

March 22, 1989

Docket No.: 50-352

Mr. George A. Hunger, Jr.  
Director-Licensing  
Philadelphia Electric Company  
Correspondence Control Desk  
P. O. Box 7520  
Philadelphia, Pennsylvania 19101

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Dear Mr. Hunger:

SUBJECT: DELETION OF ROD SEQUENCE CONTROL SYSTEM AND LOWERING OF ROD WORTH MINIMIZER LOW POWER SET POINT TO 10 PERCENT (TAC NO. 71584)

RE: LIMERICK GENERATING STATION, UNIT 1

The Commission has issued the enclosed Amendment No. 17 to Facility Operating License No. NPF-39 for the Limerick Generating Station, Unit 1. This amendment consists of changes to the Technical Specifications (TSs) in response to your application dated December 14, 1988.

This amendment changes the TSs to permit removal of the Rod Sequence Control System and to reduce the Rod Worth Minimizer Low Power Setpoint. For purposes of SIMS, please advise us when modification 5910 is implemented.

A copy of our Safety Evaluation is also enclosed. Notice of Issuance will be included in the Commission's biweekly Federal Register notice.

Sincerely,

Original signed by  
Richard J. Clark

Richard J. Clark, Project Manager  
Project Directorate I-2  
Division of Reactor Projects I/II  
Office of Nuclear Reactor Regulation

Enclosures:

1. Amendment No. 17 to License No. NPF-39
2. Safety Evaluation

cc w/enclosures:  
See next page

DFOI  
1/1

[HUNGER LETT]

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03/03/89

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3/13/89

PDI-2/D  
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3/20/89

NRR/SRXB  
WHodges  
3/20/89

*[Handwritten signature]*



UNITED STATES  
NUCLEAR REGULATORY COMMISSION  
WASHINGTON, D. C. 20555

March 22, 1989

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Director-Licensing  
Philadelphia Electric Company  
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P. O. Box 7520  
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Sincerely,

A handwritten signature in black ink that reads "Richard J. Clark".

Richard J. Clark, Project Manager  
Project Directorate I-2  
Division of Reactor Projects I/II  
Office of Nuclear Reactor Regulation

Enclosures:

1. Amendment No.17 to License No. NPF-39
2. Safety Evaluation

cc w/enclosures:  
See next page

Mr. George A. Hunger, Jr.  
Philadelphia Electric Company

Limerick Generating Station  
Units 1 & 2

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UNITED STATES  
NUCLEAR REGULATORY COMMISSION  
WASHINGTON, D. C. 20555

PHILADELPHIA ELECTRIC COMPANY

DOCKET NO. 50-352

LIMERICK GENERATING STATION, UNIT 1

AMENDMENT TO FACILITY OPERATING LICENSE

Amendment No. 17  
License No. NPF-39

1. The Nuclear Regulatory Commission (the Commission) has found that
  - A. The application for amendment by Philadelphia Electric Company (the licensee) dated December 14, 1988, complies with the standards and requirements of the Atomic Energy Act of 1954, as amended (the Act), and the Commission's rules and regulations set forth in 10 CFR Chapter I;
  - B. The facility will operate in conformity with the application, the provisions of the Act, and the rules and regulations of the Commission;
  - C. There is reasonable assurance (i) that the activities authorized by this amendment can be conducted without endangering the health and safety of the public, and (ii) that such activities will be conducted in compliance with the Commission's regulations;
  - D. The issuance of this amendment will not be inimical to the common defense and security or to the health and safety of the public; and
  - E. The issuance of this amendment is in accordance with 10 CFR Part 51 of the Commission's regulations and all applicable requirements have been satisfied.
2. Accordingly, the license is amended by changes to the Technical Specifications as indicated in the attachment to this license amendment, and paragraph 2.C.(2) of Facility Operating License No. NPF-39 is hereby amended to read as follows:

Technical Specifications

The Technical Specifications contained in Appendix A and the Environmental Protection Plan contained in Appendix B, as revised through Amendment No. 17, are hereby incorporated into this license. Philadelphia Electric Company shall operate the facility in accordance with the Technical Specifications and the Environmental Protection Plan.

8903310052 890322  
PDR ADOCK 05000352  
P FDC

3. This license amendment is effective as of its date of issuance.

FOR THE NUCLEAR REGULATORY COMMISSION

A handwritten signature in cursive script that reads "Walter R. Butler".

