Exel₀

Exelon Generation Company, LLC 1400 Opus Place Downers Grove, IL 60515-5701

www.exeloncorp.com

Nuclear

January 29, 2001

LTR:

BYRON 2001-0018

File:

2 01 0700

United States Nuclear Regulatory Commission

ATTN: Document Control Desk Washington, DC 20555-0001

Byron Station, Units 1 and 2

Facility Operating License Nos. NPF-37 and NPF-66 NRC Docket Nos. STN 50-454 and STN 50-455

Subject:

Byron Station Unit 1 Cycle 11 Core Operating Limits Report

Byron Station Unit 2 Cycle 9 Core Operating Limits Report

In accordance with Technical Specification 5.6.5, "Core Operating Limits Report (COLR)," item d., we are submitting a revised COLR for Byron Station Unit 1, Cycle 11 and Byron Station Unit 2, Cycle 9. Specifically, item 2.12.2 of each COLR was revised to reflect a revision made to our Technical Requirements Manual.

Should you have any questions concerning these reports, please contact Ms. P. Reister, Regulatory Assurance Manager, at (815) 234-5441, extension 2280.

Respectfully,

William Levis

Site Vice President

Byron Station

Attachments: 1) Revised Byron Station Unit 1 Cycle 11 COLR

2) Revised Byron Station Unit 2 Cycle 9 COLR

WL/JL/dpk

CC:

Regional Administrator – NRC Region III

NRC Senior Resident Inspector - Byron Station

1 2

ATTACHMENT 1

Revised Byron Station Unit 1 Cycle 11 COLR

	NUCLEAR FUEL MANAGEMENT DEPARTMENT TRANSMITTAL OF DESIGN INFORMATION	
SAFETY RELATED □ NON-SAFETY RELATED □ REGULATORY RELATED	Originating Organization Nuclear Fuel Management Other (specify)	NFM ID # NFM0000119 Rev. No. 3 Page 1 of 19
Station Byron To: Kenneth N. Kovar – Byron	Unit 1 Cycle 11 Generic	-
Subject Byron Unit 1 Cycle 11 R. Ng Preparer E. Wurz	auch Wurz	11/15/00 11/15/00
Reviewer D. Redden NFM Supervisor	Reviewer Signature	Date 1 / (5 00 Date
Status of Information: Method and Schedule of Verificat	○ Verified │ Unverified │ Engineering Judgement ion for Unverified NDITs:	
Description of Information: Attached is the Byron Unit 1 Cyc	le 11 Core Operating Limits Report (COLR) in the ITS format and	W(z) function.
requirement for the new TRM case. Revision 1 incorporated no Design. This COLR incorporates Limits, Reactor Trip System Instituted. Byron Station is requestransmit the COLR portion to the	edes TODI NFM0000119, Rev. 2. This revision modifies Sec TLCO 3.1.g. Revision 2 incorporated the correct K(Z) curve few W(z) values as a result of an evaluation of the Cycle 10 temp the BY1C11 cycle-specific parameters and the Expanded COLR strumentation, and RCS DNB Parameters. Furthermore, the ansted to perform a Plant Review of this document. Upon completic Nuclear Regulatory Commission pursuant to Technical Specificate's completed Plant Review and COLR submittal to the NRC.	erature coastdown effects on the Cycle 11 format which includes Reactor Core Safety alytical limit of 224 rods out position is no of the Plant Review, Byron Station is to
August 4, 2000. 2) Westinghouse Letter 00CB-G- 3) Byron Technical Specification	BY1C11 Minimum Required Boron Concentration for Modes 3, 4, 0107 (CAC-00-259), "Byron 1 Cycle 11 Input for COLR," dated S Amendment 113, dated May 15, 2000 BY1C11 Reload Design Initialization," dated August 3, 2000. 0116 (CAC-00-280), "Byron 1 Cycle 11 Input for COLR Revision	September 1, 2000.
Supplemental Distribution:	P. E. Reister / J. E. Langan (BY)	

i j

CORE OPERATING LIMITS REPORT 1.0

This Core Operating Limits Report (COLR) for Byron Station Unit 1 Cycle 11 has been prepared in accordance with the requirements of Technical Specification 5.6.5 (ITS).

The Technical Specifications affected by this report are listed below:

SL	2.1.1	Reactor Core Safety Limits (SLs)
LCO	3.1.1	Shutdown Margin (SDM)
LCO	3.1.3	Moderator Temperature Coefficient
LCO	3.1.4	Rod Group Alignment Limits
LCO	3.1.5	Shutdown Bank Insertion Limits
LCO	3.1.6	Control Bank Insertion Limits
LCO	3.1.8	Physics Tests Exceptions - Mode 2
LCO	3.2.1	Heat Flux Hot Channel Factor (F _Q (Z))
LCO	3.2.2	Nuclear Enthalpy Rise Hot Channel Factor (F ^N _{ΔH})
LCO	3.2.3	Axial Flux Difference (AFD)
LCO	3.3.1	Reactor Trip System (RTS) Instrumentation
LCO	3.3.9	Boron Dilution Protection System (BDPS)
LCO	3.4.1	Reactor Coolant System (RCS) DNB Parameters
LCO	3.9.1	Boron Concentration
The p	ortions o	of the Technical Requirements Manual affected by this report are listed

d below: The portions of

TRM TLCO 3.1.b	Boration Flow Paths - Operating
TRM TLCO 3.1.d	Charging Pumps - Operating
TRM TLCO 3.1.f	Borated Water Sources - Operating
TRM TLCO 3.1.g	Position Indication System - Shutdown
TRM TLCO 3.1.h	Shutdown Margin (SDM) – MODE 1 and MODE 2 with keff \geq 1.0
TRM TLCO 3.1.i	Shutdown Margin (SDM) - MODE 5
TRM TLCO 3.1.j	Shutdown and Control Rods
TRM TLCO 3.1.k	Position Indication System - Shutdown (Special Test Exception)

2.0 OPERATING LIMITS

ī

The cycle-specific parameter limits for the specifications listed in Section 1.0 are presented in the following subsections. These limits are applicable for the entire cycle unless otherwise identified. These limits have been developed using the NRC-approved methodologies specified in Technical Specification 5.6.5.

- 2.1 Reactor Core Limits (SL 2.1.1)
 - 2.1.1 In Modes 1 and 2, the combination of Thermal Power, Reactor Coolant System (RCS) highest loop average temperature, and pressurizer pressure shall not exceed the limits specified in Figure 2.1.1.
- 2.2 Shutdown Margin (SDM)

The SDM limit for MODES 1, 2, 3, and 4 is:

2.2.1 The SDM shall be greater than or equal to 1.3% Δ k/k (LCOs 3.1.1, 3.1.4, 3.1.5, 3.1.6, 3.1.8, 3.3.9; TRM TLCOs 3.1.b, 3.1.d, 3.1.f, 3.1.h, and 3.1.j).

