMITS REPORT for the following:

- a. The AVERAGE PLANAR LINEAR HEAT GENERATION RATE (APLHGR) for Specification 3.2.1,
- b. The MINIMUM CRITICAL POWER RATIO (MCPR) for Specification 3.2.3,
- c. The  $K_f$  core flow adjustment factor for Specification 3.2.3,
- d. The LINEAR HEAT GENERATION RATE (LHGR) for Specification 3.2.4,
- e. The upscale flow biased Rod Block Monitor setpoint and the upscale high flow clamped Rod Block monitor setpoint of Specification 3.3.6.

6.9.1.10 The analytical methods used to determine the core operating limits shall be those previously reviewed and approved by the NRC, specifically those described in the following document:

- a. NEDE-24011-P-A "General Electric Standard Application for Reactor Fuel" (Latest approved revision).

6.9.1.11 The core operating limits shall be determined such that all applicable limits (e.g., fuel thermal-mechanical limits, core thermal-hydraulic limits, ECCS limits, nuclear limits such as SHUTDOWN MARGIN, transient analysis limits, and accident analysis limits) of the safety analysis are met.

6.9.1.12 The CORE OPERATING LIMITS REPORT, including any mid-cycle revisions or supplements, shall be provided upon issuance for each reload cycle to the NRC Document Control Desk with copies to the Regional Administrator and Resident Inspector.

### SPECIAL REPORTS

6.9.2 Special reports shall be submitted to the Regional Administrator of the Regional Office of the NRC within the time period specified for each report.



UNITED STATES  
NUCLEAR REGULATORY COMMISSION  
WASHINGTON, D. C. 20555

PHILADELPHIA ELECTRIC COMPANY

DOCKET NO. 50-353

LIMERICK GENERATING STATION, UNIT 2

AMENDMENT TO FACILITY OPERATING LICENSE

Amendment No. 4  
License No. NPF-85

1. The Nuclear Regulatory Commission (the Commission) has found that
  - A. The application for amendment by Philadelphia Electric Company (the licensee) dated February 23, 1990, complies with the standards and requirements of the Atomic Energy Act of 1954, as amended (the Act), and the Commission's rules and regulations set forth in 10 CFR Chapter I;
  - B. The facility will operate in conformity with the application, the provisions of the Act, and the rules and regulations of the Commission;
  - C. There is reasonable assurance (i) that the activities authorized by this amendment can be conducted without endangering the health and safety of the public, and (ii) that such activities will be conducted in compliance with the Commission's regulations;
  - D. The issuance of this amendment will not be inimical to the common defense and security or to the health and safety of the public; and
  - E. The issuance of this amendment is in accordance with 10 CFR Part 51 of the Commission's regulations and all applicable requirements have been satisfied.
2. Accordingly, the license is amended by changes to the Technical Specifications as indicated in the attachment to this license amendment, and paragraph 2.C.(2) of Facility Operating License No. NPF-85 is hereby amended to read as follows:

Technical Specifications

The Technical Specifications contained in Appendix A and the Environmental Protection Plan contained in Appendix B, as revised through Amendment No. 4, are hereby incorporated into this license. Philadelphia Electric Company shall operate the facility in accordance with the Technical Specifications and the Environmental Protection Plan.

3. This license amendment is effective as of its date of issuance.

FOR THE NUCLEAR REGULATORY COMMISSION

/s/

Walter R. Butler, Director  
Project Directorate I-2  
Division of Reactor Projects I/II

Attachment:  
Changes to the Technical  
Specifications

Date of Issuance: May 15, 1990

PDI-2/PM  
MO'Brien  
5/14/90

PDI-2/PM  
RClark:mjt  
04/04/90

OGC 03  
4/12/90

PDI-2/D  
WButler  
5/15/90

3. This license amendment is effective as of its date of issuance.

FOR THE NUCLEAR REGULATORY COMMISSION

A handwritten signature in cursive script, reading "Walter R. Butler".

Walter R. Butler, Director  
Project Directorate I-2  
Division of Reactor Projects I/II

Attachment:  
Changes to the Technical  
Specifications

Date of Issuance: May 15, 1990

ATTACHMENT TO LICENSE AMENDMENT NO. 4

FACILITY OPERATING LICENSE NO. NPF-85

DOCKET NO. 50-353

Replace the following pages of the Appendix A Technical Specifications with the attached page. The revised pages are identified by Amendment number and contain vertical lines indicating the area of change. Overleaf pages are provided to maintain document completeness.\*

Remove

Insert

i	i
ii	ii*
v	v
vi	vi
xxvii	xxvii
xxviii	xxviii*
1-1	1-1*
1-2	1-2
3/4 2-1	3/4 2-1
3/4 2-2	3/4 2-2
3/4 2-3	-
3/4 2-4	-
3/4 2-5	-
3/4 2-6	-
3/4 2-6a	-
-	-
3/4 2-7	3/4 2-7*
3/4 2-8	3/4 2-8
3/4 2-8a	-
-	-
3/4 2-9	3/4 2-9
3/4 2-10	3/4 2-10
3/4 2-11	3/4 2-11
3/4 2-12	-
3/4 3-59	3/4 3-59*
3/4 3-60	3/4 3-60

ATTACHMENT TO LICENSE AMENDMENT NO. 4

FACILITY OPERATING LICENSE NO. NPF-85

DOCKET NO. 50-353

Remove

3/4 3-60a  
3/4 3-60b

B 3/4 2-1  
B 3/4 2-2

B 3/4 2-3  
B 3/4 2-4

B 3/4 2-5  
-

6-17  
6-18  
-  
-

Insert

3/4 3-60a  
3/4 3-60b\*

B 3/4 2-1  
B 3/4 2-2

B 3/4 2-3\*  
B 3/4 2-4

B 3/4 2-5  
-

6-17\*  
6-18

6-18a  
-



## INDEX

### DEFINITIONS

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## 1.0 DEFINITIONS

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The following terms are defined so that uniform interpretation of these specifications may be achieved. The defined terms appear in capitalized type and shall be applicable throughout these Technical Specifications.

### ACTION

1.1 ACTION shall be that part of a Specification which prescribes remedial measures required under designated conditions.

### AVERAGE PLANAR EXPOSURE

1.2 The AVERAGE PLANAR EXPOSURE shall be applicable to a specific planar height and is equal to the sum of the exposure of all the fuel rods in the specified bundle at the specified height divided by the number of fuel rods in the fuel bundle.

### AVERAGE PLANAR LINEAR HEAT GENERATION RATE

1.3 The AVERAGE PLANAR LINEAR HEAT GENERATION RATE (APLHGR) shall be applicable to a specific planar height and is equal to the sum of the LINEAR HEAT GENERATION RATES for all the fuel rods in the specified bundle at the specified height divided by the number of fuel rods in the fuel bundle.