Walter R. Butler, Director  
Project Directorate I-2  
Division of Reactor Projects I/II

Attachment:  
Changes to the Technical  
Specifications

Date of Issuance: March 22, 1989

ATTACHMENT TO LICENSE AMENDMENT NO. 17

FACILITY OPERATING LICENSE NO. NPF-39

DOCKET NO. 50-352

Replace the following pages of the Appendix A Technical Specifications with the attached pages. The revised pages are identified by Amendment number and contain vertical lines indicating the area of change. Overleaf pages are provided to maintain document completeness.\*

<u>Remove</u>	<u>Insert</u>
v	v
vi	vi*
xv	xv*
xvi	xvi
xxi	xxi*
xxii	xxii
B 2-5	B 2-5*
B 2-6	B 2-6
3/4 1-3	3/4 1-3*
3/4 1-4	3/4 1-4
3/4 1-11	3/4 1-11
3/4 1-12	3/4 1-12*
3/4 1-13	3/4 1-13
3/4 1-14	3/4 1-14*
3/4 1-15	3/4 1-15*
3/4 1-16	3/4 1-16
3/4 1-17	3/4 1-17
3/4 1-18	3/4 1-18*
3/4 10-1	3/4 10-1*
3/4 10-2	3/4 10-2
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## SAFETY LIMITS

### BASES

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#### 2.1.3 REACTOR COOLANT SYSTEM PRESSURE

The Safety Limit for the reactor coolant system pressure has been selected such that it is at a pressure below which it can be shown that the integrity of the system is not endangered. The reactor pressure vessel is designed to Section III of the ASME Boiler and Pressure Vessel Code 1968 Edition, including Addenda through Summer 1969, which permits a maximum pressure transient of 110%, 1375 psig, of design pressure 1250 psig. The Safety Limit of 1325 psig, as measured by the reactor vessel steam dome pressure indicator, is equivalent to 1375 psig at the lowest elevation of the reactor coolant system. The reactor coolant system is designed to the ASME Boiler and Pressure Vessel Code, 77<sup>th</sup> Edition, including Addenda through Summer 1977 for the reactor recirculation piping, which permits a maximum pressure transient of 110%, 1375 psig of design pressure, 1250 psig for suction piping and 1500 psig for discharge piping. The pressure Safety Limit is selected to be the lowest transient overpressure allowed by the ASME Boiler and Pressure Vessel Code Section III, Class I.

#### 2.1.4 REACTOR VESSEL WATER LEVEL

With fuel in the reactor vessel during periods when the reactor is shutdown, consideration must be given to water level requirements due to the effect of decay heat. If the water level should drop below the top of the active irradiated fuel during this period, the ability to remove decay heat is reduced. This reduction in cooling capability could lead to elevated cladding temperatures and clad perforation in the event that the water level became less than two-thirds of the core height. The Safety Limit has been established at the top of the active irradiated fuel to provide a point which can be monitored and also provide adequate margin for effective action.

## 2.2 LIMITING SAFETY SYSTEM SETTINGS

### BASES

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#### 2.2.1 REACTOR PROTECTION SYSTEM INSTRUMENTATION SETPOINTS

The Reactor Protection System instrumentation setpoints specified in Table 2.2.1-1 are the values at which the reactor trips are set for each parameter. The Trip Setpoints have been selected to ensure that the reactor core and reactor coolant system are prevented from exceeding their Safety Limits during normal operation and design basis anticipated operational occurrences and to assist in mitigating the consequences of accidents. Operation with a trip set less conservative than its Trip Setpoint but within its specified Allowable Value is acceptable on the basis that the difference between each Trip Setpoint and the Allowable Value is equal to or less than the drift allowance assumed for each trip in the safety analyses.

##### 1. Intermediate Range Monitor, Neutron Flux - High

The IRM system consists of 8 chambers, 4 in each of the reactor trip systems. The IRM is a 5 decade 10 range instrument. The trip setpoint of 120 divisions of scale is active in each of the 10 ranges. Thus as the IRM is ranged up to accommodate the increase in power level, the trip setpoint is also ranged up. The IRM instruments provide for overlap with both the APRM and SRM systems.

The most significant source of reactivity changes during the power increase is due to control rod withdrawal. In order to ensure that the IRM provides the required protection, a range of rod withdrawal accidents have been analyzed. The results of these analyses are in Section 15.4 of the FSAR. The most severe case involves an initial condition in which THERMAL POWER is at approximately 1% of RATED THERMAL POWER. Additional conservatism was taken in this analysis by assuming the IRM channel closest to the control rod being withdrawn is bypassed. The results of this analysis show that the reactor is shutdown and peak power is limited to 21% of RATED THERMAL POWER with the peak fuel enthalpy well below the fuel failure threshold of 170 cal/gm. Based on this analysis, the IRM provides protection against local control rod errors and continuous withdrawal of control rods in sequence and provides backup protection for the APRM.

