VIRGINIA ELECTRIC AND POWER COMPANY Richmond, Virginia 23261

May 16, 2001

United States Nuclear Regulatory Commission Attention: Document Control Desk Washington, D.C. 20555 Serial No. 01-198 NL&OS/GDM Docket No. 50-280 50-281 License No. DPR-32 DPR-37

Gentlemen:

VIRGINIA ELECTRIC AND POWER COMPANY SURRY POWER STATION UNITS 1 AND 2 ASME SECTION XI INSERVICE INSPECTION PROGRAM RELIEF REQUESTS SR-023 AND SR-029

Surry Power Station Units 1 and 2 are presently in their third ten-year inservice inspection interval, and examinations are conducted in accordance with the requirements of the 1989 Edition of the ASME Section XI Code. Pursuant to ASME Section XI requirements, the welds on the regenerative heat exchanger in the Chemical and Volume Control System require examination. These examinations have been determined to be a hardship without a compensating increase in safety based on: 1) the geometry of the welds which preclude full coverage (Unit 2 only), and 2) the excessive personnel dose required to perform these examinations.

As further detailed in the attached relief requests, significant dose would be received by personnel completing the inspections of the regenerative heat exchangers for each unit. Furthermore, geometric restrictions associated with the Unit 2 regenerative heat exchanger would severely limit the amount of meaningful information that could be obtained by examination concerning its condition. Therefore, relief requests SR-023 and SR-029 for Surry Units 1 and 2, respectively, are proposed to eliminate the Code-required examinations on the regenerative heat exchangers.

Relief request SR-010, which also addressed certain relief from Code-required examinations of the Surry Unit 2 regenerative heat exchanger, was previously approved by the NRC staff in a letter dated August 30, 1995. The proposed Unit 2 relief request SR-029 will, if approved, supercede the currently approved SR-010 and its associated conditions.

Therefore, pursuant to 10 CFR 50.55a(a)(3)(ii), relief is requested from certain ASME Section XI Code examination requirements associated with the regenerative heat exchangers. Relief requests SR-023 and SR-029 are provided in Attachments 1 and 2 for Surry Units 1 and 2, respectively. Similar ASME Code relief was requested by the

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Joseph M. Farley Nuclear Plant and approved by the NRC in a letter dated November 16, 1998 (TAC NO. MA3449). North Anna Power Station Unit 2 also requested elimination of the Code required examinations for the regenerative heat exchanger in relief request NDE-046 and was approved by the NRC in a letter dated March 26, 2001 (TAC NO. MB0750).

The attached relief requests for Surry Units 1 and 2 have been approved by the Station Nuclear Safety and Operating Committee. If you have questions or require additional information, please contact us.

Very truly yours,

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Mark

Leslie Hartz Vice President - Nuclear Engineering and Services

Attachments

Commitments made in this letter: None

cc: U. S. Nuclear Regulatory Commission Region II Sam Nunn Atlanta Federal Center Suite 23T85 61 Forsyth St., S.W. Atlanta, Georgia 30303-8931

> Mr. R. A. Musser NRC Senior Resident Inspector Surry Power Station

Mr. R. Smith Authorized Nuclear Inspector Surry Power Station Attachment 1

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Relief Request SR-023 Regenerative Heat Exchanger (1-CH-E-3)

> Dominion Surry Power Station Unit 1

RELIEF REQUEST SR-023 SURRY POWER STATION UNIT 1

I. IDENTIFICATION OF COMPONENTS

System: Chemical and Volume Control (CH) Component: Regenerative Heat Exchanger (1-CH-E-3) Drawing: 11448-WMKS-CH-E-3

Velds/Hangers Description		Code Item#	<u>Class</u>	
1-01	circumferential head weld	C1.20	2	
1-04	circumferential head weld	C1.20	2	
1-06	circumferential head weld	C1.20	2	
1-07	circumferential head weld	C1.20	2	
1-09	circumferential head weld	C1.20	2	
1-10	circumferential head weld	C1.20	2	
1-02	tubesheet to shell weld	C1.30	2	
1-03	tubesheet to shell weld	C1.30	2	
1-05	tubesheet to shell weld	C1.30	2	
1-08	tubesheet to shell weld	C1.30	2	
1-11	tubesheet to shell weld	C1.30	2	
1-CH-H001	support	F1.40	2	
1-CH-H002	support	F1.40	2	
1-CH-H003	support	F1.40	2	
1-CH-H004	support	F1.40	2	
1-CH-H005	support	F1.40	2	
1-CH-H006	support	F1.40	2	

II. IMPRACTICAL CODE REQUIREMENTS

Examination Categories C-A and F-A require that volumetric or visual examinations be performed as indicated by the Code item numbers above.