### CHANNEL CALIBRATION

1.4 A CHANNEL CALIBRATION shall be the adjustment, as necessary, of the channel output such that it responds with the necessary range and accuracy to known values of the parameter which the channel monitors. The CHANNEL CALIBRATION shall encompass the entire channel including the sensor and alarm and/or trip functions, and shall include the CHANNEL FUNCTIONAL TEST. The CHANNEL CALIBRATION may be performed by any series of sequential, overlapping or total channel steps such that the entire channel is calibrated.

### CHANNEL CHECK

1.5 A CHANNEL CHECK shall be the qualitative assessment of channel behavior during operation by observation. This determination shall include, where possible, comparison of the channel indication and/or status with other indications and/or status derived from independent instrument channels measuring the same parameter.

### CHANNEL FUNCTIONAL TEST

1.6 A CHANNEL FUNCTIONAL TEST shall be:

- a. Analog channels - the injection of a simulated signal into the channel as close to the sensor as practicable to verify OPERABILITY including alarm and/or trip functions and channel failure trips.
- b. Bistable channels - the injection of a simulated signal into the sensor to verify OPERABILITY including alarm and/or trip functions.

The CHANNEL FUNCTIONAL TEST may be performed by any series of sequential, overlapping or total channel steps such that the entire channel is tested.

## DEFINITIONS

### CORE ALTERATION

- 1.7 CORE ALTERATION shall be the addition, removal, relocation or movement of fuel, sources, or reactivity controls within the reactor pressure vessel with the vessel head removed and fuel in the vessel. Normal movement of the SRMs, IRMs, TIPS, or special movable detectors is not considered a CORE ALTERATION. Suspension of CORE ALTERATIONS shall not preclude completion of the movement of a component to a safe conservative position.

### CORE OPERATING LIMITS REPORT

- 1.7a The CORE OPERATING LIMITS REPORT (COLR) is the unit-specific document that provides the core operating limits for the current operating reload cycle. These cycle-specific core operating limits shall be determined for each reload cycle in accordance with Specifications 6.9.1.9 thru 6.9.12. Plant operation within these limits is addressed in individual specifications.

### CRITICAL POWER RATIO

- 1.8 The CRITICAL POWER RATIO (CPR) shall be the ratio of that power in the assembly which is calculated by application of the (GEXL) correlation to cause some point in the assembly to experience boiling transition, divided by the actual assembly operating power.

### DOSE EQUIVALENT I-131

- 1.9 DOSE EQUIVALENT I-131 shall be that concentration of I-131, microcuries per gram, which alone would produce the same thyroid dose as the quantity and isotopic mixture of I-131, I-132, I-133, I-134, and I-135 actually present. The thyroid dose conversion factors used for this calculation shall be those listed in Table III of TID-14844, "Calculation of Distance Factors for Power and Test Reactor Sites."

### $\bar{E}$ -AVERAGE DISINTEGRATION ENERGY

- 1.10  $\bar{E}$  shall be the average, weighted in proportion to the concentration of each radionuclide in the reactor coolant at the time of sampling, of the sum of the average beta and gamma energies per disintegration, in MeV, for isotopes, with half lives greater than 15 minutes, making up at least 95% of the total noniodine activity in the coolant.

### EMERGENCY CORE COOLING SYSTEM (ECCS) RESPONSE TIME

- 1.11 The EMERGENCY CORE COOLING SYSTEM (ECCS) RESPONSE TIME shall be that time interval from when the monitored parameter exceeds its ECCS actuation set-point at the channel sensor until the ECCS equipment is capable of performing its safety function, i.e., the valves travel to their required positions, pump discharge pressures reach their required values, etc. Times shall include diesel generator starting and sequence loading delays where applicable. The response time may be measured by any series of sequential, overlapping or total steps such that the entire response time is measured.

### END-OF-CYCLE RECIRCULATION PUMP TRIP SYSTEM RESPONSE TIME

- 1.12 The END-OF-CYCLE RECIRCULATION PUMP TRIP SYSTEM RESPONSE TIME shall be that time interval to complete suppression of the electric arc between the fully open contacts of the recirculation pump circuit breaker from initial movement of the associated:
- Turbine stop valves, and
  - Turbine control valves.



### 3/4.2 POWER DISTRIBUTION LIMITS

#### 3/4.2.1 AVERAGE PLANAR LINEAR HEAT GENERATION RATE

##### LIMITING CONDITION FOR OPERATION

---

3.2.1 All AVERAGE PLANAR LINEAR HEAT GENERATION RATES (APLHGRs) for each type of fuel as a function of AVERAGE PLANAR EXPOSURE shall not exceed the limits shown in the CORE OPERATING LIMITS REPORT for two recirculation loop operation. During single loop operation, the APLHGR for each fuel type shall not exceed the above values multiplied by the reduction factors shown in the CORE OPERATING LIMITS REPORT.

APPLICABILITY: OPERATIONAL CONDITION 1, when THERMAL POWER is greater than or equal to 25% of RATED THERMAL POWER.

##### ACTION:

With an APLHGR exceeding the limiting value, initiate corrective action within 15 minutes and restore APLHGR to within the required limits within 2 hours or reduce THERMAL POWER to less than 25% of RATED THERMAL POWER within the next 4 hours.

##### SURVEILLANCE REQUIREMENTS

---

4.2.1 All APLHGRs shall be verified to be equal to or less than the limiting value:

- a. At least once per 24 hours,
- b. Within 12 hours after completion of a THERMAL POWER increase of at least 15% of RATED THERMAL POWER, and
- c. Initially and at least once per 12 hours when the reactor is operating with a LIMITING CONTROL ROD PATTERN for APLHGR.
- d. The provisions of Specification 4.0.4 are not applicable.

Figures on pages  
3/4 2-2 thru 3/4 2-6  
have been removed from Technical  
Specifications, and relocated to the  
CORE OPERATING LIMITS REPORT.

Technical Specifications pages  
3/4 2-3 thru 3/4 2-6a  
have been INTENTIONALLY OMITTED.

## POWER DISTRIBUTION LIMITS

### 3/4.2.2 APRM SETPOINTS

#### LIMITING CONDITION FOR OPERATION

3.2.2 The APRM flow biased neutron flux-upscale scram trip setpoint (S) and flow biased neutron flux-upscale control rod block trip setpoint ( $S_{RB}$ ) shall be established according to the following relationships:

	TRIP SETPOINT	ALLOWABLE VALUE
During two recirculation loop operation	$S \leq (0.58W + 59\%)T$	$S \leq (0.58W + 62\%)T$
	$S_{RB} \leq (0.58W + 50\%)T$	$S_{RB} \leq (0.58W + 53\%)T$
During single recirculation loop operation	$S \leq (0.58W + 54\%)T$	$S \leq (0.58W + 57\%)T$
	$S_{RB} \leq (0.58W + 45\%)T$	$S_{RB} \leq (0.58W + 48\%)T$

where: S and  $S_{RB}$  are in percent of RATED THERMAL POWER,  
W = Loop recirculation flow as a percentage of the loop recirculation flow which produces a rated core flow of 100 million lbs/hr,  
T = Lowest value of the ratio of FRACTION OF RATED THERMAL POWER divided by the CORE MAXIMUM FRACTION OF LIMITING POWER DENSITY.  
T is applied only if less than or equal to 1.0.

