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Docket No. 50-410

DISTRIBUTION

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Dear Mr. Burkhardt:

SUBJECT: ISSUANCE OF AMENDMENT (TAC NO. 71926)

The Commission has issued the enclosed Amendment No. 12 to Facility Operating License No. NPF-69 for the Nine Mile Point Nuclear Station Unit No. 2 (NMP-2). The amendment consists of changes to the Technical Specifications in response to your application transmitted by letter dated January 13, 1989.

This amendment revises Technical Specifications Section 3/4.4.1, Recirculation System and the associated Bases, to differentiate the terms recirculation loop drive flow and jet pump flow as used in the Technical Specifications and to change two surveillance requirements for demonstrating jet-pump operability. This amendment will also incorporate final values for Reactor Coolant System flow parameters as determined from startup tests.

A copy of the related Safety Evaluation is enclosed. A Notice of Issuance will be included in the Commission's next regular bi-weekly Federal Register notice.

Sincerely,

ORIGINAL SIGNED BY:

Robert E. Martin, Senior Project Manager  
Project Directorate I-1  
Division of Reactor Projects - I/II  
Office of Nuclear Reactor Regulation

Enclosures:

1. Amendment No. 12 to NPF-69
2. Safety Evaluation

cc w/enclosures:  
See next page

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Niagara Mohawk Power Corporation

Nine Mile Point Nuclear Station  
Unit 2

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UNITED STATES  
NUCLEAR REGULATORY COMMISSION  
WASHINGTON, D. C. 20555

NIAGARA MOHAWK POWER CORPORATION

DOCKET NO. 50-410

NINE MILE POINT NUCLEAR STATION, UNIT 2

AMENDMENT TO FACILITY OPERATING LICENSE

Amendment No. 12  
License No. NPF-69

1. The Nuclear Regulatory Commission (the Commission) has found that:
  - A. The application for amendment by Niagara Mohawk Power Corporation (the licensee) dated January 13, 1989, complies with the standards and requirements of the Atomic Energy Act of 1954, as amended (the Act) and the Commission's rules and regulations set forth in 10 CFR Chapter I;
  - B. The facility will operate in conformity with the application, the provisions of the Act, and the rules and regulations of the Commission;
  - C. There is reasonable assurance (i) that the activities authorized by this amendment can be conducted without endangering the health and safety of the public, and (ii) that such activities will be conducted in compliance with the Commission's regulations;
  - D. The issuance of this amendment will not be inimical to the common defense and security or to the health and safety of the public; and
  - E. The issuance of this amendment is in accordance with 10 CFR Part 51 of the Commission's regulations and all applicable requirements have been satisfied.
2. Accordingly, the license is amended by changes to the Technical Specifications as indicated in the attachment to this license amendment, and paragraph 2.C.(2) of Facility Operating License No. NPF-69 is hereby amended to read as follows:

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(2) Technical Specifications and Environmental Protection Plan

The Technical Specifications contained in Appendix A and the Environmental Protection Plan contained in Appendix B, both of which are attached hereto, as revised through Amendment No. 12 are hereby incorporated into this license. Niagara Mohawk Power Corporation shall operate the facility in accordance with the Technical Specifications and the Environmental Protection Plan.

3. This license amendment is effective as of the date of its issuance.

FOR THE NUCLEAR REGULATORY COMMISSION



Robert A. Capra, Director  
Project Directorate I-1  
Division of Reactor Projects - I/II  
Office of Nuclear Reactor Regulation

Attachment:  
Changes to the Technical  
Specifications

Date of Issuance: November 30, 1989

ATTACHMENT TO LICENSE AMENDMENT

AMENDMENT NO. 12 TO FACILITY OPERATING LICENSE NO. NPF-69

DOCKET NO. 50-410

Revise Appendix A as follows:

Remove Pages

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Insert Pages

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B3/4 4-2

### 3/4.4 REACTOR COOLANT SYSTEM

#### 3/4.4.1 RECIRCULATION SYSTEM

##### RECIRCULATION LOOPS

##### LIMITING CONDITIONS FOR OPERATION

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3.4.1.1 Two reactor coolant system recirculation loops shall be in operation with:

- a. Total core flow greater than or equal to 45% of rated core flow, or
- b. THERMAL POWER within the unrestricted zone of Figure 3.4.1.1-1.

