

**RIO ALGOM MINING CORP.
SMITH RANCH PROJECT**

**WDEQ PERMIT #633
NRC LICENSE SUA-1548
DOCKET 40-8964**

**WELLFIELD 4 ANNEX
VOLUME 1**

**PRE-OPERATIONAL DATA
SUBMITTAL**

JUNE 1, 2000

**ATTACHMENT K
SMITH RANCH FACILITY
M SAND WELLFIELD 4A
MULTI-WELL PUMP TESTS**

FOR:

**WDEQ/LQD
PERMIT #633
NRC LICENSE SUA-1548
DOCKET 40-8964**

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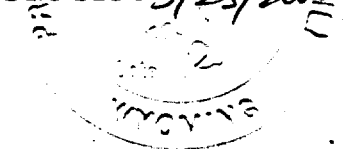


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K.1.0 INTRODUCTION, OBJECTIVES AND SUMMARY

As required by Rio Algom's Smith Ranch Project Permit #633 and NRC License SUA-1548, a pump test for each well field is required prior to operation. This report for Wellfield 4A discusses the pump tests performed to meet this requirement. The report is submitted for inclusion as Attachment K in Appendix D-6 of the DEQ permit application dated March 30, 1988.

The objectives of the pre-operational pump test as stated in Chapter 5 of the DEQ permit are to:

- 1) demonstrate communication between the area to be mined and the surrounding monitor ring;
- 2) determine the degree of hydrologic communication between the production zone and the overlying (O Sand) and the underlying (K Sand) aquifers;
- 3) determine the hydrologic properties of the production zone aquifer;
- 4) determine the presence of any hydrologic barriers.

In order to meet these objectives, two pump tests were performed in November and December of 1999. The first test, the PW4-4 test, was designed to define the southeastern half of Wellfield 4A. The second test, the PW4-3 test, was designed to define the northwestern half of Wellfield 4A. The PW4-4 test was conducted over the six days between November 5 and November 11, 1999. Pre-test data was collected for 3 days prior to the initiation of each test. Well PW4-4 was pumped for 72 hours and recovery was observed for 72 hours. The PW4-3 test was conducted over an eight-day period with well PW4-3 being pumped for 96 hours and

recovery observed for 96 hours. The PW4-3 test was conducted from November 29 through December 7, 1999.

Test results clearly demonstrate communication between the production zone and the outlying monitor wells, except for the three northwestern monitoring ring wells. These three wells showed good communications with Wellfield 4 in its multi-well test. The influence of operations in Wellfield 4 extend beyond wells M401, M402 and M434 to the southeast and, therefore, demonstrate that the M Sand near these three wells is connected with the remainder of the Wellfield 4A M Sand to the southeast. A few M Sand wells were used in both multi-well tests to demonstrate continuity between the two tests. These tests also demonstrate that there is no measurable communication across the aquitards with the overlying O Sand and underlying K Sand aquifers. Hydrologic properties and the lack of boundaries are discussed in detail in the body of this report.

K.1.1 SUMMARY OF TEST RESULTS

Two multi-well pump tests were conducted in the Wellfield 4A area. The PW4-3 and PW4-4 multi-well pump tests consisted of four and three day pumping phases and four and three days of recovery from pumping, respectively. Pumping well PW4-4 demonstrated communication with all of the southeastern monitoring ring wells. Pumping of well PW4-3 proved good communication with all of the northwestern monitoring ring wells. However, wells M401, M402 and M434, which are adjacent to Wellfield 4, had a subdued response due to interference caused by Wellfield 4 activities. Good communication between the well field patterns and the

monitor ring in this area is demonstrated by: 1) the influence of activities in Wellfield 4 during the Wellfield 4A pump test extended beyond M401, M402, and M434 into Wellfield 4A, 2) the previous Wellfield 4 pump test showed good drawdown in M401, M402 and M434, and 3) the M Sand isopach map (Figure K.2-10) shows a continuous production sand in this area. Results of these two multi-well tests are presented in Sections K.5 and K.6, respectively. Two monitoring ring wells were used in both tests to demonstrate continuity between the two tests. These wells demonstrate that all of the monitoring ring wells are in communication with the M Sand in the mine area.

Both of the multi-well pump tests demonstrated good confinement between the overlying O Sand and the M Sand production zone and between the underlying K and M Sands in Wellfield 4A.

No boundaries within the M Sand were detected by either test in Wellfield 4A. The M Sand inside of Wellfield 4A has a low transmissivity compared to the Wellfield 4 values, except near the northwestern boundary of Wellfield 4A where the transmissivity increases toward the higher Wellfield 4 value.

An average transmissivity of 160 gal/day/ft for the M Sand is thought to be representative of the majority of Wellfield 4A. A storage coefficient of 3.5E-05 and a hydraulic conductivity of 0.84 ft/day (0.26 Darcy) are representative of the M Sand aquifer in Wellfield 4A.

K.1.2 SITE LOCATION

Rio Algom Mining Corp.'s Smith Ranch Wellfield 4A is located in the southern Powder River Basin in Section 35, Township 36N, Range 74W and Section 2,

Township 35N, Range 74W in Converse County, Wyoming. The project is about 30 miles north of Douglas and 20 miles northeast of Glenrock. Figure K.2-1 shows the location of Wellfield 4A and shows the location of the wells used in these pump tests. Wellfield 4A will be connected through a pipeline to only the Central Processing Plant.

K.1.3 TEST OBJECTIVES

The objectives of the Wellfield 4A multi-well pump tests were to 1) demonstrate communication between the area to be mined (production area) and the surrounding monitoring ring; 2) determine the degree of hydrologic communication between the production zone and the overlying (O Sand) and underlying (K Sand) aquifers; 3) determine the presence of hydrologic boundaries; and 4) determine hydrologic properties of the production zone aquifer. Three day and four day (pumping) multi-well pump tests were conducted to obtain these objectives.

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K.2.0 GEOLOGIC CONDITIONS AND WELL COMPLETIONS

K.2.1 GEOLOGIC CONDITIONS

The well locations used in the Wellfield 4A pump tests are shown in blue on Figure K.2-1. Figure K.2-2 portrays the Wellfield 4A cross-section index map. This map depicts locations of the generalized cross-sections that portray the geologic conditions of the M Sand in the Fort Union formation. The M Sand is a braided stream deposit as thick as 125 ft. and as thin as 55 ft. that averages 81 ft. in thickness in Wellfield 4A.

Depending on locations across the well field, the entire M Sand interval may be divided into three separate segments, due to interbedded shale lenses. These shale lenses range from 5 to 46 ft. thick and isolate mineralization within the middle segment of the M Sand that makes it respond as a separate aquifer in Wellfield 4A. The shale between the upper and middle M Sand segments is present throughout this area and functions as an aquitard across Wellfield 4A. Therefore, only the middle segment of the entire M Sand sequence depicted on the cross section is used in the multi-well tests because this is the only portion of the M Sand where production recovery and injection wells will be completed. The three separate M Sand segments do not coalesce into a single homogeneous sand package as seen to the west in Wellfield 4. However, the upper and lower segments of the M Sand are not continuous throughout Wellfield 4A, as seen on Figures K.2-9A, B and C. The lower M Sand segment is shaded out on the southeast end of the Wellfield 4A in the region of logs 309 and MP428 (Figure K.2-9C). The upper M Sand segment is shaded out from the western side of Wellfield 4A eastward to log 993 (Figure K.2-9C) where the upper part of the M Sand segment is present.

Overlying the M Sand is the massive and ubiquitous O Sand aquifer that averages 298 ft. thick in Wellfield 4A. The underlying aquifer is the K Sand. Insufficient, penetrating data is available to estimate the average thickness of the K Sand. The N Shale aquitard separates the M Sand from the O Sand while the L Shale aquitard separates the M Sand from the K Sand. The N Shale thickness ranges from 4 ft. to 67 ft. and averages 31 feet across Wellfield 4A. Both multi-well pump tests indicated no hydrologic communication between the M and O Sands. The L Shale thickness ranges from 24 ft. to 97 ft. thick, averaging 41 ft. and, based on geologic information, is continuous across the well field. These two multi-well pump tests show that no hydrologic communication exists between the M and K Sands in Wellfield 4A. Figures K.2-10 through Figure K.2-13 are isopach maps that illustrate the thickness of these sand and shale units.

Seven generalized cross-sections were constructed to illustrate the geology of Wellfield 4A. Figure K.2-3 depicts the exterior monitor wells looking clockwise from the inside the well field outward. This section illustrates the areal extent of thickness changes in the M Sand throughout Wellfield 4A. The thickness of the M Sand varies due to the presence or absence of the lower and upper M Sand. The greatest thickness of the M Sand is toward the southeastern portion of the well field in the region of M449 where the lower, middle and upper sands are present. The N and L Shales are competent aquitards in all exterior monitor wells.

Cross-section A-A' (Figure K.2-4) is a northeast-southwest section looking southeast. The N and L Shales are competent and continuous throughout this section. The middle and lower M Sand is present in this section but the upper M Sand is missing. The top of the K Sand is relatively constant throughout the area.

Cross-section B-B' (Figure K.2-5) is a northeast-southwest section looking southeast. The thickness of the M Sand is relatively constant. The N and L Shales are competent and continuous throughout this section while the top of the K is present only in log MD414.

Cross-section C-C' (Figure K.2-6) is a northeast-southwest section looking southeast. The thickness of the total M Sand is thin on the north side relative to the area beginning at log 1150 where it thickens due to the presence of the upper M Sand. The N Shale remains competent throughout the area but thins on the south due to the presence of the upper M Sand. The top of the K Sand is seen in two of the logs illustrating a good, competent L Shale aquitard.