The SDM limits for MODE 5 are:

- 2.2.2.1 SDM shall be greater than or equal to 1.0% $\Delta k/k$ (LCO 3.1.1)
- 2.2.2.2 SDM shall be greater than or equal to 1.3% $\Delta k/k$ (LCO 3.3.9; TRM TLCO 3.1.i and 3.1.j)
- 2.3 Moderator Temperature Coefficient (LCO 3.1.3)

The Moderator Temperature Coefficient (MTC) limits are:

- 2.3.1 The BOL/ARO/HZP-MTC upper limit shall be $+3.7 \times 10^{-5} \Delta k/k/^{\circ}F$.
- 2.3.2 The EOL/ARO/HFP-MTC lower limit shall be -4.1 x $10^{-4} \Delta k/k/^{\circ}F$.
- 2.3.3 The EOL/ARO/HFP-MTC Surveillance limit at 300 ppm shall be less negative than or equal to -3.2 x 10^{-4} $\Delta k/k/^{\circ}F$.

where: BOL stands for Beginning of Cycle Life

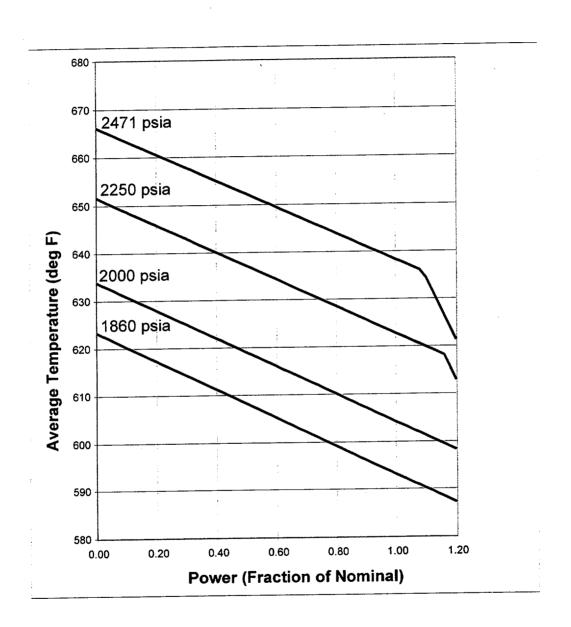
ARO stands for All Rods Out

HZP stands for Hot Zero Thermal Power

EOL stands for End of Cycle Life

HFP stands for Hot Full Thermal Power

Figure 2.1.1: Reactor Core Limits

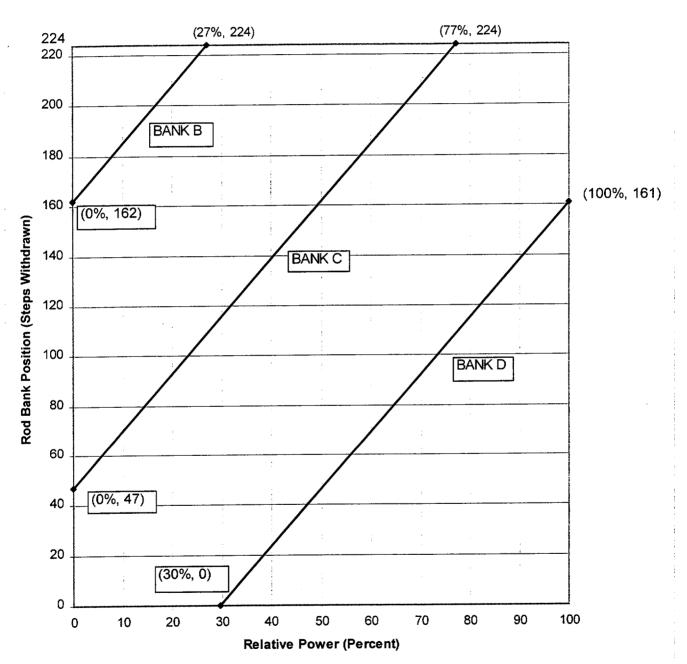


2.4 Shutdown Bank Insertion Limit (LCO 3.1.5)

î

- 2.4.1 All shutdown banks shall be fully withdrawn to at least 224 steps.
- 2.5 Control Bank Insertion Limits (LCO 3.1.6)
 - 2.5.1 The control banks shall be limited in physical insertion as shown in Figure 2.5.1.
 - 2.5.2 Each control bank shall be considered fully withdrawn from the core at greater than or equal to 224 steps.
 - 2.5.3 The control banks shall be operated in sequence by withdrawal of Bank A, Bank B, Bank C and Bank D. The control banks shall be sequenced in reverse order upon insertion.
 - 2.5.4 Each control bank not fully withdrawn from the core shall be operated with a 113 step overlap limit.

Figure 2.5.1:
Control Bank Insertion Limits Versus Percent Rated Thermal Power



2.6 <u>Heat Flux Hot Channel Factor (F_Q(Z))</u> (LCO 3.2.1)

2.6.1

$$Fq(Z) \le \frac{Fq^{RTP}}{0.5} xK(Z) \text{ for } P \le 0.5$$

$$Fq(Z) \le \frac{Fq^{RTP}}{P} xK(Z) \text{ for } P > 0.5$$

where: P = the ratio of THERMAL POWER to RATED THERMAL POWER

$$F_0^{RTP} = 2.60$$

K(Z) for assembly average burnup > 4000 MWD/MTU is provided in Figure 2.6.1. K(Z) for assembly average burnup \leq 4000 MWD/MTU is provided in Figure 2.6.1.a.

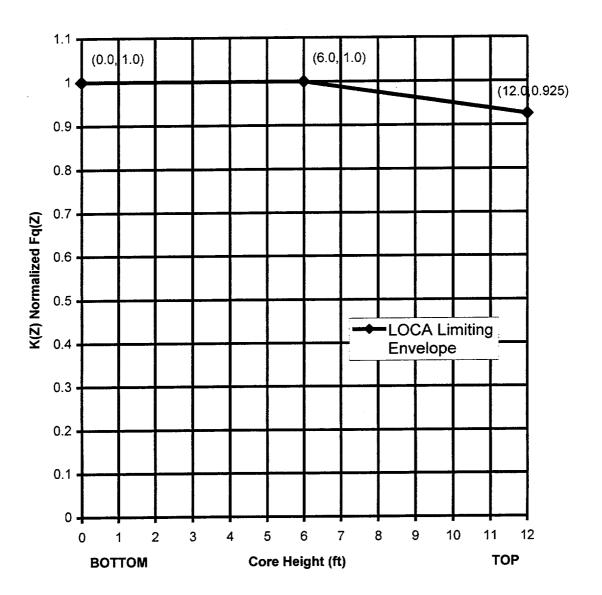
2.6.2 W(Z) is provided in Figures 2.6.2.a through 2.6.2.d.

The normal operation W(Z) values have been determined at burnups of 150, 4000, 10000, and 18000 MWD/MTU.

Table 2.6.2 shows the $F^c_{Q}(z)$ penalty factors that are greater than 2% per 31 Effective Full Power Days. These values shall be used to increase the $F^w_{Q}(z)$ as per Surveillance Requirement 3.2.1.2. A 2% penalty factor shall be used at all cycle burnups that are outside the range of Table 2.6.2.