APPLICABILITY: OPERATIONAL CONDITIONS 1\* and 2\*.

##### ACTION:

- a. With one reactor coolant system recirculation loop not in operation:
  1. Within four hours:
    - a) Place the recirculation flow control system in the Loop Manual (Position Control) mode, and
    - b) Reduce THERMAL POWER to  $\leq 70\%$  of RATED THERMAL POWER, and,
    - c) Increase the MINIMUM CRITICAL POWER RATIO (MCPR) Safety Limit by 0.01 to 1.07 per Specification 2.1.2, and,
    - d) Reduce the Maximum Average Planar Linear Heat Generation Rate (MAPLHGR) limit to a value of 0.81 times the two recirculation loop operation limit per Specification 3.2.1, and,
    - e) Reduce the Average Power Range Monitor (APRM) Scram and Rod Block and Rod Block Monitor Trip Setpoints and Allowable Values to those applicable for single recirculation loop operation per Specifications 2.2.1, 3.2.2 and 3.3.6.
    - f) Reduce the volumetric drive flow rate of the operating recirculation loop to  $\leq 41,800^{**}$  gpm.

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\* See Special Test Exception 3.10.4.

\*\* This value represents the volumetric recirculation loop drive flow which produces 100% core flow at 100% THERMAL POWER.

## REACTOR COOLANT SYSTEM

### RECIRCULATION SYSTEM

#### RECIRCULATION LOOPS

#### LIMITING CONDITIONS FOR OPERATION (Continued)

- g) Perform Surveillance Requirement 4.4.1.1.2 if THERMAL POWER is  $\leq 30\%^*$  of RATED THERMAL POWER or the jet pump loop flow in the operating loop is  $\leq 50\%^*$  of rated jet pump loop flow.
2. The provisions of Specification 3.0.4 are not applicable.
  3. Otherwise be in at least HOT SHUTDOWN within the next 12 hours.
- b. With no reactor coolant system recirculation loops in operation, immediately initiate action to reduce THERMAL POWER such that it is not within the restricted zone of Figure 3.4.1.1-1 within two hours, and initiate measures to place the unit in at least STARTUP within six hours and in HOT SHUTDOWN within the next six hours.
- c. With one or two reactor coolant system recirculation loops in operation and total core flow less than 45% but greater than 39%\*\* of rated core flow and THERMAL POWER within the restricted zone of Figure 3.4.1.1-1:
1. Determine the APRM and LPRM\*\*\* noise levels per Specification 4.4.1.1.1:
    - a) At least once per eight hours, and
    - b) Within 30 minutes after the completion of a THERMAL POWER increase of at least 5% of RATED THERMAL POWER.
  2. With the APRM or LPRM\*\*\* neutron flux noise levels greater than three times their established baseline noise levels, within 15 minutes initiate corrective action to restore the noise levels within the required limits within two hours by increasing core flow or by reducing THERMAL POWER.
- d. With one or two reactor coolant system recirculation loops in operation and total core flow  $\leq 39\%^*$  and THERMAL POWER within the restricted zone of Figure 3.4.1.1-1, within 15 minutes initiate corrective action to reduce THERMAL POWER to within the unrestricted zone of Figure 3.4.1.1-1 or increase core flow to  $> 39\%^*$  within 4 hours.

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\* Final values were determined during Startup Testing based upon the actual THERMAL POWER and jet pump loop flow which will sweep the cold water from the vessel bottom head preventing stratification.

\*\* Core flow which is equivalent to minimum core flow for 2 recirculation pumps at high speed with minimum flow control valve position.

