

April 9, 1992

11/25/92

Docket Nos. 50-412
Serial No. BV-92-017

Mr. J. D. Sieber, Vice President
Nuclear Group
Duquesne Light Company
Post Office Box 4
Shippingport, Pennsylvania 15077-0004

Dear Mr. Sieber:

SUBJECT: AMENDMENT NO. 42 - CORRECTION (TAC NO. M81759)

On March 2, 1992, the Commission issued Amendment No. 42 to Facility Operating License No. NPF-73 for the Beaver Valley Power Station, Unit 2. Amendment 42 modified Technical Specification Page 2-7, Table 2.2-1.

It has come to our attention that the amendment designation was inadvertently added to Page 2-8. The enclosed replacement page 2-8 should be substituted for that previously issued.

Sincerely,

Original signed
by

Albert W. De Agazio, Sr. Project Manager
Project Directorate I-4
Division of Reactor Projects - I/II
Office of Nuclear Reactor Regulation

Enclosure:
As stated

cc w/enclosure:
See next page

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Mr. J. D. Sieber
Duquesne Light Company

Beaver Valley Power Station
Units 1 & 2

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TABLE 2.2-1 (Continued)

REACTOR TRIP SYSTEM INSTRUMENTATION TRIP SETPOINTS
NOTATION (Continued)

T	=	Average temperature, °F;
$\frac{1}{1 + \tau_6 s}$	=	Lag compensator on measured T_{avg} ;
τ_6	=	Time constant utilized in the measured T_{avg} lag compensator, $\tau_6 = 0$ s;
T'	=	$\leq 576.2^\circ\text{F}$ (Nominal T_{avg} at RATED THERMAL POWER);
K_3	=	0.00082;
P	=	Pressurizer Pressure, psig;
P'	=	2235 psig (Nominal RCS operating pressure);
S	=	Laplace transform operator, s^{-1} ;

and $f_1(\Delta I)$ is a function of the indicated difference between top and bottom detectors of the power-range nuclear ion chambers; with gains to be selected based on measured instrument response during plant startup tests such that:

- (i) For $q_t - q_b$ between -33% and +9%, $f_1(\Delta I) = 0$, where q_t and q_b are percent RATED THERMAL POWER in the top and bottom halves of the core respectively, and $q_t + q_b$ is total THERMAL POWER in percent of RATED THERMAL POWER;
- (ii) For each percent that the magnitude of $q_t - q_b$ exceeds -33%, the ΔT Trip Setpoint shall be automatically reduced by 2.52% of its value at RATED THERMAL POWER; and
- (iii) For each percent that the magnitude $q_t - q_b$ exceeds +9%, the ΔT Trip Setpoint shall be automatically reduced by 1.75% of its value at RATED THERMAL POWER.

NOTE 2: The channel's maximum Trip Setpoint shall not exceed its computed Trip Setpoint by more than 1.6% of ΔT span.

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TABLE 2.2-1 (Continued)

REACTOR TRIP SYSTEM INSTRUMENTATION TRIP SETPOINTS
NOTATION

NOTE 1: OVERTEMPERATURE ΔT

$$\Delta T \frac{(1 + \tau_1 S)}{(1 + \tau_2 S)} \left(\frac{1}{1 + \tau_3 S} \right) \leq \Delta T_0 \left\{ K_1 - K_2 \frac{(1 + \tau_4 S)}{(1 + \tau_5 S)} \left[T \left(\frac{1}{1 + \tau_6 S} \right) - T' \right] + K_3 (P - P') - f_1 (\Delta T) \right\}$$

Where: ΔT = Measured ΔT ;

$\frac{1 + \tau_1 S}{1 + \tau_2 S}$ = Lead-lag compensator on measured ΔT ;

τ_1, τ_2 = Time constants utilized in lead-lag compensator for ΔT , $\tau_1 = 8$ s, $\tau_2 = 3$ s;

$\frac{1}{1 + \tau_3 S}$ = Lag compensator on measured ΔT ;

τ_3 = Time constants utilized in the lag compensator for ΔT , $\tau_3 = 0$ s;

ΔT_0 = Indicated ΔT at RATED THERMAL POWER;

K_1 = 1.28;

K_2 = 0.0183/ $^{\circ}F$

$\frac{1 + \tau_4 S}{1 + \tau_5 S}$ = The function generated by the lead-lag compensator for T_{avg} dynamic compensation;

τ_4, τ_5 = Time constants utilized in lead-lag compensator for T_{avg} , $\tau_4 = 30$ s, $\tau_5 = 4$ s;