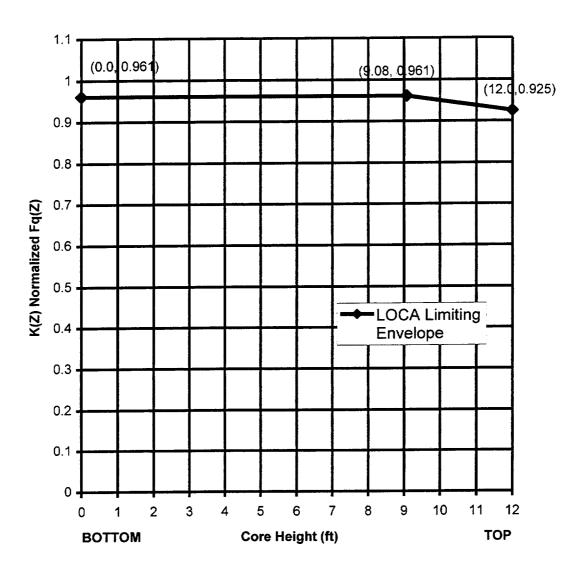
Multiplication Factor = 1.02

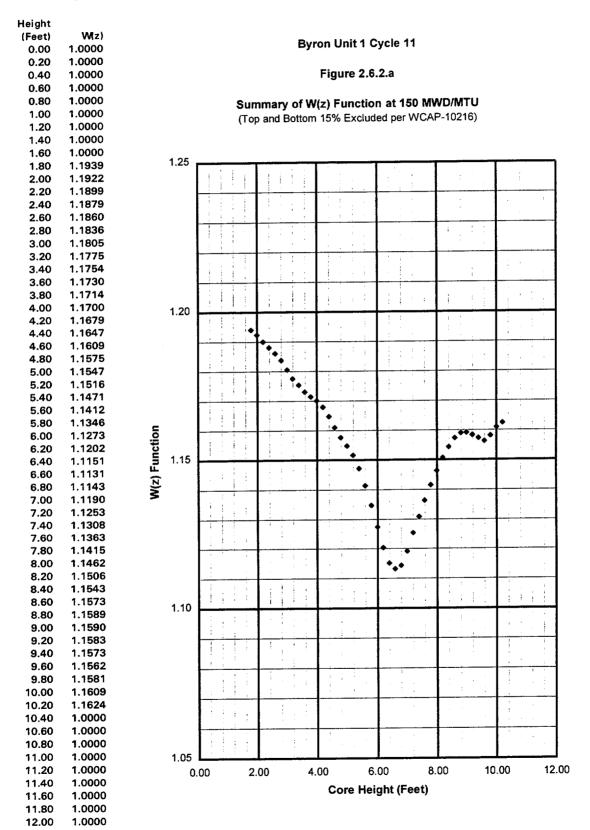
Figure 2.6.1: K(Z) - Normalized Fq(Z) as a Function of Core Height (Assembly Average > 4000 MWD/MTU)

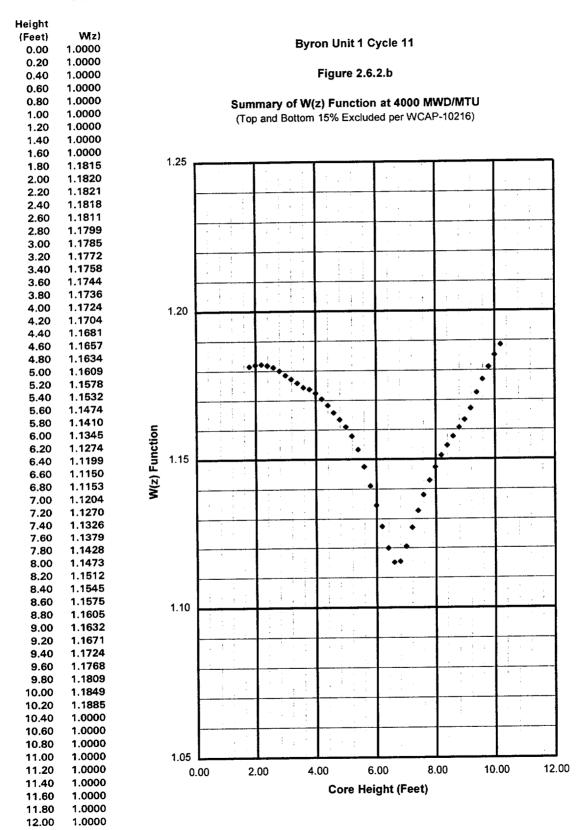


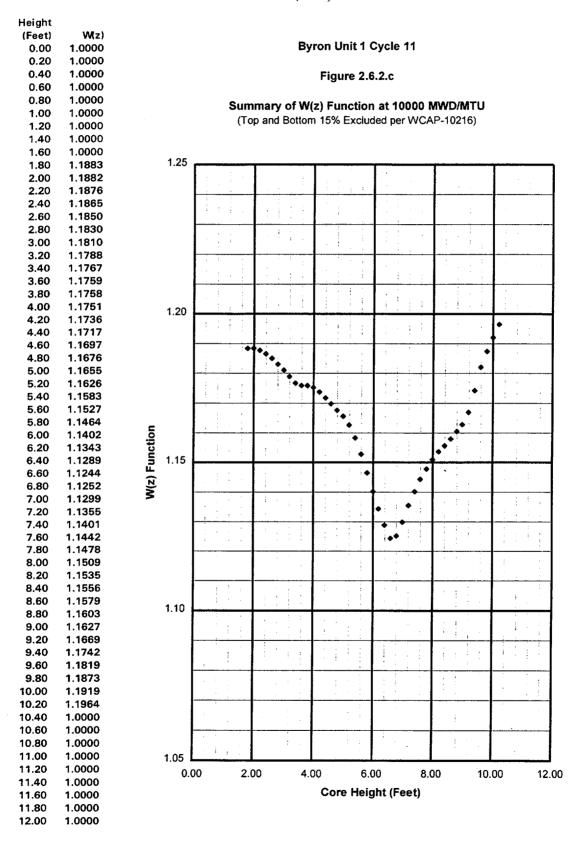
ĵ

Figure 2.6.1.a: K(Z) - Normalized Fq(Z) as a Function of Core Height (Assembly BU ≤ 4000 MWD/MTU)









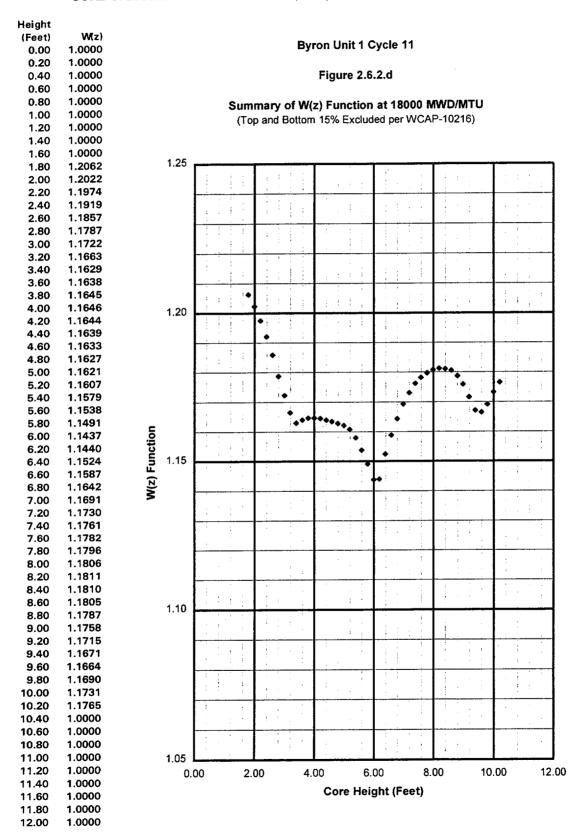


Table	2.6.2
Fq Margin Decreases in F	Excess of 2% per 31 EFPD
Cycle Burnup (MWD/MTU)	Max % Decrease in Fq Margin
150 314 479 643 808 972 1137 1301	4.15 4.31 4.40 4.40 4.27 3.99 3.59 3.09 2.54
≥1630	2.00

