



Entergy Operations, Inc.
1448 S.R. 333
Russellville, AR 72802
Tel 501 858 5000

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Subject: Arkansas Nuclear One - Unit 2
Docket No. 50-368
License No. NPF-6
2000 Annual Report of Steam Generator Tubing Inservice Inspections

Gentlemen:

Arkansas Nuclear One, Unit 2 (ANO-2) Technical Specifications 4.4.5.5.b and 6.9.1.5.b require that results of ANO-2 steam generator (SG) tubing inservice inspections performed during the report period be submitted to the NRC on an annual basis. Attached is the Steam Generator Tubing Inservice Inspection Report which presents the results from ANO-2's scheduled mid-cycle outage (2P00) and refueling outage (2R14) inspections. These inspections were conducted during July and September 2000.

The 2P00 inspections performed on both SGs involved a 100% full-length bobbin coil examination, with the exception of the tube area below the sleeves. The RPC used consists of a 0.115-inch pancake coil with both axially oriented and circumferentially oriented coils. The RPC was also utilized for confirmation of bobbin coil indications.

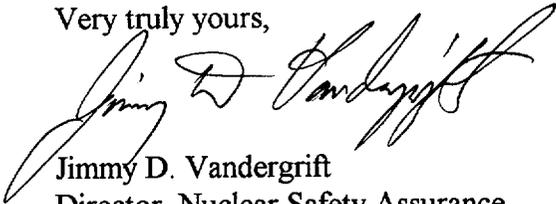
The 2R14 inspection was the baseline examination for the replacement steam generators (pre-service inspection). A 100% bobbin examination was performed on both generators in August just prior to the start of the outage. This was performed onsite. The plus point coil was used for diagnostic testing of bobbin indications.

This submittal completes the reporting requirements of ANO-2 Technical Specifications 4.4.5.5.b and 6.9.1.5.b for 2000. The attachment also provides the information designated by NEI 97-06 "Steam Generator Program Guidelines" to be included in the report to be submitted 12 months after each inservice inspection. This submittal contains no commitments.

Should you have any questions regarding this issue, please contact me.

ADD1

Very truly yours,



Jimmy D. Vandergrift
Director, Nuclear Safety Assurance

JDV/fpv
attachment

cc: Mr. Ellis W. Merschoff
Regional Administrator
U. S. Nuclear Regulatory Commission
Region IV
611 Ryan Plaza Drive, Suite 400
Arlington, TX 76011-8064

NRC Senior Resident Inspector
Arkansas Nuclear One
P.O. Box 310
London, AR 72847

Mr. Thomas W. Alexion
NRR Project Manager Region IV/ANO-2
U. S. Nuclear Regulatory Commission
NRR Mail Stop 04-D-03
One White Flint North
11555 Rockville Pike
Rockville, MD 20852

ARKANSAS NUCLEAR ONE, UNIT 2 STEAM GENERATOR TUBING INSERVICE INSPECTION ANNUAL REPORT

1 INTRODUCTION

Arkansas Nuclear One, Unit 2 (ANO-2) Technical Specification (TS) 4.4.5.5.b requires Entergy Operations to submit an annual report to the NRC that outlines the details of the steam generator (SG) tubing inservice inspections that were performed during the reporting period. The report shall include:

1. Number and extent of tubes inspected.
2. Location and percent of wall-thickness penetration for each indication of an imperfection.
3. Identification of tubes plugged or sleeved.

In addition to the above information, the 12-month report specified in NEI 97-06, "Steam Generator Program Guidelines" requires the following:

1. Scope of inspection performed.
2. Active degradation mechanisms found.
3. NDE techniques utilized for each degradation mechanism.
4. Number of tubes plugged or repaired during the inspection outage for each active degradation mechanism. Repair methods utilized and the number of tubes repaired by each repair method.
5. Total number and percentage of tubes plugged and/or repaired to date and the effective plugging percentage in each steam generator.
6. Description of tube integrity assessment.
7. Description of corrective actions implemented, if any.
8. Evaluation of circumstances if condition monitoring results exceeded the previous cycle operational assessment.