##### 2. Average Power Range Monitor

For operation at low pressure and low flow during STARTUP, the APRM scram setting of 15% of RATED THERMAL POWER provides adequate thermal margin between the setpoint and the Safety Limits. The margin accommodates the anticipated maneuvers associated with power plant startup. Effects of increasing pressure at zero or low void content are minor and cold water from sources available during startup is not much colder than that already in the system. Temperature coefficients are small and control rod patterns are constrained by the RWM. Of all the possible sources of reactivity input, uniform control rod withdrawal is the most probable cause of significant power increase.

## REACTIVITY CONTROL SYSTEMS

### 3/4.1.3 CONTROL RODS

#### CONTROL ROD OPERABILITY

##### LIMITING CONDITION FOR OPERATION

---

3.1.3.1 All control rods shall be OPERABLE.

APPLICABILITY: OPERATIONAL CONDITIONS 1 and 2.

ACTION:

- a. With one control rod inoperable due to being immovable, as a result of excessive friction or mechanical interference, or known to be untrippable:
  1. Within 1 hour:
    - a) Verify that the inoperable control rod, if withdrawn, is separated from all other inoperable control rods by at least two control cells in all directions.
    - b) Disarm the associated directional control valves\*\* either:
      - 1) Electrically, or
      - 2) Hydraulically by closing the drive water and exhaust water isolation valves.

Otherwise, be in at least HOT SHUTDOWN within the next 12 hours.
  2. Restore the inoperable control rod to OPERABLE status within 48 hours or be in at least HOT SHUTDOWN within the next 12 hours.
- b. With one or more control rods trippable but inoperable for causes other than addressed in ACTION a, above:
  1. If the inoperable control rod(s) is withdrawn, within 1 hour:
    - a) Verify that the inoperable withdrawn control rod(s) is separated from all other inoperable withdrawn control rods by at least two control cells in all directions, and
    - b) Demonstrate the insertion capability of the inoperable withdrawn control rod(s) by inserting the control rod(s) at least one notch by drive water pressure within the normal operating range\*.

Otherwise, insert the inoperable withdrawn control rod(s) and disarm the associated directional control valves\*\* either:

    - a) Electrically, or
    - b) Hydraulically by closing the drive water and exhaust water isolation valves.

---

\*The inoperable control rod may then be withdrawn to a position no further withdrawn than its position when found to be inoperable.

\*\*May be rearmed intermittently, under administrative control, to permit testing associated with restoring the control rod to OPERABLE status.

## REACTIVITY CONTROL SYSTEMS

### LIMITING CONDITION FOR OPERATION (Continued)

#### ACTION: (Continued)

2. If the inoperable control rod(s) is inserted, within 1 hour disarm the associated directional control valves\*\* either:
  - a) Electrically, or
  - b) Hydraulically by closing the drive water and exhaust water isolation valves.Otherwise, be in at least HOT SHUTDOWN within the next 12 hours.
3. The provisions of Specification 3.0.4 are not applicable.
- c. With more than 8 control rods inoperable, be in at least HOT SHUTDOWN within 12 hours.

#### SURVEILLANCE REQUIREMENTS

4.1.3.1.1 The scram discharge volume drain and vent valves shall be demonstrated OPERABLE by:

- a. At least once per 31 days verifying each valve to be open,\* and
- b. At least once per 92 days cycling each valve through at least one complete cycle of full travel.

4.1.3.1.2 When above the preset power level of the RWM, all withdrawn control rods not required to have their directional control valves disarmed electrically or hydraulically shall be demonstrated OPERABLE by moving each control rod at least one notch:

- a. At least once per 7 days, and
- b. At least once per 24 hours when any control rod is immovable as a result of excessive friction or mechanical interference.

4.1.3.1.3 All control rods shall be demonstrated OPERABLE by performance of Surveillance Requirements 4.1.3.2, 4.1.3.4, 4.1.3.5, 4.1.3.6, and 4.1.3.7.

---

\*These valves may be closed intermittently for testing under administrative controls.

\*\*May be rearmed intermittently, under administrative control, to permit testing associated with restoring the control rod to OPERABLE status.

## REACTIVITY CONTROL SYSTEMS

### CONTROL ROD DRIVE COUPLING

#### LIMITING CONDITION FOR OPERATION

---

3.1.3.6 All control rods shall be coupled to their drive mechanisms.

APPLICABILITY: OPERATIONAL CONDITIONS 1, 2, and 5\*.