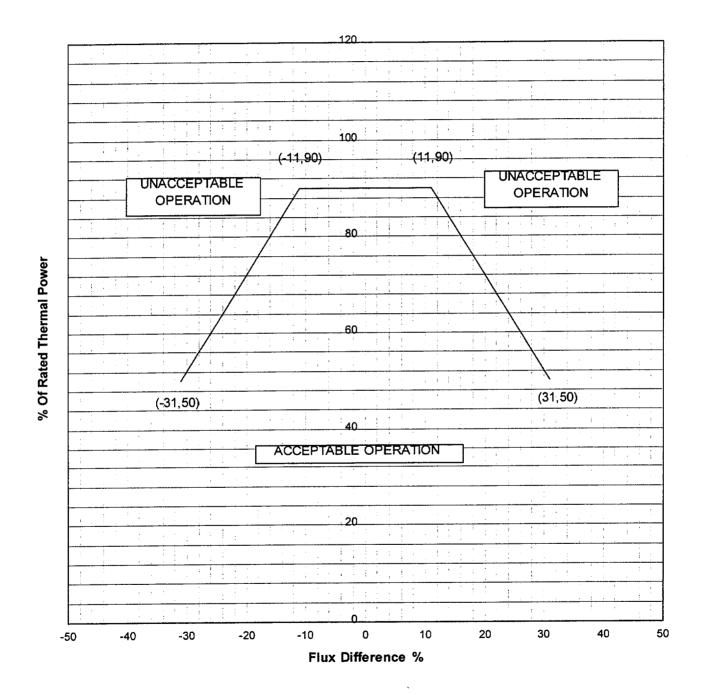
Note: All cycle burnups outside the range of the table shall use a 2% decrease in Fq margin for compliance with the 3.2.1.2 Surveillance Requirements.

- 2.7 Nuclear Enthalpy Rise Hot Channel Factor (FNAH) (LCO 3.2.2)
 - 2.7.1 $F_{\Delta H}^{N} \leq F_{\Delta H}^{RTP}[1.0 + PF_{\Delta H}(1.0 P)]$

where: P = the ratio of THERMAL POWER to RATED THERMAL POWER $F_{\Delta H}^{RTP}$ = 1.70 $PF_{\Delta H}$ = 0.3

- 2.8 Axial Flux Difference (AFD) (LCO 3.2.3)
 - 2.8.1 The AXIAL FLUX DIFFERENCE (AFD) target band is +5, -10% of the target flux difference.
 - 2.8.2 The AFD Acceptable Operation Limits are provided in Figure 2.8.1.

FIGURE 2.8.1: Axial Flux Difference Limits As A Function of Rated
Thermal Power



2.9	Reactor	Trip System Overtemperature ∆T Setpoint Parameter Values (LCO 3.3.1)
	2.9.1	The Overtemperature ΔT reactor trip setpoint K_1 shall be equal to 1.325.
	2.9.2	The Overtemperature ΔT reactor trip setpoint T_{avg} coefficient K_2 shall be equal to 0.0297 / °F.
	2.9.3	The Overtemperature ΔT reactor trip setpoint pressure coefficient K_3 shall be equal to 0.00181 / psig.
	2.9.4	The nominal T_{avg} at RTP (indicated) T^\prime shall be less than or equal to 588.4 °F.
	2.9.5	The nominal RCS operating pressure (indicated) P' shall be equal to 2235 psig.
	2.9.6	The measured reactor vessel ΔT lead/lag time constant τ_1 shall be equal to 8 sec.
	2.9.7	The measured reactor vessel ΔT lead/lag time constant τ_2 shall be equal to 3 sec.
	2.9.8	The measured reactor vessel ΔT lag time constant τ_3 shall be less than or equal to 2 sec.
	2.9.9	The measured reactor vessel average temperature lead/lag time constant τ_{4} shall be equal to 33 sec.
	2.9.10	The measured reactor vessel average temperature lead/lag time constant τ_5 shall be equal to 4 sec.
	2.9.11	The measured reactor vessel average temperature lag time constant $\tau_{\text{6}}\text{shall}$ be less than or equal to 2 sec.
	2.9.12	The $f_1(\Delta I)$ "positive" breakpoint shall be +10% ΔI .
	2.9.13	The $f_1(\Delta I)$ "negative" breakpoint shall be - 24% ΔI .
	2.9.14	The f ₁ (Δ I) "positive" slope shall be +4.11% / % Δ I.
	2.9.15	The f_1 (ΔI) "negative" slope shall be - 3.35% / % ΔI .

2.10	Reactor	Trip System Overpower ΔT Setpoint Parameter Values (LCO 3.3.1)
	2.10.1	The Overpower ΔT reactor trip setpoint K_4 shall be equal to 1.072.
	2.10.2	The Overpower ΔT reactor trip setpoint T_{avg} rate/lag coefficient K_s shall be equal to 0.02 / °F for increasing T_{avg} .
	2.10.3	The Overpower ΔT reactor trip setpoint T_{avg} rate/lag coefficient K_5 shall be equal to 0 / °F for decreasing T_{avg}
	2.10.4	The Overpower ΔT reactor trip setpoint T_{avg} heatup coefficient K_6 shall be equal to 0.00245 / °F when $T > T''$.
	2.10.5	The Overpower ΔT reactor trip setpoint T_{avg} heatup coefficient K_6 shall be equal to 0 / °F when $T \leq T''$.
	2.10.6	The nominal T_{avg} at RTP (indicated) T'' shall be less than or equal to 588.4 °F.
	2.10.7	The measured reactor vessel ΔT lead/lag time constant τ_1 shall be equal to 8 sec.
	2.10.8	The measured reactor vessel ΔT lead/lag time constant τ_2 shall be equal to 3 sec.
	2.10.9	The measured reactor vessel ΔT lag time constant τ_3 shall be less than or equal to 2 sec.
	2.10.10	The measured reactor vessel average temperature lag time constant τ_{6} shall be less than or equal to 2 sec.
	2.10.11	The measured reactor vessel average temperature rate/lag time constant τ_{7} shall be equal to 10 sec.
	2.10.12	The $f_2(\Delta I)$ "positive" breakpoint shall be 0 for all ΔI .
	2.10.13	The $f_2(\Delta I)$ "negative" breakpoint shall be 0 for all ΔI .
	2.10.14	The $f_2(\Delta I)$ "positive" slope shall be 0 for all ΔI .
	2.10.15	The $f_2(\Delta I)$ "negative" slope shall be 0 for all ΔI .

- 2.11 Reactor Coolant System (RCS) DNB Parameter Limits (LCO 3.4.1)
 - 2.11.1 The pressurizer pressure shall be greater than or equal to 2219 psig.
 - 2.11.2 The RCS average temperature (T_{avg}) shall be less than or equal to 591.2 °F.
 - 2.11.3 The RCS total flow rate shall be greater than or equal to 371,400 gpm.