\*\*\* Detector levels A and C of one LPRM string per core octant plus detectors A and C of one LPRM string in the center of the core should be monitored.

## REACTOR COOLANT SYSTEM

### RECIRCULATION SYSTEM

#### RECIRCULATION LOOPS

#### SURVEILLANCE REQUIREMENTS

4.4.1.1.1 With one reactor coolant system recirculation loop not in operation, at least once per 12 hours verify that:

- a. Reactor THERMAL POWER is  $\leq 70\%$  of RATED THERMAL POWER,
- b. The recirculation flow control system is in the Loop Manual (Position Control) mode,
- c. The volumetric drive flow rate of the operating loop is  $\leq 41,800$  gpm,\* and
- d. Core flow is  $> 39\%^{**}$  when THERMAL POWER is within the restricted zone of Figure 3.4.1.1-1.

4.4.1.1.2 With one reactor coolant system recirculation loop not in operation, within no more than 15 minutes prior to either THERMAL POWER increase or jet pump loop flow increase, verify that the following differential temperature requirements are met if THERMAL POWER is  $\leq 30\%^{***}$  of RATED THERMAL POWER or the recirculation jet pump loop flow in the operating recirculation loop is  $\leq 50\%^{***}$  of rated jet pump loop flow:

- a.  $\leq 145^{\circ}\text{F}$  between reactor vessel steam space coolant and bottom head drain line coolant,
- b.  $\leq 50^{\circ}\text{F}$  between the reactor coolant within the loop not in operation and the coolant in the reactor pressure vessel, and
- c.  $\leq 50^{\circ}\text{F}$  between the reactor coolant within the loop not in operation and the operating loop.

The differential temperature requirements of Specification 4.4.1.1.2 b. and c. do not apply when the loop not in operation is isolated from the reactor pressure vessel.

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- \* This value represents the volumetric recirculation loop drive flow which produces 100% core flow at 100% THERMAL POWER.
- \*\* Core flow which is equivalent to minimum core flow for 2 recirculation pumps at high speed with minimum flow control valve position.
- \*\*\* Final values were determined during Startup Testing based upon the actual THERMAL POWER and jet pump loop flow which will sweep the cold water from the vessel bottom head preventing stratification.

## REACTOR COOLANT SYSTEM

### RECIRCULATION SYSTEM

#### JET PUMPS

#### LIMITING CONDITIONS FOR OPERATION

3.4.1.2 All jet pumps shall be OPERABLE.

APPLICABILITY: OPERATIONAL CONDITIONS 1 and 2.

#### ACTION:

With one or more jet pumps inoperable, be in at least HOT SHUTDOWN within 12 hours.

#### SURVEILLANCE REQUIREMENTS

4.4.1.2 All jet pumps shall be demonstrated operable as follows:

- a. Each of the above required jet pumps shall be demonstrated OPERABLE within 24 hours after THERMAL POWER exceeds 25% of RATED THERMAL POWER and at least once per 24 hours while greater than 25% of RATED THERMAL POWER, by determining jet pump loop flow, recirculation loop drive flow, flow control valve position, and diffuser-to-lower plenum differential pressure for each jet pump and verifying that no two of the following conditions occur when both recirculation jet pump loop indicated flows are in compliance with Specification 3.4.1.3.
  1. The indicated jet pump loop flow differs by more than 10% from the established\* flow control valve position-jet pump loop flow characteristics.
  2. The indicated jet pump loop flow differs by more than 10% from the established\* jet pump loop flow-recirculation loop drive flow characteristic for the loop.
  3. The indicated diffuser-to-lower plenum differential pressure of any individual jet pump differs from established\* patterns by more than 20%.
- b. During single recirculation loop operation, each of the jet pumps in the operating loop shall be demonstrated OPERABLE within 24 hours after THERMAL POWER exceeds 25% of RATED THERMAL POWER and at least once per 24 hours while greater than 25% of RATED THERMAL POWER, by determining jet pump loop flow, recirculation loop drive flow, flow control valve position, and diffuser-to-lower plenum differential pressure for each jet pump and verifying that no two of the following conditions occur:
  1. The indicated jet pump loop flow in the operating loop differs by more than 10% from the established\* single recirculation loop control valve position-loop flow characteristics.
  2. The indicated jet pump loop flow differs by more than 10% from the established\* jet pump loop flow-recirculation loop drive flow characteristic for the operating loop.