APPLICABILITY: OPERATIONAL CONDITION 1, when THERMAL POWER is greater than or equal to 25% of RATED THERMAL POWER.

#### ACTION:

With the APRM flow biased neutron flux-upscale scram trip setpoint and/or the flow biased neutron flux-upscale control rod block trip setpoint less conservative than the value shown in the Allowable Value column for S or  $S_{RB}$ , as above determined, initiate corrective action within 15 minutes and adjust S and/or  $S_{RB}$  to be consistent with the Trip Setpoint values\* within 6 hours or reduce THERMAL POWER to less than 25% of RATED THERMAL POWER within the next 4 hours.

#### SURVEILLANCE REQUIREMENTS

4.2.2 The F RTP and the MFLPD shall be determined, the value of T calculated, and the most recent actual APRM flow biased neutron flux-upscale scram and flow biased neutron flux-upscale control rod block trip setpoints verified to be within the above limits or adjusted, as required:

- At least once per 24 hours,
- Within 12 hours after completion of a THERMAL POWER increase of at least 15% of RATED THERMAL POWER, and
- Initially and at least once per 12 hours when the reactor is operating with MFLPD greater than or equal to F RTP.
- The provisions of Specification 4.0.4 are not applicable.

\*With MFLPD greater than the F RTP, rather than adjusting the APRM setpoints, the APRM gain may be adjusted such that the APRM readings are greater than or equal to 100% times MFLPD, provided that the adjusted APRM reading does not exceed 100% of RATED THERMAL POWER and a notice of adjustment is posted on the reactor control panel.

## POWER DISTRIBUTION LIMITS

### 3/4.2.3 MINIMUM CRITICAL POWER RATIO

#### LIMITING CONDITION FOR OPERATION

3.2.3 The MINIMUM CRITICAL POWER RATIO (MCPR) shall be equal to or greater than the MCPR limit determined using the appropriate figure in the CORE OPERATING LIMITS REPORT, times the  $K_f$  shown in the CORE OPERATING LIMITS REPORT, provided that the end-of-cycle recirculation pump trip (EOC-RPT) system is OPERABLE per Specification 3.3.4.2, with:

$$\tau = \frac{(\tau_{ave} - \tau_B)}{\tau_A - \tau_B}$$

where:

$\tau_A$  = 0.86 seconds, control rod average scram insertion time limit to notch 39 per Specification 3.1.3.3,

$$\tau_B = 0.688 + 1.65 \left[ \frac{N_1}{\sum_{i=1}^n N_i} \right]^{1/2} (0.052),$$

$$\tau_{ave} = \frac{\sum_{i=1}^n N_i \tau_i}{\sum_{i=1}^n N_i},$$

$n$  = number of surveillance tests performed to date in cycle,

$N_i$  = number of active control rods measured in the  $i^{th}$  surveillance test,

$\tau_i$  = average scram time to notch 39 of all rods measured in the  $i^{th}$  surveillance test, and

$N_1$  = total number of active rods measured in Specification 4.1.3.2.a.

#### APPLICABILITY:

OPERATIONAL CONDITION 1, when THERMAL POWER is greater than or equal to 25% of RATED THERMAL POWER.

## POWER DISTRIBUTION LIMITS

### LIMITING CONDITION FOR OPERATION (Continued)

#### ACTION:

- a. With the end-of-cycle recirculation pump trip system inoperable per Specification 3.3.4.2, operation may continue provided that, within 1 hour, MCPR is determined to be greater than or equal to the MCPR limit as a function of the average scram time shown in the appropriate figure in the CORE OPERATING LIMITS REPORT, for EOC-RPT inoperable curve, times the  $K_f$  shown in the CORE OPERATING LIMITS REPORT.
- b. With MCPR less than the applicable MCPR limit shown in the CORE OPERATING LIMITS REPORT, initiate corrective action within 15 minutes and restore MCPR to within the required limit within 2 hours or reduce THERMAL POWER to less than 25% of RATED THERMAL POWER within the next 4 hours.

### SURVEILLANCE REQUIREMENTS

#### 4.2.3 MCPR, with:

- a.  $\tau = 1.0$  prior to performance of the initial scram time measurements for the cycle in accordance with Specification 4.1.3.2, or
- b.  $\tau$  as defined in Specification 3.2.3 used to determine the limit within 72 hours of the conclusion of each scram time surveillance test required by Specification 4.1.3.2,

shall be determined to be equal to or greater than the applicable MCPR limit determined from the appropriate figure in the CORE OPERATING LIMITS REPORT times the  $K_f$  shown in the CORE OPERATING LIMITS REPORT.

- a. At least once per 24 hours,
- b. Within 12 hours after completion of a THERMAL POWER increase of at least 15% of RATED THERMAL POWER, and
- c. Initially and at least once per 12 hours when the reactor is operating with a LIMITING CONTROL ROD PATTERN for MCPR.
- d. The provisions of Specification 4.0.4 are not applicable.

Figures on pages  
3/4 2-10 thru 3/4 2-11  
have been removed from  
Technical Specifications, and  
relocated to the CORE OPERATING  
LIMITS REPORT.

Technical Specifications pages  
3/4 2-10a and 3/4 2-11  
have been INTENTIONALLY OMITTED.

## POWER DISTRIBUTION LIMITS

### 3/4.2.4 LINEAR HEAT GENERATION RATE

#### LIMITING CONDITION FOR OPERATION

---

3.2.4 The LINEAR HEAT GENERATION RATE (LHGR) shall not exceed the value in the CORE OPERATING LIMITS REPORT.

APPLICABILITY: OPERATIONAL CONDITION 1, when THERMAL POWER is greater than or equal to 25% of RATED THERMAL POWER.

#### ACTION:

With the LHGR of any fuel rod exceeding the limit, initiate corrective action within 15 minutes and restore the LHGR to within the limit within 2 hours or reduce THERMAL POWER to less than 25% of RATED THERMAL POWER within the next 4 hours.

#### SURVEILLANCE REQUIREMENTS

---

4.2.4 LHGRs shall be determined to be equal to or less than the limit:

- a. At least once per 24 hours,
- b. Within 12 hours after completion of a THERMAL POWER increase of at least 15% of RATED THERMAL POWER, and
- c. Initially and at least once per 12 hours when the reactor is operating on a LIMITING CONTROL ROD PATTERN for LHGR.
- d. The provisions of Specification 4.0.4 are not applicable.