2.12 Boron Concentration

- 2.12.1 The refueling boron concentration shall be greater than or equal to 2000 ppm (LCO 3.9.1).
- 2.12.2 The Reactor Coolant System boron concentration shall be greater than or equal to 1894 ppm prior to initial criticality of Cycle 11, or greater than or equal to 2075 ppm at all other times in core life, to maintain adequate shutdown margin for MODES 3, 4, and 5 during performance of rod drop time measurements and during the surveillance of Digital Rod Position Indication (DRPI) for OPERABILITY (TLCO 3.1.g and TLCO 3.1.k)

ATTACHMENT 2

Revised Byron Station Unit 2 Cycle 9 COLR

	NUCLEAR FUEL MANAGEMENT DEPARTMENT NUCLEAR DESIGN INFORMATION TRANSMITTAL				
SAFETY RELATED □ NON-SAFETY RELATED □ REGULATORY RELATED	Originating Organization Nuclear Fuel Management Other (specify)	NDIT No. NFM9900202 Seq. No. 3 Page 1 of 18			
Station Byron To: Kenneth N. Kovar - Byron	Unit 2 Cycle 9 Generic				
	ore Operating Limits Report in ITS Format and W(z) Function				
R. Ng Preparer E. Wurz Reviewer	Preparer's Signature Deviewer's Signature Deviewer's Signature Deviewer's Signature	11/15/00 Date 11/15/00			
D. Redden NFM Supervisor	NFM Supervisor's Signature D	ate [1] (5) (0)			
Status of Information: Method and Schedule of Verificatio	○ Verified │ Unverified │ Engineering Judgement n for Unverified NDITs:				
Description of Information: Attached is the Byron Unit 2 Cycle	9 Core Operating Limits Report (COLR) in the ITS format and W	(z) function.			
Purpose of Information: Sequence 3 of this NDIT supersedes Sequence 2. Sequence 3 modifies Section 2.12.2 of the COLR to support the requirement for the new TRM TLCO 3.1.g. Sequence 2 revised Page 9 to include the correct Figure 2.6.1.a for the K(z) curve with assembly average burnup ≤ 4000 MWD/MTU. Sequence 1 added clarification for the minimum boron concentration for TLCO 3.1.k to include DRPI operability surveillance and it incorporated the Expanded COLR format which includes Reactor Core Safety Limits, Reactor Trip System Instrumentation, and RCS DNB parameters. The analytical 224 position limit for rods out was included in Sequence 1. Byron Station is requested to perform a Plant Review of this document. Upon completion of the Plant Review, Byron Station is to transmit the COLR portion to the Nuclear Regulatory Commission pursuant to Technical Specification 5.6.5. Please provide NFM (Raymond Ng) with a copy of Byron Station's completed Plant Review and COLR submittal to the NRC.					
 PND Calculation Number SP-18 NDIT NFM9900158, Seq. 0, "M PSS Calculation Number PSSC 1999. CAC-99-346, Rev. 3, "Safety As Byron Technical Specification A 	, Rev. 0, "Generation of W(z) Curve," Project Byron Unit 2 Cycle, "Unfavorable Exposure Time (UET) Analysis," Project Byron Ulinimum Required Boron Concentration for Control Rod Drop Tes N:99-015, "Byron Unit 2 Cycle 9 Bank Insertion Limits with 1 sessment Summary for Byron Unit 2 Cycle 9," dated October 11, mendment 113, dated May 15, 2000. CN:00-003, "Evaluation of SPIL Using 224 Steps Rod Withdrawn	Juit 2 Cycle 9, dated July 23, 1999. Sting – BY2C9," dated August 13, 1999. 16 Step Separation," dated October 15, 1999.			
Supplemental Distribution: P. F.	. Reister / J. Langan (BY)				

1.0 CORE OPERATING LIMITS REPORT

This Core Operating Limits Report (COLR) for Byron Station Unit 2 Cycle 9 has been prepared in accordance with the requirements of Technical Specification 5.6.5 (ITS).

The Technical Specifications affected by this report are listed below:

SL	2.1.1	Reactor Core Safety Limits (SLs)
LCO	3.1.1	Shutdown Margin (SDM)
LCO	3.1.3	Moderator Temperature Coefficient
LCO	3.1.4	Rod Group Alignment Limits
LCO	3.1.5	Shutdown Bank Insertion Limits
LCO	3.1.6	Control Bank Insertion Limits
LCO	3.1.8	Physics Tests Exceptions – Mode 2
LCO	3.2.1	Heat Flux Hot Channel Factor $(F_Q(Z))$
LCO	3.2.2	Nuclear Enthalpy Rise Hot Channel Factor $(F^{N}_{\ \Delta H})$
LCO	3.2.3	Axial Flux Difference (AFD)
LCO	3.3.1	Reactor Trip System (RTS) Instrumentation
LCO	3.3.9	Boron Dilution Protection System (BDPS)
LCO	3.4.1	Reactor Coolant System (RCS) DNB Parameters
LCO	3.9.1	Boron Concentration

The portions of the Technical Requirements Manual affected by this report are listed below:

TRM TLCO 3.1.b	Boration Flow Paths - Operating
TRM TLCO 3.1.d	Charging Pumps Operating
TRM TLCO 3.1.f	Borated Water Sources - Operating
TRM TLCO 3.1.g	Position Indication System – Shutdown
TRM TLCO 3.1.h	Shutdown Margin (SDM) – MODE 1 and MODE 2 with keff ≥ 1.0
TRM TLCO 3.1.i	Shutdown Margin (SDM) - MODE 5
TRM TLCO 3.1.j	Shutdown and Control Rods
TRM TLCO 3.1.k	Position Indication System - Shutdown (Special Test Exception)

2.0 OPERATING LIMITS

The cycle-specific parameter limits for the specifications listed in Section 1.0 are presented in the following subsections. These limits are applicable for the entire cycle unless otherwise identified. These limits have been developed using the NRC-approved methodologies specified in Technical Specification 5.6.5.

- 2.1 Reactor Core Limits (SL 2.1.1)
 - 2.1.1 In Modes 1 and 2, the combination of Thermal Power, Reactor Coolant System (RCS) highest loop average temperature, and pressurizer pressure shall not exceed the limits specified in Figure 2.1.1.

2.2 Shutdown Margin (SDM)

The SDM limit for MODES 1, 2, 3, and 4 is:

2.2.1 The SDM shall be greater than or equal to 1.3% Δk/k (LCOs 3.1.1, 3.1.4, 3.1.5, 3.1.6, 3.1.8, 3.3.9; TRM TLCOs 3.1.b, 3.1.d, 3.1.f, 3.1.h, and 3.1.j).