ACTION:

- a. In OPERATIONAL CONDITIONS 1 and 2 with one control rod not coupled to its associated drive mechanism, within 2 hours:
  1. If permitted by the RWM, insert the control rod drive mechanism to accomplish recoupling and verify recoupling by withdrawing the control rod, and:
    - a) Observing any indicated response of the nuclear instrumentation, and
    - b) Demonstrating that the control rod will not go to the over-travel position.Otherwise, be in at least HOT SHUTDOWN within the next 12 hours.
  2. If recoupling is not accomplished on the first attempt or, if not permitted by the RWM, then until permitted by the RWM, declare the control rod inoperable, insert the control rod and disarm the associated directional control valves\*\* either:
    - a) Electrically, or
    - b) Hydraulically by closing the drive water and exhaust water isolation valves.Otherwise, be in at least HOT SHUTDOWN within the next 12 hours.
- b. In OPERATIONAL CONDITION 5\* with a withdrawn control rod not coupled to its associated drive mechanism, within 2 hours either:
  1. Insert the control rod to accomplish recoupling and verify recoupling by withdrawing the control rod and demonstrating that the control rod will not go to the overtravel position, or
  2. If recoupling is not accomplished, insert the control rod and disarm the associated directional control valves\*\* either:
    - a) Electrically, or
    - b) Hydraulically by closing the drive water and exhaust water isolation valves.
- c. The provisions of Specification 3.0.4 are not applicable.

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\*At least each withdrawn control rod. Not applicable to control rods removed per Specification 3.9.10.1 or 3.9.10.2.

\*\*May be rearmed intermittently, under administrative control, to permit testing associated with restoring the control rod to OPERABLE status.

## REACTIVITY CONTROL SYSTEMS

### SURVEILLANCE REQUIREMENTS

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4.1.3.6 Each affected control rod shall be demonstrated to be coupled to its drive mechanism by observing any indicated response of the nuclear instrumentation while withdrawing the control rod to the fully withdrawn position and then verifying that the control rod drive does not go to the overtravel position:

- a. Prior to reactor criticality after completing CORE ALTERATIONS that could have affected the control rod drive coupling integrity,
- b. Anytime the control rod is withdrawn to the "Full out" position in subsequent operation, and
- c. Following maintenance on or modification to the control rod or control rod drive system which could have affected the control rod drive coupling integrity.

## REACTIVITY CONTROL SYSTEMS

### CONTROL ROD POSITION INDICATION

#### LIMITING CONDITION FOR OPERATION

---

3.1.3.7 The control rod position indication system shall be OPERABLE.

APPLICABILITY: OPERATIONAL CONDITIONS 1, 2, and 5\*.

ACTION:

- a. In OPERATIONAL CONDITION 1 or 2 with one or more control rod position indicators inoperable, within 1 hour:
  1. Determine the position of the control rod by using an alternate method, or:
    - a) Moving the control rod, by single notch movement, to a position with an OPERABLE position indicator,
    - b) Returning the control rod, by single notch movement, to its original position, and
    - c) Verifying no control rod drift alarm at least once per 12 hours, or
  2. Move the control rod to a position with an OPERABLE position indicator, or
  3. When THERMAL POWER is:
    - a) Within the preset power level of the RWM, declare the control rod inoperable.
    - b) Greater than the preset power level of the RWM, declare the control rod inoperable, insert the control rod and disarm the associated directional control valves\*\* either:
      - 1) Electrically, or
      - 2) Hydraulically by closing the drive water and exhaust water isolation valves.

Otherwise, be in at least HOT SHUTDOWN within the next 12 hours.
- b. In OPERATIONAL CONDITION 5\* with a withdrawn control rod position indicator inoperable, move the control rod to a position with an OPERABLE position indicator or insert the control rod.
- c. The provisions of Specification 3.0.4 are not applicable.

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\*At least each withdrawn control rod. Not applicable to control rods removed per Specification 3.9.10.1 or 3.9.10.2.

\*\*May be rearmed intermittently, under administrative control, to permit testing associated with restoring the control rod to OPERABLE status.

## REACTIVITY CONTROL SYSTEMS

### SURVEILLANCE REQUIREMENTS

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4.1.3.7 The control rod position indication system shall be determined OPERABLE by verifying:

- a. At least once per 24 hours that the position of each control rod is indicated,
- b. That the indicated control rod position changes during the movement of the control rod drive when performing Surveillance Requirement 4.1.3.1.2, and
- c. That the control rod position indicator corresponds to the control rod position indicated by the "Full out" position indicator when performing Surveillance Requirement 4.1.3.6b.

## REACTIVITY CONTROL SYSTEMS

### CONTROL ROD DRIVE HOUSING SUPPORT

#### LIMITING CONDITION FOR OPERATION

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3.1.3.8 The control rod drive housing support shall be in place.

APPLICABILITY: OPERATIONAL CONDITIONS 1, 2 and 3.

#### ACTION:

With the control rod drive housing support not in place, be in at least HOT SHUTDOWN within 12 hours and in COLD SHUTDOWN within the following 24 hours.

#### SURVEILLANCE REQUIREMENTS

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4.1.3.8 The control rod drive housing support shall be verified to be in place by a visual inspection prior to startup any time it has been disassembled or when maintenance has been performed in the control rod drive housing support area.

