Analysis File:	Preliminary Risk Analysis of Spent Fuel Pool Accidents at Decommissioning Plants
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#### **Objective of Analysis:**

To perform a generic study of spent fuel pool risks at decommissioned plants to:

- examine the full scope of potentially risk-significant issues
- determine which accident sequences are credible
- document the preliminary assessment for public review
- elicit feedback from all stakeholders regarding analysis assumptions and design/operational features, and
- conduct a complete and open discussion of the risk assessment

This analysis will be revised based on stakeholder feedback so that a consistent and predictable basis for future plant-specific decisions can be developed, based on the best available PRA assessment methodology, and actual design/ operational characteristics of the plant

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# **Risk Analysis of Spent Fuel Pool Accidents at Decommissioning Plants**

The staff's preliminary deterministic evaluations of spent fuel pool (SFP) accidents found that zirconium cladding fires could not be ruled out for spent fuel that had been transferred from reactors up to five years previously, based on a simplified, conservative analysis. To assess the risk in the time from shutdown to one year, the staff performed a simplified preliminary PRA, which modeled internal and external initiating events to assess the potential risk associated with SFPs at decommissioned nuclear power plants.

The PRA model is based on the sled-mounted systems that are used at many current decommissioned plants. Information about existing decommissioned plants was gathered by decommissioning project managers and during recent visits to four sites covering all four major nuclear steam supply system vendors (General Electric, Westinghouse, Babcock & Wilcox, and Combustion Engineering). In addition, the staff used several previously published deterministic and probabilistic evaluations of potential risks at both operating and decommissioned plants to help in this study. In the modeling of SFP configurations, this PRA considered three cases:

Case 1 assumes that the SFP and its support systems (including instrumentation and power sources) are similar to that found during staff visits to four decommissioned plants. Figure 1 is a simplified drawing of this system. In Case 1, transfer of the last fuel from the reactor to the SFP is assumed to have occurred one year previously.

Case 2 is the same as Case 1 except that the transfer of the last fuel is assumed to have occurred one month previously. This is a bounding case since it is not expected that a utility would disable all the support systems normally used to provide SFP cooling within one month of the last fuel transfer. In fact, it may not be possible for the sled mounted systems currently available to remove the heat load in the pool one month after the last transfer. However, Case 2 provides a bounding value to help determine the impact that higher decay heat loads (and therefore less recovery time) have on the frequency of fuel uncovery.

Case 3 assumes that the SFP and its support systems are configured in a manner that is only slightly better than the minimum allowed by current NRC regulations. The staff believes that no prudent utility would configure its SFP system in this way, however, the assumptions in the "minimal state" are not precluded by current NRC regulations. This case is used to help determine if there may be a need for additional regulation in this area. Case 3 assumes that the last fuel from the reactor was transferred one year previously.

Assumptions made for Cases 1 and 2:

- The SFP has instrumentation/indication/alarms in the control room to alert the operator of potential problems in the SFP. These may include level indications, temperature indications, and/or radiation monitors.
- The certified fuel handlers are former reactor operators who are knowledgeable of the facility, the maintenance procedures, and the surrounding community. It is assumed that these operators (through guidance and / or training) are aware of the available backup

sources that can be used to replenish the SFP inventory (i.e., the fire protection pumps, or offsite sources such as from fire engines).

- The site has two operable fire pumps, one diesel-driven and one electrically driven from offsite power.
- The makeup capability (with respect to volumetric flow) is assumed as follows:

Make-up pump: 20 - 30 gpm Fire pump: 100 - 200 gpm Fire Engine: 100 - 250 gpm (depending on hose size, 2½"(250 gpm) or 1½"(100 gpm)

It is therefore assumed that, for the larger loss of coolant inventory accidents, makeup through the makeup pumps is not feasible unless the source of inventory loss can be isolated.

- The operators perform walk-downs of the SFP area once per shift (8 to 12 hour shifts). A different crew member is assumed for the next shift. It is also assumed that the SFP water is clear and pool level is observable via a measuring stick in the pool that can alert operators to level changes.
- Requirements for fire detection and suppression may be reduced (when compared to those for an operating plant) and it is assumed that automatic detection and suppression capability may not be present.
- Overhead cranes have stops to help prevent heavy loads from being moved over the spent fuel pool.

Assumptions for Case 3:

- The control room has level and/or temperature indicators, however, these are not required to be maintained in an operable state. The radiation monitors and associated alarms in the control room are only required to be operable when fuel is being moved. In the PRA model, the control room instrumentation is assumed unavailable 10% of the time.
- The certified fuel handlers are individuals who meet the minimum training requirements. Plant staffing is assumed to be the minimum required. Recovery probabilities are therefore assumed to be lower for Case 3 than for Cases 1 and 2. It is also assumed that the operators would walk-down the pool area less frequently, and the probability of not noticing abnormal conditions at the pool is it therefore higher than in Cases 1 and 2.
- There is limited makeup capability (with respect to volumetric flow). Since there is no requirement that fire protection equipment to be maintained operable, no credit is taken for the fire pump's ability to provide inventory makeup or fire suppression.

• Overhead cranes have stops to help prevent heavy loads from being moved over the spent fuel pool. Cranes are operated by non-nuclear trained operators.

Assumptions that are applicable to all 3 cases:

- The emergency diesel generators and support systems such as residual heat removal and service water (that could provide SFP cooling or makeup prior to the plant being decommissioned) have been removed from service.
- The SFP cooling system, its support systems, and the electric driven fire protection pump are fed off the same electrical bus.
- Procedures exist to mitigate small leaks from the SFP or for loss of SFP cooling system. However, it is assumed that these procedures are not sufficiently detailed to provide a time-frame as to when actions have to be completed. It is also assumed that there are no automatic actuations and that all pumps or valves have to be manually operated and aligned.
- The only significant technical specification applicable to SFPs is the requirement for radiation monitors to be operable when fuel is being moved. There are no T.S. requirements for the cooling pumps, makeup pumps, fire pumps, or any of the support systems.
- In the estimation of tornado risk, it was assumed that an F4 or F5 tornado would be required if significant damage were to be possible to a PWR or BWR spent fuel pool. If a tornado of this magnitude is present at the plant site, it is assumed that the SFP integrity would be lost, leading to fuel uncovery. An F2 to F5 tornado could result in possible significant damage to the SFP support system. This is modeled as a loss of offsite power event (from severe weather).
- Shipping cask handling is the dominant heavy load operation. Spent fuel casks will be the only heavy loads moved over the spent fuel pool with sufficient mass to significantly damage the pool. It is assumed that crane operators will follow safe load path procedures when moving heavy loads near the spent fuel pool.
- In the estimation of seismic risk, it is assumed that SFPs are robust and will survive seismic events less than three times the safe shutdown earthquake (SSE).
- Generic industry data was used for initiating event frequencies for the loss of offsite power, the loss of pool cooling, and the loss of coolant inventory.
- The effects of criticality were not considered in the risk evaluation. Its potential for impact on risk is considered to be very low.

#### Identification of Initiating Events

To identify potential initiating events that could result in a loss of spent fuel pool cooling (beyond design bases), various references (INEL-96/0334; NUREG-1275, Vol. 12; NUREG-1353; Draft for Comment NUREG "Postulated Accidents for Permanently Shutdown Reactors"; Draft "Risk Analysis for Spent Fuel Pool Cooling at Susquehanna Electric Power Station"; NUREG/CR-6451; NUREG/CR-4982; NUREG/CR-5281; and NUREG/CR-5176) were reviewed. The following were found to potential initiators:

- Loss of offsite power from plant centered and grid related events
- Loss of offsite power from severe weather events
- Internal fire
- Loss of pool cooling
- Loss of coolant inventory
- Seismic event
- Cask drop
- Aircraft impact
- Tornado missile

Event trees were developed for the first six initiators above. For events initiated by a cask drop, aircraft impact or tornado missile, it is assumed that mitigation is not feasible and fuel uncovery will result. Therefore, for these events, the fuel uncovery frequency is equivalent to the initiating event frequency.

#### Data Used

The data used in the quantification of the fuel uncovery frequency for each of the initiating events and for each of the three cases is provided in Appendix A. The rationale behind the data used is also provided in the appendix.

#### Human Reliability Analysis

The time available for operator actions is based on staff calculations on the time it would take for level in the pool to reach a height of approximately 3' above the fuel. At this level, it is assumed that radiation levels in the vicinity of the pool will be such that manual recovery actions will not be possible.

In addition to rapid draining events, the staff considered pool heatup after a loss of pool cooling followed by bulk pool boiling as a possible way to uncover the fuel. It takes a relatively long time to uncover the fuel if inventory is lost in this manner due to the large amount of water in a spent fuel pool, the large specific heat of water, and the large latent heat of vaporization for water. Simple calculations for a typical-sized spent fuel pool and conservative decay heat assumptions yield the results in Table 1. These results are based on the following assumptions:

- no heat losses
- 1 atm pressure
- h<sub>fo</sub> ≈2258 kJ/kg
- base pool heat load for a full pool of 2 MW
- core thermal power of 3293 MW
- typical pool size (based on Tables 2.1 & 2.2 of NUREG/CR-4982)
  - typical BWR pool = 40' deep by 26' by 39' typical PWR pool = 43' deep by 22' by 40'

Table 1 - Time to Bulk Boiling, and Boil-off Rates													
Time after discharge (days)	Decay power from last core (MW)	Total heat load (MW)	Time to bulk boiling (hr) <sup>(1)</sup>	Boiloff rate (gpm)	Level decrease (ft/hr) <sup>(2)</sup>								
2	16.4	18.4	5.6	130	1.0								
10	8.6	10.6	9.8	74	0.6								
30	5.5	7.5	14	52	<b>0.42</b> ≈0.5								
60	3.8	5.8	18	41	0.33								
90	3.0	5.0	21	35	0.28								
180	1.9	3.9	27	27	0.22								
365	1.1	3.1	33	22	0.18≈0.2								

Notes:	(1)	multiply by 0.84 for full pool, and by 0.34 for 20' deep pools (to correct for he	at capacity of
		the fuel racks and fuel)	

(2) using the typical pool sizes, it is estimated that, for BWRs we have 1040 ft<sup>3</sup>/ft depth, and for PWRs, we have 957 ft<sup>3</sup>/ft depth. Assume ≈1000 ft<sup>3</sup>/ft depth for level decreases resulting from boil-off.

In a SFP, the depth of water above the fuel is typically 23 to 25 feet. Subtracting 3 feet to account for shielding requirements, it is estimated that approximately 20 feet of water will have to boil-off before the start of fuel uncovery. Therefore, using the above table, the available time for operator actions for the loss of cooling type accidents is estimated as follows:

For 1-year old fuel, time available = time to bulk boiling + time to boildown to 3' above fuel = 33 hr x 0.84 + 20 ft / 0.2 ft/hr = 128 hours For 1-month old fuel, time available = 14 hr x 0.84 + 20 ft / 0.5 ft/hr = 52 hours

The above simple calculations show that, for 1-year old fuel (Cases 1 & 3), it will take longer than one day to heat the water to the boiling temperature and take almost five hours to boil off

every foot of water at one year after shutdown. Therefore it would take about five days to reach the point of fuel uncovery if the only mechanism to lose water is through heat-up and boil-off. Similarly, for 1-month old fuel (Case 2), it would take in excess of 50 hours to reach the point of fuel uncovery from pool heat-up and boil-off. For loss of inventory events, the available times will be less. This is discussed more in detail in the section on accident progression.

Based on the estimation of available times, human error probabilities (HEPs) were estimated for recovery actions to mitigate potential accidents at SFPs. These HEPs are described more in Appendix A and in the section on accident progression. In this PRA, the HEPs for the different operator actions in an accident sequence are assumed to be somewhat dependent. For example, the time available (and therefore the probability of operator failure) to recover inventory using offsite sources will be dependent on the time spent on trying to repair the onsite cooling pumps or time spent trying to start make-up or fire pumps. In addition, operator misdiagnosis of the problem to begin with will fail all recovery actions. Because of these dependencies, it should be considered that HEPs within an accident sequence are conditional upon the previous events in that sequence. [The fact that this is a generic study, and since it is assumed that no detailed guidance or procedures are present to guide the operator on a time-frame as to when certain actions have to be completed, this operator action dependency has to be accounted for. The presence of more detailed procedures (e.g., ones with time-lines as a function of fuel age) would permit the consideration of the HEPs within a sequence as being more independent.]

#### Accident Sequence Progression

Given an initiating event, the modeling of accident sequence progression is modeled using the event tree methodology. The split fractions in the event tree branches are quantified using the data provided in Appendix A and the fault trees provided in Appendix B. The relationship of the event tree functional equations and the fault trees is also provided in Appendix B. (Note that the basic event probabilities for the fault trees in Appendix B are estimated based on assumptions for Case 1. These basic event probabilities may be different for the assumptions for Cases 2 or 3. The basic event values for all three cases are provided in Appendix A).

The event trees are provided in Figures 2 through 7. A description of the event trees is provided below.

#### Seismic Initiating Event (EQE)

# Event EQE - Frequency of a seismic event greater than 3 times SSE

In this analysis it is assumed that the spent fuel pools are sufficiently robust for seismic events less than three times the SSE and that the HCLPF value for the spent fuel pool integrity is equal to 3 x SSE. For the majority of plant sites, 3 x SSE is in the range of 0.4g to 0.5g. Seismic hazard curves provided by EPRI (EPRI NP-4726 dated November 1988, and EPRI NP-6395-D dated April 1989) and by LLNL (NUREG-1488 dated April 1994) show that for most plants, the mean frequency of seismic accelerations in the range of 0.4g to 0.5g is on the order of or less than  $2x10^{-5}$  per year - see Table 2.

#### Event FPI - Fuel pool intact

Using the definition for "HCLPF" (i.e., the acceleration at which there is a 95% confidence that less than 5% of the time the SSC will fail), the probability that the SFP will fail given a seismic event greater than 3xSSE is approximately 0.05.

Note that, failure frequencies obtained by applying the above approximation may be nonconservative when compared to failure frequencies obtained by the convolution of the SFP fragility curve and the seismic hazard curve. (In several test cases, applying the "HCLPF approximation" underestimates the seismic effect by a factor of 2 to 3 when compared to results obtained by the convolution of the fragility curve and the hazard curve.) However, for this generic study where site-specific hazard curves or fragility curves are not used, this approximation is adequate, especially since the assumed initiating event frequency is conservative for the majority of plants.

#### Event CSI - Structural integrity of the cooling systems

For the cases (95% of the time) where the pool remains intact, the availability of the SFP cooling and makeup systems has to be determined. In this study, it is conservatively assumed that given a seismic event greater than 3xSSE, some portion of the cooling system and regular makeup system will fail. (This includes failure of the piping, the pumps, electrical components like relays, or the loss of offsite power. This also includes failure of the surrounding structures which may damage components related to SFP cooling.) No recovery of these failed systems is assumed. Therefore, the ability for normal cooling and makeup will be lost.

Note that seismic events less than 3xSSE can also fail cooling systems or result in a loss of offsite power. These events are not included in this event tree, but can be subsumed into the "Loss of Cooling" and the "Loss of Offsite Power from Severe Weather" initiating events.

#### Event OFB - Recovery using on-site or offsite sources

This event accounts for recovery of coolant makeup using portable diesel-powered pumps or use of offsite sources such as the fire brigade. Adequate time is available for this action - in excess of 120 hours in Case 1, and approximately 50 hours in Case 2. However, recovery efforts may be hindered since there could be considerable damage to the infrastructure around the plant site at earthquake accelerations of 0.4g or greater. In addition, it is not clear if there will be adequate procedures to guide operators on recovery efforts given the loss of normal cooling and makeup systems. For this event, a failure probability of 0.05 is used.