The SDM limits for MODE 5 are:

- 2.2.2.1 SDM shall be greater than or equal to 1.0% Δk/k (LCO 3.1.1)
- 2.2.2.2 SDM shall be greater than or equal to 1.3% Δ k/k (LCO 3.3.9; TRM TLCO 3.1.i and 3.1.j)
- 2.3 <u>Moderator Temperature Coefficient</u> (LCO 3.1.3)

The Moderator Temperature Coefficient (MTC) limits are:

- 2.3.1 The BOL/ARO/HZP-MTC upper limit shall be $+3.3 \times 10^{-5} \Delta k/k/^{\circ}F$.
- 2.3.2 The EOL/ARO/HFP-MTC lower limit shall be -4.1 x 10^{-4} $\Delta k/k/^{\circ}F$.
- 2.3.3 The EOL/ARO/HFP-MTC Surveillance limit at 300 ppm shall be less negative than or equal to $-3.2 \times 10^{-4} \Delta k/k/^{\circ}F$.

where: BOL stands for Beginning of Cycle Life

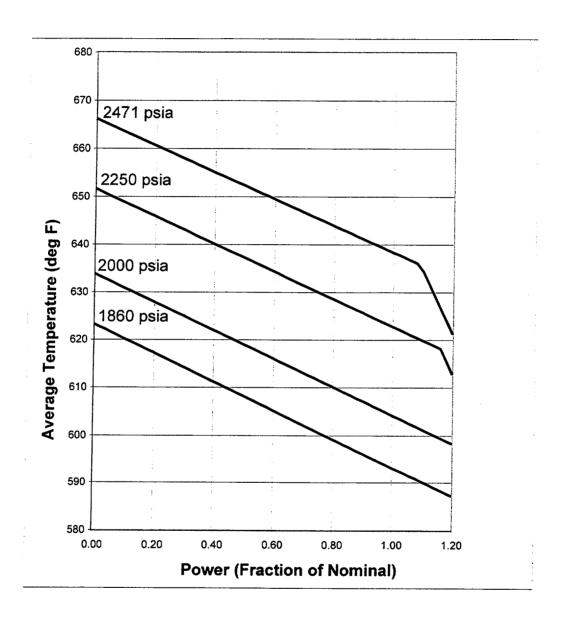
ARO stands for All Rods Out

HZP stands for Hot Zero Thermal Power

EOL stands for End of Cycle Life

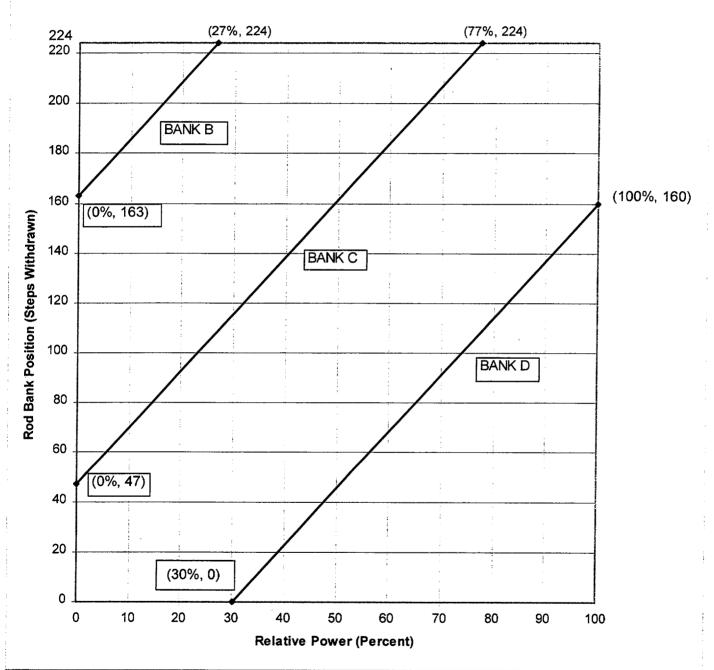
HFP stands for Hot Full Thermal Power

Figure 2.1.1: Reactor Core Limits



- 2.4 <u>Shutdown Bank Insertion Limit</u> (LCO 3.1.5)
 - 2.4.1 All shutdown banks shall be fully withdrawn to at least 224 steps.
- 2.5 Control Bank Insertion Limits (LCO 3.1.6)
 - 2.5.1 The control banks shall be limited in physical insertion as shown in Figure 2.5.1.
 - 2.5.2 Each control bank shall be considered fully withdrawn from the core at greater than or equal to 224 steps.
 - 2.5.3 The control banks shall be operated in sequence by withdrawal of Bank A, Bank B, Bank C and Bank D. The control banks shall be sequenced in reverse order upon insertion.
 - 2.5.4 Each control bank not fully withdrawn from the core shall be operated with a 115 step overlap limit.

Figure 2.5.1:
Control Bank Insertion Limits Versus Percent Rated Thermal Power



2.6 <u>Heat Flux Hot Channel Factor (F_Q(Z))</u> (LCO 3.2.1)

2.6.1

69

$$Fq(Z) \le \frac{Fq^{RTP}}{0.5} xK(Z) \text{ for } P \le 0.5$$

$$Fq(Z) \le \frac{Fq^{RTP}}{P} xK(Z) \text{ for } P > 0.5$$

where: P = the ratio of THERMAL POWER to RATED THERMAL POWER

$$F_{q}^{RTP} = 2.60$$

K(Z) for assembly average burnup > 4000 MWD/MTU is provided in Figure 2.6.1. K(Z) for assembly average burnup \leq 4000 MWD/MTU is provided in Figure 2.6.1.a.

2.6.2 W(Z) is provided in Figures 2.6.2.a through 2.6.2.c.

The normal operation W(Z) values have been determined at burnups of 150, 8000 and 18800 MWD/MTU.

Table 2.6.2 shows the $F^c_Q(z)$ penalty factors that are greater than 2% per 31 Effective Full Power Days. These values shall be used to increase the $F^w_Q(z)$ as per Surveillance Requirement 3.2.1.2. A 2% penalty factor shall be used at all cycle burnups that are outside the range of Table 2.6.2.

Multiplication Factor = 1.02

Figure 2.6.1: K(Z) - Normalized Fq(Z) as a Function of Core Height (Assembly Average > 4000 MWD/MTU)