This report is formatted to reflect the information listed above for the NEI annual report. Since item #2 from the TS requirements (location and percent of wall-thickness

penetration for each indication of an imperfection) is not included in the NEI format, it will be discussed after item #8. The information requested by items #1 and #3 from the Technical Specifications report are subsumed within the NEI 97-06 report items.

The operating period for this report includes two outages, a tri-cycle inspection (2P00) in July 2000 and the baseline inspection of the replacement steam generators in September 2000.

2 DESIGN

The previous ANO-2 generators were of a Combustion Engineering (CE) Model 2815 design that began operation in December 1978. The plant had two recirculating SGs, each having 8411 high temperature mill annealed Inconel Alloy 600 tubes with a 0.75" outer diameter and a 0.048" wall thickness. The tubes were full depth explosively expanded into the tubesheet. The tube supports in the lower part of the SG were of an eggcrate (EC) type which consisted of an array of intersecting one inch wide and two inch wide flat carbon steel plates at each support elevation. There were seven full EC support plates, two partial EC support plates, two partial drilled support plates, and five strap supports called batwings (BW) for the horizontal run of the tubing. The BW supports consisted of two diagonal and three vertical straps. Two tube sleeve types, Babcock & Wilcox (B&W) kinetic and CE tungsten inert gas (TIG) welded, were installed in the SGs.

The replacement generators are Westinghouse (W) Model Delta 109's. They consist of Inconel 690 thermally treated tubing that is 11/16" in diameter with a 0.040" wall thickness. The tubes are expanded full depth hydraulically in the tubesheet. The tube supports are constructed of stainless steel and are a broached trifoil hole design. The upper bundle supports consist of ten stainless steel anti-vibration bars (AVB's).

3 2P00 OUTAGE RESULTS

3.1 2P00 Scope

The purpose of the 2P00 outage was to validate that the tubing was capable of meeting its intended structural integrity requirements. The tubing was tested from the tube end hot (TEH) to the 07Hot support structure. Table 3.1 lists the inspection scope of 2P00.

**Table 3.1
2P00 Inspection Scope**

SG "A"

| <u>Examination Type</u> | <u>Inspections Conducted</u> | <u>% Scope</u> | <u>Expansion Req'd</u> |
|--------------------------------|-------------------------------------|-----------------------|-------------------------------|
| Bobbin | 6924 | 100 | N/A |
| Special Interest | 492 | N/A | N/A |

SG "B"

| <u>Examination Type</u> | <u>Inspections Conducted</u> | <u>% Scope</u> | <u>Expansion Req'd</u> |
|--------------------------------|-------------------------------------|-----------------------|-------------------------------|
| Bobbin | 6951 | 100 | N/A |
| Special Interest | 376 | N/A | N/A |

3.2 Degradation Mechanisms Found

Table 3.2 outlines the number of indications found during the outage for each location. The active damage mechanism is outside diameter stress corrosion cracking (ODSCC).

**Table 3.2
2P00 Inspection Results**

| <u>Location</u> | <u>SG "A"</u> | <u>SG "B"</u> |
|------------------------------------|----------------------|----------------------|
| Sludge Pile (axial and volumetric) | 0 | 0 |
| EC Support Plate (axial) | 64 | 148 |
| Free Span (axial) | 0 | 0 |

3.3 NDE Techniques Utilized

Table 3.3 identifies the non-destructive examination (NDE) technique used for each location:

**Table 3.3
2P00 NDE Techniques**

| <u>Location</u> | <u>NDE Technique</u> |
|------------------------|--|
| Sludge Pile | 0.600" bobbin with 0.115" pancake for confirmation |
| EC Support Plate | 0.600" bobbin with 0.115" pancake for confirmation |
| Free Span | 0.600" bobbin with 0.115" pancake for confirmation |

3.4 Number of Tubes Plugged or Repaired by Damage Mechanism

There were no sleeves installed during 2P00. Mechanical-rolled plugs were used for all repairs. This consisted of 58 tubes in SGA and 131 in SGB. Some tubes had multiple indications. All repairs were made due to eggcrate indications.