TABLE 3.3.6-1 (Continued)

CONTROL ROD WITHDRAWAL BLOCK INSTRUMENTATION

ACTION STATEMENTS

- ACTION 60 - Declare the RBM inoperable and take the ACTION required by Specification 3.1.4.3.
- ACTION 61 - With the number of OPERABLE channels one or more less than required by the Minimum OPERABLE Channels per Trip Function requirement, place at least one inoperable channel in the tripped condition within one hour.
- ACTION 62 - With the number of OPERABLE channels less than required by the Minimum OPERABLE Channels per Trip Function requirement, place the inoperable channel in the tripped condition within one hour.
- ACTION 63 - With the number of OPERABLE channels less than required by the Minimum OPERABLE Channels per Trip Function requirement, initiate a rod block.

NOTES

- \* With THERMAL POWER  $\geq$  30% of RATED THERMAL POWER.
- \*\* With more than one control rod withdrawn. Not applicable to control rods removed per Specification 3.9.10.1 or 3.9.10.2.
- \*\*\* These channels are not required when sixteen or fewer fuel assemblies, adjacent to the SRMs, are in the core.
- (a) The RBM shall be automatically bypassed when a peripheral control rod is selected or the reference APRM channel indicates less than 30% of RATED THERMAL POWER.
- (b) This function shall be automatically bypassed if detector count rate is > 100 cps or the IRM channels are on range 3 or higher.
- (c) This function is automatically bypassed when the associated IRM channels are on range 8 or higher.
- (d) This function is automatically bypassed when the IRM channels are on range 3 or higher.
- (e) This function is automatically bypassed when the IRM channels are on range 1.



TABLE 3.3.6-2  
CONTROL ROD BLOCK INSTRUMENTATION SETPOINTS

<u>TRIP FUNCTION</u>	<u>TRIP SETPOINT</u>	<u>ALLOWABLE VALUE</u>
1. <u>ROD BLOCK MONITOR ****</u>		
a. Upscale		
1) During two recirculation loop operation		
a. Flow Biased*	$\leq 0.66 \text{ W} + (N-66)\%$ , with a maximum of,	$\leq 0.66 \text{ W} + (N-63)\%$ , with a maximum of,
b. High Flow Clamped	$\leq N\%$	$\leq (N-3)\%$
2) During single recirculation loop operation		
a. Flow Biased*	$\leq 0.66 \text{ W} + (N-72)\%$ , with a maximum of,	$\leq 0.66 \text{ W} + (N-69)\%$ , with a maximum of,
b. High Flow Clamped	$\leq N\%$	$\leq (N+3)\%$
b. Inoperative	N.A.	N.A.
c. Downscale	$\geq 5\%$ of RATED THERMAL POWER	$\geq 3\%$ of RATED THERMAL POWER
2. <u>APRM</u>		
a. Flow Biased Neutron Flux - Upscale		
1) During two recirculation loop operation	$\leq 0.58 \text{ W} + 50\%^*$	$\leq 0.58 \text{ W} + 53\%^*$
2) During single recirculation loop operation	$\leq 0.58 \text{ W} + 45\%^*$	$\leq 0.58 \text{ W} + 48\%^*$
b. Inoperative	N.A.	N.A.
c. Downscale	$> 4\%$ of RATED THERMAL POWER	$> 3\%$ of RATED THERMAL POWER
d. Neutron Flux - Upscale, Startup	$\leq 12\%$ of RATED THERMAL POWER	$\leq 14\%$ of RATED THERMAL POWER
3. <u>SOURCE RANGE MONITORS</u>		
a. Detector not full in	N.A.	N.A.
b. Upscale	$< 1 \times 10^5 \text{ cps}$	$< 1.6 \times 10^5 \text{ cps}$
c. Inoperative	N.A.	N.A.
d. Downscale	$> 3 \text{ cps}^{**}$	$> 1.8 \text{ cps}^{**}$

TABLE 3.3.6-2 (Continued)

CONTROL ROD BLOCK INSTRUMENTATION SETPOINTS

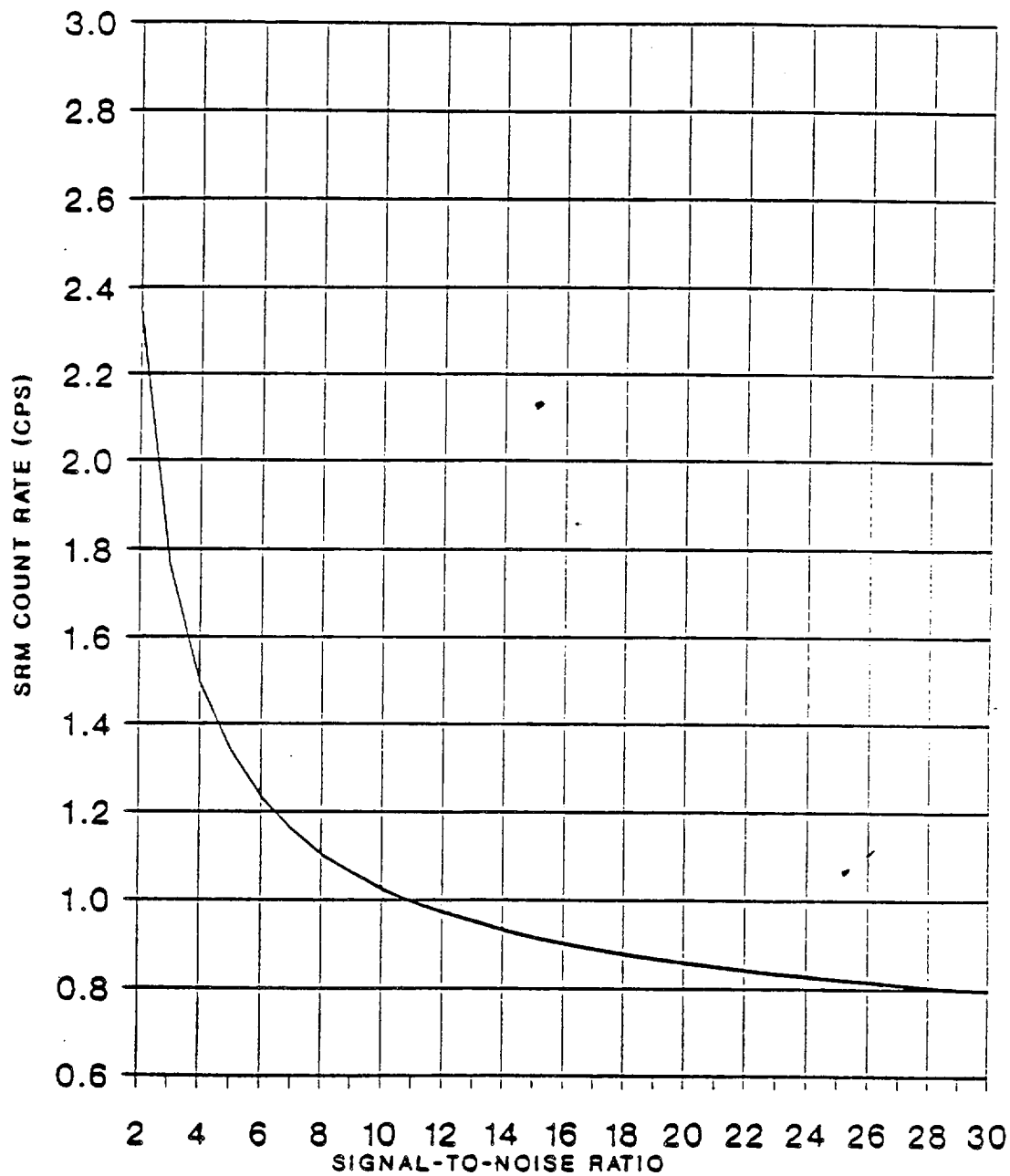
<u>TRIP FUNCTION</u>	<u>TRIP SETPOINT</u>	<u>ALLOWABLE VALUE</u>
4. <u>INTERMEDIATE RANGE MONITORS</u>		
a. Detector not full in	N.A.	N.A.
b. Upscale	< 108/125 divisions of full scale	< 110/125 divisions of full scale
c. Inoperative	N.A.	N.A.
d. Downscale	> 5/125 divisions of full scale	> 3/125 divisions of full scale
5. <u>SCRAM DISCHARGE VOLUME</u>		
a. Water Level-High	< 257' 7 3/8" elevation***	< 257' 9 3/8" elevation
a. Float Switch		
6. <u>REACTOR COOLANT SYSTEM RECIRCULATION FLOW</u>		
a. Upscale	< 111% of rated flow	< 114% of rated flow
b. Inoperative	N.A.	N.A.
c. Comparator	< 10% flow deviation	< 11% flow deviation
7. <u>REACTOR MODE SWITCH SHUTDOWN POSITION</u>	N.A.	N.A.