Cross-section D-D' (Figure K.2-7) is a northeast-southwest section looking southeast. The thickness of the total M Sand is thicker on the north due to the presence of all three segments of the M Sand and thins to the south in the region of MD416 where the lower M Sand segment shales out. The N Shale is competent throughout the area. The top of the K Sand is projected in several of the logs illustrating a good, competent L Shale aquitard.

Cross-section E-E' (Figure K.2-8) is a northeast-southwest section looking southeast. The total thickness of the M Sand is thicker on the north due to the presence of all three segments of the M Sand and thins to the south in the region of log 354 where the lower M Sand segment shales out. The N Shale is competent and continuous throughout the area. The top of the K Sand is projected in several of the logs illustrating a good, competent L Shale aquitard.

Cross-sections F1-F4 (Figures K.2-9A, K.2-9B and K.2-9C) are northwest-southeast sections through the middle of the well field looking northeast. This section illustrates the variable thickness of the entire M Sand. The N Shale is a competent

aquitard with an average thickness of 31 ft. throughout the well field. The N Shale thins slightly on the southeast end of the well field starting at log 993 where the upper M Sand is present. Here, the aquitard is still consistent across this portion of the well field. This is supported by both the presence of competent N Shale in the well logs and the pump test data that demonstrates the absence of any drawdown in the overlying O Sand. As seen in cross section F3-F4 (Figure K.2-9C), the shale between the upper and middle M Sand members coalesces into the N Shale in the vicinity of MP425 and log 993, providing a continual aquitard between the middle M and the O Sands. The upper M Sand, when present, is generally separated from the middle M Sand by an aquitard ranging from 11 to 46 ft. thick and averages 27 ft. The lack of mineralization in the upper M Sand indicates that this shale is continuous in the Wellfield 4A area. The entire M Sand package can be seen in logs 993 and 309 (Figure K.2-9C).

K.2.2 WELL COMPLETIONS

K.2.2.1 PUMPING WELL COMPLETIONS

PW4-4

PW4-4, the pumping well on the southeastern portion of Wellfield 4A, intersects a complex section of the M Sand (Figure K.2-9C). At this location there are two interbedded shale lenses (55 ft. of shale overlies the middle M Sand segment, 65 ft. of shale underlies the middle M Sand segment), that separates the M Sand into the upper and middle segments. The lower M Sand segment has been shaled out in this area. The upper M Sand segment is barren of mineralization and the production interval is limited to the middle M Sand segment. In order to meet the requirements outlined in Section 5.1.2 of the Permit to Mine #633, the production zone monitor wells in this area are completed through the middle segment of the M Sand only. To maintain

compliance with the permit requirements, the completion interval of PW4-4 corresponds directly to the adjacent production zone monitor wells, and was not completed through the upper segment of the M Sand.

PW4-3

The stratigraphy intersected by pump well PW4-3 (Figure K.2-9B) in the western portion of Wellfield 4A consists of the middle and lower segments of the M Sand with the upper M Sand segment shaled out in this region. PW4-3 is only completed in the middle M Sand segment that contains mineralization and does not include the barren lower M Sand segment. The N Shale aquitard is 45 feet thick at well PW4-3. The lower aquitard, or L Shale averages a thickness of 31 ft.

K.2.2.2 PRODUCTION ZONE WELLS AND PERIMETER MONITOR WELLS

The perimeter monitor ring wells (M) consist of twenty-seven M Sand wells that were measured to demonstrate communication with the production zone. Fifteen wells, M439 through M453, were measured during the PW4-4 test. Fourteen wells, M401, M402, M434 through M439 and M453 through M458, were measured during the PW4-3 pump test. Wells M439 and M453 were measured during both tests. Table K.2-1 presents the well completion data information for all monitor wells in Wellfield 4A. In addition, the completion intervals are illustrated on the monitor ring cross-section.

Twelve production zone (M Sand) monitor wells were used to define the aquifer properties. These wells are completed in the mineralized portion of the middle M Sand segment and are designated as "MP" wells. Seven wells, MP425 through MP431, were measured during the first pump test. Seven wells, M401, MP422 through MP426 and MP432 were measured during the second pump test. Wells MP425 and MP426 were measured during both pump tests for continuity and overlap between test areas. Many

of the MP wells were used in the construction of the generalized cross sections. The cross sections illustrate the completion of the MP wells throughout the production zone.

K.2.2.3 ADJACENT AQUIFER MONITOR WELLS

Six overlying monitor wells (MS) and six underlying monitor wells (MD) were installed throughout Wellfield 4A. The MS/MD wells were drilled in pairs in every case in Wellfield 4A so that MS415 corresponds to MD415, respectively. Figure K.2-1 illustrates the location of all monitor wells monitored during the pump tests. Specific wells MS/MD415 through MS/MD417 were monitored during the first pump test. During the second pump test, wells MS/MD412 through MS/MD415 were monitored. For continuity and overlap between both test areas, wells MS/MD415 were monitored in both pump tests.

K.2.3 GEOLOGY OF THE WELLFIELD 4A AQUITARDS

K.2.3.1 GEOLOGY OF THE N SHALE AQUITARD

The N Shale was deposited laterally away from the main channel system as a distal overbank facies resulting in an aquitard of regional extent that separates the overlying O Sand from the M Sand system. The N Shale thickness ranges between 4 ft. to 67 ft. and averages 31 ft. in thickness throughout the well field.

The thickness of the N Shale depends on the presence of the upper M Sand segment, as illustrated in all cross-sections and the N Shale and M Sand isopach maps. When the upper M Sand segment is present, the N Shale thickness ranges from 4 ft. to 25 ft., while averaging 13 ft. in Wellfield 4A. In areas where the upper M Sand segment is shaled out, an interbedded shale in the M Sand coalesces into the N Shale, that generates a thicker aquitard ranging from 28 ft. to 67 ft. with an average thickness

of 47 ft. in Wellfield 4A. The integrity of the N Shale to act as an aquitard between the M and O Sand packages is very good. Geologic logs and the results from both multi-well pump tests support this conclusion.

K.2.3.2 GEOLOGY OF THE L SHALE AQUITARD

The L Shale was deposited laterally away from the main channel system as a distal overbank facies resulting in an aquitard of regional extent that separates the M Sand system from the underlying K Sand. The L Shale ranges from 24 to 97 ft. thick and averages 41 ft. in Wellfield 4A.

K.2.3.3 DEPOSITIONAL HISTORY

The primary host for mineral deposition in the Smith Ranch region is the Paleocene Fort Union formation. The Fort Union formation is a braided fluvial, depositional system composed of interbedded sandstones and shales. The source of sand was from regional uplift and erosion of bordering mountains to the south and west. This erosion from the highlands formed a large alluvial plain that extended out into the Powder River Basin. These braided stream systems took shifting courses off the highlands and are reflected as separate pulses of sand deposition. The interbedded shales formed as distal overbank facies that graded laterally away from the major stream sediment loads dispensed off the areas of regional uplift.

The production in Wellfield 4A is in the M Sand, which is a specific, braided, fluvial sandstone unit. The M Sand is irregular with variable sand thickness, grain size, and shale content, that is characteristic of many production host sand units in the South Powder River Basin. The L and N Shales are ubiquitous facies within the Smith Ranch

Permit area. They were most likely deposited laterally away from major braided channel systems as distal overbank facies.

As stated previously, the provenance for sand deposition is from the south and west. Braided river systems flowing off the adjacent regional highlands carried large volumes of sediment toward the northwest-southeast trending axis of the Powder River Basin. Near the headwaters, the fluvial system is able to carry more sediment load due to the increased energy profile. As the braided system extends further from the headwaters, the energy of the fluvial system is reduced due to the decreased stream gradient caused by decreased elevation changes. Fluvial erosion is more active proximal to the headwaters with elevated energy profiles thus creating an elevation gradient that tapers away from the headwaters that results in a reduction of sediment transport over distance from the source area. Evidence for this gradual change in elevation may be observed on the elevation contour maps for the tops of the individual sand and shale units (Figures K.2-14 through K.2-18). These maps suggest a gentle elevation climb approaching the headwaters toward the south and west.

TABLE K.2-1. SUMMARY OF WELL COMPLETION INFORMATION FOR WELLFIELD 4A.