3.5 Number and Percent Plugged and Sleeved Following 2P00

The number of tubes plugged and inservice sleeves following 2P00 are shown in Table 3.5.

Table 3.5
Cumulative Plugs and Sleeves in Service

| | SG "A" | SG "B" |
|------------------|----------|----------|
| B&W Sleeves | 283 | 47 |
| CE TIG Sleeves | 371 | 146 |
| Plugs | 1547 | 1591 |
| Equivalent Plugs | 1571.154 | 1597.998 |
| Percent Plugged | 18.68 % | 18.99 % |

3.6 Description of Tube Integrity Assessment

The tube integrity is based on two assessments. The methodologies are condition monitoring during the outage and the operational assessment performed following the outage to evaluate the acceptable runtime following the outage. Condition monitoring was performed to evaluate both leakage and tube integrity and was submitted in Entergy letter 2CAN090004 dated September 14, 2000. The condition monitoring performance criteria were met. The operational assessment was also submitted in the same document. The operational assessment was performed using deterministic methods for the identified damage mechanism and justified operation until the next scheduled outage, which was 2R14 in September of 2000.

3.7 Description of Corrective Actions

There were no corrective actions taken since all tests met the specified criteria.

3.8 Evaluation of Exceeding Condition Monitoring

Not applicable since all conditions were met.

3.9 Item #2 of the Technical Specification (location and percent of wall-thickness penetration for each indication of an imperfection)

This topic is addressed for the 2P00 outage in Tables 1 and 2 for SG “A” and SG “B”, respectively at the end of this report.

4 2R14 BASELINE RESULTS

The replacement steam generators were installed during the 14th refueling outage (2R14). The pre-service inspection was performed on the generators while they were horizontal on site just prior to installation.

4.1 2R14 Baseline Scope

Table 4.1 lists the inspection scope of 2R14.

**Table 4.1
2R14 Baseline Inspection Scope**

| <u>SG “A”</u> | | | |
|--------------------------------|-------------------------------------|-----------------------|-------------------------------|
| <u>Examination Type</u> | <u>Inspections Conducted</u> | <u>% Scope</u> | <u>Expansion Req'd</u> |
| Bobbin | 10637 | 100 | No |
| RPC of MBM's | 33 | 20 | N/A |
| RPC of Dents* | 95 | 20 | N/A |
| Special Interest | 3 | N/A | N/A |

| <u>SG “B”</u> | | | |
|--------------------------------|-------------------------------------|-----------------------|-------------------------------|
| <u>Examination Type</u> | <u>Inspections Conducted</u> | <u>% Scope</u> | <u>Expansion Req'd</u> |
| Bobbin | 10636 | 100 | No |
| RPC of MBM's | 63 | 20 | N/A |
| RPC of Dents* | 80 | 20 | N/A |
| Special Interest | 3 | N/A | N/A |

* Testing performed on dents > 7.00 volts

4.2 Degradation Mechanisms Found

Table 4.2 outlines the number of indications found during the outage for each location. There are no active damage mechanisms in the replacement steam generators.

Table 4.2
2R14 Baseline Inspection Results (indications)

| <u>Location</u> | <u>SG "A"</u> | <u>SG "B"</u> |
|-----------------|---------------|---------------|
| Dents | 1738 | 871 |
| MBMs | 156 | 314 |

4.3 NDE Techniques Utilized

Table 4.3 identifies the NDE technique used for each degradation mechanism:

Table 4.3
2R14 NDE Techniques

| Degradation Mechanism | NDE Technique |
|------------------------------|--|
| Bobbin | 0.560" bobbin coil |
| RPC | 0.560" plus point with 0.115 pancake and 0.080 pancake coils |

4.4 Number of Tubes Plugged or Repaired by Damage Mechanism

No sleeves were installed during 2R14. There were no Mechanical-rolled plugs installed. There was one welded I-690 plug installed in SGB in tube R23C8 during fabrication.