## REACTIVITY CONTROL SYSTEMS

### 3/4.1.4 CONTROL ROD PROGRAM CONTROLS

#### ROD WORTH MINIMIZER

#### LIMITING CONDITION FOR OPERATION

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3.1.4.1 The rod worth minimizer (RWM) shall be OPERABLE.

APPLICABILITY: OPERATIONAL CONDITIONS 1 and 2\*, \*\*, when THERMAL POWER is less than or equal to 10% of RATED THERMAL POWER.

#### ACTION:

- a. With the RWM inoperable after the first 12 control rods are fully withdrawn, operation may continue provided that control rod movement and compliance with the prescribed control rod pattern are verified by a second licensed operator or technically qualified member of the unit technical staff.
- b. With the RWM inoperable before the first 12 control rods are fully withdrawn, one startup per calendar year may be performed provided that control rod movement and compliance with the prescribed control rod pattern are verified by a second licensed operator or technically qualified member of the unit technical staff.
- c. Otherwise, with the RWM inoperable, control rod movement shall not be permitted except by full scram.\*\*\*

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\*See Special Test Exception 3.10.2.

\*\*Entry into OPERATIONAL CONDITION 2 and withdrawal of selected control rods is permitted for the purpose of determining the OPERABILITY of the RWM prior to withdrawal of control rods for the purpose of bringing the reactor to criticality.

\*\*\*Control rods may be moved, under administrative control, to permit testing associated with demonstrating OPERABILITY of the RWM.

## REACTIVITY CONTROL SYSTEMS

### SURVEILLANCE REQUIREMENTS

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- 4.1.4.1 The RWM shall be demonstrated OPERABLE:
- a. In OPERATIONAL CONDITION 2 within 8 hours prior to withdrawal of control rods for the purpose of making the reactor critical, and in OPERATIONAL CONDITION 1 within 1 hour after RWM automatic initiation when reducing THERMAL POWER, by verifying proper indication of the selection error of at least one out-of-sequence control rod.
  - b. In OPERATIONAL CONDITION 2 within 8 hours prior to withdrawal of control rods for the purpose of making the reactor critical, by verifying the rod block function by demonstrating inability to withdraw an out-of-sequence control rod.
  - c. In OPERATIONAL CONDITION 1 within 1 hour after RWM automatic initiation when reducing THERMAL POWER, by verifying the rod block function by demonstrating inability to withdraw an out-of-sequence control rod.
  - d. By verifying that the control rod patterns and sequence input to the RWM computer are correctly loaded following any loading of the program into the computer.
- 3.1.4.2 DELETED
- 4.1.4.2 DELETED

## REACTIVITY CONTROL SYSTEMS

### ROD BLOCK MONITOR

#### LIMITING CONDITION FOR OPERATION

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3.1.4.3 Both rod block monitor (RBM) channels shall be OPERABLE.

APPLICABILITY: OPERATIONAL CONDITION 1, when THERMAL POWER is greater than or equal to 30% of RATED THERMAL POWER.

#### ACTION:

- a. With one RBM channel inoperable:
  1. Verify that the reactor is not operating on a LIMITING CONTROL ROD PATTERN, and
  2. Restore the inoperable RBM channel to OPERABLE status within 24 hours.

Otherwise, place the inoperable rod block monitor channel in the tripped condition within the next hour.

- b. With both RBM channels inoperable, place at least one inoperable rod block monitor channel in the tripped condition within 1 hour.

#### SURVEILLANCE REQUIREMENTS

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4.1.4.3 Each of the above required RBM channels shall be demonstrated OPERABLE by performance of a:

- a. CHANNEL FUNCTIONAL TEST and CHANNEL CALIBRATION at the frequencies and for the OPERATIONAL CONDITIONS specified in Table 4.3.6-1.
- b. CHANNEL FUNCTIONAL TEST prior to control rod withdrawal when the reactor is operating on a LIMITING CONTROL ROD PATTERN.

### 3/4.10 SPECIAL TEST EXCEPTIONS

#### 3/4.10.1 PRIMARY CONTAINMENT INTEGRITY

##### LIMITING CONDITION FOR OPERATION

---

3.10.1 The provisions of Specifications 3.6.1.1, 3.6.1.3, and 3.9.1 and Table 1.2 may be suspended to permit the reactor pressure vessel closure head and the drywell head to be removed and the primary containment air lock doors to be open when the reactor mode switch is in the Startup position during low power PHYSICS TESTS with THERMAL POWER less than 1% of RATED THERMAL POWER and reactor coolant temperature less than 200°F.

APPLICABILITY: OPERATIONAL CONDITION 2, during low power PHYSICS TESTS.

##### ACTION:

With THERMAL POWER greater than or equal to 1% of RATED THERMAL POWER or with the reactor coolant temperature greater than or equal to 200°F, immediately place the reactor mode switch in the Shutdown position.