WELL NO.	EAST COORD.	NORTH COORD.	DRILLED DEPTH (FT)	CASING DEPTH (FT)	SCREENED INTERVAL (FT)	MEASURING POINT (MP)		DRIFT	
						ELEVATION (FT-MSL)	ABOVE LSD (FT)	DISTANCE	AZ
M SAND AQUIFER									
PW4-3	355491.5	867005.6	779.7	749	751-777	5411.8	0.76	4.6	183.8
PW4-4	357284.6	865229.7	760.3	725	727-747	5382.3	1.28	3.8	288.2
M401	354371.9	867581.8	841.0	757	759-782	5439.7	0.67	1.9	352.0
M402	354511.4	868038.9	837.0	764	766-789	5444.3	0.91	10.4	257.0
M434	354092.6	867226.0	844.0	780	782-811	5458.5	0.94	1.8	10.1
M435	354435.6	866982.8	853.0	795	797-825	5464.0	1.99	12.1	160.0
M436	354886.1	866798.0	823.0	767	769-791	5432.8	0.82	5.9	77.3
M437	355223.7	866469.5	813.0	763	765-788	5424.0	1.04	14.0	223.0
M438	355567.6	866147.5	795.0	757	759-781	5417.1	1.12	6.0	160.0
M439	355808.0	865737.2	781.0	746	748-765	5403.2	1.15	3.6	269.0
M440	356171.4	865431.1	778.0	728	730-751	5391.9	0.91	8.3	223.8
M441	356550.8	865148.5	773.0	725	727-748	5385.2	1.24	4.5	145.0
M442	356929.9	864863.3	772.0	737	739-752	5382.6	1.60	0.8	263.0
M443	357123.8	864430.5	791.0	733	735-750	5378.3	0.29	17.0	232.0
M444	357319.8	863997.1	791.0	745	747-762	5393.1	1.12	0.5	78.4
M445	357760.2	863824.6	777.0	745	747-761	5390.3	1.32	8.3	221.5
M446	358170.7	864055.6	770.2	716	718-733	5368.0	2.04	6.2	165.4
M447	358413.0	864374.8	783.0	719	721-737	5375.9	0.93	14.7	218.0
M448	358482.9	864870.3	800.0	755	757-773	5412.9	0.87	17.2	259.0
M449	358167.9	865259.5	831.0	752	754-770	5412.7	0.74	1.9	295.0
M450	357803.4	865601.3	793.2	753	755-763	5407.8	0.83	6.8	170.1
M451	357350.5	865800.6	814.0	773	775-791	5435.0	0.97	16.5	217.0
M452	357169.4	866255.8	832.0	774	776-796	5438.4	0.37	20.1	303.0
M453	356847.2	866570.3	800.0	749	751-769	5410.5	1.51	6.7	309.0
M454	356454.5	866825.6	794.0	745	747-765	5408.1	1.10	16.1	256.0
M455A	356141.9	867156.1	797.0	751	753-778	5409.8	0.75	3.9	5.8
M456	355766.1	867485.5	820.0	777	779-794	5430.0	0.98	13.0	244.0
M457	355431.7	867811.1	815.1	763	765-779	5422.6	0.63	11.9	208.0
M458	354975.0	867959.7	821.2	752	754-782	5426.0	0.97	6.2	60.1
MP422	355198.7	867355.8	780.7	754	756-775	5416.2	1.23	8.3	288.7
MP423	355715.6	866876.8	797.1	754	756-774	5409.3	1.25	10.7	213.4
MP424	356071.4	866494.5	779.1	746	748-764	5402.6	0.63	8.7	272.6
MP425	356631.0	865868.3	794.8	760	762-775	5419.0	1.96	18.0	176.7
MP426	356461.4	866156.9	775.3	742	744-763	5405.0	1.04	7.2	5.0
MP427A	356876.0	865558.7	780.8	741	743-756	5397.9	0.87	11.7	230.8
MP428	357207.0	865288.2	766.0	735	737-748	5385.7	1.65	6.7	156.0
MP429	357546.2	865056.8	777.0	730	732-742	5382.1	1.10	15.2	144.9
MP430	357698.0	864936.5	781.3	726	728-744	5381.3	0.29	2.5	307.5
MP431	357707.7	864660.3	757.0	715	717-735	5371.0	1.03	3.9	215.3
MP432	354891.3	867448.4	805.0	749	751-772	5420.5	0.48	0.7	346.6

TABLE K.2-1. SUMMARY OF WELL COMPLETION INFORMATION FOR WELLFIELD 4A. (cont'd.)

WELL NO.	EAST COORD.	NORTH COORD.	DRILLED DEPTH (FT)	CASING DEPTH (FT)	SCREENED INTERVAL (FT)	MEASURING POINT (MP)		DRIFT	
						ELEVATION (FT-MSL)	ABOVE LSD (FT)	DISTANCE	AZ
<u>K SAND AQUIFER</u>									
MD412	354558.4	867531.1	941.0	871	873-892	5432.1	0.07	11.4	109.5
MD413	355357.6	867162.5	896.0	853	855-875	5413.9	0.85	8.6	213.0
MD414	355956.8	866546.4	904.2	843	845-865	5404.2	0.17	9.3	212.7
MD415	356656.5	866009.8	915.0	864	866-886	5421.7	1.74	15.1	183.0
MD416	357259.2	865232.7	902.0	818	820-840	5381.5	0.53	15.4	264.1
MD417	357876.8	864575.1	901.1	828	830-850	5368.6	0.63	10.8	209.8
<u>Q SAND AQUIFER</u>									
MS412	354549.4	867531.4	721.0	688	690-709	5432.5	0.49	8.5	151.2
MS413	355364.1	867157.9	704.1	673	675-689	5414.4	1.37	8.8	238.3
MS414	355950.1	866551.9	704.2	659	661-681	5404.7	0.69	7.0	216.5
MS415	356655.0	866019.4	716.4	661	663-683	5421.6	1.64	7.0	215.3
MS416	357249.4	865234.6	675.0	634	636-656	5381.5	0.54	6.0	150.8
MS417	357869.0	864576.9	660.0	619	621-637	5368.8	0.77	5.5	260.3

**TABLE K.2-2. WELLFIELD 4A SAND THICKNESS
AND COMPLETION INTERVALS.**

MONITOR WELL	SAND THICKNESS (FT)	COMPLETION INTERVAL	
		TOP	BOTTOM
<u>M SAND AQUIFER</u>			
PW4-3	NFP	751	777
PW4-4	75	727	747
M401	79	759	782
M402	67	766	789
M434	NFP	782	811
M435	NFP	797	825
M436	NFP	769	791
M437	NFP	765	788
M438	NFP	759	781
M439	NFP	748	765
M440	NFP	730	751
M441	78	727	748
M442	76	739	752
M443	78	735	750
M444	80	747	762
M445	78	747	761
M446	77	718	733
M447	76	721	737
M448	NFP	757	773
M449	110	754	770
M450	NFP	755	763
M451	NFP	775	791
M452	55	776	796
M453	NFP	751	769
M454	NFP	747	765
M455A	NFP	753	778
M456	NFP	779	794
M457	NFP	765	779
M458	NFP	754	782
MP422	NFP	756	775
MP423	NFP	756	774
MP424	NFP	748	764

**TABLE K.2-2. WELLFIELD 4A SAND THICKNESS
AND COMPLETION INTERVALS. (cont'd).**

MONITOR WELL	SAND THICKNESS (FT)	COMPLETION INTERVAL	
		TOP	BOTTOM

M SAND AQUIFER (cont'd.)

MP425	NFP	762	775
MP426	NFP	744	763
MP427A	NFP	743	756
MP428	67	737	748
MP429	77	732	742
MP430	85	728	744
MP431	68	717	735
MP432	NFP	751	772

K SAND AQUIFER

MD412	NFP	873	892
MD413	NFP	855	875
MD414	NFP	845	865
MD415	NFP	866	886
MD416	NFP	820	840
MD417	NFP	830	850

O SAND AQUIFER

MS412	306	690	709
MS413	298	675	689
MS414	301	661	681
MS415	288	663	683
MS416	307	636	656
MS417	308	621	637

NOTE: NFP = Not fully penetrating
FT = Feet

**THIS PAGE IS AN
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FIG. 2.1.4
SMITH RANCH PROJECT
WELLFIELD 4 ANNEX
PLAN MAP
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DOCUMENT/REPORT
FIG. 2.1.4**

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D-1

**THIS PAGE IS AN
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FIG. K.2-1
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WELLFIELD 4 ANNEX
PLAN MAP
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FIG. K.2-1**

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D-2

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FIG. 2.10.4
SMITH RANCH PROJECT
WELLFIELD 4 ANNEX
BASELINE GAMMA SURVEY
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FIG. 2.10.4**

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D-3

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FIG. D-5.22
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WELLFIELD 4 ANNEX
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FIG. D-5.22**

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D-4

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FIG. K.2-2
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WELLFIELD 4 ANNEX
CROSS SECTION INDEX MAP
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DOCUMENT/REPORT
FIG. K.2-2**

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D-5

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THAT CAN BE VIEWED AT
THE RECORD TITLED:
FIG. K.2-3, FIG. D-5.23
SMITH RANCH PROJECT WELLFIELD
4 ANNEX
GEOLOGIC CROSS SECTION
MONITOR WELL RING LOOKING
OUTWARD CLOCKWISE
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BY SEARCHING USING THE
DOCUMENT/REPORT
FIG. K.2-3, FIG. D-5.23**

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D-6

**THIS PAGE IS AN
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THE RECORD TITLED:
FIG. K.2-4, FIG. D-5.24
SMITH RANCH PROJECT
WELLFIELD 4 ANNEX
GEOLOGIC CROSS SECTION A -
A' LOOKING SOUTHEAST
WITHIN THIS PACKAGE...OR,
BY SEARCHING USING THE
DOCUMENT/REPORT
FIG. K.2-4, FIG. D-5.24**

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D-7

**THIS PAGE IS AN
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OR FIGURE,
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THE RECORD TITLED:
FIG. K.2-5, FIG. D-5.25
SMITH RANCH PROJECT
WELLFIELD 4 ANNEX
GEOLOGIC CROSS SECTION
B - B' LOOKING SOUTHEAST
WITHIN THIS PACKAGE...OR,
BY SEARCHING USING THE
DOCUMENT/REPORT
FIG. K.2-5, FIG. D-5.25**

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D-8

**THIS PAGE IS AN
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THE RECORD TITLED:
FIG. K.2-6, FIG. D-5.26
SMITH RANCH PROJECT
WELLFIELD 4 ANNEX
GEOLOGIC CROSS SECTION
C - C' LOOKING SOUTHEAST
WITHIN THIS PACKAGE...OR,
BY SEARCHING USING THE
DOCUMENT/REPORT
FIG. K.2-6, FIG. D-5.26**