4.5 Number and Percent Plugged Following 2R14

The number of tubes plugged following 2R14 are shown in Table 4.5:

Table 4.5
Cumulative Tubes Plugged

| | SG "A" | SG "B" |
|------------------|---------------|---------------|
| Plugs | 0 | 1 |
| Equivalent Plugs | 0.000 | 1.000 |
| Percent Plugged | 0.0000% | 0.0094 % |

4.6 Description of Tube Integrity Assessment

All condition monitoring performance criteria were met during the outage. This conclusion is based on the fact that there were no crack-like indications identified. The amount of denting was not significant enough to perform in-situ testing. All tubing is expected to meet the integrity requirements specified by the performance criteria in NEI 97-06.

4.7 Description of Corrective Actions

There were no corrective actions taken since all tests met the specified criteria.

4.8 Evaluation of Exceeding Condition Monitoring

There were no performance criteria exceeded during 2R14 baseline inspection.

4.9 Item #2 of the Technical Specification (location and percent of wall-thickness penetration for each indication of an imperfection)

There were no tubes identified with percent through wall imperfections.

TABLE 1
SG "A" REPAIR INDICATION LIST FOR 2P00

| No. | Row | Line | Indication | Location | | Reason for Repair |
|-----|-----|------|------------|----------|-------|-------------------|
| 1 | 1 | 145 | SAI | 01H | -0.18 | EC Axial |
| 2 | 3 | 31 | SAI | 05H | -0.35 | EC Axial |
| 3 | 3 | 45 | SAI | 01H | +0.63 | EC Axial |
| 4 | 4 | 128 | SAI | 01H | -0.20 | EC Axial |
| 5 | 4 | 160 | SAI | 02H | -0.33 | EC Axial |
| 6 | 4 | 160 | SAI | 01H | -0.35 | EC Axial |
| 7 | 5 | 141 | SAI | 02H | -0.07 | EC Axial |
| 8 | 8 | 114 | SAI | 01H | +0.70 | EC Axial |
| 9 | 8 | 144 | SAI | 02H | -0.67 | EC Axial |
| 10 | 10 | 136 | SAI | 02H | -0.36 | EC Axial |
| 11 | 10 | 136 | SAI | 02H | +0.24 | EC Axial |
| 12 | 10 | 142 | SAI | 01H | +0.83 | EC Axial |
| 13 | 16 | 148 | SAI | 02H | -0.64 | EC Axial |
| 14 | 17 | 53 | SAI | 02H | +0.32 | EC Axial |
| 15 | 20 | 148 | SAI | 02H | -0.67 | EC Axial |
| 16 | 22 | 116 | SAI | 01H | +0.72 | EC Axial |
| 17 | 23 | 59 | SAI | 01H | +0.73 | EC Axial |
| 18 | 24 | 64 | SAI | 01H | +0.23 | EC Axial |
| 19 | 24 | 136 | SAI | 01H | +0.09 | EC Axial |
| 20 | 29 | 67 | SAI | 01H | +0.24 | EC Axial |
| 21 | 29 | 107 | SAI | 02H | -0.75 | EC Axial |
| 22 | 29 | 107 | SAI | 02H | +0.18 | EC Axial |
| 23 | 32 | 68 | SAI | 01H | +0.58 | EC Axial |
| 24 | 35 | 75 | SAI | 02H | +0.39 | EC Axial |
| 25 | 36 | 20 | SAI | 01H | +0.68 | EC Axial |
| 26 | 36 | 90 | SAI | 02H | +0.80 | EC Axial |
| 27 | 37 | 87 | SAI | 01H | +0.67 | EC Axial |
| 28 | 38 | 102 | SAI | 01H | -0.50 | EC Axial |
| 29 | 39 | 61 | SAI | 01H | -0.65 | EC Axial |
| 30 | 39 | 153 | SAI | 02H | +0.57 | EC Axial |
| 31 | 41 | 83 | SAI | 02H | -0.20 | EC Axial |
| 32 | 42 | 58 | SAI | 03H | +0.50 | EC Axial |
| 33 | 42 | 110 | SAI | 01H | +0.74 | EC Axial |
| 34 | 42 | 126 | SAI | 02H | -0.45 | EC Axial |
| 35 | 43 | 137 | SAI | 02H | +0.38 | EC Axial |
| 36 | 43 | 153 | SAI | 03H | +0.66 | EC Axial |
| 37 | 44 | 52 | SAI | 01H | +0.69 | EC Axial |
| 38 | 44 | 64 | SAI | 01H | -0.73 | EC Axial |
| 39 | 45 | 117 | SAI | 01H | +0.43 | EC Axial |