III. BASIS FOR RELIEF

Background

The regenerative heat exchanger (1-CH-E-3) provides preheat for the normal charging water flowing into the reactor coolant system (RCS). The preheat is derived from normal letdown water coming from the RCS. Charging and letdown constitute the normal chemical and volume control within the RCS. The heat exchanger itself is actually three heat exchangers or sub-vessels in series

interconnected with piping. Therefore, examinations are limited to one of the heat exchangers as allowed by the Code for multiple vessels of similar design and function. (Table IWC-2500-1, Category C-A, Note (3), Reference: Figure SR-023-1.) The lower heat exchanger has historically been chosen for examination to preclude the need for scaffolding and thus minimize personnel dose.

The heat exchanger has an outside shell diameter of 9.25 inches. The shells were manufactured with ASTM A213 TP 304 stainless steel type material. The heat exchanger is ASME Class 2. The nozzles are 3 inch schedule 160 of similar material and are exempt from examination by IWC-1222(a) for components 4" nominal pipe size (NPS) and smaller.

The purpose of this relief request is to eliminate the examinations on the entire regenerative heat exchanger.

Dose Considerations

A dose evaluation has been conducted on each activity associated with the examinations of the lower regenerative heat exchanger vessel. The lower vessel was chosen to minimize dose in that scaffolding is not required. Table SR-023-1 gives the personnel dose expected from these activities. A personnel dose of 3.822 man-rem is estimated to complete the required examinations over the interval. This estimate assumes optimum inspection and preparation times; however, if difficulties are encountered a corresponding increase in dose would be expected. Shielding is not considered practical since the source of radiation is the component receiving the examinations. Again, the estimate is made under ideal work conditions and should be considered conservatively low.

Significant Leakage Considerations

As previously noted, the inlet and outlet piping for this Class 2 Regenerative Heat Exchanger is 3" NPS. Therefore, a crack or defect in the heat exchanger shell could not produce a leak greater than that allowed by the corresponding 3" inlet or outlet piping. To produce a leak greater than that produced by a 4" line would require multiple shell and/or tube failures in the group of three heat exchangers, which is not considered a credible inservice failure. Therefore, the intent of the ASME Section XI Code 4" exemption is maintained.

Conclusion

The exposure expended to perform the discussed examinations would result in a hardship without a compensating increase in the level of quality and safety. We believe the intent of the ASME Section XI Code would remain in effect in the Surry ISI program considering the NPS 4" and less exemption for Class 2

vessels, piping, pumps and valves. Considering the alternative requirements discussed in Section IV, relief from the Code required examinations on the regenerative heat exchanger is requested per the provisions of 10CFR 50.55a(a)(3)(ii).

Furthermore, similar relief requests for the elimination of the Code required examinations for regenerative heat exchangers were previously submitted for the Joseph M. Farley Nuclear Plant and North Anna Power Station Unit 2. Both the Farley and North Anna Unit 2 relief requests were approved by the NRC in letters dated November 16, 1998 (TAC NO. MA3449) and March 26, 2001 (TAC NO. MB0750), respectively.

IV. ALTERNATE REQUIREMENTS

The containment atmosphere particulate radioactivity is monitored periodically per Technical Specifications requirements. As a result, new leakage is rapidly identified and located during operation. Leakage identified from these components can be easily isolated by upstream valves that can be operated from the control room. The valves also receive an automatic control signal to close on inventory loss based on pressurizer level.

Furthermore, the heat exchanger will continue to receive a periodic pressure test in accordance with IWC 2500, category C-H, and IWC 5000.

SURRY UNIT 1 REGENERATIVE HEAT EXCHANGER (1-CH-E-3) FIGURE SR-023-1



SURRY UNIT 1 REGENERATIVE HEAT EXCHANGER (1-CH-E-3) MAN-REM ESTIMATE FOR THE LOWER HEAT EXCHANGER TABLE SR-023-1

Work Task	Job Site Man-Hrs	Dose Rates Rem/Hr	Estimated Man- Rem
Remove/install insulation	1.8	0.800	1.440
Remove/install shielding	0.25	0.800	0.200
Remove/install clamp	2.0	0.500	1.000
Weld prep	0.14	0.500	0.070
HP coverage	1.5	0.015	0.022
Circumferential head welds 1-04, 1-10	0.50	0.500	0.250
Tube sheet to shell Welds 1-11, 1-12	0.18	0.500	0.090
Hangers H-001, H002, H003, H004, H005, H-006	1.5	0.500	0.750