Table 2 - I	Mean Annual Proba	bility of Exceedan
ite	400 cm/sec <sup>2</sup>	500 cm/sec <sup>2</sup>
rkansas	2.4E-5	1.4E-5
ver Vallev	2.9E-5	1.8E-5
lefonte	2.6E-5	1.4E-5
n Rock Point	9.6E-6	6.0E-6
	7.6E-6	4.1E-6
	1.3E-5	7.1E-6
	3.75-5	2 3E-5
	1.0E-5	5 5E-6
	7.65.6	3.9E-6
	7.52-6	1.4E-5
Calvert Cliffs	2.3E-5	1.45-5
Catawba	2.0E-5	1.1E-0
Clinton	3.6E-# 5	2.2E-5
ComanchePeak	2.0E-6	1.1E-6
Cook	1.4E-5	8.8E-6
Cooper	5.9E-5	3.8E-5
Crystal River	3.6E-6	2.1E-6
Davis Besse	1.6E-5	8.5E-6
Dresden	9.4E-6	5.0E-6
Duane Arnold	2.6E-6	1.4E-6
Farley	4.2E-6	2.4E-6
Fermi	7.6E-6	4.1E-6
Fitzpatrick	8.3E-6	4.4E-6
Ft Calhoun	4.9E-5	3.2E-5
Ginna	1.7E-5	9.6E-6
Grand Gulf	7.8E-6	4.6E-6
Haddam Neck	2.6E-5	1.4E-5
Hatch	1.4E-5	8.6E-6
Hope Creek	2.7E-5	1.7E-5
Indian Point	2.6E-5	1.4E-5
Kaugunos	1 16-5	7.2E-6
Newaunee	1.12-5	R 4F-6
Lacrosse	1.35-0	1.7E_5
Lasalie	2.82-5	1.75-0
Limerick	2.8E-5	1.5E-5
Maine Yankee	2.7E-5	1.5E-5
McGuire	1.6E-5	8.1E-6

#### Internal Fire Initiating Event (FIR)

# Event FIR - Frequency of a fire event in the building housing the SFP

Typically, the SFP is located in the reactor building (in most BWRs), and either in a separate fuel handling building or the auxiliary building (for PWRs). Generic fire ignition frequencies for different plant locations can be obtained from EPRI's Fire-Induced Vulnerability Evaluation (FIVE) document (EPRI TR-100370s dated April 1992). For BWR reactor buildings, the generic initiating event frequency is 2.5E-2 yr<sup>1</sup> from pumps and 5.0E-2 yr<sup>1</sup> from electrical cabinets. For PWR auxiliary buildings, the generic initiating event frequency is 1.9E-2 yr<sup>1</sup> from pumps and 1.9E-2 yr<sup>1</sup> from electrical cabinets. These frequencies are dominated by the larger pumps and cabinets (e.g., those from the ECCS) which are assumed to be no longer present in decommissioned plants. Therefore, these frequencies are not directly applicable to our study. Fire ignition frequencies for fuel handling buildings are not provided in the EPRI FIVE report. The most similar locations would be the "radwaste area" or the "intake structure". For the radwaste area, the only ignition sources listed are for "miscellaneous components" and the ignition frequency for these components is 8.7E-3 yr<sup>1</sup>. For the intake structure, ignition frequencies are 2.4E-3 yr<sup>1</sup> for electrical cabinets, 4.0E-3 yr<sup>1</sup> for fire pumps, and 3.2E-3 yr<sup>1</sup> for "others". Therefore, for both the radwaste area and the intake structure, the fire ignition frequency is approximately 9E-3 yr<sup>1</sup>. This will be somewhat conservative for this study since some of the equipment considered in the FIVE database will not be present in a decommissioned SFP building. However, other "plant-wide" components such as junction boxes, air compressors, and transients (extension cords, heaters, etc.) which could contribute to this frequency will not be added to this total. Therefore, 9E-3 yr<sup>1</sup> will be used as initiating event frequency for Cases 1 and 3.

For Case 2, it is assumed that the dismantling of plant systems will be ongoing. Therefore, fire ignition frequency contribution from welding and cutting has to be included. From Table 1.2 of the EPRI FIVE document, this contribution is  $3.1E-2 \text{ yr}^1$ . Adding this to the 9E-3 from above yields a frequency of 0.04 yr<sup>1</sup> for Case 2.

Note: The above frequencies are comparable to those estimated from operating experience compiled by AEOD (AEOD/S97-03, "Special Study: Fire Events - Feedback of U.S. Operating Experience", dated June 1997). For example, the AEOD data shows the following fire event frequencies (per year) for periods when the plant is operating:

Table 3a - Fire Frequency by Plant Location - Power Operations												
Location	1965-1985	1986-1994	1965-1994									
Reactor building (BWR)	0.122	0.087	0.105									
Auxiliary building (PWR)	0.107	0.056	0.082									
Service water pump house	0.004	0.007	0.005									
"Other" buildings (includes Radwaste and Fuel Handling buildings)	0.041	0.020	0.031									

When the plant is shutdown (0% power), the AEOD report provides the following fire initiator frequencies:

Table 3b - Fire Frequency by Plant Location -           Shutdown										
Location	1965-1994									
Reactor building (BWR)	0.027									
Auxiliary building (PWR)	0.018									
Switchgear room	0.0065									
Diesel Generator building	0.032									

Again, the above frequencies are consistent with those used in this SFP risk analysis.

Event OSP - Probability of fire suppression and probability that the unsuppressed fire will fail the SFP cooling function

The probability of fire suppression is obtained from a EPRI report titled "Fire Requantification Studies" (NSAC-181, dated March 1993). On page 3-17 of NSAC-181, the probabilities of failure to suppress a fire for three damage times are as follows:

Table	Table 4 - Probability of Failure of Fire Suppression														
Damage Time	Automatic Actuation	Manual Recovery	Manual Suppress	Total											
3	0.05	1.0	0.7	0.035											
13	0.05	0.33	0.4	0.007											
20	0.05	0.33	0.33	0.005											

The above probabilities were estimated based on information on operating reactors. For decommissioned plants, the fire protection program may be changed (see Draft Regulatory Guide DG-1069 dated July 1998, "Fire Protection Program for Nuclear Power Plants During Decommissioning and Permanent Shutdown"). Depending on changing plant conditions, features such as automatic fire suppression systems or an onsite fire brigade may no longer be required.

The modeling of fire growth and propagation and the determination of the effects of a fire on equipment in a room would optimally take into account the combustible loading in the room, the presence of intervening combustibles, the room size and geometry, and other characteristics such as ventilation rates and presence openings in the room. Since detailed input such as these are not applicable for a generic study such as this, fire growth and propagation will have to be determined based on best estimate assumptions. A damage time in excess of 20 minutes is assumed since typical SFP buildings/areas

are relatively large and since equipment within such buildings are usually spread-out. That is, it is assumed that it will take at least 20 minutes before a fire will either fail of the cooling pumps or fail offsite power feed to the pumps. Therefore, from Table 4, the probability of failure of fire suppression is 0.005. However, given the discussion in the above paragraph, it is assumed that suppression is not as effective in a decommissioned plant as it would be in an operating reactor, and the failure probability will be increased by a factor of 10. Thus, the probability of failure of fire suppression, and the probability that this unsuppressed fire will fail the SFP cooling function is 0.05 (for Cases 1 and 3).

In Case 2, it is more likely that the SFP area will be occupied, or that operators in surrounding areas will detect a potential fire and will initiate suppression efforts. Therefore, the probability of failure to suppress in this case will be decreased by a factor of 5 to 0.01.

# Event OMK - Operator recovery using diesel fire pumps

Given a fire event that is unsuppressed and that is sufficiently large to fail the SFP cooling function, it is assumed that this fire also fails offsite power feed to the plant (failure of the bus, cabling, etc.). Therefore, recovery of cooling will be through the use of the diesel fire pump for coolant makeup. Given the amount of time available, the failure of this function is dominated by the unavailability of the diesel pump (the pump fails to start or run, or the pump is out for maintenance). Note that there may be a dependency of this event with previous event since the failure of manual suppression may be due to failure of fire pumps. However, given that there is sufficient time (120 hours in Cases 1 & 3, and 50 hours for Case 2) for recovery action, this dependency is not modeled.

The cutsets for this event consist of the unavailability of the diesel fire pump or the failure of the operator to start this pump - see gate GLPR142 in fault tree LOP-REC. For Case 1, the HEP used is 0.01, and for Case 2, the HEP is 0.08. In Case 3, this event is assumed to fail, since fire pumps are assumed to be unavailable in this case.

#### Event OFD - Recovery using offsite sources

Given the failure of recovery actions using onsite sources, this event accounts for recovery of coolant makeup by use of offsite sources such as the procurement of a portable diesel generator or the use of the fire brigade. Adequate time is available for this action provided that there is a fast enough recognition that recovery of cooling using onsite sources will not be successful, and that offsite sources are the only viable alternatives. It is not clear what plant procedures (if any) will direct the operator to do, and what the time-line would be before the operator is to resort to offsite sources. However, given adequate time and trained operators, a failure probability of 0.01 is estimated for this event.

#### Loss of Cooling Initiating Event (LOC)

#### Event LOC - Frequency of a loss of SFP cooling event

The initiating event frequency includes the loss of coolant system flow from the failure of pumps or valves, from piping failures, from an ineffective heat sink (e.g., loss of heat exchangers), or from a local loss of power (e.g., electrical connections.) Operational data from NUREG-1275, Volume 12 shows that the frequency of loss of spent fuel pool cooling events in which a temperature increase of more than 20°F occurred can be estimated to be on the order of two to three events per 1000 reactor years. The data also showed that, for the majority of events, the duration of the loss of cooling was less than one hour. Only three events where the temperature increase exceeded 20°F, with the maximum increase being 50°F.

#### Event CRA - Control room alarms

An NRR survey of SFP systems performed as part of NUREG-1275, Vol 12 identified a wide range of instrumentation designs at existing plants. Typically, each plant has some type of instrumentation to monitor the SFP system performance, although the type and extent of instrumentation varied significantly among plants. The parameters monitored include SFP level, temperature, liner leakage, pump discharge pressure, and system flow. Typically, only important parameters are monitored in the control room, while most of the other parameters are monitored/displayed on the local panel. However, many local alarms initiate a common "trouble" alarm in the control room.

For half the plants surveyed in the NUREG-1275 study, SFP temperature is indicated or recorded in the control room, for the other half, indication is on a local panel. For most plants, an abnormal temperature is individually alarmed in the control room, and for the rest of the plants, the alarm is on the local panel that initiates a common trouble alarm in the control room.

Sections 3.3 and 6.2 of NUREG-1275 Vol 12 provide an assessment of the instrumentation for SFPs, and point to the fact that the availability of instrumentation would be an important factor in the results of a risk assessment.

In this event tree, the failure of this branch event is modeled as the failure of the instrumentation (hardware failures), or the failure of the operator to respond given that the instrumentation works as designed. Hardware failures include failure of control room indicators or alarms, instrumentation channel loss of function, local electrical faults, etc.

To quantify the failure of the operator to respond to a signal, several references were researched. In Table 20-23 of NUREG/CR-1278 (Handbook of Human Reliability Analysis with Emphasis on Nuclear Power plant Applications: Final Report, dated August 1983), the estimated HEP for the annunciator response model for two competing signals (e.g., level, temperature, "trouble", radiation) is 6E-4. In a DOE report (Savannah River Site Human Error Data Base Development for Nonreactor Nuclear Facilities, WSRC-TR-

93-581, February 1994), the HEP of 3E-3 is estimated for the failure of operators to respond to a compelling signal given that there are few competing signals. For the SFP analysis, the DOE estimate of 3E-3 is used.

The fault tree combining the HEP and hardware failures is CR-ALARM.

#### Event IND - Other indications of loss of cooling

Given that control room indication is not available (or is ignored or misinterpreted by the operator), other indications of a loss of SFP cooling can come from operator walk-downs of the pool area. Indications could be from the local area alarms, steaming over the pool, temperature and humidity in the area, or low pool level once boiling starts.

From DOE report WSRC-TR-93-581, the HEP provided for the "failure of visual inspection to observe abnormal characteristics" had a range of 0.1 to 0.01. Based on the time available, and assuming an area walk-down once a shift (every 8 to 12 hours), and assuming that the walk-down is performed by a different crew member for each shift, the lower range of the value is used for this HEP.

#### Event OCS - Operator recovery of cooling system

On successfully recognizing the loss of cooling condition (via control room alarms or area walk-downs), the initial focus of the operator action (and this is the HEP) will likely be on the repair of the cooling system.

Conservatively assume mean repair time of 10 hours. (Note: from industry data, mean repair time for pumps is approximately 10 hours. For repair of instrumentation or other local electrical faults, the mean time is typically 1 to 2 hours.)

Probability of failure to repair =  $e^{-\lambda t}$ , where  $\lambda = 1/10$  hrs, and t = available time in hours

In the cases when the operator action is initiated by control room alarms, the time available for Cases 1 and 3 is 128 hours. In Case 2, 52 hours is available. Therefore,

Case 1  $\Rightarrow$  probability of failure to repair =  $e^{-1/10^{+}128}$  = 3E-6 (cap off at 1E-4)

Case 2  $\Rightarrow$  probability of failure to repair =  $e^{-1/10^{\circ}52} = 5.5E-3$ 

In Case 3, it is assumed that there are less procedures and training with regard to repair of failed equipment, and that a maintenance crew will not be available onsite. Therefore, the mean time to repair is assumed to be 40 hours.

Case 3  $\Rightarrow$  probability of failure to repair =  $e^{-1/40^{+}128} = 4.2E-2$ 

In cases when control room indication is not available (or is ignored or misinterpreted by the operator), the following assumptions apply. During walk-downs, the loss of pool cooling will not be obvious until bulk boiling begins. Therefore the available time in

Cases 1 & 3 will be (20 ft) /(0.2 ft per hour) = 100 hours; for Case 2, the available time will be (20 ft) /(0.5 ft per hour) = 40 hours. In addition, it is conservatively assumed that it will be two shifts before the operator will recognize the pool boiling or the loss of level. Therefore, the time available is: 100 - 16 = 84 hours for Cases 1 & 3; and 40 - 16 = 24 hours for Case 2. Therefore,

Case 1  $\Rightarrow$ probability of failure to repair =  $e^{-1/10^{+}84} = 2.2E-4$ Case 2  $\Rightarrow$ probability of failure to repair =  $e^{-1/10^{+}24} = 9.1E-2$ Case 3  $\Rightarrow$ probability of failure to repair =  $e^{-1/40^{+}84} = 1.2E-1$ 

#### Event OFD - Operator initiates makeup using fire pumps

Given failure to restore pool cooling using normal equipment, the operator could initiate coolant makeup by use of the makeup pumps or the fire pumps. Failure of this event consists of the failure of the operator to establish alternate cooling, or the failure of both the electric fire pump and the diesel fire pump.

This event is quantified using gates GLCR123 and GLCR163 in fault tree LOC-REC. In gate GLCR123, a HEP of 0.01 is estimated and this is used for the case where the control room alarms are functional and the operator is alerted early that a potential problem exists. In gate GLCR163, a HEP of 0.02 is estimated and this is used for the case where the control room alarms are either non-functional and operator response time is reduced. The above HEPs are for Case 1. For Case 2, the operator response time is less and HEPs of 0.08 and 0.16 are used for the control room alarm and no control room alarm scenarios respectively. In Case 3, this event is assumed to fail, since fire pumps are assumed to be unavailable in this case.

#### Event OFB - Recovery using offsite sources

This event is similar to event OFB in the internal fire event tree. A failure probability of 0.01 is used for this event.

# Loss of Coolant Inventory Initiating Event (LOI)

#### Event LOI - Frequency of a loss of coolant inventory event

This initiator includes loss of coolant inventory from events such as those resulting from configuration control errors, siphoning, piping failures, and gate and seal failures. Operational data provided in NUREG-1275, Volume 12 show that the frequency of loss of inventory events in which a level decrease of more than one foot occurred can be estimated to be (on the order of) less than one event per 100 reactor years. Most of these events were the result of operator error and were recoverable. NUREG-1275 shows that, except for one event that lasted for 72 hours, there were no events that lasted more than 24 hours. Eight events resulted in a level decrease of between one

and five feet, and another two events resulted in an inventory loss of between five and 10 feet.

# Event NLL - Loss exceeds normal makeup capacity and isolation of break is required

Using the information from NUREG-1275, it can be estimated that 6% of the loss of inventory events will be large enough and/or occur for a duration that is long enough so that isolation of the loss is required if the only system available for makeup is the spent fuel pool makeup system. For the other 94% of the cases, operation of the makeup pump is sufficient to prevent fuel uncovery.

From Table 3.2 of NUREG-1275, there were 38 events that led to a loss of pool inventory. If we do not consider the load drop event (since this is treated in a separate event tree), we have 37 events. Of these, 2 events involved level drops of greater than 5 feet. Therefore it is estimated that 2 / 37 or approximately 6 percent of events result in large loss of inventories.