TABLE 1
SG "A" REPAIR INDICATION LIST FOR 2P00

| No. | Row | Line | Indication | Location | Reason for Repair | |
|-----|-----|------|------------|----------|-------------------|----------|
| 40 | 45 | 123 | SAI | 01H | -0.46 | EC Axial |
| 41 | 45 | 123 | SAI | 01H | +0.26 | EC Axial |
| 42 | 48 | 68 | SAI | 01H | -0.31 | EC Axial |
| 43 | 50 | 84 | SAI | 01H | +0.77 | EC Axial |
| 44 | 51 | 151 | SAI | 02H | +0.20 | EC Axial |
| 45 | 52 | 86 | SAI | 01H | +0.70 | EC Axial |
| 46 | 53 | 35 | SAI | 01H | +0.74 | EC Axial |
| 47 | 54 | 88 | SAI | 02H | -0.27 | EC Axial |
| 48 | 54 | 134 | SAI | 01H | +0.52 | EC Axial |
| 49 | 56 | 44 | SAI | 01H | +0.47 | EC Axial |
| 50 | 56 | 134 | SAI | 01H | -0.71 | EC Axial |
| 51 | 59 | 77 | SAI | 01H | -0.12 | EC Axial |
| 52 | 60 | 124 | SAI | 02H | -0.25 | EC Axial |
| 53 | 64 | 124 | SAI | 02H | -0.26 | EC Axial |
| 54 | 68 | 44 | SAI | 01H | +0.61 | EC Axial |
| 55 | 68 | 44 | SAI | 01H | -0.36 | EC Axial |
| 56 | 68 | 116 | SAI | 01H | -0.77 | EC Axial |
| 57 | 84 | 104 | SAI | 01H | +0.72 | EC Axial |
| 58 | 84 | 104 | SAI | 01H | -0.52 | EC Axial |
| 59 | 84 | 118 | SAI | 03H | -0.28 | EC Axial |
| 60 | 87 | 83 | SAI | 01H | -0.47 | EC Axial |
| 61 | 91 | 65 | SAI | 01H | +0.58 | EC Axial |
| 62 | 93 | 31 | SAI | 02H | +0.43 | EC Axial |
| 63 | 95 | 143 | SAI | 03H | +0.82 | EC Axial |
| 64 | 103 | 127 | SAI | 01H | -0.41 | EC Axial |

Legend:

EC - Egg Crate Support
MAI - Multiple Axial Indication
SAI - Single Axial Indication