##### SURVEILLANCE REQUIREMENTS

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4.10.1 The THERMAL POWER and reactor coolant temperature shall be verified to be within the limits at least once per hour during low power PHYSICS TESTS.

## SPECIAL TEST EXCEPTIONS

### 3/4.10.2 ROD WORTH MINIMIZER

#### LIMITING CONDITION FOR OPERATION

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3.10.2 The sequence constraints imposed on control rod groups by the rod worth minimizer (RWM) per Specification 3.1.4.1 may be suspended for the following tests provided that control rod movement prescribed for this testing is verified by a second licensed operator or other technically qualified member of the unit technical staff present at the reactor console:

- a. Shutdown margin demonstration, Specification 4.1.1.
- b. Control rod scram, Specification 4.1.3.2.
- c. Control rod friction measurements.
- d. Startup Test Program

APPLICABILITY: OPERATIONAL CONDITIONS 1 and 2 when THERMAL POWER is less than or equal to 10% of RATED THERMAL POWER.

#### ACTION:

With the requirements of the above specifications not satisfied, verify that the RWM is OPERABLE per Specification 3.1.4.1.

#### SURVEILLANCE REQUIREMENTS

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- 4.10.2 When the sequence constraints imposed by the RWM are bypassed, verify;
- a. That movement of control rods is blocked or limited to the approved control rod withdrawal sequence during scram and friction tests.
  - b. That movement of control rods during shutdown margin demonstrations is limited to the prescribed sequence per Specification 3.10.3.
  - c. Conformance with this specification and test procedures by a second licensed operator or other technically qualified member of the unit technical staff.

## REACTIVITY CONTROL SYSTEMS

### BASES

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#### CONTROL RODS (Continued)

Control rod coupling integrity is required to ensure compliance with the analysis of the rod drop accident in the FSAR. The overtravel position feature provides the only positive means of determining that a rod is properly coupled and therefore this check must be performed prior to achieving criticality after completing CORE ALTERATIONS that could have affected the control rod coupling integrity. The subsequent check is performed as a backup to the initial demonstration.

In order to ensure that the control rod patterns can be followed and therefore that other parameters are within their limits, the control rod position indication system must be OPERABLE.

The control rod housing support restricts the outward movement of a control rod to less than 3 inches in the event of a housing failure. The amount of rod reactivity which could be added by this small amount of rod withdrawal is less than a normal withdrawal increment and will not contribute to any damage to the primary coolant system. The support is not required when there is no pressure to act as a driving force to rapidly eject a drive housing.

The required surveillance intervals are adequate to determine that the rods are OPERABLE and not so frequent as to cause excessive wear on the system components.

#### 3/4.1.4 CONTROL ROD PROGRAM CONTROLS

Control rod withdrawal and insertion sequences are established to assure that the maximum insequence individual control rod or control rod segments which are withdrawn at any time during the fuel cycle could not be worth enough to result in a peak fuel enthalpy greater than 280 cal/gm in the event of a control rod drop accident. The specified sequences are characterized by homogeneous, scattered patterns of control rod withdrawal. When THERMAL POWER is greater than 10% of RATED THERMAL POWER, there is no possible rod worth which, if dropped at the design rate of the velocity limiter, could result in a peak enthalpy of 280 cal/gm. Thus requiring the RWM to be OPERABLE when THERMAL POWER is less than or equal to 10% of RATED THERMAL POWER provides adequate control.

The RWM provides automatic supervision to assure that out-of-sequence rods will not be withdrawn or inserted.

The analysis of the rod drop accident is presented in Section 15.4.9 of the FSAR and the techniques of the analysis are presented in a topical report, Reference 1, and two supplements, References 2 and 3. Additional pertinent analysis is also contained in Amendment 17 to the Reference 4 topical report.

The RBM is designed to automatically prevent fuel damage in the event of erroneous rod withdrawal from locations of high power density during high power operation. Two channels are provided. Tripping one of the channels will block erroneous rod withdrawal to prevent fuel damage. This system backs up the written sequence used by the operator for withdrawal of control rods.

## REACTIVITY CONTROL SYSTEMS

### BASES

#### 3/4.1.5 STANDBY LIQUID CONTROL SYSTEM

The standby liquid control system provides a backup capability for bringing the reactor from full power to a cold, Xenon-free shutdown, assuming that the withdrawn control rods remain fixed in the rated power pattern. To meet this objective it is necessary to inject a quantity of boron which produces a concentration of 660 ppm in the reactor core and other piping systems connected to the reactor vessel. To allow for potential leakage and improper mixing, this concentration is increased by 25%. The required concentration is achieved by having available a minimum quantity of 4,620 gallons of sodium pentaborate solution containing a minimum of 5,500 lbs of sodium pentaborate. This quantity of solution is a net amount which is above the pump suction shutoff level setpoint thus allowing for the portion which cannot be injected. The pumping rate of 41.2 gpm provides a negative reactivity insertion rate over the permissible solution volume range, which adequately compensates for the positive reactivity effects due to elimination of steam voids, increased water density from hot to cold, reduced doppler effect in uranium, reduced neutron leakage from boiling to cold, decreased control rod worth as the moderator cools, and xenon decay. The temperature requirement ensures that the sodium pentaborate always remains in solution.