#### Event CRA - Control room alarms

A discussion of this event is provided in the writeup for the "Loss of Coolant" event tree. Specific to level alarms, the SFP level sensor usually has a narrow range, typically 4 feet, covering high and low alarm setpoints and the minimum Technical Specification level. The control room level indicator provided by this sensor is good only for this narrow range. Therefore the control room indicator cannot monitor a level below this range and may not be useful for lower level conditions expected of a gross loss of SFP coolant inventory event. The HEP of 3E-3 used in this analysis reflects this condition (i.e., some competing signals).

#### Event IND - Other indications of loss of cooling

Given that control room indication is not available (or is ignored or misinterpreted by the operator), other indications of a loss of SFP inventory can come from operator walkdowns of the pool area. Indications could be from the local area alarms (radiation alarms, building sump high level alarm, etc.), low pool level, accumulation of water in unexpected locations, etc.

From DOE report WSRC-TR-93-581, the HEP provided for the "failure of visual inspection to observe abnormal characteristics" had a range of 0.1 to 0.01. Based on the time available, and assuming an area walk-down once a shift (every 8 to 12 hours), and assuming that the walk-down is performed by a different crew member for each shift, the lower range of the value (i.e., 0.01) is used for this HEP for the small inventory loss cases. For the large losses where the available time will be much less, the upper range (i.e., 0.1) is used for this HEP. These HEP values are applicable for both Cases 1 and 2. For Case 3, where walkdown requirements may be less, and operators may be less experienced, HEPs of 0.05 and 0.2 are used for the small and large losses respectively.

# Event OIS - Operator isolates inventory loss and initiates makeup through makeup pumps

This event applies for the "large" loss of inventory events. On successfully recognizing the loss of inventory condition (via control room alarms or area walk-downs), the initial focus of the operator action will likely be on the isolation of the inventory loss, and on the initiation of makeup using the makeup pumps. Failure of this event is modeled as the failure of the operator to isolate the loss and initiate the makeup system or the failure of the makeup system itself. Gate GLIR121 of fault tree LOI-REC quantifies this event for the case where control room alarms are effective, and Gate GLIR151 of fault tree LOI-REC quantifies this event for the case where operator action is initiated by area walkdowns (and therefore, less time is available). In both these cases, hardware failure of the makeup system is the dominant cause of failure.

Timing for the "large" loss of inventory event is estimated as follows: From NUREG-1275 V12, the largest inventory loss resulted in a level drop of between 5 to 10 ft. In a foreign plant, an incident resulted in a level drop of 16'. For this analysis, assume a drop of between approximately 15 ft leaving approximately 8 ft of water above the fuel assemblies. Using similar methodology as that used to calculate timing for LOC events:

For 1-yr fuel, time available	<ul> <li>= time to bulk boiling + time to boildown to 3' above fue</li> <li>= 33 hr x 0.34 + 5 ft / 0.2 ft/hr</li> <li>= 36 hours</li> </ul>
For 1-month fuel, time availa	ble = 14 hr x 0.34 + 5 ft / 0.5 ft/hr = 15 hours

#### Event OIL - Operator initiates makeup using makeup pumps

This event is similar to event OIS except that, in this case, isolation of the inventory loss is not required since the failure size is such that the makeup pumps is of sufficient capacity to overcome the loss. In this case, the operator action is simpler and there is more time to perform the action. However, similar to event OIS, hardware failure of the makeup system is the dominant cause of failure.

The time available for operator actions in this event is similar to that for a loss of cooling event, i.e., approximately 120 hours for Cases 1 and 3, and 50 hours for Case 2.

#### Event OMK - Operator initiates makeup using fire pumps

Given failure to restore pool cooling using normal equipment, the operator could initiate coolant makeup by use of the fire pumps. Failure of this event consists of the failure of the operator to establish alternate cooling, or the failure of both the electric fire pump and the diesel fire pump.

This event is quantified using gates GLIR123, GLIR153 and GLIR183 in fault tree LOI-REC. In gate GLIR123, the HEP is estimated for the case where the control room alarms are functional and the operator is alerted early that a large loss of inventory event exists. In gate GLIR153, the HEP is estimated for the case where the control room alarms are either non-functional and operator response time is reduced. In gate GLIR183, the HEP is estimated for the case where the inventory loss is small and operator response time is expansive. Note that the HEP basic events used to quantify this event are the same as those used in events OIS and OIL to account for the potential dependencies in these events.

#### Event OFD - Recovery using offsite sources

Given the failure of recovery actions using onsite sources, this event accounts for recovery of coolant makeup by use of offsite sources such as the procurement of a portable diesel generator or the use of the fire brigade. For the small loss of inventory events, adequate time is available for this action provided that there is a fast enough recognition that recovery of cooling using onsite sources will not be successful, and that offsite sources are the only viable alternatives. It is not clear what plant procedures (if any) will direct the operator to do, and what the time-line would be before the operator is to resort to offsite sources. However, given adequate time and trained operators, a failure probability of 0.05 is estimated for this event. Note that this is higher than the 0.01 estimated for the loss of cooling type events since there will be less time available for this event. For larger leaks, even less time will be available (see timing estimated in the event OIS) Therefore, for these events, failure probabilities of 0.1 and 0.2 for were estimated for scenarios with and without control room alarms respectively

#### Loss of Offsite Power from Plant Centered and Grid Related Events (LP1)

#### Event LP1 - Frequency of a loss of offsite power from plant centered and grid related events

Plant centered events typically involve hardware failures, design deficiencies, human errors (in maintenance and switching), localized weather induced faults (e.g., lightning), or combinations of these. Grid related events are those in which problems in the offsite power grid cause the loss of offsite power. For this study, a frequency of 0.08 per year is used to be consistent with INEL-96/0334. This is also consistent with operating data as discussed below.

Using operating data at nuclear power plants for the years 1980 to 1996, NUREG/CR-5496 estimated an initiating event frequency of LOSP from plant-centered events during power operation to be 0.04 per unit critical year. In NUREG/CR-5496, LOSP is defined as an event that results in a loss of power to all safety (vital) buses and a signal for all available emergency AC generators to start and power their respective buses. Events were included if a reactor trip occurs. For these reasons, the NUREG/CR-5496 frequency may be slightly non-conservative when applied to decommissioned SFPs since LOSP could be defined to loss of power to a non-vital bus.

NUREG/CR-5496 also estimates the frequency of LOSP from plant-centered events during shutdown to be 0.18 per shutdown year. Finally, grid-related events were estimated to be relatively minor contributors at 0.0019 per site calendar year.

#### Event DG - Diesel for fire pump starts and runs

This event represents the failure of the diesel fire pump to start and run and consists of the failure of the operator to manually start the pump or hardware failure of the pump itself. Gate GLPR142 of fault tree LOP-REC models this event.

Note that the unavailability of the diesel pump is relatively high (0.18 for Cases 1 and 2, and unity for Case 3). This is consistent with data used in INEL-96/0334 and is also consistent with reliability data on non-Class 1E diesel pumps and unavailability of plant equipment not controlled by technical specifications.

# Event OPR - Offsite power recovery prior to fuel uncovery

The probability of recovery of offsite power was estimated using the methodology in NUREG/CR-5032. Given in excess of 50 hours for power recovery, a non-recovery probability of 0.001 was estimated.

#### Event OCS - Cooling system re-start and run

On recovering offsite power, the normal SFP cooling pumps will have to be re-started manually. Failure of this event consists of failure of the operator to re-start the pumps or hardware failure of the pump or the support systems. The fault tree used to quantify this event is CS-REC.

This event is not applicable for the sequences where offsite power is not recovered.

# Event OMK - Operator initiates makeup using fire pumps

Given the failure to restore pool cooling using normal equipment, the operator could initiate coolant makeup by use of the fire pumps. Failure of this event consists of the failure of the operator to establish alternate cooling, or the failure of the fire protection pumps. Fault tree LOP-REC models this event. In the sequence where the diesel successfully starts and offsite power is recovered (i.e., events DG and OPR are successful), both the electric fire pump and the diesel fire pump will be available - gate GLPR112 of LOP-REC. In the sequence where the diesel fails but offsite power is recovered, only the electric fire pump will be available - gate GLPR172 of LOP-REC.

# Event CFD - Recovery using offsite sources

This event accounts for recovery of coolant makeup using offsite sources such as portable pumps or the fire brigade. Although a failure probability of 0.01 was used for the other loss of cooling type initiators (see events LOC and FIR), a higher failure probability of 0.05 was assigned here since it is uncertain (without the benefit of plant procedures) as to how long the operator will wait for the recovery of offsite power before initiating other actions to makeup inventory.

# Loss of Offsite Power from Severe Weather Events (LP2)

# Event LP2 - Frequency of a loss of offsite power from severe weather events

Severe weather is defined as forceful and non-localized effects. A loss of offsite power was classified as a severe weather event if the weather was widespread and capable of major disruption. Examples of severe weather include hurricanes, tornadoes, snow and ice storms. When modeling the LOSP initiator, severe weather events are separated from the plant-centered and grid-related events because the probability of recovery of offsite power from these events could be substantially different.

The frequency of a LOSP from severe weather events is 0.007 per year (from NUREG/CR-5496).

# Event DG - Diesel for fire pump starts and runs

This is similar to event DG in the LP1 event tree.

# Event OPR - Offsite power recovery prior to fuel uncovery

The probability of failure to recover offsite power is obtained from Figure B-19 of NUREG/CR-5496. For Cases 1 and 3, the time to fuel uncovery is approximately 120 hours, and the probability of failure to recover power is 0.02. For Case 2, the time to fuel uncovery is approximately 50 hours, and the probability of failure to recover power is 0.1.

#### Event OCS - Cooling system re-start and run

This is similar to event OCS in the LP1 event tree. This is slightly non-conservative since offsite power recovery is likely to occur later in the sequence, thereby allowing less time for operator action.

# Event OMK - Operator initiates makeup using fire pumps

This is similar to event OMK in the LP1 event tree.

# Event OFD - Recovery using offsite sources

This is similar to event OFD in the LP1 event tree.

#### **Analysis Results**

Results are summarized in the table below

Table 4 Spent Fuel Pool Cooling Risk Analysis Frequency of Fuel Uncovery (per year)												
INITIATING EVENT	CASE 1	CASE 2	CASE 3									
Loss of Offsite Power - Plant centered and grid related events	1.3E-06 (11%)	4.2E-06 (5%)	8.0E-05 (30%)									
Loss of Offsite Power - severe weather events	1.4E-06 (12%)	9.4E-06 (12%)	1.4E-05 (5%)									
Internal Fire	8.6E-07 (7%)	1.0E-06 (1%)	9.0E-06 (3%)									
Loss of Pool Cooling	1.5E-07 (1%)	1.7E-07 (0.2%)	1.7E-05 (6%)									
Loss of Coolant Inventory	2.9E-06(25%)	6.0E-05 (75%)	1.3E-04 (49%)									
Seismic Event	2.0E-06 (17%)	2.0E-06 (3%)	2.0E-06 (0.7%)									
Cask Drop	2.5E-06 (21%)	2.5E-06 (3%)	1.5E-05 (6%)									
Aircraft Impact	4.0E-08 (0.3%)	4.0Ε-08 (ε)	4.0Ε-08 (ε)									
Tomado Missile	5.6E-07 (5%)	5.6E-07(0.7%)	5.6E-07 (0.2%)									
Total	1.2E-05	8.0E-05	2.7E-04									

The preliminary results suggest that there may be non-negligible risk associated with spent fuel pools at decommissioned plants during the period analyzed in the risk assessment (one month after removal of last fuel from the reactor to one year after removal of the last fuel.)

A breakdown of the results by accident sequences is provided in Table 5. The cutsets for Cases 1, 2 and 3 are provided in Tables 6a, 6b and 6c respectively. These cutsets are ordered by frequency, and include all the initiating events. Finally, importance rankings for a combination of all initiators are provided in Tables 7a, 7b and 7c for Cases 1, 2 and 3 respectively.

#### **Sensitivity Studies**

Sensitivity cases to determine the effect of various parameter changes on the fuel uncovery frequency is provided in Table 8. These sensitivity cases are for Case 1 SFP model.

#### Some Suggestions for Future Updates

Table 9 lists an expanded version of the cutsets provided in Table 6a. Together with the results of the sensitivity studies in Table 8, this list highlights the events where future refinement may be useful. Table 9 also shows that some modifications to the model are necessary - see for example, cutset number 17 which describes a sequence where the diesel fire pump successfully starts, but where both fire pumps fail (event FP-MKUP-FTF). So that non-minimal cutsets such as these do not occur, future revisions of the model should replace the event FP-MKUP-FTF with an AND gate consisting of the events FP-DGPUMP-FTP and FP-ELPUMP-FTF.

INITIATOR	SEQUENCE	DESCRIPTION	FREQUENCYOF CORE UNCOVERY (per year)										
			Case 1	Case 2	Case 3								
AIR	S02	AIR-FPI	4.000E-008	4.000E-008	4.000E-008								
СЅК	S02	CSK-FPI	2.500E-006	2.500E-006	1.500E-005								
EQE	S06	EQE-CSI-OFD	9.500E-007	9.500E-007	9.500E-007								
	S07	EQE-FPI	1.000E-006	1.000E-006	1.000E-006								
FIR	S04	FIR-OSP-OMK-OFD	8.550E-007	1.040E-006	9.000E-006								
LOC	S04	LOC-OCS-OFB-OFD	6.000E-011	1.485E-008	1.128E-006								
	S08	LOC-CRA-OCS-OFB-OFD	< 1.0E-012	2.325E-009	3.591E-007								
	S09	LOC-CRA-IND	1.503E-007	1.503E-007	1.575E-005								
LOI	S04	LOI-OIS-OMK-OFD	6.600E-007	3.060E-005	1.074E-005								
	S08	LOI-CRA-OIS-OMK-OFD	2.760E-008	2.732E-007	4.032E-006								
	S09	LOI-CRA-IND	3.006E-007	3.006E-007	1.260E-005								
	S13	LOI-NLL-OIL-OMK-OFD	1.410E-006	2.820E-005	4.627E-005								
	S17	LOI-NLL-CRA-OIL-OMK-OFD	7.064E-009	1.413E-007	5.157E-006								
	S18	LOI-NLL-CRA-IND	4.709E-007	4.709E-007	4.935E-005								
LP1	S04	LP1-OCS-OMK-OFD	1.438E-007	2.349E-007	0.000E+000								
	S11	LP1-DG-OCS-OMK-OFD	3.692E-007	2.883E-006	7.575E-005								
	S13	LP1-DG-OPR-OFD	7.600E-007	1.040E-006	4.000E-006								
LP2	S04	LP2-OCS-OMK-OFD	1.258E-008	1.850E-008	0.000E+000								
	S11	LP2-DG-OCS-OMK-OFD	3.230E-008	2.270E-007	6.628E-006								
	S13	LP2-DG-OPR-OFD	1.330E-006	9.100E-006	7.000E-006								
TOR	SO2	TOR-FPI	5.600E-007	5.600E-007	5.600E-007								
NOTES: AI CI CI CI CI CI CI CI CI FI FI IN LC LC LC LC LC CI CI CI CI CI CI CI CI CI CI CI CI CI	R Aircraft cra A Control roc SI Structural SK Cask drop Diesel for DE Seismic ex R Internal fin D Operator a DC Loss of co DI Loss of co DI Loss of of L Loss of of L Loss of of L Loss of of L Loss of of C C Cooling sy FB Operator i FD Recovery IL Operator i SO Operator i SP Fire suppr DR Tornado n	initiating event orm alarms alert the operator of initiator integrity of cooling systems initiating event fire pump fails to start and run vent greater than 3 times SSE e initiating event ntact lefted of initiator fron plant walkdowns olant inventory initiating event site power from plant centered or grid related event site power from plant centered or grid related event site power from severe weather events ventory exceeds makeup capacity and isolation of buster re-start and run initiates makeup using fire pumps using offsite sources (procurement of pumps, fire er initiates makeup using makeup pumps solates inventory loss and initiates makeup thru mal recovery using makeup system or fire pumps wer recovery prior to fuel uncovery ession or no effect on SFP function nissile initiating event	s reak is required ngine, etc) keup pumps										

# Table 5 - Summary of Sequence Frequencies

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# Table 6a - Cutsets for Case 1

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= CASE1.EQN = SFP-1.BED = 86 = 1.158E-005 Equation File Basic Event Data file referenced Number of cut sets in equation Top event unavailability (rare event)