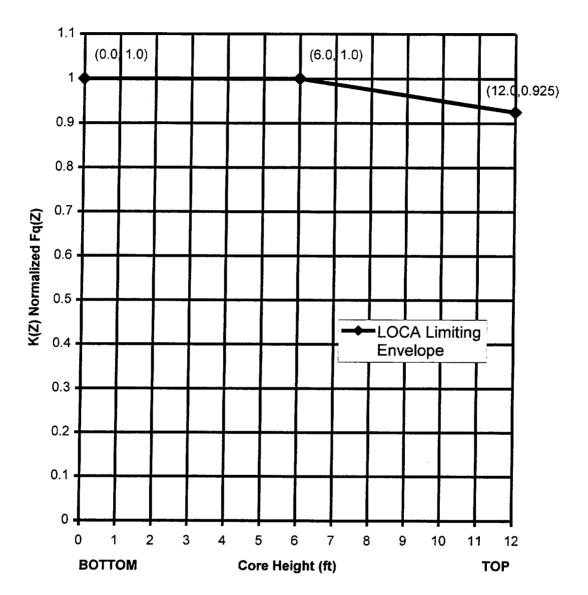
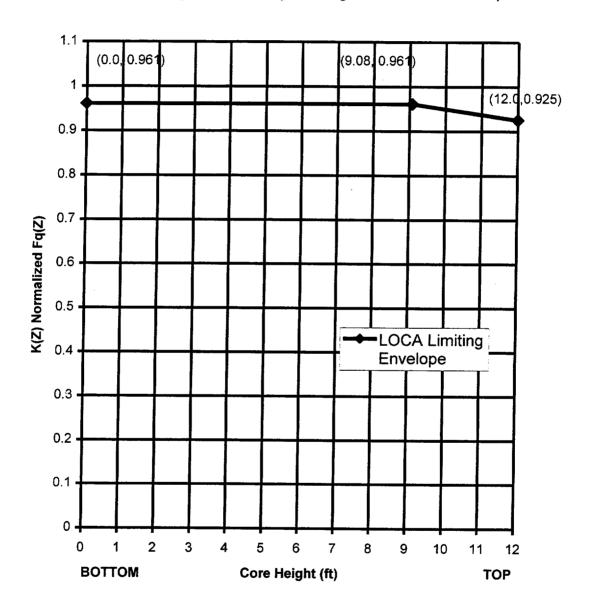
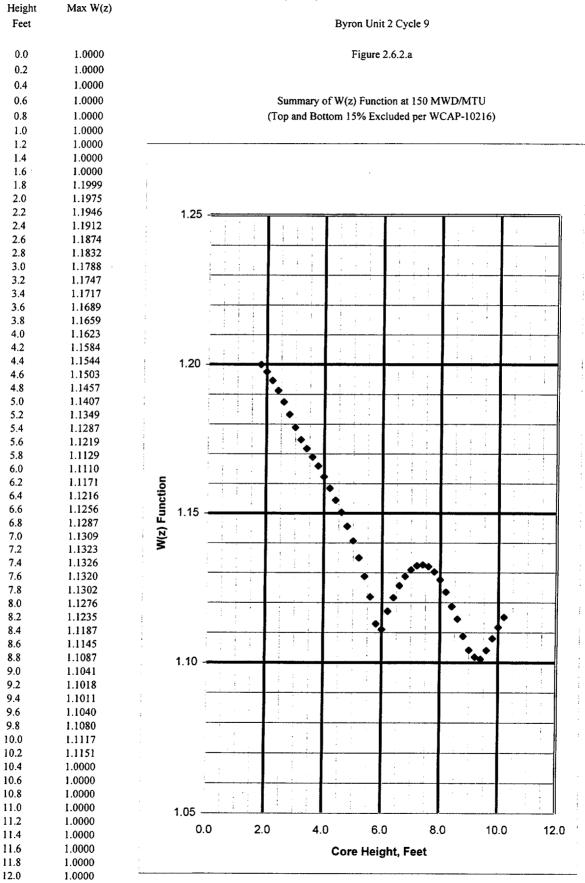
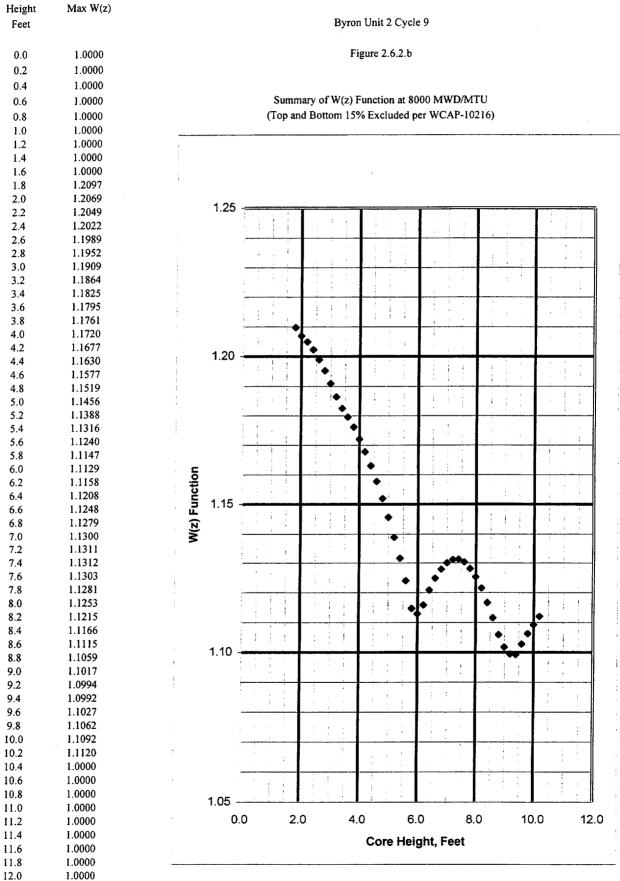


Figure 2.6.1.a: K(Z) - Normalized Fq(Z) as a Function of Core Height (Assembly Average ≤ 4000 MWD/MTU)







eet	Max W(z) Byron Unit 2 Cycle 9														
0.0	1.0000					I	igure	2.6.2.c							
0.2	1.0000														
).4).6	1.0000 1.0000			Sun	nmary of	W(2)	Functi	on at I	የጸበበ እ⁄	(WD/N	(TI)				
.8	1.0000				and Bot										
.0	1.0000			(10)	une 201			0.000	pe	<i></i>	,210)				
.2	1.0000											2,2			
.4	1.0000														
.6	1.0000														
.8 .0	1.2188 1.2148														
2	1.2099	*	1.25												_
4	1.2044				i				1	1 1		:		1	ŀ
6	1.1982			: : :	-				 	:	 		 		-
8	1.1914									. :	ļ	: :			
)	1.1846			 		-			-						\dashv
	1.1773 1.1705	:			1									1	
	1.1703				•	:		1 1				,	;	-i :	-
	1.1642	•			1.			i	:						
	1.1611				•	:			1					- :	٦
	1.1577	•	1.20 -		•	:									
	1.1538		1.20 -		•			· i				1		1	
	1.1495 1.1449				•							<u> </u>		<u>'</u> ;	
	1.1396									1	l				I
	1.1341	1			`			1 ;		<u> </u>	<u> </u>		<u> </u>		_
	1.1276				1	•							:		
	1.1203					•		·	<u> </u>	<u> </u>	-	<u>: : :</u>			4
	1.1210					•				. :			:	•	Ì
	1.1267 1.1319	u o		1 : 1	 						<u> </u>		-		$-\parallel$
	1.1363	ıcti	i			i	•			1		. :	'	1 1	1
	1.1397	Ē	1.15 -	-	+		-	1 .					╂		-
	1.1421	W(z) Function					•			144	1			1 1	1
	1.1435	∫ ≶	:					•	•	•					╢
	1.1438 1.1430	:			:	:	1	•	•			:	:	į	
	1.1410							• •				:	1		٦
	1.1386	:									-				
	1.1352	4									•	1 1			
	1.1304	ī.			1		:	. :					<u> </u>	<u>:</u>	
	1.1245	:					1						1		
	1.1178 1.1099	:	1.10 -			·	<u> </u>	1 !	<u> </u>		<u> </u>	Yes.			4
	1.1034	į	;				:] [;]						1
	1.1011				1			. :			<u> </u>		 	++	$-\parallel$
	1.1015		:	!				:			'		•	1 1	
	1.1053		ŀ		 								-		$-\parallel$
	1.1088					,			1			. :			
	1.1120 1.1149				1				<u></u>				 		-
	1.0000					•		: '						: :	
	1.0000				1						:	:			\parallel
	1.0000		1.05			i									
	1.0000		1.05 -		~	-			^						
	1.0000		0.0	υ 2	2.0	4.	U	6.	U	8.	U	10	0.0	1	12.
	1.0000 1.0000		Core Height, Feet												
	1.0000														

Tabl	e 2.6.2
Fq Margin Decreases in	Excess of 2% per 31 EFPD
Cycle Burnup	Max % Decrease
(MWD/MTU)	in Fq Margin
150	3.54
275	3.50
400	3.48
525	3.44
650	3.38
775	3.29
900	3.15
1025	2.96
1150	2.69
1275	2.37
1400	2.01
1525	2.00