\* Determined during the startup test program.

REACTOR COOLANT SYSTEM

RECIRCULATION SYSTEM

JET PUMPS

SURVEILLANCE REQUIREMENTS (Continued)

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3. The indicated diffuser-to-lower plenum differential pressure of any individual jet pump differs from established\* single recirculation loop patterns by more than 20%.
- c. The provisions of Specification 4.0.4 are not applicable provided that this surveillance is performed within 24 hours after exceeding 25% of RATED THERMAL POWER.

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\* Determined during the startup test program.

REACTOR COOLANT SYSTEM

RECIRCULATION SYSTEM

RECIRCULATION LOOP FLOW

LIMITING CONDITIONS FOR OPERATION

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3.4.1.3 Jet pump loop flow mismatch shall be maintained within:

- a. 5% of rated core flow with effective core flow\* greater than or equal to 70% of rated core flow.
- b. 10% of rated core flow with effective core flow\* less than 70% of rated core flow.

APPLICABILITY: OPERATIONAL CONDITIONS 1 and 2 during two recirculation loop operation.\*\*

ACTION:

With the jet pump loop flows different by more than the specified limits, either:

- a. Restore the jet pump loop flows to within the specified limit within 2 hours, or
- b. Shut down one of the recirculation loops and take the ACTION required by Specification 3.4.1.1.

SURVEILLANCE REQUIREMENTS

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4.4.1.3 Jet pump loop flow mismatch shall be verified to be within the limits at least once per 24 hours.

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\* Effective core flow shall be the core flow that would result if both jet pump loop flows were assumed to be at the smaller value of the two jet pump loop flows.

\*\* See Special Test Exception 3.10.4.

## REACTOR COOLANT SYSTEM

### RECIRCULATION SYSTEM

#### IDLE RECIRCULATION LOOP STARTUP

#### LIMITING CONDITIONS FOR OPERATION

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3.4.1.4 An idle recirculation loop shall not be started unless the temperature differential between the reactor pressure vessel steam space coolant and the bottom head drain line coolant is less than or equal to 145°F, and:

- a. When both loops have been idle, unless the temperature differential between the reactor coolant within the idle loop to be started up and the coolant in the reactor pressure vessel is less than or equal to 50°F, or
- b. When only one loop has been idle, unless the temperature differential between the reactor coolant within the idle and operating recirculation loops is less than or equal to 50°F and the operating jet pump loop flow is less than or equal to 50% of rated jet pump loop flow.

APPLICABILITY: OPERATIONAL CONDITIONS 1, 2, 3 and 4.

#### ACTION:

With temperature differences and/or jet pump loop flow rates exceeding the above limits, suspend startup of any idle recirculation loop.

#### SURVEILLANCE REQUIREMENTS

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4.4.1.4 The temperature differentials and jet pump loop flow rate shall be determined to be within the limits within 15 minutes before startup of an idle recirculation loop.

## 3/4.4 REACTOR COOLANT SYSTEM

### BASES

#### 3/4.4.1 RECIRCULATION SYSTEM

The impact of single recirculation loop operation upon plant safety is assessed and shows that single-loop operation is permitted if the MCPR fuel cladding safety limit is increased as noted by Specification 2.1.2, APRM scram and control rod block setpoints are adjusted as noted in Tables 2.2.1-1 and 3.3.6-2, respectively, MAPLHGR limits are decreased by the factor given in Specification 3.2.1, and MCPR operating limits are adjusted per Section 3/4.2.3.