		SFP-REGMKUP-F		HEP-COOL-LUP-E	HEP-COOL-LOP-E		IE-LO-POOL-INV			SPC-PMP-CCF	SPC-PMP-CCF	IE-LO-POOL-INV	HEP-COOL-LOP-E			SPC-HTX-FTR	HEP-COOL-LOP-E	SPC-HTX-FTR	HEP-RES-ALARM	SPC-PMP-CCF	SPC-LVL-LOP	SPC-PMP-CCF		SPC-CKV-CCF-M	SPC-CKV-CCF-M	SPC-HTX-PLG	IE-LO-POOL-INV		SPC-HTX-FTR		SPC-HTX-CCF	SPC-CKV-CCF-H		SPC-HTX-PLG	SPC-HTX-FTR	SPC-PMP-FTF-1	SPC-CKV-CCF-H
FP-DGPUMP-FTF	IE-SEISMIC IE-LO-POOL-INV IE-INT-FIRE FP-DGPUMP-FTF IE-LO-POOL-INV	IE-LO-POOL-INV HEP-RES-ALARM	SPC-LVL-LOP HEP-RES-ALARM	HEP-COOL-LOP-E	SPC-LVL-LOP IE-LOOP-LP1	HEP-ALTCL-LP-E	SFP-REGMKUP-F	IE-INT-FIRE		IE-LOOP-LP1	IE-LOOP-LP1	HEP-INV-MKUP-L	IE-LOOP-LP2	HEP-COOL-LOP-E	HEP-INV-WINUP-L	IE-LOOP-LP1	IE-LOOP-LP2	IE-LOOP-LP1	IE-LO-POOL-INV	E-LOUP-LP2	IE-LO-POOL-INV	IE-LOOP-LP2	LUI-SMALL	IE-LOOP-LP1	SPC-CKV-CCF-M IE-LOOP-LP1	IE-LOOP-LP1	LOI-SMALL	SPC-LVL-LOF	IE-LOOP-LP2 SPC UTY PLC	SPC-HTX-FTR	IE-LOOP-LP1	IE-LOOP-LP1	SPC-HTX-CCF	IE-1 OOP-1 P1	E-LOOP-LP2	IE-LOOP-LP1	IE-LOOP-LP1
IE-LOOP-LP2	REC-INV-OFFSITE LOI-SMALL FP-DGPUMP-FTF IE-LOOP-LP1 HEP-INV-MKUP-E	IE-LO-POOL-INV	NII-TOO-DOT-31	REC-INV-OFFSITE IE-LOOP-LP1	. IE-LO-POOL-INV REC-INV-OFFSITE	HEP-RES-ALARM IE-LOOP-LP2	SPC-LVL-LOP FP-MKUP-FTF	HEP-ALTCL-LP-E		REC-INV-OFFSITE	REC-INV-OFFSITE	REC-INV-OFFSITE3	REC-INV-OFFSITE	IE-LOOP-LP2	REC-INV-OFFSIIE3	REC-INV-OFFSITE	REC-INV-OFFSITE	REC-INV-OFFSITE	LOI-SMALL	REC-INV-OFFSITE	LOI-SMALL	REC-INV-OFFSITE	1-1-04W047-1-0	REC-INV-OFFSITE	IE-LOOP-LP1 REC-INV-OFFSITE	REC-INV-OFFSITE	SFP-REGMKUP-F	<b>IE-LO-POOL-INV</b>	REC-INV-OFFSITE	IE-LOOP-LP2	REC-INV-OFFSITE	REC-INV-OFFSITE	IE-LOOP-LP1	DEC.INV.OFFSITE	REC-INV-OFFSITE	REC-INV-OFFSITE	REC-INV-OFFSITE
IE-CASK-DROP REC-INV-OFFSITE IE-SEISMIC	XEON-UNITY HEP-INV-MKUP-SML REC-FIRE-EVT REC-INV-OFFSITE REC-INV-OFFSITE2	IE-TORNADO-MIS FP-MKUP-FTF Loi-Small	LOI-SMALL REC-WLKDWN-LOI-L	FP-DGPUMP-FTF REC-INV-OFFSITE	REC-WLKDWN-LOI-L	IE-LO-POOL-COOL REC-INV-OFFSITE	IE-LO-POOL-COOL REC-INV-OFFSITE2	REC-FIRE-EVT	REC-INV-UFFSITE	FP-DGPUMP-FTF	FP-MKUP-FTF	XCOM-LOI-SML	FP-DGPUMP-FTF	REC-INV-OFFSITE	XCOM-LOI-SML	FP-DGPUMP-FTF	FP-MKUP-FTF	FP-MKUP-FTF	HEP-INV-MKUP-SML	FP-DGPUMP-FTF	HEP-INV-UFFSITE	FP-MKUP-FTF	FP-MKUP-F1F	FP-DGPUMP-FTF	REC-INV-OFFSITE	FP-DGPUMP-FTF	FP-MKUP-FTF	LOI-SMALL	FP-DGPUMP-FTF	REC-INV-OFFSITE	FP-DGPUMP-FTF	FP-DGPUMP-FTF	REC-INV-OFFSITE	ED MUID ETE	FP-MKUP-FTF	FP-DGPUMP-FTF	FP-MKUP-FTF
XEQN-UNITY REC-OSP-SW SFP-INTEG-HCLPF	XCOM-SFP.INT REC.INV-OFFSITE REC.INV-OFFSITE1 REC-OSP-PC XCOM-LOI-SML	XEQN-UNITY Rec-INV-OFFSITE Rec-WLKDWN-LOI-S	REC-WLKDWN-LOI-S XCOM-LOI-SML	FP-ELPUMP-FTF HEP-ALTCL-LP-E	XCOM-LOI-SML XCOM-DG-START	REC-WLKDWN-LOC REC-OSP-SW	REC-WLKDWN-LOC XCOM-LOL-SMI	REC-INV-OFFSITE1	REC-OSP-PC XEQN-UNITY	FP-ELPUMP-FTF	HEP-ALICL-LP-E XCOM-DG-START	XCOM-IND-LOIL	HEP-RES-ALARM FP-ELPUMP-FTF	HEP-ALTCL-LP-E	XCOM-IND-LOIL	FP-ELPUMP-FTF	XCOM-DG-START	HEP-ALTCL-LP-E XCOM-DG-START	REC-INV-OFFSITE	FP-ELPUMP-FTF	HEP-ALTCL-LP-E REC-INV-OFFSITE	XCOM-DG-START	REC-INV-OFFSITE HFP-RFS-AI ARM	FP-ELPUMP-FTF	HEP-ALTCL-LP-E	FP-ELPUMP-FTF	REC-INV-OFFSITE	REC-WLKDWN-LOI-S	FP-ELPUMP-FTF	HEP-ALICL-LP-E HEP-ALTCL-LP-E	FP-ELPUMP-FTF	FP-ELPUMP-FTF	HEP-ALTCL-LP-E	HEP-ALICL-LP-E	XCOM-DG-START	FP-ELPUMP-FTF	SPU-PMP-FIF-2 XCOM-DG-START
1 2.5000E-006 2 1.2600E-006 3 1 0000E-006	4 9.5000E-007 5 9.4000E-007 6 8.1000E-007 7 7.2000E-007 8 6.000E-007 8 6.000E-007	9 5.6000E-007 10 4.7000E-007 11 2.8200E-007	12 1.8800E-007 13 1.8000E-007	14 1.5120E-007 15 1.4000E-007	16 1.2000E-007 17 1.1340E-007	18 9.0000E-008 19 7.0000E-008	20 6.0000E-008	22 4.5000E-008	23 4.0000E-008 24 4.0000E-008	25 2.5488E-008	26 2.3600E-008 27 1.9116E-008	28 1.6200E-008	29 1 3230E-008	30 1.2250E-008	31 1.0800E-008	32 1.0368E-008	33 9.9225E-009	34 9.6000E-009 35 7 7760E-009	36 2.8200E-009	37 2.2302E-009	38 2.0650E-009 39 1.8800E-009	40 1.6727E-009	41 1.4100E-009	42 1.3824E-009	43 1.2800E-009	45 9.5040E-010	46 9.4000E-010	47 9.4000E-010	48 9.0720E-010	49 8.8000E-010	51 8.2080E-010	52 8.2080E-010	53 7.6000E-010	54 7.6000E-010	55 6.8040E-010	57 6.5707E-010	58 6.1560E-010

# Table 6a (continued)

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SPC-HTX-CCF SPC-PMP-FTF-2		1	SEP-REGMKUP-F				SFP-KEGMKUP-F		SPC-CAV-CC-14		SPC-CKV-CCF-M	SPC-HIX-PLG		SPC-CKV-CCF-H	SPC-HIA-CCF			SPC-HTX-PLG	SPC-PMP-FIF-1		IE-LO-PUUL-INV				SPC-PMP-FIF-Z	SPC-PMP-PI-				SPC-LVL-LOF			SFP-KEGMKUP-F	
IE-LOOP-LP1 SPC-PMP-FTF-1	SPC-LVL-LOF	E-LOOP-LP1	ED-MKI 10-ETF				FP-MKUP-FTF		IE-LOOP-LP2	SPC-CKV-CCF-M	IE-LOOP-LP2	IE-LOOP-LP2	SPC-HTX-PLG	IE-LOOP-LP2	IE-LOOP-LP2	SPC-CKV-CCF-H	SPC-HTX-CCF	IE-LOOP-LP2	IE-LOOP-LP2		HEP-INV-MKUP-L		IE-LOOP-LP2		SPC-PMP-FTF-1	IE-LOOP-LP2		HEP-ALTCL-E	FP-MKUP-FTF	IE-LO-POOL-INV	LOI-SMALL		FP-MKUP-FTF	
REC-INV-OFFSITE IE-LOOP-LP1	IE-LO-POOL-INV	REC-INV-OFFSITE		KEC-INV-OFFOFE		SPC-LVL-LOF	REC-INV-OFFSITE3		REC-INV-OFFSITE	IE-LOOP-LP2	REC-INV-OFFSITE	REC-INV-OFFSITE	IE-LOOP-LP2	REC-INV-OFFSITE	REC-INV-OFFSITE	IE-LOOP-LP2	IE-LOOP-LP2	REC-INV-OFFSITE	REC-INV-OFFSITE		REC-INV-OFFSITE3		REC-INV-OFFSITE	REC-INV-OFFSITE	IE-LOOP-LP2	REC-INV-OFFSITE		IE-LO-POOL-COOL	IE-LO-POOL-COOL	LOI-SMALL	SFP-REGMKUP-F		REC-INV-OFFSITE3	
FP-MKUP-FTF REC-INV-OFFSITE	REC-WLKDWN-LOI-L	FP-MKUP-FTF		XCOM-LUI-SML	HEP-RES-ALARM	IE-LO-POOL-COOL	XCOM-LOI-SML	SPC-LVL-LOP	FP-DGPUMP-FTF	REC-INV-OFFSITE	FP-MKUP-FTF	FP-DGPUMP-FTF	REC-INV-OFFSITE	FP-DGPUMP-FTF	FP-DGPUMP-FTF	REC-INV-OFFSITE	REC-INV-OFFSITE	FP-MKUP-FTF	FP-DGPUMP-FTF		XCOM-LOI-SML		FP-MKUP-FTF	FP-MKUP-FTF	REC-INV-OFFSITE	FP-MKUP-FTF		<b>REC-INV-OFFSITE1</b>	<b>REC-INV-OFFSITE1</b>	HEP-INV-MKUP-SML	FP-MKUP-FTF		XCOM-LOI-SML	SPC-LVL-LOF
XCOM-DG-STAR HEP_AI TCI -I P-F	XCOM-LOI-SML	XCOM-DG-START	SPC-PMP-FIF-Z	XCOM-IND-LOIL	IE-LO-POOL-INV	REC-WLKDWN-LOC	XCOM-IND-LOIL	IE-LO-POOL-INV	FP-ELPUMP-FTF	HEP-ALTCL-LP-E	XCOM-DG-START	FP-ELPUMP-FTF	HEP-ALTCL-LP-E	FP-ELPUMP-FTF	FP-ELPUMP-FTF	HEP-ALTCL-LP-E	HEP-ALTCL-LP-E	XCOM-DG-START	FP-ELPUMP-FTF	SPC-PMP-FTF-2	XCOM-IND-LOIL	SPC-LVL-LOF	XCOM-DG-START	XCOM-DG-START	HEP-ALTCL-LP-E	XCOM-DG-START	SPC-PMP-FTF-2	HEP-COOL-LOC-E	HEP-COOL-LOC-E	REC-INV-OFFSITE	REC-INV-OFFSITE	SPC-LVL-LOF	XCOM-IND-LOIL	IE-LO-POOL-INV
59 6.1560E-010 en e nevne-nin	61 6.0000E-010	62 4.9280E-010		63 3.2400E-010		64 3.0000E-010	65 2.1600E-010		66 1.2096E-010	67 1.1200E-010	68 9.0720E-011	69 8.3160E-011	70 7.7000E-011	71 7.1820E-011	72 7.1820E-011	73 6.6500E-011	74 6.6500E-011	75 6.2370E-011	76 5.7494E-011		77 5.4000E-011		78 5.3865E-011	79 5.3865E-011	80 5.3235E-011	81 4.3120E-011		82 3.0000E-011	83 3.0000E-011	84 9.4000E-012	85 4.7000E-012		86 1.0800E-012	

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Table 6b - Cutsets for Case 2