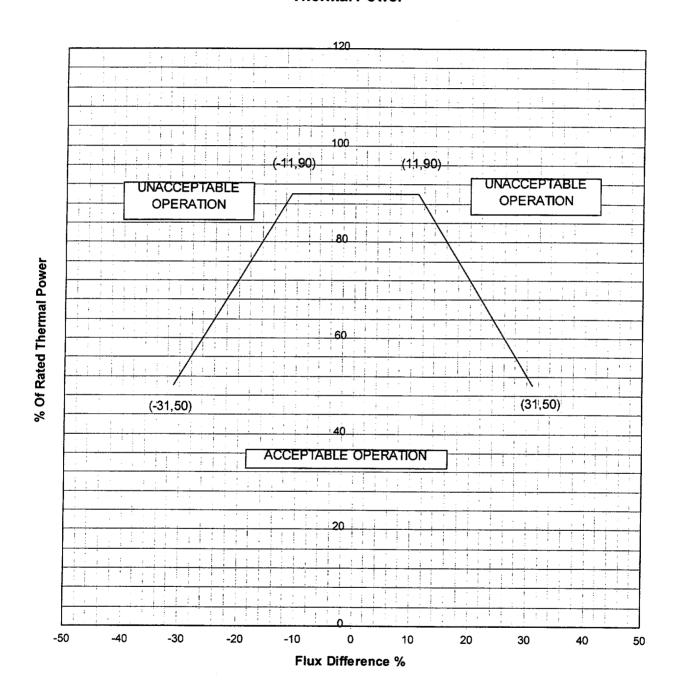
Note: All cycle burnups outside the range of the table shall use a 2% decrease in Fq margin for compliance with the 3.2.1.2 Surveillance Requirements.

- 2.7 <u>Nuclear Enthalpy Rise Hot Channel Factor (F^N_{AH})</u> (LCO 3.2.2)
 - 2.7.1 $F_{\Delta H}^{N} \leq F_{\Delta H}^{RTP}[1.0 + PF_{\Delta H}(1.0 P)]$

where: P = the ratio of THERMAL POWER to RATED THERMAL POWER $F^{RTP}_{\Delta H}$ = 1.70 $PF_{\Delta H}$ = 0.3

- 2.8 Axial Flux Difference (AFD) (LCO 3.2.3)
 - 2.8.1 The AXIAL FLUX DIFFERENCE (AFD) target band is +3, -12% of the target flux difference.
 - 2.8.2 The AFD Acceptable Operation Limits are provided in Figure 2.8.1.

FIGURE 2.8.1: Axial Flux Difference Limits As A Function of Rated
Thermal Power



2.9	Reacto	Reactor Trip System Overtemperature <u>AT Setpoint Parameter Values</u> (LCO 3.3.1)							
	2.9.1	The Overtemperature ΔT reactor trip setpoint K_1 shall be equal to 1.325.							
	2.9.2	The Overtemperature ΔT reactor trip setpoint T_{avg} coefficient K_2 shall be equal to 0.0297 / °F.							
	2.9.3	The Overtemperature ΔT reactor trip setpoint pressure coefficient K_3 shall be equal to 0.00181 / psig.							
	2.9.4	The nominal T _{avg} at RTP (indicated) T' shall be less than or equal to 588.4 °F.							
	2.9.5	The nominal RCS operating pressure (indicated) P' shall be equal to 2235 psig.							
	2.9.6	The measured reactor vessel ΔT lead/lag time constant τ_1 shall be equal to 8 sec.							
	2.9.7	The measured reactor vessel ΔT lead/lag time constant τ_2 shall be equal to 3 sec.							
	2.9.8	The measured reactor vessel ΔT lag time constant τ_3 shall be less than or equal to 2 sec.							
	2.9.9	The measured reactor vessel average temperature lead/lag time constant τ_{4} shall be equal to 33 sec.							
	2.9.10	The measured reactor vessel average temperature lead/lag time constant τ_{5} shall be equal to 4 sec.							
	2.9.11	The measured reactor vessel average temperature lag time constant τ_{e} shall be less than or equal to 2 sec.							
	2.9.12	The $f_1(\Delta I)$ "positive" breakpoint shall be +10% ΔI .							
	2.9.13	The $f_1(\Delta I)$ "negative" breakpoint shall be - 24% ΔI .							
	2.9.14	The $f_1(\Delta I)$ "positive" slope shall be +4.11% / % ΔI .							
	2.9.15	The f_1 (ΔI) "negative" slope shall be - 3.35% / % ΔI .							

2.10	Reactor Trip System Overpower <u>AT Setpoint Parameter Values</u> (LCO 3.3.1)	
	2.10.1	The Overpower ΔT reactor trip setpoint K_4 shall be equal to 1.072.
	2.10.2	The Overpower ΔT reactor trip setpoint T_{avg} rate/lag coefficient K_s shall be equal to 0.02 / °F for increasing T_{avg} .
	2.10.3	The Overpower ΔT reactor trip setpoint T_{avg} rate/lag coefficient K_5 shall be equal to 0 / °F for decreasing T_{avg} .
	2.10.4	The Overpower ΔT reactor trip setpoint T_{avg} heatup coefficient K_6 shall be equal to 0.00245 / °F when $T > T''$.
	2.10.5	The Overpower ΔT reactor trip setpoint T_{avg} heatup coefficient K_6 shall be equal to 0 / °F when $T \leq T''$.
	2.10.6	The nominal T_{avg} at RTP (indicated) T" shall be less than or equal to 588.4 °F.
	2.10.7	The measured reactor vessel ΔT lead/lag time constant τ_1 shall be equal to 8 sec.
	2.10.8	The measured reactor vessel ΔT lead/lag time constant τ_2 shall be equal to 3 sec.
	2.10.9	The measured reactor vessel ΔT lag time constant τ_3 shall be less than or equal to 2 sec.
	2.10.10	The measured reactor vessel average temperature lag time constant τ_{6} shall be less than or equal to 2 sec.
	2.10.11	The measured reactor vessel average temperature rate/lag time constant τ_7 shall be equal to 10 sec.
	2.10.12	The $f_2(\Delta I)$ "positive" breakpoint shall be 0 for all ΔI .
	2.10.13	The $f_2(\Delta I)$ "negative" breakpoint shall be 0 for all ΔI .
	2.10.14	The $f_2(\Delta I)$ "positive" slope shall be 0 for all ΔI .
	2.10.15	The $f_2(\Delta I)$ "negative" slope shall be 0 for all ΔI .

- 2.11 Reactor Coolant System (RCS) DNB Parameter Limits (LCO 3.4.1)
 - 2.11.1 The pressurizer pressure shall be greater than or equal to 2219 psig.
 - 2.11.2 The RCS average temperature (T_{avg}) shall be less than or equal to 591.2 °F.
 - 2.11.3 The RCS total flow rate shall be greater than or equal to 371,400 gpm.

2.12 Boron Concentration

غ يو جو يو

- 2.12.1 The refueling boron concentration shall be greater than or equal to 2000 ppm. (LCO 3.9.1)
- 2.12.2 The Reactor Coolant System boron concentration shall be greater than or equal to 1919 ppm to maintain adequate shutdown margin for MODES 3, 4, and 5 during performance of rod drop time measurements and during the surveillance of Digital Rod Position Indication (DRPI) for OPERABILITY. (TLCO 3.1.g and TLCO 3.1.k)