Additionally, surveillance on the volumetric drive flow rate of the operating recirculation loop is imposed to exclude the possibility of excessive core internals vibration. Drive flow is the flow rate for the recirculation pump in the operating loop. The surveillance on differential temperatures below 30% THERMAL POWER or 50% rated jet pump loop flow is to mitigate the undue thermal stress on vessel nozzles, recirculation pump and vessel bottom head during the extended operation of the single recirculation loop mode. Jet pump loop flow is the sum of the flows through the 10 jet pumps in one loop. Core flow is the sum of the two jet pump loop flows.

The objective of GE BWR plant and fuel design is to provide stable operation with margin over the normal operating domain. However, at the high-power/low-flow corner of the operating domain, a small probability of limit cycle neutron flux oscillations exists, depending on combinations of operating conditions (e.g., rod pattern, power shape). To provide assurance that neutron flux limit cycle oscillations are detected and suppressed, APRM and LPRM neutron flux noise levels should be monitored while operating in this region.

Stability tests at operating BWRs were reviewed to determine a generic region of the power/flow map in which surveillance of neutron flux noise levels should be performed. A conservative decay ratio of 0.6 was chosen as the basis for determining the generic region for surveillance to account for the plant-to-plant variability of decay ratio with core and fuel designs. This generic region has been determined to correspond to a core flow of less than or equal to 45% of rated core flow and a THERMAL POWER greater than that specified in Figure 3.4.1.1-1.

Plant-specific calculations can be performed to determine an applicable region for monitoring neutron flux noise levels. In this case, the degree of conservatism can be reduced since plant-to-plant variability would be eliminated. In this case, adequate margin will be assured by monitoring the region which has a decay ratio greater than or equal to 0.8.

Neutron flux noise limits are also established to ensure early detection of limit cycle neutron flux oscillations. BWR cores typically operate with neutron flux noise caused by random boiling and flow noise. Typical neutron

## REACTOR COOLANT SYSTEM

### BASES

#### RECIRCULATION SYSTEM

##### 3/4.4.1 (continued)

flux noise levels between 1% and 12% of rated power (peak-to-peak) have been reported for the range of low to high recirculation loop flow during both single and dual recirculation loop operation. Neutron flux noise levels which significantly bound these values are considered in the thermal/mechanical design of GE BWR fuel and are found to be of negligible consequence. In addition, stability tests at operating BWRs have demonstrated that when stability-related neutron flux limit cycle oscillations occur, they result in peak-to-peak neutron flux limit cycles of 5 to 10 times the typical values. Therefore, actions taken to reduce neutron flux noise levels exceeding three times the typical value are sufficient to ensure early detection of limit cycle neutron flux oscillations.

Typically, neutron flux noise levels show a gradual increase in absolute magnitude as core flow is increased (constant control rod pattern) with two reactor recirculation loops in operation. Therefore, the baseline neutron flux noise level obtained at a specified core flow can be applied over a range of core flows. To maintain a reasonable variation between the low-flow and high-flow end of the flow range, the range over which a specific baseline is applied should not exceed 20% of rated core flow with two recirculation loops in operation. Data from tests and operating plants indicate that a range of 20% of rated core flow will result in approximately a 50% increase in neutron flux noise level during operation with two recirculation loops. Baseline data should be taken near the maximum rod line at which the majority of operation will occur. However, baseline data taken at lower rod lines (i.e., lower power) will result in a conservative value since the neutron flux noise level is proportional to the power level at a given core flow.

An inoperable jet pump is not, in itself, a sufficient reason to declare a recirculation loop inoperable, but it does, in case of a design-basis accident, increase the blowdown area and reduce the capability of reflooding the core; thus, the requirement for shutting down the facility when a jet pump is inoperable. Jet pump failure can be detected by monitoring jet pump performance on a prescribed schedule for significant degradation.