Total – 3.822 Man-Rem

Attachment 2

Relief Request SR-029 Regenerative Heat Exchanger (2-CH-E-3)

> Dominion Surry Power Station Unit 2

RELIEF REQUEST SR-029 SURRY POWER STATION UNIT 2

I. IDENTIFICATION OF COMPONENTS

System:Chemical and Volume Control (CH)Component:Regenerative Heat Exchanger (2-CH-E-3)Drawing:11548-WMKS-CH-E-3

Welds/Hangers	Description	Code Item#	Class
1-04	circumferential head weld	B2.51	1
1-17	circumferential head weld	B2.51	1
1-19	circumferential head weld	B2.51	1
1-03	tubesheet to shell weld	B2.80	1
1-18	tubesheet to shell weld	B2.80	1
1-22	tubesheet to shell weld	B2.80	1
1-06	nozzle to vessel weld	B3.150	1
1-08	nozzle to vessel weld	B3.150	1
1-09	nozzle to vessel weld	B3.150	1
1-11	nozzle to vessel weld	B3.150	1
1-13	nozzle to vessel weld	B3.150	1
1-15	nozzle to vessel weld	B3.150	1
NIR-06	nozzle inside radius	B3.160	1
NIR-08	nozzle inside radius	B3.160	1
NIR-09	nozzle inside radius	B3.160	1
NIR-11	nozzle inside radius	B3.160	1
NIR-13	nozzle inside radius	B3.160	1
NIR-15	nozzle inside radius	B3.160	1
2-55	terminal end	B9.21	1
2-56	terminal end	B9.21	1
2-57	terminal end	B9.21	1
2-58	terminal end	B9.21	1
1-01	circumferential head weld	C1.20	2
1-21	circumferential head weld	C1.20	2
1-24	circumferential head weld	C1.20	2
1-02	tubesheet to shell weld	C1.30	2
1-20	tubesheet to shell weld	C1.30	2
1-23	tubesheet to shell weld	C1.30	2
2-CH-H001	support	F1.40	1
2-CH-H002	support	F1.40	1
2-CH-H003	support	F1.40	1
2-CH-H004	support	F1.40	2
2-CH-H005	support	F1.40	2
2-CH-H006	support	F1.40	2

II. IMPRACTICAL CODE REQUIREMENTS

Examination Categories B-B, B-D, B-J, C-A and F-A require that volumetric, surface or visual examinations be performed as indicated by the Code item numbers above.

III. BASIS FOR RELIEF

Background

The regenerative heat exchanger (2-CH-E-3) provides preheat for the normal charging water flowing into the reactor coolant system (RCS). The preheat is derived from normal letdown water coming from the RCS. Charging and letdown constitute the normal chemical and volume control within the RCS. The heat exchanger itself is actually three heat exchangers or sub-vessels in series interconnected with piping. Therefore, examinations are limited to one of the heat exchangers as allowed by the Code for multiple vessels of similar design and function. (Table IWB-2500-1, Category B-B, Note (1) and Table IWC-2500-1, Category C-A, Note (3), Reference: Figure SR-029-1.) The lower heat exchanger has historically been chosen for examination to preclude the need for scaffolding and thus minimize personnel dose.

The heat exchanger has an outside shell diameter of 9.25 inches. The shells were manufactured with ASTM A213 TP 304 stainless steel type material. The nozzles are 3 inch schedule 160 of similar material. The charging or tube side of the heat exchanger is classified ASME Class 1. The classification of the letdown (shell) side of the heat exchanger is ASME Class 2. All Class 1 nozzles are required to be examined, and the examinations are not limited to one heat exchanger.

The purpose of this relief request is to eliminate the examinations on the entire regenerative heat exchanger including terminal ends.

Geometric Restrictions

The nozzle-to-vessel welds and nozzle inside radius sections for this vessel were not designed for ultrasonic examination from the outside diameter of the vessel. The small diameter of the vessel and nozzles prevents a meaningful ultrasonic examination of these components. The joint design of the nozzle weld specifies a 3" schedule 160 weldolet joined to a 9.25" O.D. x 0.875" thick vessel. The configuration of the weldolet precludes axial ultrasonic examination from the nozzle side and circumferential examination in either direction. This limits volumetric examination to a single axial scan from the vessel side of the nozzle. It is our opinion that a meaningful ultrasonic examination cannot be performed on the weld or inner radius with a single axial scan, due to the small diameter of the vessel and weldolet. Further, the change in dihedral around the joint results in a corresponding change in the ultrasonic beam angle, which makes position measurements unreliable. It would also be necessary to extend the beam path to at least two full Vee paths, which would further complicate this examination. These limitations would substantially diminish our ability to discriminate flaw indications from the geometry existing around the joint. The configuration also precludes placement of film on the outside diameter for radiography, and the inside surfaces are inaccessible.