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Equat Basic Numb Top e	tion File Event Data fil ber of cut sets i vent unavailat	e referenced in equation sility (rare event)	= CASE2.EQN = SFP-2.BED = 91 = 7.975E-005			
۰ ا	0000E-005	XCOM-LOI-SML		XEQN-UNITY	IE-LO-POOL-INV VIL-DOOL-INV	
0 0 0 0	8800E-005 4000E-006	FP-MKUP-FTF	LOI-SMALL	XEQN-UNITY	IE-LO-POOL-INV	SFP-REGMKUP-F
4 6	3000E-006 8000E-006	REC-OSP-SW REC-OSP-SW	REC-INV-OFFSITE REC-INV-OFFSITE	IE-LOOP-LP2 IE-LOOP-LP2	FP-DGPUMP-FTF HEP-ALTCL-LP-E	
i (i 0	5000E-006	XEQN-UNITY	IE-CASK-DROP			
N 4	2400E-006	HEP-ALTCL-LP-E	REC-INV-OFFSITE IF_SFISMIC	IE-LOOP-LP1	HEP-COOL-LUP-E	
- 06 0 09	5000E-007	XCOM-SFP-INT	XEQN-UNITY	REC-INV-OFFSITE	IE-SEISMIC	
10 1	2000E-007	REC-OSP-PC	REC-INV-OFFSITE	IE-LOOP-LP1 EP_ACPI MP_FTF	FP-DGPUMP-F1F IE-INT-FIRE	
12 0	.2000E-007	XCOM-LOI-SML	FP-MKUP-FTF	XEQN-UNITY	IE-LO-POOL-INV	SFP-REGMKUP-F
13 5	.6000E-007	XEQN-UNITY	IE-TORNADO-MIS			
43	.2000E-007	REC-OSP-PC	REC-INV-OFFSITE DEC.EIRE-EVT	HEP-ALTCL-LP-E	IE-INT-FIRE	
10.0	.240E-007	FP-ELPUMP-FTF	FP-DGPUMP-FTF	REC-INV-OFFSITE	IE-LOOP-LP1	HEP-COOL-LOP-E
17 2	.8200E-007	REC-WLKDWN-LOI-S	LOI-SMALL	IE-LO-POOL-INV	HEP-RES-ALARM	
18 18 18 18	.0720E-007	XCOM-DG-START	FP-MKUP-FIF REC-INV-OFFSITE	IE-LOOP-LP1	SPC-PMP-CCF	
2 8	.8800E-007	REC-WLKDWN-LOI-S	LOI-SMALL	IE-LO-POOL-INV	SPC-LVL-LOP	
21 1	.8000E-007	XCOM-LOI-SML	REC-WLKDWN-LOI-L	IE-LO-POOL-INV	HEP-RES-ALARM	HEP-COOL-LOP-E
ន	.7640E-007	XCOM-REC-USP2 XCOM-IND-LOIL	XCOM-LOI-SML	HEP-INV-MKUP-L	XEQN-UNITY	IE-LO-POOL-INV
-	100-10070	HEP-RES-ALARM				
24 1	2000E-007	XCOM-LOI-SML	REC-WLKDWN-LOI-L	IE-LO-POOL-INV HEP.INV/MKLIP.I	SPC-LVL-LOP XFON-LINITY	IE-LO-POOL-INV
-	.000-30000.	SPC-LVL-LOP	VOOIL-FOI-OUT			
80	0000E-008	REC-WLKDWN-LOC	IE-LO-POOL-COOL	HEP-RES-ALARM	SPC.HTX-FTR	
				SPC-LVL-LOP		
58 29 58 29	.000E-008	HEP-INV-MIKUP-SML	LOI-SMALL	XEQN-UNITY	IE-LO-POOL-INV	HEP-RES-ALARM
30 4	.0000E-008	XEQN-UNITY	IE-AIRCRAFT-IMP			
31 3	1,7600E-008 18200E-008	HEP-INV-MKUP-SML FP-MKUP-FTF	LOI-SMALL SFP-REGMKUP-F	XEQN-UNITY LOI-SMALL	XEQN-UNITY	IE-LO-POOL-INV
;		HEP-RES-ALARM				
33 2	2814E-008	FP-ELPUMP-FTF XCOM-RFC-OSP2	FP-DGPUMP-FTF FP-ELPUMP-FTF	REC-INV-OFFSITE FP-DGPUMP-FTF	IE-LOOP-LP1 REC-INV-OFFSITE	SPC-PMP-CCF IE-LOOP-LP2
ч 5		HEP-COOL-LOP-E				
35 1	.8800E-008	FP-MKUP-FTF SPC:1 VI -1 OP	SFP-REGMKUP-F	LOI-SMALL	XEQN-UNIT	
36.1	7464E-008	XCOM-DG-START	EP-MKUP-FTF XCOM-DG-START	REC-INV-OFFSITE	IE-LOOP-LP1 REC-INV-OFFSITE	SPC-PMP-CCF IE-LOOP-LP2
- \o	000-31100.	HEP-COOL-LOP-E				
38 1	4868E-008	XCOM-REC-OSP2	HEP-ALTCL-LP-E	REC-INV-OFFSITE		SPC-PMP-CCF
39 1 40 1	.3200E-008 0368F-008	HEP-COOL-LOC-E	FP-DGPUMP-FTF	REC-INV-OFFSITE	IE-LOOP-LP1	SPC-HTX-FTR
4	.0240E-008	HEP-ALTCL-LP-E	REC-INV-OFFSITE	IE-LOOP-LP1	SPC-CKV-CCF-M	
44	1040E-009	XCOM-DG-START	FP-MKUP-F1F REC-INV-OFFSITE	REC-INV-UFFSILE	SPC-HTX-PLG	
34	.0800E-009	HEP-ALTCL-LP-E	REC-INV-OFFSITE	IE-LOOP-LP1	SPC-HTX-CCF	
45 6	.0800E-009	HEP-ALTCL-LP-E	REC-INV-OFFSITE	IE-LOOP-LP1	SPC-CKV-CCF-H	SDC.HTY.ETR
40 5	0480E-009	ACOM-REC-OSP2 HEP.AI TCI -I P.F	REC-INV-OFFSITE	IE-LOOP-LP1	SPC-PMP-FTF-1	SPC-PMP-FTF-2
i 61 i 49	0072E-009	XCOM-REC-OSP2	FP-ELPUMP-FTF	FP-DGPUMP-FTF	REC-INV-OFFSITE	IE-LOOP-LP2
5	eenne_mo	SPC-PMP-CCF	DEC.INV.OFFSITE1	16-1 0-POOL-COOL	FP-MKUP-FTF	
505	6200E-009	XCOM-IND-LOIL	XCOM-LOI-SML	FP-MKUP-FTF	SFP-REGMKUP-F	XEQN-UNITY
۲ ۲	3R24F-009		HEP-RES-ALARM FP-DGPUMP-FTF	REC-INV-OFFSITE	IE-LOOP-LP1	SPC-CKV-CCF-M
52 1	.3753E-009	XCOM-REC-OSP2	XCOM-DG-START	FP-MKUP-FTF	REC-INV-OFFSITE	IE-LOOP-LP2
53 1	I.3104E-009	HEP-ALTCL-L	HEP-COOL-LOC-L	REC-INV-OFFSITE	IE-LO-POOL-COOL	HEP-RES-ALARM

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# Table 6b (continued)

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54 1.0800E-009	XCOM-IND-LOIL	XCOM-LOI-SML	FP-MKUP-FTF	SFP-REGMKUP-F	XEQN-UNITY
	IE-LO-POOL-INV	SPC-LVL-LOP			
55 9.5040E-010	FP-ELPUMP-FTF YCOM-DC-START	EP-DGPUMP-FTF EP-MKIIP-ETF	REC-INV-OFFSITE	IE-LOUP-LP1	SPC-CKV-CCF-M
57 9.4000E-010	REC-WLKDWN-LOI-S	POI-SMALL	IE-LO-POOL-INV	SPC-LVL-LOF	
58 8.7360E-010	HEP-ALTCL-L	HEP-COOL-LOC-L	REC-INV-OFFSITE1	IE-LO-POOL-COOL	SPC-LVL-LOP
59 8.2080E-010	FP-ELPUMP-FTF	FP-DGPUMP-FTF	REC-INV-OFFSITE	IE-LOOP-LP1	SPC-CKV-CCF-H
60 8.2080E-010	FP-ELPUMP-FTF	EP-DGPUMP-FTF	CD DCDIMD.CTC	IE-LOOP-LP1 DEC_INV_DEFOITE	
	SPC-HTX-FTR				4 5 5 1
62 8.0640E-010	XCOM-REC-OSP2	HEP-ALTCL-LP-E	<b>REC-INV-OFFSITE</b>	IE-LOOP-LP2	SPC-CKV-CCF-M
63 6.5707E-010	FP-ELPUMP-FTF	FP-DGPUMP-FTF	REC-INV-OFFSITE	IE-LOOP-LP1	SPC-PMP-FTF-1
010 10010 10	SPC-PMP-FTF-2				
64 6.5120E-010	XCOM-DG-STAKI				91-410-010
66 5 6240F-010	XCOM-DG-START	FP_MKUP_FTF	REC-INV-OFFSITE	IE-LOOP-LP1	SPC-CKV-CCF-H
67 5.6240E-010	XCOM-DG-START	FP-MKUP-FTF	REC-INV-OFFSITE	IE-LOOP-LP1	SPC-HTX-CCF
68 5.5944E-010	XCOM-REC-OSP2	XCOM-DG-START	FP-MKUP-FTF	<b>REC-INV-OFFSITE</b>	IE-LOOP-LP2
	SPC-HTX-FTR				
69 5.5440E-010 70 5.4000E-010	XCOM-REC-USP2 XCOM-IND-LOIL	HEP-ALICL-LP-E XCOM-LOI-SML	HEP-INV-UFFSITE	XEQN-UNITY	SPC-POOL-INV
	SPC-LVL-LOF				
71 4.7880E-010	XCOM-REC-OSP2	HEP-ALTCL-LP-E	REC-INV-OFFSITE	IE-LOOP-LP2	SPC-HTX-CCF
72 4.7880E-010	XCOM-REC-USP2	HEP-ALTCL-LP-E	REC-INV-OFFSITE		SPC-CKV-CCF-H
10 4'SUZZE-U IV	SPC-PMP-FTF-2				
74 3.8329E-010	XCOM-REC-OSP2	HEP-ALTCL-LP-E	REC-INV-OFFSITE	IE-LOOP-LP2	SPC-PMP-FTF-1
	SPC-PMP-FTF-2				
75 3.0000E-010	REC-WLKDWN-LOC	IE-LO-POOL-COOL	SPC-LVL-LOF		
76 1.8800E-010		LOI-SMALL	KEUN-UNITY	IE-LU-POUL-INV	SPU-LVL-LUP
1/ 1.U000E-UIU	SPC-CKV-CCE-M				
78 9.4000E-011	FP-MKUP-FTF	SFP-REGMKUP-F	LOI-SMALL	XEQN-UNITY	IE-LO-POOL-INV
	SPC-LVL-LOF				
79 8.1900E-011	FP-MKUP-FTF	HEP-COOL-LOC-L	REC-INV-OFFSITE1	IE-LO-POOL-COOL	HEP-RES-ALARM
80 7.4844E-011	XCOM-REC-OSP2	FP-ELPUMP-FTF	FP-DGPUMP-FTF	REC-INV-OFFSITE	IE-LOOP-LP2
81 7.4592E-011	XCOM-REC-OSP2	XCOM-DG-START	FP-MKUP-FTF	REC-INV-OFFSITE	IE-LOOP-LP2
	SPC-CKV-CCF-M				
82 6.4638E-011	XCOM-REC-OSP2	FP-ELPUMP-FTF	FP-DGPUMP-FTF	REC-INV-OFFSITE	IE-LOOP-LP2
83 6.4638E-011	XCOM-REC-OSP2	FP-ELPUMP-FTF	FP-DGPUMP-FTF	REC-INV-OFFSITE	IE-LOOP-LP2
	SPC-HTX-CCF				
84 5.4600E-011 85 5 4744E 014	FP-MKUP-FTF	HEP-COOL-LOC-L	REC-INV-OFFSITE1	IE-LO-POOL-COOL	
	SPC-PMP-FTF-1	SPC-PMP-FTF-2			
86 5.1282E-011	XCOM-REC-OSP2	XCOM-DG-START	FP-MKUP-FTF	REC-INV-OFFSITE	IE-LOOP-LP2
07 1 1000L 011	SPC-HTX-PLG		ED MALID ETE	DEC INV DECOTE	
8/ 4.4289E-UII	SPC-HTX-CCF	INAIS-DU-MOUX			
88 4.4289E-011	XCOM-REC-OSP2	XCOM-DG-START	FP-MKUP-FTF	REC-INV-OFFSITE	IE-LOOP-LP2
89 3.5455E-011	XCOM-REC-OSP2	XCOM-DG-START	FP-MKUP-FTF	REC-INV-OFFSITE	IE-LOOP-LP2
	SPC-PMP-FTF-1	SPC-PMP-FTF-2			
80 3.4000E-012	IE-LO-POOL-INV	SPC-LVL-LOF			
91 4.3680E-012	HEP-ALTCL-L	HEP-COOL-LOC-L	REC-INV-OFFSITE1	IE-LO-POOL-COOL	SPC-LVL-LOF

# Table 6c - Cutsets for Case 3

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Equation File Basic Event Data fi Number of cut sets Top event unavailal	le referenced in equation bility (rare event)	= CASE3.EON = SFP-3.BED = 53 = 2.653E-004			
1 7.2000E-005 2 4.7000E-005 3 4.2065E-005	XEQN-UNITY REC-WLKDWN-LOI-S XCOM-CR-ALARM SEP.AFCMK119-F	REC-INV-OFFSITE LOI-SMALL REC-INV-OFFSITE	IE-LOOP-LP1 IE-LO-POOL-INV LOI-SMALL	HEP-COOL-LOP-E SPC-LVL-LOF XEQN-UNITY	NNI-100d-01-31
4 1.5000E-005	REC-WIKDWN-LOC	IE-LO-POOL-COOL	SPC-LVL-LOF		
9 1.2000E-005	XCOM-LOI-SML	REC-WLKDWN-LOI-L	IE-LO-POOL-INV	SPC-LVL-LOF	
7 9.0000E-006 8 7.0000E-006	XEON-UNITY XEON-UNITY	REC-INV-OFFSITE1 REC-OSP-SW	REC-FIKE-EV I REC-INV-OFFSITE	IE-LOOP-LP2	
9 6.3000E-006	XEON-UNITY	REC-INV-OFFSITE	IE-LOOP-LP2	HEP-COOL-LOP-E	
10 5.3700E-006	XCOM-CR-ALARM HEP-INV-MKUP-E	XCOM-LOI-SML	REC-INV-OFFSILEZ	VEGN-ONIT	
11 5.3700E-006	XCOM-CR-ALARM	XCOM-LOI-SML	REC-INV-OFFSITE2	XEQN-UNITY	IE-LO-POOL-INV
12 4.4650E-006	XCOM-IND-LOIS	REC-INV-OFFSITE	SFP-REGMKUP-F	LOI-SMALL	XEQN-UNITY
13 4.2065E-006	IE-LO-POOL-INV XCOM-CR-ALARM	SPC-LVL-LOF REC-INV-OFFSITE	LOI-SMALL	XEQN-UNITY	IE-LO-POOL-INV
	HEP-INV-MKUP-SML				
14 4.0000E-006 15 2.8800E-006	XCOM-IND-LOIL	KEC-UST-FUC	REC-INV-OFFSITE3	HEP-INV-MKUP-L	XEQN-UNITY
	IE-LO-POOL-INV	SPC-LVL-LOF			
15 2.3600E-006 17 1.4100E-006	REC-WLKDWN-LOI-S		IE-LO-POOL-INV	HEP-RES-ALARM	
18 1.1277E-006	XCOM-CR-ALARM	HEP-COOL-LOC-E	XEQN-UNITY	REC-INV-OFFSITE1	IE-LO-POOL-COOL
19 1.0000E-006	SFP-INTEG-HCLPF XCOM-IND-LOI	IE-SEISMIC XCOM-LOI-SML	REC-INV-OFFSITE3	SFP-REGMKUP-F	XEQN-UNITY
	IE-LO-POOL-INV	SPC-LVL-LOF			
21 9.6000E-007	XEQN-UNITY	REC-INV-OFFSITE	IE-LOOP-LP1 DEC_INIV_DEFSITE	SPC-HTX-FTR IE-SEISMIC	
22 9.5000E-00/ 23 9.4000E-007	REC-WIKDWN-LOI-S	LOI-SMALL	IE-TO-POOL-INV	SPC-LVL-LOP	
24 5.6000E-007	XEQN-UNITY	IE-TORNADO-MIS			
25 4.5000E-007	REC-WLKDWN-LOC	IE-LO-POOL-COOL	HEP-RES-ALARM	OLSMALL YFON-UN	7
26 4.4650E-007	IE-LO-POOL-INV	SPC-LVL-LOF		FUI-OWALL AEGIV-UN	-
27 3.6000E-007	XCOM-LOI-SML	REC-WLKDWN-LOI-L	IE-LO-POOL-INV	HEP-RES-ALARM	
28 3.4200E-007	XCOM-IND-LOC SPC-LVL-LOF	HEP-COOL-LOC-L	XEQN-UNITY	REC-INV-OFFSILE1	
29 3.0000E-007	REC-WLKDWN-LOC	IE-LO-POOL-COOL	SPC-LVL-LOP		
30 2.4000E-007	XCOM-LOI-SML	REC-WLKDWN-LOI-L	1E-LO-POOL-INV 1E-LOOP-LP2	SPC-LVL-LOP SPC-PMP-CCF	
32 1.3395E-007	XCOM-IND-LOIS	REC-INV-OFFSITE	SFP-REGMKUP-F	LOI-SMALL	XEQN-UNITY
20 1 2000E 007	IE-LO-POOL-INV	HEP-RES-ALARM		SPC-CKV-CCF-M	
34 8.9300E-008	XCOM-IND-LOIS	REC-INV-OFFSITE	SFP-REGMKUP-F	LOI-SMALL	XEQN-UNITY
	IE-LO-POOL-INV	SPC-LVL-LOP		S IG, YTT, DOS	
35 8.8000E-008 36 8.6400E-008	XCOM-IND-LOIL	XCOM-LOI-SML	REC-INV-OFFSITE3	HEP-INV-MKUP-L	XEQN-UNITY
	IE-LO-POOL-INV	HEP-RES-ALARM			
37 8.4000E-008 38 7.6000E-008	XEON-UNITY XEON-UNITY	REC-INV-OFFSITE REC-INV-OFFSITE	IE-LOOP-LP1 IE-LOOP-LP1	SPC-CKV-CCF-H	
39 7.6000E-008	XEQN-UNITY	REC-INV-OFFSITE	IE-LOOP-LP1	SPC-HTX-CCF	
40 6.0840E-008	XEQN-UNITY	REC-INV-OFFSITE	IE-LOOP-LP1 DEC INV/DEERITE3	SPC-PMP-FTF-1 HED_INV/MK110_1	SPC-PMP-FTF-2 XEON-LINITY
41 3./ DUVE-UVO	IE-LO-POOL-INV	SPC-LVL-LOP			
42 4.0000E-008	XEQN-UNITY	IE-AIRCRAFT-IMP			
43 2.8800E-008	XCOM-IND-LOIL	XCOM-LOI-SML HEP-RES-ALARM	REC-INV-OFFSILES	ULT-REGMINUL-L	
44 1.9200E-008	XCOM-IND-LOIL	XCOM-LOI-SML	REC-INV-OFFSITE3	SFP-REGMKUP-F	XEQN-UNITY
45 1.3385E-008	IE-LO-POOL-INV XCOM-IND-LOIS	SPC-LVL-LUP REC-INV-OFFSITE	HEP-INV-MKUP-SML	LOI-SMALL	XEQN-UNITY
	IE-LO-POOL-INV	HEP-RES-ALARM		M-300-1010-000	
46 1.1200E-008	XEQN-UNITY	REC-INV-CFT011		るというとうとう	