\*The rod block function varies as a function of recirculation loop drive flow (W). The trip setting of the average power range monitor rod block function must be maintained in accordance with Specification 3.2.2.

\*\*May be reduced, provided the source range monitor has an observed count rate and signal-to-noise ratio on or above the curve shown in Figure 3.3.6-1.

\*\*\*Equivalent to 13.56 gallons/scram discharge volume.

\*\*\*\*The value of N is shown in the CORE OPERATING LIMITS REPORT in accordance with Specifications 6.9.1.9 thru 6.9.1.12.



SRM COUNT RATE VERSUS SIGNAL-TO-NOISE RATIO

Figure 3.3.6-1

### 3/4.2 POWER DISTRIBUTION LIMITS

#### BASES

---

The specifications of this section assure that the peak cladding temperature following the postulated design basis loss-of-coolant accident will not exceed the 2200°F limit specified in 10 CFR 50.46.

#### 3/4.2.1 AVERAGE PLANAR LINEAR HEAT GENERATION RATE

The peak cladding temperature (PCT) following a postulated loss-of-coolant accident is primarily a function of the average heat generation rate of all the rods of a fuel assembly at any axial location and is dependent only secondarily on the rod to rod power distribution within an assembly. The peak clad temperature is calculated assuming a LHGR for the highest powered rod which is equal to or less than the design LHGR corrected for densification. This LHGR times 1.02 is used in the heatup code along with the exposure dependent steady state gap conductance and rod-to-rod local peaking factor. The AVERAGE PLANAR LINEAR HEAT GENERATION RATE (APLHGR) limit as shown in the CORE OPERATING LIMITS REPORT is the LHGR of the highest powered rod divided by its local peaking factor. The limiting value for APLHGR is shown in the CORE OPERATING LIMITS REPORT.

The calculational procedure used to establish the APLHGR shown in the CORE OPERATING LIMITS REPORT is based on a loss-of-coolant accident analysis. The analysis was performed using General Electric (GE) calculational models which are consistent with the requirements of Appendix K to 10 CFR Part 50. A complete discussion of each code employed in the analysis is presented in Reference 1. Differences in this analysis compared to previous analyses can be broken down as follows.

#### a. Input Changes

1. Corrected Vaporization Calculation - coefficients in the vaporization correlation used in the REFLOOD code were corrected.
2. Incorporated more accurate bypass areas - The bypass areas in the top guide were recalculated using a more accurate technique.
3. Corrected guide tube thermal resistance.
4. Correct heat capacity of reactor internals heat nodes.

#### b. Model Change

1. Core CCFL pressure differential - 1 psi - Incorporate the assumption that flow from the bypass to lower plenum must overcome a 1 psi pressure drop in core.
2. Incorporate NRC pressure transfer assumption - The assumption used in the SAFE-REFLOOD pressure transfer when the pressure is increasing was changed.

## POWER DISTRIBUTION LIMITS

### BASES

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#### AVERAGE PLANAR LINEAR HEAT GENERATION RATE (Continued)

A few of the changes affect the accident calculation irrespective of CCFL. These changes are listed below.

a. Input Change

1. Break Areas - The DBA break area was calculated more accurately.

b. Model Change

1. Improved Radiation and Conduction Calculation - Incorporation of CHASTE 05 for heatup calculation.

A list of the significant plant input parameters to the loss-of-coolant accident analysis is presented in Bases Table B 3/4.2.1-1.

The MAPLHGR limits shall be reduced to the value shown in the CORE OPERATING LIMITS REPORT times the two recirculation loop operation limit when in single recirculation loop operation. The constant factor shown in the CORE OPERATING LIMITS REPORT is derived from LOCA analyses initiated from single loop operation to account for earlier boiling transition at the limiting fuel node compared to the standard LOCA evaluations.

#### 3/4.2.2 APRM SETPOINTS

The fuel cladding integrity Safety Limits of Specification 2.1 were based on a power distribution which would yield the design LHGR at RATED THERMAL POWER. The flow biased neutron flux-upscale scram trip setpoint and flow biased neutron flux-upscale control rod block functions of the APRM instruments must be adjusted to ensure that the MCPR does not become less than the Safety Limit MCPR or that  $> 1\%$  plastic strain does not occur in the degraded situation. The scram and rod block setpoints are adjusted in accordance with the formula in this specification when the combination of THERMAL POWER and CMFLPD indicates a higher peaked power distribution to ensure that an LHGR transient would not be increased in the degraded condition.