Jet pump loop flow mismatch limits are in compliance with the ECCS LOCA analysis design criteria for two recirculation loop operation. The limits will ensure an adequate core flow coastdown from either recirculation loop after a LOCA. In the case where the mismatch limits cannot be maintained during two loop operation, continued operation is permitted in a single recirculation loop mode.

In order to prevent undue stress on the vessel nozzles and bottom head region, the recirculation loop temperatures shall be within 50°F of each other before startup of an idle loop. The loop temperature must also be within 50°F of the reactor pressure vessel coolant temperature to prevent thermal shock to the



UNITED STATES  
NUCLEAR REGULATORY COMMISSION  
WASHINGTON, D. C. 20555

SAFETY EVALUATION BY THE OFFICE OF NUCLEAR REACTOR REGULATION

RELATED TO AMENDMENT NO. 12 TO FACILITY OPERATING LICENSE NO. NPF-69

NIAGARA MOHAWK POWER CORPORATION

NINE MILE POINT NUCLEAR POWER STATION, UNIT NO. 2

DOCKET NO. 50-410

1.0 INTRODUCTION

The licensee, Niagara Mohawk Power Corporation (NMPC), in its letter of January 13, 1989, requested a revision to the technical specifications (TS) for Nine Mile Point Unit 2 (NMP-2). The proposed amendment relates to TS Section 3/4.4 reactor coolant system.

2.0 DISCUSSION

As stated in the licensee's application, the recirculation system consists of two parallel external loops, each containing a recirculation pump and motor, suction and discharge block valves, flow control valve, and the connecting piping to the reactor vessel. Each external recirculation loop takes suction from the vessel downcomer annulus via the recirculation pump and delivers drive flow to multiple nozzles on the vessel shell from which internal piping conducts the flow to the jet pump inlets. This driving flow will cause the jet pumps to pump additional water from the vessel annulus. The combined flow will then pass through the reactor core.

Section 4.4.1.2 provides the surveillance requirements for demonstrating that all jet pumps are operable. Verification of jet pump operability is required to verify that operation is consistent with the licensing basis. In order to determine jet pump operability, it is necessary to perform certain performance measurements, compare these measurements against established nominal data, and look for a deviation from nominal as an indication of a potential problem. These performance measurements (Surveillance Requirements) are designed to detect the significant degradation in jet pump performance that would precede failure.

Surveillance Requirements 4.4.1.2.a.2 and 4.4.1.2.b.2 compare indicated total core flow against established core flow derived from recirculation loop drive flow measurements, with a differential of 10% or greater being unacceptable. This performance measurement has been determined by General Electric testing (Service Information Letter No. 330, dated June 9, 1980) to be relatively insensitive to jet pump degradation. This Technical Specification amendment revises the requirement so that it now compares

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indicated jet pump loop flow to the established jet pump loop flow-recirculation pump drive flow characteristic with a differential of 10% or greater being unacceptable. Surveillance Requirements 4.4.1.2.a.2 applies this criterion to both loops while in two-loop operation, and 4.4.1.2.b.2 applies the criterion to the operating loop while in single recirculation loop operation.

Surveillance Requirements 4.4.1.2.a.3 and 4.4.1.2.b.3 compare the indicated diffuser-to-lower plenum differential pressure of any individual jet pump to established patterns with a differential of 10% being unacceptable. The 10% allowable differential currently in the Technical Specifications is incorrect and is not in conformance with the guidelines of General Electric Service Information Letter No. 330. The Service Information Letter recommends that an allowable differential of 20% be used when comparing individual jet pump diffuser differential pressure to established normal patterns. Continued use of the 10% differential figure could provide incorrect evidence of jet pump degradation resulting in an unwarranted shutdown, thus having a negative impact on plant availability and capacity factor.

The proposed TS changes differentiate the terms recirculation loop drive flow and jet pump flow as used in the TS. The term recirculation loop flow has been used throughout the TS to identify both recirculation loop drive flow and jet pump loop flow. The dual use of the term has caused operator confusion.