# Table 6c (continued)

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IE-LO-POOL-COOL	XEQN-UNITY	1000-100d-01-3I	SPC-PMP-FTF-2
REC-INV-OFFSITE1	LOI-SMALL	SPC-HTX-PLG REC-INV-OFFSITE1	SPC-CKV-CCF-H SPC-HTX-CCF SPC-PMP-FTF-1
XEQN-UNITY	HEP-INV-MKUP-SML	IE-LOOP-LP2 XEQN-UNITY	IE-LOOP-LP2 IE-LOOP-LP2 IE-LOOP-LP2
HEP-COOL-LOC-L	REC-INV-OFFSITE SPC-LVL-LOP	REC-INV-OFFSITE HEP-COOL-LOC-L	REC-INV-OFFSITE REC-INV-OFFSITE REC-INV-OFFSITE
XCOM-IND-LOC HEP-RES-ALARM	XCOM-IND-LOIS	XEQN-UNITY XCOM-IND-LOC	SECRA-UNITY XEQN-UNITY XEQN-UNITY
47 1.0260E-008	48 B.9300E-009	49 7.7000E-009 50 6.8400E-009	51 6.6500E-009 52 6.6500E-009 53 5.3235E-009

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Table 7a	- Importance	Ranking	for	Case	1

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<u>Rank</u>	EVENT NAME	Point Estimate	Fussell-Vesely Importance	Risk Achievement Worth	Risk Reduction Worth
1	REC-INV-OFFSITE	5.000E-002	4.331E-001	9.23	1.764
2	XEON-UNITY	1.000E+000	3.498E-001	1.00	1.538
3	EP-DGPUMP-FTF	1.800E-001	2.589E-001	2.18	1.349
4	IE-LO-POOL-INV	1.000E-002	2.484E-001	25.59	1.330
5	IE-CASK-DROP	2.500E-006	2.159E-001	86361.17	1.275
ě	IE-SEISMIC	2.000E-005	1.684E-001	8420.97	1.203
7	LOLSMALL	9.400E-001	1.630E-001	1.01	1.195
8	IE-LOOP-LP2	7.000E-003	1.187E-001	17.84	1.135
ğ	REC-OSP-SW	2.000E-002	1.149E-001	6.63	1.130
10	IE-LOOP-LP1	8.000E-002	1.099E-001	2.26	1.124
11	SFP-INTEG-HCLPF	5.000E-002	8.636E-002	2.64	1.095
12	XCOM-LOI-SML	6.000E-002	8.534E-002	2.34	1.093
13	XCOM-SEP-INT	9.500E-001	8.204E-002	1.00	1.089
14	HEP-INV-MKUP-SML	2.000E-003	8.159E-002	41.71	1.089
15	REC-INV-OFFSITE1	1.000E-002	7.384E-002	8.31	1.080
16	REC-FIRE-EVT	5.000E-002	7.384E-002	2.40	1.080
17	IE-INT-FIRE	9.000E-003	7.384E-002	9.13	1.080
18	REC-OSP-PC	1.000E-003	6.563E-002	66.57	1.070
19	FP-MKUP-FTF	1.000E-002	5.953E-002	6.89	1.063
20	REC-INV-OFFSITE2	1.000E-001	5.700E-002	1.51	1.060
21	HEP-INV-MKUP-E	1.000E-002	5.182E-002	6.13	1.055
22	HEP-RES-ALARM	3.000E-003	4.946E-002	17.44	1.052
23	IE-TORNADO-MIS	5.600E-007	4.836E-002	86361.34	1.051
24	SFP-REGMKUP-F	1.000E-001	4.602E-002	1.41	1.048
25	REC-WLKDWN-LOI-S	1.000E-002	4.067E-002	5.03	1.042
26	HEP-COOL-LOP-E	3.500E-003	3.800E-002	11.82	1.039
27	SPC-LVL-LOP	2.000E-003	3.298E-002	17.45	1.034
28	HEP-ALTCL-LP-E	1.000E-002	3.006E-002	3.98	1.031
29	REC-WLKDWN-LOI-L	1.000E-001	2.596E-002	1.23	1.027
30	FP-ELPUMP-FTF	6.000E-002	1.800E-002	1.28	1.018
31	XCOM-DG-START	8.100E-001	1.350E-002	1.00	1.014
32	IE-LO-POOL-COOL	3.000E-003	1.299E-002	5.32	1.013
33	REC-WLKDWN-LOC	1.000E-002	1.298E-002	2.29	1.013
34	SPC-PMP-CCF	5.900E-004	6.406E-003	11.85	1.006
35	IE-AIRCRAFT-IMP	4.000E-008	3.454E-003	86361.39	1.003
36	SPC-HTX-FTR	2.400E-004	2.606E-003	11.85	1.003
37	XCOM-IND-LOIL	9.000E-001	2.383E-003	1.00	1.002
38	<b>REC-INV-OFFSITE3</b>	2.000E-001	2.383E-003	1.01	1.002
39	HEP-INV-MKUP-L	5.000E-002	2.336E-003	1.04	1.002
40	SPC-CKV-CCF-M	3.200E-005	3.474E-004	11.86	1.000
41	SPC-HTX-PLG	2.200E-005	2.388E-004	11.86	1.000
42	SPC-HTX-CCF	1.900E-005	2.063E-004	11.86	1.000
43	SPC-CKV-CCF-H	1.900E-005	2.063E-004	11.86	1.000
44	SPC-PMP-FTF-1	3.900E-003	1.651E-004	1.04	1.000
45	SPC-PMP-FTF-2	3.900E-003	1.651E-004	1.04	1.000
46	SPC-LVL-LOF	1.000E-005	1.649E-004	17.49	1.000
47	HEP-COOL-LOC-E	1.000E-004	5.182E-006	1.05	1.000
48	HEP-ALTCL-E	1.000E-002	2.591E-006	1.00	1.000

<u>Rank</u>	EVENT NAME	Point Estimate	Fussell-Vesely Importance	Risk Achievement Worth	Risk Reduction Worth
4		1 000E±000	7 933E-001	1 00	4.838
2		1.000E 000	7.500E-001	75 47	4 036
2		6 000E-002	3 000 -001	7 12	1.642
3		5.000E-002	3.303E-001	8 15	1 603
4	HEP-INV-MILUP-E	5.000E-002	3.7020-001	1 02	1.566
5	LUI-SMALL	9.4002-001	3.013E-001	110.22	1 310
6	HEP-INV-MKUP-SML	2.000E-003	2.309E-001	119.23	1.010
7	REC-INV-OFFSITE	5.000E-002	1.812E-001	4.44	1 4 4 9
8	FP-MKUP-FTF	1.000E-002	1.292E-001	13.79	1.140
9	SFP-REGMKUP-F	1.000E-001	1.260E-001	2.13	1,144
10	IE-LOOP-LP2	7.000E-003	1.172E-001	17.62	1.133
11	REC-OSP-SW	1.000E-001	1.141E-001	2.03	1.129
12	FP-DGPUMP-FTF	1.800E-001	1.017E-001	1.46	1.113
13	HEP-ALTCL-LP-E	8.000E-002	7.749E-002	1.89	1.084
14	IE-LOOP-LP1	8.000E-002	5.214E-002	1.60	1.055
15	HEP-COOL-LOP-E	7.000E-003	3.719E-002	6.28	1.039
16	IE-CASK-DROP	2.500E-006	3.135E-002	12540.66	1.032
17	IE-SEISMIC	2.000E-005	2.445E-002	1223.60	1.025
18	REC-INV-OFFSITE1	1.000E-002	1.326E-002	2.31	1.013
19	REC-OSP-PC	1.000E-003	1.304E-002	14.03	1.013
20	IE-INT-FIRE	4.000E-002	1.304E-002	1.31	1.013
21	REC-FIRE-EVT	1.000E-002	1.304E-002	2.29	1.013
22	SFP-INTEG-HCLPF	5.000E-002	1.254E-002	1.24	1.013
23	XCOM-SFP-INT	9.500E-001	1.191E-002	1.00	1.012
24	HEP-RES-ALARM	3.000E-003	1.005E-002	4.34	1.010
25	IE-TORNADO-MIS	5.600E-007	7.022E-003	12540.68	1.007
26	SPC-LVL-LOP	2.000E-003	6.701E-003	4.34	1.007
27	REC-WLKDWN-LOI-S	1.000E-002	5.905E-003	1.58	1.006
28	FP-ELPUMP-FTF	6.000E-002	4.638E-003	1.07	1.005
29	REC-WLKDWN-LOI-L	1.000E-001	3.769E-003	1.03	1.004
30	XCOM-IND-LOIL	9.000E-001	3.426E-003	1.00	1.003
31	HEP-INV-MKUP-I	1.000E-001	3.392E-003	1.03	1.003
32	XCOM-DG-START	7.400E-001	3.178E-003	1.00	1.003
33	SPC-PMP-CCF	5 900E-004	3.135E-003	6.31	1.003
34	XCOM-REC-OSP2	9.000E-001	3.079E-003	1.00	1.003
35		3.000E-003	2.100E-003	1.70	1.002
36	REC-WI KDWN-LOC	1.000E-002	1.885E-003	1.19	1.002
37	SPC-HTX-FTR	2 400E-004	1.275E-003	6.31	1.001
38		4 000E-008	5 016E-004	12540.69	1.001
30		5 500E-003	1 862E-004	1.03	1.000
40		3 2005-005	1 700E-004	6.31	1.000
40		8 000E-002	1.655E-004	1.00	1 000
41		2 2005 005	1 1605-004	6 31	1 000
42		1 0005 005	1 0105-004	6.31	1 000
43		1.9002-003	1.0102-004	6.31	1 000
44	SPU-HIX-UUP	1.9005-000	1.010E-004	1.02	1.000
45	SPU-PMP-F1F-2	3.900E-003	0.0022-000	1.02	1.000
40	5PU-PMP-F1F-1	3.9002-003	0.U02E-UUD	1.02	1.000
47	SPU-LVL-LUF	1.0002-005	3.3300-003	4.30	1.000
48	HEP-COOL-LOC-L	9.100E-002	2.9132-003	1.00	1.000
49	HEP-ALTCL-L	1.600E-001	2./441-005	1.00	1.000

# Table 7b - Importance Ranking for Case 2

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# Table 7c - Importance Ranking for Case 3

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<u>Rank</u>	EVENT NAME	Point Estimate	Fussell-Vesely Importance	Risk Achievement Worth	Risk Reduction Worth
4		1 000E+000	7.034E-001	1.00	3.371
2		5.000E-002	5 494E-001	11.44	2.219
2		1 000E-002	4 830E-001	48.82	1.934
3		9 400E-001	3 798E-001	1.02	1.613
		1 000E-001	3 132E-001	3.82	1.456
5 6		8 000E-007	3.006E-001	4.46	1.430
7		1 800E-002	2 951E-001	17.10	1.419
0		8 950E-002	2 191E-001	1.03	1.281
0		1 000E-001	2.003E-001	2.80	1.250
9 10	SFF-REGWROF-F	5.000E-007	1 860E-001	4.53	1.229
10		5.000E-002	1.000E-001	2 62	1.115
10		3 0005-002	6 497E-002	22.59	1.069
12		5.000E-003	5 936E-002	2.13	1.063
13		1.500E-002	5.654E-002	3770.06	1.060
14		7.000E-003	5.004E-002	8 29	1.054
15		2.00000-000	A 749E-002	1 19	1.050
10	REC-WERDWIN-LOI-L	2.000E-001	4.0485-002	1.36	1.042
17	REC-INV-OFFSITE2	1.000E-001	2 053E-002	4 91	1.041
18	REC-INV-OFFSITET	0.0005-002	3.302E-002	4.01 A 74	1.035
19		9.000E-003	3.3925-002	1 21	1.035
20	REC-FIRE-EVI	2.0005.002	3.392C-002	2.29	1 027
21		1 0005 001	2.030E-002	1 18	1 021
22		0.5005-001	1 9445-002	1.10	1 020
23	NED INV MELID SMI	1.000E-007	1 762E-002	2 74	1.018
24		2.000E-002	1.520E-002	1.06	1.015
20		8 000E-001	1.520E-002	1.00	1.015
20		1 0005-003	1.508E-002	16.06	1.015
20		3 000E-000	1 140E-002	1.03	1.012
20		5 900E-004	9 673E-003	17.39	1.010
29		3 000E-003	9.396E-003	4.12	1.009
30		2.000E-005	7 350E-003	368.48	1.007
32	SPC-1 VI -L OP	2.000E-003	6 264E-003	4.13	1.006
32	HEP-COOL-LOC-E	4 200E-002	4.250E-003	1.10	1.004
34	SPC-HTX-FTR	2.400E-004	3.935E-003	17.39	1.004
35	SFP-INTEG-HCLPF	5.000E-002	3.769E-003	1.07	1.004
36	XCOM-SEP-INT	9.500E-001	3.581E-003	1.00	1.004
37	IF-TORNADO-MIS	5.600E-007	2.111E-003	3770.11	1.002
38	XCOM-IND-LOC	9.500E-001	1.353E-003	1.00	1.001
39	HEP-COOL-LOC-L	1.200E-001	1.353E-003	1.01	1.001
40	SPC-CKV-CCE-M	3.200E-005	5.247E-004	17.40	1.001
40	SPC-HTX-PLG	2.200E-005	3.607E-004	17.40	1.000
42	SPC-HTX-CCF	1.900E-005	3.115E-004	17.40	1.000
43	SPC-CKV-CCF-H	1.900E-005	3.115E-004	17.40	1.000
44	SPC-PMP-FTF-1	3.900E-003	2.494E-004	1.06	1.000
45	SPC-PMP-FTF-2	3.900E-003	2.494E-004	1.06	1.000
46	IE-AIRCRAFT-IMP	4.000E-008	1.508E-004	3770.11	1.000

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	Table 8 - Results of Ser	nsitivity Analysis for	Case 1	
Sensitivity Case	Description	Basic Events Affected	Frequency of Fuel Uncovery (per year)	Comments
S0a	Base case (all initiators) - all basic event probabilities as shown in Appendix A	n/a	1.158E-05	This case is based on the "Case 1" analysis assumptions
SOD	Base case - only initiators that lead directly to fuel uncovery (includes cask drop, aircraft impact, tornado missiles, and seismic events that fail the SFP)	n/a	4.100E-06	This fuel uncovery frequency is independent of human error probability or equipment availability since the contributing IEs are assumed to lead directly to fuel uncovery
S1a	All human actions to mitigate the initiating event is assumed failed, i.e., event probabilities set to 1.0. Human actions to related to "recognition" of the event is not included in this sensitivity case	HEP-ALTCL-E HEP-ALTCL-LP-E HEP-COOL-LOC-E HEP-INV-MKUP-E HEP-INV-MKUP-L HEP-INV-MKUP-SML REC-INV-OFFSITE REC-INV-OFFSITE1 REC-INV-OFFSITE2 REC-INV-OFFSITE3	1.026E-01	Note that, the fuel uncovery frequency in this case approaches the sum of the initiating events of 1.090E-01 per year
S1b	All human actions assumed to be successful, i.e., event probabilities set to 0.0	same as in case S1a	5.022E-06	Even with all human actions assumed successful, this frequency is not equal to the case S0b frequency because the failure of the operator to recognize the event (control room indications or walkdowns) also contribute to this frequency.