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D-9

**THIS PAGE IS AN
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THE RECORD TITLED:
FIG. K.2-7, FIG. D-5.27
SMITH RANCH PROJECT
WELLFIELD 4 ANNEX
GEOLOGIC CROSS SECTION
D - D' LOOKING SOUTHEAST
WITHIN THIS PACKAGE...OR,
BY SEARCHING USING THE
DOCUMENT/REPORT
FIG. K.2-7, FIG. D-5.27**

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D-10

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THE RECORD TITLED:
FIG. K.2-8, FIG. D-5.28
SMITH RANCH PROJECT
WELLFIELD 4 ANNEX
GEOLOGIC CROSS SECTION
E - E' LOOKING SOUTHEAST
WITHIN THIS PACKAGE...OR,
BY SEARCHING USING THE
DOCUMENT/REPORT
FIG. K.2-8, FIG. D-5.28**

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D-11

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FIG. K.2-9A, FIG. D-5.29
SMITH RANCH PROJECT WELLFIELD
4 ANNEX
GEOLOGIC CROSS SECTION
F1 - F2 (NORTHWEST) LOOKING
NORTHEAST
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FIG. K.2-9A, FIG. D-5.29**

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D-12

**THIS PAGE IS AN
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THE RECORD TITLED:
FIG. K.2 - 9B, FIG. D-5.30
SMITH RANCH PROJECT
WELLFIELD 4 ANNEX
GEOLOGIC CROSS SECTION F2
- F3 (MIDDLE)
LOOKING NORTHEAST
WITHIN THIS PACKAGE...OR,
BY SEARCHING USING THE
DOCUMENT/REPORT
FIG. K.2 - 9B, FIG. D-5.30**

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D-13

**THIS PAGE IS AN
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FIG. K.2 - 9C, FIG. D-5.31
SMITH RANCH PROJECT
WELLFIELD 4 ANNEX
GEOLOGIC CROSS SECTION F3
- F4 (SOUTHEAST)
LOOKING NORTHEAST
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DOCUMENT/REPORT
FIG. K.2 - 9C, FIG. D-5.31**

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FIG. K.2 - 10
SMITH RANCH PROJECT
WELLFIELD 4 ANNEX M
SAND ISOPACH
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FIG. K.2 - 10**

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D-15

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FIG. K.2 - 11
SMITH RANCH PROJECT
WELLFIELD 4 ANNEX
N SHALE ISOPACH
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FIG. K.2 - 11**

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D-16

**THIS PAGE IS AN
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FIG. K.2 - 12
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WELLFIELD 4 ANNEX
L SHALE ISOPACH
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FIG. K.2 - 12**

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D-17

**THIS PAGE IS AN
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THE RECORD TITLED:
FIG. K.2 - 13
SMITH RANCH PROJECT
WELLFIELD 4 ANNEX
O SAND ISOPACH
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FIG. K.2 - 13**

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D-18

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FIG. K.2 - 14
SMITH RANCH PROJECT
WELLFIELD 4 ANNEX
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FIG. K.2 - 14**

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D-19

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FIG. K.2 - 15
SMITH RANCH PROJECT
WELLFIELD 4 ANNEX
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DOCUMENT/REPORT
FIG. K.2 - 15**

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D-20

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FIG. K.2 - 16
SMITH RANCH PROJECT
WELLFIELD 4 ANNEX
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FIG. K.2 - 16**

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D-21

**THIS PAGE IS AN
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FIG. K.2 - 17
SMITH RANCH PROJECT
WELLFIELD 4 ANNEX
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FIG. K.2 - 17**

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D-22

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THE RECORD TITLED:
FIG. K.2 - 18
SMITH RANCH PROJECT
WELLFIELD 4 ANNEX
TOP OF K SAND
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FIG. K.2 - 18**

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D-23

**GRAPHICAL DATA
STRIPS EXIST AT
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DOCUMENT BUT
WERE NOT SCANNED
DUE TO THEIR
ABNORMAL SIZE.**

**PAPER VERSIONS
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NRC FILE CENTER.**

Rio Algom Mining Corp.

Smith Ranch Project

Wellfields 4 and 4A

Table L-1.2

MP Wells-Interior Ore Zone Baseline Water Quality Summary

Major Ions mg/L	Sample Count	Sample Count >DL	Mean	St. Dev.	Min. Value	Max. Value	K Factor	Lower Tol.	Upper Tol.	Target Restoration Value
Calcium	62	62	56.8	4.6	48.0	67.0	3.056	42.7	70.9	56.8
Magnesium	62	62	16.0	1.2	13.0	18.9	3.056	12.4	19.6	16.0
Sodium	62	62	24.1	2.2	21.8	29.1	3.056	17.5	30.7	24.1
Potassium	61	62	7.7	0.6	6.8	9.3	3.06	5.8	9.6	7.7
Carb	62	0	0.5	0.0	0.5	0.5	3.056	0.5	0.5	0.5
Bicarb	59	59	193.0	3.8	183.0	201.0	3.072	181.4	204.5	193.0
Sulfate	124	124	107	16	77	148	2.898	46	152	107
Chloride	122	122	3.6	0.9	1.6	6.0	2.896	1.1	6.1	3.6
Ammonium	61	48	0.08	0.04	0.03	0.21	3.06	-0.05	0.21	0.08
Nitrite+Nitrate	62	0	0.05	0.00	0.05	0.05	3.056	0.05	0.05	0.05
Fluoride	62	62	0.53	0.03	0.47	0.58	3.056	0.45	0.60	0.53
Silica	62	62	15.7	0.9	14.0	17.5	3.056	13.1	18.3	15.7
TDS	124	124	329	32	257	419	2.898	236	423	329
SC@25 - umoh/cm	124	124	499	26	449	555	2.898	423	576	499
Alkalinity	124	124	158	6	139	168	2.898	139	176	158
pH - SU	124	124	7.56	0.14	7.15	7.97	2.898	7.15	7.98	7.56

Trace Metals										
Arsenic	122	87	0.0019	0.0012	0.0005	0.0050	2.896	-0.0016	0.0053	0.0019
Boron	62	0	0.05	0.00	0.05	0.05	3.056	0.05	0.05	0.05
Cadmium	62	0	0.003	0.000	0.003	0.003	3.056	0.003	0.003	0.003
Chromium	62	0	0.03	0.00	0.03	0.03	3.056	0.03	0.03	0.03
Iron	58	14	0.03	0.02	0.03	0.10	3.077	-0.03	0.10	0.03
Manganese	62	21	0.01	0.00	0.01	0.01	3.056	0.01	0.01	0.01
Molybdenum	62	62	0.05	0.00	0.05	0.05	3.056	0.05	0.05	0.05
Selenium	123	0	0.0005	0.0000	0.0005	0.0005	2.9	0.0005	0.0005	0.0005
Vandium	62	62	0.05	0.00	0.05	0.05	3.056	0.05	0.05	0.05
Zinc	62	62	0.01	0.00	0.01	0.01	3.056	0.01	0.01	0.01

Radiometric										
U _{nat} - mg/L	117	117	0.0370	0.0226	0.0095	0.0990	2.909	-0.0287	0.1026	0.0370
Radium-228 - pCi/L	122	108	3.7	2.1	0.5	8.9	2.896	-2.5	9.9	3.7
Radium 226 - pCi/L	124	124	605.4	406.3	31.0	1700.0	2.898	-572.2	1783.0	605.4