TABLE 2
SG "B" REPAIR INDICATION LIST FOR 2P00

| No. | Row | Line | Indication | Location | | Reason for Repair |
|-----|-----|------|------------|----------|-------|-------------------|
| 1 | 1 | 29 | SAI | 03H | -0.41 | EC Axial |
| 2 | 2 | 24 | SAI | 01H | +0.62 | EC Axial |
| 3 | 2 | 24 | SAI | 01H | +0.15 | EC Axial |
| 4 | 3 | 145 | SAI | 02H | +0.59 | EC Axial |
| 5 | 3 | 145 | SAI | 03H | -0.61 | EC Axial |
| 6 | 3 | 151 | SAI | 01H | +0.56 | EC Axial |
| 7 | 4 | 40 | SAI | 04H | -0.24 | EC Axial |
| 8 | 4 | 122 | SAI | 01H | -0.39 | EC Axial |
| 9 | 4 | 122 | SAI | 02H | -0.62 | EC Axial |
| 10 | 4 | 122 | SAI | 02H | +0.56 | EC Axial |
| 11 | 4 | 138 | SAI | 02H | -0.58 | EC Axial |
| 12 | 5 | 19 | SAI | 02H | +0.23 | EC Axial |
| 13 | 5 | 41 | MAI | 01H | +0.71 | EC Axial |
| 14 | 5 | 41 | MAI | 01H | +0.52 | EC Axial |
| 15 | 5 | 41 | SAI | 04H | +0.50 | EC Axial |
| 16 | 6 | 112 | SAI | 02H | -0.50 | EC Axial |
| 17 | 7 | 21 | SAI | 01H | +0.77 | EC Axial |
| 18 | 8 | 26 | SAI | 03H | +0.08 | EC Axial |
| 19 | 8 | 150 | SAI | 02H | +0.63 | EC Axial |
| 20 | 9 | 29 | SAI | 02H | +0.71 | EC Axial |
| 21 | 10 | 34 | SAI | 01H | +0.79 | EC Axial |
| 22 | 10 | 126 | SAI | 01H | +0.64 | EC Axial |
| 23 | 10 | 140 | MAI | 01H | -0.49 | EC Axial |
| 24 | 10 | 140 | MAI | 01H | -0.57 | EC Axial |
| 25 | 11 | 17 | SAI | 02H | +0.67 | EC Axial |
| 26 | 11 | 37 | SAI | 01H | +0.54 | EC Axial |
| 27 | 11 | 39 | SAI | 01H | +0.59 | EC Axial |
| 28 | 11 | 147 | SAI | 02H | -0.58 | EC Axial |
| 29 | 12 | 26 | SAI | 02H | +0.51 | EC Axial |
| 30 | 12 | 138 | SAI | 04H | +0.19 | EC Axial |
| 31 | 13 | 107 | SAI | 02H | +0.72 | EC Axial |
| 32 | 14 | 34 | SAI | 02H | -0.53 | EC Axial |
| 33 | 15 | 27 | MAI | 03H | +0.45 | EC Axial |
| 34 | 15 | 27 | MAI | 03H | -0.22 | EC Axial |
| 35 | 15 | 115 | SAI | 01H | -0.38 | EC Axial |
| 36 | 17 | 33 | SAI | 01H | +0.63 | EC Axial |
| 37 | 17 | 53 | SAI | 02H | +0.17 | EC Axial |
| 38 | 17 | 127 | SAI | 02H | +0.57 | EC Axial |
| 39 | 18 | 30 | SAI | 01H | +0.89 | EC Axial |

TABLE 2
SG "B" REPAIR INDICATION LIST FOR 2P00

| No. | Row | Line | Indication | Location | | Reason for Repair |
|-----|-----|------|------------|----------|-------|-------------------|
| 40 | 18 | 148 | SAI | 01H | -0.74 | EC Axial |
| 41 | 20 | 32 | SAI | 02H | +0.80 | EC Axial |
| 42 | 20 | 34 | SAI | 03H | +0.76 | EC Axial |
| 43 | 22 | 16 | SAI | 01H | +0.50 | EC Axial |
| 44 | 22 | 114 | SAI | 01H | -0.57 | EC Axial |
| 45 | 23 | 145 | SAI | 02H | -0.45 | EC Axial |
| 46 | 24 | 130 | SAI | 01H | -0.54 | EC Axial |
| 47 | 25 | 131 | MAI | 02H | +0.82 | EC Axial |
| 48 | 25 | 131 | MAI | 02H | +0.62 | EC Axial |
| 49 | 26 | 30 | SAI | 01H | +0.68 | EC Axial |
| 50 | 26 | 38 | SAI | 01H | +0.33 | EC Axial |
| 51 | 26 | 44 | SAI | 03H | -0.62 | EC Axial |
| 52 | 27 | 131 | SAI | 02H | -0.41 | EC Axial |
| 53 | 29 | 33 | SAI | 01H | +0.02 | EC Axial |
| 54 | 29 | 47 | SAI | 02H | -0.11 | EC Axial |
| 55 | 30 | 58 | SAI | 05H | +0.64 | EC Axial |
| 56 | 30 | 138 | SAI | 01H | +0.63 | EC Axial |
| 57 | 32 | 122 | SAI | 01H | +0.58 | EC Axial |
| 58 | 32 | 140 | SAI | 03H | -0.14 | EC Axial |
| 59 | 34 | 48 | SAI | 02H | +0.18 | EC Axial |
| 60 | 35 | 63 | SAI | 02H | -0.46 | EC Axial |
| 61 | 36 | 68 | SAI | 01H | -0.29 | EC Axial |
| 62 | 37 | 37 | SAI | 01H | +0.68 | EC Axial |
| 63 | 39 | 75 | SAI | 02H | -0.20 | EC Axial |
| 64 | 40 | 60 | SAI | 01H | +0.45 | EC Axial |
| 65 | 40 | 86 | SAI | 02H | +0.43 | EC Axial |
| 66 | 40 | 108 | SAI | 01H | +0.48 | EC Axial |
| 67 | 44 | 52 | SAI | 01H | -0.40 | EC Axial |
| 68 | 44 | 80 | SAI | 01H | -0.23 | EC Axial |
| 69 | 46 | 50 | SAI | 02H | -0.40 | EC Axial |
| 70 | 46 | 54 | SAI | 02H | -0.54 | EC Axial |
| 71 | 46 | 54 | SAI | 02H | +0.31 | EC Axial |
| 72 | 46 | 90 | MAI | 01H | -0.63 | EC Axial |
| 73 | 46 | 90 | MAI | 01H | +0.02 | EC Axial |
| 74 | 48 | 40 | SAI | 02H | +0.79 | EC Axial |
| 75 | 52 | 52 | SAI | 01H | +0.17 | EC Axial |
| 76 | 52 | 60 | MAI | 02H | +0.70 | EC Axial |
| 77 | 52 | 60 | MAI | 02H | +0.75 | EC Axial |

