

From: "Tom Thompson" <TThompson@nacintl.com>
To: Tim McGinty <TJM1@nrc.gov>
Date: Mon, Jun 12, 2000 7:14 AM
Subject: Re: Maine Yankee submittal dated 5/31/00

Tim,

I am forwarding these to Jim Ballowe and Mike Yaksh for responses and SAR changed pages ASAP.

I would note with respect to the SA182 (forging) and SA240 (plate) material; they are both Type 304 austenitic stainless steel and thus, there is no concern for a ductile to brittle transition. The NAC note requires that the ultimate and yield strengths of the materials be at least equal, so no concerns for the analysis.

Tom

Tim McGinty <TJM1@nrc.gov>
06/11/00 07:34 PM

To: TThompson@nacintl.com
cc:
Subject: Maine Yankee submittal dated 5/31/00

Tom:

I received the following from David Tang regarding the 5/31/00 Maine Yankee submittal. I believe we should connect Mike Y and David to make sure we are on the same page, in particular with regard to the fracture toughness of the alternate material, David thinks it is important with respect to the critical flaw size determination. I also think we should talk about Item 5. I'll be in tomorrow (Monday), but I have a doctor's appointment at 3.

Tim

Review Comments on SAR Revision UMSS-00D, Dated 5/31/00

1. Is the fracture toughness of the alternate material SA182 comparable to that of SA240 for its effects on determining critical flaw sizes for the TSC closure plate?

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2. On SAR page 3.3-2, revise the retaining ring bolts material to ASTM A193, Grade B6 high alloy steel.

3. The pad and foundation parameters shown SAR page 11.2.15-4 are those for UMS. They should be called out in SAR Subsection 11.2.12. Since both Section 12, B3.4.1 and B3.4.2 are revised, there are two sets of parameters to be called out in the SAR text. One for UMS and another for MY. Also, the parameters are for tip-over analysis only. The case for end drop has not been analyzed in the SAR because of the unyielding surface assumption for the 24-inch vertical drop analysis.

4. In Subsection 9.2.4, add a description of transfer cask periodic inspection program to ensure trunnion welds are not damaged after repeated use. Use ANSI N14.6 standards, as appropriate. (This is being addressed for the UMS rulemaking)

5. In Subsection 11.2.16, for the damaged fuel assembly with missing grid spacers, the side impact stress evaluation should consider the cladding stress components due to rod internal pressure, similar to that addressed in LLNL Report 21246, in which the failure criteria may not have to be based on the maximum shear theory.

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CC: "Mike Yaksh" <MYaksh@nacintl.com>