With redundant pumps and explosive injection valves and with a highly reliable control rod scram system, operation of the reactor is permitted to continue for short periods of time with the system inoperable or for longer periods of time with one of the redundant components inoperable.

The SLCS system consists of three separate and independent 100% capacity pumps and explosive valves. Only two of the separate and independent pumps and explosive valves are required to meet the minimum requirements of this technical specification and satisfy the single failure criterion.

Surveillance requirements are established on a frequency that assures a high reliability of the system. Once the solution is established, boron concentration will not vary unless more boron or water is added, thus a check on the temperature and volume once each 24 hours assures that the solution is available for use.

Replacement of the explosive charges in the valves at regular intervals will assure that these valves will not fail because of deterioration of the charges.

1. C. J. Paone, R. C. Stirn and J. A. Woolley, "Rod Drop Accident Analysis for Large BWR's," G. E. Topical Report NEDO-10527, March 1972.
2. C. J. Paone, R. C. Stirn, and R. M. Young, Supplement 1 to NEDO-10527, July 1972.
3. J. M. Haun, C. J. Paone, and R. C. Stirn, Addendum 2, "Exposed Cores," Supplement 2 to NEDO-10527, January 1973.
4. Amendment 17 to General Electric Licensing Topical Report NEDE-24011-P-A, "General Electric Standard Application for Reactor Fuel".

## 3/4.10 SPECIAL TEST EXCEPTIONS

### BASES

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#### 3/4.10.1 PRIMARY CONTAINMENT INTEGRITY

The requirement for PRIMARY CONTAINMENT INTEGRITY is not applicable during the period when open vessel tests are being performed during the low power PHYSICS TESTS.

#### 3/4.10.2 ROD WORTH MINIMIZER

In order to perform the tests required in the technical specifications it is necessary to bypass the sequence restraints on control rod movement. The additional surveillance requirements ensure that the specifications on heat generation rates and shutdown margin requirements are not exceeded during the period when these tests are being performed and that individual rod worths do not exceed the values assumed in the safety analysis.

#### 3/4.10.3 SHUTDOWN MARGIN DEMONSTRATIONS

Performance of shutdown margin demonstrations with the vessel head removed requires additional restrictions in order to ensure that criticality does not occur. These additional restrictions are specified in this LCO.

#### 3/4.10.4 RECIRCULATION LOOPS

This special test exception permits reactor criticality under no flow conditions and is required to perform certain startup and PHYSICS TESTS while at low THERMAL POWER levels.

#### 3/4.10.5 OXYGEN CONCENTRATION

Relief from the oxygen concentration specifications is necessary in order to provide access to the primary containment during the initial startup and testing phase of operation. Without this access the startup and test program could be restricted and delayed.

#### 3/4.10.6 TRAINING STARTUPS

This special test exception permits training startups to be performed with the reactor vessel depressurized at low THERMAL POWER and temperature while controlling RCS temperature with one RHR subsystem aligned in the shutdown cooling mode in order to minimize contaminated water discharge to the radioactive waste disposal system.



UNITED STATES  
NUCLEAR REGULATORY COMMISSION  
WASHINGTON, D. C. 20555

SAFETY EVALUATION BY THE OFFICE OF NUCLEAR REACTOR REGULATION  
SUPPORTING AMENDMENT NO. 17 TO FACILITY OPERATING LICENSE NO. NPF-39  
PHILADELPHIA ELECTRIC COMPANY  
LIMERICK GENERATING STATION, UNIT 1  
DOCKET NO. 50-352

1.0 INTRODUCTION

By letter dated December 14, 1988, Philadelphia Electric Company (the licensee) requested an amendment to Facility Operating License No. NPF-39 for the Limerick Generating Station, Unit 1. The proposed amendment would change the Technical Specifications (TSs) to permit removal of the Rod Sequence Control System (RSCS) and to reduce the Rod Worth Minimizer (RWM) low power setpoint.