Rio Algom Mining Corp.
Smith Ranch Project
Wellfield 4
Table L-2.1
M Wells

Well #	Date and Time Sampled	Ca mg/L	Mg mg/L	Na mg/L	K mg/L	CO3 mg/L	HCO3 mg/L	SO4 mg/L	Cl mg/L	NH4 mg/L	NO3+NO2 mg/L	F mg/L	SiO2 mg/L	TDS mg/L	SC@25 µmho/cm	Alkalinity mg/L	pH std.units	As mg/L	B mg/L	Cd mg/L	Cr mg/L	Fe mg/L	Mn mg/L	Mo mg/L	Se mg/L	V mg/L	Zn mg/L	Unat mg/L	Ra226 pCi/L	Ra228 pCi/L
1M453	2/24/00@1453	59.6	15.8	27.4	8.3	<1.0	195	98.0	4.0	0.05	<0.10	0.49	16.8	287	499	161	7.59	<0.001	<0.10	<0.005	<0.05	0.15	0.01	<0.10	<0.001	<0.10	<0.01	0.011	19.4	<1.0
2M453	3/9/00@1259	N/R	N/R	N/R	N/R	N/R	N/R	94.6	3.5	N/R	N/R	N/R	N/R	327	495	162	7.62	<0.001	N/R	N/R	N/R	N/R	N/R	N/R	<0.001	N/R	N/R	0.01	6.6	<1.0
3M453	3/22/00@0943	N/R	N/R	N/R	N/R	N/R	N/R	98.5	2.4	N/R	N/R	N/R	N/R	316	502	162	7.40	<0.001	N/R	N/R	N/R	N/R	N/R	N/R	<0.001	N/R	N/R	0.0109	6.6	<1.0
4M453	4/3/00@1224	57.3	14.9	26.1	8.5	N/R	199	90.9	4.1	0.11	N/R	0.52	15.0	313	499	164	7.42	<0.001	N/R	N/R	N/R	0.24	0.02	N/R	<0.001	N/R	N/R	0.0105	7.7	5.5
1M454	2/23/00@1438	51.1	13.8	24.3	7.7	<1.0	196	82.6	4.6	<0.05	<0.10	0.53	15.4	288	470	161	7.63	0.001	<0.10	<0.005	<0.05	0.20	0.01	<0.10	<0.001	<0.10	<0.01	0.012	8.3	1.5
2M454	3/8/00@1241	N/R	N/R	N/R	N/R	N/R	N/R	90.7	3.7	N/R	N/R	N/R	N/R	318	485	164	7.63	0.001	N/R	N/R	N/R	N/R	N/R	N/R	<0.001	N/R	N/R	0.006	10.2	<1.0
3M454	3/20/00@1221	N/R	N/R	N/R	N/R	N/R	N/R	92.5	3.3	N/R	N/R	N/R	N/R	308	492	161	7.36	0.001	N/R	N/R	N/R	N/R	N/R	N/R	<0.001	N/R	N/R	0.0073	8.8	<1.0
4M454	4/3/00@1137	55.6	14.5	25.8	8.4	N/R	197	87.9	6.9(1)	N/R	N/R	0.52	14.7	304	491	162	7.47	0.001	N/R	N/R	N/R	<0.05	0.01	N/R	<0.001	N/R	N/R	0.007	6.6	4.3
1M455A	2/23/00@1358	51.0	13.9	24.4	7.6	<1.0	197	83.2	5.2	0.05	<0.10	0.52	15.3	294	476	162	7.60	0.001	<0.10	<0.005	<0.05	0.10	0.01	<0.10	<0.001	<0.10	<0.01	0.008	13.8	<1.0
2M455A	3/8/00@1212	N/R	N/R	N/R	N/R	N/R	N/R	85.3	3.5	N/R	N/R	N/R	N/R	307	473	163	7.59	0.001	N/R	N/R	N/R	N/R	N/R	N/R	<0.001	N/R	N/R	0.0062	10.3	<1.0
3M455A	3/20/00@1113	N/R	N/R	N/R	N/R	N/R	N/R	85.9	2.9	N/R	N/R	N/R	N/R	307	480	162	7.34	0.001	N/R	N/R	N/R	N/R	N/R	N/R	<0.001	N/R	N/R	0.0074	8.4	<1.0
4M455A	4/3/00@1145	54.5	14.6	25.4	8.2	N/R	198	83.6	2.7	0.08	N/R	0.54	14.7	298	480	163	7.44	0.002	N/R	N/R	N/R	0.22	0.02	N/R	<0.001	N/R	N/R	0.0079	7.4	1.5
1M456	2.23/00@1417	52.0	13.8	24.6	8.1	<1.0	197	90.9	5.4	<0.05	<0.10	0.49	15.3	297	490	162	7.61	0.001	<0.10	<0.005	<0.05	0.12	0.01	<0.10	<0.001	<0.10	<0.01	0.0097	11.4	<1.0
2M456	3/8/00@1021	N/R	N/R	N/R	N/R	N/R	N/R	81.4	3.1	N/R	N/R	N/R	N/R	305	468	164	7.64	0.001	N/R	N/R	N/R	N/R	N/R	N/R	<0.001	N/R	N/R	0.0071	8.3	<1.0
3M456	3/20/00@0906	N/R	N/R	N/R	N/R	N/R	N/R	82.8	3.6	N/R	N/R	N/R	N/R	301	471	161	7.50	0.001	N/R	N/R	N/R	N/R	N/R	N/R	<0.001	N/R	N/R	0.0089	9.6	<1.0
4M456	4/3/00@0821	53.2	14.2	25.2	8.1	N/R	195	77.1	3.2	N/R	N/R	0.55	15.0	281	472	161	7.45	0.002	N/R	N/R	N/R	0.08	0.01	N/R	<0.001	N/R	N/R	0.0074	6.3	1.2
1M457	2/23/00@1113	47.5	13.0	23.0	7.3	<1.0	195	77.3	4.1	0.05	<0.10	0.53	14.8	276	462	161	7.63	<0.001	<0.10	<0.005	<0.05	0.09	0.01	<0.10	<0.001	<0.10	<0.01	0.013	16.8	2.6
2M457	3/8/00@1007	N/R	N/R	N/R	N/R	N/R	N/R	77.8	3.3	N/R	N/R	N/R	N/R	296	459	160	7.65	<0.001	N/R	N/R	N/R	N/R	N/R	N/R	<0.001	N/R	N/R	0.0082	11.6	1.7
3M457	3/20/00@0846	N/R	N/R	N/R	N/R	N/R	N/R	78.9	3.3	N/R	N/R	N/R	N/R	281	466	160	7.52	<0.001	N/R	N/R	N/R	N/R	N/R	N/R	<0.001	N/R	N/R	0.0086	9.0	<1.0
4M457	4/3/00@0809	51.2	13.8	24.3	7.7	N/R	197	77.8	4.0	0.10	N/R	0.55	14.8	283	464	162	7.44	<0.001	N/R	N/R	N/R	0.03	0.01	N/R	<0.001	N/R	N/R	0.0098	11.9	1.7
1M458	2/23/00@1054	48.8	13.5	23.4	7.4	<1.0	193	82.6	5.0	<0.05	<0.10	0.52	15.4	284	464	159	7.59	<0.001	<0.10	<0.005	<0.05	0.18	0.01	<0.10	<0.001	<0.10	<0.01	0.018	46.5	3.2
2M458	3/8/00@0955	N/R	N/R	N/R	N/R	N/R	N/R	81.1	3.3	N/R	N/R	N/R	N/R	297	464	160	7.61	<0.001	N/R	N/R	N/R	N/R	N/R	N/R	<0.001	N/R	N/R	0.0079	28.4	3.0
3M458	3/20/00@0847	N/R	N/R	N/R	N/R	N/R	N/R	80.2	3.1	N/R	N/R	N/R	N/R	302	468	160	7.50	<0.001	N/R	N/R	N/R	N/R	N/R	N/R	<0.001	N/R	N/R	0.0093	26.4	2.3
4M458	4/3/00@0759	53.3	14.9	25.3	7.2	N/R	196	78.4	2.3	N/R	N/R	0.54	16.4	289	468	161	7.36	<0.001	N/R	<0.005	N/R	0.05	<0.01	N/R	<0.001	N/R	N/R	0.0096	41.1	2.9

Rio Algom Mining Corp.

Smith Ranch Project

Table L-2.2

M Wells

Parameter	Units	Mean	Five Std. Dev.	Mean + 5 Std. Dev.	Adjustmen	Upper Control Limit
Chloride	mg/L	3.5	0.8	7.5	15	18.5
Total Alkalinity	mg/L	158	20	178	N/A	178
Specific Conductivity	umhos/cm	508	185	693	N/A	693

Rio Algom Mining Corp.
Smith Ranch Project
Table L-2.3
M Wells
Upper Control Limit Calculated

1M401	477	3.0	162	3M415	521	2.7	156	1M430	488	4.0	159
2M401	483	3.1	159	4M415	518	1.4	155	2M430	495	2.7	157
3M401	478	3.1	162	1M416	557	2.0	155	3M430	490	3.1	159
4M401	476	2.8	161	2M416	556	2.4	157	4M430	476	3.6	158
1M402	455	4.0	156	3M416	542	3.1	157	1M431	427	4.0	117(1)
2M402	454	3.4	155	4M416	540	1.8	157	2M431	455	3.1	130(1)
3M402	449	3.4	156	1M417	553	8.0(1)	148	3M431	470	3.8	142(1)
4M402	448	3.5	157	2M417	559	5.1	149	4M431	466	3.9	148
1M403	431	5.0	152	3M417	547	4.5	154	1M432	498	4.0	157
2M403	441	4.1	156	4M417	544	2.2	153	2M432	500	2.7	157
3M403	434	4.1	155	1M418A	533	5.0	148	3M432	497	3.8	156
4M403	431	3.8	153	2M418A	557	3.1	152	4M432	490	3.9	157
1M404	438	5.0	160	3M418A	554	3.4	151	1M433	517	4.0	160
2M404	440	2.7	161	4M418A	549	2.5	151	2M433	517	3.1	158
3M404	435	3.4	159	1M419	555	4.0	154	3M433	513	3.8	160
4M404	432	2.8	160	2M419	569	3.1	160	4M433	503	3.0	158
1M405	444	5.0	158	3M419	557	3.1	159	1M434	506	4.0	159
2M405	444	3.8	159	4M419	554	1.6	156	2M434	506	3.1	158
3M405	438	3.8	159	1M420	555	3.0	150	3M434	500	3.4	161
4M405	436	3.2	160	2M420	562	2.4	152	4M434	499	4.3	159
1M406	440	4.0	158	3M420	563	2.4	155	1M435	528	2.9	157
2M406	443	3.4	159	4M420	547	3.0	156	2M435	521	3.3	159
3M406	438	2.7	158	1M421	561	3.0	159	3M435	528	2.6	160
4M406	436	3.4	159	2M421	568	2.4	159	4M435	529	2.8	160
1M407	451	4.0	154	3M421	562	2.4	159	1M436	535	3.8	160
2M407	459	3.4	157	4M421	551	2.0	159	2M436	528	3.5	159
3M407	453	2.7	157	1M422	554	4.0	157	3M436	541	2.8	162
4M407	452	4.4	159	2M422	562	2.7	157	4M436	536	4.4	158
1M408	439	5.0	156	3M422	558	2.7	157	1M437	534	2.4	158
2M408	451	3.8	142(1)	4M422	538	3.3	154	2M437	523	4.2	161
3M408	454	4.1	149	1M423	554	4.0	159	3M437	534	2.8	160
4M408	449	6.3(1)	147	2M423	557	2.7	158	4M437	534	3.5	158
1M409	463	4.0	153	3M423	554	2.4	159	1M438	505	3.7	145(1)
2M409	466	3.4	152	4M423	540	1.7	159	2M438	534	3.7	161
3M409	461	3.8	154	1M424	538	4.0	153	3M438	524	3.3	156
4M409	457	5.4	152	2M424	546	2.4	154	4M438	523	4.2	157
1M410	466	4.0	152	3M424	546	3.1	156	1M439	536	6.0(1)	159
2M410	469	3.4	149	4M424	531	3.2	157	2M439	509	3.8	152
3M410	465	3.4	153	1M425	541	4.0	154	3M439	541	3.5	159
4M410	457	3.9	152	2M425	545	3.8	155	4M439	541	2.9	160
1M411	474	6.0(1)	138(1)	3M425	538	3.1	156	1M440	540	5.0	157
2M411	478	2.4	154	4M425	526	3.7	156	2M440	539	3.8	160
3M411	469	3.4	154	1M426	534	4.0	158	3M440	542	3.5	160
4M411	466	3.2	155	2M426	539	3.1	157	4M440	544	3.8	159
1M412	486	4.0	148	3M426	535	3.4	157	1M441	529	3.0	154
2M412	491	3.1	151	4M426	521	2.7	155	2M441	528	4.0	153
3M412	481	3.4	154	1M427	509	4.0	157	3M441	539	3.5	157
4M412	479	3.6	155	2M427	512	3.1	156	4M441	539	4.4	155
1M413	488	3.0	149	3M427	508	3.8	158	1M442	533	3.0	160
2M413	499	3.4	150	4M427	494	3.4	157	2M442	534	3.8	158
3M413	489	3.4	154	1M428	508	5.0	158	3M442	540	2.8	161
4M413	489	1.8	155	2M428	513	3.1	158	4M442	540	3.1	161
1M414	499	6.0(1)	138(1)	3M428	510	3.4	159	1M443	544	5.0	160
2M414	504	4.8	146(1)	4M428	496	4.1	158	2M443	548	3.5	161
3M414	497	4.1	151	1M429A	510	4.0	158	3M443	553	3.3	160
4M414	498	4.1	153	2M429A	515	3.1	158	4M443	551	1.9	162
1M415	524	3.0	156	3M429A	513	3.4	159	1M444	542	10.8(1)	162
2M415	531	2.7	158	4M429A	498	5.4	158	2M444	549	3.8	160