TABLE 2
SG "B" REPAIR INDICATION LIST FOR 2P00

| No. | Row | Line | Indication | Location | | Reason for Repair |
|-----|-----|------|------------|----------|-------|-------------------|
| 78 | 52 | 106 | SAI | 01H | -0.66 | EC Axial |
| 79 | 53 | 49 | SAI | 02H | -0.20 | EC Axial |
| 80 | 53 | 59 | SAI | 01H | -0.24 | EC Axial |
| 81 | 57 | 115 | SAI | 02H | +0.74 | EC Axial |
| 82 | 58 | 76 | SAI | 03H | +0.29 | EC Axial |
| 83 | 60 | 62 | SAI | 01H | +0.52 | EC Axial |
| 84 | 61 | 67 | SAI | 03H | -0.26 | EC Axial |
| 85 | 61 | 129 | SAI | 01H | +0.71 | EC Axial |
| 86 | 62 | 62 | SAI | 03H | +0.72 | EC Axial |
| 87 | 63 | 85 | MAI | 01H | -0.29 | EC Axial |
| 88 | 63 | 85 | MAI | 01H | -0.52 | EC Axial |
| 89 | 64 | 126 | SAI | 04H | +0.37 | EC Axial |
| 90 | 65 | 69 | SAI | 01H | +0.26 | EC Axial |
| 91 | 65 | 85 | MAI | 01H | +0.44 | EC Axial |
| 92 | 65 | 85 | MAI | 01H | +0.18 | EC Axial |
| 93 | 65 | 105 | SAI | 02H | +0.38 | EC Axial |
| 94 | 67 | 107 | SAI | 02H | +0.55 | EC Axial |
| 95 | 67 | 117 | SAI | 01H | +0.46 | EC Axial |
| 96 | 67 | 121 | SAI | 01H | -0.39 | EC Axial |
| 97 | 69 | 41 | SAI | 01H | +0.81 | EC Axial |
| 98 | 69 | 135 | SAI | 05H | +0.66 | EC Axial |
| 99 | 69 | 141 | SAI | 03H | +0.81 | EC Axial |
| 100 | 69 | 141 | SAI | 03H | +0.32 | EC Axial |
| 101 | 70 | 104 | SAI | 01H | +0.68 | EC Axial |
| 102 | 71 | 101 | SAI | 01H | +0.70 | EC Axial |
| 103 | 73 | 109 | SAI | 03H | +0.53 | EC Axial |
| 104 | 74 | 62 | SAI | 01H | +0.55 | EC Axial |
| 105 | 75 | 99 | SAI | 01H | +0.00 | EC Axial |
| 106 | 76 | 100 | SAI | 01H | +0.70 | EC Axial |
| 107 | 77 | 75 | SAI | 01H | +0.63 | EC Axial |
| 108 | 77 | 95 | SAI | 01H | +0.69 | EC Axial |
| 109 | 77 | 109 | SAI | 01H | +0.15 | EC Axial |
| 110 | 77 | 121 | SAI | 01H | +0.50 | EC Axial |
| 111 | 77 | 123 | SAI | 02H | +0.25 | EC Axial |
| 112 | 78 | 62 | SAI | 02H | +0.82 | EC Axial |
| 113 | 79 | 45 | SAI | 01H | -0.33 | EC Axial |
| 114 | 79 | 75 | SAI | 01H | +0.22 | EC Axial |
| 115 | 79 | 133 | SAI | 01H | +0.85 | EC Axial |
| 116 | 80 | 98 | SAI | 02H | +0.55 | EC Axial |