	Table 8 - Results of Ser	sitivity Analysis for	Case 1	
Sen <del>s</del> itivity Case	Description	Basic Events Affected	Frequency of Fuel Uncovery (per year)	Comments
S1c	The probability of failure of all human actions were assumed 10 times higher than in the base case. When event probabilities exceed 1.0, these probabilities are capped at a value of 1.0	same as in case S1a	4.050E-04	
S1d	The probability of failure of all human actions were assumed 10 times lower than in the base case	same as in case S1a	5.478E-06	
S2a	All recovery actions using offsite sources (i.e., procurement of pumps, fire engines, etc.) assumed failed, i.e., event probabilities set to 1.0	REC-INV-OFFSITE REC-INV-OFFSITE1 REC-INV-OFFSITE2 REC-INV-OFFSITE3	1.976E-04	
S2b	All recovery actions using offsite sources assumed successful, i.e., event probabilities set to 0.0	same as in case S2a	5.022E-06	Note that this frequency is the same as that in case S1b since offsite recovery events are modeled in all sequences where operator action is feasible.
S2c	The probability of failure of all recovery actions using offsite sources were assumed 10 times higher than in the base case. When event probabilities exceed 1.0, these probabilities are capped at a value of 1.0	same as in case S2a	7.046E-05	
S2d	The probability of failure of all recovery actions using offsite sources were assumed 10 times lower than in the base case	same as in case S2a	5.678E-06	

	Table 8 - Results of Sei	nsitivity Analysis for	· Case 1	
Sensitivity Case	Description	Basic Events Affected	Frequency of Fuel Uncovery (per year)	Comments
S3a	All operator actions to mitigate accident using onsite equipment (i.e., restarting or repairing cooling pumps, use of makeup pumps or fire pumps, etc.) assumed failed, i.e., event probabilities set to 1.0	HEP-ALTCL-E HEP-ALTCL-LP-E HEP-COOL-LOC-E HEP-COOL-LOP-E HEP-INV-MKUP-E HEP-INV-MKUP-L HEP-INV-MKUP-SML	5.024E-03	
S3b	All operator actions to mitigate accident using onsite equipment assumed to be successful, i.e., event probabilities set to 0.0	same as in case S3a	9.372E-06	Note that this frequency is not the same as those in cases S1b and S2b because onsite recovery events are not modeled in all sequences where offsite operator action may be feasible (e.g., seismic events where SFP is intact but where other equipment fails; or in LOSP sequences where power is not restored and the onsite diesel fire pump fails to start)
S3c	The probability of failure of all operator actions to mitigate accident using onsite equipment were assumed 10 times higher than in the base case. When event probabilities exceed 1.0, these probabilities are capped at a value of 1.0	same as in case S3a	4.515E-05	
S3d	The probability of failure of all operator actions to mitigate accident using onsite equipment were assumed 10 times lower than in the base case	same as in case S3a	9.579E-06	

	Table 8 - Results of Ser	nsitivity Analysis for	Case 1	
Sensitivity Case	Description	Basic Events Affected	Frequency of Fuel Uncovery (per year)	Comments
S4a	All onsite equipment assumed to be failed. This "equipment" does not include the SFP structure itself, i.e., the fragility of the SFP is assumed to be the same as in the base case.	FP-DGPUMP-FTF FP-ELPUMP-FTF FP-MKUP-FTF SFP-REGMKUP-F SPC-CKV-CCF-H SPC-CKV-CCF-M SPC-HTX-CCF SPC-HTX-FTR SPC-HTX-PLG SPC-HTX-PLG SPC-LVL-LOF SPC-LVL-LOP SPC-PMP-CCF SPC-PMP-FTF-1 SPC-PMP-FTF-2	5.754E-02	Note that the results in cases S4a thru S4d are not quite the same as those for cases S3a thru S3d since the S4 sensitivity cases include equipment used for control room indication.
S4b	All onsite equipment assumed to be successful	same as in case S4a	7.468E-06	
S4c	The probability of failure of all onsite equipment assumed to be 10 times higher. When event probabilities exceed 1.0, these probabilities are capped at a value of 1.0	same as in case S4a	1.238E-04	
S4d	The probability of failure of all onsite equipment assumed to be 10 times lower	same as in case S4a	7.809E-06	
S5a	Operator recognition of initiator, either from control room or from walkdowns, assumed to be failed	HEP-RES-ALARM REC-WLKDWN-LOC REC-WLKDWN-LOI-L REC-WLKDWN-LOI-S	1.304E-02	
S5b	Operator recognition of initiator, either from control room or from walkdowns, assumed to be always successful	same as in case S5a	1.064E-05	

Table 8 - Results of Sensitivity Analysis for Case 1				
Sensitivity Case	Description	Basic Events Affected	Frequency of Fuel Uncovery (per year)	Comments
S5c	Probability of the failure of operator recognition of initiator, either from control room or from walkdowns, increased by a factor of 10. When event probabilities exceed 1.0, these probabilities are capped at a value of 1.0	same as in case S5a	6.974E-05	
S5d	Probability of the failure of operator recognition of initiator, either from control room or from walkdowns, decreased by a factor of 10	same as in case S5a	1.068E-05	
	Table 8 - Results of Sensitivity Analysis for Case 1			
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Sensitivity Case	Description	Basic Events Affected	Frequency of Fuel Uncovery (per year)	Comments
S6a	All onsite and offsite recovery actions and all equipment assumed to be failed.	FP-DGPUMP-FTF FP-ELPUMP-FTF FP-MKUP-FTF HEP-ALTCL-E HEP-ALTCL-LP-E HEP-COOL-LOC-E HEP-COOL-LOP-E HEP-INV-MKUP-L HEP-INV-MKUP-L HEP-INV-MKUP-SML HEP-RES-ALARM REC-FIRE-EVT REC-INV-OFFSITE REC-INV-OFFSITE1 REC-INV-OFFSITE2 REC-INV-OFFSITE3 REC-WLKDWN-LOC REC-WLKDWN-LOC REC-WLKDWN-LOI-L REC-WLKDWN-LOI-L REC-WLKDWN-LOI-L REC-WLKDWN-LOI-S SFP-REGMKUP-F SPC-CKV-CCF-H SPC-CKV-CCF-M SPC-HTX-FTR SPC-HTX-PLG SPC-LVL-LOF SPC-LVL-LOF SPC-PMP-FTF-1 SPC-PMP-FTF-2	1.090E-01	This is equal to the sum of all the initiating event frequencies

	Table 8 - Results of Sensitivity Analysis for Case 1				
Sensitivity Case	Description	Basic Events Affected	Frequency of Fuel Uncovery (per year)	Comments	
S6b	All onsite and offsite recovery actions and all equipment assumed to be successful.	same as in case S6a	4.100E-06	This is the same as the frequency for the "non-recoverable" initiators - see case S0b	
S6c	The probability of failure of all onsite and offsite recovery actions and all equipment increased by a factor of 10. When event probabilities exceed 1.0, these probabilities are capped at a value of 1.0	same as in case S6a	3.004E-03		
S6d	The probability of failure of all onsite and offsite recovery actions and all equipment decreased by a factor of 10	same as in case S6a	4.242E-06		
S7	Availability of diesel fire pump set to be the same as that for the electric fire pump, i.e., from 0.18 to 0.06	FP-DGPUMP-FTF XCOM-DG-START	9.604E-06		
S8	Probability that a fire event will affect SFP function, i.e., fire will be suppressed or will not be large enough to affect function. Probability changed from 0.05 to 0.01	REC-FIRE-EVT	1.090E-05		
S9	Conditional probability that a loss of inventory event will be "large" changed from 6% to 1%	LOI-SMALL XCOM-LOI-SML	1.086E-05		

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1	2.50E-06	Cask drop event leading to failure of SFP structure 2.5E-06 per year			
2	1.26E-06	LOSP from severe weather events	Diesel fire protection pump fails to start and run	Failure to recover offsite power	Failure to recover inventory using offsite sources
		7.0E-03 per year	0.18	0.02	0.05
3	1.00E-06	Seismic event greater than 3 times SSE	Probability of SFP failure given event		
		2.0E-05 per year	0.05		
4	9.50E-07	Seismic event greater than 3 times SSE	Probability that SFP does not fail given event	Failure of onsite equipment from direct & indirect failure modes	Failure to recover inventory using offsite sources
		2.0E-05 per year	0.95	1.0	0.05
5	9.40E-07	Loss of inventory initiating event	Probability that loss is small	Operator fails to initiate makeup of inventory	Failure to recover inventory using offsite sources
		0.01 per year	0.94	2.0E-03	0.05
6	8.10E-07	Internal fire initiating event	Probability that fire event is not suppressed or is not large enough to affect SFP function	Diesel fire protection pump fails to start and run	Failure to recover inventory using offsite sources
		9.0E-03 per year	0.05	0.18	0.01
7	7.20E-07	Loss of offsite power from plant centered & grid related events	Diesel fire protection pump fails to start and run	Failure to recover offsite power	Failure to recover inventory using offsite sources
		0.08 per year	0.18	1.0E-03	0.05
8	§.00E-07	Loss of inventory initiating event	Probability that loss is large	Operator fails to initiate makeup of inventory	Failure to recover inventory using offsite sources
		0.01 per year	0.06	0.01	0.1
9	5.60E-07	Tomado event leading to SFP failure			

# Table 9 - A Simplified Explanation of the Dominant Cutsets for Case 1

5.6E-07 per year

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10	4.70E-07	Loss of inventory initiating event	Probability that loss is small	SFP make-up pumps fails (hardware failure)	Both fire pumps fail (hardware failure)	Failure to recover inventory using offsite sources
		0.01 per year	0.06	0.01	0.01	0.05
11	2.82E-07	Loss of inventory initiating event	Probability that loss is small	Operator fails to respond to control room alarm	Operator fails to note condition during walkdown	
		0.01 per year	0.06	3.0E-03	0.01	
12	1.88E-07	Loss of inventory initiating event	Probability that loss is small	SFP level instrumentation fails due to local electrical faults	Operator fails to note condition during walkdown	
		0.01 per year	0.06	2.0E-03	0.01	
13	1.80E-07	Loss of inventory initiating event	Probability that loss is large	Operator fails to respond to control room alarm	Operator fails to note condition during walkdown	
		0.01 per year	0.94	3.0E-03	0.1	
14	1.51E-07	Loss of offsite power from plant centered & grid related events	Operator fails to re- start or re-align cooling system	Diesel fire protection pump fails to start and run	Electric fire pump fails to start and run	Failure to recover inventory using offsite sources
		0.08 per year	3.5E-03	0.18	0.06	0.05
15	1.40E-07	Loss of offsite power from plant centered & grid related events	Operator fails to re- start or re-align cooling system	Operator fails to start fire pumps	Failure to recover inventory using offsite sources	
		0.08 per year	3.5E-03	0.01	0.05	
16	1.20E-07	Loss of inventory initiating event	Probability that loss is large	SFP level instrumentation fails due to local electrical faults	Operator fails to note condition during walkdown	
		0.01 per year	0.94	2.0E-03	0.01	
17	1.13E-07	Loss of offsite power from plant centered & grid related events	Operator fails to re- start or re-align cooling system	Both fire pumps fail (hardware failure)	Failure to recover inventory using offsite sources	
		0.08 per year	3.5E-03	0.01	0.05	
18	9.00E-08	Loss of pool cooling initiating event	Operator fails to respond to control room alarm	Operator fails to note condition during walkdown		
		3.0E-03 per year	3.0E-03	0.01		

## Table 9 - A Simplified Explanation of the Dominant Cutsets for Case 1

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Figure 2a



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Figure 2b



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Figure 2c





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Figure 3b





Figure 49



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Figure 4b



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Figure 5 b



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Figure 5c



Figure ba

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Figure 6b



C Figure



Figure 7a



Figure 7b



Figure 7c

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# APPENDIX A

## Event Probabilities/Frequencies Used in the SFP Risk Analysis

EVENT NAME	DESCRIPTION	EVENT PROBABILITY	SOURCE/REFERENCE
FP-DGPUMP-FTF	Diesel powered fire pump fails to start and run	Cases 1,2,3: 1.8E-01	estimate based on event EPS-DGN- FC-1ARE in INEL-96/0334
FP-ELPUMP-FTF	Electric fire pump fails to start and run	Cases 1,2,3: 6.0E-02	estimate based on event FP- DGPUMP-FTF and on operating experience.
FP-MKUP-FTF	Failure to makeup inventory in SPF using either the electric or       Cases 1,2,3: 1.0E-02         diesel fire protection pumps       Cases 1,2,3: 1.0E-02		based on event SPF-MKUP-ALT-F in INEL-96/0334
HEP-ALTCL-E	Operator fails to establish alternate cooling (use of fire pumps) given a loss of "normal" SFP cooling - early indication from control room alarms. There is in excess of 120 hrs available in Cases 1and 3 and approximately 52 hrs available in Case 2. [Timing for Case 1 is based on time to bulk boiling of 27 hours and a boildown rate of 0.2ft/hr. Timing for Case 2 is based on time to bulk boiling of 12 hours and a boildown rate of 0.5ft/hr.]	Case 1: 1.0E-02	based on event ALT-XHE-XM-SFP in INEL-96/0334
		Case 2: 8.0E-02	based on event ALT-XHE-XM-SFPL in INEL-96/0334
		Case 3: N/A	fire pumps are assumed to be unavailable in Case 3
HEP-ALTCL-L	HEP-ALTCL-L Operator fails to establish alternate cooling (use of fire pumps) given a loss of "normal" SFP cooling - indication from		assume twice the probability for HEP- ALTCL-E
	walkdowns. Less time is available than in HEP-ALTCL-E since time will elapse for bulk pool boiling to begin and for pool level to decrease (to a level that will be obvious to the operator)	Case 2: 1.6E-01	assume twice the probability for HEP- ALTCL-E
		Case 3: N/A	fire pumps are assumed to be unavailable in Case 3

EVENT NAME	DESCRIPTION	EVENT PROBABILITY	SOURCE/REFERENCE
HEP-ALTCL-LP-E	Operator fails to establish alternate cooling (use of fire pumps) given a loss of offsite power. There is in excess of 120 hrs available in Cases 1 & 3 and approximately 52 hrs available in Case 2.	Case 1: 1.0E-02	based on event ALT-XHE-XM-SFPP in INEL-96/0334 this should be 3E-2. However, in a decommissioned plant, this HEP is more similar to event HEP-ALTCL-E. Therefore use 1E-2
		Case 2: 8.0E-02	similar to HEP-ALTCL-E
		Case 3: N/A	fire pumps are assumed to be unavailable in Case 3
HEP-COOL-LOC-E	Operator fails to restore cooling system given a loss of cooling event -early indication from control room alarms. There is in excess of 120 hrs available in Cases 1 & 3 and approximately 52 hrs available in Case 2. Mean time to repair is assumed to be 10 hours for Cases 1 & 3 and 40 hours for Case 2.	Case 1: 1.0E-04	assume probability of failure to repair = exp (-lambda * time available) = exp (-1/10 * 128) = 3E-6 (cap off at 1E-4)
		Case 2: 5.5E-03	probability of failure to repair = exp (-1/10 * 52) = 5.5E-3
		Case 3: 4.2E-02	probability of failure to repair = exp (-1/40 * 128) = 4.2E-2
HEP-COOL-LOC-L	Operator fails to restore cooling system given a loss of cooling event - indication from walkdowns. Less time is available than in HEP-ALTCL-E since time will elapse for bulk pool boiling to	Case 1: 2.2E-04	assume probability of failure to repair = exp (-lambda * time available) = exp (-1/10 * 84) = 2.2E-4
	begin and for pool level to decrease (to a level that will be obvious to the operator). Assume that it is the second shift (i.e., time to bulk boiling plus 16 hours) that recognizes the need for action. Therefore time available for Cases 1 & 3 is 84 hours and 24 hours for Case 2.	Case 2: 9.1E-02	probability of failure to repair = exp (-1/10 * 24) = 9.1E-2
		Case 3: 1.2E-01	probability of failure to repair = exp (-1/40 * 84) = 1.2E-1
HEP-COOL-LOP-E	Operator fails to restart/re-align cooling system given a loss of offsite power -early indication from control room alarms. There is in excess of 120 hrs available in Cases 1 & 3 and approximately 52 hrs available in Case 2.	Case 1: 3.5E-03	based on methodology provided in INEL-96/0334 for event SFP-XHE-XE- LP but for low stress, and for a response type action. See also event SFP-XHE-XE-PLR in INEL-96/0334