2.0 DISCUSSION

The Rod Sequence Control System restricts rod movement to minimize the individual worth of control rods to lessen the consequences of a Rod Drop Accident (RDA). Control rod movement is restricted through the use of rod select, insert, and withdrawal blocks. The Rod Sequence Control System is a hardwired (as opposed to a computer controlled), redundant backup to the Rod Worth Minimizer. It is independent of the Rod Worth Minimizer in terms of inputs and outputs but the two systems are compatible. The RSCS is designed to monitor and block when necessary operator control rod selection, withdrawal and insertion actions, and thus assist in preventing significant control rod pattern errors which could lead to a control rod with a high reactivity worth (if dropped). A significant pattern error is one of several abnormal events all of which must occur to have a RDA which might exceed fuel energy density limit criteria for the event. It was designed only for possible mitigation of the RDA and is active only during low power operation (currently generally less than 20 percent power) when a RDA might be significant. It provides rod blocks on detection of a significant pattern error. It does not prevent a RDA. A similar pattern control function is also performed by the RWM, a computer controlled system. All reactors having a RSCS also have a RWM.

In response to a topical report submitted by the BWR Owner's Group, on December 27, 1987 the NRC staff issued a letter with a supporting safety evaluation approving 1) elimination of the RSCS while retaining the RWM to provide backup to the operator for control rod pattern control and 2) lowering the setpoint for turnoff of RWM to 10% of rated thermal power from its current 20% level. (Letter, A. C. Thadani, NRC to J. S.

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Charnley, GE, Subject: Acceptance for Referencing of Licensing Topical Report NEDE-24011-P-A, "General Electric Standard Application for Reactor Fuel," Revision 8, Amendment 17).

### 3.0 EVALUATION

The letter of December 27, 1987 and supporting safety evaluation approving the topical report concluded that the modifications proposed by PECO were acceptable provided:

- 1) The Technical Specifications (TS) should require provisions for minimizing operations without the RWM system operable.
- 2) The occasional necessary use of a second operator replacement should be strengthened by a utility review of relevant procedures, related forms and quality control to assure that the second operator provides an effective and truly independent monitoring process. A discussion of this review should accompany the request for RSCS removal.
- 3) Rod patterns used should be at least equivalent to Banked Position Withdrawal Sequence (BPWS) patterns.

With respect to item 1) above, the proposed TSs submitted with this amendment application allow only one reactor startup per calendar year with the RWM unavailable prior to or during the withdrawal of the first 12 control rods. We conclude that item 1) is adequately satisfied.

With regard to item 2) above, PECO described the programs and procedures that would be provided during instances when the RWM is not available to independently verify the correctness of the first operator's actions during rod movements. The procedure for "Bypassing the Rod Worth Minimizer," procedure S73.O.D, Rev. 7 dated October 31, 1988 has been reviewed by the resident inspectors and the NRR Project Manager and it provides acceptable controls when used in conjunction with the specific procedural restrictions listed in the December 14, 1988 submittal. During the January 11, 1989 shutdown of Unit 1 for the second refueling outage, the resident inspectors observed management's attention to the procedures. We conclude that the procedural controls are acceptable.

The RWM at Limerick Unit 1 utilizes the BPWS patterns recommended in the staff's December 27, 1987 letter. This satisfies item 3) above.

PECO's proposal to remove the RSCS and to lower the RWM low power setpoint from 20 to 10 percent at Limerick Unit 1 meets the requirements detailed in the staff's letter of December 27, 1987 approving the topical report on these modifications. Accordingly, the modifications proposed in PECO's letter of November 9, 1988 are found to be acceptable and are approved. We have also reviewed the proposed changes to the TSs and find

them to be consistent with the intent of the staff's safety evaluation approving the topical report and find the changes acceptable.

#### 4.0 ENVIRONMENTAL CONSIDERATION

This amendment involves a change to a requirement with respect to the installation or use of a facility component located within the restricted area as defined in 10 CFR Part 20 and changes to the surveillance requirements. The staff has determined that the amendment involves no significant increase in the amounts, and no significant change in the types, of any effluents that may be released offsite and that there is no significant increase in individual or cumulative occupational radiation exposure. The Commission has previously issued a proposed finding that this amendment involves no significant hazards consideration and there has been no public comment on such finding. Accordingly, this amendment meets the eligibility criteria for categorical exclusion set forth in 10 CFR 51.22(c)(9). Pursuant to 10 CFR 51.22(b), no environmental impact statement nor environmental assessment need be prepared in connection with the issuance of this amendment.

#### 5.0 CONCLUSION

The Commission made a proposed determination that the amendment involves no significant hazards consideration which was published in the Federal Register (54 FR 5172) on February 1, 1989 and consulted with the State of Pennsylvania. No public comments were received and the State of Pennsylvania did not have any comments.

The staff has concluded, based on the considerations discussed above, that: (1) there is reasonable assurance that the health and safety of the public will not be endangered by operation in the proposed manner, and (2) such activities will be conducted in compliance with the Commission's regulations and the issuance of this amendment will not be inimical to the common defense and the security nor to the health and safety of the public.

Principal Contributor: Dick Clark

Dated: March 22, 1989