TABLE 2
SG "B" REPAIR INDICATION LIST FOR 2P00

| No. | Row | Line | Indication | Location | | Reason for Repair |
|-----|-----|------|------------|----------|-------|-------------------|
| 117 | 80 | 104 | SAI | 02H | +0.39 | EC Axial |
| 118 | 80 | 110 | SAI | 02H | -0.25 | EC Axial |
| 119 | 81 | 109 | SAI | 01H | -0.66 | EC Axial |
| 120 | 82 | 52 | SAI | 03H | +0.65 | EC Axial |
| 121 | 82 | 58 | SAI | 02H | -0.30 | EC Axial |
| 122 | 82 | 62 | SAI | 01H | +0.38 | EC Axial |
| 123 | 82 | 96 | SAI | 02H | -0.66 | EC Axial |
| 124 | 82 | 106 | SAI | 01H | +0.41 | EC Axial |
| 125 | 83 | 93 | SAI | 02H | +0.24 | EC Axial |
| 126 | 86 | 82 | MAI | 02H | +0.02 | EC Axial |
| 127 | 86 | 82 | MAI | 02H | +0.65 | EC Axial |
| 128 | 86 | 102 | SAI | 02H | +0.66 | EC Axial |
| 129 | 87 | 59 | SAI | 01H | +0.74 | EC Axial |
| 130 | 87 | 101 | SAI | 01H | +0.77 | EC Axial |
| 131 | 88 | 104 | SAI | 03H | +0.65 | EC Axial |
| 132 | 91 | 67 | SAI | 02H | +0.46 | EC Axial |
| 133 | 92 | 96 | MAI | 01H | +0.71 | EC Axial |
| 134 | 92 | 96 | SAI | 01H | +0.61 | EC Axial |
| 135 | 95 | 99 | SAI | 02H | -0.14 | EC Axial |
| 136 | 96 | 64 | SAI | 01H | +0.51 | EC Axial |
| 137 | 96 | 98 | SAI | 01H | -0.81 | EC Axial |
| 138 | 96 | 120 | SAI | 02H | -0.16 | EC Axial |
| 139 | 98 | 94 | SAI | 02H | +0.59 | EC Axial |
| 140 | 98 | 108 | SAI | 02H | +0.18 | EC Axial |
| 141 | 101 | 55 | SAI | 01H | -0.31 | EC Axial |
| 142 | 103 | 53 | SAI | 03H | +0.66 | EC Axial |
| 143 | 103 | 121 | SAI | 02H | +0.43 | EC Axial |
| 144 | 104 | 94 | SAI | 02H | -0.20 | EC Axial |
| 145 | 105 | 47 | SAI | 04H | +0.69 | EC Axial |
| 146 | 114 | 116 | SAI | 03H | +0.37 | EC Axial |
| 147 | 125 | 55 | SAI | 02H | -0.68 | EC Axial |
| 148 | 127 | 57 | SAI | 02H | -0.33 | EC Axial |

Legend:

EC - Egg Crate Support
MAI - Multiple Axial Indication
SAI - Single Axial Indication