Rio Algom Mining Corp.

Smith Ranch Project

Table L-2.3

M Wells

Upper Control Limit Calculated

Well #	SC@25	Cl	Alkalinity	Well #	SC@25	Cl	Alkalinity	Well #	SC@25	Cl	Alkalinity
	µmho/cm	mg/L	mg/L		µmho/cm	mg/L	mg/L		µmho/cm	mg/L	mg/L
1M401	477	3.0	152	3M415	521	2.7	156	1M430	488	4.0	159
2M401	483	3.1	159	4M415	518	2.4	155	2M430	495	2.7	157
3M401	478	3.1	152	1M416	557	2.9	155	3M430	490	3.1	159
4M401	476	2.8	151	2M416	556	2.4	157	4M430	476	3.5	158
1M402	455	4.0	156	3M416	542	3.1	157	1M431	427	4.0	147(1)
2M402	454	3.4	155	4M416	540	1.8	157	2M431	455	3.1	130(1)
3M402	449	3.4	156	1M417	553	8.0(*)	148	3M431	470	3.8	142(1)
4M402	448	3.5	157	2M417	559	5.1	149	4M431	456	3.9	148
1M403	431	5.0	152	3M417	547	4.5	154	1M432	498	4.0	157
2M403	441	4.1	156	4M417	544	2.2	153	2M432	500	2.7	157
3M403	434	4.1	155	1M418A	533	5.0	148	3M432	497	3.8	156
4M403	431	3.8	153	2M418A	557	3.1	152	4M432	490	3.9	157
1M404	438	5.0	160	3M418A	554	3.4	151	1M433	517	4.0	160
2M404	440	2.7	161	4M418A	549	2.5	151	2M433	517	3.1	158
3M404	435	3.4	159	1M419	555	4.0	154	3M433	513	3.8	160
4M404	432	2.8	160	2M419	569	3.1	160	4M433	503	3.0	158
1M405	444	5.0	158	3M419	557	3.1	159	1M434	506	4.0	159
2M405	444	3.8	159	4M419	554	1.8	156	2M434	506	3.1	158
3M405	438	3.8	159	1M420	555	3.0	150	3M434	500	3.4	161
4M405	436	3.2	160	2M420	562	2.4	152	4M434	499	4.3	159
1M406	440	4.0	158	3M420	563	2.4	155	1M435	528	2.9	157
2M406	443	3.4	159	4M420	547	3.0	156	2M435	521	3.3	159
3M406	438	2.7	158	1M421	561	3.0	159	3M435	528	2.5	160
4M406	436	3.4	159	2M421	568	2.4	159	4M435	529	2.8	160
1M407	451	4.0	154	3M421	562	2.4	159	1M436	536	3.8	160
2M407	459	3.4	157	4M421	551	2.0	159	2M436	528	3.5	159
3M407	453	2.7	157	1M422	554	4.0	157	3M436	541	2.8	162
4M407	452	4.4	159	2M422	562	2.7	157	4M436	536	4.4	158
1M408	439	5.0	156	3M422	558	2.7	157	1M437	534	2.4	158
2M408	451	3.8	142(*)	4M422	538	3.3	154	2M437	523	4.2	161
3M408	454	4.1	149	1M423	554	4.0	159	3M437	534	2.8	160
4M408	449	6.3(1)	147	2M423	557	2.7	158	4M437	534	3.5	158
1M409	463	4.0	153	3M423	554	2.4	159	1M438	505	3.7	145(1)
2M409	466	3.4	152	4M423	540	1.7	156	2M438	534	3.7	161
3M409	461	3.8	154	1M424	538	4.0	153	3M438	524	3.3	159
4M409	457	5.4	152	2M424	546	2.4	154	4M438	523	4.2	167
1M410	466	4.0	152	3M424	546	3.1	156	1M439	536	6.3(1)	159
2M410	469	3.4	149	4M424	531	3.2	157	2M439	509	3.8	162
3M410	465	3.4	153	1M425	541	4.0	154	3M439	541	3.5	164
4M410	457	3.9	152	2M425	545	3.8	155	4M439	541	2.9	160
1M411	474	6.0(1)	138(1)	3M425	538	3.1	156	1M440	540	5.0	157
2M411	478	2.4	154	4M425	526	3.7	156	2M440	539	3.8	160
3M411	469	3.4	154	1M426	534	4.0	158	3M440	542	3.5	160
4M411	466	3.2	155	2M426	539	3.1	157	4M440	544	3.8	159
1M412	466	4.0	148	3M426	535	3.4	157	1M441	529	3.8	164
2M412	491	3.1	151	4M426	521	2.7	155	2M441	528	4.0	153
3M412	481	3.4	154	1M427	509	4.0	157	3M441	539	3.5	157
4M412	479	3.5	155	2M427	512	3.1	156	4M441	549	4.4	156
1M413	488	3.0	149	3M427	508	3.8	158	1M442	543	3.0	160
2M413	499	3.4	150	4M427	494	3.4	157	2M442	544	3.4	168
3M413	489	3.4	154	1M428	508	5.0	158	3M442	540	2.8	161
4M413	489	1.8	155	2M428	513	3.1	155	4M442	543	3.1	161
1M414	499	6.3(1)	138(1)	3M428	510	3.4	159	1M443	544	5.0	160
2M414	504	4.8	146(1)	4M428	496	4.1	158	2M443	548	3.5	161
3M414	497	4.1	151	1M429A	519	4.0	158	3M443	553	3.3	160
4M414	498	4.1	153	2M429A	515	3.1	158	4M443	551	1.9	167
1M415	524	3.8	156	3M429A	513	3.4	159	1M444	542	6.0(1)	160
2M415	531	2.7	158	4M429A	498	6.4	156	2M444	549	2.8	160

Rio Algom Mining Corp.
Smith Ranch Project
Table L-2.3
M Wells
Upper Control Limit Calculated

3M444	555	3.8	162	3M458	468	3.1	160
4M444	554	4.0	161	4M458	468	2.3	161
1M445	535	6.8(1)	158				
2M445	543	3.0	158	Maximum	569	5.5	169
3M445	550	3.7	156	Minimum	427	1.4	147
4M445	551	<1.0(1)	159	Count	232	220	224
1M446	544	3.5	161	K Factor	2.810	2.800	2.798
2M446	538	2.6	163	St. Dev.	37	0.8	4
3M446	544	3.5	161	K*St. Dev.	104	2.2	11
4M446	545	1.7	162	Mean	508	3.5	158
1M447	533	4.8	160	Upper Tol.	612	5.7	169
2M447	529	3.8	156	Lower Tol.	404	1.3	147
3M447	538	3.4	162				
4M447	534	4.3	164	Mean + 5 St. Dev.	693	7.5	178
1M448	530	4.8	161	15 mg/L + Mean	N/A	18.5	N/A
2M448	525	3.3	162	UCL	693	18.5	178
3M448	532	3.5	162				
4M448	531	7.4(1)	163				
1M449	522	1.9	158				
2M449	517	3.1	163				
3M449	523	3.5	163				
4M449	520	6.6(1)	164				
1M450	528	5.1	167				
2M450	524	3.8	168				
3M450	530	3.7	167				
4M450	532	6.9(1)	169				
1M451	517	4.7	158				
2M451	512	3.5	162				
3M451	519	3.7	162				
4M451	517	5.5	162				
1M452	510	3.4	161				
2M452	505	3.8	163				
3M452	510	4.0	160				
4M452	510	5.5	164				
1M453	499	4.0	161				
2M453	495	3.5	162				
3M453	502	2.4	162				
4M453	499	4.1	164				
1M454	470	4.6	161				
2M454	485	3.7	164				
3M454	492	3.3	161				
4M454	491	6.9(1)	162				
1M455A	476	5.2	162				
2M455A	473	3.5	163				
3M455A	480	2.9	162				
4M455A	480	2.7	163				
1M456	490	5.4	162				
2M456	468	3.1	164				
3M456	471	3.6	161				
4M456	472	3.2	161				
1M457	462	4.1	161				
2M457	459	3.3	160				
3M457	466	3.3	160				
4M457	464	4.0	162				
1M458	464	5.0	159				
2M458	464	3.3	160				

(1) - Outlier

Rio Algom Mining Corp.