BASES TABLE B 3/4.2.1-1

SIGNIFICANT INPUT PARAMETERS TO THE  
LOSS-OF-COOLANT ACCIDENT ANALYSIS

Plant Parameters:

Core THERMAL POWER ..... 3430 Mwt\* which corresponds  
to 105% of rated steam flow

Vessel Steam Output ..... 14.86 x 10<sup>6</sup> lbm/h which  
corresponds to 105% of rated  
steam flow

Vessel Steam Dome Pressure ..... 1055 psia

Design Basis Recirculation Line  
Break Area for:

a. Large Breaks 4.1 ft<sup>2</sup>, 1.0 ft<sup>2</sup>

b. Small Breaks 1.0 ft<sup>2</sup>, 0.07 ft<sup>2</sup>, 0.09 ft<sup>2</sup>, 0.02 ft<sup>2</sup>

Fuel Parameters:

FUEL TYPE	FUEL BUNDLE GEOMETRY	PEAK TECHNICAL SPECIFICATION LINEAR HEAT GENERATION RATE (kw/ft)	DESIGN AXIAL PEAKING FACTOR	INITIAL MINIMUM CRITICAL POWER RATIO
Initial Core	8 x 8	13.4	1.4	1.20

A more detailed listing of input of each model and its source is presented in Section 11 of Reference 1 and subsection 15.0.2 of the FSAR.

\*This power level meets the Appendix K requirement of 102%. The core heatup calculation assumes a bundle power consistent with operation of the highest powered rod at 102% of its Technical Specification LINEAR HEAT GENERATION RATE limit.

## POWER DISTRIBUTION LIMITS

### BASES

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#### 3/4.2.3 MINIMUM CRITICAL POWER RATIO

The required operating limit MCPRs at steady-state operating conditions as specified in Specification 3.2.3 are derived from the established fuel cladding integrity Safety Limit MCPR and an analysis of abnormal operational transients. For any abnormal operating transient analysis evaluation with the initial condition of the reactor being at the steady-state operating limit, it is required that the resulting MCPR does not decrease below the Safety Limit MCPR at any time during the transient assuming instrument trip setting given in Specification 2.2.

To assure that the fuel cladding integrity Safety Limit is not exceeded during any anticipated abnormal operational transient, the most limiting transients have been analyzed to determine which result in the largest reduction in CRITICAL POWER RATIO (CPR). The type of transients evaluated were loss of flow, increase in pressure and power, positive reactivity insertion, and coolant temperature decrease.

The evaluation of a given transient begins with the system initial parameters shown in FSAR Table 15.0-2 that are input to a GE-core dynamic behavior transient computer program. The codes used to evaluate transients are discussed in Reference 2.

The purpose of the  $K_f$  factor shown in the CORE OPERATING LIMITS REPORT is to define operating limits at other than rated core flow conditions. At less than 100% of rated flow the required MCPR is the product of the MCPR and the  $K_f$  factor. The  $K_f$  factors assure that the Safety Limit MCPR will not be violated during a flow increase transient resulting from a motor-generator speed control failure. The  $K_f$  factors may be applied to both manual and automatic flow control modes.

The  $K_f$  factors values shown in the CORE OPERATING LIMITS REPORT were developed generically and are applicable to all BWR/2, BWR/3, and BWR/4 reactors. The  $K_f$  factors were derived using the flow control line corresponding to RATED THERMAL POWER at rated core flow.

For the manual flow control mode, the  $K_f$  factors were calculated such that for the maximum flow rate, as limited by the pump scoop tube set point and the corresponding THERMAL POWER along the rated flow control line, the limiting bundle's relative power was adjusted until the MCPR changes with different core flows. The ratio of the MCPR calculated at a given point of core flow, divided by the operating limit MCPR, determines the  $K_f$ .

## POWER DISTRIBUTION LIMITS

### BASES

#### MINIMUM CRITICAL POWER RATIO (Continued)

For operation in the automatic flow control mode, the same procedure was employed except the initial power distribution was established such that the MCPR was equal to the operating limit MCPR at RATED THERMAL POWER and rated thermal flow.

The  $K_f$  factors shown in the CORE OPERATING LIMITS REPORT are conservative for the General Electric Boiling Water Reactor plant operation because the operating limit MCPRs of Specification 3.2.3 are greater than the original 1.20 operating limit MCPR used for the generic derivation of  $K_f$ .

At THERMAL POWER levels less than or equal to 25% of RATED THERMAL POWER, the reactor will be operating at minimum recirculation pump speed and the moderator void content will be very small. For all designated control rod patterns which may be employed at this point, operating plant experience indicates that the resulting MCPR value is in excess of requirements by a considerable margin. During initial start-up testing of the plant, a MCPR evaluation will be made at 25% of RATED THERMAL POWER level with minimum recirculation pump speed. The MCPR margin will thus be demonstrated such that future MCPR evaluation below this power level will be shown to be unnecessary. The daily requirement for calculating MCPR when THERMAL POWER is greater than or equal to 25% of RATED THERMAL POWER is sufficient since power distribution shifts are very slow when there have not been significant power or control rod changes. The requirement for calculating MCPR when a limiting control rod pattern is approached ensures that MCPR will be known following a change in THERMAL POWER or power shape, regardless of magnitude, that could place operation at a thermal limit.

#### 3/4.2.4 LINEAR HEAT GENERATION RATE

This specification assures that the Linear Heat Generation Rate (LHGR) in any rod is less than the design linear heat generation even if fuel pellet densification is postulated.

#### References:

1. General Electric Company Analytical Model for Loss-of-Coolant Analysis in Accordance with 10 CFR 50, Appendix K, NEDE-20566, November 1975.
2. "General Electric Standard Application for Reactor Fuel," NEDE-24011-P-A (latest approved revision).
3. Deleted.
4. Deleted.
5. Increased Core Flow and Partial Feedwater Heating Analysis for Limerick Generating Station Unit 2 Cycle 1, NEDC-31578P, March 1989 including Errata and Addenda Sheet No. 1 dated May 31, 1989.
6. General Electric Boiling Water Reactor Extended Load Line Limit Analysis for Limerick Generating Station Unit 2, Cycle 1, NEDC-31677P, March 1989.



## ADMINISTRATIVE CONTROLS

### ANNUAL RADIOLOGICAL ENVIRONMENTAL OPERATING REPORT (Continued)

covering all sampling locations keyed to a table giving distances and directions from the centerline of the reactor plant; the results of licensee participation in the Interlaboratory Comparison Program, required by Specification 3.12.3; discussion of all deviations from the Sampling Schedule of Table 4.12.1-1; and discussion of all analyses in which the LLD required by Table 4.12.1-1 was not achievable.

### SEMIANNUAL RADIOACTIVE EFFLUENT RELEASE REPORT\*

6.9.1.8 Routine Semiannual Radioactive Effluent Release Reports covering the operation of the unit during the previous 6 months of operation shall be submitted within 60 days after January 1 and July 1 of each year. The period of the first report shall begin with the date of initial criticality.