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EVENT NAME	DESCRIPTION	EVENT PROBABILITY	SOURCE/REFERENCE
		Case 2: 7.0E-03	Same as Case 1 except for less time and higher stress levels. The factor of 2 increase is consistent with INEL- 96/0334 methodology.
		Case 3: 1.8E-02	Factor of 5 higher than HEP-COOL- LOC-E to account for less operator training. The 5 times is consistent with INEL-96/0334 methodology.
HEP-INV-MKUP-E Operator fails to isolate a large inventory loss and initiate normal coolant makeup - early indication from control room alarms. From NUREG-1275 V12, the largest inventory loss		Case 1: 1.0E-02	based on events SFP-XHE-MANIOS- E (7E-3)and SFP-XHE-XE-LINVR (4E- 3) in INEL-96/0334
	resulted in a level drop of between 5 to 10 ft. In a foreign plant, an incident resulted in a level drop of 16'. Assume a drop of between 15 to 20ft leaving 5ft of water above the fuel assemblies. Therefore, time available for Case 1 is 36 hours and 15hrs for Case 2.	Case 2: 5.0E-02	Assume 5 times Case 1
		Case 3: 1.0E-01	based on event SFP-XHE-MANIOS-L (8E-2) in INEL-96/0334
HEP-INV-MKUP-L	Operator fails to isolate a large inventory loss and initiate	Case 1: 5.0E-02	assume 5 times HEP-INV-MKUP-E
	normal coolant makeup - indication from walkdowns. Less time is available than in HEP-INV-MKUP-E since the walkdown could take place as much as 8 hours later	Case 2: 1.0E-01	Estimate
		Case 3: 3.0E-01	Estimate
HEP-INV-MKUP-SML	Operator fails to initiate normal coolant makeupfor small leaks. There is in excess of 120 hrs available in Cases 1 & 3and approximately 50 hrs available in Case 2.	Case 1: 2.0E-03	based on event SFP-XHE-XE-LINVR in INEL-96/0334, but divide by 2 since there is less stress than in re-fueling situations
		Case 2: 2.0E-03	same as Case 1
		Case 3: 1.0E-02	a factor of 5 higher due to lack of guidance and operator training
HEP-RES-ALARM	Operator fails to respond given an alarm in the control room	Cases 1,2,3: 3.0E-03	DOE Savannah River report WSRC- TR-93-581, and NUREG-1278

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EVENT NAME	DESCRIPTION	EVENT PROBABILITY	SOURCE/REFERENCE
IE-AIRCRAFT-IMP	Frequency (per year) of an aircraft impact event causing damage to SFP integrity - this event is assumed to lead directly to fuel uncovery	Cases 1,2,3: 4.0E-08	Estimate based on DOE-STD-3014-96 and other studies (see Appendix 10I)
IE-CASK-DROP	Frequency (per year) of a cask drop event causing damage to SFP integrity - this event is assumed to lead directly to fuel uncovery. For this event, plant procedures for the moving of	Case 1: 2.5E-06	Estimate based on industrial data (NUREG-0612 and other studies - see Appendix 9)
	heavy loads is assumed to be present and followed.	Case 2: 2.5E-06	Estimate based on industrial data (NUREG-0612 and other studies - see Appendix 9)
		Case 3: 1.5E-05	Estimate based on industrial data (NUREG-0612 and other studies - see Appendix 9)
IE-INT-FIRE	Frequency (per year) for an internally initiated fire event - postulated plant conditions one year after shutdown	Case 1: 9.0E-03	Derived using methodology given in EPRI TR-100370s
		Case 2: 4.0E-02	Derived using methodology given in EPRI TR-100370s - postulated plant conditions one month after shutdown - welding and cutting operations are ongoing
		Case 3: 9.0E-03	Similar to Case 1
IE-LOOP-LP1	Initiating event frequency (per year) for loss of offsite power from plant centered and grid related events	Cases 1,2,3: 8.0E-02	INEL-96/0334 NUREG/CR-5496
IE-LOOP-LP2	Initiating event frequency (per year) for loss of offsite power event initiated by severe weather	Cases 1,2,3: 7.0E-03	NUREG/CR-5496
IE-LO-POOL-COOL	Initiating event frequency (per year) for loss of pool cooling events	Cases 1,2,3: 3.0E-03	NUREG-1275 Vol. 12
IE-LO-POOL-INV	Initiating event frequency (per year) for loss of pool inventory events	Cases 1,2,3: 1.0E-02	NUREG-1275 Vol. 12

	DESCRIPTION	EVENT PROBABILITY	SOURCE/REFERENCE
IE-SEISMIC	Frequency (per year) for a 0.4 to 0.5 g earthquake	Cases 1,2,3: 2.0E-05	Estimate based on information obtained from NUREG-1488
IE-TORNADO-MIS	Frequency (per year) of a tornado generated missile causing damage to SFP integrity - this event is assumed to lead directly to fuel uncovery	Cases 1,2,3: 5.6E-07	Estimate based on data from the National Climatic Data Center for F4 and F5 tornadoes. The potential loss of support systems from F3 tornadoes (approx. 1E-5 per year) is subsumed into the LP2 initiating event.
REC-FIRE-EVT	Probability that a fire event is sufficiently large to fail OSP cables or components of the SFP cooling pumps.	Case 1: 5.0E-02	Estimate. Manual suppression is assumed to be less likely since occupancy by plant personnel in the building is unlikely.
		Case 2: 1.0E-02	Estimate. Manual suppression is assumed to be possible since occupancy by plant personnel in the building is likely.
		Case 3: 1.0E-01	Estimate. Same as Case 1 except fire protection equipment and training is assumed to be less.
REC-INV-OFFSITE	Failure to recover inventory using offsite sources (e.g., fire engines) - time available in excess of 50 hours	5.0E-02	Estimate. Used in Cases 1,2&3 of LP1, LP2, and Seismic events where there is no pool failure. Also used in Cases 1&3 of small LOI
REC-INV-OFFSITE1	Failure to recover inventory using offsite sources (e.g., fire engines) -events where pool heatup is very slow	1.0E-02	Estimate. Used in Cases 1,2&3 of LOC and Fire.
REC-INV-OFFSITE2	Failure to recover inventory using offsite sources (e.g., fire engines) - time available is less than 36 hours	1.0E-01	Estimate. Used in Case 3 of LOC (w/o CR alarms), and Cases 1&3 of large LOI (with CR alarms)
REC-INV-OFFSITE3	Failure to recover inventory using offsite sources (e.g., fire engines) - time available in excess of 50 hours	2.0E-01	Estimate. Used in Cases 1&3 of large LOI (w/o CR alarms)

EVENT NAME	DESCRIPTION	EVENT PROBABILITY	SOURCE/REFERENCE
REC-OSP-PC	Probability of recovery of offsite power (from plant centered or grid related events)	Cases 1,2,3: 1.0E-03	Conservative probability based on methodology in NUREG/CR-5032
REC-OSP-SW	Probability of recovery of offsite power (from severe weather	Case 1: 2.0E-02	Figure B-19 of NUREG/CR-5496
	events)	Case 2: 1.0E-01	Figure B-19 of NUREG/CR-5496
		Case 3: 2.0E-02	Similar to Case 1
REC-WLKDWN-LOC	Operator fails to notice loss of cooling event during walkdowns.	Case 1: 1.0E-02	Similar to REC-WLKDWN-LOI-S
	Indications include pool steaming and low pool level.	Case 2: 1.0E-02	same as Case 1
		Case 3: 5.0E-02	same as Case 1, except walkdown requirements are less and operators are less experienced.
REC-WLKDWN-LOI-L	Operator fails to notice a relatively fast decreasing level in the SFP during walkdowns. Similar to REC-WLKDWN-LOI-S except time available is less, but observable signs are more obvious.	Case 1: 1.0E-01	Estimate based on REC-WLKDWN- LOI-S
		Case 2: 1.0E-01	same as Case 1
		Case 3: 2.0E-01	same as Case 1, except walkdown requirements are less and operators are less experienced.
REC-WLKDWN-LOI-S	Operator fails to notice a relatively slow decreasing level in the SFP during walkdowns. Indications include low level in pool, and water in sump or in unexpected locations. Time available is in excess of 50 hours.	Case 1: 1.0E-02	From DOE Savannah River report WSRC-TR-93-581 event "failure of visual inspection to observe abnormal characteristics"
		Case 2: 1.0E-02	same as Case 1
		Case 3: 5.0E-02	same as Case 1, except walkdown requirements are less and operators are less experienced.
SFP-REGMKUP-F	Regular SFP Makeup system fails	Cases 1,2,3: 1.0E-01	based on event SFP-MKUP-REG-F in INEL-96/0334

EVENT NAME	DESCRIPTION	EVENT PROBABILITY	SOURCE/REFERENCE
SPC-CKV-CCF-H	Common cause failure of fuel pool cooling heat exchanger discharge check valves to open/remain open	Cases 1,2,3: 1.9E-05	based on event SPC1-CKV-CF-2F in INEL-96/0334
SPC-CKV-CCF-M	Common cause failure of fuel pool cooling pump discharge check valves to open/remain open	Cases 1,2,3: 3.2E-05	based on event SPC1-CKV-CF-MP2F in INEL-96/0334
SPC-HTX-CCF	Common cause failure of both fuel pool heat exchangers	Cases 1,2,3: 1.9E-05	based on event SPC1-HTX-CF-2F in INEL-96/0334
SPC-HTX-FTR	SPF heat exchanger cooling system fails to operate	Cases 1,2,3: 2.4E-04	based on event SPC1-HTX-FC-COOL in INEL-96/0334
SPC-HTX-PLG	Plugging failure of the SPF heat exchanger - includes the heat exchanger and 2 manual valves	Cases 1,2,3: 2.2E-05	based on event SPC1-HTX-FC-1A in INEL-96/0334
SPC-LVL-LOF	Level channel - loss of function during standby	Case 1: 1.0E-05	NUREG-1740
		Case 2: 1.0E-05	similar to Case 1
		Case 3: 1.0E-01	estimated based on the assumption that availability of instrumentation is not required
SPC-LVL-LOP	Level channel - local electrical faults	Cases 1,2,3: 2.0E-03	Estimate based on information in NUREG-1275 Vol. 12
SPC-PMP-CCF	Common cause failure of fuel pool cooling pumps	Cases 1,2,3: 5.9E-04	based on event SPC1-MDP-CF-2F in INEL-96/0334
SPC-PMP-FTF-1	Spent Fuel Pool cooling pump 1 fails to start and run	Cases 1,2,3: 3.9E-03	based on event SPC1-MDP-FC-1A in INEL-96/0334
SPC-PMP-FTF-2	Spent Fuel Pool cooling pump 2 fails to start and run	Cases 1,2,3: 3.9E-03	based on event SPC1-MDP-FC-1A in INEL-96/0334

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### **Functional Assignments for the Event Trees**

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	Event	Equation	Fault Tree	Comments
	FOE	JE-EQE	SET E	colve at gate GFFT1A0, single event IE-SEISMIC
	FPI	SFP-INT	FFT-MISC	solve at gate GFFT140, single event SFP-INTEG-HCLPF
4.6	CSI	UNITY	FFT-MISC	solve at gate GFFT111, single event "TRUE" flag
	CSF	n/a		
	ocs	n/a		
	OFB	REC-OSS	FFT-REC	solve at gate GFFT110, single event REC-INV-OFFSITE

#### Table B-1 - Functional Assignments for the Seismic Event Tree

#### Table B-2 - Functional Assignments for the Internal Fire Event Tree

Event	Equation	Fault Tree	Comments
FIR	IE-FIR	FFT-IE	solve at gate GFFT142, single event IE-INT-FIRE
OSP	OSP-FIR	FFT-REC	solve at gate GFFT150, single event REC-FIRE-EVT
ОМК	OMK-DGFP	LOP-REC	solve at gate GLPR142 for Cases 1 & 2. For Case 3, use UNITY
OFD	REC-OSS1	FFT-REC	solve at gate GFFT111, single event REC-INV-OFFSITE1

Table B-3 - Functional Assignments for the Loss of Cooling Event Tree

Event	Equation	Fault Tree	Comments
LOC	IE-LOC	FFT-IE	solve at gate GFFT172, single event IE-LO-POOL-COOL
CRA	CR-ALARM	CR-ALARM	solve at gate GCRA112
IND	IND-LOC	FFT-REC	solve at gate GFFT130, single event REC-WLKDWN-LOC
ocs	OCSE-LOC	LOC-REC	solve at gate GLCR121
	OCSL-LOC	LOC-REC	solve at gate GLCR161
OFD	OFDE-LOC	LOC-REC	solve at gate GLCR123 for Cases 1 & 2. For Case 3, use UNITY
	OFDL-LOC	LOC-REC	solve at gate GLCR163 for Cases 1 & 2. For Case 3, use UNITY
OFB	REC-OSS1	FFT-REC	solve at gate GFFT111, single event REC-INV-OFFSITE1

**B-1** 

Event Equation Fault Tree			Comments						
LOI	IE-LOI	FFT-IE	solve at gate GFFT174, single event IE-LO-POOL-INV						
NLL	LOI-SML	FFT-MISC	solve at gate GFFT142, single event LOI-SMALL						
CRA	CR-ALARM	CR-ALARM	solve at gate GCRA112						
IND 👘	IND-LOIL FFT-REC solve at gate GFFT132, sin		solve at gate GFFT132, single event REC-WLKDWN-LOI-L						
	IND-LOIS	FFT-REC	solve at gate GFFT134, single event REC-WLKDWN-LOI-S						
OIS	OIS-E LOI-REC		solve at gate GLIR121						
	OIS-L	LOI-REC	solve at gate GLIR151						
OIL	OIMU	LOI-REC	solve at gate GLIR181						
ОМК	ОМК-Е	LOI-REC	solve at gate GLIR123 for Cases 1 & 2. For Case 3, use UNITY						
	OMK-L	LOI-REC	solve at gate GLIR153 for Cases 1 & 2. For Case 3, use UNITY						
	OMK-LOI	LOI-REC	solve at gate GLIR183 for Cases 1 & 2. For Case 3, use UNITY						
OFD	REC-OSS	FFT-REC	solve at gate GFFT110, single event REC-INV-OFFSITE						
	REC-OSS2	FFT-REC	solve at gate GFFT112, single event REC-INV-OFFSITE2						
	REC-OSS3	FFT-REC	solve at gate GFFT114, single event REC-INV-OFFSITE3						

Table B-4- Functional Assignments for the Loss of Inventory Event Tree

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Table B-5 - Functional Assignments for the Loss of Offsite Power (Plant Centered) Event Tree

Event	Equation	Fault Tree	Comments
LP1	IE-LP1	FFT-IE	solve at gate GFFT144, single event IE-LOOP-LP1
DG	DG-START	LOP-REC	solve at gate GLPR142 for Cases 1 & 2. For Case 3, use UNITY
OPR	REC-OSP1	FFT-REC	solve at gate GFFT170, single event REC-OSP-PC
ocs	OCSE-LOP	CS-REC	solve at gate GCSR112
омк	OMK-FPS	LOP-REC	solve at gate GLPR112 for Cases 1 & 2. For Case 3, use UNITY
	OMK-DGFP	LOP-REC	solve at gate GLPR142 for Cases 1 & 2. For Case 3, use UNITY
	OMK-EPFP	LOP-REC	solve at gate GLPR172 for Cases 1 & 2. For Case 3, use UNITY
OFD	REC-OSS	FFT-REC	solve at gate GFFT110, single event REC-INV-OFFSITE

# Table B.6 - Functional Assignments for the Loss of Offsite Power (Severe Weather) Event Tree

and an a state of the second	Comments	eenT Hus-T	Equation	Event
. 22	Solve at gate OFFT170, single event E-LOOP-LP2	<b>3-14</b>	E-Tb5	153
	Solve at gate GLPR142 for Cases 1 & 2. For Case 3, use UNITY	LOP-REC	DC-START	DC
Margin Activities	solve at gate GFFT172, single event REC-OSP-SW		KEC O265	SPPR *
	solve at gate GCSR112	CS-REC	OCSE-LOP	SOCS
	Solve at gate GLPR112 for Cases 1 & 2. For Case 3, use UNITY	LOP-REC	SATAMO	OWK
	solve at gate GLPR142 for Cases 1 & 2. For Case 3, use UNITY	LOP-REC	OWK-DGEb	
	solve at gate GLPR172 for Cases 1 & 2. For Case 3, use UNITY	LOP-REC	<b>OW</b> K-E6E6	
an a	solve at gate GFFT110, single event REC-INV-OFFSITE	FFT-REC	REC-055	OFD

 $2^{M_{\rm ext}} \sim 1^{M_{\rm ext}} \sim 1^{M_{\rm ext}}$ 

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