Smith Ranch Project

Table L-2.3

M Wells

Upper Control Limit Calculated

Well #	SC@25	Cl	Alkalinity	Well #	SC@25	Cl	Alkalinity
	µmho/cm	mg/L	mg/L		µmho/cm	mg/L	mg/L
3M444	555	3.8	162	3M458	468	3.1	160
4M444	554	4.0	161	4M458	468	2.3	161
1M445	535	6.8(*)	158				
2M445	543	3.0	158	Maximum	569	5.5	169
3M445	550	3.7	156	Minimum	427	1.4	147
4M445	551	<1.0(*)	159	Count	232	220	224
1M446	544	3.5	161	K Factor	2.810	2.800	2.798
2M446	538	2.6	163	St Dev	37	0.8	4
3M446	544	3.5	161	K*St Dev	104	2.2	11
4M446	545	1.7	162	Mean	508	3.5	158
1M447	533	4.8	160	Upper Tol	612	5.7	169
2M447	529	3.8	156	Lower Tol	404	1.3	147
3M447	538	3.4	162				
				Mean + 5			
4M447	534	4.3	164	St Dev	693	7.5	178
				1.5 mg/L +			
1M448	530	4.3	161	Mean	N/A	18.5	N/A
2M448	525	3.3	162	UCI	693	18.5	178
3M448	532	3.5	162				
4M448	531	7.4(*)	163				
1M449	522	1.9	158				
2M449	517	3.1	163				
3M449	523	3.5	163				
4M449	520	6.3(1)	164				
1M450	528	5.1	167				
2M450	524	3.8	168				
3M450	530	3.7	167				
4M450	532	6.3(1)	169				
1M451	517	4.7	158				
2M451	512	3.5	162				
3M451	519	3.7	162				
4M451	517	5.5	162				
1M452	510	3.4	161				
2M452	505	3.8	163				
3M452	510	4.0	160				
4M452	510	5.5	164				
1M453	499	4.0	161				
2M453	495	3.5	162				
3M453	502	2.4	162				
4M453	499	4.1	164				
1M454	470	4.5	161				
2M454	485	3.7	164				
3M454	492	3.3	161				
4M454	491	6.3(1)	162				
1M455A	470	5.2	162				
2M455A	473	3.5	163				
3M455A	480	2.9	162				
4M455A	460	2.7	163				
1M456	490	5.4	162				
2M456	468	3.1	164				
3M456	471	3.6	161				
4M456	472	3.2	161				
1M457	462	4.1	161				
2M457	450	3.3	160				
3M457	406	3.3	161				
4M457	464	4.0	162				
1M458	484	5.0	160				
2M458	464	3.3	160				

(*) - Outlier

Rio Algom Mining Corp.

Smith Ranch Project

Wellfields 4 and 4A

Table L-3.1

MS Wells

Well#	Date and Time Sampled	Ca mg/L	Mg mg/L	Na mg/L	K mg/L	CO3 mg/L	HCO3 mg/L	SO4 mg/L	Cl mg/L	NH4 mg/L	NO3+NO2 mg/L	F mg/L	SiO2 mg/L	TDS mg/L	SC@25 µmho/cm	Alkalinity mg/L	pH std.units	As mg/L	B mg/L	Cd mg/L	Cr mg/L	Fe mg/L	Mn mg/L	Mo mg/L	Se mg/L	V mg/L	Zn mg/L	Unat mg/L	Ra226 pCi/L	Ra228 pCi/L
1MS416	2/24/2000@1122	67.6	16.7	24.9	7.5	<1.0	192	138	3.0	<0.05	<0.10	0.62	16.9	359	557	158	7.56	0.004	<0.10	<0.005	<0.05	<0.05	0.03	<0.10	<0.001	<0.10	<0.01	0.010	2.8	1.9
2MS416	3/9/2000@1407	N/R	N/R	N/R	N/R	N/R	N/R	138	3.1	N/R	N/R	N/R	N/R	385	564	159	7.53	0.005	N/R	N/R	N/R	N/R	N/R	N/R	<0.001	N/R	N/R	0.0097	5.7	3.8
3MS416	3/21/2000@846	N/R	N/R	N/R	N/R	N/R	N/R	140	3.3	N/R	N/R	N/R	N/R	392	574	159	7.51	0.004	N/R	N/R	N/R	N/R	N/R	N/R	<0.001	N/R	N/R	0.0104	4.9	1.7
4MS416	4/4/2000@1110	69.2	17.4	26.4	8.2	N/R	192	130	4.4	N/R	N/R	0.62	16.3	383	568	158	7.40	0.005	N/R	N/R	N/R	N/R	0.03	N/R	<0.001	N/R	N/R	0.011	4.1	2.1
1MS417	2/24/2000@1101	68.5	16.9	24.5	7.6	<1.0	195	140	3.0	<0.05	<0.10	0.64	17.0	363	563	160	7.57	0.001	<0.10	<0.005	<0.05	<0.05	0.03	<0.10	<0.001	<0.10	<0.01	0.018	5.3	3.1
2MS417	3/9/2000@1340	N/R	N/R	N/R	N/R	N/R	N/R	139	3.8	N/R	N/R	N/R	N/R	396	569	161	7.56	0.001	N/R	N/R	N/R	N/R	N/R	N/R	<0.001	N/R	N/R	0.0098	2.7	4.7
3MS417	3/21/2000@820	N/R	N/R	N/R	N/R	N/R	N/R	140	3.5	N/R	N/R	N/R	N/R	395	526	161	7.47	0.001	N/R	N/R	N/R	N/R	N/R	N/R	<0.001	N/R	N/R	0.0098	5.8	7.2
4MS417	4/4/2000@1228	71.5	17.7	26.4	0.3	N/R	195	131	5.3	N/R	N/R	0.62	16.7	383	577	161	7.44	0.001	N/R	N/R	N/R	N/R	0.04	N/R	<0.001	N/R	N/R	0.0112	5.5	7.5

(1) - Outlier For Cl, SC@25, or Alkalinity

Rio Algom Mining Corp.

Smith Ranch Project

Wellfields 4 and 4A

Table L-3.2

MS Wells

Parameter	Units	Mean	Five Std. Dev.	Mean + 5 Std. Dev.	Adjustment	Upper Control Limit
Chloride	mg/L	3.4	6.5	9.9	15	18.4
Total Alkalinity	mg/L	158	15	173	N/A	173
Specific Conductivity	umhos/cm	543	90	633	N/A	633

Rio Algom Mining Corp.

Smith Ranch Project

Wellfields 4 and 4A

Table L-3.3

MS Wells

Upper Control Limits Calculated

Well #	SC@25 umoh/cm	Chloride mg/L	Alkalinity mg/L	Well #	SC@25 umoh/cm	Chloride mg/L	Alkalinity mg/L
1MS401	556	4.0	158	4MS413	561	3.4	160
2MS401	551	3.4	159	1MS414	563	3.5	158
3MS401	548	2.4	159	2MS414	554	2.4	159
4MS401	549	2.5	157	3MS414	564	3.1	160
1MS402	544	3.0	159	4MS414	570	2.3	159
2MS402	546	2.7	161	1MS415	561	3.0	159
3MS402	537	2.7	161	2MS415	563	3.3	160
4MS402	548	3.7	160	3MS415	571	3.3	158
1MS403	528	2.0	149	4MS415	571	6.9	160
2MS403	531	1.7	154	1MS416	557	3.0	158
3MS403	527	2.1	154	2MS416	564	3.1	159
4MS403	536	1.0	158	3MS416	574	3.3	159
1MS404	527	5.0	139(1)	4MS416	568	4.4	158
2MS404	535	3.1	150	1MS417	563	3.0	160
3MS404	529	2.7	155	2MS417	569	3.8	161
4MS404	536	2.7	160	3MS417	526	3.5	161
1MS405	527	2.8	156	4MS417	577	5.3	161
2MS405	531	3.1	159				
3MS405	524	3.8	156	Maximum	577	6.9	162
4MS405	532	1.4	158	Minimum	511	1.0	149
1MS406	532	6.0	157	Count	60	58	59
2MS406	533	3.8	159	K Factor	3.066	3.077	3.072
3MS406	521	4.1	158	St. Dev.	18	1.3	3
4MS406	525	3.6	159	K*St. Dev.	55	4.0	9
1MS407	515	6.0	155	Mean	543	3.4	158
2MS407	519	5.8	157	Up. Tol.	598	7.4	167
3MS407	515	4.8	156	Low. Tol.	488	-0.6	149
4MS407	511	3.9	157				
1MS408	534	10.0(1)	154	Mean + 5 St. Dev.	633	9.9	173
2MS408	533	8.9(1)	154	15 mg/L + Mean		18.4	
3MS408	523	6.5	156	UCL	633	18.4	173
4MS408	524	5.1	156				
1MS409	523	3.0	159				
2MS409	525	2.4	159				
3MS409	518	3.1	159				
4MS409	524	1.7	160				
1MS412	556	1.6	159				
2MS412	550	2.4	162				
3MS412	558	3.1	161				
4MS412	556	5.7	159				
1MS413	557	2.9	159				
2MS413	553	2.1	160				
3MS413	563	2.8	161				

(1) - Outlier

Rio Algom Mining Corp.