The Semiannual Radioactive Effluent Release Reports shall include a summary of the quantities of radioactive liquid and gaseous effluents and solid waste released from the facility as outlined in Regulatory Guide 1.21, "Measuring, Evaluating, and Reporting Radioactivity in Solid Wastes and Releases of Radioactive Materials in Liquid and Gaseous Effluents from Light-Water-Cooled Nuclear Power Plants," Revision 1, June 1974, with data summarized on a quarterly basis following the format of Appendix B thereof.

The Semiannual Radioactive Effluent Release Report to be submitted 60 days after January 1 of each year shall include an annual summary of hourly meteorological data collected over the previous year. This annual summary may be either in the form of an hour-by-hour listing on magnetic tape of wind speed, wind direction and atmospheric stability, and precipitation (if measured), or in the form of joint frequency distributions of wind speed, wind direction, atmospheric stability.\*\* This same report shall include an assessment of the radiation doses due to the radioactive liquid and gaseous effluents released from the unit or station during the previous calendar year. This same report shall also include an assessment of the radiation doses from radioactive liquid and gaseous effluents to MEMBERS OF THE PUBLIC due to their activities inside the SITE BOUNDARY (Figures 5.1.3-1a and 5.1.3-1b) during the report period. All assumptions used in making these assessments (i.e., specific activity, exposure time and location) shall be included in these reports. The assessment of radiation doses shall be performed in accordance with the methodology and parameters of the OFFSITE DOSE CALCULATION MANUAL (ODCM).

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\*A single submittal may be made for a multiple unit station. The submittal should combine those sections that are common to all units at the station.

\*\*In lieu of submission with the first half year Semiannual Radioactive Effluent Release Report, the licensee has the option of retaining this summary of required meteorological data on site in a file that shall be provided to the NRC upon request.

## ADMINISTRATIVE CONTROLS

### SEMIANNUAL RADIOACTIVE EFFLUENT RELEASE REPORT (Continued)

The Semiannual Radioactive Effluent Release Report to be submitted 60 days after January 1 of each year shall also include an assessment of radiation doses to the likely most exposed MEMBER OF THE PUBLIC from reactor releases and other nearby uranium fuel cycle sources (including doses from primary effluent pathways and direct radiation) for the previous calendar year to show conformance with 40 CFR Part 190, Environmental Radiation Protection Standards for Nuclear Power Operation. Acceptable methods for calculating the dose contribution from liquid and gaseous effluents are given in Regulatory Guide 1.109, Rev. 1, October 1977.

The Semiannual Radioactive Effluent Release Reports shall include the following information for each type of solid waste (as defined in 10 CFR Part 61) shipped offsite during the report period:

- a. Container volume,
- b. Total curie quantity (specify whether determined by measurement or estimate,
- c. Principal radionuclides (specify whether determined by measurement or estimate),
- d. Source of waste and processing employed (e.g., dewatered spent resin, compacted dry waste, evaporator bottoms),
- e. Type of container (e.g., LSA, Type A, Type B, Large Quantity), and
- f. SOLIDIFICATION agent or absorbent (e.g., cement; urea formaldehyde).

The Semiannual Radioactive Effluent Release Reports shall include a list and description of unplanned releases from the site to UNRESTRICTED AREAS of radioactive materials in gaseous and liquid effluents made during the reporting period.

The Semiannual Radioactive Effluent Release Reports shall include any changes made during the reporting period to the PROCESS CONTROL PROGRAM (PCP) and to the ODCM, as well as a listing of new locations for dose calculations and/or environmental monitoring identified by the land use census pursuant to Specification 3.12.2.

## ADMINISTRATIVE CONTROLS

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### CORE OPERATING LIMITS REPORT

6.9.1.9 Core operating limits shall be established prior to each reload cycle, or prior to any remaining portion of a reload cycle, and shall be documented in the CORE OPERATING LIMITS REPORT for the following:

- a. The AVERAGE PLANAR LINEAR HEAT GENERATION RATE (APLHGR) for Specification 3.2.1,
- b. The MINIMUM CRITICAL POWER RATIO (MCPR) for Specification 3.2.3,
- c. The  $K_f$  core flow adjustment factor for Specification 3.2.3,
- d. The LINEAR HEAT GENERATION RATE (LHGR) for Specification 3.2.4,
- e. The upscale flow biased Rod Block Monitor setpoint and the upscale high flow clamped Rod Block Monitor setpoint of Specification 3.3.6.

6.9.1.10 The analytical methods used to determine the core operating limits shall be those previously reviewed and approved by the NRC, specifically those described in the following document:

- a. NEDE-24011-P-A "General Electric Standard Application for Reactor Fuel" (Latest approved revision).

6.9.1.11 The core operating limits shall be determined such that all applicable limits (e.g., fuel thermal-mechanical limits, core thermal-hydraulic limits, ECCS limits, nuclear limits such as SHUTDOWN MARGIN, transient analysis limits, and accident analysis limits) of the safety analysis are met.

6.9.1.12 The CORE OPERATING LIMITS REPORT, including any mid-cycle revisions or supplements, shall be provided upon issuance for each reload cycle to the NRC Document Control Desk with copies to the Regional Administrator and Resident Inspector.

### SPECIAL REPORTS

6.9.2 Special reports shall be submitted to the Regional Administrator of the Regional Office of the NRC within the time period specified for each report.



UNITED STATES  
NUCLEAR REGULATORY COMMISSION  
WASHINGTON, D. C. 20555

SAFETY EVALUATION BY THE OFFICE OF NUCLEAR REACTOR REGULATION

SUPPORTING AMENDMENT NOS. 37 AND 4 TO FACILITY OPERATING

LICENSE NOS. NPF-39 AND NPF-85

PHILADELPHIA ELECTRIC COMPANY

LIMERICK GENERATING STATION, UNITS 1 AND 2

DOCKET NOS. 50-352 AND 50-353

**1.0 INTRODUCTION**

By letter dated February 23, 1990, Philadelphia Electric Company (the licensee) requested an amendment to Facility Operating License Nos. NPF-39 and NPF-85 for the Limerick Generating Station, Units 1 and 2. These proposed amendments would change the Technical Specifications (TSs) to remove cycle specific parameter limits in accordance with NRC Generic Letter (GL) 88-16, "Removal of Cycle Specific Parameter Limits from Technical Specifications" issued October 4, 1988. The proposed changes would replace the values of cycle-specific parameter limits with a reference to the Core Operating Limits Report, which contains the values of those limits. In addition, the Core Operating Limits Report (COLR) has been included in the Definitions Section of the TSs to note that it is the unit-specific document that provides these limits for the current operating reload cycle. Furthermore, the definition notes that the values of these cycle-specific parameter limits are to be determined in accordance with the Specification 6.9.1. This Specification requires that the Core Operating Limits be determined for each reload cycle in accordance with the referenced NRC-approved methodology for these limits and consistent with the applicable limits of the safety analysis. Finally, this report and any mid-cycle revisions shall be provided to the NRC upon issuance.