Dose Considerations

A dose evaluation has been conducted on each activity associated with the examinations for the entire regenerative heat exchanger. Table SR-029-1 provides the personnel dose expected from these activities. A personnel dose of 12.268 man-rem is estimated to complete these examinations over the interval. This estimate utilizes dose savings by limiting the circumferential head and tubesheet to shell welds to the lower heat exchanger as allowed by the code. Optimum inspection and preparation times were assumed. However, if difficulties are encountered, a corresponding increase in dose would be expected. Shielding is not considered practical since the source of radiation is the component receiving the examinations.

Conclusion

If the Code required examinations were performed, the geometric restrictions would severely limit the amount of meaningful information that could be obtained concerning the condition of the heat exchanger. Therefore, the significant personnel dose involved with performing the examinations would result in a hardship without a compensating increase in the level of quality and safety. Considering the alternative requirements discussed in Section IV, relief from the Code required examinations on the regenerative heat exchanger is requested pursuant to the provisions of 10CFR 50.55a(a)(3)(ii).

Furthermore, similar relief requests for the elimination of the Code required examinations for regenerative heat exchangers were previously submitted for the Joseph M. Farley Nuclear Plant and North Anna Power Station Unit 2. Both the Farley and North Anna Unit 2 relief requests were approved by the NRC in letters dated November 16, 1998 (TAC NO. MA3449) and March 26, 2001 (TAC NO. MB0750), respectively.

IV. ALTERNATE REQUIREMENTS

Technical Specifications require that the RCS leak rate be limited to 1 gallon per minute unidentified leakage. This value is calculated periodically in accordance

with Technical Specification requirements. Additionally, the containment atmosphere particulate radioactivity is monitored periodically per Technical Specification requirements. As a result, new leakage is rapidly identified and located during operation. Leakage identified from these components can be easily isolated by upstream valves with manual operation from within the control room. The valves also receive an automatic control signal to close on inventory loss based on pressurizer level.

Furthermore, the Class 1 side of the regenerative heat exchanger receives a system leakage test prior to start up after each refueling outage. During this system leakage test the components receive a visual (VT-2) examination. The Class 2 side of the heat exchanger will continue to receive a periodic pressure test in accordance with IWC 2500, category C-H and IWC 5000.

SURRY UNIT 2 REGENERATIVE HEAT EXCHANGER (2-CH-E-3) FIGURE SR-029-1



SURRY UNIT 2 REGENERATIVE HEAT EXCHANGER (2-CH-E-3) MAN-REM ESTIMATE FOR THE ENTIRE HEAT EXCHANGER TABLE SR-029-1

	Job Site	Dose	Estimated	Est. Man-
Work Task	Man-	Rates	Man-Rem	Rem/Interval
	hours	Rem/Hr		20/28 welds
				required
Insulation removal/installation	5.3	0.800	4.240	4.240
Install/remove shielding	0.25	0.800	0.200	0.200
Install/remove scaffolding	2	0.800	1.600	1.600
Remove/Install clamp	2	0.500	1.000	1.000
Weld prep	1.25	0.500	0.625	0.446
HP coverage	6.25	0.015	0.094	0.067
Nozzle-to-vessel welds 1-06,1- 08,1-09,1-11,1-13,1-15	3	0.800	2.400	2.400
Nozzle-to-inside radius NIR-06, NIR-08, NIR-09, NIR-11, NIR-13, NIR-15	2.25	0.800	1.800	1.800
Circumferential head welds, Class 1: 1-04, 1-17, 1-19 Class 2: 1-01, 1-21, 1-24	0.75	0.500	0.375	0.125
Tube sheet to shell welds, Class 1: 1-03, 1-18, 1-22 Class 2: 1-02, 1-20, 1-23	0.54	0.500	0.270	0.090
Terminal end welds 2-55, 2-56, 2-57, 2-58	0.750	0.400	0.300	0.000
Hangers (VT-3) H-001, H-002, H-003, H-004, H-005, H-006	0.750	0.400	0.300	0.300

Total – 12.268 Man-Rem/Interval