Smith Ranch Project

Wellfields 4 and 4A

Table L-4.1

MD Wells

1MD414	2/24/2000@1519	54.1	16.3	30.0	8.6	<1.0	190	112.0	6.5(1)	0.14	<0.10	0.49	13.7	306	521	156	7.71	<0.001	<0.10	<0.005	<0.05	<0.05	0.02	<0.10	<0.001	<0.10	<0.01	0.001	4.2	2.9
2MD414	3/10/2000@1113	N/A	N/A	N/A	N/A	N/A	N/A	106.0	3.6	N/A	N/A	N/A	N/A	319	507	159	7.72	<.001	N/A	N/A	N/A	N/A	N/A	N/A	<0.001	N/A	N/A	0.0006	4.1	<1.0
3MD414	3/22/2000@836	N/A	N/A	N/A	N/A	N/A	N/A	109.0	3.5	N/A	N/A	N/A	N/A	316	519	159	7.56	<0.001	N/A	N/A	N/A	N/A	N/A	N/A	<0.001	N/A	N/A	0.0008	2.9	<1.0
4MD414	4/4/2000@1425	54.7	17.2	30.6	8.3	N/A	192	103.0	5.5	N/A	N/A	0.51	13.6	333	522	158	7.54	<0.001	N/A	N/A	N/A	N/A	0.02	N/A	<0.001	N/A	N/A	<0.0003	7.5	<1.0
1MD415	2/24/2000@1357	52.7	16.1	28.8	8.2	<1.0	192	107.0	4.4	0.15	<0.10	0.53	14.1	313	522	158	7.72	<0.001	<0.10	<0.005	<0.05	<0.05	0.02	<0.10	<0.001	<0.10	<0.01	0.0009	11.2	<1.0
2MD415	3/9/00@1512	N/A	N/A	N/A	N/A	N/A	N/A	107.0	4.2	N/A	N/A	N/A	N/A	323	515	159	7.70	<0.001	N/A	N/A	N/A	N/A	N/A	N/A	<0.001	N/A	N/A	<0.0003	5.2	1.5
3MD415	3/21/2000@1134	N/A	N/A	N/A	N/A	N/A	N/A	110.0	4.3	N/A	N/A	N/A	N/A	335	521	159	7.55	<0.001	N/A	N/A	N/A	N/A	N/A	N/A	<0.001	N/A	N/A	<0.0003	10.7	<1.0
4MD415	4/4/2000@1206	54.5	17.0	30.3	8.4	N/A	193	103.0	4.1	N/A	N/A	0.52	13.7	332	524	159	7.54	<0.001	N/A	N/A	N/A	N/A	N/A	N/A	<0.001	N/A	N/A	<0.0003	2.5	<1.0
1MD416	2/24/2000@1200	52.6	15.1	28.4	7.4	<1.0	193	107.0	4.3	0.15	<0.10	0.50	13.8	308	518	159	7.79	<0.001	<0.10	<0.005	<0.05	<0.05	0.01	<0.10	<0.001	<0.10	<0.01	0.0004	6.5	<1.0
2MD416	3/9/2000@1452	N/A	N/A	N/A	N/A	N/A	N/A	105.0	3.8	N/A	N/A	N/A	N/A	335	512	161	7.73	<0.001	N/A	N/A	N/A	N/A	N/A	N/A	<0.001	N/A	N/A	<0.0003	12.3	1.7
3MD416	3/21/2000@834	N/A	N/A	N/A	N/A	N/A	N/A	105.0	4.3	N/A	N/A	N/A	N/A	337	516	160	7.60	<0.001	N/A	N/A	N/A	N/A	N/A	N/A	<0.001	N/A	N/A	<0.0003	3.1	7.5
4MD416	4/4/2000@1157	55.0	16.7	30.4	7.9	N/A	195	98.5	1.9(1)	N/A	N/A	0.48	14.0	319	518	160	7.55	<0.001	N/A	N/A	N/A	N/A	0.02	N/A	<0.001	N/A	N/A	0.0006	14.4	4.1
1MD417	2/24/2000@1134	54.7	14.6	28.8	7.8	<1.0	194	104.0	4.7	0.11	<0.10	0.44	14.5	309	517	160	7.81	<0.001	<0.10	<0.005	<0.05	<0.05	<0.01	<0.10	<0.001	<0.10	<0.01	0.001	8.5	<1.0
2MD417	3/9/2000@1417	N/A	N/A	N/A	N/A	N/A	N/A	106.0	4.5	N/A	N/A	N/A	N/A	332	512	160	7.80	<0.001	N/A	N/A	N/A	N/A	N/A	N/A	<0.001	N/A	N/A	0.0003	2.8	<1.0
3MD417	3/21/2000@828	N/A	N/A	N/A	N/A	N/A	N/A	105.0	4.2	N/A	N/A	N/A	N/A	332	517	161	7.57	<0.001	N/A	N/A	N/A	N/A	N/A	N/A	<0.001	N/A	N/A	0.0004	19.5	1.4
4MD417	4/4/2000@1351	55.4	15.6	30.3	8.0	N/A	195	98.5	2.4(1)	N/A	N/A	0.43	14.1	322	520	161	7.63	<0.001	N/A	N/A	N/A	N/A	0.02	N/A	<0.001	N/A	N/A	0.0004	3.9	<1.0

(1) - Outlier For Cl, SC@25, or Alkalinity

Rio Algom Mining Corp.

Smith Ranch Project

Wellfields 4 and 4A

Table L-4.2

MD Wells

Parameter	Units	Mean	Five Std. Dev.	Mean + 5 Std. Dev.	Adjustment	Upper Control Limit
Chloride	mg/L	4.2	3.0	7.2	15	19.2
Total Alkalinity	mg/L	157	15	172	N/A	172
Specific Conductivity	umhos/cm	506	80	586	N/A	586

Rio Algom Mining Corp.

Smith Ranch Project

Wellfields 4 and 4A

Table L-4.3

MD Wells

Upper Control Limit Calculations

Well #	SC@25 umoh/cm	Chloride mg/L	Alkalinity mg/L	Well #	SC@25 umoh/cm	Chloride mg/L	Alkalinity mg/L
1MD401	491	4.0	152	1MD412	524	4.4	154
2MD401	490	3.4	152	2MD412	520	4.2	157
3MD401	491	4.1	154	3MD412	526	3.3	158
4MD401	495	3.4	155	4MD412	526	3.0	157
1MD402	486	5.0	153	1MD413	523	5.2	151
2MD402	494	3.4	157	2MD413	519	3.5	152
3MD402	487	4.5	155	3MD413	525	4.7	155
4MD402	495	4.1	157	4MD413	525	4.8	156
1MD403	488	6.0(1)	156	1MD414	521	6.5(1)	156
2MD403	496	4.8	157	2MD414	507	3.6	159
3MD403	490	3.8	157	3MD414	519	3.5	159
4MD403	498	3.9	158	4MD414	522	5.5	158
1MD404B	493	4.0	154	1MD415	522	4.4	158
2MD404B	498	3.8	157	2MD415	515	4.2	159
3MD404B	492	4.1	156	3MD415	521	4.3	159
4MD404B	501	3.4	158	4MD415	524	4.1	159
1MD405	499	4.0	159	1MD416	518	4.3	159
2MD405	500	4.5	163	2MD416	512	3.8	161
3MD405	491	4.8	160	3MD416	516	4.3	160
4MD405	496	3.8	160	4MD416	518	1.9(1)	160
1MD406	509	7.0(1)	140(1)	1MD417	517	4.7	160
2MD406	519	5.1	150	2MD417	512	4.5	160
3MD406	521	4.1	154	3MD417	517	4.2	161
4MD406	524	3.5	159	4MD417	520	2.4(1)	161
1MD407	495	7.0(1)	155				
2MD407	498	4.1	157	Maximum	530	5.5	163
3MD407	492	4.8	158	Minimum	462	3.0	148
4MD407	493	4.3	159	Count	68	60	66
1MD408	492	6.0(1)	158	K Factor	3.029	3.066	3.038
2MD408	494	5.1	160	St. Dev.	16	0.6	3
3MD408	484	5.1	158	K*St. Dev.	48	1.8	9
4MD408	490	4.4	160	Mean	506	4.2	157
1MD409	462	4.0	148	Up. Tol.	554	6.0	166
2MD409	479	4.8	156	Low. Tol.	458	2.4	148
3MD409	475	4.1	158				
4MD409	480	3.4	159	Mean + 5 St. Dev.	586	7.2	172
1MD410	524	8.3(1)	161	15 mg/L+mean		19.2	
2MD410	519	3.8	155	UCL	586	19.2	172
3MD410	521	4.1	151				
4MD410	521	4.4	153				
1MD411	528	4.7	160				
2MD411	520	4.5	142(1)				
3MD411	525	4.5	163				
4MD411	530	3.1	162				

(1) - Outlier