Guidance on the proposed changes was developed by NRC on the basis of the review of a lead-plant proposal submitted on the Oconee plant docket that was endorsed by the Babcock and Wilcox Owners Group. This guidance was provided to all power reactor licensees and applicants by Generic Letter 88-16, dated October 4, 1988.

**2.0 EVALUATION**

The licensee's proposed changes to the TS are in accordance with the guidance provided by Generic Letter 88-16 and are addressed below.

- (1) The Definitions section of the TS was modified to include a definition of the COLR that requires cycle/reload-specific parameter limits to be established on a unit-specific basis in accordance with

an NRC-approved methodology that maintains the limits of the safety analysis. The definition notes that plant operation within these limits is addressed by individual specifications.

- (2) The following specifications were revised to replace the values of cycle-specific parameter limits with a reference to the COLR that provides these limits.

(a) Revise the Index.

- i. Remove figure references currently in Sections 3/4.2.1, "Average Planar Linear Heat Generation Rate," and 3/4.2.3, "Minimum Critical Power Ratio (MCPR)," for figures which are being relocated to the COLR. Insert a note on Index pages v and vi which describes the TS pages which have information intentionally omitted and references a note on a designated page. This note lets the reader know that information has been intentionally omitted and also gives a reference where the reader can find further information.
- ii. Move information (which is not being deleted) on the affected Index pages vi and via (for Unit 1 only) to reflect deletion of the figure references.
- iii. Eliminate page via (for Unit 1 only), since it is no longer required to accommodate references to figures which are being deleted.
- iv. Insert "Core Operating Limits Report," into the "Administrative Controls Section," 6.9, "Reporting Requirements" under Section 6.9.1, "Routine Reports."

(b) Revise Section 3/4.2, "Power Distribution Limits."

- i. Revise Section 3/4.2.1, "Average Planar Linear Heat Generation Rate," by deleting the phrase "which have been approved" and inserting in its place the phrase "determined by approved methodology." Remove all figure references and add a reference to the COLR in Section 3/4.2.1 for the limiting values. Remove Figures 3.2.1-1 thru 3.2.1-5, and for Unit 1 only, also remove Figures 3.2.1-6 thru 3.2.1-8. Insert a note on page 3/4 2-2 describing which pages have been removed and that the information previously on pages 3/4 2-2 thru 2-6a (thru 3/4 2-6c for Unit 1) has been relocated to the COLR.
- ii. Revise Section 3/4.2.3, "Minimum Critical Power Ratio," to remove Figures 3.2.3-1a, 3.2.3-1b and Figure 3.2.3-2. Remove Figures 3.2.3-1c and 3.2.3-1d from the Unit 1 TS

only. Remove Table 3.2.3-1 from the Unit 2 TS only and note that the page has been intentionally left blank. Remove all figure and table references and add a reference to the COLR for the limiting values and the  $k_f$  curve. Insert a note on page 3/4 2-10 describing which pages have been removed and that the information previously on pages 3/4 2-10 thru 3/4 2-11 has been relocated to the COLR.

- iii. Revise Section 3/4.2.4, "Linear Heat Generation Rate (LHGR)," to reference the COLR for limiting values.
  - iv. Revise Section 3/4.3.6, "Rod Block Monitor (RBM)," Table 3.3.6-2, Trip Function 1.a (RBM upscale) by replacing the RBM high flow clamped setpoint of 106 with the constant "N." Revise all other cycle specific constants to functions of "N" (e.g., change 109 to (N+3)). The value of "N" is a cycle specific limit and is therefore referenced in the COLR.
- (c) Modify Bases 3/4.2.1 and 3/4.2.3 to reference the COLR.
  - (d) Insert Sections 6.9.1.9 thru 6.9.1.12 into the "Administration Controls" Section 6.9.1, "Routine Reports." These Sections specify the information to be included in the COLR and the requirement to submit the COLR to the NRC. Specifically, this specification requires that the COLR be submitted, upon issuance, to the NRC Document Control Desk with copies to the Regional Administrator and Resident Inspector. The report provides the values of cycle-specific parameter limits that are applicable for the current fuel cycle. Furthermore, this specification requires that the values of these limits be established using the NRC-approved methodology in NEDE-24011-P-A "General Electric Standard Application for Reactor Fuel" (Latest approved revision) and consistent with all applicable limits of the safety analysis. Finally, the specification requires that all changes in cycle-specific parameter limits be documented in the COLR before each reload cycle or remaining part of a reload cycle and submitted upon issuance to NRC, prior to operation with the new parameter limits.
  - (e) Move Section 6.9.2, "Special Reports," from page 6-18 to 6-18a to accommodate the addition of Sections 6.9.1.9 thru 6.9.1.12.

On the basis of the review of the above items, the NRC staff concludes that the licensee provided an acceptable response to those items as addressed in the NRC guidance in Generic Letter 88-16 on modifying cycle-specific parameter limits in TS. Because plant operation continues to be limited in accordance with the values of cycle-specific parameter limits that are established using an NRC-approved methodology, the NRC

staff concludes that this change is administrative in nature and there is no impact on plant safety as a consequence. Accordingly, the staff finds the proposed changes acceptable. The NRC staff, with the knowledge and consent of the licensee, made minor typographical and administrative corrections to the licensee's incoming Technical Specification pages.

As part of the implementation of Generic Letter 88-16, the staff has also reviewed a sample COLR that was provided by the licensee. On the basis of this review, the staff concludes that the format and content of the sample COLR are acceptable.

### 3.0 ENVIRONMENTAL CONSIDERATION

These amendments involve changes in recordkeeping, reporting, or administrative procedures or requirements. Accordingly, the amendments meet the eligibility criteria for categorical exclusion set forth in 10 CFR 51.22(c)(9) and (10). Pursuant to 10 CFR 51.22(b), no environmental impact statement or environmental assessment need be prepared in connection with the issuance with the issuance of these amendments.

### 4.0 CONCLUSION

The Commission made a proposed determination that these amendments involve no significant hazards consideration which was published in the Federal Register (55 FR 10543) on March 21, 1990 and consulted with the Commonwealth of Pennsylvania. No public comments were received and the Commonwealth of Pennsylvania did not have any comments.

The staff has concluded, based on the considerations discussed above, that: (1) there is reasonable assurance that the health and safety of the public will not be endangered by operation in the proposed manner, and (2) such activities will be conducted in compliance with the Commission's regulations and the issuance of these amendments will not be inimical to the common defense and the security nor to the health and safety of the public.

Dated: May 15, 1990

#### Principal Contributors:

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