In the recirculation system TS many design parameters were included as preliminary value which were to be finalized after the start-up tests. The start-up tests are now completed and hence the preliminary values have been changed to the values derived from the start-up tests.

### 3.0 EVALUATION

The staff's evaluation of the specific changes follows.

#### TS 3.4.1.1.a.1.t and 4.4.1.1.1.1.C

The recirculation loop drive flow for 100% core flow at 100% thermal power is given as 41,000 GPM as a design estimate for 2-loop operation. Start-up tests have determined the loop drive flow to be 41,800 GPM. An analysis, using start-up test data, has shown no internal flow induced vibration at loop drive flow less than 45,000 GPM. The maximum recirculation loop drive flow change to 41,800 GPM is acceptable.

The note "the actual value will be established during the start-up test program" is no longer applicable since the tests are already completed. The proposed change to delete the note is acceptable.

The term "recirculation loop flow" is changed to "recirculation loop drive flow" for more clarity. This is acceptable.

TS 3.4.1.1.a.1.g

The term "recirculation loop flow" is changed to "jet pump loop flow" to indicate the surveillance for single loop operation. The jet pump loop flow measurement is indicative of the core flow under these conditions. Hence, it is more applicable and therefore acceptable.

The notes are changed to indicate that the values are derived from the start-up tests. This is acceptable.

TS 4.4.1.2

The licensee proposes replacing the current surveillance requirement for jet pump operability, which is based on established recirculation loop flow, and total core flow with another criterion recommended in SIL 330-1 based on jet pump loop flow. Since this is reported to be a more effective indicator of jet pump performance, we find this proposed change acceptable.

The proposed change to the specified acceptable deviation from patterns established for individual jet pump diffuser to lower plenum differential pressure from 10% to 20% is consistent with the recommendation of both NUREG/CR-3052 and SIL 330 which established 20% as an acceptable indication of jet pump operability. Thus, the TS changes in Sections 4.4.1.2.a.(3) and 4.4.1.2.b.(3) are acceptable.

TS 3.4.1.3. and 3.4.1.4

The term "recirculation loop flow" is changed to "jet pump loop flow" for more clarity. This is acceptable.

TS 3/4.4.1

The Bases is revised to define the recirculation drive flow and the jet pump flow. This is acceptable.

4.0 SUMMARY

The staff has reviewed the proposed technical specifications changes for NMP-2 to modify the surveillance requirements for determination of jet pump operability and other changes. We have determined that the proposed changes will assure improved surveillance of jet pump operability based on methods previously approved by the staff, and are therefore acceptable. The clarification of terminology in regard to recirculation loop drive flow and jet pump flow will reduce the chances of misinterpretation of TS requirements.

ENVIRONMENTAL CONSIDERATION

This amendment involves a change in the installation or use of the facility components located within the restricted areas as defined in 10 CFR 20 and changes to the surveillance requirements. The staff has determined that this amendment involves no significant increase in the amounts, and no significant change in the types, of any effluents that may be released offsite and that there is no significant increase in individual or cumulative occupational radiation exposure. The Commission has previously issued a proposed finding that this amendment involves no significant hazards consideration and there has been no public comment on such finding. Accordingly, this amendment meets the eligibility criteria for categorical exclusion set forth in 10 CFR Sec 51.22(c)(9). Pursuant to 10 CFR 51.22(b) no environmental impact statement or environmental assessment need be prepared in connection with the issuance of this amendment.

CONCLUSION

We have concluded, based on the considerations discussed above, that: (1) there is reasonable assurance that the health and safety of the public will not be endangered by operation in the proposed manner, and (2) such activities will be conducted in compliance with the Commission's regulations and the issuance of these amendments will not be inimical to the common defense and security or to the health and safety of the public.

Dated: November 30, 1989

PRINCIPAL CONTRIBUTOR:

G. Thomas